

# wireless world

NOVEMBER 1977 40p

## E.M. transceiver Distortion—no mystery

Bow Shockwave

Polar Cusp

Van Allen Belt

Radius of GEOS (6.7R<sub>E</sub>)  
Earth Radius = 6,378 km

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10 kHz

120 MHz



NEW

# The mi Signal Generator for vlf·lf·mf·hf·vhf bands

AM/FM Signal Generator TF 2016 is a general purpose instrument for receiver testing. Its facility for battery operation and its rugged construction make it ideal for field as well as factory use.

TF 2016 will deliver up to 4V e.m.f. and yet has a leakage level that is so low that even receivers with a sensitivity of 0.1  $\mu$ V can be tested without ambiguity. And the **total** output level accuracy of  $\pm 1$  dB ensures confidence every time.

Fundamental frequency generation is used over the entire frequency range thus ensuring the total absence of non-harmonics. The good tuning discrimination makes narrow band receiver testing quick and easy.

Amplitude modulation up to 100% modulation depth and frequency modulation up to 75 kHz deviation are available using the internal 400 Hz and 1 kHz oscillators. External modulation can be applied and, if required, internal a.m. and external f.m., or internal f.m.

and external a.m., can be applied simultaneously.

A version of TF 2016 will shortly be available equipped with a 150 Hz preset pilot tone f.m. for use on Clansman receivers.

Pulse Modulator, TF 2169, may be fitted to the signal generator to provide pulsed r.f. for radar i.f. testing. IF probes can be supplied to help tuning to receivers fitted with battery economizer circuits. Alternative output level calibration plates, matching pads, attenuators and r.f. fuse units are included in the wide range of optional accessories.

### Digital Synchronizer

The addition of this clip-on unit (as shown in our photograph) converts the TF 2016 into a synthesizer. It provides a stability of  $\pm 1$  part in  $10^6$  and allows the frequency to be set in 10 Hz steps.

Full information gladly supplied on request.

**mi MARCONI INSTRUMENTS**

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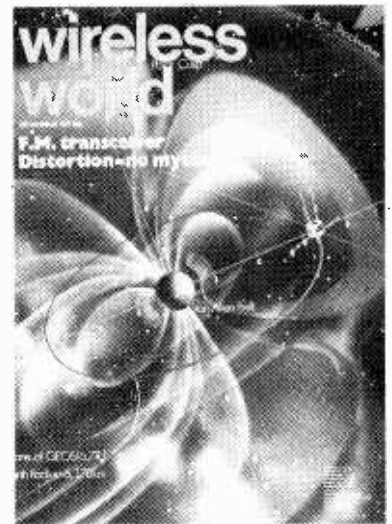
# wireless world

Electronics, Television, Radio, Audio

NOVEMBER 1977 Vol 83 No 1503

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Front cover is an imaginative painting by J. G. Dougherty, of the GEOS satellite in orbit, showing the natural phenomena it was designed to investigate. A report on GEOS appeared in the August issue, p.33. Picture by courtesy of British Aircraft Corporation.

## IN OUR NEXT ISSUE

**Telex decoder modifications.** An article describing the circuit changes and additions needed to enable the *Wireless World* decoder design to decode the latest control characters — graphics hold, double height, separated graphics and background colour.

Ernie Lowinger describes how to make a **thread-suspended pickup arm**, as expected to be shown this month on *Tomorrow's World*. This one doesn't need a lathe!

ISSN 0043 6062



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100pA to 100 $\mu$ A on 6 decade logarithmic scale.

Accuracy of current measurement  $\pm 15\%$  of indicated value.

Input voltage drop is approximately 20mV at 100pA, 200mV at 100nA and 400mV at 100 $\mu$ A.

Maximum safe continuous overload is 50mA.

##### MEASUREMENT TIME

$< 3$ s for resistance on all ranges relative to CAL position.

$< 10$ s for resistance of 10G  $\Omega$  across 1 $\mu$ F on 50V to 500V.

Discharge time to 1% is 0.1s per  $\mu$ F on CAL position.

##### RECORDER OUTPUT

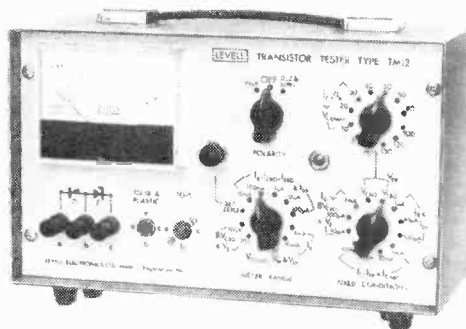
1V per decade  $\pm 2\%$  with zero output at scale centre.

Maximum output  $\pm 3$ V. Output resistance 1k  $\Omega$ .

type  
TM14

**£120**

#### TRANSISTOR TESTER



Tests bipolar transistors, diodes and zener diodes. Measures leakage down to 0.5 nA at 2V to 150V. Current gains are checked from 1 $\mu$ A to 100mA. Breakdown voltages up to 100V are measured at 10 $\mu$ A, 100 $\mu$ A and 1mA. Collector to emitter saturation voltage is measured at 1mA, 10mA, 30mA and 100mA for  $I_C/I_B$  ratios of 10, 20, 30. The instrument is powered by a 9V battery.

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$I_{CBO}$  &  $I_{EBO}$ : 10nA, 100nA, 1 $\mu$ A, 10 $\mu$ A and 100 $\mu$ A f.s.d. acc.  $\pm 2\%$  f.s.d.  $\pm 1\%$  at voltages of 2V, 5V, 10V, 20V, 30V, 40V, 50V, 60V, 80V, 100V, 120V, and 150V acc.  $\pm 3\%$   $\pm 100$ mV up to 10 $\mu$ A with fall at 100 $\mu$ A  $< 5\%$  + 250mV.

$BV_{CBO}$ : 10V or 100V f.s.d. acc.  $\pm 2\%$  f.s.d.  $\pm 1\%$  at currents of 10 $\mu$ A, 100 $\mu$ A and 1mA  $\pm 20\%$ .

$I_B$ : 10nA, 100nA, 1 $\mu$ A ... 10mA f.s.d. acc.  $\pm 2\%$  f.s.d.  $\pm 1\%$  at fixed  $I_E$  of 1 $\mu$ A, 10 $\mu$ A, 100 $\mu$ A, 1mA, 10mA, 30mA, and 100mA acc.  $\pm 1\%$ .

$h_{FE}$ : 3 inverse scales of 2000 to 100, 400 to 30 and 100 to 10 convert  $I_B$  into  $h_{FE}$  readings.

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$V_Z$ : Breakdown ranges as  $BV_{CBO}$  for transistors.

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# F.M. TUNERS, MODULES & KITS by

# Icon Design



This tuner must surely provide the best value for money available today. Combining the best of the modules shown below, it includes a full digital readout of frequency to a resolution of 0.1 MHz, so that exact station identification can be made. In addition, six pre-set stations may be selected by touch controls having internal solid state lamps, while manual tuning allows easy searching for distant stations under the guidance of the digital meter.

A switchable mute system allows reception of the weakest stations while muting inter-station noise and spurious responses. Perfect reception is assured by not permitting any station to be heard which is far enough out of tune to cause distortion. The tuning indicator lamp provides a means of very fine tuning, and is automatically extinguished between stations.

A powerful A.F.C. system is also incorporated which holds all stations in tune, while not preventing manual tuning.

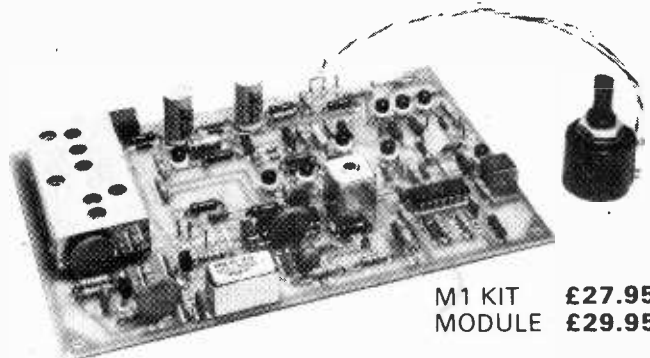
Good stereo reception is assured by the use of a phase locked decoder with full 'birdie' and spurious output filtering.

Finally, but not least, the external appearance and styling bring a fresh new look to Hi-Fi. The sturdy wooden cabinet is finished in mat teak veneer, housing an attractive gold and brown, anodised aluminium front panel, which carries black controls and inscriptions. The indicator lamps and digital displays are in red, giving the finishing touches to a tuner you will be proud to own.

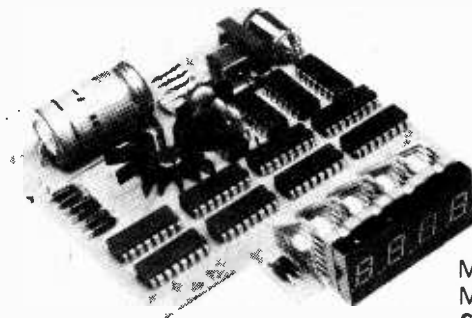
	<b>Tuner</b>	<b>Kit</b>
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T3 DIGITAL (AS SHOWN) .....	<b>£149.00</b>	<b>£139.00</b>

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M1 KIT **£27.95**  
MODULE **£29.95**



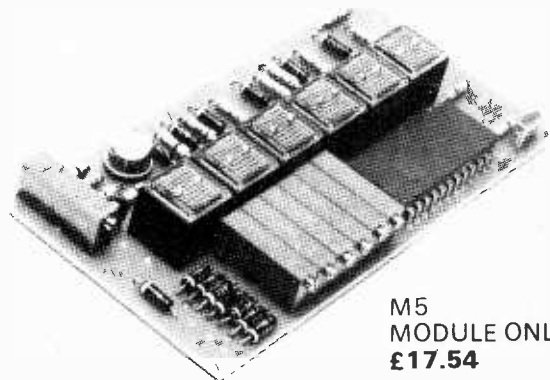
M6  
MODULE ONLY  
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## DIGITAL FREQUENCY METER M6

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M5  
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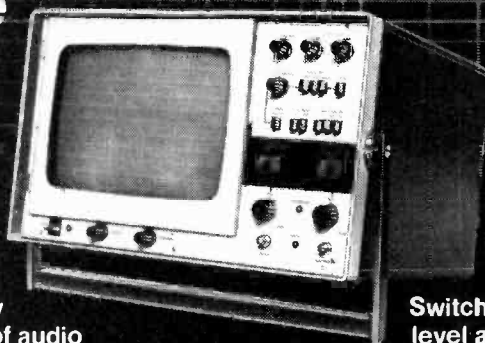
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That's not ladylike, I says. No, she says—impatient like—COSMOS! That does it—wash your mouth out or explain.

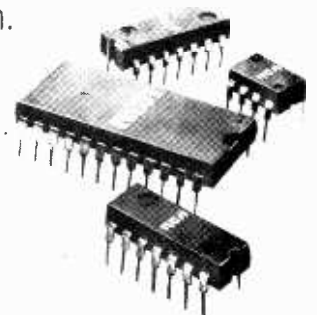
She does, and I've quoted it word for word below. If you understand it you're a better man than her.

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But the COSMOS 4000B series gates can be buffered or unbuffered. If you want unbuffered gates, you add 'U' to the code—e.g. 4011UB. If you specify nothing, you get buffered automatically—e.g. 4011B.

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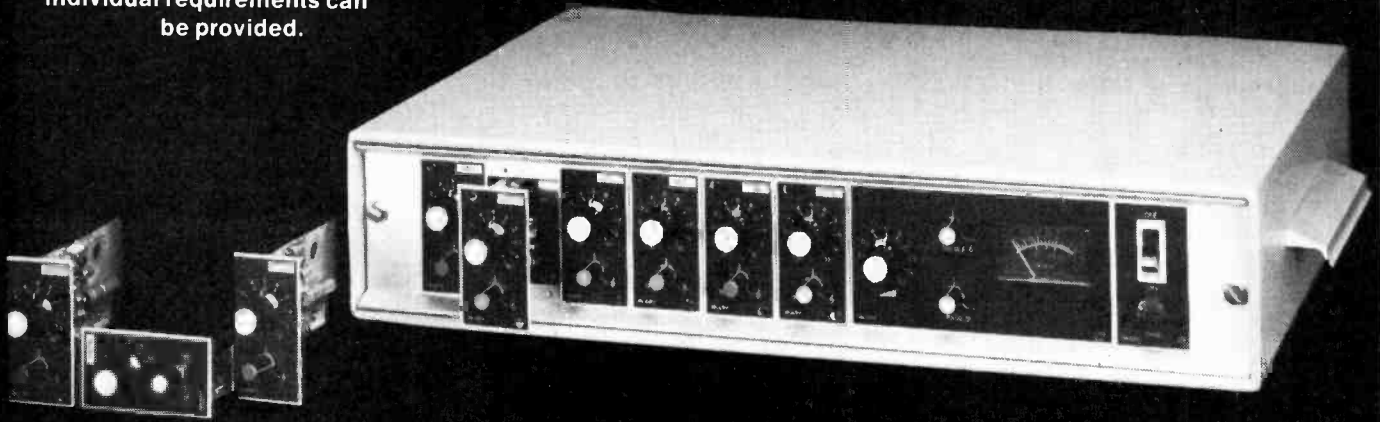
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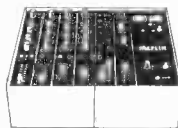
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# MAPLIN

in a modern world of electronics

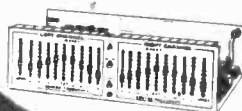
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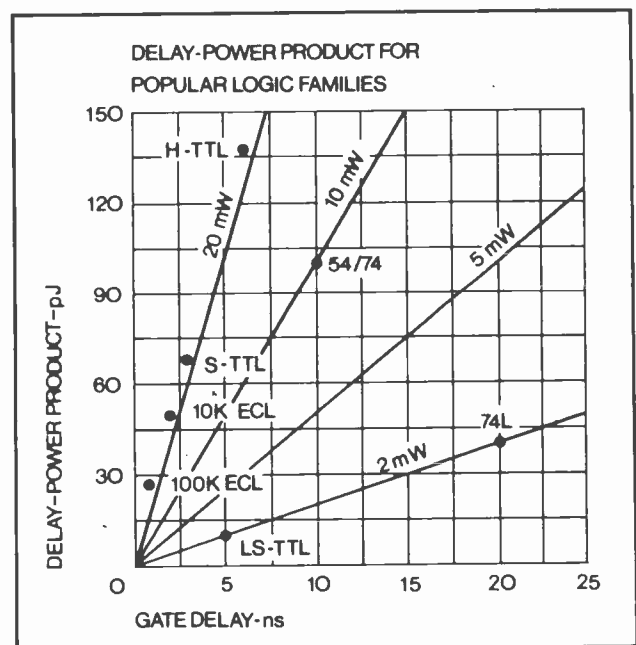
# Low Power Schottky TTL cuts down on everything. Except performance.

Motorola Low Power Schottky TTL cuts down on supply current and noise. As well as the size, cost and weight of equipment.

But it additionally offers far more than that. Now you don't have to choose between speed and power in performance terms. As the graph clearly shows, it dissipates eleven times less power than 74S, suffering a delay of only 1.7 times.

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Please send me full information on the Motorola Low Power Schottky TTL.

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WW/12/77



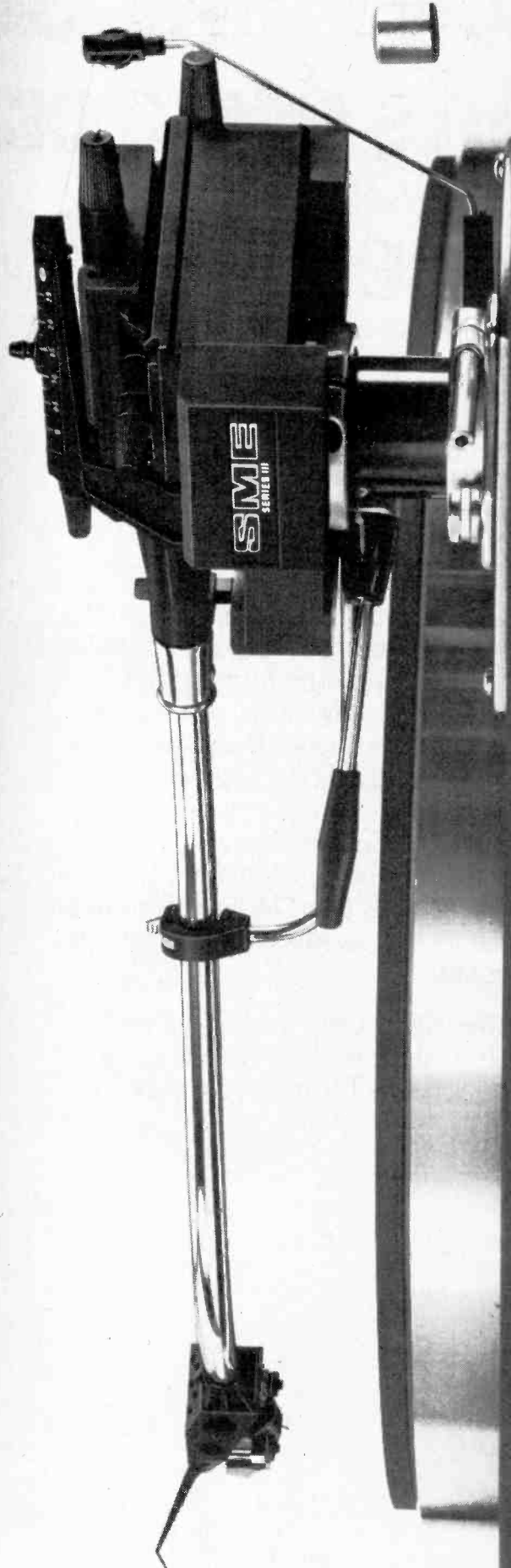
Crellon Electronics Ltd.,  
(incorporating ECS and GDS Sales)



WW — 065 FOR FURTHER DETAILS

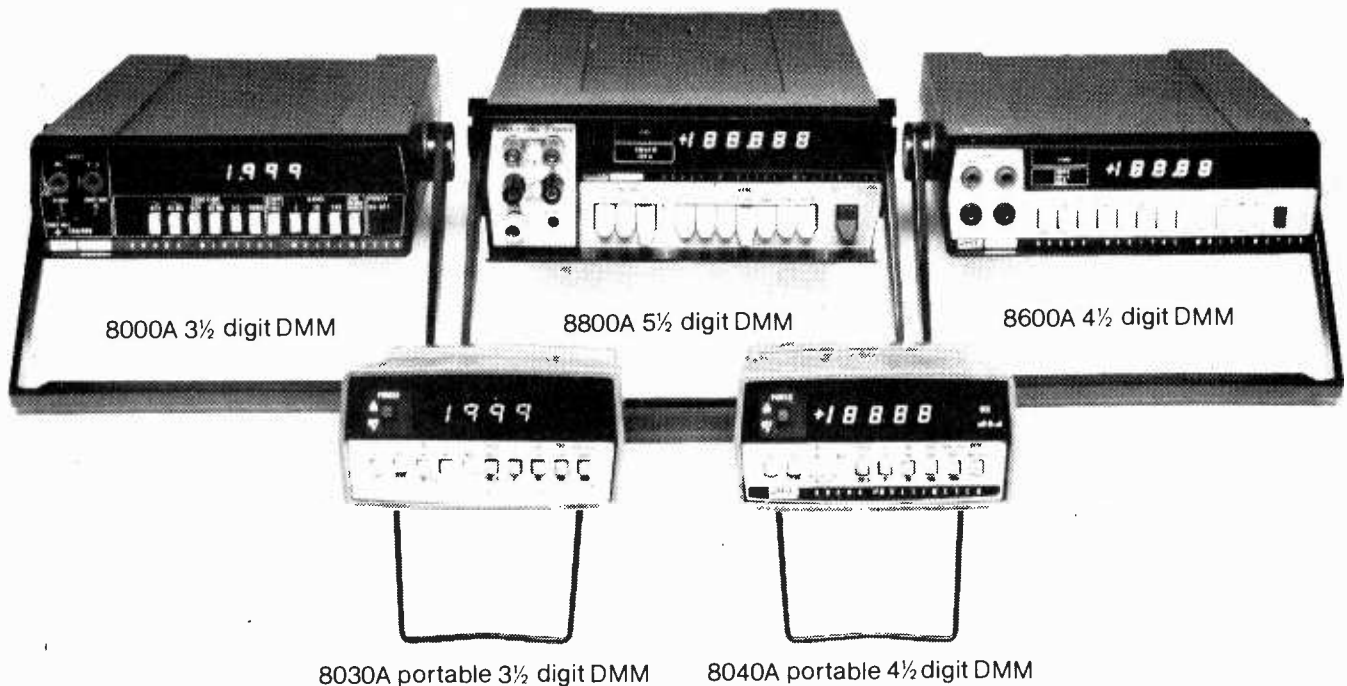
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ITT Electronic Services, Edinburgh Way, Harlow, Essex CM20 2DF

## Greenwood Electronics

Greenwood Electronics, Portman Road, Reading RG3 1NE  
Telephone: 0734-595844, Telex: 848659

\*Illustration actual size

WW-010 FOR FURTHER DETAILS

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### TITAN MINI KIT DRILL

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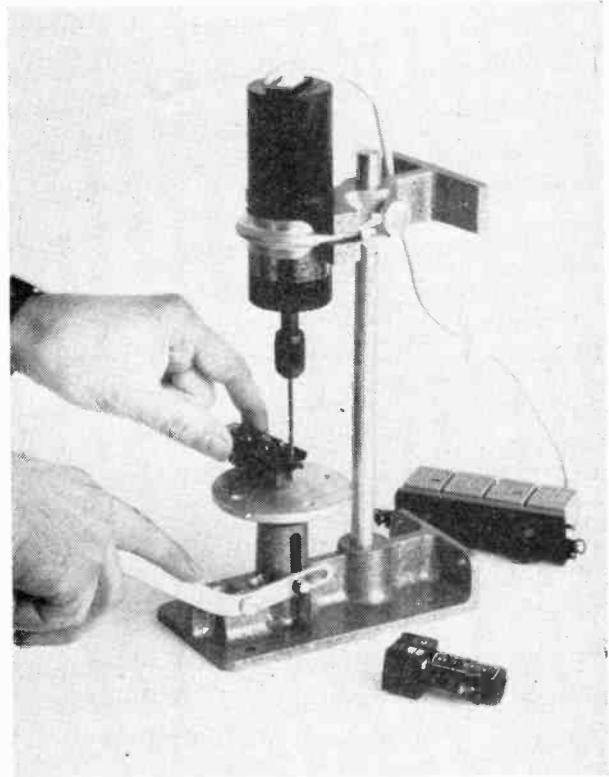
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These are examples of the extensive range of power tools designed to meet the needs of development engineers, laboratory workers, model makers and others requiring small precision production aids.

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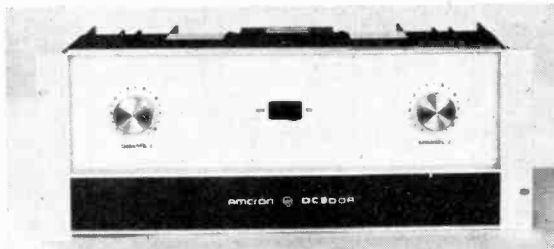


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WW-024 FOR FURTHER DETAILS

## HIGH POWER DC-COUPLED AMPLIFIER



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- ★ FULLY PROTECTED AGAINST SHORT CCT, MISMATCH, ETC.
- ★ 3 YEAR WARRANTY ON PARTS AND LABOUR

The DC300A Power Amplifier is the successor to the world famous DC300 which is so widely used in Industrial, and Research applications in this country. It is DC-coupled throughout so providing a power bandwidth from DC to over 20,000Hz. The ability of the DC300A to operate without fuss into totally reactive loads while delivering its full power, and maintaining its faithful reproduction of Pulse or complex waveforms has established the DC300A as the world's leading power amplifier. Each of the two channels will operate into loads as low as 1 ohm, and the amplifier can be rapidly connected as a single ended amplifier providing over 650 watts RMS into a 4 ohms load, and still providing a bandwidth down to DC. Below is a brief specification of the DC300A, but if you require a data sheet, or a demonstration of this fine equipment please let us know.

Power Bandwidth	DC-20kHz @ 150 watts + 1db. - 0db.	Slewing Rate	8 volts per microsecond
Power at clip point (1 chan)	500 watts rms into 2.5 ohms	Load impedance	1 ohm to infinity
Phase Response	+0. -15° DC to 20kHz. 1 watt 8Ω	Input sensitivity	1.75 V for 150 watts into 8Ω
Harmonic Distortion	Below 0.05% DC to 20kHz	Input Impedance	10K ohms to 100K ohms
Intermod. Distortion	Below 0.05% 0.01 watt to 150 watts	Protection	Short, mismatch & open cct. protection
Damping Factor	Greater than 200 DC to 1kHz at 8Ω	Power supply	120-256V. 50-400Hz
Hum & Noise (20-20kHz)	At least 110db below 150 watts	Dimensions	19" Rackmount, 7" High, 9 1/2" Deep
Other models in the range: D60 — 60 watts per channel		D150A — 150 watts per channel	

Other models available from 100 watts to 3000 watts



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WW-039 FOR FURTHER DETAILS



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**Photoelectric Switches**

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Plus **Proximity Switches**—A new range covering AC/DC types to DIN standards.

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**IMO. There's more to us than you may know.**

IMO Precision Controls Ltd, 349 Edgware Road,  
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# Something of interest if you're impressed with our relays.

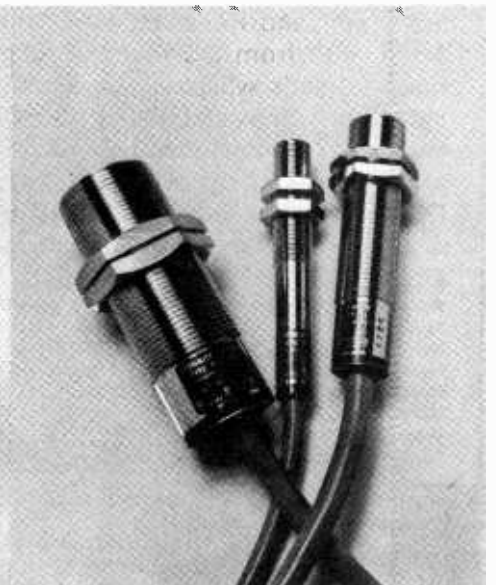
Limit Switches



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Proximity Switches



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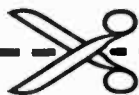
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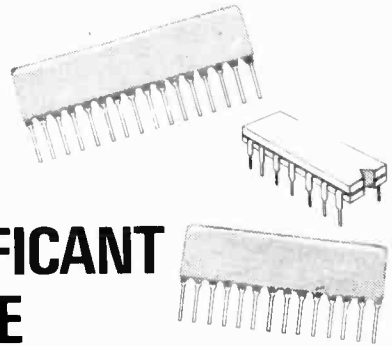
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WW-015 FOR FURTHER DETAILS

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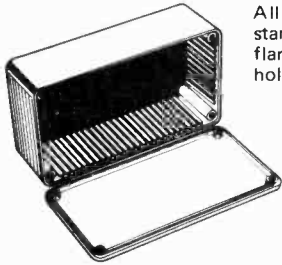
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RF power. We can deliver.



# BIMCONSOLES BIMBOXES BIMBOARDS BIMDRILLS BIMDICATORS

## ABS & DIECAST BIMBOXES

5 sizes, in either ABS or Diecast Aluminium ABS moulded in Orange, Blue, Grey or Black Diecast Aluminium available in Grey Hammettone or Natural



All boxes incorporate guides on all sides for holding 1.5mm thick pcb's and stand-off bosses in base for supporting small sub-assemblies etc. Close fitting flanged lids held by screws running into integral brass bushes (ABS) or tapped holes (Diecast).

	ABS	Diecast	Hammettone	Natural
(100x50x25mm)	BIM2002/12 £0.87*	BIM5002/12 £1.20*		£0.97*
(112x62x31mm)	BIM2003/13 £0.97*	BIM5003/13 £1.50*		£1.20*
(120x65x40mm)	BIM2004/14 £1.05*	BIM5004/14 £1.86*		£1.49*
(150x80x50mm)	BIM2005/15 £1.18*	BIM5005/15 £2.38*		£1.91*
(190x110x60mm)	BIM2006/16 £1.84*	BIM5006/16 £3.41*		£2.85*

Also available in Grey Polystyrene (112x61x31mm) with no slots and self tapping screws BIM2007/17 £0.82\*

## MINI DESK BIMCONSOLES

Moulded in Orange, Blue, Black or Grey ABS and incorporating guides on all sides for holding 1.5mm thick pcb's. 1mm Grey Aluminium panel sits recessed into front of console and held by screws running into integral brass bushes. Stand-off bosses in base for supporting small sub-assemblies etc. 4 self adhesive rubber feet also included.

BIM1005 (161x96x58mm) £1.97\*  
BIM1006 (215x130x75mm) £2.70\*



## LOW PROFILE BIMCONSOLES



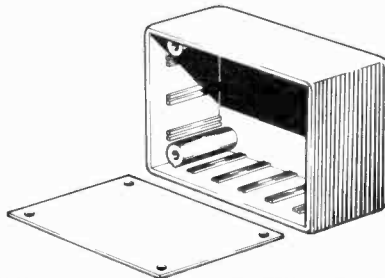
1mm Grey Aluminium panel sits recessed into front of console base, which is moulded in Orange, Blue, Black or Grey ABS and sits on 4 self adhesive rubber feet. Incorporating guides for holding 1.5mm thick pcb, the base also has stand-off bosses for supporting small sub-assemblies etc. and ventilation slots. Front panel is held by 4 screws which run into integral brass bushes.

BIM6005 (143x105x55.5[31.5] mm) £2.14\*  
BIM6006 (143x170x55.5[31.5] mm) £2.73\*  
BIM6007 (214x170x82[31.5] mm) £3.75\*

## MULTI-PURPOSE BIMBOXES

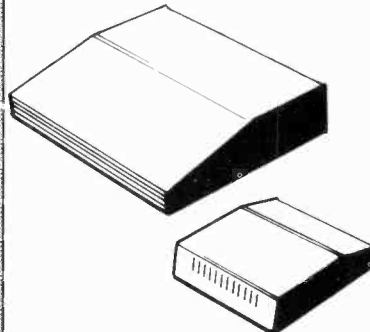
Moulded in Orange, Blue, Black or Grey ABS with 1mm thick Grey aluminium recessed front cover which is retained by 4 screws running into integral brass bushes. 1.5mm pcb guides are incorporated on all sides and as with all ABS boxes they are 85°C rated. 4 self adhesive rubber feet also included.

BIM 4003 (85x56x28.5mm) £1.13\*  
BIM 4004 (111x71x41.5mm) £1.42\*  
BIM 4005 (161x96x52.5mm) £1.87\*



All aluminium, 2 piece desk consoles with either 15° or 30° sloping fronts, sit on 4 self-adhesive non slip rubber feet. Ventilation slots in base and rear panels permit efficient cooling.

Colour Code	Top Panel	Base	15° Sloping Panel
A	Off White	Blue	BIM7151 (102x140x51[28] mm) £ 7.66*
B	Sand	Green	BIM7152 (165x140x51[28] mm) £ 8.51*
C	Satin Black	Gold	BIM7153 (165x216x51[28] mm) £ 9.35*



BIM7154 (165x211x76[33] mm) £10.21\*  
BIM7155 (254x211x76[33] mm) £11.05\*  
BIM7156 (254x287x76[33] mm) £11.92\*  
BIM7157 (356x211x76[33] mm) £12.76\*  
BIM7158 (356x287x76[33] mm) £13.60\*

### 30° Sloping Panel

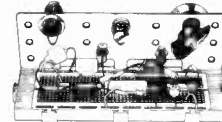
BIM7301 (102x140x76[28] mm) £ 7.66\*  
BIM7302 (165x140x76[28] mm) £ 8.51\*  
BIM7303 (165x183x102[28] mm) £ 9.35\*  
BIM7304 (254x140x76[28] mm) £10.21\*  
BIM7305 (254x183x102[28] mm) £11.05\*  
BIM7306 (254x259x102[28] mm) £11.92\*  
BIM7307 (356x183x102[28] mm) £12.76\*  
BIM7308 (356x259x102[28] mm) £13.60\*

## DIL COMPATIBLE BIMBOARDS

Bimboards accept all sizes of DIL packages as well as resistors, diodes, capacitors and LED's etc. They have integral Bus Strips running up each side for carrying Vcc and ground as well as Component Support Brackets for holding lamps, fuses and switches etc. Available as either single or multiple units, the latter mounted on 1.5mm thick, matt black aluminium back plates which stand on non slip rubber feet and have 4 screw terminals for incoming power.

Bimboard 1 contains 500 individual sockets whereas the multiple units containing 2, 3 or 4 Bimboards incorporate 1,100, 1,650 or 2,200 individual sockets, all arranged on a 2.5mm(0.1") matrix.

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Bimboard 3 £32.40\* Bimboard 4 £42.12\*



## BIMDICATORS

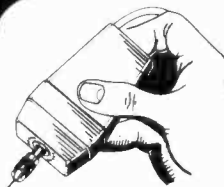


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# the impact of electronics

## A major international conference organised by Electronics Weekly.

**Hilton Hotel, Park Lane, London. Thursday, December 8th, 1977**

An opportunity to discover how developments in electronics will bring far-reaching changes to industry, commerce, leisure and society.

This major international conference is an attempt to create an awareness of what is happening in terms of the social and economic effects of the electronics revolution, which can only be minimised and turned to good account if all those concerned understand what is involved.

In a series of papers, leading figures in electronics from Britain and other countries will explain that while new technology may be disruptive, this can be lessened if long-term plans based on sound knowledge are made.

This conference can be your first step towards acquiring this knowledge—the key to choosing the right way ahead.

**Subjects and speakers will include:**

**The Impact of Electronics—Past, Present and Future**, by Jack Akerman (Managing Director of Mullard Ltd., Chairman of the Electronic Component Industry Federation, and member of Electronics EDC).

**The Impact of New Technology in Telecommunications**, by Kenneth Cortfield (Deputy Chairman and Managing Director of Standard Telephone and Cables Ltd., and Senior Officer of ITT in the United Kingdom).

**The Microprocessor in the Home**, by Dr Steve Forte (Managing Director of General Instrument Microelectronics Ltd since 1971 and has many years experience of the Semiconductor industry).

**The Microcomputer in Industry and Commerce**, by Alex d'Agapeyett, OBE, (Chairman of Computer Analysts and Programmers Ltd).

**The Impact of Microelectronics on Employment**, by Dr Alfred Prommer (Vice President of Siemens AG, West Germany, and head of sales and marketing in the company's components group).

Lord Orr-Ewing, OBE, C.Eng. (Chairman of Ultra Electronics Ltd); Sir Ieuan Maddock, CB, OBE, FRS (Deputy Chairman of the National Electronics Council) and Lord Thorneycroft (Chairman of Pye of Cambridge Ltd) have all agreed to chair the sessions.

The concluding **Open Forum** will feature a panel of experts which will include William C Hittinger (Executive Vice President, research and engineering, RCA Corporation USA); Gerrit Jeelof (Chairman and Managing Director of Philips Industries UK); Derek Roberts (Managing Director of Plessey Microsystems Division) and Frank Chorley (Managing Director, Plessey Electronic Systems Ltd).

The conference commences at 9.00am and closes at 5.30pm.

The fee is £60 plus 8% VAT (£4.80) per delegate.

To be sure of reserving your seat for this occasion please complete the form on right:



Kenneth Cortfield

Jack Akerman

Dr Steve Forte

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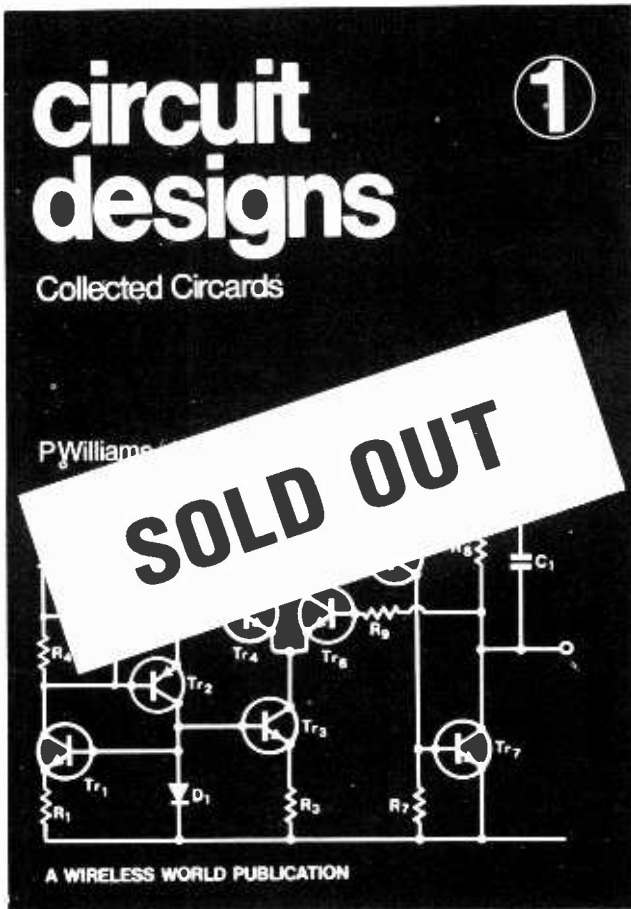
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# Two books from Wireless World

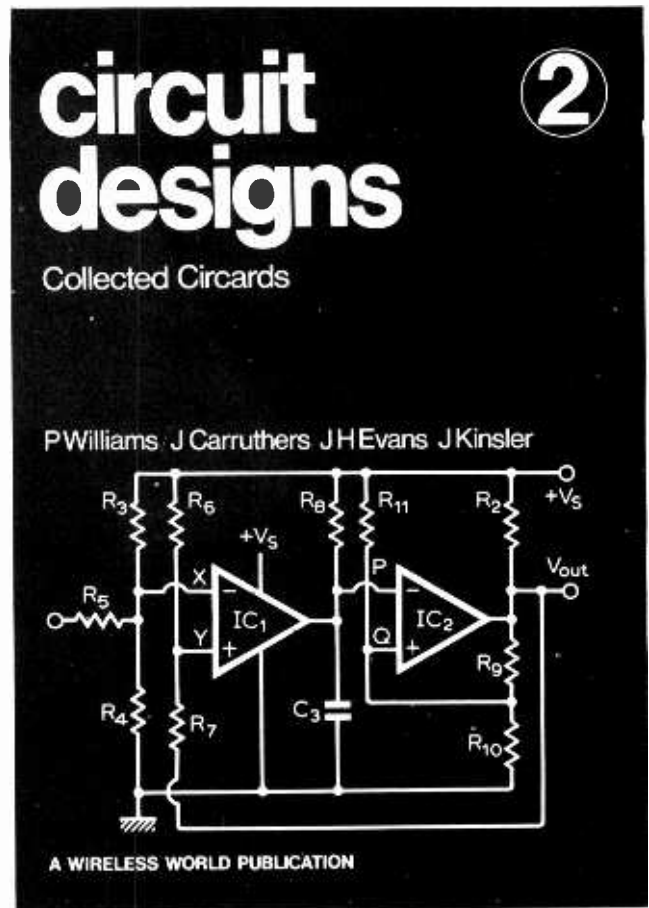
These books are of very special appeal to all concerned with designing, using and understanding electronic circuits. They comprise information previously included in Wireless World's highly successful

Circards – regularly published cards giving selected and tested circuits, descriptions of circuit operation, component values and ranges, circuit limitations, modifications, performance data and graphs. Each of these magazine-size hard cover books contains ten sets of Circards plus additional circuits and explanatory introduction.



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- Basic active filters
- Switching circuits
- Waveform generators
- AC measurements
- Audio circuits
- Constant-current circuits
- Power amplifiers
- Astable circuits
- Optoelectronics
- Micropower circuits



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- Wideband amplifiers
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All static memory with selected 2102 IC's allows processor to run at its maximum speed at all times. No refresh system is needed and no time is lost in memory refresh cycles. Each board holds 4,096 words of this proven reliable and trouble free memory. Cost—only £80.00 for each full 4K memory.

## INTERFACE—

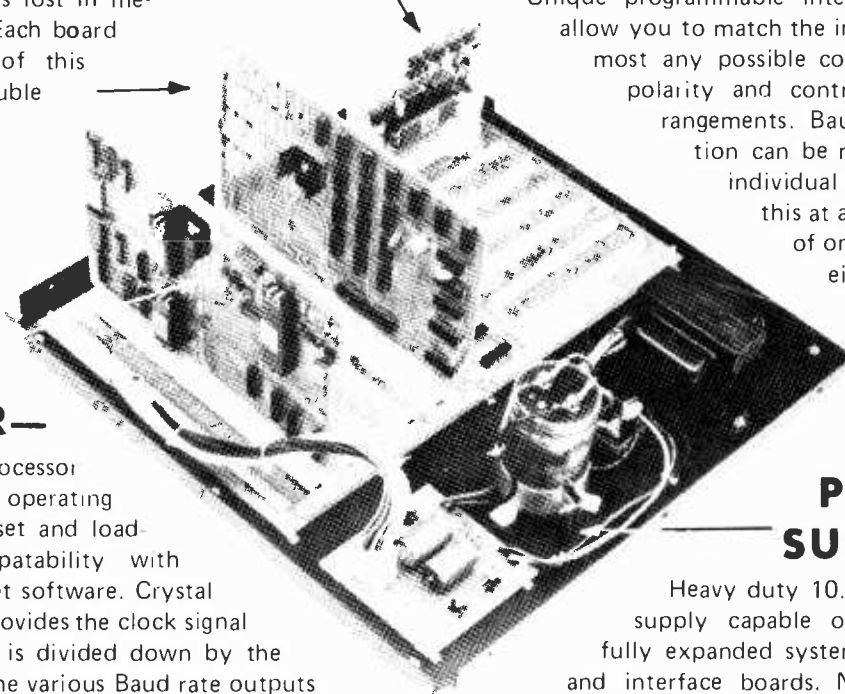
Serial control interface connects to any RS-232, or 20 Ma. TTY control terminal. Connectors provided for expansion of up to eight interfaces. Unique programmable interface circuits allow you to match the interface to almost any possible combination of polarity and control signal arrangements. Baud rate selection can be made on each individual interface. All this at a sensible cost of only £30.00 for either serial, or parallel type

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"Motorola" M6800 processor with Mikbug® ROM operating system. Automatic reset and loading, plus full compatibility with Motorola evaluation set software. Crystal controlled oscillator provides the clock signal for the processor and is divided down by the MC14411 to provide the various Baud rate outputs for the interface circuits. Full buffering on all data and address busses insures "glitch" free operation with full expansion of memory and interfaces.

## POWER SUPPLY—

Heavy duty 10.0 Amp power supply capable of powering a fully expanded system of memory and interface boards. Note 25 Amp rectifier bridge and 91,000 mfd computer grade filter capacitor.



## DOCUMENTATION—

Probably the most extensive and complete set of data available for any microprocessor system is supplied with our 6800 computer. This includes the Motorola programming manual, our own very complete assembly instructions, plus a notebook full of information that we have compiled on the system hardware and programming. This includes diagnostic programs, sample programs and even a Tic Tac Toe listing.

*Mikbug® is a registered trademark of Motorola Inc.*

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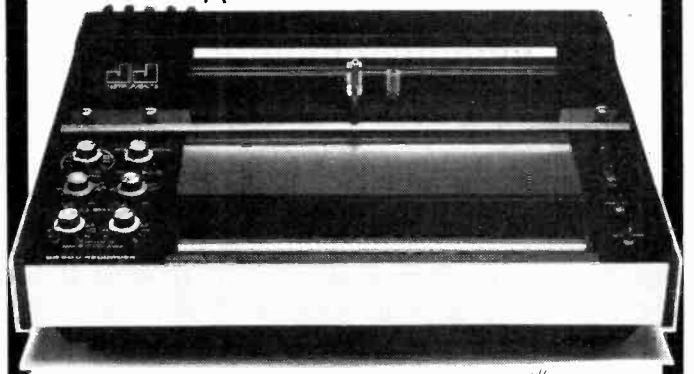
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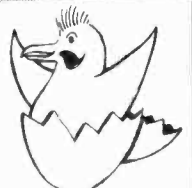
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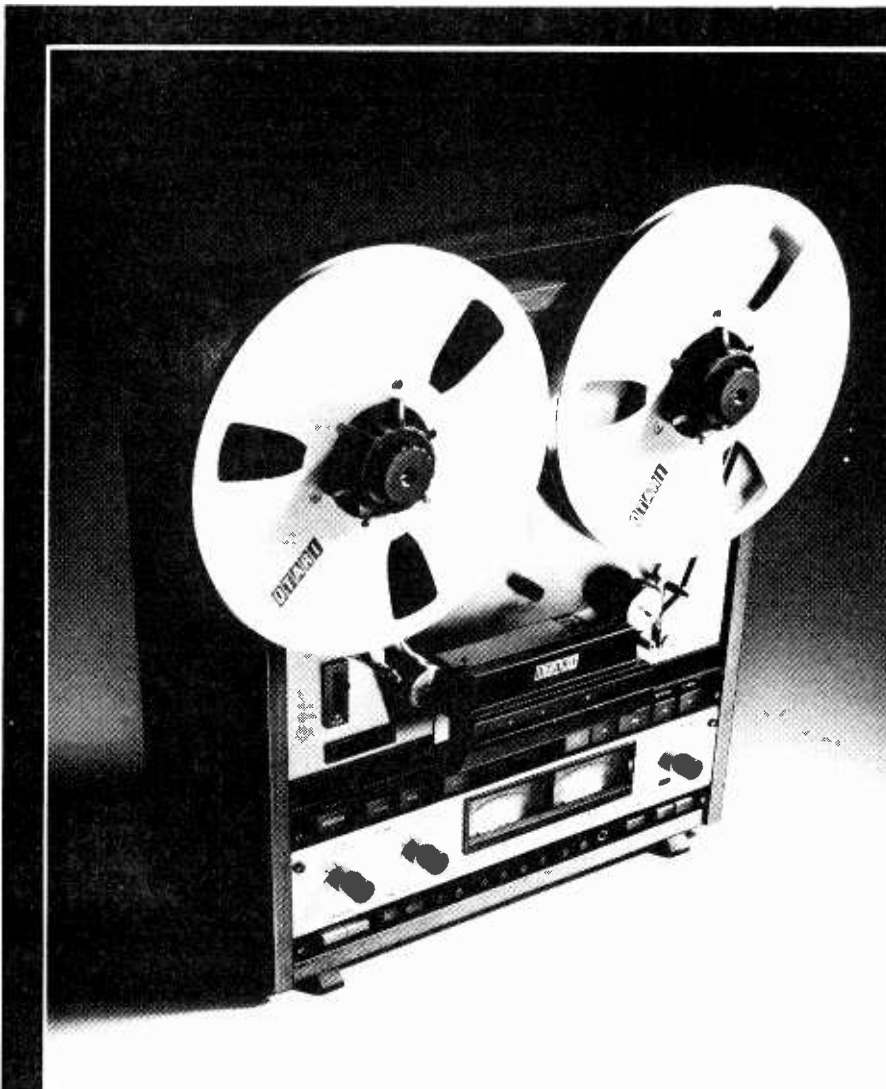


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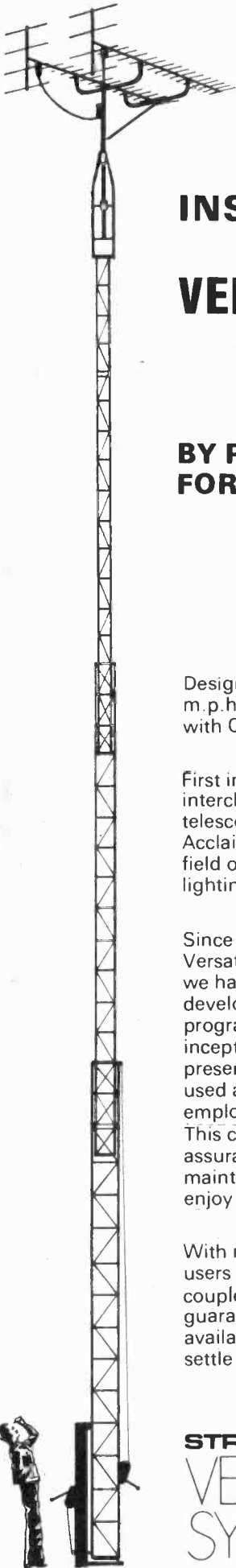
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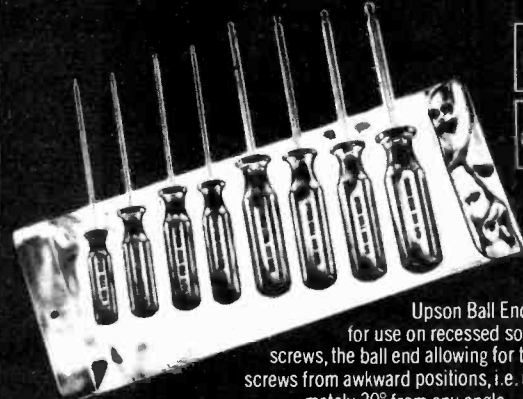
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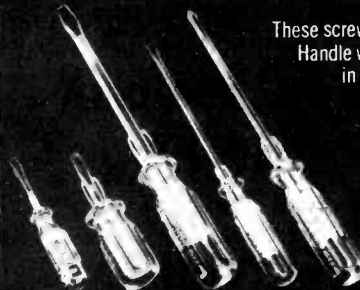
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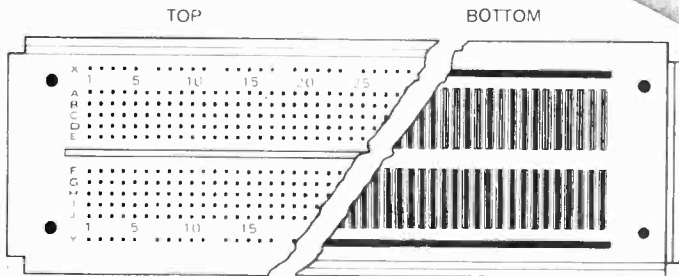
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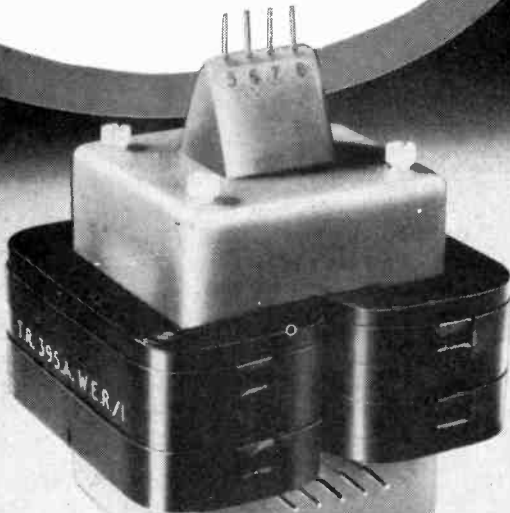
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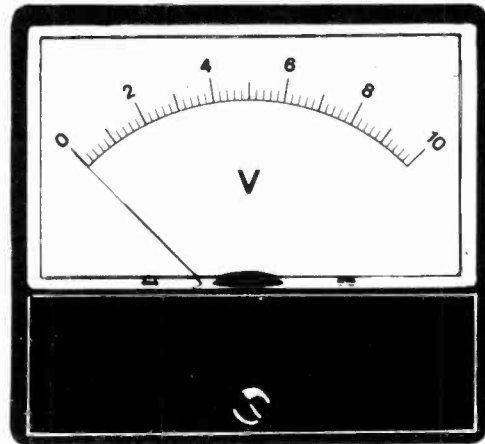
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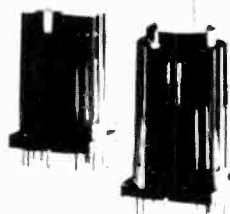
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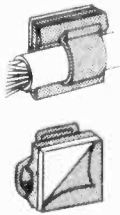
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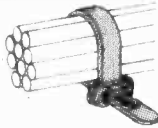
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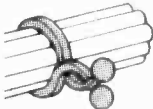


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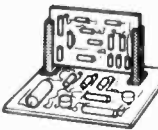
**CABLE STRAPS** are semi-permanent fasteners for strapping wires and cables into tight, compact looms. The ratchet fastener is adjustable and can be released by pinching-in the sides of the fastener head. Cable straps are made from black nylon.



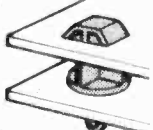
**WIRE TIES** are a flexible means of fastening wires and small cables into orderly, compact looms. They are quick and easy to fit and can be re-used, greatly reducing re-loomng times. Wire ties are made from nylon and are available in various sizes each determined by a different colour.



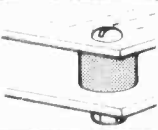
The **P.C. BOARD GUIDE** is a self-retaining edge support for printed circuit boards. It has good panel retention and grips p.c. boards firmly and securely. The guide is available in two types of material - yellow acetal or grey Noryl, for high temperature and voltage applications.



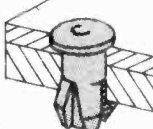
**P.C. BOARD SPACERS** are simple to fit, one-piece mouldings for use with p.c. boards. They have a self retaining shank for fastening into panels and a T-shaped anchor for securing p.c. boards of 0.062" thickness. They have good resistance to vibration and are suitable for board-to-board or board-to-chassis use.



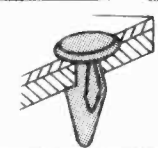
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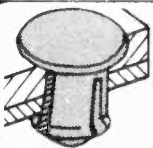
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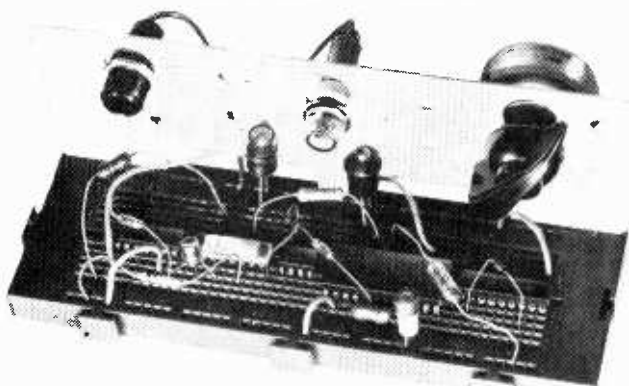
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# seen from the professional angle



the 201 is something  
quite personal...

The M 201 Hypercardioid moving coil microphone is designed for recording or broadcasting. The M 201 offers excellent separation characteristics in extreme accoustical conditions.

**Specifications:**

Frequency Response: 40-18000 Hz.  
Output Level at 1 kHz: 0,14 mV/μ bar  
± -56 dbm (0 dbm ± 1 mW/10  
dynes/cm<sup>2</sup>). EIA Sensitivity Rating:  
-149 dbm. Hum Pickup Level:  
5 μ V/5 μ Tesla (50 Hz). Polar Pattern:  
Hypercardioid. Output Impedance:  
200 Ω. Load Impedance: > 1000 Ω.  
Connections: M 201 N (C) = Cannon  
XLR-3-50 T or Switchcraft: 2+3 =  
200 Ω., 1 = ground. M 201 N = 3-pin  
DIN plug T 3262: 1+3 = 200 Ω  
2 = ground. M 201 N (6) = 6 pin  
Tuchel.  
Dimensions: length 6", shaft Ø 0,95".  
Weight: 8,60 oz.



**BEYER DYNAMIC (GB) LIMITED**

1 Clair Road, Haywards Heath, Sussex.  
Tel: Haywards Heath 51003

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# Peaks Transients

Our Unit Conquers

## The Allen and Heath Broadcast Feed Forward Delay Limiter.

The only limiter that makes it **IMPOSSIBLE** for a transient peak to pass through the unit, without the use of clipping devices. Included in its design is a revolutionary bucket brigade integrated circuit. This delays the main signal path by approximately one thousandth of a second. Thus gain reduction is fed forward before there is any increase in the programme level. The unit can be used with high powered equipment such as broadcast units and P.A. systems. Use it too in studios with effects units.

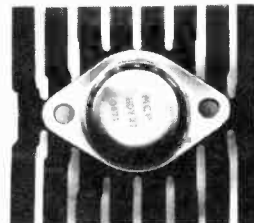
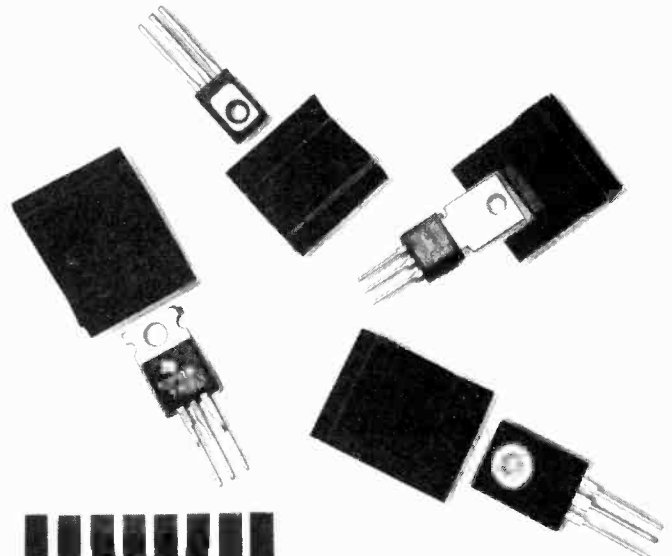
Try and test one at our demo. studio. Pembroke House, Campsbourne Road, Hornsey, London N8. Or, for more information, call Andrew Stirling at 01-340 3291.

**AH** Allen and Heath Limited.

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# Cut costs by 50% with the same high performance.

## Isn't that what new ideas are all about?



Light in weight and low in cost, new Thermalloy heat sinks are designed specifically for plastic or metal case power devices.

They are remarkably simple to use, no extra mounting hardware is required—and they can be attached to the device after board assembly.

The slip on types have positive retention and can be supplied with locking tabs.

For full details of the range, simply return the coupon—cutting costs without cutting performance is a good idea you ought to know about.



**Thermalloy**

MCP Electronics Ltd. Alperton, Wembley, Middlesex  
Tel: 01-902 5941.



Please send me full details on Thermalloy heat sinks.

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Company \_\_\_\_\_

Address \_\_\_\_\_

Tel: \_\_\_\_\_

WW.11/77

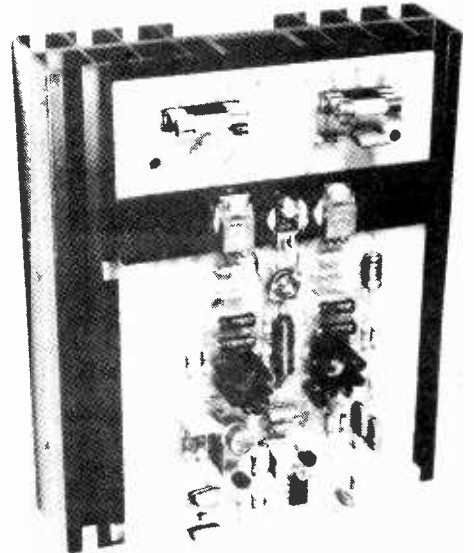


# We know of only one other Power Amplifier Module superior to our JPS 100 The JPS 150

For starters, JPS Power Amplifier Modules are designed, manufactured and tested in England, yet sold throughout the world.

Incorporating comprehensive protection circuits including mismatch, short and open circuits, impedance and thermal protection, these Modules will ensure a high standard of both reliability and top performance.

Unlike other models, they offer an indefinite life-span! Should they ever require any attention or repair, all components on both Modules are easily replaceable. And, what's more, they both also carry a full two-year guarantee. That's confidence for you!



	<b>JPS 100 £25.85</b>	<b>JPS 150 £32.61</b>
Power Output	110 watts RMS ohms	170 watts RMS 8 ohms
Frequency Response	10 22kHz -02dB	10-30kHz +0dB -02dB
Power Bandwidth	10 22kHz -02dB	10 22kHz +0dB -02dB
Slewing Rate	8.4 Volts per microsecond	9.00 Volts per microsecond
Total Harmonic Distortion	0.04% @ 1kHz	0.04 @ 1kHz
Hum and Noise	115dB below 100 watts	115dB below 150 watts
Damping Factor	Greater than 300 to 1kHz	Greater than 400 to 1kHz
Input Sensitivity	0dB (0.775 Volts) 100 watts	0dB (0.775 volts) 150 watts
Input Impedance	47k	47k
Power Requirements	- 45 Volts	- 55 Volts
Transistor Complement	12 transistors 1 integrated circuit	12 transistors 1 integrated circuit
Module Dimensions	4"H x 5"W x 2"D	6"H x 5"W x 2"D
Guarantee	Full 2 year	Full 2 year

\*These parameters may be changed to suit particular requirements  
For industrial usage frequency response can be extended DC to 30kHz +0dB -0.2dB (150 only)

**POWER SUPPLIES**  
PS 100 powers 1 JPS 100 price **£15.51**  
PS 150 powers 1 JPS 150 price **£19.22**  
PS 50 powers 1 JPS60 price **£13.50**  
PS 100 2 powers 2 JPS100 price **£28.82**  
PS 150 2 powers 2 JPS150 price **£30.75**

All module drive cards are based on industry standard Eurocard system (100 x 150 mm)

All Prices are subject to 8% VAT

A 60 watt version is also available with a similar specification Price £20.62 + VAT

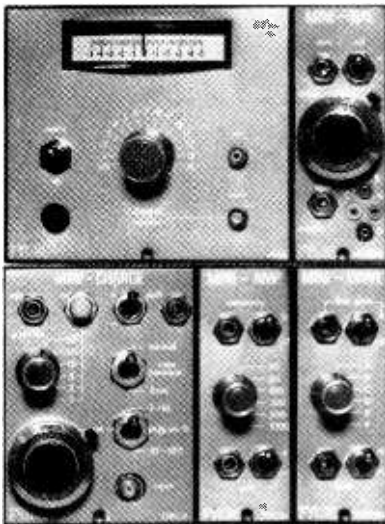
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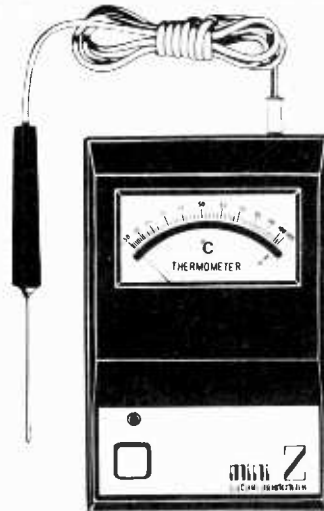
**FYLDE**

Fylde Electronic Laboratories Limited.

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## ELECTRONIC INDUSTRIAL THERMOMETER



### THE MODERN WAY TO MEASURE TEMPERATURE

A Thermometer designed to operate as an Electronic Test Meter. Will measure temperature of Air, Metals, Liquids, Machinery, etc., etc. Just plug-in the Probe, and read the temperature on the large open scale meter. Supplied with carrying case. Probe and internal 1 1/2 volt standard size battery.

Model "Mini-Z 1" measures from -40° C to + 70° C. Price £25.00  
Model "Mini-Z 2" measures from -5° C to + 105° C Price £25.00  
Model "Mini-Z Hi" measures from + 100° C to + 500° C £27.50 (VAT 8% EXTRA)

Write for further details to

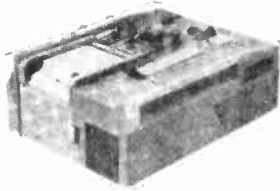
**HARRIS ELECTRONICS (LONDON)**  
138 GRAY'S INN ROAD, LONDON, WC1X 8AX  
(Phone 01-837 7937)

WW-046 FOR FURTHER DETAILS

# FAST RESPONSE STRIP CHART RECORDERS

Made in USSR

## Series H3020

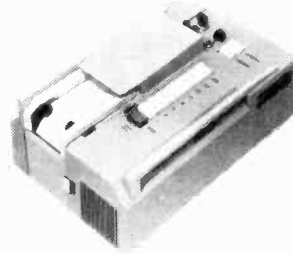


Basic error 2.5%  
Sensitivity 8mA F.S.D.  
Response 0.2 sec.  
Width of each channel:  
Single and three-pen  
recorders 80mm  
Five-pen recorders 50mm

Chart speeds, selected by push buttons: 0.1-0.2-0.5-1.0-2.5-5.0-12.5-25 mm/sec.  
Chart drive: 200-250V 50Hz  
Recording: Syphon pen directly attached to moving coil frames.  
Curvilinear co-ordinates  
Equipment: Marker pen, timer pen, paper footage indicator, 10 rolls of paper, connectors, etc.

**H3020-1 (Single pen):** 285mm wide x 384mm deep x 165mm high  
**PRICE £108.00**  
**H3020-3 (Three pen):** 475mm wide x 384mm deep x 165mm high  
**PRICE £160.00**  
**H3020-5 (Five pen):** 475mm wide x 384mm deep x 185mm high  
**PRICE £295.00**

## Series H327



Polarized moving iron movements with syphon pens directly attached. Built-in solid state amplifier (one per channel) provides 8 calibrated sensitivity steps. Two marker pens are provided.  
Basic error 4% Frequency response from DC to 100Hz 2dB.

Sensitivity: 0.02 - 0.05 - 0.1 - 0.2 - 0.5 - 1 - 2 - 5 volts/cm  
Width of each recording channel: 40mm  
Chart drive: 220-250V 50Hz  
Chart speeds: 1-2-5-10-50-125-250mm/sec.

**Type H3271-1. Single pen:** Dimensions: 259 x 384 x 165mm  
Weight 15 kilos **PRICE £265.00**  
**Type H327-3. Three pen:** Dimensions 335 x 384 x 165mm  
Weight 20 kilos **PRICE £520.00**  
**Type H327-5. Five pen.** Dimensions 425 x 385 x 165mm  
Weight 25 kilos **PRICE £770.00.**

Note: Prices are exclusive of VAT

Available for immediate delivery

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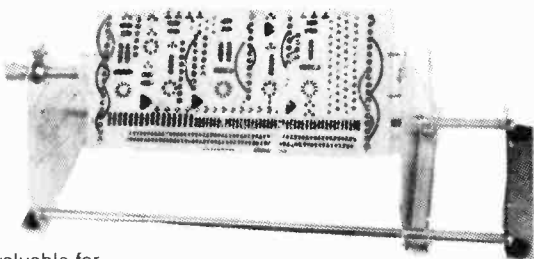
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# NEW for electronic design engineers!

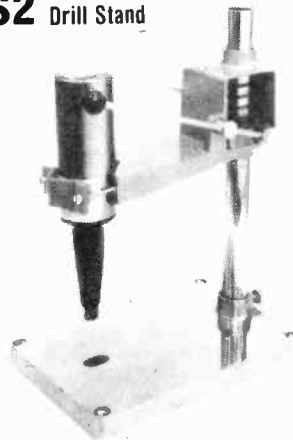
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Invaluable for holding P.C.B.s and other panels when inserting and soldering components. Can be adjusted to suit work up to 280mm, rotating to gain access to reverse side and locks in any position. All metal.

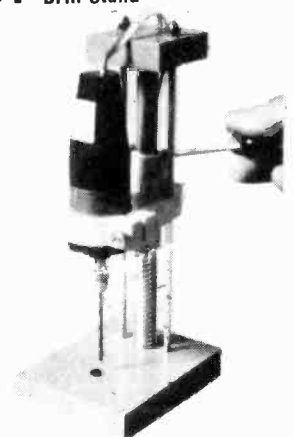
Price £10 inc. VAT. P&P £1

## S2 Drill Stand



Robust, all metal with ample throat dimensions. Adjustable height cantilever with lever actuated feed. Spring return. Will accept both P1 & P2 drills.  
Price £18.50 inc. VAT. P&P 106p.  
P2 Drill £18.50 inc. VAT. P&P 106p

## S1 Drill Stand



Constructed to take the popular P1 drill and ensure a high degree of accuracy in all types of electrical precision work.  
Price £5.13 inc. VAT. P&P 38p  
P1 Drill £9.67 inc. VAT. P&P 38p

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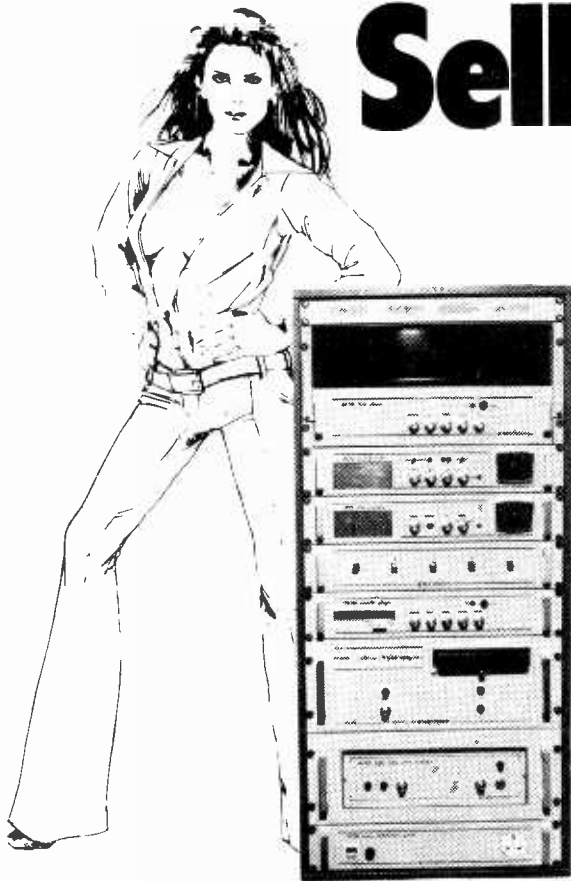
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Our equipment is used by such household names as Redifon, Carrefour, Rank Hovis McDougall, British Airways, Cunard, I.B.M., Grand Metropolitan Hotels and National Museums. And it's designed to interface with most other manufacturers' ranges. What more could we want? Well, right now we're looking for more overseas representation in those areas where we don't already have agents.

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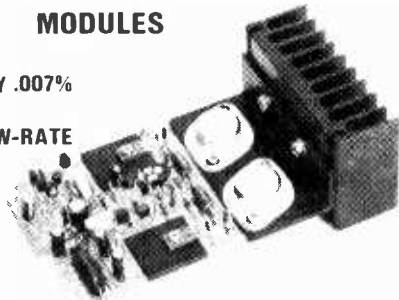
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## AUDIBLY SUPERIOR AMPLIFICATION

### HIGH DEFINITION — 'MUSICAL' — POWER AMP MODULES

- ★ T.H.D. TYPICALLY .007% @ 10W, 500HZ
- ★ ZERO T.I.D. (SLEW-RATE LIMIT 16 V/μS)

Module size: 120 × 80 × 25 mm. using glass fibre pcb with ident and solder resist. Illustrated with light duty heatsink.



CRIMSON ELEKTRIK power amplifier modules are fast gaining a reputation as the best sounding, most musical modules available. Perhaps the most important features of this design are: exceptional freedom from crossover distortion (due to the use of output triodes) and zero T.I.D. The amplifier is 'proton fed' (gains) - uses anti short circuit loads, and yet will drive a highly reactive (lower impedance) load, which is more representative of a real loudspeaker. Square waves maintain their rise times up to full power whilst simulated electrostatic loads are easily handled, with negligible overshoot and a settling time of 12 μS. Other specs: S/N: 110dB. Rise time: 10 μS. Sensitivity: 75mV DC-coupled 5Hz-35kHz. THD: 0.15% 100mW clipping 500Hz.

CRIMSON ELEKTRIK power supplies are in kit form for making an 'in-the-field' and feature a low field silicone toroidal transformer with a 120-240V primary and screen, two large capacitors, bridge rectifier and diode fixings.

Heatsinks are attractive black anodised extrusions - 80mm wide.

POWER AMP MODULES	HOME	EUROPE
CE 608 60W rms 8 ohms 35v dc	£16.30	£16.30
CE 1004 100W rms 8 ohms 35v dc	£19.22	£19.00
CE 1008 100W rms 8 ohms 45v dc	£23.22	£22.70
POWER SUPPLIES		
CPS 1 For 2xCE608 or 1xCF1004	£12.85	£14.20
CPS 2 For 2xCE1004 or 2 or 4xCE608	£14.55	£17.90
CPS 3 For 2xCE1008	£15.85	£19.20
HEATSINKS		
Light Duty 50mm 2 C/W	.90	£1.30
High power 100mm 1.4 C/W	£1.60	£2.40
Disc group 1500mm 1.1 C/W	£2.30	£3.65

### CRIMSON ELEKTRIK (WW)

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Interested?

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### Total systems capability.



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**Catronics**

### NEW FACILITIES AVAILABLE FOR WW TELETEXT DECODER

'Board 3' is now available as an additional unit to update the 'Wireless World' Teletext Decoder to give double height characters, colour background, conceal/reveal, etc., as described in this issue of 'Wireless World'. Our Kit includes plated-through hole P.C.B., all components and installation instructions. Price £33.68 + VAT (£3.47) + P&P (30p) = £37.45 total.

Our main kits contain all the printed circuit boards and components necessary to build the complete decoder.

A reprint of the series of articles is available at £1.50 + large 15p SAE (included free in complete kit)

	Standard version using 2513	New version with Texas X887	Post & Packing 30p
Set of 5 PCBs	£21.70	£21.65	£1.50
Component Kit (incl. PCBs)	£120.95	£133.70	—
Add-on Unit for lower case PCB	£2.70	—	—
Component Kit (incl. PCB)	£13.75	£14.85	—
Cabinet	£14.85	—	£1.00

PLATED THROUGH HOLE PCBs for TEXAS version only at additional cost of £27.00

COMPONENTS ALSO AVAILABLE SEPARATELY — RAE for price list

READY BUILT & TESTED DECODERS — £241.87 + £5 Carr.

DE LUXE VERSION WITH NEW FACILITIES — £292.50 + £5 Carr.

### WW MATRIX H DECODER

Based on the design for a MATRIX H DECODER published in June issue of *Wireless World*, with subsequent corrections, this Catronics Decoder is now generally available from stock in two versions:

Kit: comprising P.C.B.s, i.e. and all components to mount on the boards at £39.30.

Ready built: housed in attractive cabinet with integral power supply and Stereo/Quad switching at £89.37.

These prices include Sansui Royalty Fee, VAT and P&P.

### VHF FREQUENCY COUNTERS

200MHz, 7 digit, D.F.M. for direct readings up to the mobile radio VHF 'High Band'

Will operate on mains or 12V supply, making it ideal for use with mobile equipment.

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Demand for reprints of Wireless World constructional projects for audio equipment is so high that we have gathered 25 of the best of them together in High Fidelity Designs. These are the 'most requested' articles which **you** have asked for and all have been fully updated. Hurry for your copy — it's likely to sell out fast!

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# PROTECTION FOR YOUR TAPES!

## R.B. ANNIS HAN-D-KITS NOW AVAILABLE IN EUROPE!

Valuable audio and video tapes can be damaged when played on equipment that is not thoroughly and regularly demagnetized. Magnetism can easily build up in capstans, tape guides or recorder heads to a point where it will degrade the magnetically recorded signal on tapes passing over them. Tape damage is first apparent as a loss of recorded high frequencies and a progressive increase in background noise each time they are played on magnetized equipment.

Until recently, there has been no easy way to tell when demagnetizing was needed, and most

Demagnetizers on the market were far too weak to be effective, particularly on offending hardened steel guides or capstans, etc. Now, with the introduction of the Audiophile Hand-D-Kit, both measurement and correction problems can be solved easily at modest cost.

Here in one convenient package is everything needed to measure magnetic levels quickly, along with a handy, powerful unit to demagnetize components completely before they can spoil valuable tapes



Photo shows extra long probe — and standard Han-D-Mag. Both so powerful that they can be used for occasional bulk erasing of cassettes and 1/4" tapes.

### HERE'S WHAT THE AUDIOPHILE HAN-D-KIT CONTAINS

**ANNIS POCKET MAGNETOMETER**  
Measures level of magnetism in components  
Calibrated to read directly in gauss  
Model 20/B5 shown

**TEST STRIPS**  
One of these sensor strips is magnetically soft and the other magnetically hard. For experiments and testing your demagnetizing technique

**CLIP-ON EXTENSION PROBE**  
Extension probe is 1 3/4" long. Can be formed with fingers. Improves checking of magnetism in hard to reach components



**"NOTES ON DEMAGNETIZING" ETC.**  
Explains causes of magnetism, with particular reference to tape recorders. How to measure it accurately and how to eliminate it  
Interesting experiments also included

**ANNIS AUDIOPHILE HAN-D-MAG**  
A rugged dual-use Demagnetizer having a powerful sine wave demagnetizing field strength of over 350 oersteds 1/4" beyond the tip of the 2 1/4" long probe

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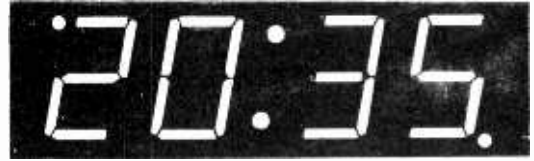
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The MA1012 LED digital clock module is a full 12/24 hour format clock unit, operating from 50/60Hz mains and offering a host of features: Hours, minutes display in bright 0.5" LEDs, with optional seconds, sleep and snooze alarms, fast and slow setting, PM indicator, switched output for radio, but the most important feature is the non-multiplexed directly driven display. This means no RFI, so the MA1012 is ideal for use in any type of radio/tuner etc. The neat fitting means it can be slotted into many existing cabinets/chassis - only 1.75 x 3.75 x 0.7" total!! £9.45 per module - isolating mains transformer £1.50 (8% vat) Two modules and two transformers for £20.00 + 8% VAT.

AMBIT announce a new addition to the catalogue - information on TOKO's new ceramic ladder filters, 2.4kHz SSB filters etc. HF coils, new flat faced low cost panel meters. Catalogue 45p.

## DETECKNOWLEDGEY

Metal locator principles and practise, including some of the facts that the manufacturers of £100+ metal locators wouldn't like you to know !! £1.00  
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### SEMICONDUCTORS

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KB4402	FM IF	1.94	40238	shld.RF	0.25*	EF5600U	5 varicap	FM	£12.95
HA1137W	FM IF	2.20	BF224	.6GHz RFO	0.22	NT3302UG	3 gang	FM	£7.50
TBA120	FM IF	0.75	BF274	.7GHz	0.18	EF5800	6 varicap	FM	£14.00
TBA120S	FM IF	1.00	ZTX212	50v/.3W	0.17	EF5801(5800+osc opl)			£17.50
SN76660N	FM IF	0.75	ZTX213	30v/.3W	0.16	8319	4varicap mos mix		£11.45
uA720	AM radio	1.40	ZTX214	30v/.3W	0.17	7252	fm tunerest		£26.50
CA3122E	AM radio	1.40	ZTX451	60v/1W	0.18	7253	stereo tunerest		£26.50
HA1197	AM radio	1.40	ZTX551	60v/1W	0.18	7020	cer. filt. fm if		£6.95
TBA651	AM radio	1.40	BD515	45v/10W	0.27	7030	linear phase if		£10.95
MC1350	agg gain	1.00	BD516	45v/10W	0.30	NB FM kit for 455-470kHz			£12.95
uA753	FM gain	1.80	BD535	60v/50W	0.52	nbm if filter/amp/detector			for +12v
LM1496	Bal mix	1.25	BD538	60v/50W	0.53	92310	mpx decoder		£6.95
MC1310P	mpx dec	2.20	BD609	80v/90W	0.70	91196	mpx decoder & birdy filter		£11.35
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tda2020	15w AF	2.99	MEM616	(40673)	0.57*	NW	for LWJ kit		£9.00
tca940e	10w AF	1.80	MEM680	lo noise	0.75*	940k	as above with tca 940E (both kits inc heatsink)		£3.95
tb810as	7w AF	1.08	BA102	vhf varic.	0.30	NB All our audio ICs are "short circuit" protected as defined by the manufacturer. All our mpx decoders are provided with TOKO mpx notch filters. All our FM IF modules use the improved mute version HA1137W.			
LM301an	op amp	0.39	BA121	..	0.30	Others: (from gen. price list)			
CA3130T	mos oa	0.85	BB104	dual varic	0.45	FX1115	ferrite beads		10/25p
uA741	op amp	0.34	BB105	uhf varic	0.40	FR1	mw/liw ferrite rod		£0.90
LM3900	op amps	0.68	mvam2	dual am	1.48	Min.	foil trimmers by Dau:		
7805uc	5v/1A	1.55	mvam115	25v/AM	1.05	5/10/20pF	swing		7.5 0.18
tda1412	12v/.6A	0.95	mvam125	25v am	0.90	33/42pF	swing		7.5 0.26
78M20uc	20v/.5A	1.20	TOKO COILS & filters			60pF	swing		10mm dia 0.24
78M24uc	24v/.5A	1.20	10mm			22turn	100k diode law		trimtops for varicaps 0.45
uA723cn	variable	0.80*	AM IFts with cap.	0.30		1000pF	feedthrus		0.05
NE550a	variable	0.80*	FM IFts with cap.	0.33		1000uH	F63v		1.15
TAA550b	32v ref.	0.50*	eg			Chokes 1uH to 124mH OA.			
ic18038cc	sig gen	4.50	YHCS1	1098AC2	0.30				
NE555v	timer	0.70	YHCS1	2374AC2	0.30				
NE566v	vco	2.50	YHCS1	1100AC2	0.30				
NE587v	tone dec.	2.50	KACSK	586GHM	0.33				
NE560B	hf pll	3.50	7mm	IFs for RC	0.33				
NE561B	hf pll	3.50	CFS10.7	ceramic	0.50				
NE565k	lf quad	2.50	BLR3107N	mpx	1.90				
MC1312	puall	1.50	HBR3132	ipole fm	2.25				
11C90	650MHz	14.00	MF1	2.4kHz 455	9.95				
ZTX107	50v/.3W	0.14	MF1T	4.57kHz	1.95				
ZTX108	30v/.3W	0.14	MFK	79kHz	1.65				
ZTX109	30v/.3W	0.14							

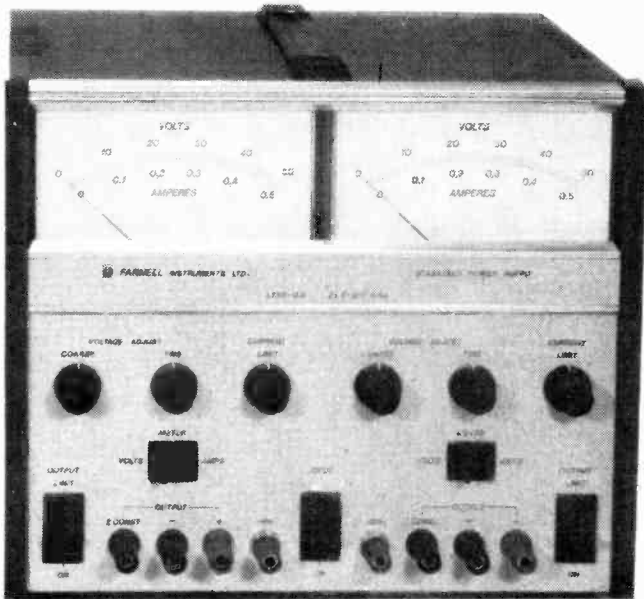
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WW-022 FOR FURTHER DETAILS

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L12-10C*	0-10V, 10A
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LT30-1 twin output unit	2 x 0-30V, 1A
LT30-2 twin output unit	2 x 0-30V, 2A

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WW-087 FOR FURTHER DETAILS

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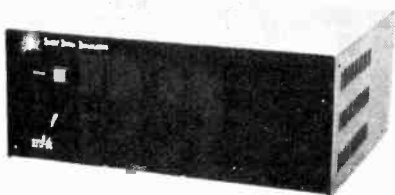
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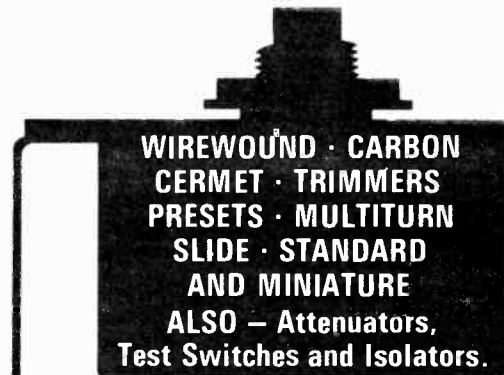
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SOCKETS</b></p> <p>8 pin .11              14 pin .12              16 pin .13              24 pin .48              28 pin .60</p> <p><b>400mW ZENER DIODES</b></p> <p>2.7v-33v .09 each              .80 for 10              3.50 for 50              6.25 for 100              Any Mix</p>	<p><b>ELECTROLYTICS</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>uf</th> <th>16v</th> <th>25v</th> <th>40v</th> <th>63v</th> </tr> <tr> <td>1</td> <td>.045</td> <td>.06</td> <td>.085</td> <td>.08</td> </tr> <tr> <td>2</td> <td>.045</td> <td>.05</td> <td>.055</td> <td>.06</td> </tr> <tr> <td>2.2</td> <td>.045</td> <td>.05</td> <td>.055</td> <td>.06</td> </tr> <tr> <td>3.3</td> <td>.045</td> <td>.05</td> <td>.055</td> <td>.06</td> </tr> <tr> <td>4.7</td> <td>.045</td> <td>.05</td> <td>.055</td> <td>.06</td> </tr> <tr> <td>6.8</td> <td>.05</td> <td>.055</td> <td>.06</td> <td>.07</td> </tr> <tr> <td>10</td> <td>.05</td> <td>.06</td> <td>.07</td> <td>.08</td> </tr> <tr> <td>22</td> <td>.06</td> <td>.07</td> <td>.09</td> <td>.13</td> </tr> <tr> <td>33</td> <td>.07</td> <td>.085</td> <td>.10</td> <td>.15</td> </tr> <tr> <td>47</td> <td>.08</td> <td>.10</td> <td>.12</td> <td>.19</td> </tr> <tr> <td>100</td> <td>.10</td> <td>.13</td> <td>.18</td> <td>.28</td> </tr> <tr> <td>150</td> <td>.11</td> <td>.15</td> <td>.20</td> <td>.28</td> </tr> <tr> <td>220</td> <td>.12</td> <td>.16</td> <td>.22</td> <td>.32</td> </tr> <tr> <td>330</td> <td>.14</td> <td>.18</td> <td>.26</td> <td>.36</td> </tr> <tr> <td>470</td> <td>.16</td> <td>.20</td> <td>.29</td> <td>.40</td> </tr> <tr> <td>680</td> <td>.18</td> <td>.24</td> <td>.35</td> <td>.48</td> </tr> <tr> <td>1000</td> <td>.20</td> <td>.28</td> <td>.41</td> <td></td> </tr> <tr> <td>2200</td> <td>.24</td> <td>.38</td> <td>.60</td> <td></td> </tr> <tr> <td>4700</td> <td>.39</td> <td>.52</td> <td>.85</td> <td></td> </tr> </table> <p><b>RECTIFIERS</b>              35 amp 30v Anode case Press-fit type .15              150 amp 100v Stud anode 1.00</p> <p><b>1 WATT ZENER DIODES</b>              4.3 - 100v .18</p>	uf	16v	25v	40v	63v	1	.045	.06	.085	.08	2	.045	.05	.055	.06	2.2	.045	.05	.055	.06	3.3	.045	.05	.055	.06	4.7	.045	.05	.055	.06	6.8	.05	.055	.06	.07	10	.05	.06	.07	.08	22	.06	.07	.09	.13	33	.07	.085	.10	.15	47	.08	.10	.12	.19	100	.10	.13	.18	.28	150	.11	.15	.20	.28	220	.12	.16	.22	.32	330	.14	.18	.26	.36	470	.16	.20	.29	.40	680	.18	.24	.35	.48	1000	.20	.28	.41		2200	.24	.38	.60		4700	.39	.52	.85		<table border="1" style="width: 100%; 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FOR COMPLETE LIST *</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>1N4006 .095</td> <td>2N2906 .18</td> <td>CMOS .15</td> <td>4034 2.00</td> </tr> <tr> <td>1N4007 .10</td> <td>2N3053 .17</td> <td>4000 .15</td> <td>4035 1.28</td> </tr> <tr> <td>1N4148 .05</td> <td>2N3054 .42</td> <td>4001 .19</td> <td>4036 2.40</td> </tr> <tr> <td>1N5400 .13</td> <td>2N3055 .42</td> <td>4002 .19</td> <td>4037 .99</td> </tr> <tr> <td>1N5402 .16</td> <td>2N3440 .50</td> <td>4066 1.00</td> <td>4038 1.00</td> </tr> <tr> <td>1S44 .05</td> <td>2N3450 .08</td> <td>4067 .19</td> <td>4040 1.00</td> </tr> <tr> <td>1S4020 .11</td> <td>2N3704 .07</td> <td>4008 .98</td> <td>4042 .82</td> </tr> <tr> <td>1S920 .06</td> <td>2N3705 .07</td> <td>4010 .56</td> <td>4043 .95</td> </tr> <tr> <td>1S921 .07</td> <td>2N3707 .08</td> <td>4011 .19</td> <td>4044 .99</td> </tr> <tr> <td>1S922 .08</td> <td>2N3710 .07</td> <td>4012 .19</td> <td>4046 1.32</td> </tr> <tr> <td>1S923 .09</td> <td>2N3819 .20</td> <td>4013 .50</td> <td>4047 .96</td> </tr> <tr> <td>1S951 .10</td> <td>2N3905 .12</td> <td>4014 1.00</td> <td>4048 .63</td> </tr> <tr> <td></td> <td>2N3906 .12</td> <td>4016 .50</td> <td>4049 .55</td> </tr> <tr> <td></td> <td>2N4058 .12</td> <td>4017 .95</td> <td>4050 .50</td> </tr> <tr> <td></td> <td>2N4062 .12</td> <td>4018 1.00</td> <td>4054 1.10</td> </tr> <tr> <td></td> <td>2N438 .50</td> <td>2N5133 .16</td> <td>4019 .52</td> </tr> <tr> <td></td> <td>2N696 .15</td> <td>2N5142 .18</td> <td>4020 1.05</td> </tr> <tr> <td></td> <td>2N697 .15</td> <td></td> <td>4021 .95</td> </tr> <tr> <td></td> <td>2N706 .20</td> <td></td> <td>4022 .95</td> </tr> <tr> <td></td> <td>2N929 .20</td> <td></td> <td>4023 .19</td> </tr> <tr> <td></td> <td>2N1306 .35</td> <td></td> <td>4024 .75</td> </tr> <tr> <td></td> <td>2N1307 .35</td> <td></td> <td>4025 .19</td> </tr> <tr> <td></td> <td>2N2219 .20</td> <td></td> <td>4026 1.65</td> </tr> <tr> <td></td> <td>2N2221 .17</td> <td></td> <td>4027 .60</td> </tr> <tr> <td></td> <td>2N2222 .18</td> <td></td> <td>4028 .85</td> </tr> <tr> <td></td> <td>2N2222A .20</td> <td></td> <td>4029 1.16</td> </tr> <tr> <td></td> <td>2N2368 .20</td> <td></td> <td>4030 .55</td> </tr> <tr> <td></td> <td>2N2368 .22</td> <td></td> <td>4033 1.50</td> </tr> <tr> <td></td> <td>2N2648 .42</td> <td></td> <td></td> </tr> </table> <p style="text-align: center;">ALL PRICES INCLUDE VAT</p> <p style="text-align: center;">FULL LIST OF LINEARS, CMOS AND 7400 TTL AVAILABLE.</p>	1N4006 .095	2N2906 .18	CMOS .15	4034 2.00	1N4007 .10	2N3053 .17	4000 .15	4035 1.28	1N4148 .05	2N3054 .42	4001 .19	4036 2.40	1N5400 .13	2N3055 .42	4002 .19	4037 .99	1N5402 .16	2N3440 .50	4066 1.00	4038 1.00	1S44 .05	2N3450 .08	4067 .19	4040 1.00	1S4020 .11	2N3704 .07	4008 .98	4042 .82	1S920 .06	2N3705 .07	4010 .56	4043 .95	1S921 .07	2N3707 .08	4011 .19	4044 .99	1S922 .08	2N3710 .07	4012 .19	4046 1.32	1S923 .09	2N3819 .20	4013 .50	4047 .96	1S951 .10	2N3905 .12	4014 1.00	4048 .63		2N3906 .12	4016 .50	4049 .55		2N4058 .12	4017 .95	4050 .50		2N4062 .12	4018 1.00	4054 1.10		2N438 .50	2N5133 .16	4019 .52		2N696 .15	2N5142 .18	4020 1.05		2N697 .15		4021 .95		2N706 .20		4022 .95		2N929 .20		4023 .19		2N1306 .35		4024 .75		2N1307 .35		4025 .19		2N2219 .20		4026 1.65		2N2221 .17		4027 .60		2N2222 .18		4028 .85		2N2222A .20		4029 1.16		2N2368 .20		4030 .55		2N2368 .22		4033 1.50		2N2648 .42		
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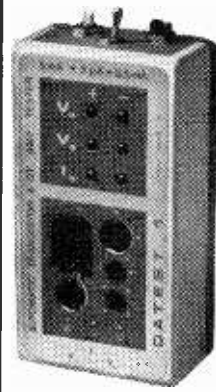
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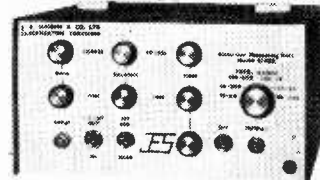
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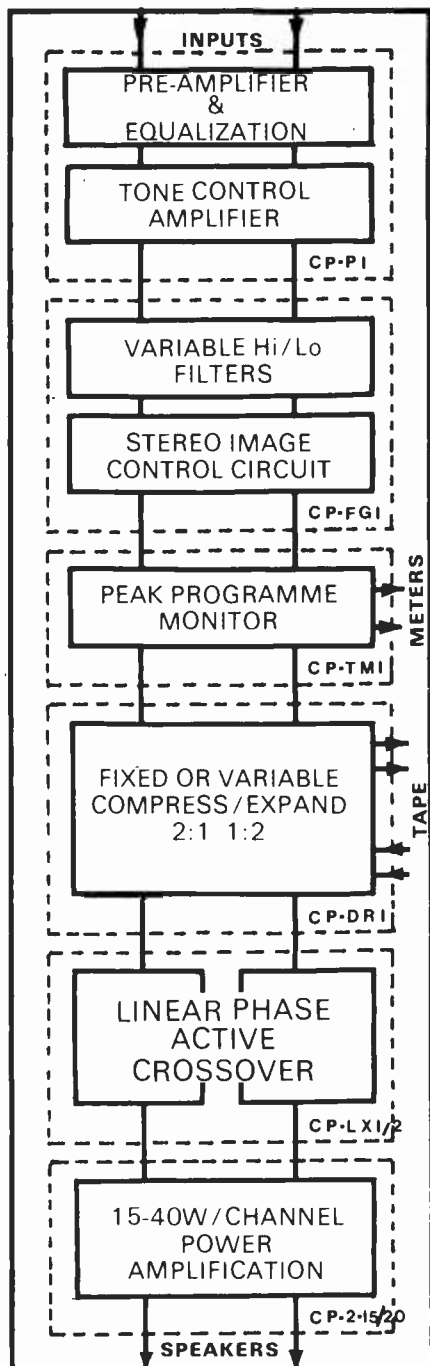
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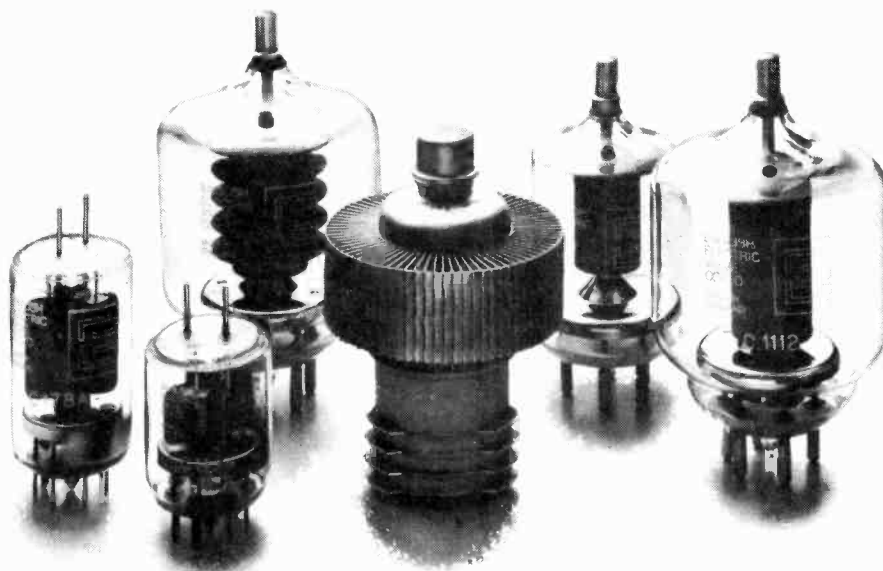
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## Microcomputers and *Wireless World*

Computers, it has been said, are hard-working idiots. This means that they are ready and able to cope repetitively with masses of figures that a large company needs, or thinks it needs, to run its business efficiently. They can do this at high speed, without making mistakes, but have to be programmed to carry out the work and must be provided with the data on which to work.

All that seems a long way from the domestic use of computers. The amount of number-crunching going on in the average household is not, one would have thought, at a level which requires the assistance of a computer — even the Christmas-present four-tab calculator is usually grossly under-employed. But in spite of this, a growing number of private users are acquiring microcomputers and, presumably, using them.

The uses to which microcomputers are applied appear to be trivial when the cost of a useable machine is considered — “on the road”, so to speak. But it is inevitable that not only will the cost of the electronics be reduced, but that worthwhile work for this still fairly expensive hardware to perform will emerge — perhaps in information retrieval or self-education.

To cater for this interest, a series will describe the construction of a set of equipment, preceded by a look at micro-computers in general. That being done, there will probably be a variety of interfaces and peripheral equipment to make and there this journal's involvement might be supposed to end.

After all, *Wireless World* is a journal for those interested in electronics and programming is scarcely a related topic, unless the programme is concerned with the design of circuitry or systems. As an analogy, television is our concern, in so far as the studio, transmitter, transmission path and receiver are of interest to engineers, but programmes are not the business of *Wireless World*.

Nevertheless, processors and computers are probably going to have a marked effect on our kind of engineering and to ignore the applications of these devices would be unrealistic. The boom in the use of private computers in America may or may not be repeated here, but there is evidently a degree of interest here already and in due course readers will be provided with the type of information that they need. It seems probable that the educational and small-company use of microcomputers will come first, followed by hobby applications, but this is mere guesswork. Observations from readers will be welcome and will help us to decide on the way the subject is treated.

As a start, the first of a series of articles describing a general-purpose microcomputer is published in this issue. The series is not “constructional”, but is an introduction to the subject to familiarise readers with microcomputers, in general. At a later date, it is the intention to publish a set of articles on the assembly and use of a microcomputer.

# Microcomputer design

## 1 — Introduction to digital hardware based on a microprocessor

by Phil Pittman, B.Sc. in association with NASCO Ltd

The low cost computing power of the microprocessor is now being used to replace not only other forms of digital electronics but also analogue electronics and electromechanical and pure mechanical control systems. It is not unreasonable to assume that within the next five years or so there will be hardly any companies engaged in electronics which are not using microprocessors in one area or another. One implication of this technology is that engineers skilled in the design of more conventional electronic circuits and systems now have to acquire new disciplines — those of digital computer system design and programming. This series of articles will present the theory and application of microcomputers by reference to a particular commercially available microprocessor, and to its use in a particular microcomputer system available to amateur experimenters as a kit (see panel). This low-cost kit includes memory, input/output circuits and a keyboard, and can be used in the home with a domestic television set as a display unit and an audio cassette recorder for permanent storage of programmes. The first article examines the hardware components and principles of operation of such a general purpose computer system. Future articles will explore programming languages, the organization of the central processing unit, and practical design techniques for both the hardware and software of microprocessor-based systems.

In its most general form a digital computer system has the structure shown in Fig. 1. The central processing unit (c.p.u.), memory and input and output units are the essential hardware blocks which any computer must have. The c.p.u. does the work, manipulating data as directed by a programme stored in the memory. The memory may also be used for storing data. Information is transferred to and from the outside world by the c.p.u. via the input and output units.

The c.p.u. being the most complex part and the heart of all operations in the system, will be examined first. It

may be viewed as two parts. One part, called the arithmetic and logic unit, actually does the work, while another part controls the sequence in which the various functions are performed. For the moment our main attention will be given to the arithmetic and logic unit (a.l.u.).

Any digital computer, including a microprocessor-based system, performs its data manipulation operations by utilising various combinations of the basic Boolean logic functions AND, OR,

NAND, NOR etc. Of course, in a processor system many of the operations are often compounded from these basic functions to provide more complex operations. Programme instructions are used to selectively activate the various logic and arithmetic functions of the processing unit in order to achieve the required result. Consequently, a processor may be viewed as a programmable, general purpose logic block.

In this concept lies one of the reasons

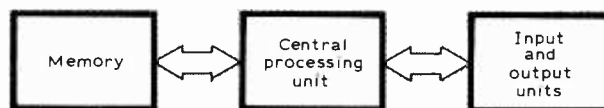


Fig 1

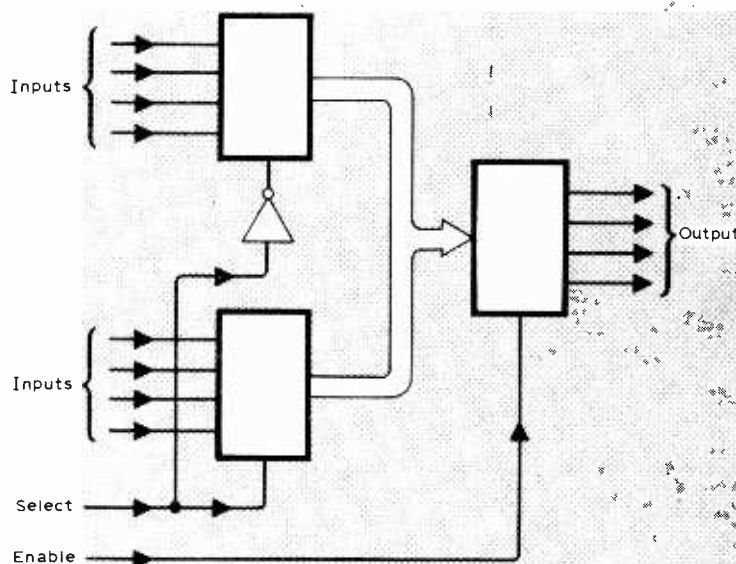


Fig 2

Fig. 1. Basic structure of a digital computer.

Fig. 2. A typical standard logic block, considered in the article as a step on the way to programmable logic.



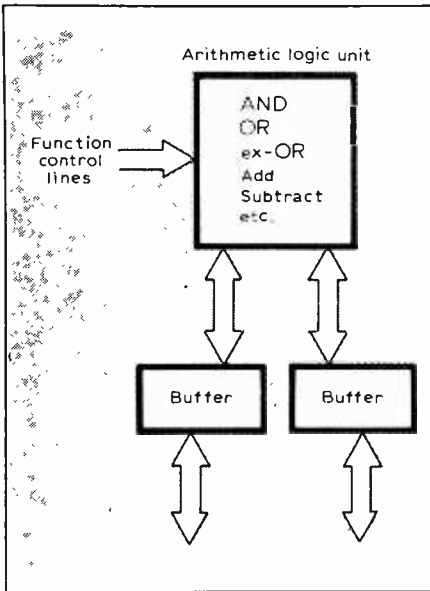


Fig. 3. A general purpose arithmetic/logic block.

for the use of the microprocessor, not only for the more usual computer type applications of data processing, but also for dedicated controllers and logic replacement devices. The low cost of microprocessors has now made them an economic solution for countless applications.

It is worth exploring this programmable logic concept further in order to understand more fully the operation and application of the central processing unit. Consider a standard quad 2-input multiplexer logic circuit as shown in Fig. 2. Here we see a standard logic block having a number of data input and output lines. The functions performed within the block are implemented with conventional logic gates. The exact function performed is dependent on the state of other inputs to the "system". The source of input data is determined by the state of the "select" line and the data is transmitted to the output under control of the "enable" line. Extending this concept further, we can arrive at the example of Fig. 3. The logic block has now been enhanced to include binary arithmetic functions. Also, there must be several more control lines available to select both the a.l.u. function and the data source and destination.

This programmable logic system now looks remarkably similar to the a.l.u. of a computer or microprocessor. In the processor the function control lines are derived, usually via decoding logic within the processor, from the binary instruction words which form the computer's programme. In order to control the sequential fetching and execution of the control codes, or instructions, from the programme memory the processor has a counter called a programme counter. If we now add a memory unit to the system of Fig. 3, together with additional a.l.u.

operations to transfer data to and from the memory, the resulting structure is virtually identical to the general purpose computer of Fig.1.

Internally the c.p.u. processes information as parallel rows of bits (binary digits) and so information usually flows in and out in the same format. The multiplexer circuit example given in Fig. 2 receives and issues data in 4-bit parallel form. Common microprocessor organisations are based on 4-, 8-, 12- and 16-bit word lengths. Of these, the 4-bit devices were the earliest types to appear commercially, partly because they were useful in calculators operating with binary coded decimal data, but also because the a.l.u., being only 4 bits "wide," was less complex, this allowing more circuit functions for a given cost on a semiconductor chip of given area.

Nowadays the technology has developed such that a complex 8-bit processor or even a complete micro-computer can be built on a single chip, resulting in the fact that hardly any manufacturers are introducing new 4-bit designs now. Eight bits has proved to be the most popular word length for microprocessing since the majority of applications can conveniently be dealt with by 8-bit quantities. Also, 8 bits represents the best cost/performance trade-off compared with other word lengths. Current 16-bit microprocessors offer surprisingly little increase in performance over 8-bit machines, even for applications requiring the manipulation of 16-bit quantities. Using a 16-bit processor where an 8-bit one will suffice will also inevitably incur higher system hardware costs.

**Microprocessor systems**

By adding more detail to the diagram of Fig. 1 we can evolve a block diagram of a practical microprocessor system. In this case it represents part of the commercial microcomputer kit referred to above, which uses a Mostek Z80 microprocessor, and is shown in Fig. 4.

A microcomputer system is merely an l.s.i. (large scale integration) imple-

mentation of the basic computer structure. The c.p.u., or microprocessor, is usually a single integrated circuit containing the a.l.u. plus programme sequence control and instruction decoding logic. The internal structure of the Mostek Z80 c.p.u. is shown in Fig. 5. The memory may consist of anything from one to a great many components of various types of memory. The input and output circuits may transfer data in serial or parallel fashion, the number of bits in a transfer being determined by the design, or more specifically the word length, of the microprocessor. Broadly speaking, the majority of input/output circuits (commonly abbreviated to i/o) in a microprocessor system will be of a parallel nature. Each i/o block is commonly called a port, where again the number of bits constituting a port is given by the microprocessor's word length. Each i/o port may be a complete integrated circuit, although many microprocessor families, including the Z80, have circuits containing a number of i/o functions.

All microprocessors use some form of clock circuit as a basic timing reference for instruction executions, memory and i/o operations. In the case of the Z80 a single-phase square wave has to be supplied to the c.p.u. component. This is provided by a simple t.t.l. circuit in the kit.

In order to form a working system these components must, of course, be suitably interconnected. Herein lies the elegance of microcomputer hardware. The microprocessor has a number of external connexions which may be used directly or indirectly to provide three categories of information for the remainder of the system. These information "buses", as they are called (shown by broad arrows in the diagrams), are connected in a standard manner to the memory and i/o devices regardless of the end application and regardless of the number of memory and i/o components to be used. Consequently a microprocessor system

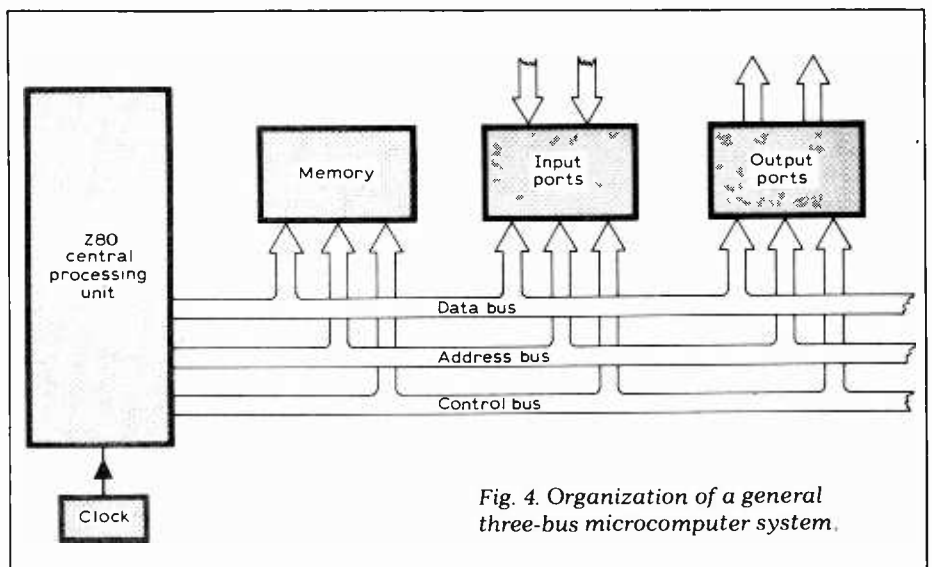


Fig. 4. Organization of a general three-bus microcomputer system.

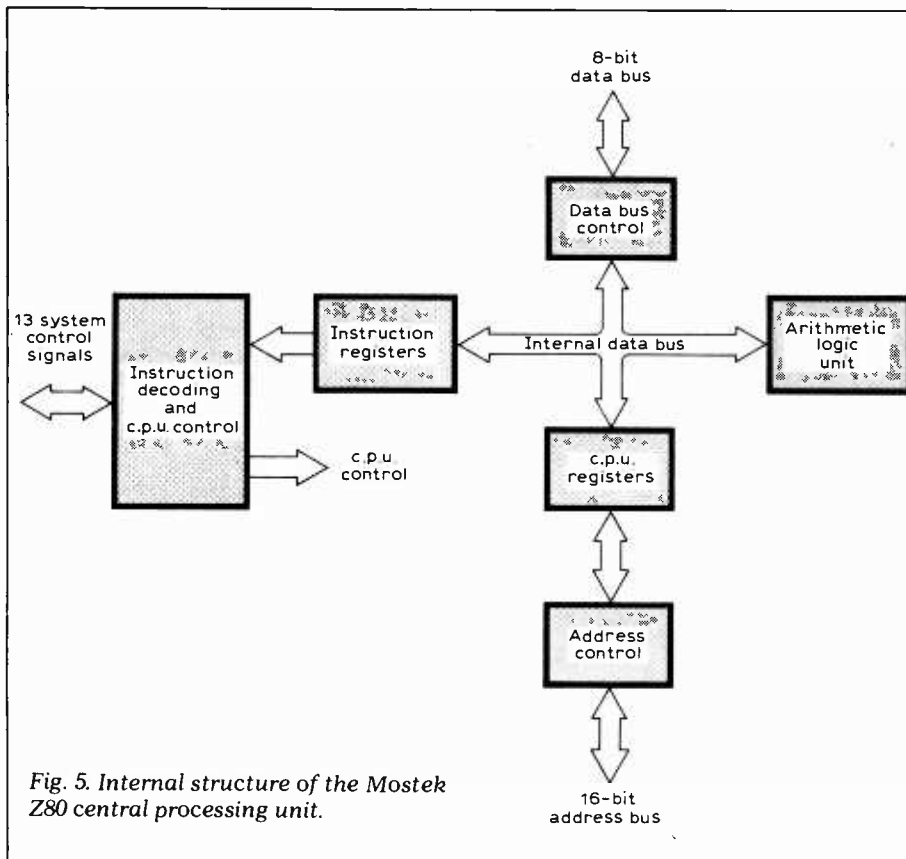


Fig. 5. Internal structure of the Mostek Z80 central processing unit.

may be usefully programmed and reprogrammed for a variety of applications. Similarly, a system with minimal hardware, if well designed, may be expanded at will to a more powerful configuration. This was the philosophy of the kit design.

Consider these three information buses which are shown in Fig. 4. They are the data bus, the address bus and the control bus. The data bus is a bidirectional one used for transfer of both data and instructions into and out of the c.p.u. The number of lines constituting the data bus is the same as the number of bits in the machine's word length. The Z80, being an 8-bit c.p.u., has an 8-bit data bus. This means that the system memory must also be organised as locations of 8 parallel bits. Similarly, i/o transfers will be to and from 8-bit ports. The data bus is connected around the components of the system such that all devices are placed on the common bus. All information transferred under programme control travels on this bus via the c.p.u.; for example, to transfer an item of data stored in the memory to a port, the data must first be fetched from the memory and passed into the c.p.u. and then sent from the c.p.u. to the output port.

Now let us consider the address bus. The number of bits constituting this bus has no direct relationship to the word length of the microprocessor. The address bus is used to select, or address, the location in the memory or the particular i/o port required for the current operation. The Z80 processor has an address bus of 16 bits, allowing the kit to be expanded to a maximum of

$2^{16} = 65536$  memory locations (or 64K bytes, where 1K = 1024). The value placed on the bus by the processor depends on the operation being performed, e.g. at the beginning of the instruction cycle the processor must supply the address of the next instruction in sequence to be fetched from programme memory. Then, during the execution of the instruction, data may be required to be moved between the c.p.u. and either the memory or an i/o port. If this is the case then the data memory address or i/o port address must be placed on the address bus by the c.p.u.

The third bus is the control bus. This is slightly different from the other two buses in that it is really a collection of individual control lines for memory, i/o and c.p.u. control. For example, in the case of the Z80 the main control signals are a "read" strobe pulse used to strobe data on the data bus into the c.p.u. from memory or i/o, and a "write" strobe to indicate that valid data is on the data bus from the c.p.u. to memory or i/o. This may be used to strobe data into a port or memory. Also there is an "input/output request" signal to indicate that the address bus contains a valid i/o port address, rather than a memory address. Similarly, there is a "memory request" signal indicating a valid memory address on the address bus, rather than an i/o address. Other control signals include a "reset" to the c.p.u., interrupt control (a concept explained later) and signals for suspending c.p.u. operation and de-activating the buses (useful in more complex, e.g. multiprocessor, systems).

A complete microcomputer system

has now been evolved which contains all the necessary functional blocks. In a future article the Z80 c.p.u. (Fig. 5) will be explained in more detail, along with the concepts which influence its design and use. For now it is sufficient to say that in addition to the a.l.u., the c.p.u. contains various register stores. In the case of the Z80 there are 18 eight-bit registers and 4 sixteen-bit registers which are accessible to the programmer via the various c.p.u. instructions. Some of these registers serve special functions and others are general purpose stores similar to the main memory locations.

### Memory organisation

It has already been implied that the memory of a computer system is used for two things – remembering instruction sequences (the programme) and remembering data. Semiconductor memory components may be one of two basic types, i.e. fixed, non-alterable memory and alterable, read/write memory. In dedicated microprocessor applications it is desirable to have the applications programmes fixed in permanent memory so that they are not lost when electrical power is removed. When power is applied, automatic operation of the system is then to be guaranteed. Such memory is called "read only memory" (r.o.m.). A true r.o.m. as such generally has its information fixed in it during the manufacturing process according to the particular customer's requirements. Consequently there is a minimum manufacturing quantity for this "customising" which is typically in the region of 100 to 1000 units. A popular alternative for lower volume and prototyping applications is the p.r.o.m. This is a programmable r.o.m. where the information may be fixed by the user by an electrical process which still results in permanent storage. A further development of this is the erasable p.r.o.m. or e.p.r.o.m.. These devices may have their data erased by exposure to short wavelength ultra-violet light, thereby enabling them to be reprogrammed.

Strictly speaking all these memories have the feature of being "random access". This means that any memory location may be reached, or "accessed", with equal ease, at random, by applying the appropriate address. However, the term "random access memory", or r.a.m., has commonly come to mean a read/write, or alterable, memory, e.g. the type used as a data storage element in a microprocessor system. In a general purpose computer system this r.a.m. may also be used as a programme store, thereby enabling different programmes to be loaded and executed at will.

The microcomputer kit referred to above employs a combination of the memories just described. In order to allow meaningful user communications with this system there is a 1024-location

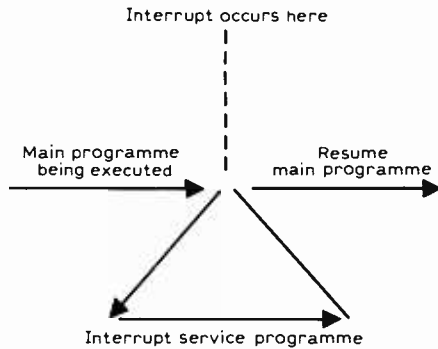


Fig. 6. Representation of the programme interrupt sequence.

(1K × 8 or 1K byte) e.p.r.o.m. containing a fixed programme. There is also a 2048-location (2K × 8 or 2K byte) r.a.m., a small amount of which is used

#### SPECIAL TERMINOLOGY

**Microcomputer.** A digital computer which uses a microprocessor as its central processing unit. The prefix "micro" does not mean literally "a millionth part of" but is derived from the word "microcircuit," an early name for the integrated circuit.

**Microprocessor.** A digital processing unit constructed as one or more integrated circuits, using l.s.i. manufacturing technology. Can be used as part of a microcomputer.

**Instruction.** An expression that defines a computer operation and identifies its operands.

**Programme.** A prepared list of instructions, written in a special "language" or code, to be carried out in sequence by a computer or other programmable device.

**Bit.** Abbreviated form of **binary digit**. The basic unit of binary coding (1 or 0) used to represent numbers, instructions or addresses.

**Byte.** Unit of binary information, normally consisting of eight bits.

**Word.** A group of binary digits representing a number, instruction or any other item of information. Often specified by its length, e.g. 16-bit word.

**K.** Abbreviation for 1024 (to be distinguished from the common lower-case prefix "k" that represents 1000).

**Serial.** Representation of binary information in which the binary digits occur in time sequence (e.g. on a single wire).

**Parallel.** Representation of binary information in which the binary digits occur simultaneously (e.g. 4 bits on 4 wires).

**Bus.** Abbreviated form of "bus-bar" derived from "omnibus". A group of conductors carrying words in parallel (one bit per conductor) in either direction; usually common to several devices and identified by function, e.g. address bus.

for variable data required by this programme. However, the main purpose of this r.a.m. is to allow the system to function as a general purpose computer, i.e. the user may enter his own programmes to the r.a.m., via the i/o peripherals and under control of the e.p.r.o.m. programme, for subsequent execution.

#### Input/output organisation

Data may be transferred to and from a microprocessor system in several ways, some under programme control and some initiated by external events not under control of the processor. The most commonly used type of input/output operation is generally that which is initiated by programmed instructions. The Z80 can transfer an 8-bit value to or from an i/o port with an instruction taking 4 microseconds for its execution. Alternatively, a single instruction may be used to transfer a complete block of data at a rate of 8 microseconds per byte. The i/o instructions are used to transfer the state of data existing on the lines of an input port into the c.p.u. or, conversely, data from the c.p.u. to the lines of an output port. The circuits of the i/o ports frequently have the capability of temporarily storing the i/o data. That is, incoming data may be latched on the port by the peripheral device until it is accepted by the processor executing an input instruction. Similarly, data output from the processor is often latched on the port until required by the peripheral. A subsequent output to the same port could then change the state of the output lines.

Other ways of implementing input/output in a system are by direct memory access (d.m.a.) or by programme interrupts.

Programme interrupts are a method of initiating a data transfer independent of the normal programme flow. For example, suppose the processor has to interrogate several peripheral i/o ports to see if they have any data to be collected for processing. One way for the c.p.u. to handle such a situation is for the system programme to control a "polling" routine whereby each device is periodically examined in turn for data. The disadvantage of this is that a great deal of valuable processing time may be consumed by checking for valid data at a port when frequently there may be none ready. Interrupt operation overcomes this limitation. Now the c.p.u. does not have to periodically check for valid data: it is told, or interrupted, by the peripheral when this data is available. This interrupt, usually sent as a signal from an interrupt control circuit, has the effect of suspending the execution of the programme and then forcing the c.p.u. to a new programme which services the interrupting device. Upon completion of the service programme the c.p.u. is allowed to resume the previous execution of the programme. Fig. 6 shows the interrupt

sequence diagrammatically. In a system with a number of separate interrupt sources it is usual to assign a priority to each one to ensure a sequence of servicing if multiple interrupts occur.

Direct memory access is generally a faster method of transferring data than may be achieved under programme control. D.m.a. transfers occur directly between the system's memory and the i/o device without involving the c.p.u. Consequently the speed of data transfer is limited essentially only by the speed of main memory. A typical d.m.a. transfer rate would be in excess of 1 megabyte/s. A special d.m.a. controller circuit initiates and controls the transfer in response to an external request. The c.p.u. operation must be suspended during the transfer and is allowed to resume operation when the transfer is complete. This is so that both c.p.u. and d.m.a. controller will not try to use the system buses simultaneously. D.m.a. is generally used in more complex systems when large blocks of data have to be transferred to or from peripherals at a speed greater than can be achieved by programme instructions. It is also possible to do single byte transfers under d.m.a., often without stopping the processor if the transfer can take place while the c.p.u. is not using the buses. This is often called "cycle stealing".

The actual i/o parts of a microprocessor may be implemented with standard t.t.l. logic circuits, e.g. 8-bit latches or buffers, or with the more integrated members of a manufacturer's l.s.i. microcomputer family.

Part 2 of this series will give a practical example of hardware and will also deal with software.

#### Microcomputer kit

This kit, known as NASCOM I, includes a Mostek Z80 microprocessor, MK3880; 2Kbyte of r.a.m. using Mostek 1024-bit r.a.ms, MK4102; 1Kbyte of e.p.r.o.m. using the Mostek 1024 × 8-bit e.p.r.o.m. MK2708; u.a.r.t. type M6402; character generator MCM6571A; i.cs. for video r.a.m. logic; zener diodes; 16MHz crystal; interfaces; a keyboard; and p.c. boards. Price £197.50 (ex. v.a.t.).

The microcomputer is designed to use a domestic tv set as a visual display and a standard audio cassette tape recorder for programme storage. It can be adapted for use with a teleprinter and allows memory expansion to 64Kbyte.

Further information from the suppliers: Lynx Electronics (London) Ltd., 92 Broad Street, Chesham, Bucks. (tel: Chesham (02405) 75154).



**626,000 visitors/486 exhibitors from 27 countries/1000 new products/"reserved optimism" for entertainment electronics to 1980/8-10% increase for 1977/colour tv reaches 50% penetration/two techniques for picture insets/microprocessors, in tv?/set-makers sell r.o.m.-cartridge game/Videotext problems: publishers vs broadcasters/Viewdata plans/next IFA: Berlin 24.8-2.9 1979.**

"There is justifiable reason for reserved short and medium-term optimism" was how Professor Dr H Jurgensen, director of the Hamburg Institute for European Economic Policy, assessed the immediate future of the entertainment electronics market in Germany. "Provided," he added, "the producers do not overestimate the doubtlessly available market potential . . ." a clear reference to the embarrassing over-production of tv sets, which occurred earlier in the year.

Isolating the main market factors he cited the increasing percentage of adults in the population. From 1975 to 1980 the number of people between 16 and 30 will increase by two million — and with it the number of small households — the total population being due to fall by one million. The proportion of educated and highly skilled people with purchasing power is expected to increase and low income groups will become less significant, he said. (An income of 3000DM per month is already enjoyed by 90% of the self-employed and 10% of pensioners.) Expenditure on leisure and education, currently 10% in middle and higher income groups, is growing faster than incomes and has tripled in the decade from 1966. In addition, there are signs that consumers are getting more quality conscious, want greater participation and more variety in their entertainment, all trends which Prof Jurgensen argued will benefit entertainment

# Television developments in Germany

## A report from the Internationale Funkausstellung, Berlin

by Geoffrey Shorter

electronics in coming years. "What all this adds up to," he concluded, are "well-above average" prospects to expand "with due caution."

Taking a wider view and putting numbers to their forecasts, Grundig, who are the colour tv market leaders, see business as "reasonably safe" in Europe and estimate a growth in demand of half-a-million sets a year. This would bring the total demand for colour tv in Western Europe up to 9.5 million units by 1980; an average rise of 5% per year, and giving a market penetration of 51%.

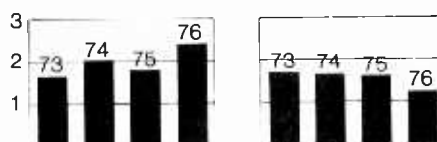
Manufacturing industry for entertainment electronics in Germany showed an increase in turnover last year of 1000 million DM or 20% (excluding record players) — a real revenue increase of 8.5% — mainly as a result of increased colour tv production. Production of black and white tv sets and radio receivers fell by 25% but was largely compensated for by increased production of portable radios, car radios and hi-fi systems.

Sales of German-made colour sets, 2.3 million, did particularly well (up to 24% in value, higher for exports which were a third of production) apparently at the expense of black and white sets, which sold 1.2 million units including exports (1975: 1.6 million). There is little doubt that the Olympic Games and

Bundestag elections helped achieve this high level of sales, though there are underlying trends beneath that surface. Now that colour television is becoming the norm in Germany — one in two households have a colour set (1976: 46%) — there is a gradual change from black and white to colour, as well as colour renewals now that colour tv in Germany is a decade old.

The only other equipment to get anywhere near the colour tv growth is car radio, increasing sales from 2.5 million in 1975 to over 3 million. First half figures for 1977 show a 17% growth. More than half the vehicles in Germany now have car radio, though how many sales are due to the traffic information system isn't clear. 1977 does not appear to be off to a good start in tv with a fall of 4% in sales in the first half compared with the same period in 1976 — colour share in this is up only 1.2% — but it is argued that the majority of business is done in the second half of the year, especially an IFA year.

In addition to falling demand for black and white tv sales (–15% first half of this year), market share for 67cm colour sets is falling whilst the share of smaller screen sizes is increasing. One forecast expects sales of 67cm sets to remain constant in Germany at around 1.7 million until 1982, when penetration would be 77%, with portables of 37 to 50cm increasing by 50% to give a share of 25%, and intermediate sizes increasing by 60%, the large screen slipping from 70 to 62% of the market. In Europe, the large screen size will have fallen from 64% in 1976 to 50% in 1980. In response to this manufacturers are fitting sales-attracting features on their portable sets, like remote control (half the sets in Germany now have remote control), automatic search tuning, and tv games.



These figures, in millions of units, for German television production are derived by adding imports to home production and subtracting exports. Colour figures on left, black and white on right.

The most significant aspect of receiver development in the decade of German colour television has been its conversion to semiconductor engineering. This has not only helped to keep prices stable — our 1967 Berlin show report gave the price of a large-screen colour set as 2,300DM about the same as now and production costs of equivalent table-model colour sets have in fact fallen by 15% — when the retail price index has increased by 57%, but has had a major effect on reliability as measured by repair calls. “The owner of a colour set using valves could expect an average of one to three repair calls a year,” recalls Gunter Kroll of the manufacturers association ZVEI, “Whereas this need has been reduced to 0.15 to 0.5 calls in today’s television sets.”

Actually, the service technician has never had it so good. For as well as producing equipment of increasing reliability, manufacturers have made diagnosis a very simple affair with their various Servicefreundlichkeit aids, and repair straightforward with the modul-technik, now almost universal following the lead of Körting, and Grundig. But it must be considered, comments Kroll, to what extent modular construction is important for servicing when frequency of repairs is that low. Highly integrated circuits could “usurp the role of the module completely.” (Could they not have their own fault diagnosis and indication circuitry built in, we ask?)

The attractions of avoiding mechanical tuning contraptions were appreciated fairly early in European tv sets, for both geographical and mechanical reasons. Mechanically, the use of variable-capacitance diodes meant that the tuner could be situated on the same p.c. board as the rest of the circuitry, it made it much easier to tune and band switch remotely. It was also easier to produce variants — there wouldn’t be so much difference between a continental 16-channel model for the border areas, and, say, a UK-only set of three or four channels capability.

In our last Berlin show report we said Philip’s proposed an all-electronic m.o.s. tuning system that would encompass search tuning with memory, memorized analogue control settings, on-screen displays and remote control. Now, the system is in use in Philips, Loewe-Opta and some other top-line sets and does away with the 8, 12, 16, or more tuning potentiometers, storing the station frequencies in a random access memory. In this frequency synthesis approach to digital tuning the frequency of the local oscillator is measured directly. Digital information representing a desired channel is called up from a memory i.c. and compared, coincidence causing a control i.c. to lock the tuning.

The system, called TRD for tuning, remote control and digital, originally needed four i.c.s with an option of a further five for special functions like on-screen display and search tuning,

but now Philips say they can provide all functions with seven. When a channel is ordered, a binary-coded oscillator frequency is recalled from a SAB2014 read-only memory and compared with the output from an SAB1078 e.c.l. prescaler, whose output is the oscillator frequency divided by 256. If the difference is more than a certain amount pulses are generated whose width is proportional to error and which are used to retune the oscillator until code parity is obtained. A further i.c. is a SAB2015 r.a.m. which can store b.c.d. information on 16 user-selected channels. The full technique permits direct channel selection without having to go through a fixed sequence, as well as automatic search and sequencing modes, and sets using it can be tuned without access to tv transmission. Cost is higher than the voltage-synthesis technique and is therefore only found on the luxury-class set.

Automatic search and elimination of tuning potentiometers were also primary aims with ITT Intermetall’s open-loop voltage synthesis method. The tuning voltage is generated in steps and it is the number of steps required for accurate tuning that is stored. The two key m.o.s. i.c.s, a SAA1021 control circuit and an SAA1020 static shift-register memory, are both compatible with two others, one for handling ultrasonic remote control codes SAA1130 and one for on-screen channel number display, an SAA1008 or a derivative that also acts as an on-screen indicator for tuning voltage, tv band, and brightness, colour saturation and volume control movements.

The 66/67cm in-line c.r.t dominate the German colour tv market, though 51 and 56cm sets are gaining a larger share and 36cm is the most popular size in portables. Precision in-line or PIL tubes have gained ground in medium-size sets, but “problems” in large screen sizes make the 20AX in-line variety the popular choice. By all accounts these two formats will be with us for some time to come. But while one industry spokesman was saying we couldn’t expect “spectacular innovations providing visible advantages” in picture tubes, ITT Components were announc-

ing a tube with a visibly brighter picture. By changing the glass colour, making some alteration to the slots in the mask, and improving the phosphor, they claim an increase in brightness of 70%. But with 600,000 sets unsold — half as much again at the same time in 1975 — there were feelings that its introduction should have been delayed. Nevertheless both ITT brands, Schaub-Lorenz and Graetz, and Körting have taken up the new tube: “We know Mullard are working on something,” confessed an ITT spokesman.

As market penetration of colour television passes the half way mark, set makers will need to rely more on “convincing innovations and the rationalization of production,” as Gunter Kroll puts it, than on having tv sets in the right place, at the right time and in the right quantity. Already the German TV market has probably seen more market-oriented innovations than any other, starting with diode tuning and band switching, switched-mode power supplies, provision for connecting external equipment, high quality sound, large-signal p-i-n diode tuners, touch sensor channel selection, ultrasonic remote control, modular chassis construction, self-diagnostic service aids, infra-red sound links, permanent pre-set control settings, on-screen colour display of control settings, on-screen, display of time and channel numbers, infra-red remote control, and automatic search tuning systems with memory. You name it. And this year adds reduced power dissipation, built-in games, inset second program pictures and microprocessors to the list.

In competing for new features the makers with the large market shares (Grundig is biggest with around 30%, Philips next with 12-14%, followed by Telefunken and Saba with around 10% each) have a built-in advantage. They have the production to justify the “¼ to ½ million quantities that the i.c. makers need” points out Dr Böhme, chief of Körting, alluding to Grundig’s latest “Vollbild-im-bild” scoop, in which a reduced-size picture of another programme is inset into the main picture. With their enormous production — a million sets or more — Grundig have

*Synchronization of inset black and white pictures of a second tv programme relies on closeness of sync pulses from different transmitters, but small differences give rise to inset movement. Banding is avoided by switching inset into different quadrants. Alternative is to read out the inset from a memory: new bucket-brigade charge transfer device can store 1 in 4 lines.*



been able to tie up the ITT-Intermetall i.c.s exclusively for a 6-month period. The tv manufacturing subsidiary of ITT, in Germany, Schaub-Lorenz, must be waiting to see how this expensive luxury goes down before committing themselves. They dropped the clock idea, which had added 200DM to the price of their tv sets, as a "silly gimmick". If they want to know the time, comments Charles J. Zsakovits, ITT's tv product manager, most people just look at their watch. And at an additional cost of 300DM for the Grundig/Intermetall inset picture approach, ITT must feel its appeal is fairly limited: "For that you can get another black and white set," muses Zsakovits.

In the face of such deals with semiconductor device manufacturers, firms with smaller shares of the market like Körting — Dr Böhme declined to give their share — had to think up ideas first.

On-screen colour display of control settings was a Körting idea of three or four years ago and their latest is the use of hi-fi loudspeakers as microphones and in tv, a set that *speaks* its channel number. They have other ideas anyway for implementing the picture-in-picture facility and they are investigating switching the local oscillator at 700MHz, Dr Böhme told *Wireless World*, so that only one r.f., i.f. and demodulator sections would be needed.

With the i.c. approach, a stable second picture location is made possible by using a memory to store the reduced-size picture. Video information is written in synchronism with a transmission to be inset but read out in sync with the main picture signal. Two new charge transfer devices, type UAA1000, of area or matrix format rather than line or row format, store and read the inset picture line-by-line under control of a third i.c., SAA3000. One of the memories is storing information while the other is reading, both under read, write and shift direction from the SAA3000 i.c. Only every fourth scan is stored — the inset picture is quarter-height — and horizontally the writing speed is limited to 1.5MHz with read out four times faster. The Belgian manufacturer Barco say they will also be using charge transfer devices in this application.

The other way of tackling the problem, adopted by Saba and Telefunken, relies on the  $1$  in  $10^6$  tolerance of the colour subcarrier and consequent closeness of sync pulses from different transmitters, making it possible to display part of a second programme with the receiver deflection circuits locked to a primary programme. The incomplete second picture with full resolution, measures 16 x 18cm on a 67cm tube. Snag is a horizontal wandering of the inset due to small errors in synchronization, but the marketeers are quick to point out that this gives a greater effective sampling area than would otherwise be the case! And these sync differences would also

give rise to black horizontal or vertical bands some of the time; so logic circuitry is included that decides which corner of the screen to use for the inset so that the black bands do not show.

Nordmende had thought of it all before of course. Their Spectra Colour Studio with its three 20cm monitors beneath the main 66cm picture was wheeled out, as if to ask what all the fuss was about. Their set, or rather its predecessor, had simultaneous four-channel capability back in 1967!

The combination of large-scale integration with digital signal processing enables developments to be made in tv sets the cost of which would otherwise be prohibitive. Though memories are coming to tv sets in increasing numbers and complexity — still full-picture stores will soon be in sets — there are differences of opinion about microprocessors. While some manufacturers are dabbling with microprocessors, one engineer with the ZVEI asserts that in spite of inroads into process control and data handling, it is certain *not* to find use in TV sets in its present form. "In most cases," says Gunter Kroll, it is "not a suitable component for the functions required of a tv set — its capacity is too large," and argues that specific i.c.s for tv use yield a better price-performance ratio. Time will tell whether Blaupunkt's use of a microprocessor will be confined to its luxury-class set.

In the Blaupunkt PS19 set, a 30-key remote unit is used to select any of 19 channels. The three-chip Fairchild F8 microprocessor allows storage of 20 switch-on, switch-off or switch-over commands, with or without date, selection of the desired channel, or switch off five minutes after transmitter close-down, as well as the other facilities common to digital tuning, remote control using the SAA1024 and on-screen display of time, date, tuning voltage, channel number and band. A non-volatile m.n.o.s. electrically alterable r.o.m. stores switching commands; coarse and fine tuning voltages and four standard values for the analogue controls of saturation, brightness, contrast and volume for up to 19 programmes.

The other European set maker to show sets using a microprocessor is Barco. A combination of Texas and National chips, enables a programme tuner to switch four pre-set programmes at chosen times, and to jump from one programme to another at eight-second intervals every minute or half-minute. The set uses the voltage-synthesis search tuning and storage technique.

A teletext version of their Gauguin set, which they say will be available next March, will switch to teletext at a pre-set time and is being made with reception of the French teletext system — Antiope — in mind.

Barco say their new tuner-amplifier incorporates a microprocessor. Using a frequency synthesizer technique for tuning in 1kHz, steps on the a.m. bands

and in 25kHz, steps on f.m., up to 16 frequencies can be stored in the non-volatile memory. A search mode is available, which can select only stereo stations if required. Such facilities have been available for some years on other digital f.m. tuners, though not with a "32-function" remote control unit as far as we know, and it's not altogether clear what additional benefits the microprocessor confers.

Notorious for inducing boredom fairly quickly, the first generation of television games born in 1972 were never really marketed extensively in Europe. The second generation types, using purpose-designed integrated circuits, some of which offer a choice of up to ten "ball and paddle" games, are now being built into tv sets and selling alongside the newer third generation programmable games. The Fairchild, programmable unit, which they call a "video entertainment system," was introduced in the USA in June 1976 and approved by the FCC last November. (In the USA games for connection to tv antenna sockets require FCC type approval to keep r.f. radiation below  $15\mu\text{V/m}$  at 1m from the set.) Fairchild's entry on the European tv games market seemed to come at a time when they were experiencing problems in their watch business. "We took a fairly big bang in losing \$8 million in three months," explained R. H. Bohnet, international marketing director, who told how Fairchild had gone "from zero to \$80 million in digital watches in one year". They appear to have been successful in their European efforts. They cancelled a Berlin press conference, booked earlier in the year, because they "didn't need it." And Saba, now owned by General Telephone & Electronics, have the Fairchild game, selling it with their own markings. Luxor too, who have taken a commitment in Sweden, and "a lot of companies at the show are evaluating" according to Fairchild.

In the U.S.A. the unit sells to retailers (as "Channel F") because of established links, but in Europe it is sold to the set maker for resale: "a tv set would cost too much if it were built in," they say. The game is based on the F-8 microprocessor with a range of Videocart r.o.m. cartridges — 10 now, 15 by the end of the year — with up to four games per cartridge. They include things like blackjack, various races, shooting gallery, doodles, tank fights, and one can store thousands of different mazes. The player control sticks are described as having "eight degrees of freedom" (they mean four) and both colour and size changes can be made from it. There are options for playing the "machine" as well. "It's not very interesting playing backgammon with a machine," admits Mr Bohnet, "but we're working on chess".

Out of the other r.o.m.-cartridge games recently approved by the FCC only the Atari game was seen in

operation, on the Telefunken exhibit. They are test marketing the unit this autumn at 500DM and 50DM per cartridge (with a maximum of 50 programmes): similar pricing to Fairchild's. "The unit is too expensive to build into sets", said a Telefunken marketing executive "2,500DM is the magic barrier for colour tv".

But the biggest innovation that German colour television is likely to see in the near future are the text transmission systems and practically every European set maker at the IFA had to show their sets were text-capable. Some sections of the industry are setting their sights on 1982 as the starting year for a text service, assuming Medienpolitik problems are sorted out. "We don't want it before" Körting's boss told *Wireless World*. After the 2/3 penetration point has been reached and tv production falls off, he argues, is the time to introduce the system. Other interests may not agree, but it is difficult to see how there can be an early start to a broadcast system when there is no agreement over who should run it.

Different laws govern press freedom and broadcasters independence, neither having foreseen a hybrid service like teletext or Videotext as it is called in Germany. The problem is that newspaper publishers do not take to the idea of broadcasters controlling the written word – they say they should stick to the spoken word – while the broadcasters say that as long as the programme comes from a transmitter it is certainly a matter for them. "The newspaper industry is afraid of teletext," admits Dietrich Ratzke, managing editor of the *Frankfurter Allgemeine* and editorial consultant of *Bildschirmzeitung*, the publishers teletext. It's not that there is an immediate danger of newspapers disappearing, he explained, but that "it's not good for the long-term health of newspapers." And who will say that an alternative source of on-demand information traditionally supplied by newspapers – e.g. sports results, stock market data, entertainment guides and the like – will not affect them?

In Germany the radio and television stations are not state-controlled but are self-governing non-profit public corporations, with their legal basis either on Land legislation or in a treaty between Länder. Most Länder do not appear to want to authorize a newspaper-run text-transmission service, presumably because as the law stands, programmes can only be provided by the station and not by a private organisation. There are some special situations recognized but the wording is vague. Obviously the exhibition was deemed a special case and the Berlin Land gave permission for trials only on a closed-circuit basis and only for the duration of the exhibition.

Last autumn 24 newspapers belonging to the publishers association BDZV sent editors to form the *Bildschirm Zeitung*. They made numerous visits to London, consulting with GEC, and the



BBC and IBA teletext units, preparing themselves for the two-week competition with the broadcasters at the Berlin show. The editing team took current affairs information, e.g. via telex from Springer, transcribed and edited it on the GEC stand and sent it round the exhibition on channel 35. The broadcasters for their part formed a joint ARD/ZDF Videotext unit and following test transmission during July (ZDF) and August (ARD) went on the air from the SFB transmitter on channels 7 and 39 for the duration of the exhibition.

"The publishers aim is clear" Alexander Kulpok of the joint Videotext unit at SFB told *Wireless World* "but they don't know how to achieve it. They are only interested in getting into the business." The answer, thought Kulpok, depended on "a political solution and upon the future of commercial television." The situation could change "if the Christian Democrats get in or if there is cable television within say five years." And a service could come very soon, he said, "if it comes to a fight" and a Court of Law had to decide.

Now that the exhibition is over the publishers feel sure the ARD/ZDF unit at SFB will continue elsewhere, perhaps at Mainz with ZDF or Munich with IRT. And next move by the BDZV will probably be to seek permission to market a service from the respective Landesregierung. But it's difficult to see an outcome that will please everyone; Ratzke thinks that the publishers will be allowed to run a service, but it would have to accept the ultimate control of the tv stations. "And what of the law that forbids outside control of the free press?"

By comparison, the problems of the wired interactive version, given its first public showing in Berlin and which is identical to the UK Viewdata system even to the extent of using the same model of computer, are not so great. But until the question of whether viewdata, or *Bildschirmtext* as it is

*G.E.C. stand was host to journalists producing Bildschirmzeitung, a teletext service run by newspaper publishers. Publishers want to run teletext in Germany, but how they can achieve this is still not clear.*

called, is purely telecommunications – the Bundespost argue it is a federal matter as the telephone is used – or whether it is also a broadcasting matter, the German post office are not allowed to operate a full service. "In strict adherence to the principle of fair network utilization," said Bundespost executive Theodor Irmer at a press conference, "the post office has expressly refrained in its demonstrations from the reproduction of any information having a content which has not been legally established as germane to the medium".

A Viewdata trial is starting immediately after the exhibition, the basis of which, Herr Irmer later explained, was that it will use "bilateral" information only in a non-public way up until 1980, when it is hoped the issue will be resolved. This phase will be followed by a field test for 2000 private subscribers, in effort to get answers to the questions of who wants to know what and when, and who will provide input, by 1982 when it is hoped a full public service can begin.

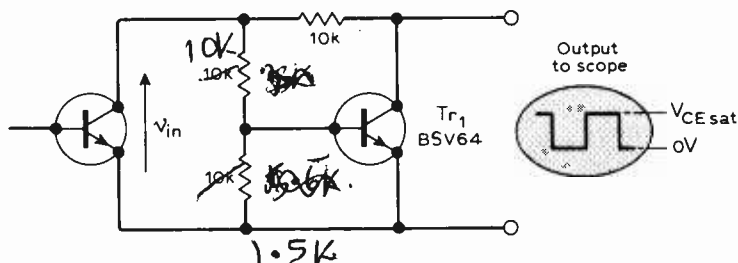
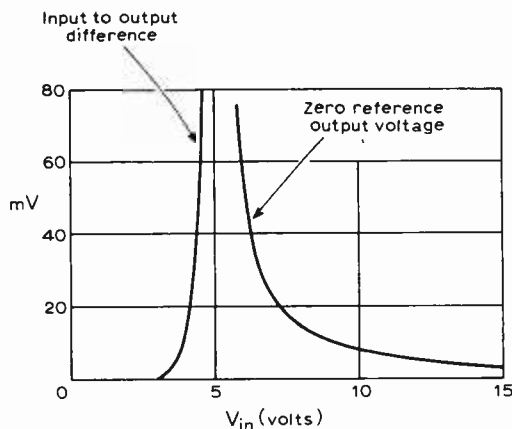
On August 23, a "substantial" contract between the British Post Office and the Bundespost was announced in which the Bundespost gets a duplicate of the Viewdata programme and expertise (they already have an identical computer). Under the contract, the technical information passed on by the Bundespost to German electronics firms is restricted for use only in Germany for the next three years, and German firms are not permitted to compete with British firms in exporting Viewdata equipment to other countries until after March 1980. This is unlikely to worry the German manufacturers, as it's highly improbable that there will be any large scale use of Viewdata before then. even in the U.K.

# Circuit Ideas

## Measuring $V_{CE\text{SAT}}$ in power transistors

To determine the saturation loss in power transistors it is necessary to measure the saturation voltage, which may be about 1 to 2V. The measuring circuit must also accommodate the high collector voltage which is present when the switching transistor is in the off state. A problem therefore arises if a d.c. coupled oscilloscope is used as it is often difficult to obtain adequate voltage resolution without overloading the deflection amplifier during the off state of the transistor. Furthermore, a very small disparity between a.c. and d.c. gain in the deflection channel can lead to a substantial error in the apparent saturation voltage.

The circuit shown is inserted between the switching transistor and an oscilloscope which may then be a.c. coupled. Output to the oscilloscope is a rectangular waveform with a low voltage state representing 0V and the high voltage state being the transistor



saturation voltage. Errors in the circuit are typically less than 10mV, and may be established by d.c. measurements if desired. Accurate measurements of saturation voltage may be made simply by reading the peak to peak voltage of the displayed waveform. When the collector voltage of the power switch is below 4V,  $Tr_1$  is non-conducting. During the off state of the switch, its collector voltage is assumed to be greater than 10V in which case  $Tr_1$  is

heavily saturated and the zero reference output is typically less than 10mV. Note that  $Tr_1$  is a large-chip transistor operating at low collector current. The same technique may be used to drive an integrating wattmeter which, by sampling collector current, will show saturation power loss directly.

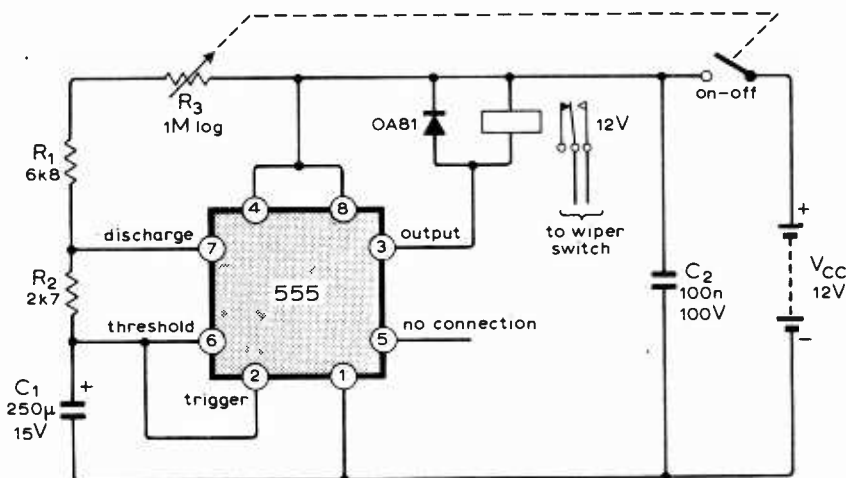
D. R. Boit,  
Charlwood,  
Surrey.

## Windscreen wiper controller

The delay between successive sweeps of self-parking wiper blades can be altered by a single variable resistor. Any delay between approximately three seconds and three minutes can be obtained with the values shown. The wiper blades can easily be made to perform two or more successive sweeps between the delays instead of one double sweep. When the delay is set to the minimum value, the wipers operate almost continuously.

The relay contacts are connected across the existing wiper switch and merely override the existing controls.

J. B. Dance,  
Alcester,  
Warwicks.





## Resistance-capacitance meter

This circuit was designed as an addition to a six-digit frequency meter in which gate 5, with its following counters, drivers, and display, forms part of the instrument. It displays resistance in ohms up to  $1M\Omega$  or capacitance in pF up to  $1\mu F$ . Gates 3, 4, 5 and the b.c.d. counters etc form a 200kHz stop-watch which is started and stopped by negative-going pulses at gate 4 and 3 respectively. Reset is achieved by

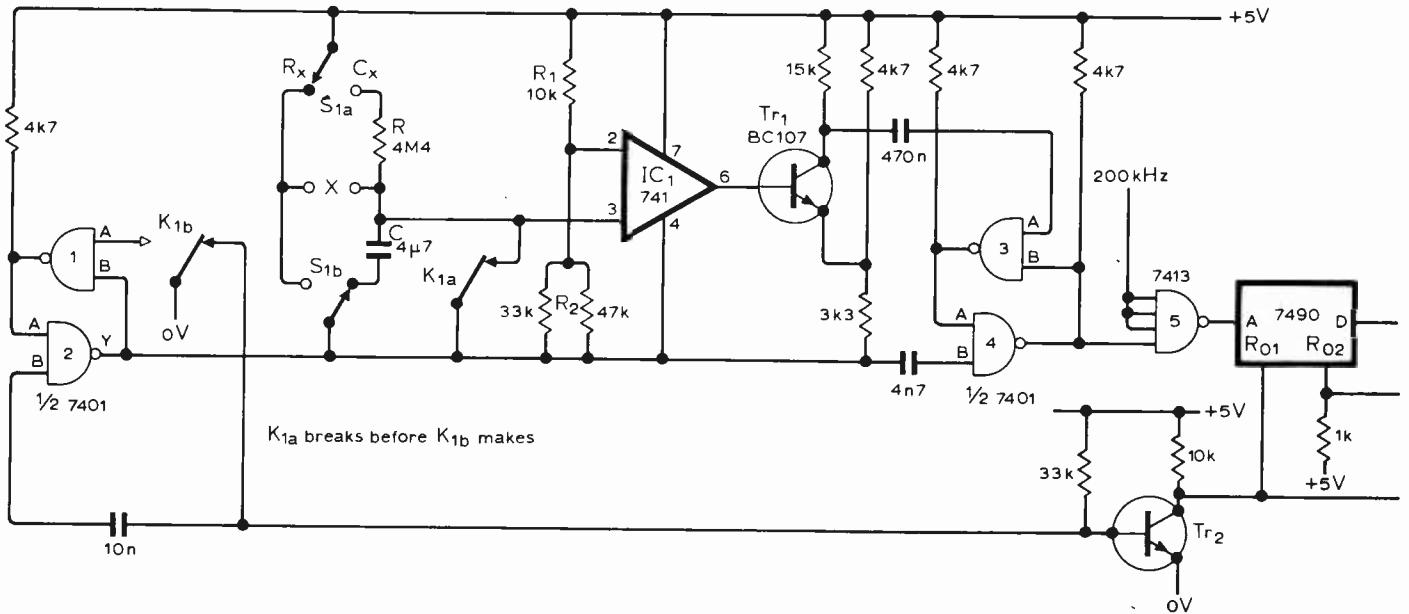
applying a zero at the base of  $Tr_2$ . Resistor  $R_x$  or capacitor  $C_x$  is connected in series with capacitor  $C$  or resistor  $R$ , according to the position of  $S_1$ . When  $K_{1a}$  is normal, the output of gate 2 is high,  $C$  is short-circuited,  $IC_1$  and  $Tr_1$  are off and the counters are reset by  $Tr_2$ .

When operated,  $K_{1a}$  removes the short from  $C$ , and  $K_{1b}$  removes the reset condition from  $Tr_2$  and applies a 0 at gate 1. Gate 4 receives a 0 from gate 2 and starts the stopwatch. Simultaneously,  $C$  starts to charge via  $R_x$ . After time  $t = CR_x \log_e (R_1 + R_2)/R_1 =$

$1.065CR_x$ , the voltage at  $IC_1$  pin 3 reaches that at pin 2 and the output goes high. Transistor  $Tr_1$  then turns on and a negative pulse to gate 3 stops the timer. The meter, having counted 200kHz for  $t$  seconds, displays the value of  $R_x$  or  $C_x$ .

Although there are small errors developed in the circuit when measuring an unknown resistor or capacitor, this simple design is a useful addition to a frequency meter.

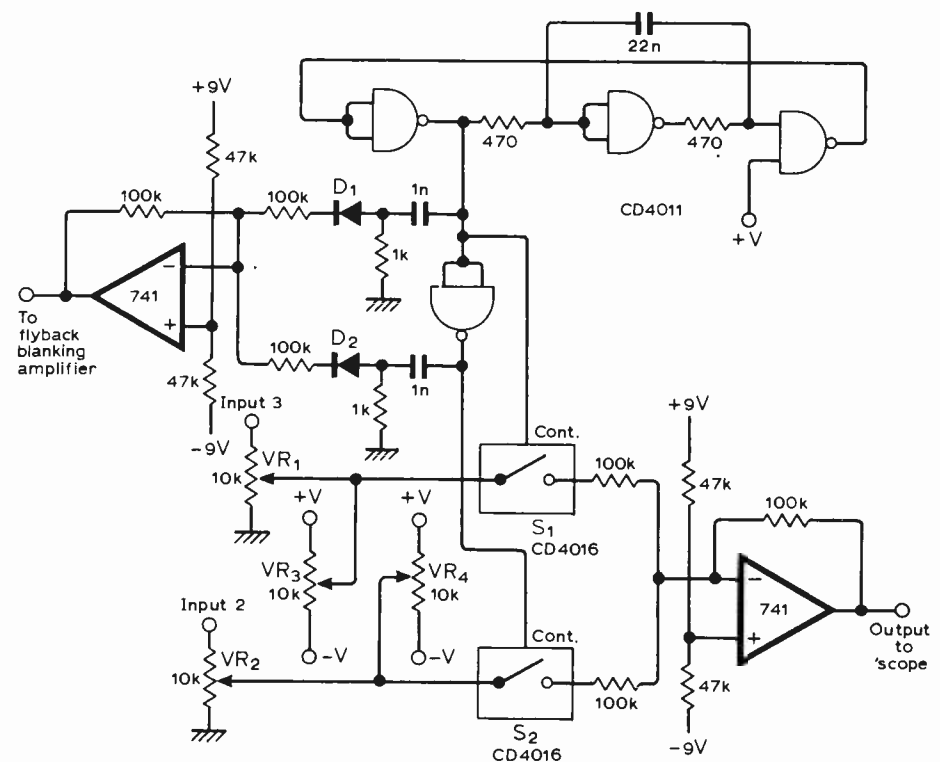
G. Jackson,  
Creigiau,  
Cardiff.

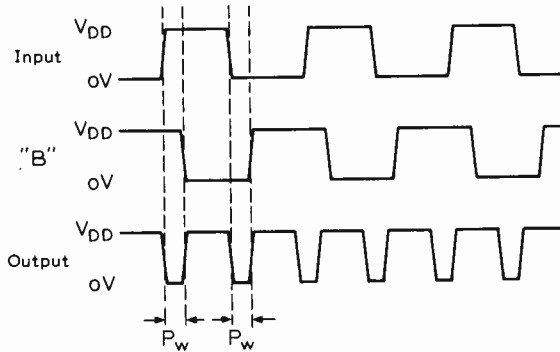
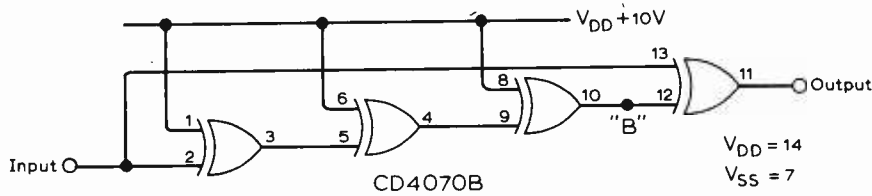


## Oscilloscope trace doubler

The 4011 forms an astable oscillator with a frequency of 53kHz. Two out-of-phase pulse trains are fed to the 4016 which alternately switches two inputs into the unity gain mixer amplifier. The output of the 741 is then fed to an oscilloscope. Input levels are controlled by  $VR_1$  and  $VR_2$ , and the position is controlled by  $VR_3$  and  $VR_4$ . The remainder of the circuit is used to blank the beam between sweeps by differentiating the oscillator outputs to produce spikes. Positive spikes are then mixed and inverted by the 741 which drives the flyback blanking amplifier.

J. S. Paterson,  
East Lothian,  
Scotland.





### Change-of-state detector

A conventional change-of-state detector uses the OR'ed outputs of two monostables triggering from opposite polarity edges. This circuit uses only one exclusive-OR gate i.e., and performs frequency doubling or change-of-state detection. The first three gates are connected as buffers and the final gate exclusive-ORs the output of the buffers and the input. An output pulse of width equal to the total propagation delay of the buffers is obtained, in practice about 100ns, from the CD4070B. This pulse may be extended if necessary by the addition of a <math>< 5\text{nF}</math> capacitor from point B to ground.

If the line shown tied to  $V_{DD}$  is connected to  $V_{SS}$  instead, the output polarity is inverted.

S. Roberts,  
Sheffield.

### Audio overload monitor

This circuit uses two of the four comparators in an LM339 package to provide detection of excessive positive or negative signal peaks. Pulse-stretching is used to ensure that a clear indication of short-duration peaks is given. Bidirectional peak measurement is important as positive and negative peaks may vary by up to 8dB.

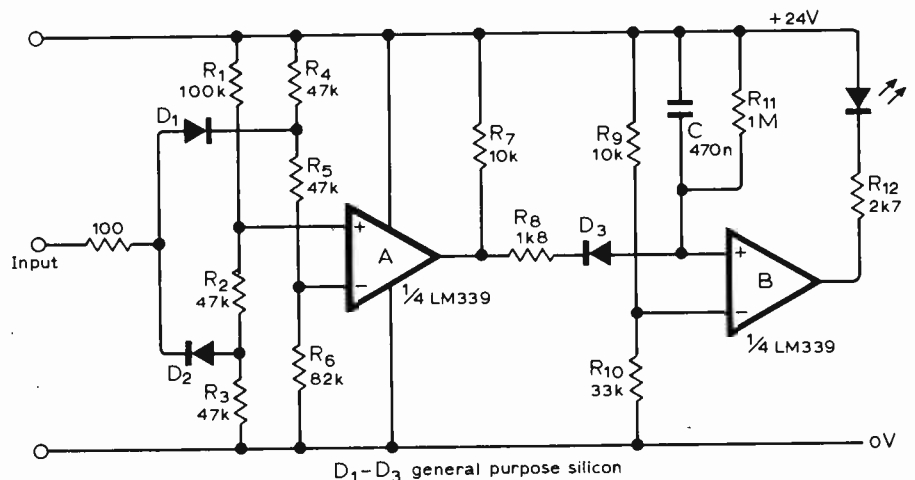
Comparator A detects peaks of either polarity, and the two potential dividers hold the inverting input 400mV below the non-inverting input. If the audio input exceeds the trip point on a positive peak,  $D_1$  conducts which pulls up the inverting input and causes the comparator to change state. Likewise, a suitably large negative peak will make  $D_2$  conduct and pull down the non-inverting input, again causing the comparator output to go low.

When output A goes low, storage capacitor C charges rapidly through  $D_3$  and  $R_8$ . When the peak is past, C remains charged and keeps the output of comparator B low so the l.e.d. remains on. The output goes high again after C has discharged through  $R_{11}$ , and the l.e.d. is extinguished.

With the values shown, the circuit trips at a peak level equivalent to a 5V r.m.s. sine wave. This is 3dB below the maximum voltage swing to be expected from an amplifying stage operating from a 24V rail. Note that the circuit should not be driven from a high impedance point because the diodes may cause distortion.

A stereo version may be conveniently made using a single LM339 package.

D. Self,  
London E.17.

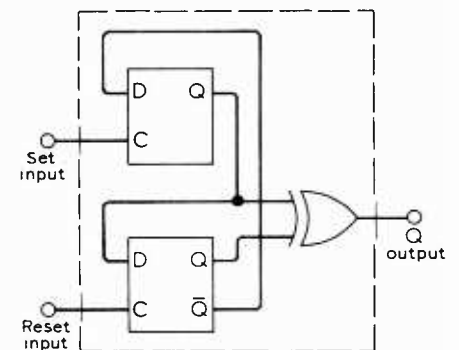


### SR flip-flop

Using a c.m.o.s. dual D-type flip-flop and one exclusive-OR gate an SR flip-flop may be made which is triggered by a positive edge on either input, irrespective of the level of the other input.

A positive edge on the set input will force the two flip-flops into opposite states and hence one input to the exclusive-OR will be a 1 and the Q output will be a 1. A positive edge on the reset input will force both flip-flops to the same state, the two exclusive-OR inputs will be equal and the Q output will be a 0.

K. Dillon,  
Epsom,  
Surrey.



# News of the Month

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## OTS failure: "no sabotage"

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Those involved in the Orbital Test Satellite (OTS) project are adopting a philosophical attitude to the rocket failure that forced NASA control to destroy the craft seven miles above the launch pad. Nasa Engineers are still investigating the failure of the September 13 launch, but their report may be delayed if, as some suspect, the McDonnell Douglas Delta rocket turns out to be suffering signs of age or, as a Hawker Siddeley Dynamics spokesman put it, "shelf-lifing".

When Geos went wrong (WW August p.33) experimenters were quick to point out that it was suspicious that so many failures had lately coincided with European projects. That may be because ESA had not insured the scientific projects, and so the loss to those involved was that much harder to bear. The comparative cheerfulness of the OTS workers may be because ESA had decided, since the satellite was its first applications project, that it should be insured. An ESA spokesman told *Wireless World* that the \$30 million price tag included "the integration and launch of the second flight, so the relaunch will cost ESA nothing". An earlier report in *The Times* had quoted Dr Roy Gibson, ESA's director general, as saying that although the rocket and launch costs were insured, for \$17 million, the satellite was not, and a spokesman for the prime contractors, Hawker Siddeley, part of British Aerospace, agreed; their contract was worth £25 million, but this includes some work on the back up satellite.

ESA point out that the Delta launcher's success rate is over 90%. The OTS launcher, code named Delta 124, was the third launch of a Delta 3914, and the 3914's first failure. There are two possible causes: either a fault in one of the nine strap-on Thiokol solid fuel booster rockets, or a leak in the liquid oxygen tank of the first stage itself.

A new timetable will not be set until

the results of the NASA enquiry are known, but engineers expect the new launch date to be between February and April next year. The accident is not expected to affect seriously the European Communications Satellite programme which OTS was to have forerun, and which was to compete with communications projects by American firms like Hughes and Aeronutronic Ford. Had OTS been successful, a Hawker spokesman said, "it would have given us credibility, but we can't identify any more concrete effect than that."

ESA said: "If OTS could be launched in about April '78 we don't think that would affect the communications programme. The main aim of OTS was to test the system due for launch in 1980 and this is just a six month delay. So if we work a bit harder we could still launch the 1980 project on time." It also appears that some of the markets the contractors were hoping to sell to, in Brazil and the Middle East, are having delays of their own, either for financial or organisational reasons.

As to sabotage, mentioned in some reports of the accident, Hawkers will say nothing publicly other than that it would have tarnished the reputation of

Nasa and the Americans, and given greater credibility to the Ariane launch vehicle which will launch the ECS programme in 1980. ESA concur: "The rocket until now was going all right. It's bad for NASA, as well as us, bad for their image, and for McDonnell Douglas's marketing. No-one benefits from this."

The Panel investigating the failure are: George Hardy, manager of the Space Shuttle solid rocket booster project at Marshall space flight centre; Henry Plohr, associate chief of the space propulsion and power division, space systems and technology directorate, Lewis research centre, Cleveland, Ohio; Ison Rigell, Space Shuttle payload director at Kennedy centre; Alton Jones, deputy director of engineering, Goddard space centre, Maryland; Joseph Thibodaux jr, chief, propulsion and power division, directorate of engineering and development, Johnson space centre, Texas; Haggai Cohen, director, reliability, quality and safety, Nasa HQ, Washington; Harvey Herring, metallic materials division, materials and processing lab, Marshall centre; and observers appointed by the air force and ESA. The panel's first meeting was on September 16.

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## Consumer men split over controls

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British leaders of the consumer electronics industry were recently given a good-natured but firm dressing down over their advocacy of protectionism. Mr James Goodson, vice president of ITT Consumer Products, told retailers and manufacturers at the Radio Industries Convention on September 14 that they should be directing their energies to the industry as such rather than to countering the imports from other countries, notably Japan. Speaking of the increasing threat of foreign imports he said: "Of course it's not fair. I'm not sure that the solution, however, is to go to the government. We can't expect help from governments. We have to get our own house in order regardless of what competition does and regardless of what governments do. . . . The answer isn't going to Whitehall to ask for protection. The attitude should be to build this industry into what it can be, to ask which is the greatest promoter and catalyst of technological progress in world trade. The options are absolutely unlimited."

It was a mistake to think that the best way to beat the competition was to cut corners: "The answer is not to make things cheaper, to cut costs. It's to put a few bells and whistles on the thing and sell it for a higher price."

On quality control he said: "The boys and girls on the line are the quality control. The Japanese don't need quality control because they think that's a duplication of effort."

On industrial relations: "Industrial relations is a question of motivation of effort. The Japanese have motivated people to the point where they feel it's their company."

On investment: "I do believe investment is the name of the game, spread over various countries and over various activities."

On protectionism: "If England starts cutting imports then they start cutting imports from the UK. We believe in free world trade so let's believe in it. Let's do our homework right, get our quality right and get the right features."

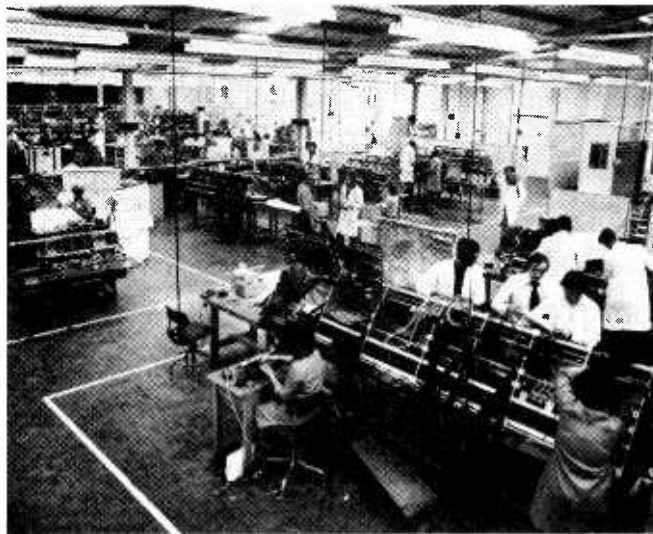
Mr Goodson appeared saddened by the willingness of the industry to face both ways. Earlier speeches had attacked the Government for even considering Hitachi's proposal to build a factory in Washington, Tyne and Wear, and for manipulating VAT rates to regulate demand without considering the consequences on the consumer industries involved. "We're been suffering from years of government interference," said Thorn chairman Sir Richard Cave. Yet he continued by saying: "The private enterprise system we all believe in and free trade all over the world don't seem to have worked very well for the tv industry . . . We do support free world trade. We don't believe the Japanese do. We see they can and do in times of world economic difficulty build up substantial world balances. Why? The answer is that if free world trade was encouraged in

Japan as it is in Europe, would it be possible for them to achieve these results? The answer must be 'no' . . . We must either expect proper free trade to take place in Japan or we must realise that this is not happening and we must impose restrictions . . . We have got to go on lobbying government and explaining the position to them."

Mullard managing director Jack Akerman's view of his own industry was bluntly put: "The state of the British components industry is not good. In fact, if the lady at the back will forgive me, it's bloody awful." Ninety-two per cent of i.c.s, up to 75% of transistors and 60% of such components as capacitors were imported, he said. In view of the massive investments being made in l.s.i. manufacture being made in France, Germany and particularly Japan (£500 million over the next three years), the £25 million of government help for the industry was very small: "We're going to need to spend a lot more than that. We can't afford to go it alone." His proposal, echoed by other speakers, was for Europe to make joint efforts to defeat the Japanese and Americans. The electronic home, based around the colour tv set, Viewdata and teletext, would be here "in the late 1990s", and the industry must make ready for that.

Later James Goodson remarked that he had to disagree with that estimate. "It isn't the latter part of the 1990s, and even if it were we would have to accelerate it . . . If you wait until the late 1990s then everybody will leapfrog you."

Mr Akerman was not entirely gloomy. Apart from predicting a



Neve's new 20,000 ft<sup>2</sup> factory at Melbourn, Cambs, was opened by Mr Francis Pym MP, on September 20, and visited by the Duke of Kent the following week. Neve's turnover has quadrupled in five years and they now export over 75% of production. Recent orders went to Capitol Records, Sydney Opera House, Austrian Broadcasting (ORF), Kuwait, Iran, Citroen cars and Jacques Loussier's Miraval Studio, both in France, and Stockholm's Polyvox studio.

glowing future for developments based on Viewdata and teletext, disagreeing, incidentally with the view that teletext would "fade away" as Viewdata came into general use, he said: "Our strike record is good and the workforce works extremely well." He also noted the view that British manufacturers would not sacrifice short term profit for long term advantage, where the Japanese planned and invested 20 years ahead. "This," he added, "is at the root of our problems."

Not so cheerful was Dr Ian Mackintosh, of the firm of European electronics consultants, who said that, for example, his firm had predicted the large rise in the music centre market, which had caused falls in other parts of audio,

three years ago. "It's sad that people didn't pick it up in time . . . The music centre boom was more clearly foreseen and acted upon by the Japanese than any other national producers in the world." He also asserted that "the development of Viewdata and teletext owes as much to our entrepreneurial public corporations as it does to industrial companies . . . I fear there will be a further slow deterioration in Britain's ability to compete, and when in ten years' time the Japanese have made the same inroads into your market as they did into the American market, ten years ago, then I think my company may be asked to conduct a post mortem into what went wrong."

## Doppler men fighting for m.l.s. decision

No agreement on an international microwave landing system (m.l.s.) is expected before May next year, but the British Civil Aviation Authority is conducting a campaign to make sure that the British Doppler system wins (See *Wireless World*, May 1977, p.66). The latest in a series of tests took place at Gatwick at the end of August, when a Royal Aircraft Establishment HS748 made five consecutive automatic landings on runway eight using a Doppler m.l.s. alongside the existing instrument landing system (i.l.s.). The Department of Industry, in a statement issued on behalf of the CAA, said they were "The first ever automatic landings at an international civil airport."

The trials have been conducted jointly by the CAA, the Department of Industry, the Ministry of Defence and Plessey, who are developing the system. After an abortive meeting of the All Weather Operations Panel last May, at

which Britain abstained to show disapproval of the way the decision was being reached, the various protagonists went away to muster more information. The International Civil Aviation Organisation, and some of the countries represented, including Britain, felt that it was improper that the panel had tried to reach a decision when so little information about the competing systems was available. This accounted, they say, for the rather strange voting pattern.

The Americans assumed the aggressive and produced a computer simulation of conditions at Brussels airport which claimed to prove that the British system would not work there while the American time-reference scanning beam (t.r.s.b.) would. The British went ahead with their series of trials, which they hoped would refute the American evidence, and show that the Doppler system would work in various environments.

The British installed a system at Brussels, with the co-operation of the Belgian authorities. It seems that the British system worked, and that the Americans had fed incorrect data into their simulation: according to the CAA, they had put in a building that doesn't exist at Brussels airport. Learning a lesson from the Decca Navigator's failure to beat the American enroute navigation system many years ago, the CAA then took the gloves off. Until Brussels, they say, they had kept an open mind: "If it were proven that it was better than the British vote would have gone to t.r.s.b." But when the one month trial at Brussels came to an end this summer the view was that "We have now proved that the Doppler system is the best system."

After that "We adopted tactics which would never have been dreamt of in the 1950s. We had the Russians over here, for example, and showed them every nut and bolt on the thing." In doing this the British were willing to run the risk of the severe disapproval of other countries since the Russians had

shown favour towards a German scheme based on the existing system, though it is no longer thought a serious contender.

The next step is to take the Doppler equipment to Norway as an example of what the system can do at airports whose terrain makes them "troublesome". When the Air Navigation Commission which set up the All Weather Operations Panel reports to its parent, the ICAO council, in May 1978 the decision will, it is hoped, be a foregone conclusion, avoiding the wrangling that has so far caused delays. And the CAA hopes they will have enough evidence to show that the t.r.s.b. is too expensive and inflexible to be adopted.

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## System X stirs

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The Post Office's announcement of contracts worth £20 million for System X development, though following closely the criticisms by the Carter committee that the Post Office had been too slow to press ahead with the system, do not appear to be a response to those criticisms. After preparatory work which, they say, involved 500 engineers, the Corporation had merely reached a point where they felt ready to move into the next phase of development.

The orders are for the design of electronic trunk, tandem and small to medium capacity local exchanges. System X will be based on a number of sub-systems or modules which includes: stored program control (s.p.c.) processors; digital switching modules which interconnect digital circuits connected to the switch; signal interworking modules, used on calls to existing exchanges; A/D and D/A convertors; message transmission modules to transmit control and management information between s.p.c. processors in different exchanges.

GEC will develop the digital trunk and small to medium local exchanges, and the s.p.c. processors; System X will be based around the GEC 2BL processor. Plessey will be responsible for digital switching, signal interworking with existing exchanges, A/D convertors, network timing and synchronisation, and maintenance and exchange management software sub-systems, all for the Tandem exchanges. It is believed that Plessey's seven contracts are worth some £10 million of the £20 million total and will employ around 80 people each at Liverpool, Taplow and Poole by the end of next year.

STC will develop the message transmission systems which connect the exchanges' computers and form the data network which carries control and signalling information. STC also have a contract to develop the local administration centre monitoring and logging information on a network of exchanges.

"Typically," say STC, "a centre will administer such tasks as recording maintenance information, keeping statistics on telephone traffic and recording call charges."

The Post Office say a large supply programme based on System X will begin in the 1980s, reaching a total of £100 million, though this will produce savings in capital and operating costs. The Post Office also emphasises that the three companies involved should be able to sell System X-based exchange equipment abroad. One supplier noted that the Post Office seemed more aware of the need for the telecommunications companies to make exportable equipment, as a result both of the Carter criticisms (WW September, p.72) and the strongly expressed views of the companies themselves.

News of the orders follows some delay in placing the contracts. In November 1975 the *Financial Times* reported that about a dozen major contracts were about to be placed but nothing has been heard until now. The entire development programme will cost at least £100 million of which between £50 and £60 million is to be spent on development work outside the Post Office. This leaves roughly £30 million unaccounted for, although some contracts, notably for the processor, have already been placed. A large part of the missing element will concern the large capacity local exchanges.

Another element missing from the present equipment is transmission equipment. The contracts just announced are largely for modules and

control functions, with the smallest number of the just over a dozen contracts, perhaps a couple, going to STC, who are dealing with some of the transmission development. Even then, according to a report in *Electronics Weekly* STC will not be required to produce hardware when the first prototypes emerge in 1979. The Post Office say, however, that many orders for digital transmission equipment have been placed over the last few years, though they have not been linked with the development of System X.

Another sidelight on the project is that Pye TMC, who recently installed electronic directors for the Post Office (WW September, p.73) were not offered any of the contracts. One reason for this is that they have not been involved in switching for as long as the other three and the big three companies have said in the past that Pye could not be included in the programme because, as a subsidiary of Philips, they could be in competition with their own parent company.

This ignores the fact that STC is a subsidiary of ITT. Pye have also a long history of supplying the Post Office, notably in telegram retransmission and 60MHz transmission equipment. Without doubt the big three, who were first on the System X scene, feel that there is little enough to go round without a fourth party sharing the contracts.

However, that may be the final form of System X is still unclear, and it will remain so until the Post Office decides to give the project a name.

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## Libya buys British

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Libya's £9 million order with Marconi for fast tuning systems at Tripoli and Benghazi airports, one of the largest ever, say Marconi, for civil aviation communications equipment, is but the latest in a series of orders that the Socialist People's Libyan Arab Jamahiriya has placed in Britain. In June Marconi announced one £3 million order for tv cameras, telecines, vision mixers, OB vans and other equipment, and another worth nearly £½ million for radio equipment for the Arab Revolutionary News Agency. Marconi had already supplied the news agency with its original equipment in 1974.

More surprising, though, in view of Libya's export of arms to various terrorist groups, including the IRA, is that our own Post Office should be helping the Libyans set up their telephone network. The consultancy contract, also announced in June, was worth £6.75 million to the BPO, and followed one a year before worth £650,000 to help build the telephone link between Tripoli and Benghazi. Such trade is usually excused on the grounds

that communications equipment is "neutral" and the way it is used is none of the supplier's business. Even if it were not neutral, the argument goes, someone else would supply it, otherwise any less distasteful regime than that of Colonel Gaddafi would find itself without vital parts of its infrastructure.

Our dependence on Libya for oil is now decreasing. Last year we imported only £128 million of our £4.3 billion oil imports from Libya, compared with roughly a third some years ago, but the Marconi statement emphasises "the rapidly increasing importance of Libya as the gateway between Europe and Africa." The country is "of paramount importance for the future development of civil aviation in the area." Clearly exports to Libya could lead to substantial sales in other parts of Africa.

The present Marconi contract is for four communications services for the two airports: access to the aeronautical fixed traffic network to provide long distance speech and teleprinter links to flight information centres in North Africa and the Mediterranean, an

aeronautical mobile service for ground to air speech traffic, a search and rescue communications service, and facsimile and teletype links between meteorological centres.

Two types of Marconi fast tuning transmitter will be used, the 1kW H1040 and the 10kW H1140, both powered by the H1540 synthesised drive. All the receivers are type H2540. Marconi say the aeriels they will supply at Tripoli will be among the most complex they have ever installed, including resonant and wideband dipoles, single and double rhombics, confians and directional and omnidirectional, fixed and rotatable log-periodics.

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## New tv game generation by Christmas

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Predictions about the "electronic Home", based around teletext and Viewdata, are now falling thick and fast and some of them are quite surprising. Those concerned with Oracle, for example, are now trying to play down a prediction made by Mr George Cooper, Oracle's chairman, at a press conference to announce the service's expansion from updating 42 hours a week to 90. He foresaw "a national air call service with small pocket sets."

Each set would have a code, and when the code for a particular pocket set were transmitted, the set would emit a bleep. Using the broadcast network, a set could be called anywhere in the country, and the user would then telephone a pre-arranged number.

Since press reports of this have appeared the IBA have been flooded with phone calls asking where the beepers can be bought, and of course the service, if it overcame the inevitable opposition of the mobile radio and paging lobby, wouldn't start until well into the next decade.

EMI and General Instrument Corporation have jointly applied for patents for a technique for storing up to 1.6 million bits on each side of a C60 cassette. GIM are to sell an electronic interface which can be used with standard cassette recorder heads to carry out data retrieval and error correction. The interface is to be part of a complete programmable television terminal microcircuit chip set, and GIM and EMI will collaborate in developing computer programs and voice and data cassettes which will be sold in tape and record shops.

GIMs decoder for teletext and Viewdata already contains a microprocessor, and they say they are developing a set of compatible m.o.s. circuits for interfacing the tv set with their CP1600 microprocessor family. These interface circuits could offer a wide range of extras to the standard tv culminating, say GIM, in a complete home computer system. The interfaces can decode teletext and Viewdata and the cassette mechanism can be connected through them to play back tv games and educational programs.

GI say the first of the home hardware will be available next summer, and EMI will make cassettes available for manufacturers to sell under their own names.

EMI say they have abandoned traditional error correction techniques to enable data to be stored on conventional audio cassette tape. The new method of error correction is to cope with dropouts which could otherwise destroy large chunks of data. They have not given further details but they say that very roughly 50,000 bits can be read from the cassette in 26s. EMI say they have duplicated the cassettes "above real time" without difficulty.

The new technique is necessary because of the use of ordinary audio tape, which is cheaper, and can store both data and sound through an ordinary mechanism and electronics. This makes the educational, language tuition

and programmed learning market a natural target, with spoken commentaries matching text as it appears on the home TV screen.

EMI's target for the price of the hardware is between £100 and £200. When the first games appear on the American market next summer, probably five-move-ahead chess games, they should sell for around \$5, a quarter to a third of the price of the equivalent r.o.m. cassette.

The r.o.m. plug-in cassettes will be on sale in Europe by Christmas. These are the next generation referred to by a new Mackintosh report. NISC examples by Fairchild, RCA and Otari were seen at the Chicago Consumer Electronics Show this year.

From next year GI begin to supply chips to manufacturers wishing to serve the home data market and EMI will supply the programmed cassettes. The competition in the home data market is now fierce and bound to become even more so. One familiar problem may crop up yet again, that of standardisation. This is not just a matter of which physical links to use in the system. If cassettes don't sweep the board the 16K r.o.m. attachment and associated electronics could be combined with a cassette mechanism to give the user the greatest benefit from his equipment. What is important is that the data contained in a r.o.m. can be understood by that on a cassette. The data will have to be in a common data "language", and it may be that, since the Post Office has a great influence on such matters in view of the importance of Viewdata to the whole idea, the programming language may be one that suits the Post Office. But what about the rest of the world? EMI stress they don't want another standards battle.

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## News in brief

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Soviet Scientists at the Lebedev Physics Institute, Moscow, claim that they have used a laser to move a 20,000 cm<sup>3</sup> helium-filled balloon. The laser operated on carbon dioxide and had an energy of "a few kilojoules". Laser pulses pushed the balloon to speeds of up to 2m/s, each flight lasting about 30s.

In April next year GEC is to deliver £2 million worth of 30 channel p.c.m. equipment to the Post Office, the largest order, they say, since the tests on a trial link between Liverpool and Formby were completed. The equipment will carry telephone and data signals. GEC are also designing interfaces between p.c.m. links and exchanges.

We have had a number of enquiries about part three of "Multi-system ambisonic decoder", by Michael Gerzon. The publication of this article has been delayed but we will publish it as soon as we are able.



*Mr George A. Cooper, chairman of the Oracle board of Independent Television, announced an increase in the number of hours during which the service would be updated. It is now, like the BBC Ceefax system, updated seven days a week. See "Electronic home".*

# Harrogate: the turntable war

The disc is one old contemptible that shows no sign of ill health

In the 100th year of sound reproduction Edison's original idea—a point thrown about in a moving groove — is still here, and even gaining ground. Why else would so many manufacturers still be introducing new turntables?

This might, of course, be interpreted as a sign of the disc's imminent demise: when the transistor became easy to get the valve improved astoundingly, and some of the turntables shown at Harrogate this year have become almost absurdly sophisticated. The disc, too, shows signs of improving to match the lack of breakfast noise that makes the cassette so attractive despite its disadvantages. A number of demonstrations at Harrogate used direct cut discs, a development whose results are very spectacular, but which a combination of its inconvenience to the studio engineer, who has come to rely on tape, and recording industry economics will prevent from coming into general use. Another disc development, the p.c.m. recording, is much more likely to succeed, though even here the improvement in sound quality is not one which addresses the main complaint about records. If music enthusiasts are turning to tape it is not because they do not like the tape hiss on records. The other improvements direct cutting brings do not compensate for the irregular intrusive noise caused by dust and scratches.

Perhaps that is why Garrard have sought to protect their turntable market by launching a scratch suppressor. It is interesting that they should do this just as they say they have established "a foothold" after a year in the cassette player market, and it would seem to show that the record market is still worth protecting. That market does not make Garrard reliant, as cassette players might, on buying mechanisms from abroad.

The scratch suppressor appears, on a brief hearing, to be very effective. The amount of suppression is continuously variable. It will be available towards the end of this year for just over £100.

Garrard have launched three new turntables this year, all the result, they say, of extensive market research. Surveys of this kind have been an easy



*Garrard's direct drive DD75, introduced last year. It has pitch and off-arm bias controls.*



*Thorens TD126 mk2. Note the straight arm and the 78 speed on the left. Like many of the turntables shown at Harrogate, this has a variable pitch control.*



*Trio's new KD2070 direct drive unit.*

target ever since the Ford Edsel, and it is little help to repeat Lord Reith's dictum that if you give people what they want they will want what they get. Garrard say their research has established that the punter wants an S-shaped arm, die-cast platter, a wood and metallic look, an acrylic dust cover, and an anti-static mat. So far so good, but it's a little worrying that Garrard should have been quite so ready, as they admit, to over-ride their engineers, who had good reason to object, for example, to plug-in headshells. It is sometimes better to temper the poll arithmetic with a little common sense. Does the product work, and is it well-finished? Some informed observers think Garrard haven't yet got it quite right, but it is good to see the new Garrard, under Derek Moon, keen to do battle with foreign competition.

Garrard's research also seemed to show that parallel or tangential tracking arms are not popular in the UK. Such an arm, which they were to sell here, is now available only in the United States, and may even be withdrawn from there. Yet **Revox**, who don't have a strong image outside the tape market, choose to launch themselves on the disc tide with a radial arm. It won't be available until early next year, but the prototype demonstrated at Harrogate performed very well even when thumped or tilted severely. The platter uses direct drive.

Some years ago **Strathearn** also launched itself on the turntable market with a parallel tracker. As far as one could tell the prototypes worked beautifully, but they couldn't make them reliably. Now, under chairman Graham Bish, they say they have solved the production problems, though the range is now confined to conventional arms, and intend to sell 30,000 ST4 and SMA2 pivoted arm turntables in the next year with a rejection rate of no higher than one in 100, compared with the more normal three or four per cent. "We only have two bites at the cherry," Bish said, "not three."

Another product Strathearn say they have high hopes for is the planar speaker, which has been seen in a number of forms in the last few years.

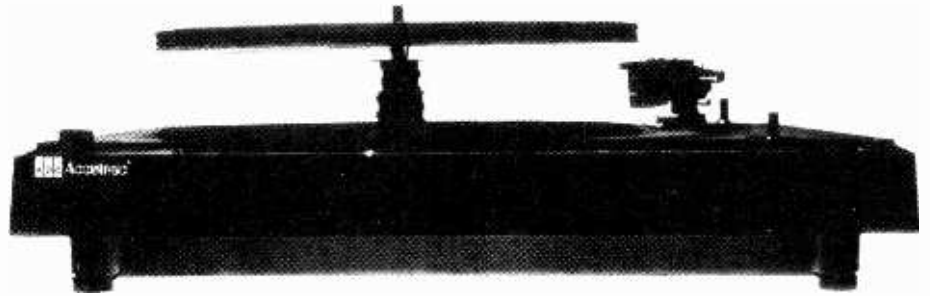
Now it has been separated from its bass units, and the combined mid and high frequency driver can be hung on a wall while the bass cabinet is hidden somewhere behind the furniture. Since bass notes appear to be non-directional the buyer could even get away with one bass unit and two planar speakers. JR's "Super Woofer", to be used with two of their cylindrical speakers, uses the same idea. The Strathearn speaker was demonstrated at Harrogate among an audience that seemed to become more and more enthusiastic.

BSR's new pickup arm also contradicts Garrard's research, since it's carbon fibre and straight. It comes in two versions, with and without plug-in headshell. Thorens, too, have launched a new series of turntables with integral arms based on the principle, they say, that "the shortest distance between two points is a straight line." It also results in lower mass. On the Thorens Isostrack arm the point of connection of the plug-in headshell is near the pivot, also to reduce the effective mass. When you change cartridges you also change about two-thirds of the arm.

The electronic control in the top Thorens deck, the TD126, will allow pitch variations of 6% either side of the three main speeds: 33, 45 and 78, also electronically controlled. Like many of the more expensive turntables at Harrogate, this one has a separate motor to drive the automatic arm functions. In Thorens's case this operates when the increase in speed of the arm towards the middle of the record is detected. To work well this will have to have some pretty complicated electronics. Thorens also make versions of their turntables without arms.

Another comment offered on the Thorens stand was that, "direct drive is a fashionable trend. There's a surge back to belt drive. . . It's not just a one way stream any more." The competing arguments for the two systems were echoed in various forms all round the Harrogate show, the only point of agreement being that the idler wheel or rim drive was out for all except the low fidelity market. Direct drive is not a new idea. According to Thorens, both they and Garrard were using it 40 years ago, and Thorens also say they had a belt drive patent in 1924.

The power behind direct drive is Matsushita, who make many of the motors in other makers' turntables, and there are some who believe that the growth in direct drive turntables, now a tenth of the market, according to Garrard's figures, has been as much the result of a skilful marketing exercise as of any intrinsic merit in the system. Certainly there is so much argument that whoever does have the advantage can't be leading by very much. Thorens say their lab tests have "proved" that belt drive is less prone to rumble. A man on the Pickering stand agreed: "Direct drives were the first turntables made and belt drives were an improvement on



*Silhouette of the ADC Accutrac plus 6, showing the inner platter spiralling up to receive the bottom disc in the stack. This will then be lowered on to the platter.*

them. Belt drive is preferred by the top end of the market, those who are interested in music, and not just buying because it's expensive." There was an audible difference at the top end, he said, which was "more detailed" on a belt drive turntable. If this is true, about which we make no comment, it may be attributed either to the notching effect, where the platter is driven round in tiny pulses of speed rather than smoothly, as from a synchronous motor, or by hum transferred to the cartridge by stray fields.

But Strathearn's Graham Bish has no doubts: "Belt drive is on its way out, fast. That was very obvious in Berlin. Belt drive is dead."

Along with speakers, turntables are one of the few things that British manufacturers are still selling well abroad, with a few exceptions. Even Collaro, now owned by Philips subsidiary Magnavox, is coming back into the battle with a range of cheap, idler-driven turntables for that part of the market that BSR exploited so effectively. Goldring, too, is back, though they weren't at Harrogate; Gerry Sharp has bought the assets, stock and goodwill of the company, now based at Bury St Edmunds. Connoisseur showed a large range of turntables, all belt-driven. Three-quarters of their production goes abroad.

Some aspects of the record player are changing. On many of them, such as the cheaper Pioneer models, the bias or anti-skating adjustment can be made while the record is playing, instead of lowering the stylus, lifting it, changing the bias, and lowering the stylus again. The thread and weight system seems to be losing ground.

Some decks were beyond the reach of most of us. Harman, now a subsidiary of the Beatrice Food Corporation since Sidney Harman joined the Carter administration, are agents for the Micro Seiki turntable, which costs £400. It is free-standing, having no plinth, and can take up to three arms. It looks, to say the least, distinctive, and, by contrast, the even more expensive Technics SP10 mk2, at £1,000 or so, looks plain. In between is the ADC Accutrac plus six, a

belt-driven turntable which can be programmed to play, in any order, any number of tracks from six l.p.s. The records are gently lowered on to the platter by an inner platter which spirals up through the centre of the turntable, and then they are raised back up to the starting position. The tracks are searched out and counted by a small beam of light which is reflected back to a detector between record bands, and scattered in the middle of bands. The functions can be controlled either at the deck or on a remote control unit, and the player also has a volume control.

ADC have also produced a new range of cartridges at the top end of which is the ZLM, available with an even tighter spec (10Hz to 20kHz  $\pm 1/2$ dB instead of within 1dB) for the lunatic fringe. At the Andromeda stand *Wireless World* was told, "The ADC cartridge is superb. It's the best cartridge here, and we've tried every one."

Another amazing record player was the JVC Quartz-controlled QL10, which uses a digital speed readout, and has an electronic pitch control which adjusts in steps of 1Hz. That costs £680 including VAT. Pioneer's PLC 590 had a fashionable look because there is no stroboscope round the rim of the platter. Pioneer say there's no need because speed is "perfect all the time," but other quartz-controlled decks in their range have strobes.

Andromeda have followed a philosophy of which perhaps Bose is the most well-known exponent, using four medium size speakers instead of one large bass unit. Farnell has the same idea, their speakers use one, two or four 5in. units.

Other underlying trends include the increasing use of separate amplifiers for moving coil pickup cartridges. Room equalisers may be one of the best sellers this year, and that bandwagon is carrying a number of manufacturers, including ADC again and JVC. One of the more notable things about the Harrogate show was the way electronic logic control is making it easier to use equipment, as in the Pioneer CTF1000 cassette deck. And Stag Audio appear to have found an answer to the surround sound system problem. They have an amplifier with a gap in it into which you can plug a decoding module of your choice, and they'll even be offering H matrix models. Perhaps the BBC might like to buy some.



# Letters to the Editor

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## RADAR IN WAR

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May I draw attention to the existence of a historical document of a unique character since it contains accounts of the doings of some 50 RAF ground radar stations in two-thirds of England and Wales between 1 December 1943 and 31 July 1944?

The country at this time was organised into four RAF radar "wings" each having a Senior Technical Officer with the rank of Wing Commander who was responsible for installation, maintenance and operations. Holding this post in 73 Wing I conceived the project of producing a brochure containing reports from official sources of the more important day-to-day work of the stations in defending Britain from air attack, directing our own outgoing and returning bombers, air-sea rescue work and what became probably the most useful work – the plotting of ships in the Irish Sea and North Sea. This was to be a tribute to some 4,000 officers, radar mechanics and operators (women and men) who did the work.

Our surveillance of the sea was a daily routine and involved shepherding convoys, plotting stragglers from these convoys, reporting the positions of individual units of the Royal Navy or ships of the merchant navy, reporting German E-boats which were engaged in attacking convoys or laying mines.

Although classic sea battles occurred, in most cases the E-boats engaged in mine-laying and by virtue of their high speed escaped unharmed. Nevertheless, by reporting their tracks, the naval authorities could send mine-sweepers to clear a channel and warn our surface vessels. Radar saved hundreds of vessels from following wrong courses and proceeding into mine-fields or even sandbanks. (Earlier in the war 400 vessels were wrecked on Happisburgh Sands.)

The brochure contains personal letters of appreciation and thanks from Admiral-of-the-Fleet Sir Jack Tovey (Nore Command), Admiral Sir William Whitworth (Rosyth Command) and Rear-Admiral J. S. M. Ritchie (I/C Liverpool).

All types of stations were involved in the radar activities of 73 Wing, some reporting aircraft, others being engaged in the exciting direction of our fighters against enemy bombers and 10cm "K" stations watching the sea. Before this confidential brochure was issued to our stations the overall work of the wing was generally unknown. Often a particular station was unaware of the degree

that it had helped in a particular operation. Thus the bomber raid on Hull on 19 March 1944, which was repelled with nine German planes shot down, is here recounted by several stations – a triumph for radar. What was originally a morale-building exercise has now become a unique historical account.

The original is officially stamped "Historical Document for Permanent Preservation" but it is now no longer confidential and photocopies may be obtained post free from the Public Record Office, Chancery Lane, London WC2A 1LR, by sending a remittance of £6.24 and quoting "73 Wing in Action" Air 16 – 914.

But for the publicity given by this letter this document would remain unknown in the musty recesses of the Public Record Office.

*John Scott-Taggart,  
Beaconsfield,  
Bucks.*

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## GMT/BST CONVERTER

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I would like to point out that there may have been an error in Mr C. G. Armstrong's Circuit Idea on a GMT/BST converter (August issue, p. 53).

The GMT/BST converter is required to add one hour to the transmitted code. The circuit given will work, but the "hours" converter needs to be a decade, not a binary, device, i.e. 74192 not 74193, since the 193 will only produce a "carry" out of pin 12 at 15-to-16 hours, whereas we need a "carry" at 9-to-10 hours.

So either two 74192s should be used or the hours and 10 hours devices changed over.

Pin 4 of both devices must be fixed at a "1" for the system to work reliably.

*Russell Greenberg  
Totteridge  
London N20*

*Mr Armstrong replies:*

I would like to thank Mr Greenberg for noting the error in my article. It is entirely my fault and a reversal of the types of i.c.s used is sufficient for satisfactory working. In retrospect it would appear I must have paid more attention to a satisfactory working model than to the correct identification of the i.c.s.

A logic "1" applied to pin four of both i.c.s is, of course, correct technique. Being somewhat sloppy I chose to leave the pins "floating" and have found that the system works quite satisfactorily without the need for the additional wiring.

The pole identification of the GMT/BST switch should be reversed, as my original note only intended to identify the function of the switch as a unit.

Because of the time delay between submission and publication of the Circuit Idea it was not possible to state that the NPL have modified their code format to allow an automatic GMT/BST correction. By applying the bit immediately following the first parity bit to the pin 5 of the 7408 and disconnecting the switch the automatic facility is enabled.

*C. G. Armstrong*

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## SURROUND SOUND

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In his letter in the September issue Mr J. E. A. Fison bases his criticism of the stereo compatibility of Matrix H on one transmission. Having listened to several broadcasts, I

have concluded along with Messrs Ratliff and Meares that "images may be localized outside the space enclosed by the loudspeakers". Hence the sound completely fills the front quadrant.

Although 9dB may appear to be a poor figure for separation the phase difference is of the order of 45°. Since the human ear responds considerably to phase at mid band this factor is dominant. In addition, does Mr Fison realise that most stereo sources rarely have a separation exceeding 20dB? A typical pickup will have a separation of only 10dB at the limits of the spectrum. Similarly the acoustic separation when using a coincident pair of microphones is of this order of magnitude.

Mr Fison goes on to condemn Matrix H and praise Ambisonics. Since the two systems are almost identical except in detail how does he expect the 45J system to have a better separation? In listening to Matrix H in stereo I have concluded that in general the image width is satisfactory on loudspeakers and if anything is slightly too wide. Also, when listening on stereo headphones the effect is rather objectionable. For this reason it would be wise to reduce the front sector angle to 45° or less which would reduce the width of the stereo image.

On one point I will agree with Mr Fison. The BBC would be wise to change to 45J which would result in only a minor alteration to the results on H decoders but which would allow for the introduction of a logical and expandable quadrasonic system. I fear, however, that the BBC may dig in its heels.

*R. T. White  
Lancing  
West Sussex*

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## TELEPHONE EXCHANGE TECHNOLOGY

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With regard to your article "Telephones and new technology," in the September issue, I suggest that Mr Dwyer examines his sources of information more closely. I quote from p. 72: "The Post office crossbar system does not use multifrequency signalling, as the foreign market requires." If this is so, then perhaps Mr Dwyer could tell me what I've been working on over the past few weeks. Although m.f. is by no means as venerable as Strowger equipment, or TXK, for that matter, I can unequivocally state that m.f., as an integral part of a Group Switching Centre signalling system, has been in operational use for some years.

I must also draw your attention to Mr Dwyer's glib assumption that there are no common areas between the basic exchange systems in common use. In TXK, (son of Strowger, remember?) interchangeability of components seems to be its main asset. Many of its circuits are, in fact, adapted TXS circuits, the actual electro-mechanical hardware being identical. It is also increasingly commonplace to find adapted TXE shelves mounted in cross-bar racks; (one look inside a sector switching centre will verify the fact).

*A. Graver  
Birchanger  
Herts*

*John Dwyer replies:* The source was STC's submission to the Carter committee, section five, paragraph 20, which STC have rechecked and say is correct. The Post Office at first agreed but, after we had asked Mr

Graver for more details, issued the following statement: "Technically the statement is incorrect in that both TXK1 and TXK4 do not (sic) provide multifrequency signalling facilities (SSMF2 which is the current UK national m.f. signalling system.) However in essence the article is probably correct because the context within which the statement appears refers to export possibilities and here the requirement is for the CCITT R2 m.f. signalling system and m.f. keyphones are not yet provided in the British Post Offices crossbar systems."

As to Mr Graver's second point, if he re-reads what I wrote he will discover that I did not even suggest the five systems had nothing in common.

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## AMPLIFIER DESIGN

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While we do not want to join the present fashion of "knocking" audio amplifier designs, we do feel that we must make two comments, one specific and one general, concerning recent articles and correspondence.

First, Mr Taylor's RIAA pre-amplifier published in the September issue. Mr Taylor states his long-tailed pair input stage operates at a collector current of 90  $\mu$ A per device, which will, with low gain devices, result in a base current of approximately 0.36  $\mu$ A. Owing to the difference in resistance between the 47k $\Omega$  resistor and the parallel cartridge most of this current will flow through the cartridge. If one now calculates the signal current from the cartridge at an average output of 5mV the current is 0.106  $\mu$ A, a factor of 3.4 less than the d.c. flowing in the cartridge. This must offset the cartridge magnetic circuit and may result in a significant increase in distortion from the cartridge. We wonder if Mr Taylor has consulted cartridge manufacturers on this point.

Secondly, there seems to be an amount of mysticism regarding transient intermodulation distortion and slew rate, which has never been explained as we see it. Any amplifier will have an open loop risetime depending on its open loop bandwidth and roll-off rate. If now under the closed loop condition the amplifier output is required to rise faster than the open loop risetime, the feedback is operating in a manner which speeds the amplifier up. This will result in an increased error within the loop, showing itself as a transient reduction in gain within the loop accompanied by a transient increase in distortion. Ultimately when the error stage saturates, the amplifier hits slew rate limit and its output will go no faster. From the point at which the closed loop output is required to rise faster than the open loop risetime to the point at which slew rate limit is reached, the t.i.d. obviously increases from zero to 100 per cent.

Mr Sundqvist's solution of making the first stage determine the open loop bandwidth is to some extent avoiding the point, as, unless the open loop bandwidth exceeds the audio range, at high audio frequencies, an increase in distortion and reduction in damping factor is inevitable. Thus, wide open loop bandwidth and large internal error capability are necessary, together with low open loop distortion.

A. Dytch and K. Bishop  
Rugeley  
Staffordshire

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## CITIZENS' BAND AND SOCIETY

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Mr Dwyer's remark (*Wireless World*, January 1977, p.36) that a written constitution makes a difference in the adoption of citizens' band policies of the US and the UK is a reminder that the structures of societies make a big difference in the risks that technologies bring. Most of the US was not disturbed much by the blackout and looting of New York, and possibly many chambers of commerce felt it was good news for their growth programmes. The results for the UK of the same thing happening in London would probably be far more catastrophic since London is a governmental centre and a larger part of the country's gross national product. One might want to play with expectation formulae to establish a number and call it a Chaos Criterion, based on a country's currency value, per capita police ratio, number of languages, and other factors to find how many c.b. sets a country might expect to tolerate and not consider threatening to national security.

For instance, the number of cars and the ease of making Molotov cocktails might mean that with 15,000 c.b. sets loose, the South African police would have to contend with an army force more powerful than the tank divisions of the Warsaw Pact. The Soviet bloc may be more secure in terms of one ethnic group being outnumbered, but in terms of the number of languages is even more vulnerable. Since the Soviet bloc is so much bigger and has less economic tension and more recent memories of a major war than South Africa, I would say that its Chaos Criterion would be over one million sets.

The US may have about fifty million c.b. sets in the 1980s. It is also adopting a standard technique for secure encryption of digital transmissions. If such encryption becomes standard on a large percentage of the sets used in the US, the potential for abuse will be staggering. But then, so is the number of handguns.

Don Olliff,  
La Mesa  
California.

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## POST OFFICE RADIO INTERFERENCE SERVICE

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Mr Doo of BREMA, writing in June letters, offers the comment that "the procedure whereby the Post Office notifies the appropriate manufacturer of an unresolved case of interference is often not being invoked". As an engineer with many years' practical experience, I have struggled continuously against this very situation which is brought about by public ignorance. The Post Office gives no publicity to its Radio Interference Service, and defends its position by saying that a Complaint Form A6328 is available at main offices.

Unfortunately there is absolutely no way in which a person can discover, in the first place, that such a service exists, until he is told by a third party already aware of it. The local general manager of the telephone service controls this specialist group of engineers, and one telephone call to the office is often sufficient. As the service is financed by a proportion of the television licence one would think that an obvious

place for reference would be on the licence itself.

How many radio and tv users realize that they are supporting a free assistance service, which has always been available, and which offers expert technical advice to anyone with a radio or tv interference problem?

This unfortunately does nothing to help the owner of purely audio equipment. Present experience suggests that modern transistorised units respond to unwanted r.f. signals far too easily. This is amply demonstrated in their response to noise from thermostats on central heating systems etc., often discovered on the exchange of an older valve system for a more modern equivalent.

If BREMA gets too few complaints to justify taking general action it behoves all of us involved in these difficulties to ensure that the Post Office participates when it can do so, and that every complaint, even if solved locally, reaches the manufacturers.

G. Openshaw  
Bolton  
Lancs

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## BAND II FERRITE AERIAL UNIT

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It should be pointed out to readers of Mr Thoday's article in the September issue that some portables, if fitted with an r.f. stage between the whip aerial and the input coil, will work satisfactorily (by "portable" standards) with the aerial completely closed. I possess a 1965 Sony receiver so fitted that picks up Wrotham indoors on the South Coast, with the whip pushed fully in. The set uses a BF180 r.f. stage rough peaked to 93MHz. Radio London is receivable by pulling out the aerial just 10cm — which can hardly be called "dangerous"!

Curiously, although the whip aerial is, naturally, vertical, it is markedly, though not annoyingly so, directional in a similar manner to the m.w.-l.w. ferrite rod. Whether the rod in some way contributes I have not investigated.

Certainly, it seems to me that the somewhat expensive device developed by the BBC seems unnecessary.

Ronald G. Young  
Peacehaven  
Sussex

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## THE OPERATING CLASS

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Your September editorial "The engineering class" suggests that the "profession" has to earn rather than expect the esteem of the public. John Dwyer in his "Telephones and new technology" in the same issue points out that the intervention of electronic engineering in telecommunications is leading to the situation where "one worker will be needed where there were once 27" and adds "what will happen to the 26? Who will support them?". With electronic development engineering apparently so predominantly concerned not with creating new human activities but with de-skilling or eliminating altogether the need for ancillary workers or "operators" is it to be wondered that the public increasingly withholds its approbation from the engineering class?

Would society continue to have esteem for the medical profession if its main preoccupa-

tion was intentionally to remove from active life unnecessary humans? Or the legal profession if it was concerned solely with removing from society the innocent as well as the guilty?

Your "appointments" column further underlines the engineering view of equipment users. One finds an advertisement for a "radio telegraphy operator" who must be able: (1) to receive and transcribe on a typewriter Morse code at 25 wpm; (2) make aural or visual recognition of signalling codes used in communications systems; (3) be able to operate complex modern communications receivers; (4) be able to operate radio teleprinter equipment; (5) understand radio propagation and frequency usage; (6) be able to correct, log and identify incoming material; and (7) possess "perfect" hearing and be prepared to submit to entrance examinations in Morse typing and signal recognition.

Apparently, however, I am alone in regarding this as a demanding list of qualifications, since the basic salary offered is £2334 — or roughly some two-thirds of what appears to be the going rate for electronic technicians and less than about half that of those development engineers whose main purpose appears to be to eliminate "operator" jobs altogether!

Surely, to gain public esteem the electronics institutions should be prepared to prove that the engineer creates more socially-acceptable jobs than he destroys and does not regard those who use his equipment as so much electronic-fodder. Electronic automation, ergonomics and human-engineering were "sold" to society in such terms in the 1950s — were we only being conned?

Pat Hawker

London S.E.22

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## REQUEST FOR OLD SET

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I am anxious to obtain a Romac personal radio receiver which is completely self-contained; the chassis, batteries and loudspeaker are housed in an all-metal body, camera shaped, finished in ripple black and polished chrome, and the aerial is contained in a flat p.v.c. covered black shoulder strap.

This receiver, the first miniature portable after the second world war, was manufactured by the Romac Radio Corporation Ltd., The Hyde, Hendon, London from 1946 to 1949.

Gordon Bussey

(Author, "Vintage Crystal Sets 1922-1927")

19 The Pines

Purley

Surrey

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## RADIO AND AIR SAFETY

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Your correspondent Mr T. R. Wiltshire, under the heading "Radio and Air Safety", (August letters), makes the point that it is difficult to obtain a British made v.h.f. communication radio suitable for light and general aviation aircraft of adequate quality. This is not so and sets are available which show a price advantage over most of the American models, of which, it is agreed, there is a much greater variety.

There is an enormous discrepancy in the size of the market in the UK and that in the United States where the number of general

aviation aircraft is over 40 times that existing here. This large market in the USA combined with their numerous well organized sales outlets, coupled with the American flair for mass production makes it surprising that British firms are able to compete at all.

Mr Wiltshire's suggestion that British manufacturers are badly placed because of the "enormous investment required due to complex Civil Aviation Authority regulations" is not valid. That Authority, pursuing its general policy of encouraging the use of airborne radio in sporting aviation, has been at great pains to minimize the cost of achieving approval. For light aircraft, over six different categories have been evolved dependent on the use to which a radio is put and each of these implies substantial concessions in the matter of testing when compared with the full transport category equipment. It must be obvious that a light aircraft flying in controlled air space to a busy airport must have equipment which is likely to have substantially the same performance and integrity as that in use by the scheduled airliners with which it will become involved.

Even so, an examination of the regulations will reveal that the cost of testing such a device has been contrived to be substantially less than that of the fully approved equipment. It may be of interest to Mr Wiltshire to know that the Authority has approved a number of home designed v.h.f. transceivers for use in gliders where the only requirements have been a power limitation of the transmitter output and proof that the frequency stability and the spurious radiation levels were in accordance with the ITU regulations.

In conclusion, I would state that the problem of effective audio quality is not simple. For example, microphone characteristics and microphone technique and the problem of acquainting the user when he is misusing a particular microphone all degrade quality significantly. This is recognized by the formulation of internationally agreed phraseology and forms of speech which provide appropriate information redundancy. Investigations of the misunderstandings which do occur from time to time show that these are frequently caused by users "short circuiting" some of the agreed phrases.

P. F. Cook

Civil Aviation Authority

Airworthiness Division

Redhill

Surrey

I think the majority of the aviation community would endorse Mr Townson's comments (October letters) on the desirability of reducing dependence on voice communications, although the rate of introduction of data link systems will be determined by cost and by the growth of confidence in their safety.

Regarding modulation standards, the relative merits of a.m. and f.m. in a 25kHz channel are debatable, but what is certain is that the vast amount of money which would be needed to convert all airborne transceivers would contribute more to air safety if spent in other fields (e.g. improving navigation aids).

An important consideration is the operational requirement for some ground stations to use up to 5 transmitters on a single channel to extend the service area. The offset-carrier (Climax) system is used, with carrier offsets of 4kHz minimum. This requires the receiver audio bandwidth, 8kHz at the detector, to be low-pass filtered to

2.5kHz to avoid 4kHz heterodyne whistles. Offset carrier techniques cannot be used with f.m., and while synchronous-carrier f.m. might allow slightly increased audio bandwidth, it is doubtful whether distortion would be acceptably low. (For further discussion of a.m./f.m. tradeoffs see Mr Drybrough's articles in *Wireless World*, November and December 1976 issues, and March 1977 issue).

R. A. Keall

Hawker Siddeley Aviation Ltd

Hatfield

Hertfordshire.

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## RIAA EQUALIZATION IN PRE-AMPLIFIERS

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I was very interested to read the comments of Mr de Paravicini (Letters, May issue) on passive RIAA preamplifiers. From my own studies and limited tests and from discussions and reading, I have reached the following conclusions on amplifier design:

1. The greatest contribution to sound quality of feedback RIAA pre-amps is to split the equalisation into two stages.
2. The better the quality of the basic amplifier circuit, the less the advantage in using passive equalisation.
3. Because amplification stages are not perfect, they introduce conflicting problems with high frequency phase response, low frequency phase response, input impedance at the inverting input (which may not be constant and will include some capacitance), gain required to avoid stage overload or noise level of next stage. Careful design is needed at each stage to produce an amplifier capable of reproducing music.
4. The quality that each amplification stage can attain as a straight amplifier is an important factor in determining the overall sound quality. The nine transistor amplifiers described by Mr Self<sup>2</sup> in his advanced preamplifier (with a few slight modifications) are capable of better sound quality than any other amplifier stage I have tried.
5. The sound quality obtained by using passive equalisation and the nine transistor amplifiers in every stage can only be maintained if the number of touching contacts are kept to a minimum (potentiometers, switches, and plugs and sockets). Additional switches and connectors to facilitate A-B switching tend to make comparison between very high quality amplifiers difficult.
6. The sound quality can never be better than the weakest stage. If an amplifier is of such a quality that a simple emitter follower creates noticeable distortion<sup>3</sup> then that must be replaced by a stage comparable with the rest of the amplifier even if nine transistors have to be used.
7. The input capacitance to ground at the disc input should be kept to an absolute minimum. R.F. interference should be avoided by a series inductance and any high frequency response rise corrected by a lower input resistance. The purpose of the lower resistance is to avoid resonance which will impair the quality of sound produced by the cartridge. This point has been made by leading hi-fi reviewers.<sup>4,5</sup>
8. The sound quality of almost every commercial amplifier can be improved considerably at little extra cost.

To turn to transient distortion, I fail to see

how the term "transient intermodulation distortion" can mean anything in the English language. To my understanding it is a description of a form of distortion to a transient waveform (musical signal) which occurs in passing through a circuit though that circuit introduces very little harmonic or intermodulation to a sine wave. Hence the term "intermodulation" is meaningless and confusing. No wonder that there is no one who understands it and can describe it in simple terms backed up by experimental evidence. In musical terms, it may seem like intermodulation between the sounds due to confused stereo images, but not in engineering terms.<sup>6</sup>

Finally I feel that it is unfortunate that Mr Vereker (June letters) finds it necessary to introduce a new term "loss of information". This is really the true meaning of the word "distortion".

Graham Nalty  
Borrowash, Derby

### References

1. T. de Paravicini, letter, *Wireless World*, May 1977.
2. D. Self, "Advanced pre-amplifier design". *Wireless World*, Nov. 1976.
3. A. King, letter, *Wireless World*, April 1977.
4. Angus McKenzie, "Reviewing reviewed". *Hi fi for Pleasure*, April 1977.
5. B. J. Webb, "Goldring 900SE" (review). *Hi fi News*, December 1976.
6. Graham Nalty, "Amplifiers examined – what is an amplifier?" *Practical Hi Fi & Audio*, July 1977.

## DOPPLER RADAR

I was most interested in the article on Doppler radar by M. W. Hosking in the July issue. I was immediately reminded of a very simple set-up using mainly Government surplus equipment which a colleague and I put together whilst both employed at the Royal Military College of Science, Shrivenham, somewhere in the period 1949/1950.

Separate small 12-inch paraboloids were used for transmitting and receiving. A low power 3cm klystron was used in the transmitter. This was of the type commonly used as a local oscillator in radar equipment of the period, as was also the crystal diode used in the receiving assembly. The object of the exercise was to demonstrate the principles of Doppler radar to young officers on degree courses.

We were not anticipating a lot of success, and time and equipment available were both limited. However, we were encouraged by most satisfactory noises from the loudspeaker made by personnel and vehicles passing in our beam. We were of course aware that the Doppler output was a function of the size and range of the reflecting object. Imagine our surprise and pleasure therefore when, on directing the beam down the cricket pitch, some 150m distant, the flight of the ball towards the batsman produced most satisfactory squeals! It was not long after this that we added a simple frequency counter which also displayed the instantaneous velocity of the ball on a large meter. All arguments as to the fastest bowlers were subsequently scientifically settled! No doubt in these more enlightened days we would have fitted a digital counter with a stored maximum velocity read-out!

As may be imagined this proved for some time a most popular demonstration. It would be most interesting to hear from any young officers of that day who remember these events at Shrivenham.

K. J. Neighbour  
Christchurch, Dorset

## INTEGRATED CIRCUIT OF THE 1920s

Accompanying this letter is a photograph of a valve, type 3NF, believed to have been manufactured by the German company Loewe in the 1920s. In my experience this is the earliest attempt at integration for it contains in one envelope three separate triode valves and all RC coupling components for a simple wireless receiver. The only external components required are the aerial tuning circuit, loudspeaker and power supplies. The circuit diagram and operating data are given on the only part of the original carton which remains.

Each resistor and capacitor is separately encapsulated in glass, presumably to preserve the vacuum against outgassing of these components, and the circuit provides an object lesson in economy of components to enable the valve to be mounted on its 6-pin base. The base has sliding contacts (not plug in) and uses a bayonet fitting base with three staggered locating dowels.

I am indebted to a colleague, Mr R. F. Wright, for the opportunity to examine this valve and several other collectors' pieces which he retrieved while clearing his family home in Australia. I retained it for long enough to find that it is still in working order and gives good loudspeaker reception on local stations on about 6ft of wire as an aerial, giving 400mV r.f. at the first grid. In operation the valve is quite isolated acoustically from the loudspeaker to prevent microphonic oscillation.

I would be very interested if any of your readers could provide any historical information on this device or on the Loewe company, which is unknown to me.

T. R. Thompson  
Dungeness 'B' Nuclear Power Station  
Romney Marsh  
Kent

*Editor's note: The firm Loewe Opta of Berlin, maker of radio and television sets, is of course well known in Germany.*



## HOTEL RADIO

If one makes use of the switchable radio installations which are provided in the bedrooms of modern hotels, the result is almost invariably disappointing. They are seldom in full working order. Typical faults are:

- Mis-tuning of all or some channels, with subsequent distortion and even, in areas of low signal strength, ignition interference; or some channels wholly missing.
- Faults in the amplifier and distribution network, resulting again in distortion and large variations in power level at the loudspeaker.
- Noisy switches (usually press-button) and volume controls.

These faults are found all over the world. I recall two satisfactory switched systems: one in West Germany where the audio signals are fed via a rotary switch to a valve amplifier and a modern push-button system in East Germany. The best all-round solution is found in many hotels in the USA – a simple continuously tunable f.m. receiver, firmly screwed to the wall. Why do European hoteliers not follow this practice?

John Want  
Pinner  
Middlesex

## TRAINING IN A DEVELOPING COUNTRY

I am writing to you on behalf of the International Voluntary Service in the Seychelles. We are part of the British Volunteer Programme, which is a voluntary organisation with a view to training technicians etc. in the developing countries. At present the college in which I am teaching has a City and Guilds of London 235A and 235B electricians course, and we are trying to start a basic electronics course, which is (in the electrical industry) a vital part of training.

The islands. I should explain, have just received independence, and of course have a limited budget, therefore we have problems in supplying texts for our students and component parts for building circuits. I would add that a lot of British technology is exported to the islands but only a limited training is available. Part of the plan is to expand on this training, so I would like to appeal to you and your readers to help in as many ways as possible. One very practical way would be with back issues of your magazines which I feel would be a tremendous help in the work. Also old or used textbooks would certainly be gratefully received, and, of course, what we call "junk," old p.c.bs, resistors, diodes, transistors (not too old), capacitors etc. The students are hard working and would be grateful for any help in developing the skills of our industry. My colleagues and I feel that the possibilities are excellent. The British people have given political independence to the Seychellois; we can give them economic independence by giving as generously as possible the technical training that they need.

Gordon Catto  
Seychelles Technical School  
P.O. Box 48  
Victoria  
Mahe, Seychelles

# Audible amplifier distortion is not a mystery

*Some things are believed because people feel as if they must be true, and in such cases an immense weight of evidence is necessary to dispel the belief.*

BERTRAND RUSSELL

by Peter J. Baxandall, *B.Sc.(Eng.), F.I.E.E., F.I.E.R.E.*

There is a very widely held belief that all amplifiers sound different, and that the reasons for this are so subtle and mysterious that no-one has yet properly understood them. I do not agree with these views, and confidently maintain that all first-class, competently designed, amplifiers, tested under completely fair and carefully-controlled conditions, including the avoidance of overloading, sound absolutely indistinguishable on normal programme material no matter how refined the listening tests, or the listeners, may be; and that when an inferior amplifier is compared with a very good one and a subjective quality difference is genuinely and reliably established, it is always possible, by straightforward scientific investigation, to find a rational explanation for this difference.

## Subjective reactions

When people claim to have detected a difference in the sound of two amplifiers, the true explanation for this may be any of the following:

- the amplifiers actually did produce different audible distortions,
- there was a slight difference, probably unsuspected, in the test conditions,
- psychological factors were exerting an influence.

It is possible to be quite misled by some small physical effect, thought to be of no consequence at the time. I well remember a particular case some years ago when a friend claimed to be able to detect by ear the difference between a good valve amplifier and a good transistor amplifier. He invited me to his house and had a changeover switch which I was asked to operate, not knowing which position was which. I soon found I could indeed detect a slight difference, one position seeming just a little smoother and less "grainy" than the other. I supposed this to be the valve position, which was correct, and we were both pretty well convinced we were hearing a trace of crossover distortion. It then occurred to me to wonder just how accurately the volumes had been set to equality in the

two positions, and the outcome of this was that we found that a reduction of not more than about 1dB in the volume from the transistor amplifier made it absolutely impossible for either of us to tell which amplifier was operating! More recently it was found that by choosing the moment of switchover in relation to the musical phrasing, to coincide with a change in sonority, one could produce the reaction that either one or the other of two systems was the better. This sort of thing can, of course, happen spontaneously, without anyone being aware of it. Another possible cause of deception is a trace of hum in one system but not in the other, due to insufficient care over earthing arrangements in the test set-up — this hum can get misinterpreted as a degradation in general quality.

With regard to psychological factors, I think it should be openly recognised that those of us claiming to have "golden ears" in matters of sound quality judgement can nevertheless be very easily led astray in various ways. For instance if, without being aware of it, we have listened for a long period to some equipment with, say, a 6dB dip in the frequency response at 3kHz, but otherwise of first-class performance, removal of the dip is very likely to produce the reaction, at least initially, that the reproduction has become too strident. However, if it was known to the listeners beforehand that a dip had been intentionally introduced, removal of it is then more likely to produce the reaction "Yes, now the violin tone is more realistic" or something of the sort! Such pre-conditioning and psychological influences are quite strong, and should be allowed for. Another psychological phenomenon, very significant I think, is that few of us like to admit that we "just cannot tell the slightest difference" in the presence of others who have professed to hear subtle differences. So most people will succeed in convincing themselves that they really have managed to notice small changes in sound quality. In properly conducted subjective tests, however, the participants should not know which system they are listening to at any given

time, and the number of switchovers, some genuine and some not, should be large enough for a proper statistical interpretation of results to be made. Guesswork, maybe unconscious, is then largely prevented from influencing the results.

An amusing illustration of some of these psychological ideas arose on an exhibition stand by a well-known firm, who had arranged things so that visitors could listen, at precisely the same volume, to three of their amplifiers, being invited to identify the most expensive model. In fact it was found that voting for "the best amplifier" was about equally distributed between the three, so that, naturally, about a third of the visitors picked the right one. When told they had been successful, the almost universal reaction of these individuals was one of pleasure at their evident skill, whereas, of course, an equally logical reaction would have been to congratulate themselves on their good luck!

The BBC Research Department is well aware of the dangers of reaching quite wrong conclusions from subjective tests. Very careful precautions are taken to eliminate as many psychological and physical disturbing factors as possible, and even to derive, where appropriate, a quantitative estimate of the reliability of the results<sup>3</sup>. It is very evident that in many other places such precautions are not properly taken.

## Recording systems and amplifiers

Unlike amplifiers, conventional tape and disc recorders, even those of the highest professional grade, have distortion levels and signal-to-noise ratio which are only just about good enough subjectively. A very instructive experiment is to record the same mono programme source on both tracks of a good stereo tape recorder, with a level difference of, say, 10dB. The replay gains are then adjusted to give outputs of equal magnitudes, and these are subtracted one from the other to give, ideally, nothing but noise and distortion. The distortion is mainly that of the

more heavily recorded track, whereas the noise is mainly that of the weaker track. (In practice a little h.f., and possibly l.f., phase correction may be necessary to get fully satisfactory programme cancellation.) With gains set to give normal listening volume when only one track is reproduced, the distortion heard with both tracks operating is quite horrible and is loud enough to be very easily audible all over the room even in conditions of moderately high ambient noise level. This gritty, blasting, distortion is only somewhere about 40dB below the uncanceled programme level during loud passages, yet it is virtually unnoticeable when accompanied by the music. Tests with tone input show that the distortion is mainly third-harmonic, the percentage distortion being proportional to the square of the output voltage and reaching about 2% at peak recording level. The distortion is fairly independent of frequency over most of the audio band. Thus a first-class professional tape recorder gives distortion of about the same magnitude and character as a push-pull class A amplifier having a distortion figure of about 2%, assuming this also to be reasonably frequency-independent.

Experiments I have done with class A push-pull amplifier circuits, involving balancing out the programme and listening to the distortion by itself, do indeed show that it sounds much the same as that produced by a good tape recorder, and that 1 or 2% distortion is low enough for results of the highest quality, provided the amplifier performance is clean enough in all other respects.

Similar experiments with class B push-pull circuits, adjusted to give considerable crossover distortion, show, not surprisingly, that the distortion is rougher and more unpleasant sounding, and tends to be nearly as loud during fairly quiet parts of the programme as during the loud parts – it appears as an almost continuous background fuzz. For absolutely first-class quality, distortion of this type must be reduced to much less than 1% at all output levels and over most of the audio spectrum. This topic will be considered in greater detail later on.

In recording systems, unless very refined and expensive digital techniques are used, there is always the need for a careful compromise between signal-to-noise ratio and distortion. Compandor systems, of which 'dbx' is the latest, and very welcome, development<sup>4,5</sup>, can achieve an impressive improvement in subjective signal-to-noise ratio, together with some reduction in peak distortion level, but they do not actually affect very greatly the signal-to-noise ratio existing during loud passages. Thus reliance is still being placed on the masking effect<sup>6,7</sup>, whereby unwanted sounds, which would be very easily audible on their own, become virtually inaudible when

accompanied by the wanted programme.

With amplifiers, on the other hand, it is comparatively easy to reduce the audible distortion and internally-generated noise to far lower levels than in any normal recording system, and this is what is done in equipment of the highest grade. Provided such amplifiers are tested under sufficiently carefully controlled and fair conditions, are free from faults such as hum and r.f. interference susceptibility, have insignificant differences in frequency response, and are not overloaded, the quite inevitable result is that one amplifier is absolutely indistinguishable from another, on normal programme material, no matter how "golden" may be the ears involved.

Quad have shown<sup>8,9</sup> that, with their transistor power amplifiers, if the amplifier distortion, including hum and noise, is reproduced by itself at its normal level, without the music, the result is *total silence* under ordinary listening conditions. This is enormously better than the result obtained when a somewhat similar test, as described above, is done on a high-grade professional recorder. But, to me, the most amazing thing is that Peter Walker tells me that few of the people who have witnessed this experiment seem able to appreciate its true significance, which is, quite inescapably, that such amplifiers are subjectively perfect with a large margin to spare and give an audible performance which can never be improved upon. Quad do not maintain, however, that theirs are the only amplifiers about which this may truly be said. Of course if, during the above experiment, such amplifiers are allowed to overload, even momentarily, the silence is broken and the distortion fairly cracks forth. But amplifiers should not be allowed to overload, and if they do, the only proper solutions are to turn the volume down or employ more powerful amplifiers.

A few people have raised the objection to the above experiment that though the distortion may be inaudible on its own, the ear and brain are exceedingly complex and subtle, and the effect of the distortion might conceivably be perceived when it is accompanied by the music. This, however, is quite contrary to what is found to happen in the tape-recorder experiment referred to earlier, where the distortion is easily heard on its own but is very well masked when accompanied by the music. Experiments I have done involving crossover distortion show that it too is fortunately subject to a considerable degree of masking in the presence of the associated programme.

#### A diagnostic tool

The technique employed by Quad<sup>8,9</sup> for listening to amplifier distortion by itself, on programme input, provides a very useful tool for assessing the subjective

goodness of amplifiers in a quantitative manner and for establishing criteria that should be met if an amplifier is to be totally free from audible distortion. The technique can obviously be implemented in various detailed ways, and Fig. 1 shows one arrangement which is suitable when the amplifier under test is of the phase-inverting type. When, as is more usual, there is no phase-inversion, a very low-distortion phase inverter must be introduced into the circuit in one of several possible places.

For setting the circuit up, it is found in practice that an audio noise source is more suitable than normal programme input, since all frequencies are present all the time. Thus  $S_1$  and  $S_2$  are both closed, and  $P_1$  plus the several adjustments in the frequency-response and phase-balancing network are adjusted for minimum output from the monitoring system. The potentiometer  $P_2$  should initially be set to a low resistance value, the value being raised as the balance condition is made more and more nearly perfect. Potentiometer  $P_2$  should finally be set so that, with  $S_1$  or  $S_2$  opened, the voltage fed to the monitor system loudspeaker is the same as that fed to the load circuit of the amplifier under test. With both switches again closed, the distortion alone will then be reproduced by the monitoring system loudspeaker at its proper level. Having thus got the circuit correctly set up – a rather tedious operation because of the number of adjustments involved – a little thought will show that a variety of interesting and very informative tests may then readily be done, such as:

- The gain of the monitoring system may be increased until the distortion does become audible by itself, thus obtaining a measure of the margin by which it was previously inaudible.
- The effect on the audible distortion of loading the amplifier under test with loudspeakers and/or dummy loads having various different impedance characteristics may be investigated. (When a loudspeaker load is used, it is necessary, of course, to prevent the sound from this loudspeaker from reaching the person listening to the distortion on the monitoring system loudspeaker. Rather than use well-separated rooms and very long leads, a more convenient procedure is to tape record the distortion and listen to it later on.)
- The two loudspeakers of Fig. 1 may be placed next to each other,  $P_2$  then being adjusted to determine by how much the distortion may be increased above its "natural" level before a just-detectable degradation in music quality begins to become evident.
- With  $S_2$  only closed, and then  $S_1$  only closed,  $P_2$  being set for a suitable listening volume from the monitoring-system loudspeaker, reproduction via the amplifier under test may be compared with that via the passive network. With a first-rate amplifier,

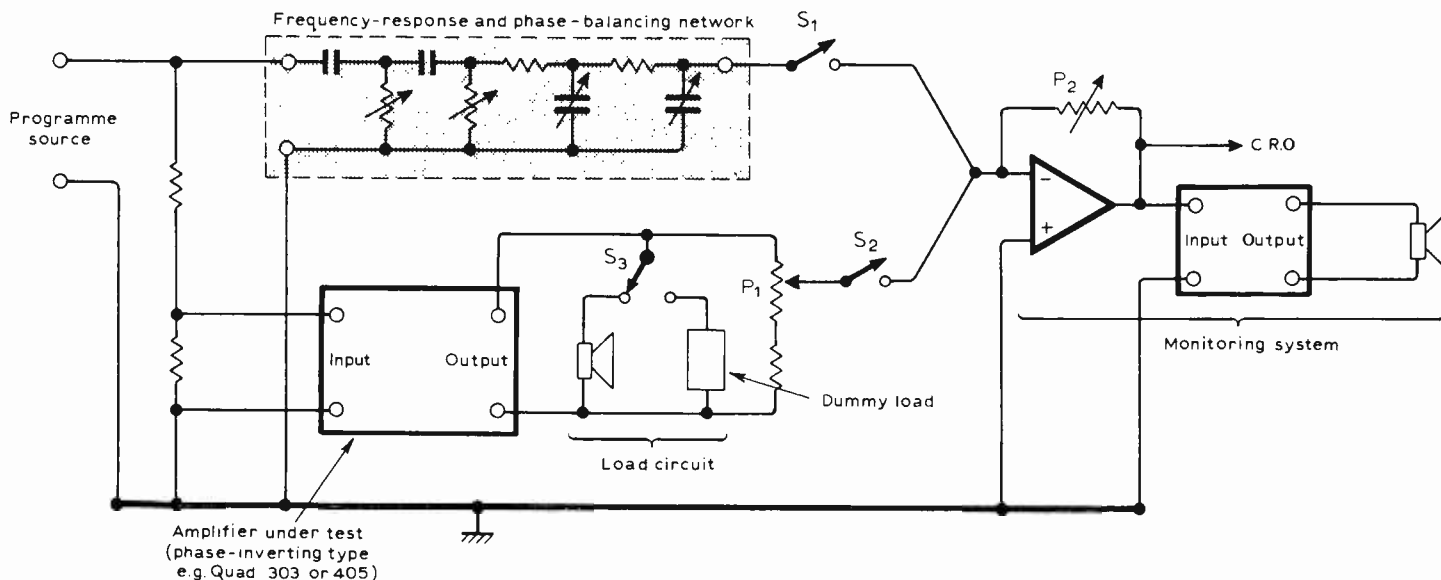


Fig. 1. The diagnostic set-up. A modified frequency-response and phase-balancing network may sometimes be required.

absolutely no difference whatsoever should be detectable on any kind of music programme input, provided that no overloading of the amplifier under test is allowed to occur. The test may be extended to assessing the degree of unpleasantness of various degrees of overloading, with and without protective circuits in operation, etc.

● When two amplifiers are found to sound genuinely different in ordinary subjective tests, they may then be tested in a circuit of the Fig. 1 type to see whether the distortion is audible when reproduced by itself. It may be found that the distortion is of an overloading type, though perhaps happening at a lower output level than the expected clipping level because of the operation of protective circuitry within the amplifier — or it may be that the amplifier has been badly designed with regard to its slew-rate capability. Such possibilities may then be looked into in detail. On the other hand, if both amplifiers give inaudible, or very unobtrusive, distortion, it is worth testing one amplifier in the Fig. 1 circuit with the frequency-response and phase-balancing values adopted for the other amplifier in place. Then, if there is a noticeable difference in quality when only  $S_1$  or only  $S_2$  is closed, the mid-frequency gains having been set to precise equality, it is likely to be because of the slightly different frequency responses — in particular, the response below the audio spectrum may be important in influencing the amount of rumble or other sub-audio-frequency signal reaching the loudspeaker, where it may cause large cone movements and thereby affect the loudspeaker distortion.

● By using an oscilloscope with the Fig. 1 set-up, much can be learnt about the relationship between the type of distortion waveform observed and the corresponding subjective nature of the distortion. The system also has the great virtue, when used with tone input,

that the true waveform of the amplifier distortion is displayed, unaffected by oscillator distortion or by slight harmonic phase shifts contributed by the notch filter that would normally have to be used.

The Fig. 1 type of arrangement can also be made the basis for an accurate and very satisfactory technique for harmonic and intermodulation distortion measurement, which has the advantage of not demanding a high degree of oscillator waveform purity.

### Some conclusions

One of the conclusions to be drawn from tests such as those just outlined is that amplifiers do tend to differ somewhat in the degree of unpleasantness of the distortion they produce when allowed to overload, but, apart from this I feel sure that nobody who has actually himself used these largely subjective investigational techniques could possibly continue to believe that all amplifiers sound different or that the subjectively perfect amplifier has yet to be designed. This is why Quad have been prepared to stake their reputation and say without reservation that they would be prepared to accept a challenge to have their 303 or 405 amplifiers compared effectively, using the Fig. 1 type of set-up, with what they have called a "straight wire with gain"<sup>10</sup>. Provided certain quite reasonable test conditions are satisfied, their claim is simply that no-one will genuinely be able to detect the slightest difference in sound quality on any programme input derived from normal sources.

The unconvinced may well say "if subjective perfection has already been achieved, then why are amplifier

manufacturers still devoting a lot of research and development effort to making better amplifiers?". The cynical reply might be "to produce even more impressive-looking figures for reviews"! But in fact the enlightened designer is probably spending most of his time struggling with far more difficult problems, such as how to achieve greater reliability, how to simplify the design and hence reduce the manufacturing costs, how to eliminate the need for preset adjustments, how to increase the maximum available output, how to improve the ability of the amplifier to cope with a wider range of load impedances, how to eliminate "switch-on plonks" etc. None of these problems directly involves the concept of subjective listening quality.

It is when problems such as those just mentioned are considered that the true nature of the enormous advances made in audio-amplifier technology becomes evident. In 1938, a British 14-watt high-quality amplifier sold for about £19, yielding a figure of 0.74 watt per £1. A recent 200-watt stereo amplifier, of smaller size and weight, sells at £115 and gives 1.7 watts per £1. Allowing for inflation, it is clear that the true cost per watt using modern solid-state techniques is down by a factor of the order of ten on what could be achieved in the valve era<sup>2</sup>. This is undoubtedly a great engineering achievement.

As a designer of audio amplifiers and other equipment, of which some is currently in use in BBC studios and elsewhere, I must have spent many thousands of hours inventing, thinking about and experimenting with audio amplifier circuits, but I cannot recollect ever having carried out subjective quality-assessment tests as a direct part of the design and development process. Subjective tests have been done separately from the design work and for the purpose of helping to establish criteria which need to be satisfied by the equipment designed.

Without knowledge of such subjectively-derived criteria, it is natural to "play for safety" and make the performance far better than it actually needs to be. This is particularly the case with preamplifier or control-unit design, where the non-linearity distortion is usually of the simple smooth-curvature type, which does not need to be reduced anything like as far as it is possible to reduce it in order to become quite inaudible. To elaborate the design, with consequent increase in cost, to the point where the distortion is, say, a hundred times, or more, below the subjective detection limit — which it is quite possible to do — is surely not in the true interests of the customer. Needless to say, very great care indeed must nevertheless be taken with things that really do matter, such as leaving sufficient "headroom" to accommodate all pickup sensitivities<sup>2</sup>, achieving very low hum and interference susceptibility, etc.

Once the designer has freed himself from various quite irrational and unfounded beliefs, e.g. that there is an inherent subtle difference between valve and transistor sound, that transformers always produce detectable subjective distortion, that class B amplifiers can never sound quite as clean as class A ones, that feedback should only be used in small amounts, etc., he can then proceed in a proper scientific manner to develop designs of good economy and reliability, and immaculate subjective performance. He will appreciate that there are countless ways of designing equally good-sounding amplifiers, and concentrate his efforts largely on seeking the optimum engineering solution.

### Amplifier reviews

The belief that all amplifiers sound different seems to be even more deeply rooted with the popular hi-fi press and their reviewing teams than it is with designers. I feel that a great disservice is being done both to the buying public and to some manufacturers by reports on amplifiers and control units of the type which have appeared, for example, in *"Hi Fi for Pleasure"*<sup>11,12</sup>. The reviewers claim to have been able to detect by ear specific deficiencies in virtually all units submitted to them, including differences between "cancel" and "tone controls flat" in all cases where such a comparison was possible. But ones incredulity is surely stretched beyond the limit when one finds a well-known control unit, widely adopted by discriminating professional users, described as having a mid-range that is forward yet lacking in detail, with some compression of peaks and an unstable image, and a top end performance that is thin and rounded off, but with a splashy character imparted on cymbals, and similar explosive sounds, the overall performance being summarized as dull, with a great loss of presence and

ambience and "seeming to make the music sound amateur"! Enquiries revealed that the unit in question was subsequently retested by the manufacturers and found to be in perfect order. When descriptions such as the above, which could only properly apply to equipment with quite gross faults, are used in relation to items known to be first-rate, it is clear that either something was wrong with the test set-up or that the reviewers — not to question their sincerity — had fallen prey to their own imaginations.

Since the belief that all amplifiers sound different has become so widely accepted, it is natural for people to want to find technical explanations for it. Since little correlation with performance as ordinarily measured can be found, the notion has built up that something extremely subtle and elusive is involved. To explain these supposed subtleties, those with more imagination than scientific understanding proceed to evolve a series of wilder and yet wilder pseudo-scientific hypotheses. New jargon is created — "musicality", "loss of information", etc. An article of French origin which has recently appeared in *Hi-Fi News*<sup>13</sup> — accompanied, however, by an expression of editorial neutrality and non-commitment — says the quality of copper used in loudspeaker leads influences the quality of the information transmission, the best wires having a purity as high as 99.99995%. The alternating magnetic field generated by a loudspeaker cable is said to represent a significant loss of information. Even in the wiring of electric-bell circuits, the use of Litz wire is claimed to give "tintinabular superiority". How silly can we get? All this sort of thing, which seems to be encouraged by some of the hi-fi magazines, for whom it no doubt provides easy material for filling their pages, is surely not good for the future of the audio industry, being liable to bring it to a state of disrepute with intelligent people.

Admittedly the subtleties and difficulties of many aspects of good sound reproduction are enormous, but it seems a pity that an atmosphere of quite irrational mysticism should be encouraged to invade even those parts of the field where things are properly understood and quite straightforward.

Finally, lest some readers may feel that the views here expressed are representative only of an engineering outlook, it may, perhaps, be relevant to add that I have a passionate interest in music, that I frequently go to concerts, do a good deal of recording of live music, and that much music making, some professional, goes on in my household.

*The next article will discuss some detailed technical matters relating to amplifier design.*

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### Harold W. Barnard

Many people in the electronics industry will be saddened to hear of the death of Harold W. Barnard, editor of *Wireless World* from 1965 to 1973. Although he held this post for only eight years he had in fact given a lifetime of devoted service to the journal. Starting in 1925 as an assistant to the production manager, he transferred in 1936 to the news side of the (then weekly) journal to become what was known as a "leg-man" — getting news the hard way without the assistance of today's information services and publicity organizations — and eventually took complete charge of the news section. During the 1939-45 war he was a member of a small team that kept the journal going under extremely difficult conditions. In 1959 he was appointed assistant editor, a fitting tribute to his journalistic abilities.

When he retired in 1973 we wrote this of him: "Kindness, courtesy and dedication are three qualities not very much in evidence in the modern industrial scene. They are the three qualities which one would most likely pick if one were asked to characterize in a few words the retiring Editor of *Wireless World*, Harold W. Barnard. Readers may wonder what such things have to do with technical journalism: they don't seem to be relevant to the business of turning out good articles and news on radio and electronics. But technical journalism, like many other professional and industrial activities, runs on the fuel of human contacts. What is printed in each issue is the final result of much talking, listening, letter writing, discussion, argument, persuasion, joking, threatening, criticizing, and praising. All these are necessary functions, but it is the personal qualities an editor brings to exercising them that makes all the difference. It would not be fanciful to claim that kindness, courtesy and dedication have been significant factors in the making of *Wireless World* during the eight years of Harold Barnard's editorship."



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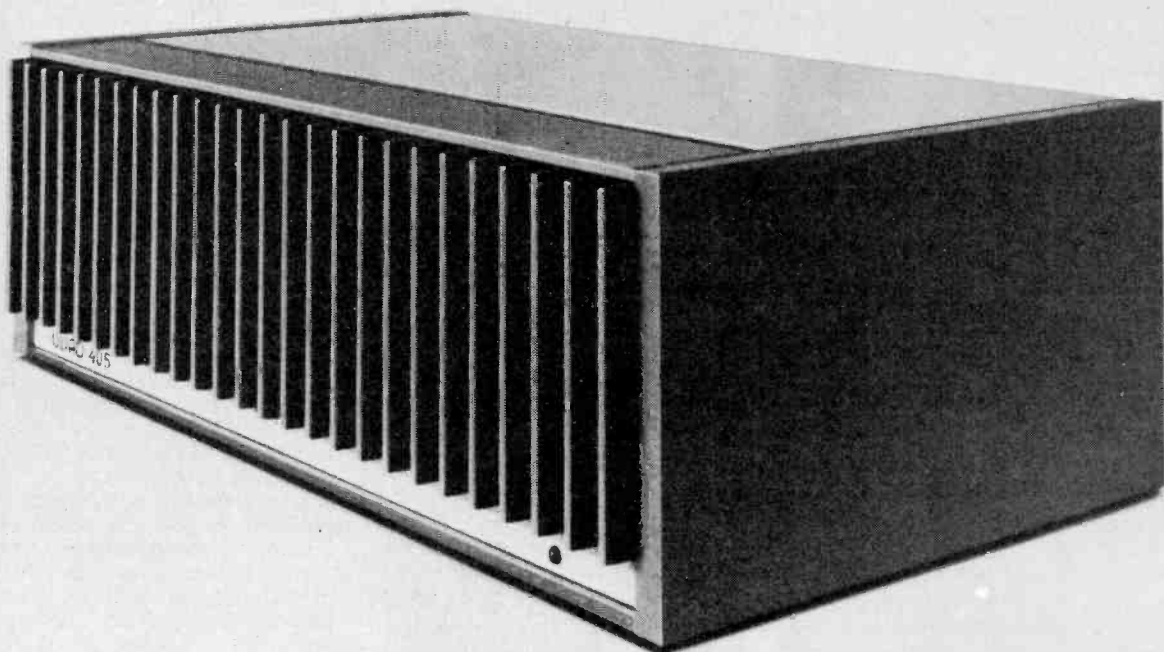
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# Microwave voice link — 2

## 10GHz unit uses Gunn oscillator

by M. W. Hosking, M.Sc., M.I.E.E., *British Aircraft Corporation*

**This low-power communication link uses a similar type of receiver to that in the domestic intruder alarm circuit described in the July and August issues. This article completes constructional details of a 10GHz pulse-modulated voice link, including waveguide and horn antenna and a simple calibration procedure.**

The receiver is in two parts: a microwave detector as the front end, followed by a combined filter and amplifier circuit. The detector is a Schottky-barrier diode in a waveguide assembly similar to the transmitter. The operation of this and other types of microwave diode were described in *Realm of Microwaves*, part 5, August 1973 issue. For use as a straightforward video detector, as opposed to a mixer, it is necessary to provide a small, forward d.c. bias of about 40µA to start efficient rectification. With this applied, the output impedance of the diode is about 800 ohm.

The rectified output from the detector, which consists of the 50kHz position-modulated pulse train is fed directly into the filter/amplifier circuit of Fig. 11. To keep the noise level to a minimum, the first section up to the base of  $Tr_1$  is a low pass filter which starts to roll-off at 50kHz. Transistor  $Tr_1$  has a fairly low noise figure of about 4dB and, together with  $IC_1$ , gives a stage voltage gain of about 1000.

The first stages of the inverting and

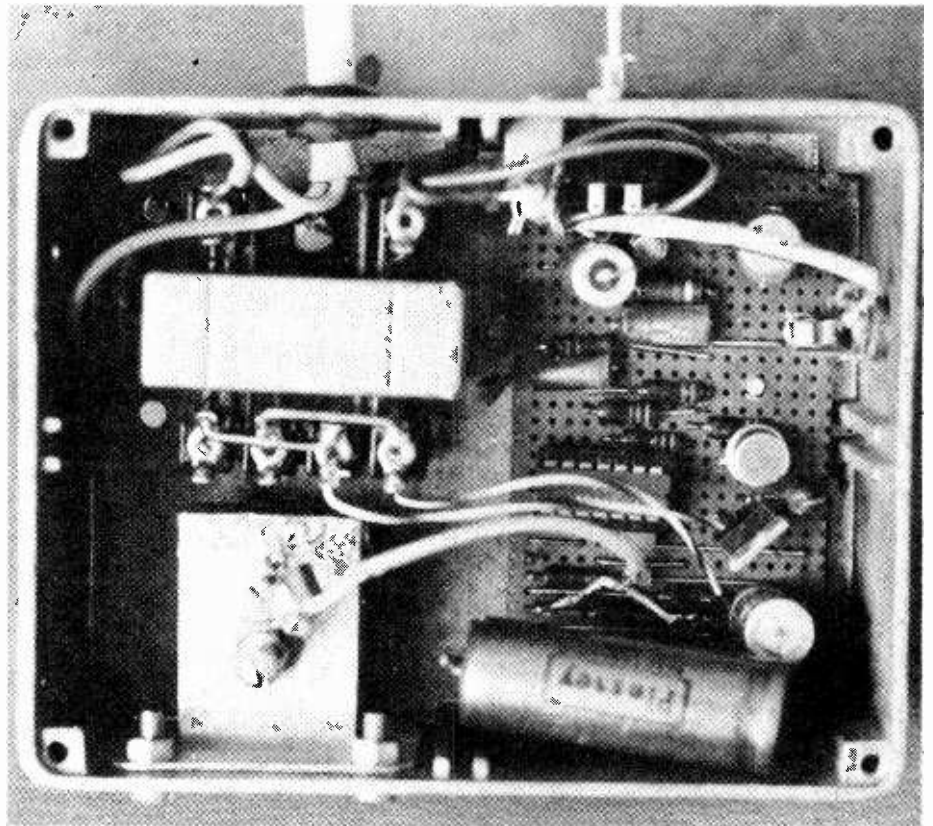


Fig. 10. Complete modulator and transmitter packaged in a standard die-cast box showing the general interconnections, as described in the October issue.

non-inverting inputs to the op-amp are bypassed, Fig. 11. These stages impose a relatively slow response on the amplifier and the present circuit provides a

cheap means of obtaining both fast response and high gain. The normally low noise figure is maintained with  $Tr_1$ .

In similar fashion, the second stage can also provide a voltage amplification of up to 1000, but this can be varied with  $R_{28}$ . In practice, amplification of a few hundred only has been possible before the onset of self-oscillation. As mentioned earlier, no high power stage is provided, the output from  $IC_2$  going directly to a pair of high-impedance (4kΩ) headphones. Current drain is quite low at about 5mA per rail and thus the receiver can be operated quite conveniently from a pair of PP3 dry batteries.

### Receiver construction

The microwave detector is mounted in a waveguide circuit constructed in the same manner and to the same dimensions as the transmitter. Positioning is not quite so critical as with

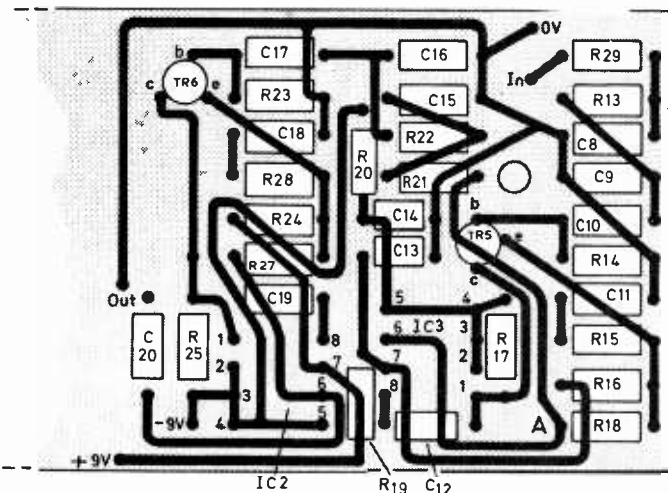


Fig. 9. Component and track layout for the receiver printed circuit board. (Extra component spaces were originally for the intruder detector circuitry.)

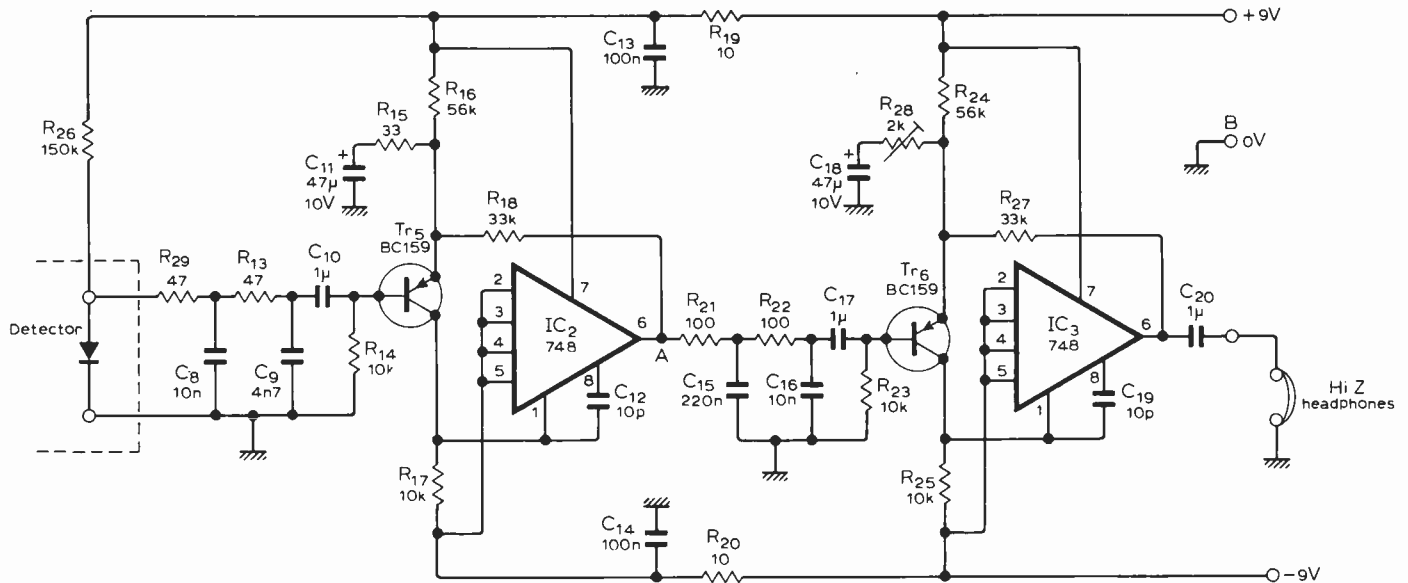


Fig. 11. Receiver/demodulator consists of a two-stage amplifier with two low-pass filtering sections. Output can be fed directly to high-impedance headphones or to an audio power amplifier for loudspeaker reception. Resistors are  $\frac{1}{8}$ -watt, 5% types, capacitors 10% tolerance, except electrolytics.

the Gunn device and, as shown in Fig. 12, the tuning screw has been omitted. If you wish to experiment for optimum performance you can include this and also vary the position of the short circuit.

Remove the collet from the diode, taking care not to exert too much torque on the ceramic-to-metal joints, and solder a lead to the base, then insert the collet through the waveguide wall and bond into position with a bead of Araldite. It is important that a good electrical contact is maintained between the collet and the guide, so take care to ensure that no adhesive seeps between the two. In similar fashion to the transmitter, r.f. shielding is provided at the other end of the diode by forming a bypass capacitor from a layer of foil and adhesive tape. Ensure that the foil does not short out the diode

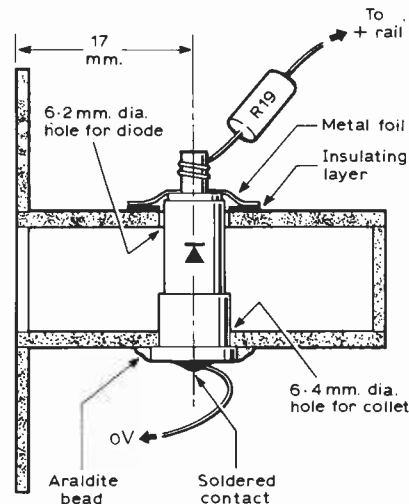


Fig. 12. Final assembly details of the microwave detector in a similar cavity to the transmitter. Metal foil, insulated from the guide, acts as microwave choke and helps screen the diode from external interference.

Fig. 13. General layout of the receiver system in standard die-cast box showing internal lid-mounted batteries.

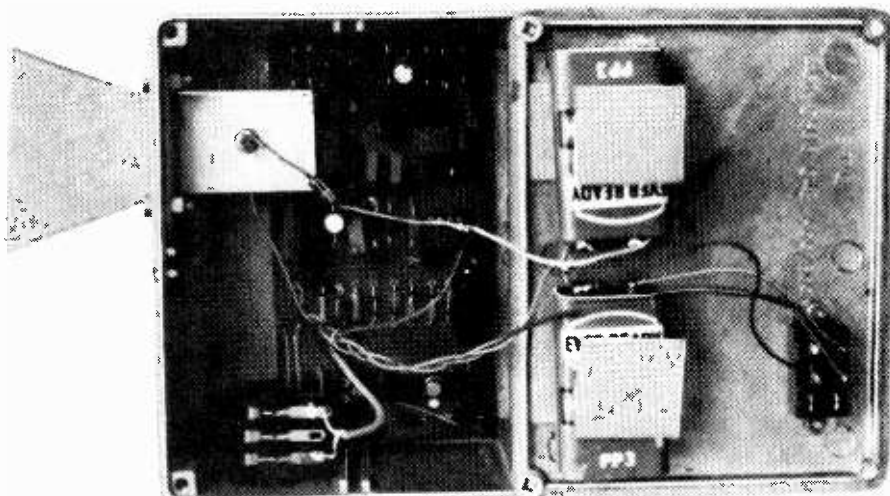
directly to the mount. The detector diode junction is easily damaged by voltage spikes, so it should not be touched with the soldering iron. Forward biasing with a multimeter when checking resistance will probably burn it out.

A printed circuit board has been produced for the main receiver and the component layout is shown in Fig. 9. All parts of the receiver system have again been designed to fit into a  $4\frac{1}{4} \times 3\frac{3}{4} \times 2$  in ( $150 \times 120 \times 50$  mm) die-cast box, the complete assembly being shown in Fig. 13. Additional mounting details are given in Fig. 14.

### Antenna

Open-ended X-band waveguide, such as used for the transmitter and detector, has an acceptable impedance match when radiating into free space and a gain of about 4.5dB. However, the receiver signal-to-noise ratio can be greatly increased by using more directive antennas. The prototype used two pyramidal horns with a design aim of 20dB gain; measurement showed that 19.3dB had been achieved. The prototype horn was constructed from 0.013in (0.3mm) thick aluminium sheet, but this is not critical and may be varied up to the limits of easy fabrication. Fig. 15(a) presents the folded-out dimensions of the horn and Fig. 15(b) shows the final assembly. Flange size and circular hole positions are as given in Fig. 4(d) but the rectangular hole is slightly smaller, as indicated.

Hold a rigid straight-edge along the fold lines of the horn and carefully bend the aluminium into shape, trying to achieve as sharp and even a corner as possible. With the mating edges held together, run a bead of Araldite down the join, first ensuring that the metal is clean, dry and free from fingerprints. Bond the flange in place and heat-cure the adhesive. It is worth taking trouble to ensure that the narrow end of the horn matches exactly the rectangular



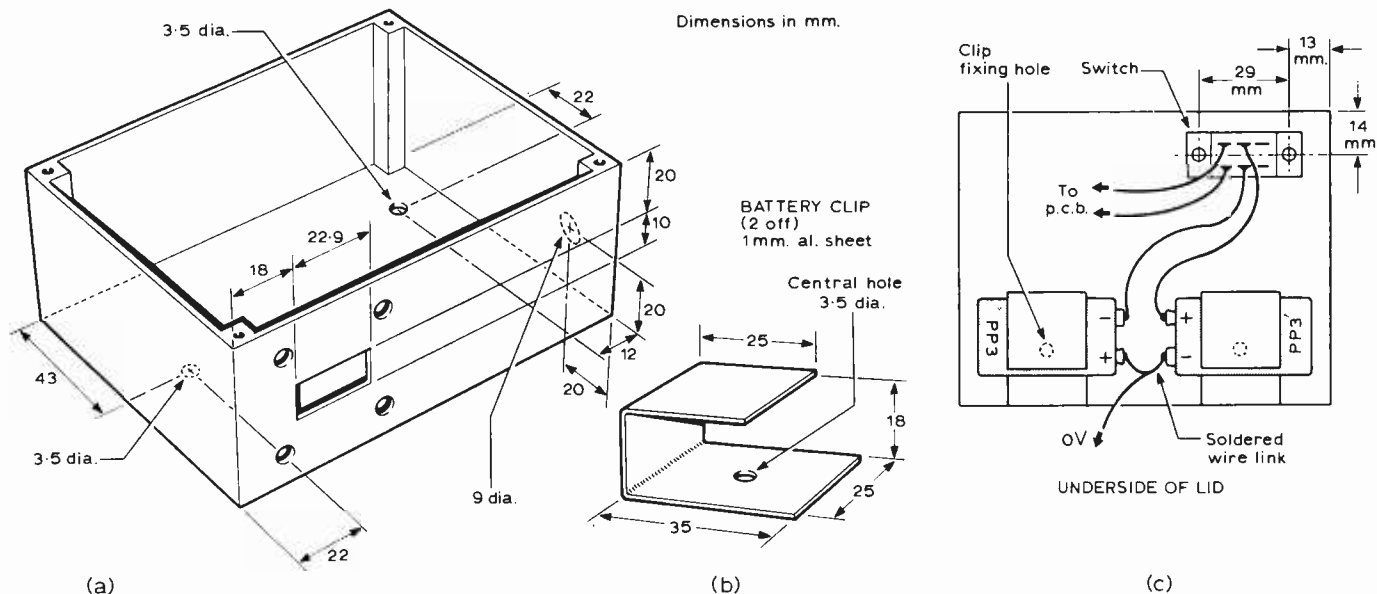


Fig. 14. Hole positions on the receiver box, together with battery mounting details.

Fig. 15. Antennas are constructed from thin (0.3mm) aluminium sheet bent to the dimensions shown and give gain of about 19dB.

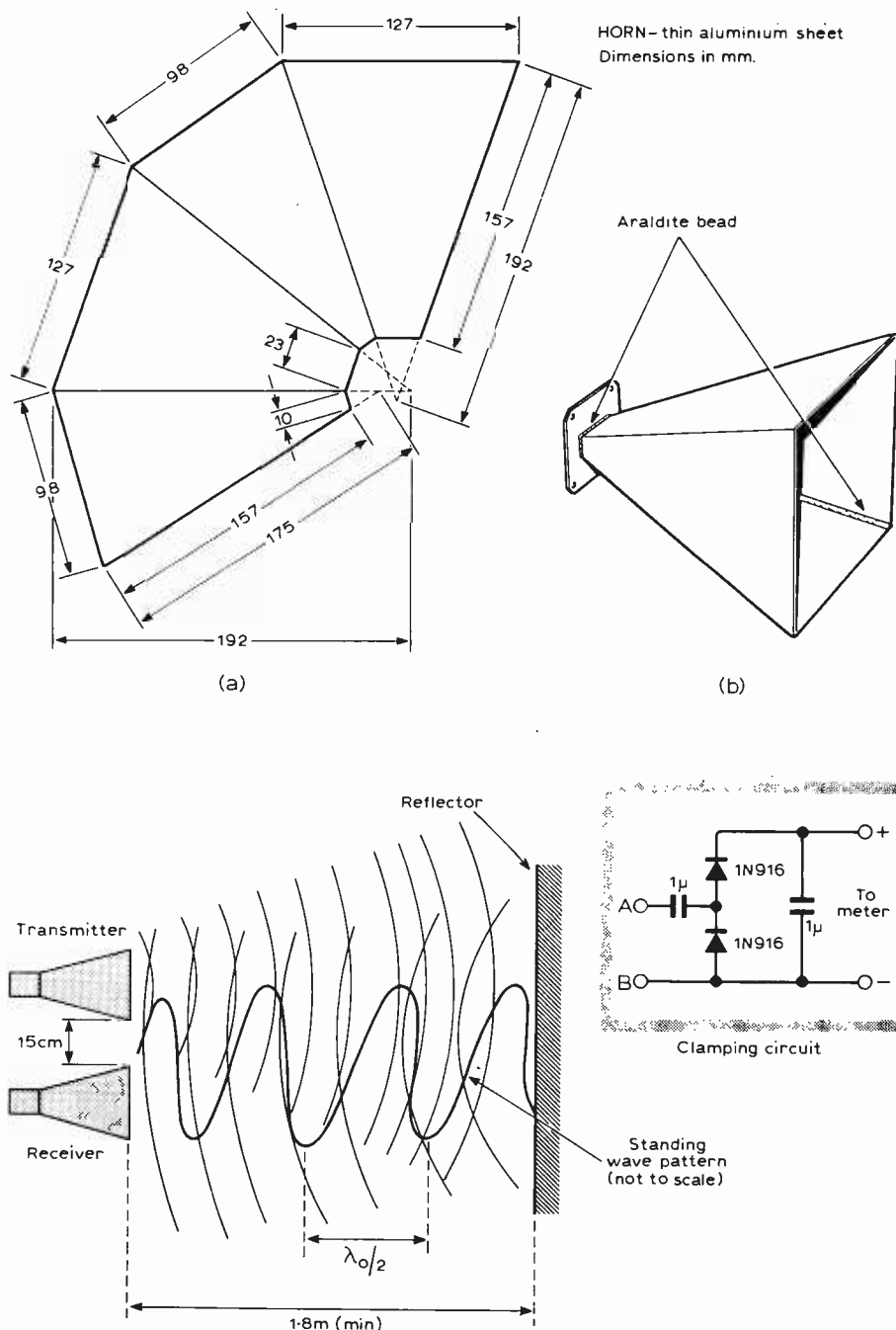
waveguide. Any overlap will have the properties of an inductance or capacitance, depending on which plane it's in and will affect the resonant frequency of the transmitter.

**Frequency calibration**

The Home Office transmission regulations require that a speech link with this particular modulation be operated within the frequency band 10.050 to 10.450GHz. Few readers will possess or have access to microwave frequency-measuring equipment and so the following technique is suggested.

When electromagnetic radiation is reflected from an object, the incident and reflected waves will combine with a phase difference dependant on the reactance of the object. This sets up a standing wave pattern having sharp nulls and smooth peaks, repeating every half-wavelength. Thus, a measurement of the standing wave pattern will yield the frequency. As indicated schematically in Fig. 16, place the transmitter and receiver side by side about 6in (15cm) apart and at least 6ft (1.8m) from the reflecting object. A convenient arrangement is to support the horns on a box on the floor of a room and pin a sheet of aluminium foil onto the wall. A constant amplitude signal is required for the test and this can be obtained by connecting the input to the diode

Fig. 16. Experimental arrangement for measuring transmitter frequency by the free-space standing wave pattern produced by reflecting screen.



continued on page 92

# Logic design — 9

## More shift registers — ring counters and maximum-length sequence generators

by B. Holdsworth\* and D. Zissos†

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The simplest type of shift register counter is the ring counter where feedback is provided from the last stage and feeds the inputs of the first stage as shown in Fig. 8(a). In this circuit there are ten stages: it can be used as a decimal ring counter, since the number of stages is equal to the number of counter states. The information contained in each stage is shifted to the next stage on the receipt of a clock pulse and the counter circulates a 1 which is initially preset in the first stage, all other stages being simultaneously cleared to 0. The counting sequence of the register is shown in Fig. 8(b).

The circuit of Fig. 8(a) can be modified so that it becomes self-starting as shown in Fig. 8(c). The input  $J_A = \bar{A}\bar{B}\bar{C}\bar{D}\bar{E}\bar{F}\bar{G}\bar{H}\bar{I}$  and this can only be a 1 providing  $A = B = C = D = E = F = G = H = I = 0$ . Clearly if any section of the counter except the last one contains a 1,  $J_A = 0$ , and the counter will now enter the required sequence within a maximum of ten clock pulses.

The ten outputs of this counter can be used directly to drive a decimal display without the need of decoding networks or alternatively it can be used to enable a group of circuits sequentially, as the 1 moves through the various stages of the shift register. The number of stages required in the latter case will be equal to the number of circuits that have to be enabled.

An obvious advantage of the decimal ring counter is its simplicity and since it requires no feedback logic or decoding circuits it uses fewer components. It does, though, have the disadvantage of not having a binary readout, and its counting sequence is radically changed if circuit misoperation occurs, as for example when a section other than that containing the counting 1 is, due to

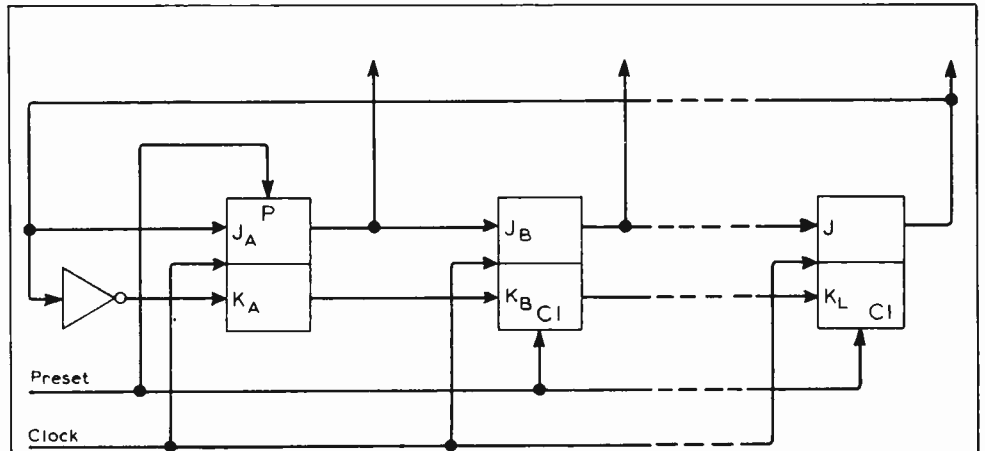


Fig 8(a)

Clock pulse	L	I	H	G	F	E	D	C	B	A
0	0	0	0	0	0	0	0	0	0	1
1	0	0	0	0	0	0	0	0	1	0
2	0	0	0	0	0	0	0	1	0	0
3	0	0	0	0	0	0	1	0	0	0
4	0	0	0	0	0	1	0	0	0	0
5	0	0	0	0	1	0	0	0	0	0
6	0	0	0	1	0	0	0	0	0	0
7	0	0	1	0	0	0	0	0	0	0
8	0	1	0	0	0	0	0	0	0	0
9	1	0	0	0	0	0	0	0	0	0

Fig 8(b)

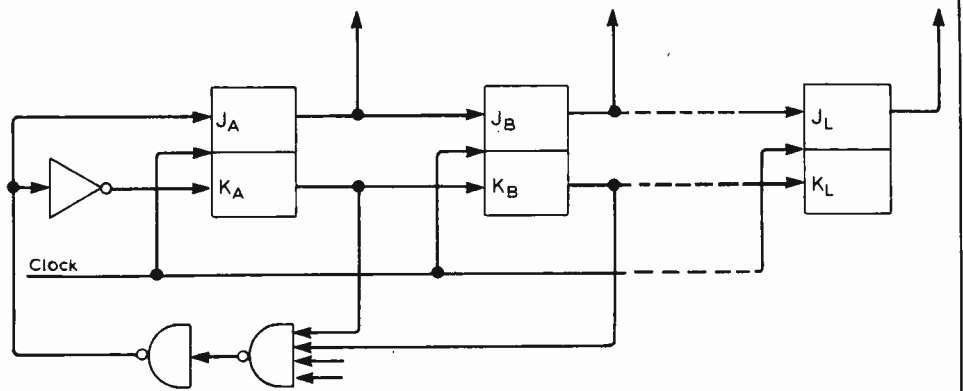


Fig 8(c)

Fig. 8. A basic ring counter (a) and the counting sequence for a decimal type. The two gates in (c) facilitate self starting and the circuit in (d) detects the presence of superfluous '1' states caused by malfunctions. The lack of a '1' in any stage is detected by the circuit at (e).

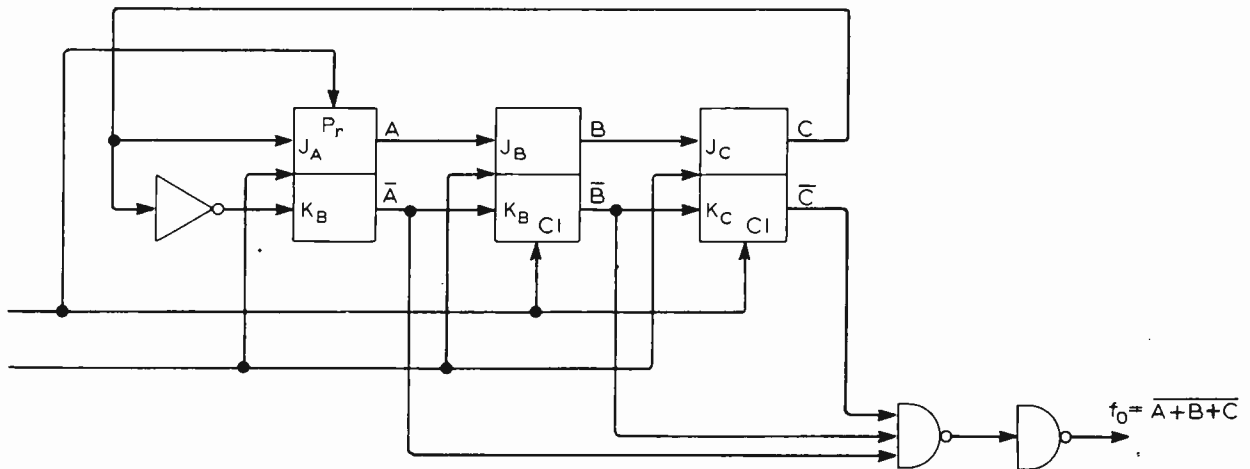


Fig 8(d)

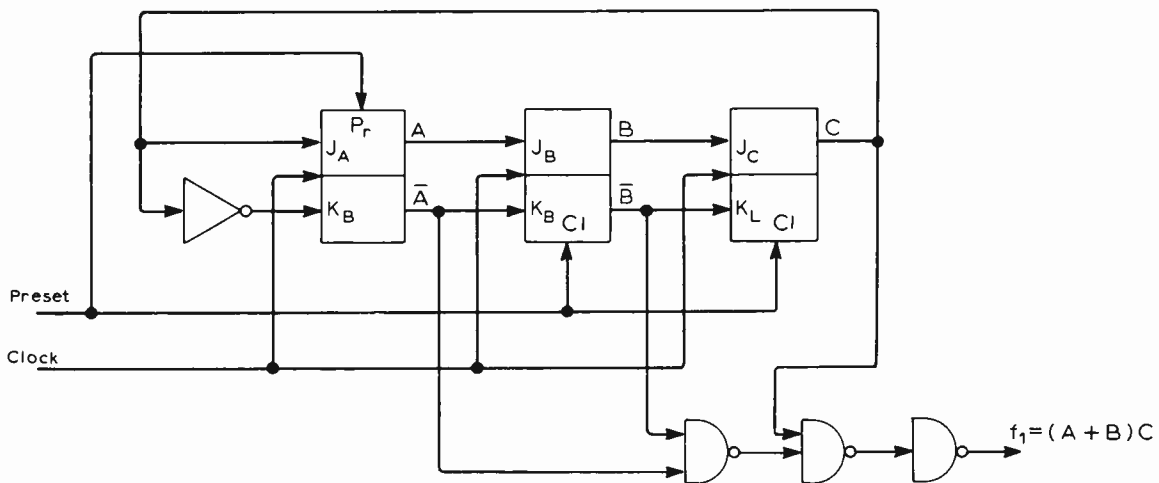


Fig 8(e)

some circuit fault also set to 1, or alternatively when the counting 1 is accidentally set to 0. However, it is not difficult to introduce simple logical networks which detect the presence of additional 1's. A three-stage ring counter having this facility is shown in Fig. 8(d). Similarly, it is not difficult to introduce a network which will indicate whether all sections of the shift register contain 0's. A circuit which will provide this facility is shown in Fig. 8(e).

The function required for the detection of additional 1's in the three stage circuit is  $f_1 = (A + B)C$ , and the function for indicating that all stages of the same circuit contains 0's is  $f_0 = \overline{A + B + C}$ .

**Twisted ring or Johnson counter**

As the name implies, the difference between the twisted ring counter and the ordinary ring counter is that the feedback connexions are reversed and in this case the complementary output of the last stage is connected to the J input of the first stage, whilst the inverted form of this signal is fed to the K input. If all the flip-flops are initially preset to the same state, either 0 or 1,

then the number of different states of the counter is equal to twice the number of stages in the shift register. Hence a decade counter can be constructed from a five-stage shift register as illustrated in Fig. 9(a). The counting sequence of the circuit, assuming that initially all the flip-flops are cleared to zero is given in Fig. 9(b).

This is a ten-state sequence which could have been selected from the universal state diagram of a five-stage shift register. The feedback logic could have been developed by first tabulating the required value of the feedback function in the column headed 'f' in the table of Fig. 9(b) and then plotting this function in conjunction with the unused states on a Karnaugh map as shown in Fig. 9(c). Simplifying, using the normal techniques, gives  $f = J_A = \overline{E}$ .

For this circuit, decoding logic is required to obtain a decimal count. This logic is obtained from a five-variable Karnaugh map on which the decimal equivalent for each of the states in the counting cycle has been marked as shown in Fig. 9(d). The unmarked states on this map represent the unused states. The simplifying adjacencies for decimal 0 and 1 have also been marked on the

map and if the reader cares to continue the process of simplification he will find that it is always possible to combine seven unused states with each decimal entry.

There are also three other undesired and independent count sequences for this counter. They are:

- (1)  $S_2 - S_5 - S_{11} - S_{23} - S_{14} - S_{29} - S_{26} - S_{20} - S_8 - S_{17} - S_2$
- (2)  $S_4 - S_9 - S_{19} - S_6 - S_{13} - S_{27} - S_{22} - S_{12} - S_{25} - S_{18} - S_4$
- (3)  $S_{10} - S_{21} - S_{10}$

If the counter should enter any one of these sequences, due to circuit misoperation, it will remain in that sequence unless arrangements are made to return the counter to the required sequence. This could be done by using the logic of the unused states to clear all stages of the counter and if required the same logic could be used to raise an alarm and stop the counter. It is left to the reader to show that the Boolean function that represents the unused states is:

$$f_u = \overline{A}DE + \overline{A}BC + \overline{A}CD + \overline{A}BC + \overline{A}DE + \overline{A}CD$$

If it is required to make the counter self-starting it is only necessary to choose three adjacent states on the Karnaugh map, such as  $S_6$ ,  $S_{14}$  and  $S_{10}$ ,

each of these states being from one of the unwanted sequences. If the Boolean function that represents these three states,  $f = \bar{A}BDE + \bar{A}BC\bar{E}$ , is used to clear the five stages of the counter then within a maximum of ten clock pulses it will return to the desired sequence.

The Johnson counter has an even-numbered cycle length of  $2n$ , where  $n$  is the number of stages in the register. However, with a suitable modification of the feedback it is possible to achieve an odd-numbered cycle length of  $2n-1$ . For example, if the 00000 state is omitted the counting cycle becomes that shown in the table of Fig. 10(a) and the value of the new feedback function required to produce this sequence is tabulated in the column headed  $f$ . Plotting this function in conjunction with the unused states on the Karnaugh map of Fig. 10(b) and minimizing leads to the revised feedback function  $f = \bar{D} + \bar{E}$ . Similarly, if the 11111 state is omitted rather than the 00000 state the revised feedback function can be shown to be  $f = \bar{D}\bar{E}$ .

**Shift registers with exclusive-OR feedback**

The four-stage shift register shown in Fig. 11(a) has exclusive-OR feedback from stages C and D such that the input to the first stage  $J_A = C \oplus D$ . To determine the sequence of states for the register it is assumed that initially the shift register is in the state  $D = 0, C = 0, B = 0$  and  $A = 1$  in which case  $J_A = 0 \oplus 0$ , and on receipt of the next clock pulse the register enters the state  $D = 0, C = 0, B = 1$  and  $A = 0$ . The complete sequence of states for the register is shown in Fig. 11(b), the value of the feedback function for each state being tabulated in the column headed  $f$ .

In all there are fifteen states and this is the maximum number of states a four-stage register can have, so this sequence is termed the maximum length sequence. The  $S_0 = 0000$  state is not included in the sequence since this is a 'lock-in' state. If the register enters this state  $J_A = 0 \oplus 0 = 0$ , so that the register is unable to leave this state when the next and subsequent clock pulses arrive. In general the maximum length sequence for such a circuit is given by the expression  $p_{max} = 2^n - 1$ , where  $n$  is the number of stages in the shift register.

Not all exclusive-OR connexions result in a maximum length sequence. The table in Fig. 12 gives the feedback functions which will give the maximum length sequence for values of  $n$  up to and including  $n = 10$ .

Clearly the circuit shown in Fig. 11(a) can be used as a binary sequence generator, the output sequence being taken directly from the output of one of the flip-flops in the register. In this case the binary sequence appearing at the output of flip-flop D is

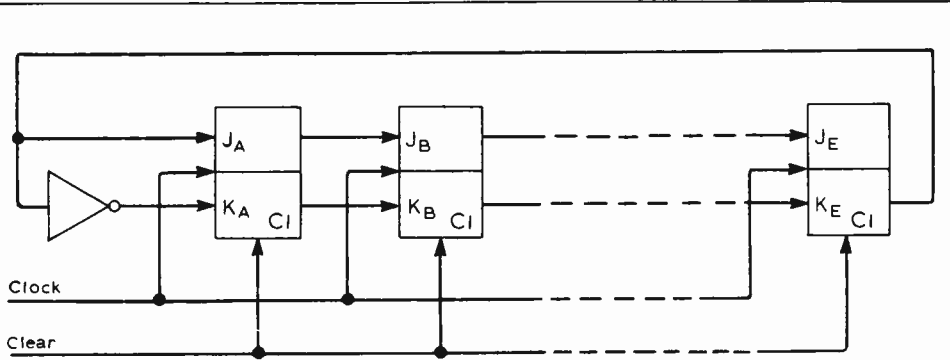


Fig 9(a)

Fig. 9. Twisted-ring decade counter (a) and its counting sequence (b). Maps at (c) indicate the method of determining the feedback function and at (d) the logic to decode the counter states for decimal indication.

Decode logic for outputs 0-9 is  $\bar{A}\bar{E}, A\bar{B}, \bar{B}\bar{C}, \bar{C}\bar{D}, \bar{D}\bar{E}, AE, \bar{A}B, \bar{B}C, \bar{C}D, \bar{D}E$ .

Clock pulse	E	D	C	B	A	f
0	0	0	0	0	0	1
1	0	0	0	0	1	1
2	0	0	0	1	1	1
3	0	0	1	1	1	1
4	0	1	1	1	1	1
5	1	1	1	1	1	0
6	1	1	1	1	0	0
7	1	1	1	0	0	0
8	1	1	0	0	0	0
9	1	0	0	0	0	0

Fig 9(b)

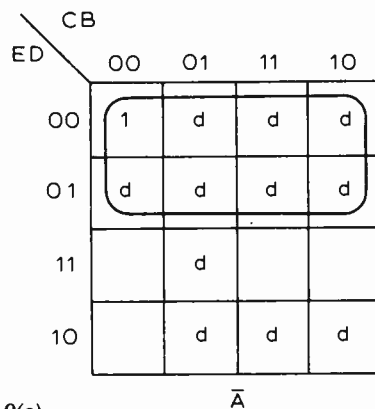


Fig 9(c)

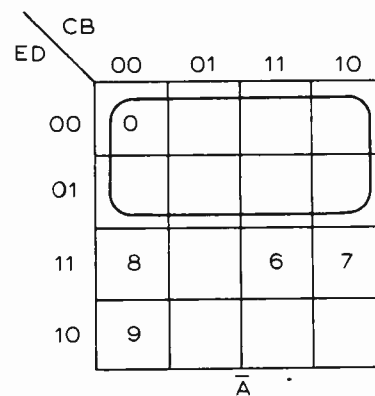
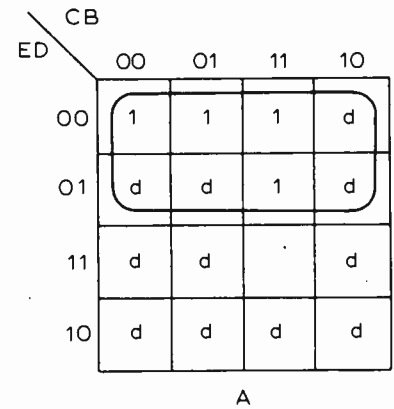


Fig 9(d)



E	D	C	B	A	f
0	0	0	0	1	1
0	0	0	1	1	1
0	0	1	1	1	1
0	1	1	1	1	1
1	1	1	1	1	0
1	1	1	0	0	0
1	1	0	0	0	0
1	0	0	0	0	1

Fig 10(a)

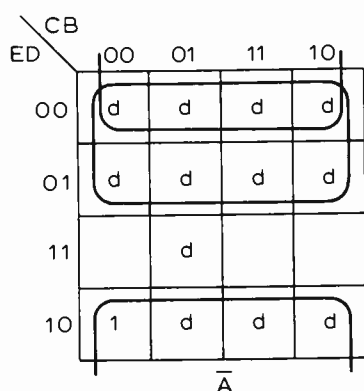
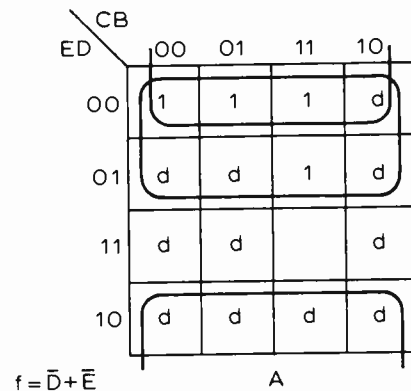


Fig 10(b)



$f = \bar{D} + \bar{E}$

Fig 10(c)

Fig. 10. Counting sequence of an odd-numbered cycle-length ring counter and the determination of its feedback function.

Fig. 11. Maximum-length four-stage register with exclusive-OR feedback ( $f = J_A = C \oplus D$ ).

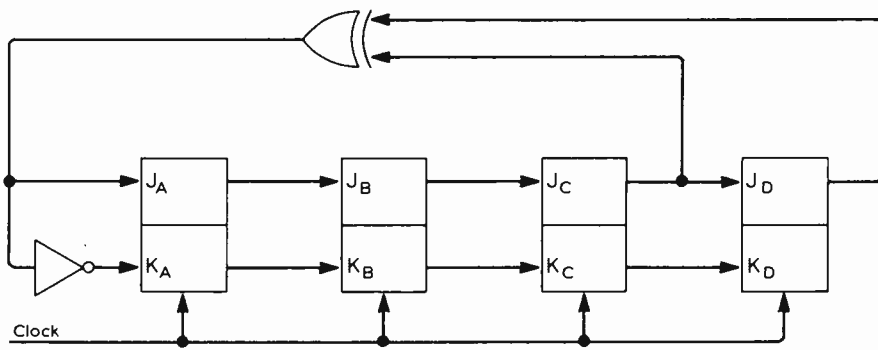


Fig 11(a)

0-0-0-1-0-0-1-1-0-1-0-1-1-1-1.

Non-maximum length sequences can be generated with the register shown in Fig. 11(a) if some other exclusive-OR function is used as the feedback. For example, if the feedback function is  $B \wedge D$ , one of the following sequences, tabulated in Fig. 13, will be generated. The sequence generated will depend upon the initial state of the register.

**Generation of long register sequences**

For values of  $n$  greater than five it is difficult to develop the de Bruijn diagram and hence the problem of designing a generator having more than thirty-one states using this diagram becomes quite complicated. A possible method of approach is to start with a maximum-length sequence generator using exclusive-OR feedback and then, if it is required, reduce the length of the sequence with additional feedback. The method will be described for a four-stage shift register, but it can also be used for shift registers having a number of stages in excess of four.

It will be assumed that a maximum length sequence generator having four stages is in the state  $D=0, C=0, B=1$  and  $A=1$ .

Hence:  
 $S = A \times 2^0 + B \times 2^1 + C \times 2^2 + D \times 2^3$   
 $= 1 \times 2^0 + 1 \times 2^1 + 0 \times 2^2 + 0 \times 2^3$   
 $= 3 = S_3$

If when the generator is in this state, the feedback is a 0 then the next state of the generator is  $D=0, C=1, B=1$  and  $A=0$ .

Then:  
 $S = 0 \times 2^0 + 1 \times 2^1 + 1 \times 2^2 + 0 \times 2^3$   
 $= 6 = S_6$

Alternatively, if the feedback had been 1 then the next stage of the generator would have been  $D=0, C=1, B=1$  and  $A=1$ .

Hence:  
 $S = 1 \times 2^0 + 1 \times 2^1 + 1 \times 2^2 + 0 \times 2^3$   
 $= 7 = S_7$

Examination of the table for a four-stage maximum length sequence generator, given in Fig. 11(b), shows that the feedback  $D \oplus C = 0$  when in the state  $S_3$  and the next state is therefore  $S_6$ . However, if the feedback is modified so that it is 1 then the next state is  $S_7$ .

The state diagram for the maximum length sequence generator having four stages is shown in Fig. 14(a) and it can be seen that by modifying the feedback the states  $S_6, S_{13}, S_{10}, S_5$  and  $S_{11}$  will be omitted from the sequence thus reducing its length from fifteen to ten states.

The modified sequence for the generator is shown in Fig. 14(b) and the modified value of the feedback function for state  $S_3$  is encircled. The feedback function in conjunction with the unused states  $S_6, S_{13}, S_{10}, S_5$  and  $S_{11}$  and the 'lock-in' state  $S_0$  are plotted on the Karnaugh map and simplified in the normal way as shown Fig. 14(c). This gives a modified feedback function of:

$f_m = C \oplus D + AB\bar{D} + \bar{A}BD$

The complexities of designing a generator to produce a long binary sequence without computing aids are obviously formidable. However, a computer programme has been deve-

S	D	C	B	A	f
$S_1$	0	0	0	1	0
$S_2$	0	0	1	0	0
$S_4$	0	1	0	0	1
$S_9$	1	0	0	1	1
$S_3$	0	0	1	1	0
$S_6$	0	1	1	0	1
$S_{13}$	1	1	0	1	0
$S_{10}$	1	0	1	0	1
$S_5$	0	1	0	1	1
$S_{11}$	1	0	1	1	1
$S_7$	0	1	1	1	1
$S_{15}$	1	1	1	1	0
$S_{14}$	1	1	1	0	0
$S_{12}$	1	1	0	0	0
$S_8$	1	0	0	0	1

Fig 11(b)

(b)

veloped for shift registers using exclusive-OR feedback to give the maximum length sequence, which gives the following information:

- the present state of the generator,
  - the next state of the generator,
  - the jump state,
  - the number of states excluded by the jump,
  - the length of the modified sequence.
- The designer has merely to scan the computer print-out to locate the length of sequence required and all the other

n	f	n	f
1	A	6	$E \oplus F$
2	$A \oplus B$	7	$F \oplus G$
3	$B \oplus C$	8	$D \oplus E \oplus F \oplus H$
4	$C \oplus D$	9	$E \oplus I$
5	$C \oplus E$	10	$H \oplus L$

Fig 12

Fig. 12. Feedback function for maximum length sequences.

Fig. 13. A different feedback function ( $f = B \oplus D$ ) results in non-maximum-length sequence.

Fig. 14. State diagram of a 4-stage register with modified feedback, showing the jump.

S	D	C	B	A	f
S <sub>1</sub>	0	0	0	1	0
S <sub>2</sub>	0	0	1	0	1
S <sub>5</sub>	0	1	0	1	0
S <sub>10</sub>	1	0	1	0	0
S <sub>4</sub>	0	1	0	0	0
S <sub>8</sub>	1	0	0	0	1

S	D	C	B	A	f
S <sub>3</sub>	0	0	1	1	1
S <sub>7</sub>	0	1	1	1	1
S <sub>15</sub>	1	1	1	1	0
S <sub>14</sub>	1	1	1	0	0
S <sub>12</sub>	1	1	0	0	1
S <sub>9</sub>	1	0	0	1	1

S	D	C	B	A	f
S <sub>6</sub>	0	1	1	0	1
S <sub>13</sub>	1	1	0	1	1
S <sub>11</sub>	1	0	1	1	0

Fig 13

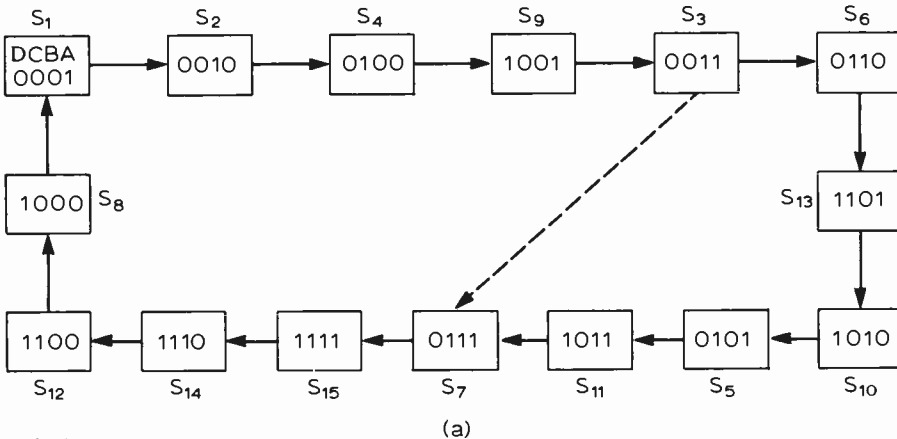


Fig 14(a)

S	D	C	B	A	f
S <sub>1</sub>	0	0	0	1	0
S <sub>2</sub>	0	0	1	0	0
S <sub>4</sub>	0	1	0	0	1
S <sub>9</sub>	1	0	0	1	1
S <sub>3</sub>	0	0	1	1	1
S <sub>7</sub>	0	1	1	1	1
S <sub>15</sub>	1	1	1	1	0
S <sub>14</sub>	1	1	1	0	0
S <sub>12</sub>	1	1	0	0	0
S <sub>8</sub>	1	0	0	0	1

Fig 14(b)

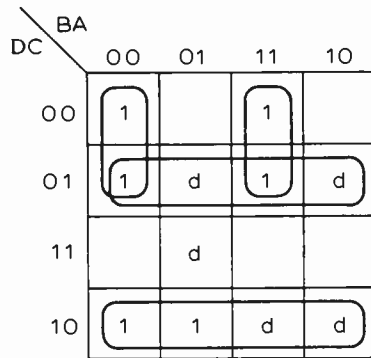


Fig 14(c)

information is immediately available. Finally it is necessary to develop the combinational logic which will provide the modification to the exclusive-OR feedback logic required to produce the desired jump.

**Further reading**

For further information on this subject the reader is referred to the following

- texts: Digital Engineering. G. K. Kostopolous. Wiley 1975.
- Shift Register Sequences. S. W. Golomb. Holden-Day 1967.
- Digital Logic and Switching Circuits. J. C. Boyce. Prentice-Hall 1975.
- Electronic Counters. R. M. M. Oberman. Macmillan 1973.
- Design of Digital Systems. J. B. Peatman. McGraw-Hill 1972.

# Literature Received

A catalogue of general electronic chassis hardware from Verospeed, the distributor company of the Vero group, is now available. New this time are metal-glaze resistors, trimmer pots, indicators and switches. Verospeed, 10 Barton Park Industrial Estate, Eastleigh, Hants. .... WW401

The Medilog electro-cardiogram analysis system is described in a 6-page brochure. The system provides hard copy of irregularities and variations from recorded data. Brochures can be obtained from Oxford Electronic Instruments Ltd, Ashville Industrial Park, Nuffield Way, Abingdon, Oxon OX14 1BZ ..... WW402

A catalogue giving full electrical and mechanical details of the Roband range of power supplies and regulators for both bench use and for use in equipment is obtainable from Roband Electronics Ltd, Charlwood, Horley, Surrey RH6 0BU ..... WW403

A booklet describing the use of Marconi instruments to measure automatically the quality of television systems by means of insertion test signals is produced by M.I. The booklet describes the use of TF2914A analyzer and monitor TF2915, which will provide limits comparison, auto scanning and control. For remote operation, data selector TK2917 is used and is also described. Marconi Instruments Ltd., Longacres, St Albans, Herts AL4 0JN ..... WW404

The British Standards Institution has just published BS5373, which is concerned with the electrical safety aspect of room aerials for radio and television. It can be obtained from BSI Sales Department, 101 Pentonville Road, London N1 9ND at £1.20.

Projex Distribution hold ranges of components by Bulgin, ITT (semiconductors), Lorlin (switches and capacitors), Multimech (switches) and Richco printed circuit hardware. A shortform catalogue has been produced and is obtainable from 303 Morland Road, Croydon CR0 6HF ..... WW406

**High quality book-shelf speaker**

The author has informed us that some dimensions in the parts list were incorrect. These have been amended below.

- Front grille mounting frame
- 4 off 18½ × ½ × ¼in.
- 4 off 12 × ½ × ¼in.

- Front grille
- 4 off 10⅞ × ½ × ¼in. hardwd square sec.
- 4 off 17⅞ × ½ × ¼in. hardwd square sec.
- 4 off 10⅞ × ½ × ¼in. triangular section.
- 4 off 17⅞ × ½ × ¼in. hardwd triang sec.

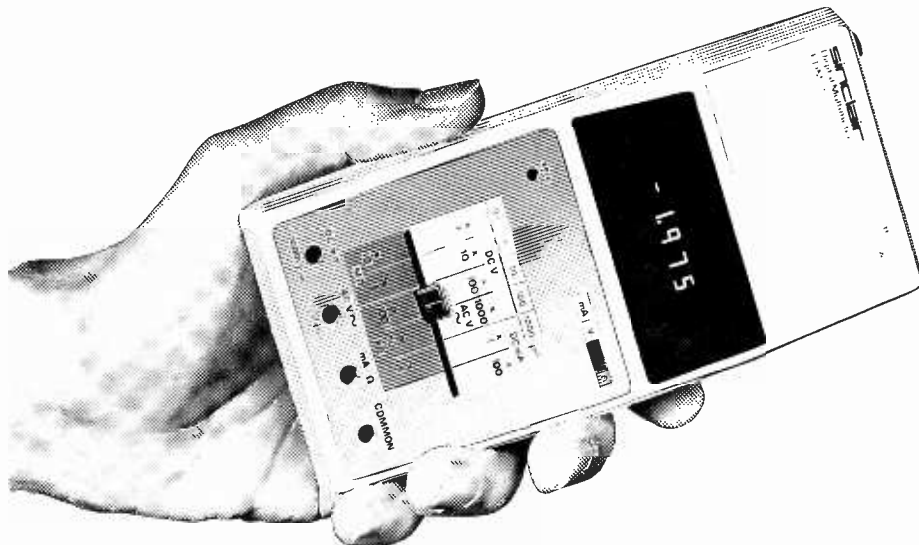
In Fig 9(c) the vertical dimension shown as 9in should be 9¼in. Dimensions for the two pieces of BAF wadding are 54 × 12in.

We understand that the T15 high frequency unit is no longer in production. Wilmslow Audio, 10 Swan Street, Wilmslow, Cheshire SK9 1HF, have informed us that they still have a quantity of these devices and are able to supply them ex stock.

# The Sinclair PDM35.

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Range: 1 mV to 1000 V.  
Accuracy of reading 1.0% ± 1 count.  
Note: 10 MΩ input impedance.  
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Range: 1 V to 500 V.  
Accuracy of reading: 1.0% ± 2 counts.  
**DC Current (6 ranges)**  
Range: 1 nA to 200 mA.  
Accuracy of reading: 1.0% ± 1 count.  
Note: Max. resolution 0.1 nA.

### Resistance (5 ranges)

Range: 1Ω to 20 MΩ.  
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Note: Also provides 5 junction-test ranges.

**Dimensions:** 6 in x 3 in x 1½ in.

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AC adaptor for 240 V 50 Hz power  
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I enclose cheque/PO for.....  
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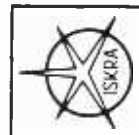
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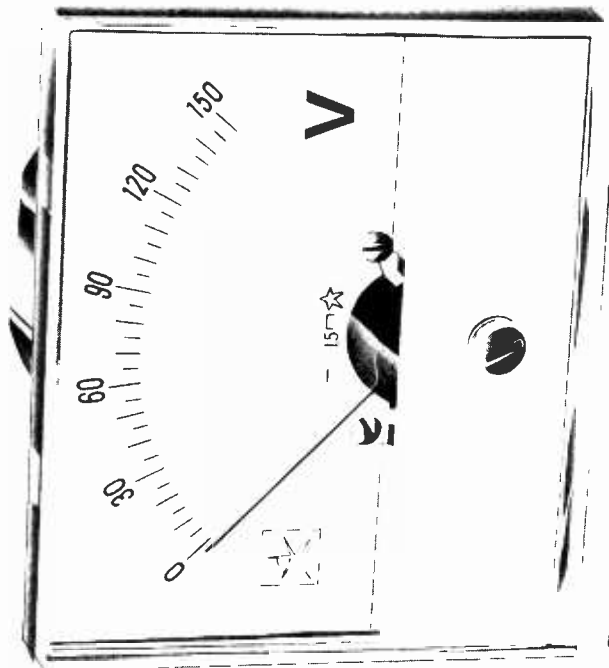
If you prefer a modern, easy-to-read range of meters, go for the Iskra Series N. Housed in a resilient plastic, with acrylic front, these panel instruments conform to IEC standards of mechanical and climatic conditions. There are 213 versions to choose from, covering AC and/or DC currents from 40µA to 40A, and AC and/or DC voltages from 100mV to 600V. Accuracy is ± 1.5% FSD.

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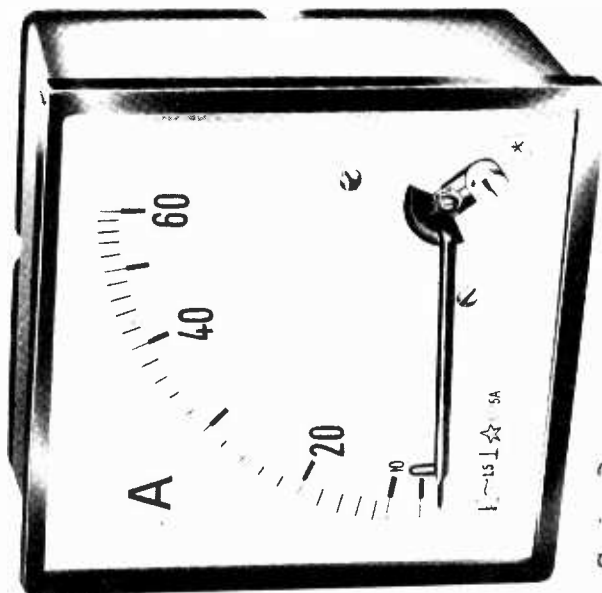
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# A check on Fourier

With some sidelights on the controversy about phase shifts

by M. G. Scroggie

One of the things we are all taught is that there is no kind of repetitive waveform which cannot be constructed by adding together pure sine waves. This is known as the Fourier principle. The frequencies of the component sine waves are all whole-number multiples of the basic or fundamental frequency of the waveform concerned (although a sine wave of that frequency is not necessarily present), these multiples being the harmonic frequencies.

This idea is not hard to accept when the wave has a smooth flowing shape. It is easy to see that the result of adding together the fundamental and third harmonic shown separately in Fig. 1 (a) is the rather peaky distortion of a sine wave shown at (b), and that therefore waveform (b) can be truly said to consist of the two sine waves (a). The degree of peakiness in (b) is obviously determined by the amplitude of the harmonic relative to that of the fundamental.

Note that even if the harmonic has the same relative amplitude, but a different phase relationship to the fundamental (c), the resulting waveform is quite different (d). This example shows the opposite kind of distortion — flattening of the peaks, such as could be caused by an amplifier with an input/output (or transfer) characteristic like Fig. 2 (a), compared with the perfect linear characteristic, (b).

But what about the sort of waveforms in television and radar? Fig. 3 shows a few typical ones. Is it really believable that such shapes can be made up of sine waves and nothing else?

A long time ago, when I was teaching students the elements of radar, I found that it was rare for anyone to question what was taught. In the Forces, at least, it was generally accepted that such awkwardness could only lead to trouble. It was prudent to keep one's head down. The teacher, on the other hand, could arrive at the alternative explanation that only the exceptional trainee had sufficient intelligence to ask a perceptive question. A more than usually perceptive one led ultimately to

an article in the December 1945 issue of *Wireless World*. Current discussion on the subject of phase, sparked off by the controversy on "linear phase" loudspeakers, suggested to me that certain diagrams in that article might be worth repeating for present readers, many of whom would not even have been born in 1945.

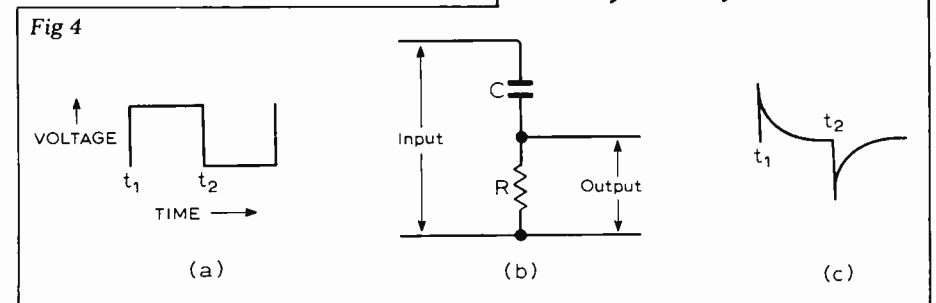
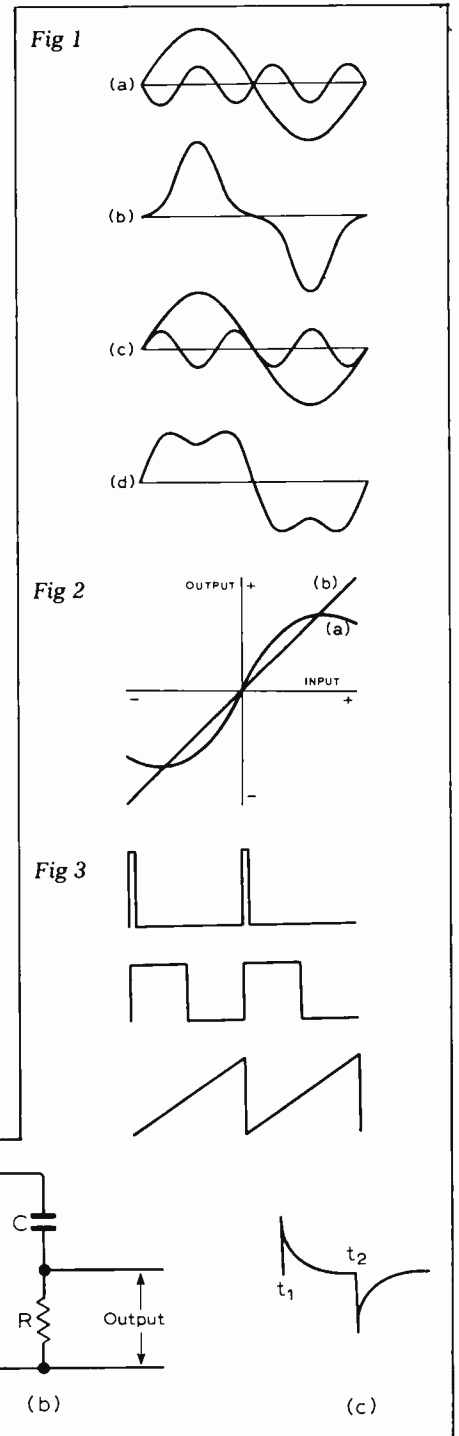
The question, quite awkward when first put without notice, but welcome as evidence that intelligently inquiring minds had not become extinct, was something like this: "Sir; you know you

Fig. 1 (a) shows a fundamental sine wave and third harmonic, and in (b) they are added together. (c) is the same as (a) except that the harmonic has been phase-shifted, and (d) shows how this changes the combined waveform.

Fig. 2 (a) is the sort of transfer characteristic that would distort a sine wave as in Fig. 1 (d), compared with the linear characteristic, (b).

Fig. 3 Typical sharp-cornered waveforms as used in television, etc. Can these too be made from sinewaves only?

Fig. 4 When square waves, of which a sample is shown at (a), are applied to the input of a CR circuit (b) having a shortish time constant, the output is a peaked wave (c). This conclusion is arrived at by an unusual route in the diagrams that follow.



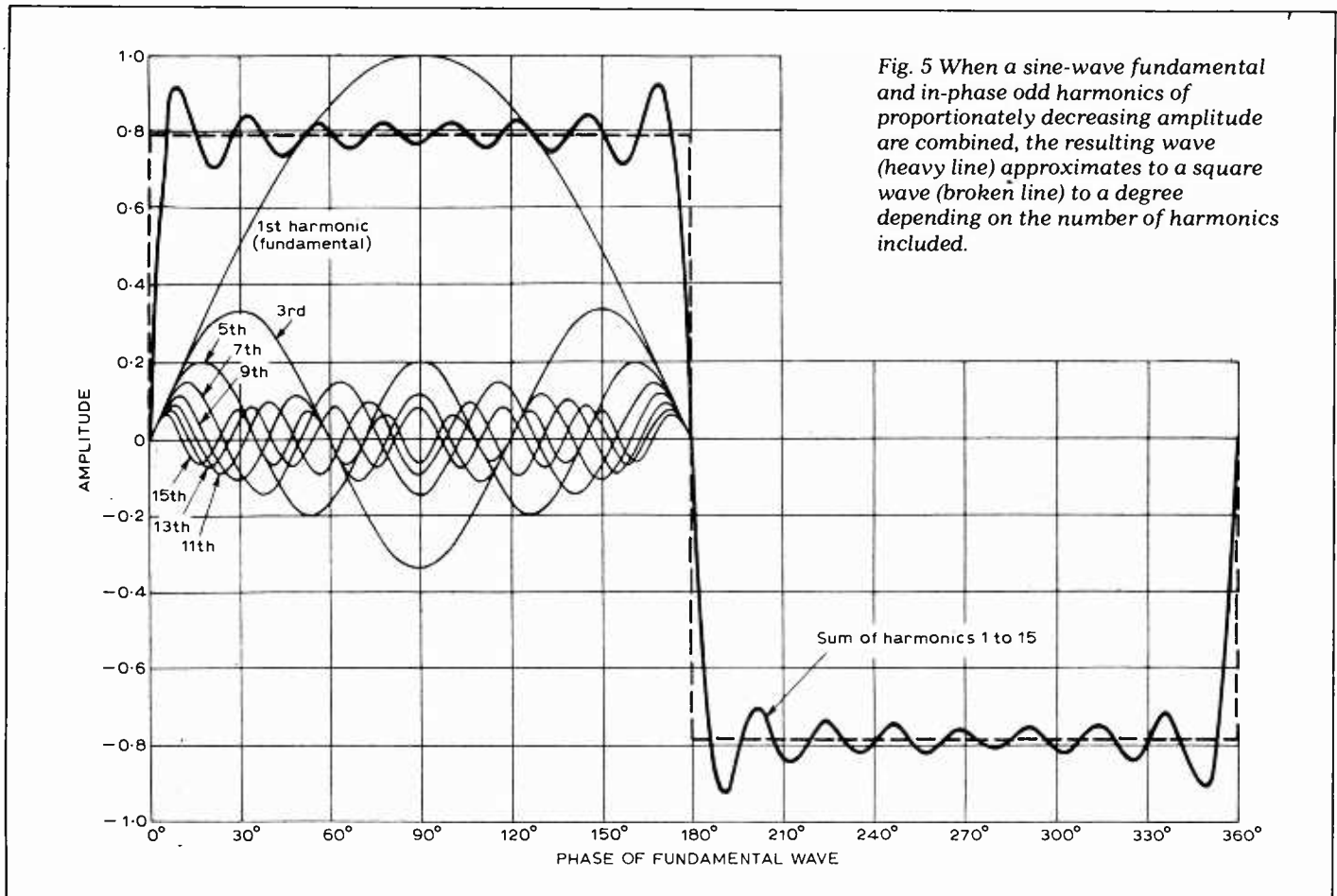


Fig. 5 When a sine-wave fundamental and in-phase odd harmonics of proportionately decreasing amplitude are combined, the resulting wave (heavy line) approximates to a square wave (broken line) to a degree depending on the number of harmonics included.

told us that all waveforms can be made up of sine waves? Well, how does that fit in with the way square waves are used to make pulses by passing them through short-time-constant circuits?" The technique to which he was referring can be seen in Fig. 4. The usual explanation of the process says nothing about the sine waves of which (a) is alleged to be composed. If these sine waves are followed separately through (b) will the results add up to the same as (c)?

The normal classroom treatment might say that at time  $t_1$  in the cycle of the perfect square wave (Fig. 4 (a)) the circuit (b) instantaneously receives a certain positive voltage. It is impossible for a capacitor to acquire a new voltage instantaneously through a resistor, as it needs time to charge; and therefore the whole of the applied voltage momentarily appears across R, as shown at (c), causing a current to start flowing through R into C, charging it in the well-known exponential manner. The smaller R is, the greater the current; and the smaller C is, the quicker a given current will charge it; therefore if  $C \times R$  is small the voltage across C will rise rapidly. Because the applied voltage is constant, that part of it which is across R will correspondingly die away, as shown by the exponential curve in (c) between  $t_1$  and  $t_2$ . Such a circuit in which CR is small is described as having a short time constant; the time constant being the time during which the capacitor charges to 63% of the constant applied voltage. It is numerically equal

to CR. At  $t_2$  the process is repeated in the negative direction. And so on for successive cycles.

Now for the synthetic method. The sine waves needed for constructing certain definite waveforms, such as those in Fig. 3, can be defined by a simple formula or prescription for each shape. The set of harmonics so defined is called a Fourier series. For a perfect square wave it consists of the fundamental and odd-numbered harmonics only — all of them; to infinity — the amplitude of each harmonic being inversely proportional to the number of the harmonic. Each starts off from scratch, with no phase delay. It is this mass start of an infinite number of sine waves that adds up to make the infinitely steep front of the square wave.

Expressed mathematically, and assuming for simplicity that the peak amplitude of the fundamental sine wave is 1, the series is therefore

$$\sin \omega t + \frac{\sin 3\omega t}{3} + \frac{\sin 5\omega t}{5} + \frac{\sin 7\omega t}{7} + \dots \text{to infinity}$$

where  $\omega$  is  $2\pi$  times the frequency of the square wave and  $t$  is time. As tables of sines are in terms of angles, it is more convenient to express the series as

$$\sin \theta + \frac{\sin 3\theta}{3} + \text{etc.}$$

each whole cycle of the square wave, or fundamental, being divided into  $2\pi$

radians or 360 degrees. Fig. 5 shows the series plotted up to and including the 15th harmonic, for half a cycle. Adding up the ordinates at frequent intervals along the half-cycle gives the waveform drawn in heavy line. It is obvious from the way the harmonics come into phase again at the end of the half-cycle that if they were continued for the second half-cycle they would make the same pattern, but inverted; and so the complete waveform has been repeated upside-down to complete the cycle. You will see that it fits fairly closely around a square wave drawn in heavy broken line with amplitude  $\pi/4$  (nearly 0.8) times that of the fundamental sine wave. The frequency of the superimposed ripple is the same as that of the highest harmonic included. You can either take my word for it that the difference between the ripply waveform and the perfect square wave is due solely to the limited number of component sine waves I had the patience to draw and add up (and that was quite a lot of patience), or else keep on drawing more of them yourself until belief sets in.

Incidentally, the diagram shows the amount of distortion that would be suffered by a perfect square wave in passing through a low-pass system having a sharp cut-off just above 15 times the frequency of the square wave.

Since each harmonic in the series is reduced in scale from the fundamental by the same factor in both horizontal and vertical dimensions, it has the same

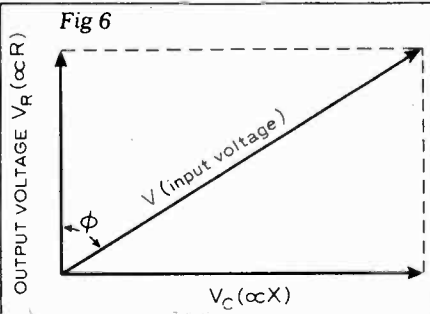


Fig. 6 Familiar graphical method for determining relative amplitudes and phase angles of output and input sine waves.

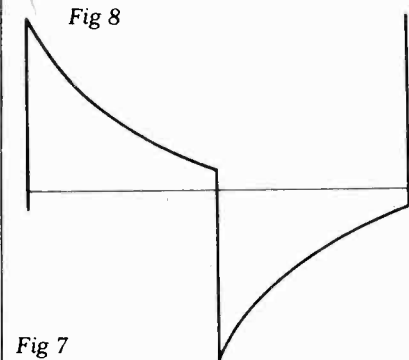


Fig. 8 A CR circuit that attenuates the fundamental of a square wave by only 1dB is accompanied by a phase shift that distorts the square wave as shown here.

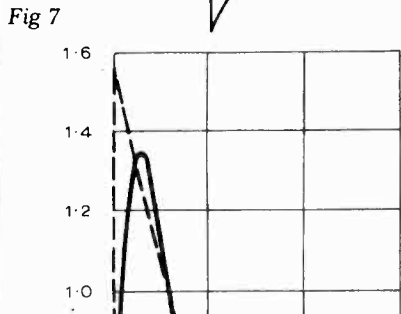


Fig. 7 (below) Recombining the separate harmonics at the output gives a waveform (heavy line) approximating to that (broken line) obtained by the usual method (or by including all the harmonics to infinity).

slope as the fundamental and the other harmonics at all corresponding parts of their cycles. The 1,000,001th harmonic starts off just as steeply as the fundamental, and as all start together the slope of the combined wave is infinitely great. It is only at half-cycle intervals that all the harmonics come into phase to form the vertical parts of the square wave; everywhere else the increasing values of some harmonics are offset by decreasing values of others, and the total remains constant

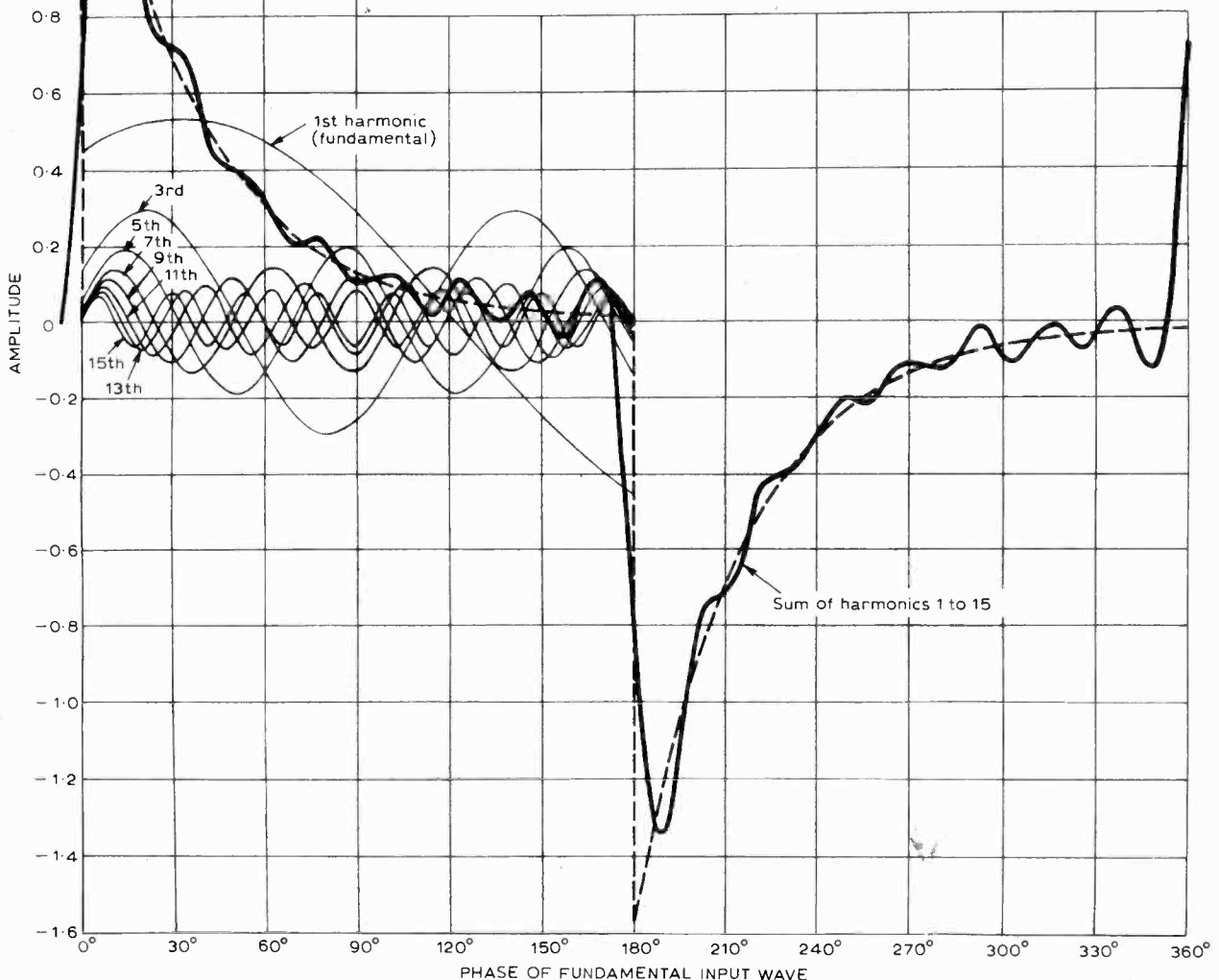
to form the flats of the square wave.

Having pondered this sufficiently for the manufacture of sharp corners using only smoothly curved ingredients to look less like a confidence trick, one can turn to consider the simple device through which it is proposed to pass the mixture: the short-time-constant circuit, Fig. 4 (b). Again there is absolutely no deception; only well-understood basic principles of simple sine-wave a.c. are to be used.

There are several methods for finding the amplitude and phase of the voltage at the output of this circuit, relative to the input. In all of them it is necessary to know the ratio of the capacitor's reactance,  $X$ , to the resistance,  $R$ ; and this is derived from the time constant. For the sake of a nicely proportioned diagram and simple numbers I have chosen a time constant equal to one tenth of a cycle of the fundamental. As the duration of a cycle is the reciprocal of the frequency, this relationship can be written as

$$CR = \frac{1}{10f_1}$$

where the suffix 1 indicates that  $f_1$  is the frequency of the fundamental (and other suffixes will distinguish the harmonics). The reactance,  $X_1$ , of the



capacitor at the fundamental frequency is

$$X_1 = \frac{1}{2\pi f_1 C}$$

which, from the foregoing,

$$= \frac{10R}{2\pi} = 1.6R \text{ (very nearly)}$$

Similarly

$$X_3 = \frac{1.6R}{3}, \quad X_5 = \frac{1.6R}{5},$$

and so on.

A graphical method for deriving the output phase and amplitude for each harmonic is shown in Fig. 6. The lengths of  $V$  and  $V_R$  respectively represent to the same scale the input and output voltages, and  $\phi$  is the angle by which the phase of the output is advanced by the circuit. For the fundamental,  $V_C$  is drawn 1.6 times as long as  $V_R$  (that is to say, in proportion to  $X_1$  and  $R$  respectively) and at right angles to it; and, if the drawing is accurate, the amplitude ratio,  $V_{R1}/V_1$ , is found to be 0.53, and  $\phi$  is  $58^\circ$ . For the third harmonic,  $V_C$  is drawn one-third as long, so  $\phi_3$  is much less and  $V_{R3}$  (third harmonic voltage across  $R$ ) is more nearly equal to  $V_3$ . But it is really  $V_{R3}/V_1$  (ratio of third-harmonic output to *fundamental*) that we want for plotting, and of course this is one-third as much. Similarly the phase shift in terms of the fundamental cycle is one-third of  $\phi_3$ .

The graphical method necessitates an accurate large-scale drawing, and as  $\phi_n$  is the angle whose tangent is  $X_n/R_1$ , and  $V_{Rn}/V_1$  is  $\cos \phi_n/n$  it is easier to get them from  $\tan$  and  $\cos$  tables. Here are the results tabulated up to the 15th harmonic:

n	$X_n/R$	$\phi_n$	$\phi_n/n$	$\cos \phi_n$	$\cos \phi_n/n$
1	1.600	$58^\circ$	$58^\circ$	0.53	0.53
3	0.5333	28	9.33	0.88	0.29
5	0.3200	17.6	3.52	0.95	0.19
7	0.2285	12.9	1.84	0.975	0.14
9	0.1777	10.1	1.12	0.985	0.11
11	0.1455	8.3	0.75	0.989	0.09
13	0.1230	7.0	0.54	0.99	0.076
15	0.1067	6.0	0.40	0.995	0.066

Columns 4 and 6 give the data by which each harmonic that emerges from the "peaker" was plotted in Fig. 7. Reassembling these mangled bits by adding ordinates again, we get the heavy-line curve. Comparing this with the heavy broken line, which is the exponential curve obtained by the "classroom" method, one must admit that the resemblance is too close to be dismissed as (in the film sense) "purely coincidental". In the geometrical sense it would actually coincide if all the (infinite number of) harmonics were included.

Some of us, oppressed by experience of our own fallibility, are never very confident about the correctness of our

calculations, be they financial or scientific, unless the same result is arrived at by at least two entirely different routes. So the recognizably similar results achieved by such diverse approaches as the exponential charging of a capacitor, and Fourier analysis and synthesis combined with plain a.c. theory, should enhance confidence in both these methods.

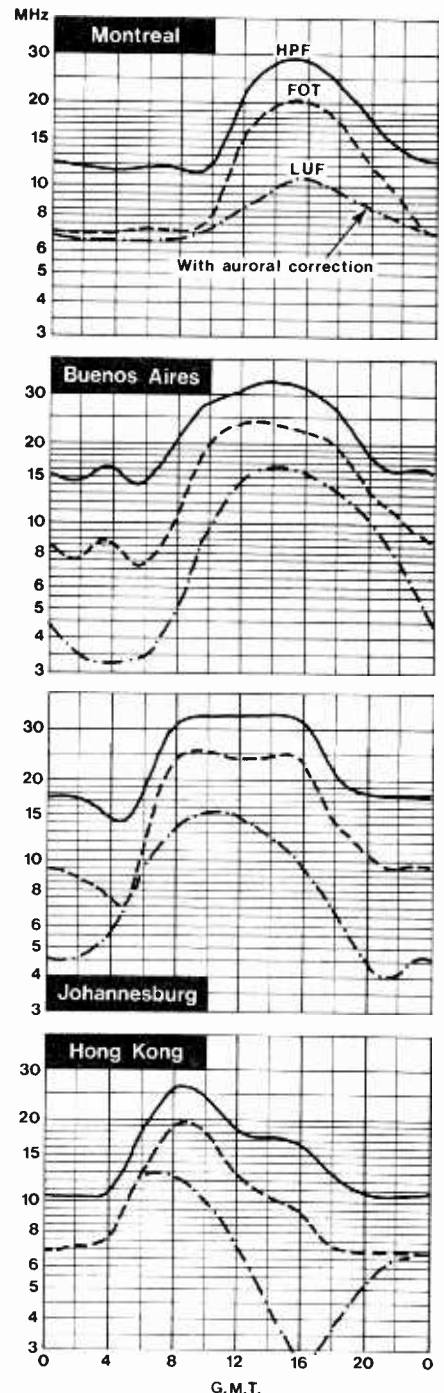
Some may consider all this to be merely academic, or even antiquarian. But now that the audio world is a battlefield between the forces of the establishment who contend that phase distortion, however drastic to the eye (compare (b) and (d) in Fig. 1), is imperceptible to the ear, and the revolutionaries who challenge this easy option for audio designers and claim that "linear phase" loudspeakers make all the difference to the discriminating listener, any sidelights on phase may be helpful. I don't intend to be caught in the crossfire, nor of course do I suggest that the gross distortion in Fig. 7 has any close connection with hi-fi, but one or two facts emerge in passing.

Phase shifts are inevitable in the audio chain, and, as James Moir has emphasized more than once, phase distortion can only be avoided if they are confined overall to equal *time* shifts at all frequencies. This condition is fulfilled in the direct sound path between loudspeakers and ears (but not necessarily in indirect paths) and in general it tends not to be fulfilled by electrical and mechanical circuits. This is exemplified in the fourth column of the table. True, this is an exaggerated case. But it also illustrates another fact, that even when what used to be called frequency distortion is kept within acceptable limits the accompanying phase distortion is much larger — numerically, that is to say; I refrain from assessing its impact, if any, on the listener!

For example, a CR circuit that reduces amplitude at a certain frequency by only 1dB causes a phase shift of  $27^\circ$ ; enough to distort the waveform visually more than might be expected. Working on the same lines as with Fig. 7, but making  $R = 2X$  (which gives 1dB loss of fundamental), we find that what the circuit does to a square wave input turns out as Fig. 8. And this assumes perfect representation of all frequencies above the fundamental. In practice there is bound to be a fall-off from some higher frequency upwards (as in Fig. 7, heavy line) with inevitable further distortion. And Fig. 8 is based on the assumption that the 1dB fundamental loss is due to one CR circuit; in practice it is likely to be split up among several of them in the audio system. With only two CR circuits, each causing 0.5dB loss, the total phase shift is more than  $38^\circ$ , which would make Fig. 8 look even less like a square wave. And so on for more CR circuits. There are counter-measures, of course; but it makes one think, perhaps.

# HF predictions

Circuit reliability is the product of the probability of ionospheric reflection and the probability of achieving a desired signal to noise ratio and is thus at a maximum somewhere between FOT and LUF. The term FOT, which is the French equivalent of OWF (optimum working frequency), is thus a misnomer since it relates only to skywave probability. However since LUF is dependent on many factors which cannot be generalised it is found satisfactory in practice to take FOT as being what it says it is.





# World of Amateur Radio

## Russian amateur-radio satellites

The long-rumoured Russian intention of setting up an amateur satellite system ("RS") has now been confirmed with the registration by the USSR of details with the ITU. RS will be based on three or four satellites carrying active transponders (up-link 145.8-145.9MHz, down-link 29.3-29.4MHz) with "maximum" communication distances of 6000km. The intended orbit has an inclination of 82° and will be circular at about 950km height with a period of 102 minutes. 144MHz transmissions should be possible with powers of about 10-15 watts to aerials of 10-12dB gain. The system is due in 1977-78 and the first launch could be as early as October.

The next Amsat-Oscar launch may be February 23, 1978. The ARRL has recently introduced a "DXCC" award for Oscar operation. Pat Gowen, G3IOR, with over 90 countries worked through Oscar, appears nearest to qualifying.

## "A. J. Alan", G2ST

Pre-war radio listeners will remember "A. J. Alan" as arguably the most polished radio storyteller of all time, who combined the writer's craft of a "Saki" (H. R. Munro) with an entirely original grasp of broadcasting techniques.

When he died, in December 1941, his true identity — Leslie Harrison Lambert — was at last revealed and he was said to have been a senior civil servant. He was also known as the holder, since the early 1920s, of the amateur call-sign G2ST.

In a recent radio tribute to A. J. Alan, Tony Bilbow, aided by the researches of Norman Duret of Bristol, filled in a number of missing details — for instance his early career as a professional entertainer — but curiously failed to follow up the clues that suggest Lambert's real occupation throughout the inter-war years.

The programme noted that in 1915 Lambert was at the Admiralty's secret

radio interception station at Hunstanton. This was one of the network of receiving stations set up by Commander R. Bayntun Hippersley (HLX, later G2CW), a prominent Somerset landowner, after he and E. Russell Clarke (THX), a barrister, had proved to the Admiralty that experimental amateurs were able to receive, in the UK, German navy traffic at ranges much greater than had been supposed. This in turn led directly to the setting up of the Room 40 code-breaking unit at the Old Admiralty Building in Whitehall, with its many triumphs under Sir Reginald Hall, and working jointly with the early d.f. stations built by H. J. Round of Marconi's.

It would seem Lambert stayed with this organisation as a signals expert when in 1919 it was renamed as a "Code and Cypher School" and again later in 1926 when it came under MI6 and moved to that organisation's headquarters near St James's Park. Yet Tony Bilbow, misled by the "cover name", described this as "Certainly no longer secret work"! In 1939, as GCCS, the codebreakers moved to Bletchley Park and became what has been called "possibly the most crucial factor in enabling the Allies to defeat Germany" as a result of cracking the Enigma and other German codes. The cryptographers included Alastair Denniston, Alfred Dilwyn Knox and the still largely unrecognised genius of the tragic Alan Turing, whose dream of a "universal machine" led directly to the first electronic computers, such as "Colossus" built by T. H. Flowers of Post Office Research and used for codebreaking from about 1943.

"A. J. Alan" may thus, throughout the time he was a highly popular radio "star", have been not only G2ST, but also — without the BBC knowing it — a key figure in the most successful department of the British secret intelligence service!

## In the air

The GB3LER beacon station on Lerwick, The Shetlands, has been re-activated after an interval of many years; it transmits on 145.965MHz with a power of 10 watts to two aerials, beaming south and north-east. The new 10GHz beacon on Alderney, Channel Islands (Gunn oscillator with 15dB horn aerial) has been heard by amateurs along the south and south-east coast of England at distances up to 170km. 144.2MHz c.w. signals from TU2EF (Ivory Coast, West Africa) were heard in Sao Paulo, Brazil by PY2OB during June, possibly the first Atlantic crossing for two-metre signals.

From January 14 to 22, 1978, a special event station, KM1CC, will mark the 75th anniversary of the first two-way radio transmission by Marconi between the USA and England. KM1CC will operate on all h.f. bands from the original site of station "CC" (later MCC

and WCC) in the Cape Cod National Seashore Park in South Wellfleet, Mass, although part of the site is now submerged in the Atlantic Ocean due to soil erosion. It will be permitted to use A2 c.w. to reproduce the sound of the old 240Hz rotary spark gap. The Cornish Radio Club will similarly operate a special station at Poldhu, Cornwall. A message from President Carter will be transmitted from KM1CC.

*Mercury*, the journal of the Royal Signals Amateur Radio Society, has published what may be the first account of the use of a 725Hz transversal filter (based on 741 op-amp all-pass filters) to provide coherent addition of amateur c.w. signals, while filtering out non-coherent static and electrical interference without the "ringing" of conventional sharp filters. One model, described by F. J. H. Charman, G6CJ, uses four all-pass-filter sections, with each section introducing 180° phase shift with outputs added in a different amplifier and with a bandpass filter to reduce side lobes.

Reg Patrick, G2BBX, acting on the advice of W. B. Whalley of California, author of the paper "Radio-frequency eradication of tumours" (IEE's *Electronics & Power*, May 1977) recently successfully treated one of his geese, using a few watts of 14MHz r.f. power. This improved technique for r.f. diathermy uses electric-field coupling rather than the conventional electromagnetic field coils used over many years for r.f. diathermy.

The sixth National Amateur Radio Exhibition, organised by the Amateur Radio Retailers' Association, is being held at the Granby Halls, Leicester, on October 27, 28 and 29 (10a.m. to 6p.m. daily).

## In brief

The RSGB has set up an ad hoc committee to consider the geographical coverage, frequencies, modes, times and contents of the GB2RS weekly news broadcasts . . . The FCC has postponed for the time being the introduction in the United States of a phone-only "communicator licence" for the 220 and 420 MHz bands which would not have required a Morse test . . . The ten-metre beacon station GB3SX has changed frequency to 28.215MHz. . . The IEE's recent "Report on the use of the radio spectrum" comments that "the allocations of frequency spectrum for the use of amateur communicators and experimenters should be preserved in view of their significant contribution to the radio art". The report also notes that "interference from non-conforming broadcast stations has rendered some amateur h.f. allocations almost unusable" . . . The ARRL is to have a full-time staff lobbyist at Washington, DC.

PAT HAWKER, G3VA

# Synthesized f.m. transceiver — 1

## A simple 40-channel, two-metre design

by T. D. Forrester, G8GIW

This article describes the design and construction of a two-metre (145 to 146MHz) f.m. transceiver. The two main design considerations for the unit were ease of mobile operation and low power consumption for portable operation. To comply with the former criterion, channelized operation was chosen, the appropriate channel being selected by means of thumbwheel switches.

Standard and well-proven circuitry is used in the receiver section of the transceiver and it requires little

alignment to achieve maximum performance. The selectivity of the receiver is determined by the bandwidth of the 10.7MHz crystal filter. In the prototype a 25kHz filter was used to accommodate some of the wider n.b.f.m. stations, again to minimize i.f. alignment.

The transmitter section uses conventional Class C frequency multipliers and, to obtain maximum efficiency, the driver and p.a. stages are also run in the Class C mode. The transmitter, which is a modified Mullard design, has been

used by the author for several years in various applications and should present no difficulties in alignment.

### Operation

The operation of any radio equipment while mobile is hazardous, so in an attempt to lessen the danger, all controls are kept simple and easy to operate.

The synthesizer has only two controls; mode and channel selection. The mode switch selects normal transceiver operation, repeater opera-

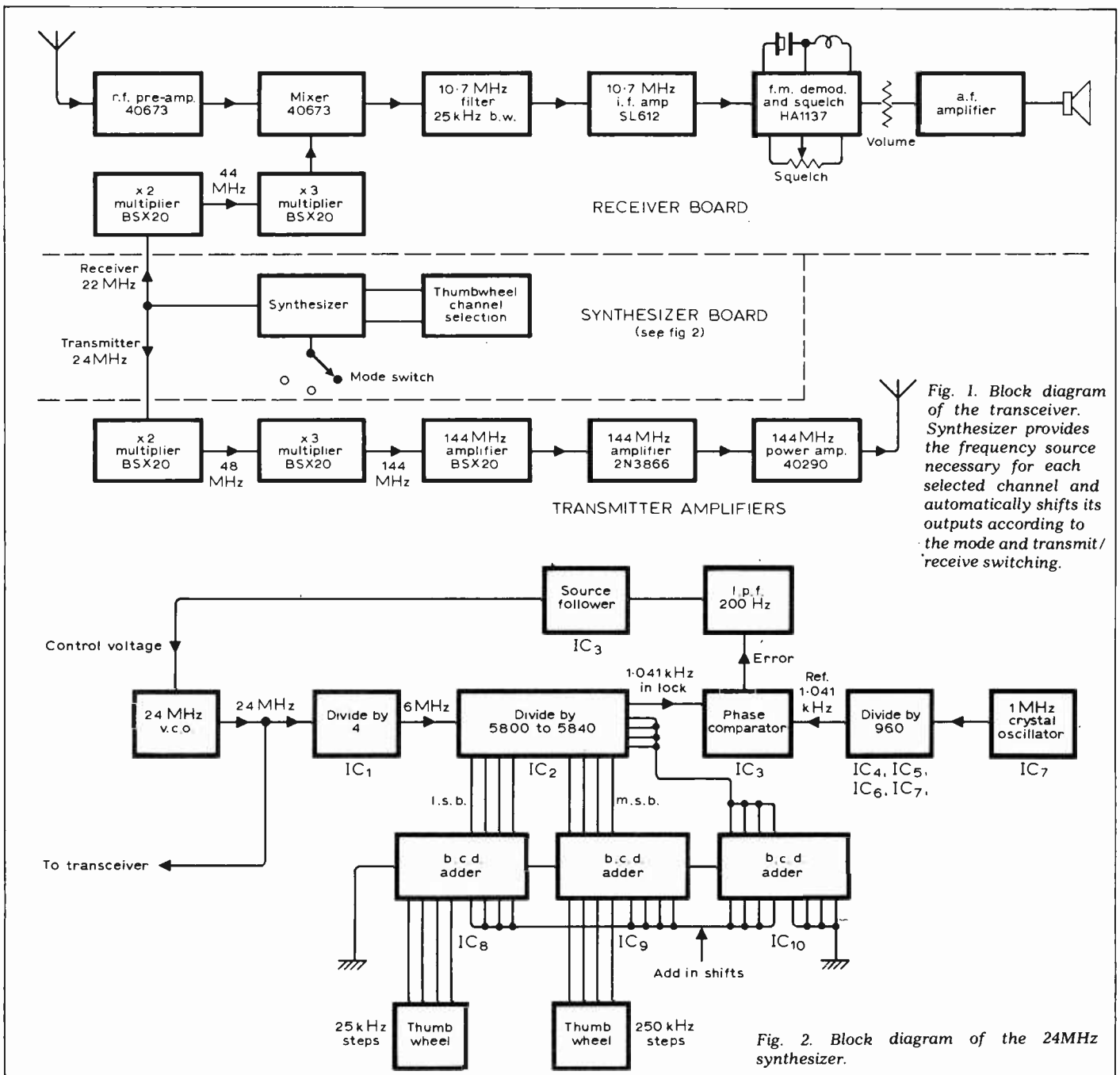


Fig. 1. Block diagram of the transceiver. Synthesizer provides the frequency source necessary for each selected channel and automatically shifts its outputs according to the mode and transmit/receive switching.

Fig. 2. Block diagram of the 24MHz synthesizer.

tion (where the transmitter operates 600kHz below the selected channel), or inverse repeater operation (where the receiver operates 600kHz below the selected channel).

Two thumbwheel switches are used to select any channel between 00 and 40; channel 00 corresponds to S0 (145MHz), channel 20 corresponds to S20 (145.500MHz), and so on, enabling easy channel identification. See Fig. 2.

The receiver has a volume control and a squelch control. The squelch control serves its normal function of muting the receiver in the absence of a signal. It may be adjusted once for one

channel and then left, requiring no further adjustment for any other channel.

The volume control requires little comment, as it serves its usual purpose of controlling the audio output power, in this case up to a maximum of 200mW. This audio level may seem rather low, but it has been found to be sufficient under all but the noisiest of environments.

The transmitter has only a deviation control, which may also be preset so that it requires no adjustment when changing channels or switching on or off.

**The synthesizer**

To avoid using a costly v.h.f. prescaler, a 24MHz generation system was chosen for the synthesizer. The 25kHz channel spacing in the 145MHz band then becomes 4.1666kHz with respect to 24MHz. Also, by employing a generation frequency of 24MHz on transmit and 22MHz on receive, as in Fig. 1, it enables the synthesizer to be used separately with most commercial transceivers with little or no modification.

The heart of the synthesizer is the integrated circuit (IC<sub>2</sub>), which is a programmable five-stage divider type.

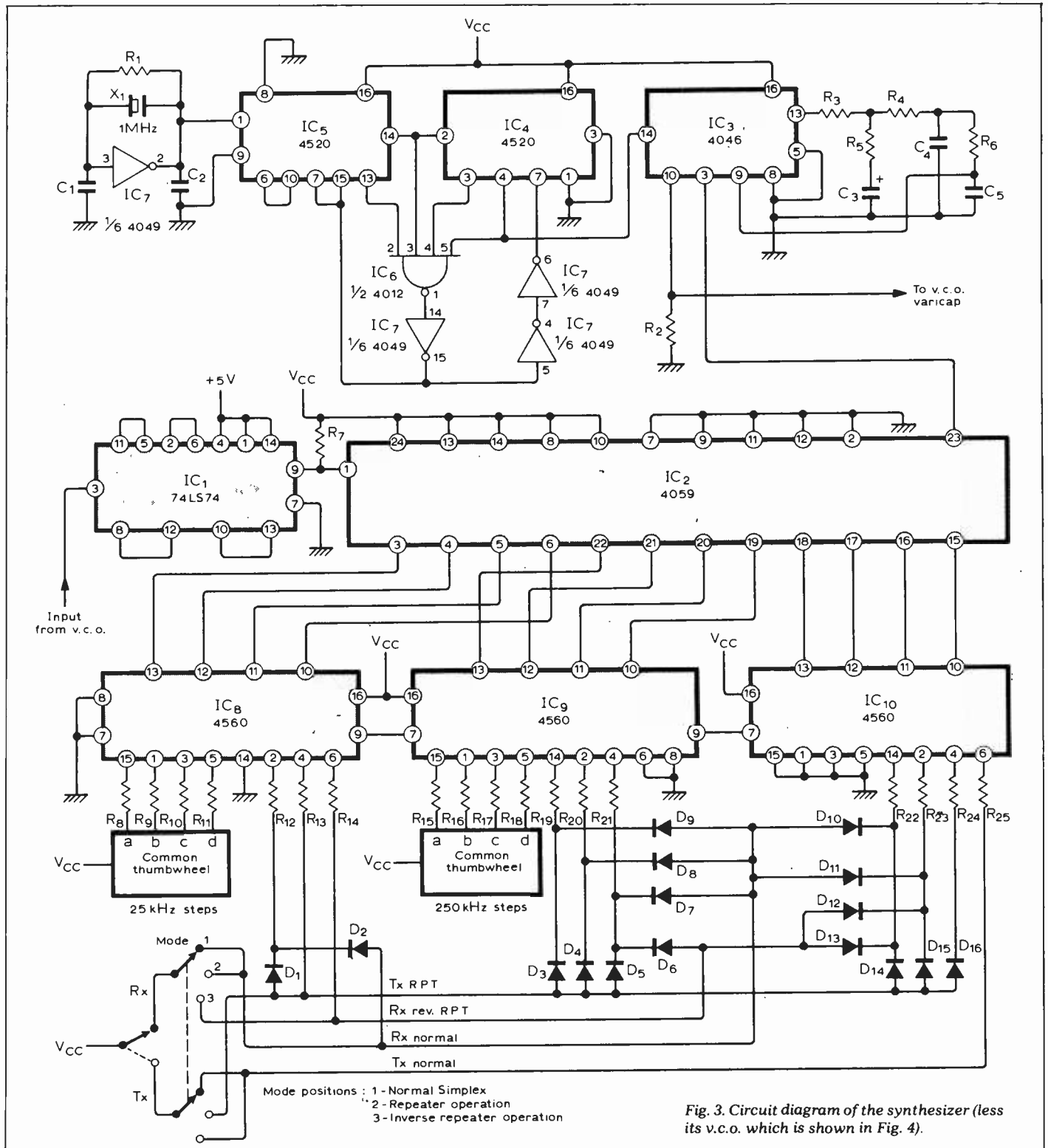


Fig. 3. Circuit diagram of the synthesizer (less its v.c.o. which is shown in Fig. 4).

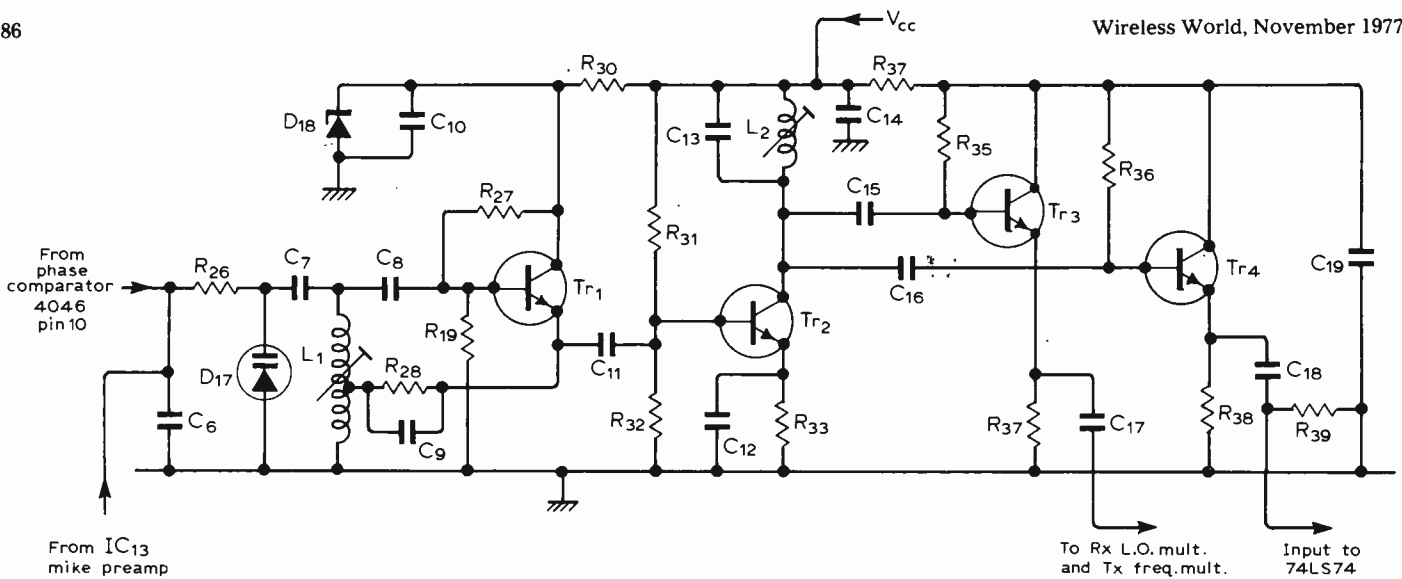


Fig. 4. Circuit diagram of the voltage controlled oscillator which is controlled by the synthesizer phase lock loop.

4059. However, only four of these stages are used. Unfortunately, because the 4059 is a c.m.o.s. device, it has a maximum frequency of 6MHz, so a divide-by-four prescaler is required to accommodate the 24MHz generation frequency. This function is achieved by a 74LS74 dual-D-type flip flop.

This further division of four reduces the channel spacing to 1.041666kHz at 6MHz, and also sets the phase-comparison frequency at 1.041666kHz.

The 1.041666kHz reference frequency is derived by dividing a 1MHz crystal oscillator by 960. This division is accomplished by IC<sub>4</sub>, IC<sub>5</sub>, IC<sub>6</sub> and IC<sub>7</sub>. IC<sub>7</sub> also functions as the 1MHz oscillator, as shown in Fig. 3.

For the synthesizer to generate the appropriate frequencies, for channel 00 operation for example, the divide-by-N divider (IC<sub>2</sub>) must divide by 5800 for normal transmit, 5372 for normal receive, 5776 for repeater transmit, and 5348 for inverse repeater receive.

Since the 5 is common to all of the above, this is hardwired on the 4059. The '800, '372, '776 and '348 are added to the selected channel in IC<sub>3</sub>, IC<sub>9</sub> and IC<sub>10</sub>, which are four-bit binary-coded-decimal (b.c.d.) adders.

Consider the normal transmit case above, where the 4059 must divide by 5800 to generate 145MHz. In the 24MHz region, 145MHz is represented by 24.1666MHz, and for this to be phase locked to 1.041666kHz it must be divided by 23,200. As the 4059 is preceded by a divide-by-four prescaler, it has only to divide by 23,200/4, which is 5800.

If channel 21 (145.525MHz) is selected, this number is added in b.c.d. form to the appropriate shift in the b.c.d. adders. Therefore, on transmit, the 4059 would be programmed to divide by 5821, and so on.

The 4046 (IC<sub>3</sub>) serves as the phase comparator and source follower, which then feeds the error signal to the v.c.o., (see Fig. 4). The low pass filter is needed to remove the 1.041666kHz ripple from the phase comparator and is formed by

the RC network associated with the 4046. The v.c.o. used conventional transistor circuitry and operates between approximately 22 and 24.5MHz, depending upon which mode and channel is selected.

(to be continued)

**Components list**

**Resistors** (all 10% 1/4W unless otherwise stated)

1	1M	49	82
2	18k	50	120
3	1k	51	10
4	2.7k	52	3.9k
5	4.7k	53	10k
6	2.2k	54	3.3k
7	2.2k	55	1k
8 to 25	220k	56	33k
26	12k	57	100
27	5.6k	58	1k
28	680	59	47
29	3.9k	60	100
30	220	61	100
31	5.6k	62	390
32	3.9k	63	1
33	330	64	1
34	100	65	18 to 47
35	39k		(see text)
36	39k	66	120k
37	470	67	10
38	470	68	470
39	3.3k	69	1.8k
40	39k	70	3.3k
41	47k	71	180
42	220	72	47
43	100	73	10k
44	10k	74	150
45	3.3k	75	10
46	470	76	100k
47	680	77	1k
48	470	78	27k
		79	220

**Crystals**

1	1MHz
2	10.7MHz

**Coils**

1	10 turns 30 s.w.g., tapped 2 turns from earth, 4mm int. dia.
2	15 turns 30 s.w.g., tapped 2 turns from earth, 4mm int. dia.
3	5 turns 20 s.w.g. 1/4in int. dia. 1/2in long
4	As L3
5	As L3
6	470µH choke
7	7 turns 32 s.w.g. 4mm int. dia.
8	As L3
9	As L7
10	As L3
11	4 turns 20 s.w.g. 1/4in. int. dia. 5/8in. long
12	As L3
13	3 turns 20 s.w.g. 1/4in int. dia. 1/2in. long
14	As L13

All r.f.cs use three turns of 32 s.w.g. wire, on a FX1115 ferrite bead.

**Variable resistors**

80	25k linear
81	25k log.
82	100k linear preset

**Capacitors** (µF unless otherwise stated)

1	56p	30	100n
2	22p	31	2.2n
3	1.35V tant	32	10n
4	220n	33	10n
5	220n	34	100
6	2.2n disc	35	100n
7	68p	36	100n
8	15p	37	1n disc
9	2.2n disc	38	33p
10	2.2n disc	39	1n disc
11	2.2n disc	40	10p
12	2.2n disc	41	1n disc
13	10p	42	1n disc
14	2.2n disc	43	470, 16V
15	15p	44	220, 16V
16	15p	45	1.35V tant
17	2.2n disc	46	1n disc
18	2.2n disc	47	2.2n
19	2.2n disc	48	2.2n
20	1n disc	49	15p
21	1n disc	50 to 58	1n disc
22	1n disc	59	10
23	10n	60	4.7n
24	10n	61	2.2
25	2.2n	62	50
26	56p	63	100n
27	10p	64 to 73	3.3p
28	2.2n		trimmers
29	10n	74	1000p

**Transistors**

1 to 4	2N3707	11	2N3707
5	40673	12	BSX20
6	40673	13	BSX20
7	2N3707	14	BSX20
8	BFR79	15	2N3866
9	BFR39	16	40290
10	BSX20		

**Diodes**

1 to 16	1N914	20	7.5V zener
17	BA121	21	OA200
18	8.2V zener	22	6.1V zener
19	1N914		

**Integrated circuits**

1	74LS74	8	4560
2	4059	9	4560
3	4046	10	4560
4	4520	11	SL612
5	4520	12	HA1137
6	4012	13	SL622
7	4049		

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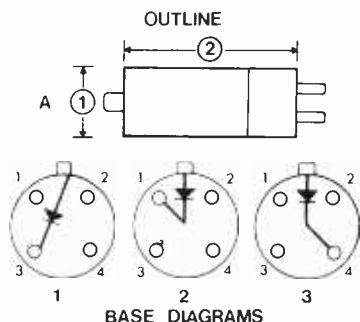


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- 1K24, 2-100A/100R, 2G/402A, 2G/472B, 2H28, 2H66, 2V/400A, 3B24, 3B24W, 3B24WA, 3B25, 3B28, 4B31, 4B32, 4H32, 4H72, 4H73, 4H88, 4Q025, 5AU4, 5AW4, 5AZ4, 5Q105, 5R4, 5R4GY, 5R4WGA, 5R4WGB, 5R4WGY, 5T4, 5U4, 5URGT/G, 5U4GB, 5V3, 5V4, 5V4G, 5W4, 5W4G/T, 5Y3, 5Y3GT/G, 5Y3WGT, 5Z3, 5Z4, 5Z4GT/G, 6AU4, 6AX4, 6AX5, 6BL4, 12AX4, 17AX4, 25W4, 52KU, 80, 82, 83, 83V, 100R, 249C, 428T, 575A, 673, 732A, B16, B36, 866A, 866JR, 872A, 966A, 974A, 975A, 3572, 3885A, 4064B, 6012, 8008, 8020, 8020/100R, 8020W
- AG5006, AG5014, AH201, AH217, AX-224, AX-230, AX673, CE230, CR273, CR274, CR275, DCG4/1000G, DCG5/5000GB, DCG5/5000GS, DCX4/1000, DCX4/5000, DQ2, DQ4, DQ4C, DQ45, DQ51C, DX2, ESU103, F366A, F353A/B, G5A, GL451, GL512A, GL-816, GL-836, GLe13000/1.5/6, GU12, GU25, GXU1, GXU2, GZ30, GZ34, ML727, O24, O24A, PA5021, R52, R66, R72, R6146, RG3-250A, RG1000-3000, RR3-250, RR3-1250, RY12-100, TH5021B, TH5221V/B, TH5031B, U50, U52, V40, VH530A, VH7400, VT42A, VT46A, VT216, W-816, WL578.

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816-SS	8000	250	12.0	A	35	105	1	A4-9	C1.1
866A-SS	10000	300	14.0	A	35	140	3	A4-10	C1.5
3B24-SS	20000	500	28.0	A	35	140	3	A4-10	C1.5
RR3-1250-SS	10000	1250	14.0	A	48	208	2	A4-29	C1.5
DCG5/5000GB-SS	10000	1500	14.0	A	48	208	2	A4-29	C1.5
8008-SS	10000	1250	14.0	A	56	198	2	A4-18	C1.5
WL-575A-SS	15000	1750	20.0	A	48	208	2	A4-29	C1.5
4H73-SS	15000	1750	20.0	A	56	246	2	A4-18	C1.5
8020/100R-SS	40000	100	60.0	A	35	105	2	A4-10	.375
8020W-SS*	parameters available on request			A	35	105	2	A4-10	.375
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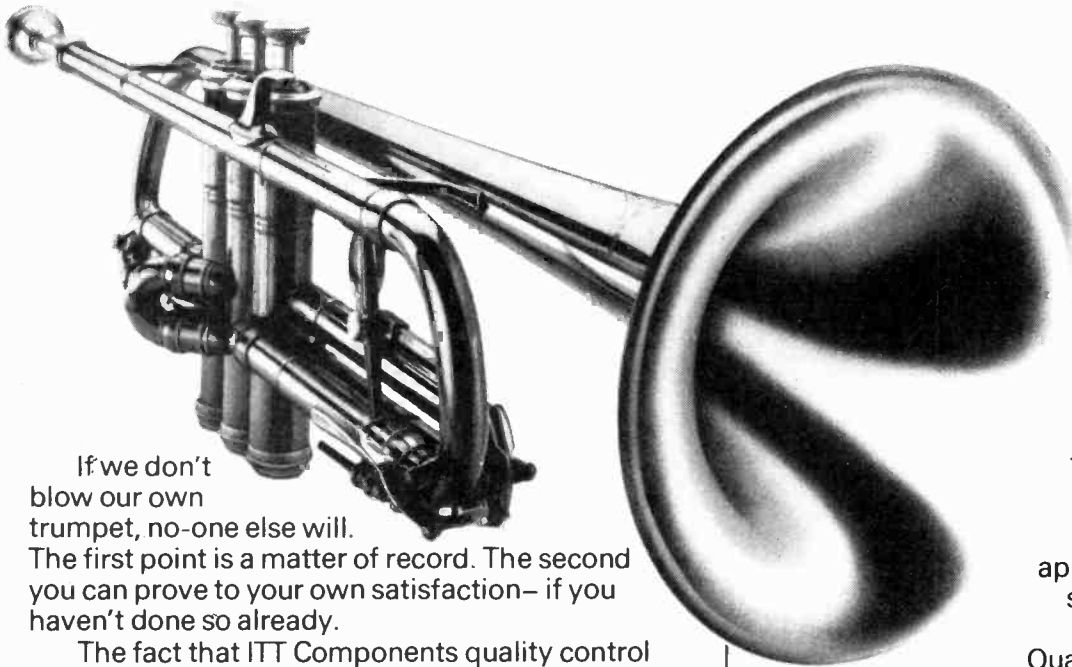
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# Antennas for mobile communications via satellite

## Design considerations for aircraft and ships

by D. I. Spooner B.Sc. *British Aircraft Corporation Limited*

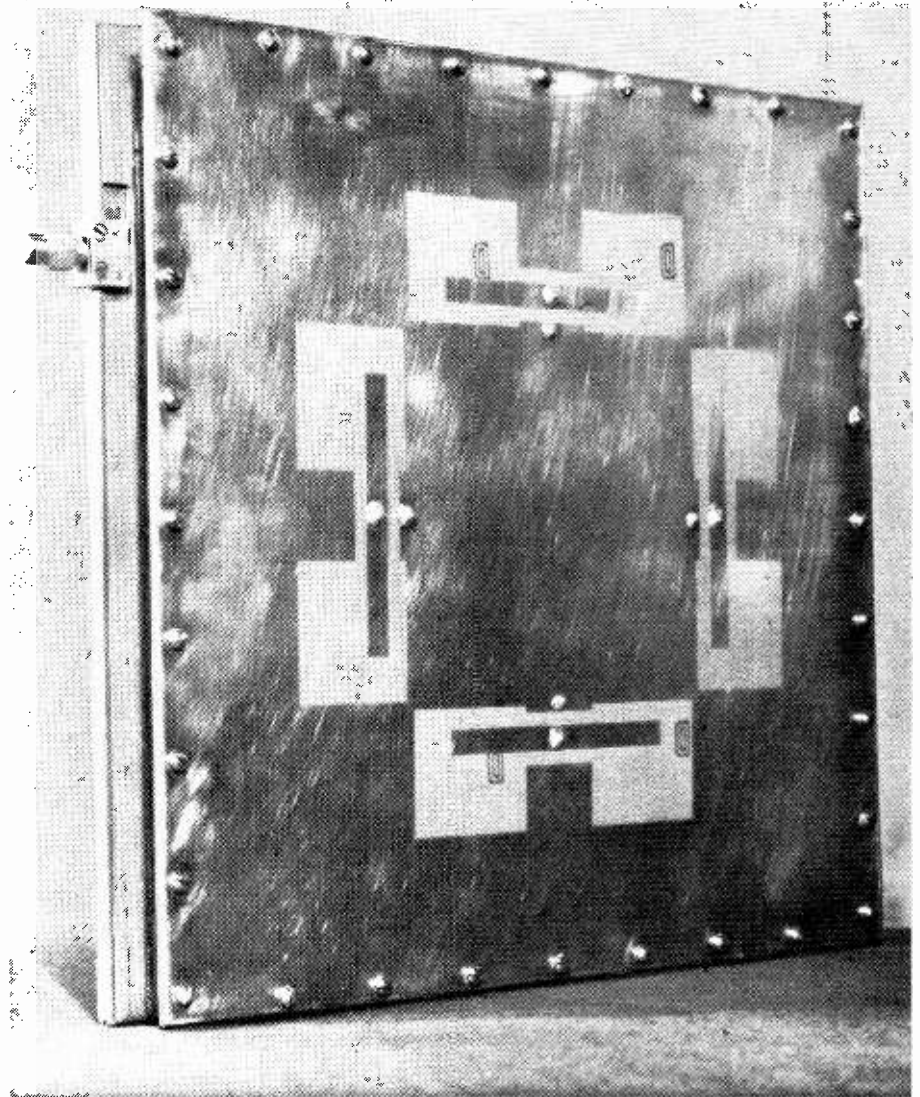
**This article is concerned with the design of antennas for use on aircraft and ships for communication to shore-stations via satellites. Some of the problems encountered in these applications are discussed, and solutions are described for a range of gain level options.**

Although the basic principles relating to a particular antenna design remain the same for both aircraft and ships, much of the design and installation differs considerably.

### Antenna polarisation

Antennas can be designed for either linear polarisation (horizontal or vertical) or circular polarisation (left-handed or right-handed). In reality the radiation from an antenna is elliptically polarised, the ratio of the major-to-minor axes giving an indication of the polarisation purity or ellipticity. When an electromagnetic wave passes through the various regions of the ionosphere, its plane of polarisation rotates. This is known as Faraday rotation.

When circularly polarised radiation passes through the ionosphere, the worst-case polarisation degradation that could occur is from circular to linear. When this signal is received on earth by a circularly polarised antenna (of either hand) the signal loss resulting from this worst-case polarisation degradation is 3dB. However, if a linearly polarised antenna is used to receive the radiation, it is possible that the signal arriving at the antenna will be linear but orthogonal to the plane of polarisation of the receiving antenna. In this situation the loss would be enormous and in theory no signal would be received. It is for this reason that extensive use is made of circular polarisation in satellite communications. Where two-way communication is required with an object within or beyond the ionosphere, circular polarisation is used at both ends of the link. However, where one-way communication is required, for example telemetry transmission from a satellite or missile to a ground station, linear polarisation is used on the satellite or missile and



*Fig. 1. Prototype circularly-polarised Quadslot antenna, designed for 1600MHz, consisting of four folded slots which are inductively loaded at each end and are spaced one half-wavelength apart. The slots are photo-etched from a single-sided, copper laminate board.*

circular polarisation at the ground station. In fact, many ground stations have the ability to select any polarisation they require, circular or linear, in order to optimise the communications link. However, this is a luxury not normally available on mobile stations such as aircraft or ships.

One of the many differences between a mobile and a fixed ground station is that the former has three axes of possible rotation, and that in many cases there is extensive divergence from the straight and level in operation. For example, civil aircraft and container vessels can have roll angles of  $\pm 30$  degrees. Consequently, the mobile satellite-communications antenna should provide circular polarisation over a wide angle. It is this requirement that presents such a problem. Even if the coverage/ellipticity requirement could be met by the antenna in isolation, the installation of the antenna on an irregular shaped body, such as an aircraft, can produce different antenna radiation characteristics from those that are predicted. This problem does not exist to the same extent on maritime installations. However, there are other problems that serve to tax the antenna designer's ingenuity and these will be discussed later.

### Printed circuit techniques

The manufacture of antennas using printed circuit techniques allows quantity production of complex antennas and their associated feed networks, cheaply and with great accuracy. The printed-circuit type of antenna, which is often used for aerospace applications, has the advantages of being lightweight and of rugged construction, because the radiating elements and feed lines are in intimate contact with the board material (a substrate), so eliminating soldered connections. The resulting antenna normally has a small cross section allowing, for example, the antenna to be packaged between spacecraft structural members, or mounted externally on an aircraft fuselage without the penalty of excessive drag.

The choice of a suitable board material is a compromise between the requirements of good electrical and mechanical characteristics. Since the antenna is normally required to work over a wide temperature range, typically  $-65^{\circ}\text{C}$  to  $+95^{\circ}\text{C}$ , the material should not creep or warp over this range. For most applications the material must also be machine workable. In addition, its electrical loss must be low and the peel strength of the copper, bonded to the board, must be high over the whole temperature range. Typical materials used in microwave antennas are p.t.f.e. - fibreglass laminates (Fluorglas and RT-Duroid), a cross-linked styrene copolymer (Rexolite), and for prototype use, a high density polyolefin laminate (Polyguide).

Fig. 1 shows the Quadslot<sup>1</sup>, a circularly polarised antenna designed for a frequency of 1600 MHz, in prototype form. It consists of four folded slots which are inductively loaded at each end and are spaced one half wavelength apart. The

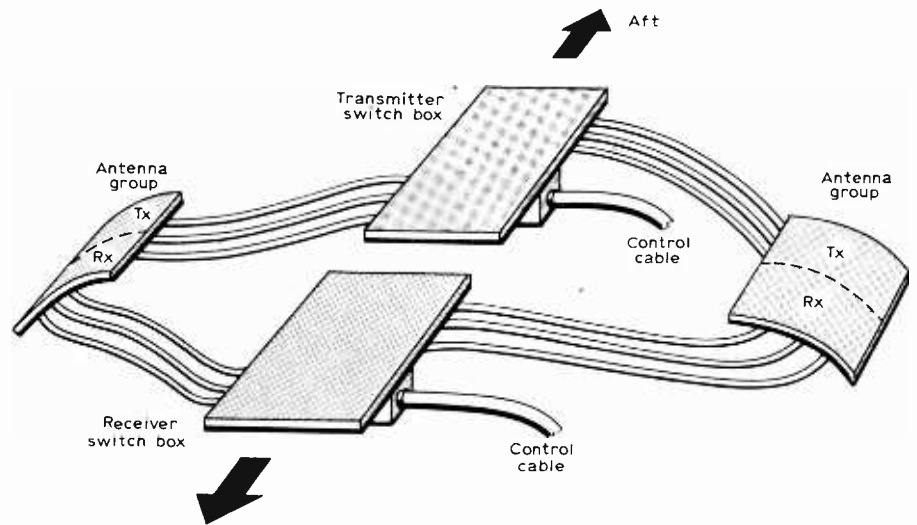


Fig. 2. Schematic of an aircraft antenna installation for use with the Aerosat communications satellite. It consists of two antenna groups, each mounted on a shoulder of the aircraft (see Fig. 3). Each antenna group consists of two arrays of three antenna elements, one transmit array and one receive array (see text).

slots are mounted above a shallow cavity and are photo-etched from a single-sided copper laminate board; the board material being p.t.f.e.-impregnated fibreglass. They are fed from a stripline phasing network mounted at the rear of the cavity, which produces a phase progression of 90 degrees from one slot to another. The Quadslot has a peak gain (relative to an isotropic radiator) of 9dBi, and an ellipticity of better than 3dB over a beamwidth of 70 degrees.

The use of printed circuit antennas allows active circuits to be integrated with antennas on a common substrate. This is of particular value in phased array antennas because distributed amplifiers can be constructed. In this concept, every antenna element in an array, which may have thousands of elements, has its own miniature amplifier and phase shifter, resulting in a high, total radiated power without the problems associated with high-power microwave sources. In addition, circuit losses are reduced to a minimum. This gives improved efficiency and greatly increases system reliability.

### Satellite communication antennas for aircraft

The problems involved in designing an antenna for use on an aircraft are severe and extensive. There is a growing demand for antennas that are, at best, to be flush mounted on an aircraft or, at worst, of low profile in order that the resultant aerodynamic drag is minimised. Aircraft manufacturers and operators require antennas that are suitable for retro-fitting, are lightweight, require little modification

of the aircraft fuselage, are simple to install and maintain, resulting in a minimum "down time" of the aircraft, and yet are, of course, cheap.

Electrically the antenna must have a low v.s.w.r. over the operating band (1.3:1 or less), good circularity (better than 3dB over a large proportion of the coverage), adequate gain over the complete upper hemisphere and good multipath rejection.

An aircraft flying over a reflecting surface, for example the sea, will receive a direct signal from the satellite, and a reflected signal. If the path length of the reflected signal is such that it arrives 180 degrees out of phase with the direct signal, then cancellation will occur. This results in a significant drop in the received signal quality and possibly a complete break in communications. In addition, at low angles of incidence with a reflecting surface, a circularly polarised signal is reflected with the opposite hand of polarisation to the incident wave. One can see from these comments that in order to minimise multipath effects the aircraft antenna should have low level sidelobes, good circularity at low elevation angles and a sharp cut-off below the horizontal plane.

For many years the subject of an aeronautical satellite (Aerostat) has been a controversial one. During the discussions on such a satellite system, various gain levels for the aircraft terminal antenna have been proposed, ranging from the low-gain 4dBi solution to the high-gain 10dBi solution.

If virtually complete coverage of the upper hemisphere is required, with a gain level of 4dBi or above, a single antenna will not comply. Accordingly, antenna designers have proposed solutions that utilise a phased array concept. By taking a number of low gain antennas and feeding them with the correct phase and amplitude, one can control the position and, to a lesser extent, the shape of the resulting beam. If the phase relationship between one antenna and another is varied, the beams can be steered to almost any point in space. As the gain of the array is increased, the beamwidth becomes

1. Patent applied for.



progressively narrower, requiring a greater degree of accuracy in beam-pointing. This in turn leads to the need for a larger beam steering computer. A compromise is therefore needed between the costs and reliability of a large satellite and the need to keep the aircraft terminal as small and as cheap as possible.

Fig. 2 shows a schematic of a system designed and developed by the British Aircraft Corporation in conjunction with the Royal Aircraft Establishment, Farnborough. This system has been designed for use with the Aerosat communications satellite. It consists of two antenna groups, each mounted on a shoulder of an aircraft, fed by two switch units. Each switch unit is linked to the antennas by a set of three phase-matched cables. Each antenna group consists of two arrays of three antenna elements, one transmit array and one receive array. The antenna element is a cavity-backed, slot-dipole having a folded dipole within and in the plane of a slot. Since the dipole and slot are complementary (Babinet's principle) their radiation patterns are identical but with orthogonal polarisation. From this it can be seen that, with suitable phasing between the slot and the dipole, the antenna element inherently has circularly polarised radiation having good ellipticity over a large solid angle.

Separate transmit and receive arrays are used to allow optimisation of pattern and ellipticity over the respective frequency bands. Also, the use of separate arrays provides additional isolation between the transmitter and the receiver. Each antenna group of six elements is printed on a flexible double-sided, copper laminate board. This board is bolted to an aluminium casting, which forms the backbone of the antenna and also provides the cavity for each element. This casting is curved to the radius of the aircraft fuselage. A p.t.f.e. fibreglass radome covers the group of elements. The completed antenna group is  $\frac{3}{4}$ in thick, 15in long and 7in wide.

Fig. 3 shows a production antenna group fitted to an RAE Comet aircraft, used for experimental purposes. The antenna is designed for mounting on a blister, as shown, or flush with the aircraft skin. Each antenna group provides coverage of one half of the hemisphere, the beam being steered to one of three overlapping positions. By using three elements in each array, the system gain level is maintained at or above the minimum requirement of 4dBi over the complete hemisphere.

This antenna system was used in an extensive series of experiments sponsored by the European Space Research Organisation (ESRO), which is now the European Space Agency (ESA), with the satellite ATS-6 in the spring of 1975. The tests proved the reliability and performance of the antenna system, with an aircraft-satellite voice link to

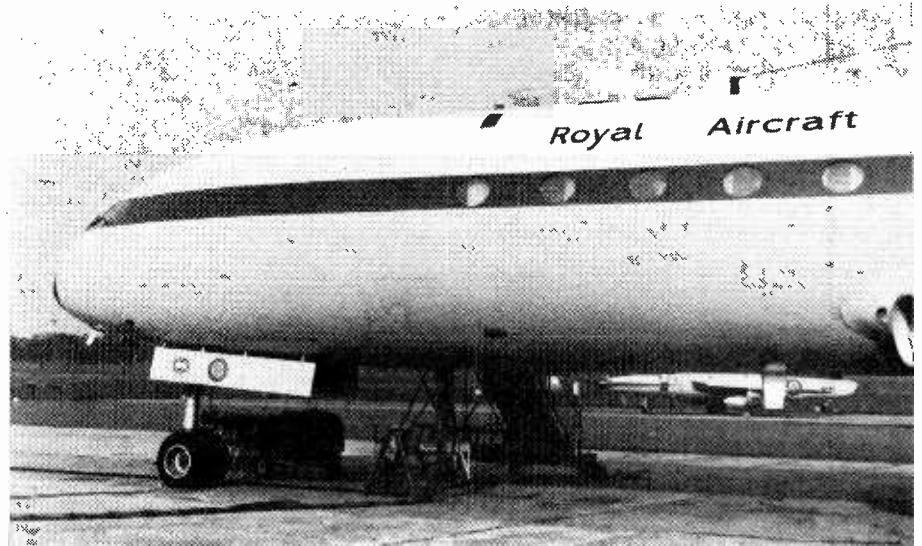


Fig. 3. Picture shows an Aerosat antenna group (see Fig. 2) mounted on the shoulder of an RAE Comet. Only the left-hand group can be seen (the rectangular plate above the foremost window), the second group is located at the other side of the aircraft's vane.

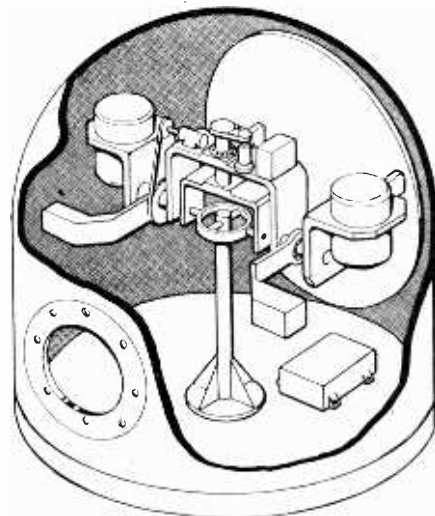


Fig. 4. Illustration of a maritime dish antenna (for a Marisat/Marots ship terminal) which, when mounted on a ship at sea, uses a double momentum wheel to stabilise its platform in the roll and pitch axes. The elements have been modified to show general constructional features (see text).

America of a standard well in excess of land-line sound quality.

A possible development of this type of antenna is to integrate the phasing circuits into a common printed circuit board with the antenna, so providing a solution having a smaller profile and an increased efficiency. However, at the present time, it is unlikely that the required input power of 200W c.w. could

be handled, due to power dissipation within the circuit board itself.

### Satellite communication antennas for ships

A satellite, dedicated to marine communications, is expected to be launched early in 1976. This event has prompted the design and development of many shipborne terminals. The various antenna options that have been considered fall into two broad categories; those using parabolic dishes, and those based on multiple phased elements.

Although the motion of a ship at sea is extremely complex, the antenna is required to be accurately pointed towards the satellite at all times. Not only must the terminal cope with the motion of the ship but also the change in elevation of the satellite as the ship moves in latitude, because the satellite is in geostationary orbit over the equator.

The first generation of satellites will have a low radiated power and will require a shipborne antenna having a gain of 23dBi. Since the cost of a phased array having this gain is high, solutions have been proposed which use a parabolic dish as the antenna. In this situation the design of the antenna is straightforward and either a crossed dipole or a spiral is used as the dish feed. The problem lies in the design of the stabilised platform that the dish is to be mounted on. The conventional solution is to use a servo-driven platform, designed to compensate for movement in roll and pitch by minimising error signals generated by gyroscopes and accelerometers. Movement in azimuth is compensated for by slaving the platform to the ship's compass.

Alternatively, compensation can be obtained by using a pendulum attached to the platform. However, a simple pendulum gives damping problems due to the complex motions involved. This can be overcome by using a double momentum wheel<sup>2</sup>, in place of the

2. Patent applied for.

simple pendulum, to stabilise the platform in the roll and pitch axes. This technique has the advantage of eliminating the precision rate sensors and associated servo control electronics and torque motors. This in turn makes it a highly reliable system. Fig. 4 shows a diagrammatic representation of this system. The severe environment necessitates the use of a dielectric cover over the dish, its stabilised platform and the above deck electronics. Warm air heaters can be used to control the temperature within the cover and to prevent the formation of ice, which can lead to an unacceptable loss in signal quality.

If a parabolic dish having a gain of 23dBi is used, at least one voice channel and one teletype channel can be received aboard the vessel. For smaller ships, requiring only teletype facilities, or for the second generation of satellites having a higher radiated power, it is feasible to use ship terminals of lower gain.

With the present state of technology, phased arrays having gain levels of 15dB or less become a possible alternative to parabolic dishes. Fig. 5 shows the prototype of a ship terminal based on a planar array, which does not require a stabilised platform. The array has twelve crossed-dipole elements printed on a single-sided copper, laminate board which is bonded to a low-dielectric foam block, rigidly positioning the elements above a ground plane. The beam formed by the array is scanned electronically in elevation, with overhead coverage provided by the Quadslot, described earlier. Rotation in azimuth is achieved by mounting the array on a

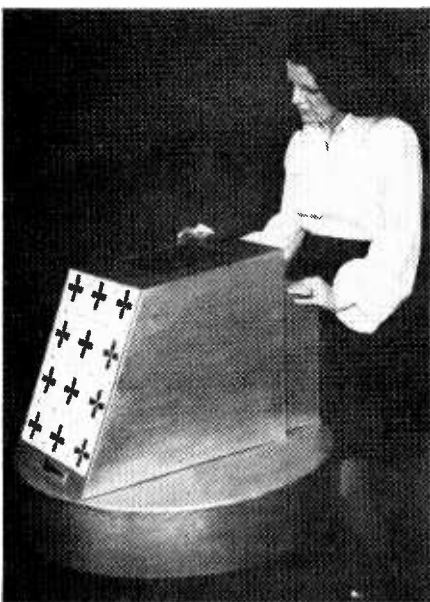


Fig. 5. Prototype phased-array maritime terminal. This unit does not require a stabilised platform, instead it scans electronically in elevation and provides overhead coverage by using a Quadslot.

turntable driven by a stepping motor. The use of electronic scanning in a single plane only, considerably simplifies the beam-steering computer and lowers production costs, since fewer phase shifters are required. This terminal, which has a peak gain of 12dBi, eliminates the need for mechanical stabilisation and provides circularly polarised coverage over a section larger than a hemisphere.

A lower gain solution has been proposed which uses a vertical stack of horizontal crossed dipoles mounted on a simple stabilised platform. This solution removes the need to slave the antenna to the ship's compass since it radiates omnidirectionally in azimuth. By varying the phase difference

between the crossed dipoles, the toroid of radiation is steered in elevation, resulting in a cone-shaped radiation pattern. This type of antenna, which requires a stabilised platform with its accompanied servos and-gyros, suffers the disadvantage of poor circularity, particularly at low elevation angles. It has a peak gain of nearly 10dB.

### Acknowledgements

My thanks go to Mr R. A. Burberry for his help and advice and to the British Aircraft Corporation for allowing this article to be published. The aircraft antennas described were developed under contract to the Royal Aircraft Establishment, Farnborough.

## Microwave voice link

continued from page 71

clamping circuit of Fig. 16 to points A and B of Fig. 11, thus tapping the 50kHz square wave before it is filtered out. The voltage output from this circuit can then be monitored with a meter, the reading being proportional to the amplitude of the microwave input signal.

Even though the p.p.m. function of the transmitter is not being used, it is necessary in this and all other instances to keep the input to the modulator on load, so plug in the microphone. Having done this, it should also be muffled, as noise will cause a variation in the meter reading. Alternatively a 1k $\Omega$  resistor can be connected across the microphone input. When all is set up and a meter reading obtained, carefully and slowly slide the transmitter/receiver away from the reflector and observe the meter. This will fluctuate in reading as the receiver moves through the free-space standing wave pattern. It is easier to locate the position of a null than it is a peak of this pattern so by counting a large number of nulls, of half wavelengths (at least 40 is recommended) and measuring the total distance moved, a sufficiently good estimate of the frequency can be made. Adjustment should be aimed for the mid-band value of 10.250GHz, a wavelength of 29.27mm.

A movement through 40 nulls of the standing wave pattern will be a distance of 585.4mm. Assuming that this can be measured to an accuracy of 2mm, then the transmitter frequency can be determined to an accuracy of 35MHz: a value well within the allocated band.

### Components

Mullard microwave devices CXY11A and BAV46 with collet are obtainable from Townsend-Coates Ltd, Loneford Road, Leicester LE5 0HH. IC<sub>1</sub>, Fairchild type  $\mu$ A715DC, is obtainable from Macro Marketing Ltd, 396 Bath Road, Slough, Bucks SL1 6JD. Printed boards for modulator and receiver are available from M. R. Sagin, 23 Keynes Road, London NW2 costing £4 inclusive.

### Appendix — range performance

The power density at a range R from a transmitter radiating power  $P_t$  from an antenna of gain  $G_t$  is  $P_t G_t / 4\pi R^2$ . A receiving antenna at R having an effective area  $A_r$  will capture some of this power, leading to a received level,  $P_r$ . Antenna gain and effective area are related by  $A_r = \lambda^2 G_r / 4\pi$  where  $\lambda$  is the wavelength. Thus, the received power is  $P_r = P_t G_t G_r \lambda^2 / (4\pi R)^2$ . The ability of the receiver to detect a signal is governed largely by the sensitivity of the detector diode. A subjectively measured parameter called the tangential sensitivity is used, which roughly corresponds to a level 4dB higher than the minimum detectable signal. For this particular system, after allowing 3dB loss in the input filter, the minimum detectable signal is about  $5 \times 10^{-9}$  watt. Gains  $G_t$  and  $G_r$  are both equal at the measured 19.3dB and  $\lambda = 2.93$ cm,  $P_t$  can be taken as 5mW.

Inserting these values into the above equation gives a theoretical range of about 400m. This is for a s/n ratio of unity and would not be expected in practice without more elaborate signal processing. The prototype gave a very satisfactory performance over 100m range with the transmitter and receiver being hand-held. A more stable alignment of the antennas would be expected to improve this.

### Transmission regulations

In common with the regulations governing other frequency bands, the operation of a speech link at these microwave frequencies requires an amateur radio licence. Annual fee is £3, subject to passing an examination and further details can be obtained from: Home Office, Radio Regulatory Department, Licensing Branch (Amateur and Special), Waterloo Bridge House, Waterloo Road, London SE1 8UA.

# Economical time-mark generator

## Simple time and frequency comparator

by S. Roberts

In any establishment where oscilloscopes are in use, a time-mark generator can be a valuable tool when assessing time-base accuracy. Unfortunately, commercially-produced generators are usually too expensive for small workshops, laboratories and enthusiasts. The device to be described combines modest cost with accuracy, and may be easily constructed using readily available parts. Although described here as a complete unit, the generator could well be incorporated into a digital frequency counter, where the clock oscillator and decade divider chain would already be available, or even into an oscilloscope as part of the calibrator function.

A time-mark generator is essentially a pulse generator where the time between pulses has been accurately specified. The pulse width is made sufficiently small compared to the spacing between pulses that when looking at the output on an oscilloscope, only a single vertical line for each pulse is evident. Thus, the time-base frequency may be adjusted until the pulses are coincident with the appropriate graticule lines.

### Circuit description

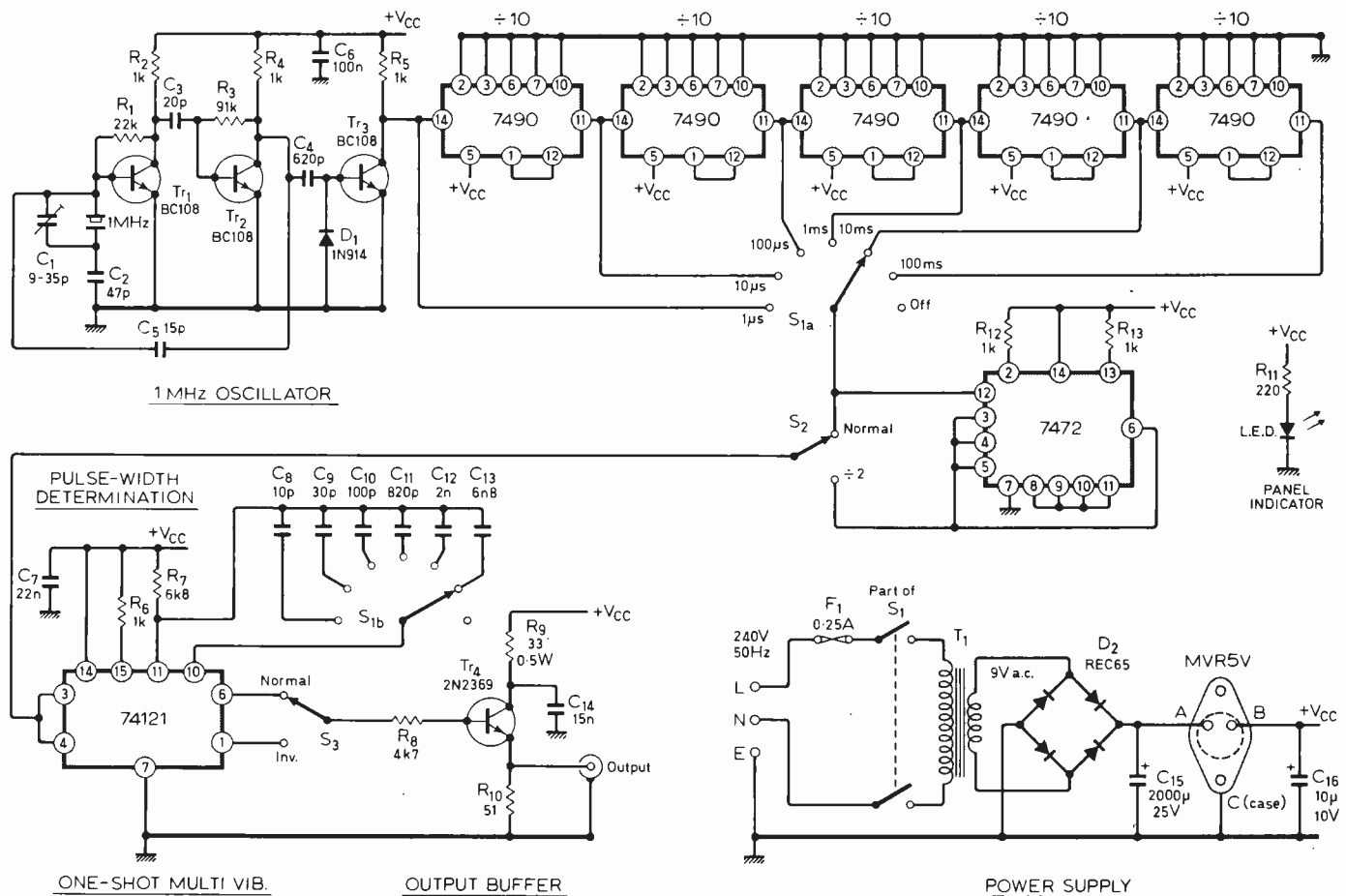
A 1MHz crystal-controlled oscillator,  $Tr_1$  and  $Tr_2$ , provides an accurate frequency source. Transistor  $Tr_3$  acts as an output buffer and its collector switches between 0V and 5V at a 1MHz rate. This is connected directly to the

input of a series of SN7490 decade dividers,  $IC_1-IC_7$ , whose outputs will be 100kHz, 10kHz, 1kHz, 100Hz and 10Hz respectively.

The desired frequency, and hence time-mark interval, is selected by means of  $S_{1a}$ , and fed to  $IC_7$  either directly or via  $IC_6$ . The SN7472,  $IC_6$ , provides further frequency division if selected by means of  $S_2$ , so doubling the number of time-mark intervals available.

It was found during experimentation that for the output marker pulses to be sufficiently narrow to ensure that accuracy was not degraded, yet wide enough that the pulses were easily

Fig. 1. Time mark generator circuit diagram.



visible, different pulse widths were necessary for different mark intervals. The optimum pulse widths, derived experimentally, range from 50ns to 35 $\mu$ s, as may be seen from Table 1.

**Table 1**

Range	Frequency	Pulse width
1 $\mu$ s	1 MHz	50 ns
2 $\mu$ s	500 kHz	
10 $\mu$ s	100 kHz	150 ns
20 $\mu$ s	50 kHz	
100 $\mu$ s	10 kHz	500 ns
200 $\mu$ s	5 kHz	
1 ms	1 kHz	4 $\mu$ s
2 ms	500 Hz	
10 ms	100 Hz	10 $\mu$ s
20 ms	50 Hz	
100 ms	10 Hz	35 $\mu$ s
200 ms	5 Hz	

The various widths are determined by IC<sub>7</sub>, which is a monostable multivibrator. The "Q" output at pin 6 goes high when the input (pins 3, 4) changes from high to low. The length of time for which it remains high is dependent upon the values of the timing components R<sub>7</sub> and the capacitor selected by means of S<sub>1b</sub>.

The values of the timing capacitors are calculated from the formula:-

$$t_{p(out)} = C_T R_T \log_e 2$$

where  $t_{p(out)}$  = output pulse width in  $\mu$ s

$C_T$  = timing capacitor in  $\mu$ F

$R_T$  = timing resistor in k $\Omega$   
( $R_7 = 6.8k\Omega$ )

$$\log_e 2 = 0.7$$

Pin 1 of IC<sub>7</sub> is the "Q" output and will be the inverse of the "Q" output. One of the two possible outputs is selected by means of S<sub>3</sub> ("NORM/INV") and taken to the output buffer, Tr<sub>4</sub>, which serves to isolate the output from IC<sub>7</sub> and to provide a low impedance source. The resistor R<sub>9</sub> is included to limit the current should the output be shorted.

The R.S. Components MVR5V voltage regulator has been used for the power supply, which simplifies construction. Other regulators such as the LM309 could of course be used, or a supply using discrete components could be constructed. About 500mA at 5V is required. Any low-voltage transformer with a secondary of around 9V at a sufficient current rating is suitable, such as the R.S. Components Type 633.

### Construction

The layout of the generator is not critical, although adequate decoupling of the supply lines and good earthing is essential for a clean output pulse. The prototype was constructed with the ubiquitous Veroboard, and no problems were encountered with stray capacitance. For switch S<sub>1</sub>, a Doram miniature Maka switch was used, with two 1-pole 12-way wafers. The mechanical stop was adjusted to limit the movement to

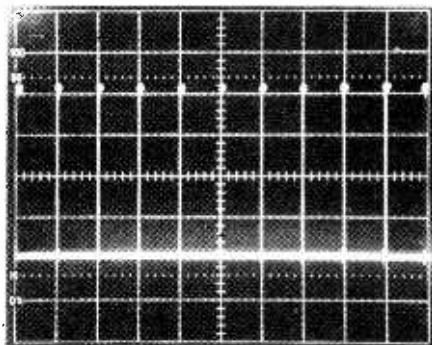


Fig. 2. Time and linearity checking of an oscilloscope sweep.

seven positions, the extra position being used to control a mains switch also mounted on the spindle. If desired, a separate mains switch could be used, in which case a single 2-pole 6-way wafer would suffice for S<sub>1</sub> since only six positions would then be necessary.

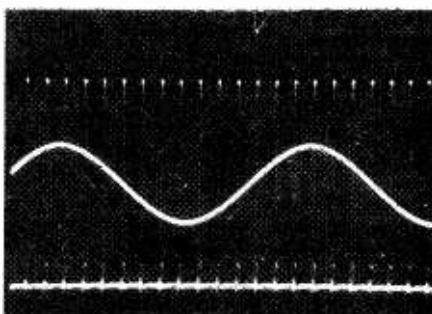
When constructing the oscillator portion, some adjustment of R<sub>3</sub> may be necessary to ensure that the oscillator remains reliably locked to the crystal frequency. If desired, a 10MHz oscillator could be constructed, which, in conjunction with an additional divider stage, would provide 100ns and 200ns markers.

### Applications

Figure 2 is a photograph of the output on an oscilloscope screen. By adjusting the oscilloscope sweep speed, the markers can be made to coincide with the vertical graticule lines with each setting of the time-base switch. The markers then serve to show the accuracy of the time-base and the horizontal linearity. Selection of a suitable marker pulse will permit the vertical geometry to be checked - the pulse should be parallel with the vertical graticule lines.

With dual-trace oscilloscopes, the generator provides a quick and accurate means of checking the oscilloscope internal calibrator frequency - usually 1kHz if not derived from the a.c. mains. A 1ms time-mark is displayed on the upper trace, the calibrator on the lower trace, and with the oscilloscope time-base synchronised with the generator, the calibrator frequency may be adjusted until the lower trace is stationary on the screen. Other

Fig. 3. Measuring frequency by means of the time-pulses.



oscillators may be calibrated by the same method.

An unknown frequency may be measured on an oscilloscope with a non-linear or uncalibrated time-base by displaying the frequency and time-marks simultaneously, and counting the number of time-mark intervals in one cycle. Figure 3 demonstrates this possibility. In this case, the time-mark generator was set for 1 $\mu$ s pulses. 13.3 time-mark periods can be seen over the duration of one cycle, indicating a frequency of:-

$$f = \frac{1}{P} = \frac{1}{13.3 \times 10^6} = 75.2 \text{ kHz}$$

In this application, the time markers may be considered to be an "electronic graticule".

These ideas represent the more obvious uses of a time-mark generator - other applications may well occur to the ingenious user.

It should be borne in mind that this design is probably the simplest possible. There is therefore scope for improvements, further facilities or modifications to suit the requirements of individual users. In its present form, however, the generator is a most useful device and sufficient for most purposes.

## Sixty Years Ago

It was difficult to persuade Senatore Guglielmo Marconi to write for publication, but our November 1917 issue contained an interview given to the editor of *The Wireless Age* in America. His remarks were intended for American amateurs, and strike a very odd note indeed to a 1977 reader. It is worth bearing in mind, though, that we had been at war three years by this time.

"... The most striking features of my observation since I have been on this official visit to the United States is the surprising ignorance of your wireless men concerning the conditions in the fighting zone abroad. It has required a readjustment of viewpoint for me to appreciate the fact that so much of the scientific development of the wireless art has been kept secret for military reasons; naturally the United States cannot know of things which to us have seemingly become elementary.

"... It can be readily seen... that the Allies faced some serious problems in supplying the right sort of men for this duty, and, in fact in supplying the armies with sufficient wireless men for their needs. We were far better equipped, however, than the Americans, because of the fact that the European nations had large standing armies with men well trained for their soldierly duties. It was simpler for us to take soldiers and train them as operators, and this we did. We had very little choice in the matter, however, because we had no great body of amateurs to call upon as you have in this country.

# New Products

## Tantalum capacitors

A family of resin-coated, solid tantalum capacitors has been introduced by Sprague for the low-cost, domestic equipment market. The components are in six case sizes with a variety of lead shapes for several different printed-board spacings. Values are in the 20% tolerance decade values between 0.1 $\mu$ F and 680 $\mu$ F and work at voltages from 3V d.c. to 50V d.c. up to 85°C. Sprague Electric (UK) Ltd, 159 High Street, Yiewsley, West Drayton, Middlesex.

WW 301

## Spectrum analyser

A 50MHz spectrum analyser from Parametron is intended for general and field operation in addition to work in the laboratory. Centre frequencies of 200kHz to 50MHz are continuously tuned at dispersions of 100kHz to 50MHz and sweep speed is 20ms to 10s. Spurious responses are said to be -66dB and intermodulation products are at -50dB. The tuning range can be extended to 350MHz by means of a converter. Wessex Electronics Ltd, Stover Trading Estate, Yate, Bristol BS17 5QP.

WW 302

## Thumbwheel switches

Plessey's Series 33 thumbwheel switches are said to have up to ten switching positions and mount from either the front or rear of a panel. Black with white legends, they have a number of switching codes. Extended printed circuit boards can be provided to mount extra components, and the switch can be illuminated by a 5V 60mA lamp. The contacts are rated at 100mA at 50V d.c. with a temperature range from -20°C to 70°C. G.E. Electronics (London) Ltd, Eardley House, 182 to 184 Campden Hill Road, Kensington, London W8 7AS.

WW 303

## Opto-couplers

A range of photo-couplers, from National Semiconductors Ltd, utilize gallium phosphide I.e.d.s and fast-responding cadmium-selenide photocell detectors. The couplers, in the 5S range, are a.c.-compatible and enable emitter-to-detector isolation voltages of up to 10kV to be achieved. They are rated up to 320V with 250mW dissipation and an I.e.d. current of 25mA, giving maximum on, and minimum dark resistances of 2k $\Omega$  and 100M $\Omega$  respectively. The devices are available in either four-pin TO-5 size cans, 0.625in long by 0.32in diameter cylindrical packages, or in 0.75in square modules. National Semiconductors Limited, Stamford House, Stamford New Road, Altrincham, Cheshire WA 141DR.

WW 304

## Plastic solder

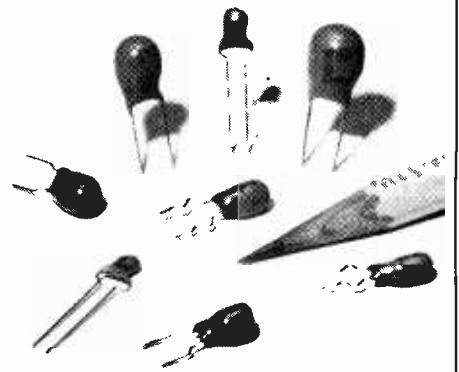
Eccobond Solder 56C is a plastic adhesive which, when cured, has an extremely low electrical resistance (its volume resistivity is typically  $2 \times 10^{-4}$  ohm-cm). It can be cured at temperatures as low as 49°C in 2h, or in a few minutes at much higher temperatures. The adhesive, which is supplied in paste form, bonds to metal, glass, ceramic and plastics. It may be used for making electrical connections where hot soldering is impractical, for example, to nichrome wire or conductive plastics, and at locations which cannot be subject to high temperatures. Other specifications include a lap shear strength of 56Kg/sq.cm., flexural strength 857Kg/sq.cm. and thermal expansion  $36 \times 10^{-6}$  per degree Centigrade. Emerson and Cuming (UK) Limited, Colville Road, Acton, London W3.

WW 305

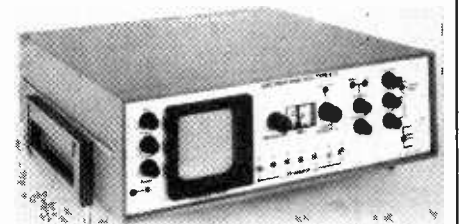
## Magnetic film recorders

Sondor Libra M03a magnetic film recorders have been designed to handle acetate or polyester films. They have straight-line lacing paths, small size and combination pinch-wheels and sprocket-drives. Models available range from simple single-channel replay only types to three-channel record/replay types. The machines are pre-wired to take extra amplifiers and can therefore be converted to the full three-channel record/replay specification. Type M03a uses the standard Sondor method of synchronization and can therefore easily be locked to projectors, telecine machines and time-code interlock equipment. This machine is also available in a video version containing a holoscope prism system. Hayden Laboratories Limited, Hayden House, Churchfield Road, Chalfont St. Peter, Bucks., SL9 9EW.

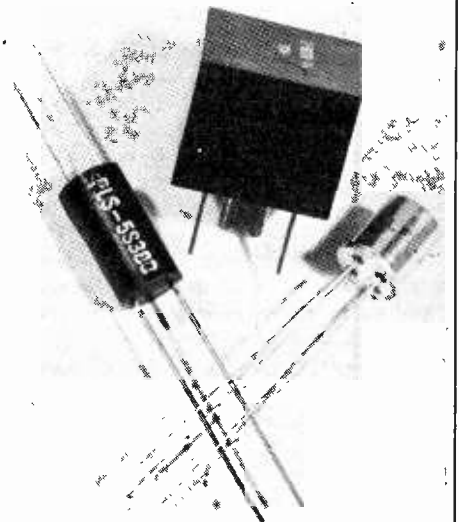
WW 306



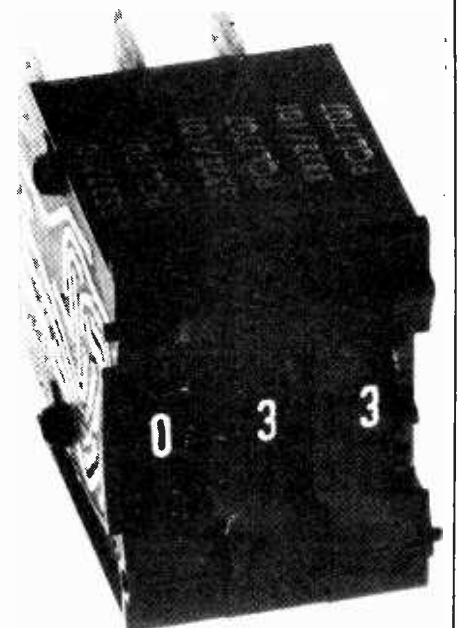
WW 301



WW 302



WW 304



WW 303

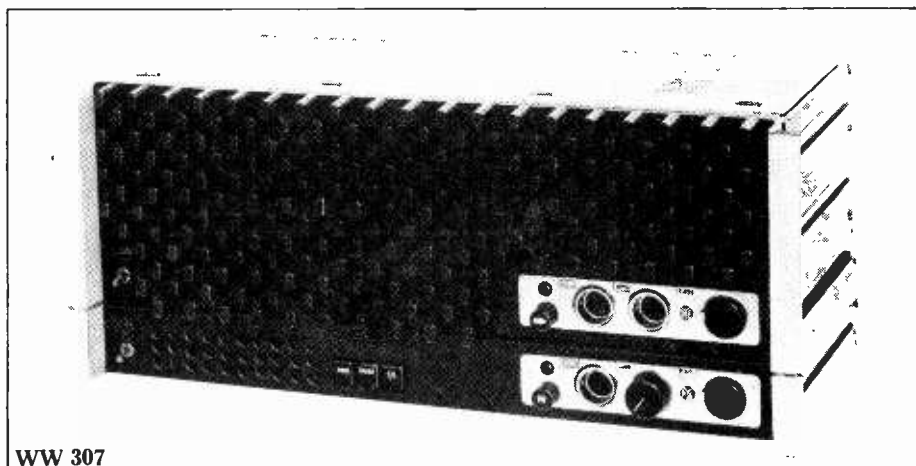
## A.m. transmitters and receivers

A range of fixed-station amplitude modulated transmitters and receivers have been introduced by Pye Telecommunications Ltd. The transmitters, type T401, are 25W solid-state modular designs suitable for simplex or duplex operation in the frequency range 68 to 174MHz. They have been designed using low intermodulation products specifically to make them usable on multiple transmitter sites, and they may also be fitted with tone-lock encoder (c.t.c.s.s. — continuous tone controlled sub-audio squelch) devices to ensure that only mobiles fitted with the appropriate decoder receive the message.

The receivers, type R401, use phase-lock-loop synchronous detectors so

that they can receive high modulation signals with low distortion. To reduce spurious responses the receivers are based on a single-conversion design, which also results in simpler, more-reliable circuits. Helical resonators and f.e.t.s in the r.f. section give the receivers high selectivities (typically  $0.5\mu\text{V}$  p.d. input for 1W min. output and 30% modulation with 1kHz tone), with a signal-to-noise performance of 12dB SINAD at  $0.5\mu\text{V}$  p.d. signal input (at 60% mod. with 1kHz tone). Blocking and intermodulation figures, measured to MPT1302, are in excess of 100dB and 60dB respectively. Both units can be supplied for standard 19in rack mounting and operate on a.c. or 24V d.c. supplies. Pye Telecommunications Limited, Newmarket Road, Cambridge CB5 8PD.

WW 307



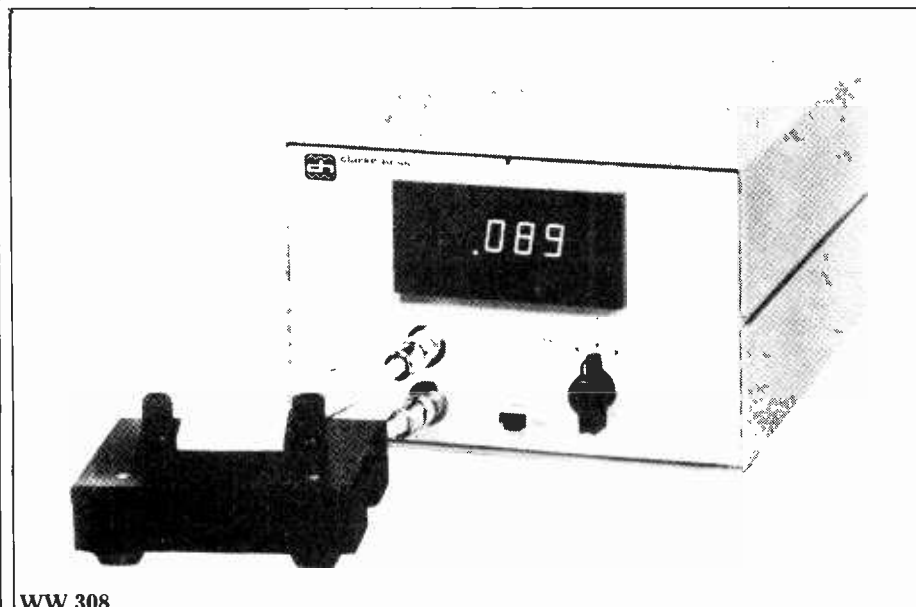
WW 307

## ESR meter

Equivalent series resistance of capacitors is indicated digitally by the Clarke-Hess 273A meter. Capacitors in the range 5000pF to over 1F can be tested and subjected to less than 10mV d.c. and 100mV r.m.s. at 100kHz. Resolution of the e.s.r. measurement is 0.1 milliohm up to 200 milliohms, 1

milliohm up to 2 ohms and 10 milliohms up to 20 ohms. Measurement time is normally 0.5s, but when externally clocked this is reduced to as little as 20ms, a b.c.d. output being provided for automatic test. The instrument is available in the UK from Lyons Instruments, Hoddesdon, Herts.

WW 308



WW 308

## Multiplier

An eight bit multiplier from Monolithic Memories Inc is claimed to generate a 16-bit product in around 100ns. Two versions of the multiplier are available, the 67558, suited to signal processing in radar, fast Fourier transforms, sonar, speech processing, and speed multiplication in brain and body scanners, and a military version, the 57588 which extends the 67558's temperature range from between 0 and 70°C to between -55°C to 125°C. Memory Devices, Central Avenue, East Molesey, Surrey KT8 0SN.

WW 309

## Power transistors

Two complementary power transistors, types BD135 and BD136, are silicon n-p-n/p-n-p devices having the following absolute maximum ratings: the total power dissipation for a 70°C case temperature is 8W, the collector current is 1A and the collector-emitter voltage is 45V. These transistors show a gain bandwidth product of 50MHz, a d.c. forward current transfer ratio voltage of 40 to 250 and a collector-emitter saturation voltage of 500mV. The devices are packaged in a TO126 case. Norbain Semiconductor Division, Norbain House, 2 Arkwright Road, Reading, Berks.

WW 310

## Sequence timer

The RST rotary timer from Appliance Components has been extended with the introduction of a new unit which is capable of taking twenty switches of either the rotary wafer or the cam-operated microswitch variety or a combination of both. A common shaft drives all the switches and is operated by a synchronous motor. The rotary switches consist of a wiper and silver contacts and the cams can be shaped to provide up to 24 microswitch operations per revolution. Appliance Components Ltd, Cordwallis Street, Maidenhead, Berks SL6 7BQ.

WW 311

## Cam switches

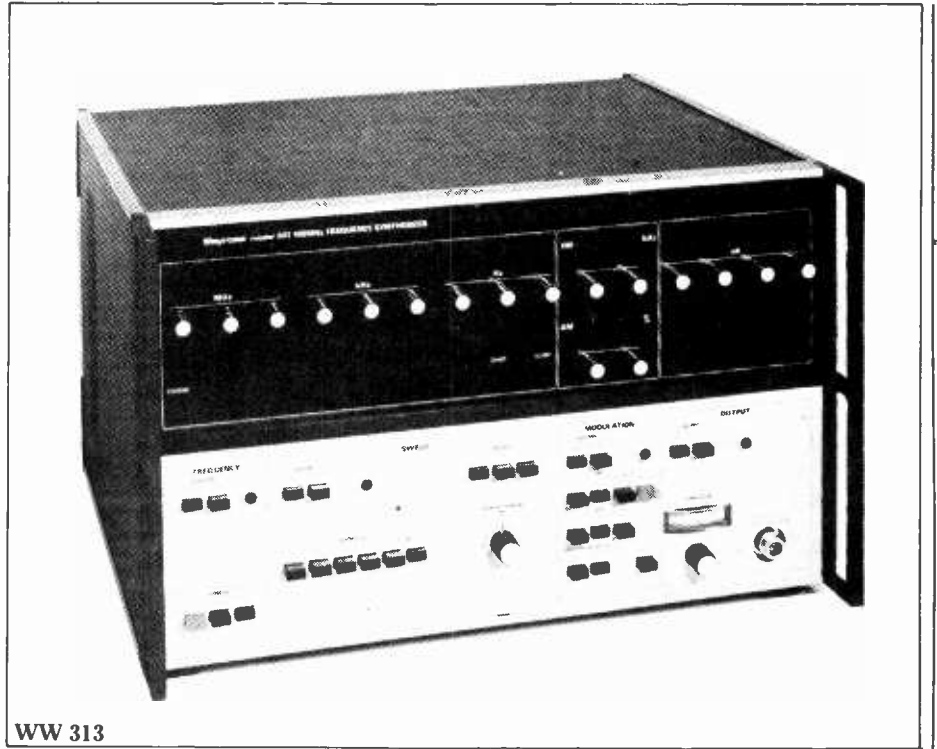
Rotary cam switches, in a modular form for assembly by the user, are available from Entrelec. Up to twelve contacts can be operated on a single shaft, which can be 90° or 45° indexed, key-operated, spring return, limited rotation and front or rear mounted. Switches in this V range are rated at up to 55A and are said to be suitable for motor control and as isolator switches. The units can be obtained from Triscott Electrical Ltd, 23 Wansford Way, Felpham, Sussex PO22 7N6.

WW 312

## Frequency synthesizer

A fully-programmable frequency synthesizer, the Model 601, has a frequency range from 10kHz to 180MHz with a resolution of 1Hz. Built-in modulation facilities are a.m. up to 99% and f.m. in two ranges to 9.9kHz and 99kHz at modulation rates to 100kHz. The signal output level is 2V (e.m.f.) from 50Ω. A built-in step attenuator has a range from 0 to 139.9dB in 0.1dB steps and a sweep facility, having a maximum range of  $\pm 1$ MHz, is available as an option. The frequency reference is a 5MHz crystal oscillator with a daily ageing rate of less than one part in  $10^{-9}$  and a long-term stability of one part in  $10^{-7}$  over a period of six months. All functions are b.c.d.-programmable via multiway connectors on the rear panel. Sayrosa Engineers Limited, Wey River House, High Street, Alton, Hants.

WW 313



WW 313

## Rechargeable batteries

Lead-acid batteries in the Varley range, stocked by Electroplan Ltd, are low-cost and offer high power-to-weight ratio and safe spill-proof operation. These batteries are available in 2V cells and 6 and 12V packs, in capacities from 4.5 to 90Ah. They are constructed from compressed layers of highly-absorbent separator material and thin lead plates. This construction enables high capacities to be achieved in a small volume and also removes the risk of plate material becoming detached and bridging between plates. Since the electrolyte is completely absorbed by the porous separators, the batteries can be charged and used in any position without spillage, and will need topping up less often than a conventional free-acid battery. Electroplan Limited, P.O. Box 19, Orchard Road, Royston, Herts., SG8 5HH.

WW 314

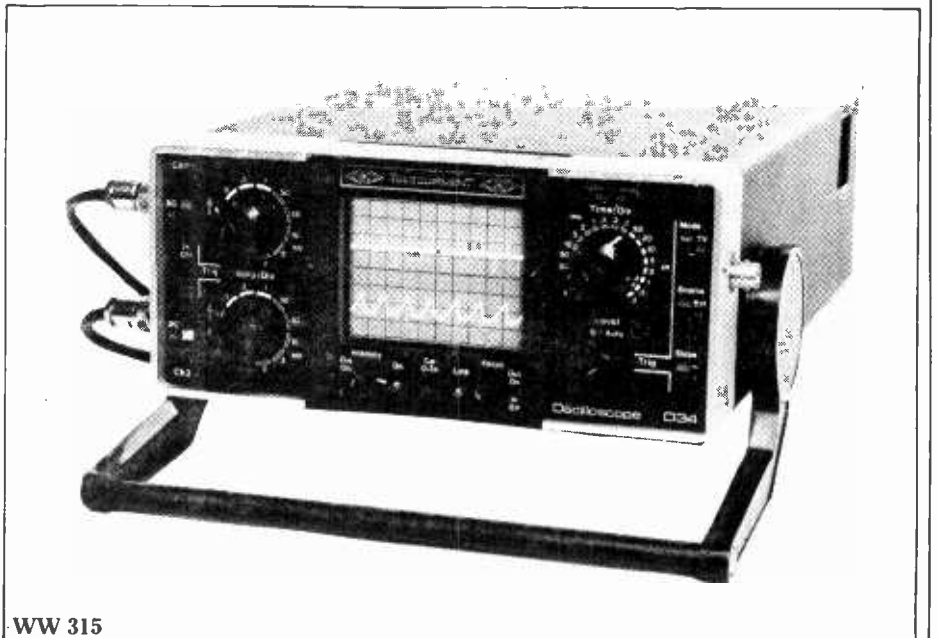


WW 314

## 15MHz battery oscilloscope

The D34 dual-trace portable oscilloscope, from Telequipment, has all the features of the model D32, but it has been given a greater bandwidth and a higher sensitivity (the maximum deflection sensitivity has been raised to 2mV/division up to 15MHz). To match this increased performance, the maximum switch speed is now 0.2μs/division, and a signal delay has been included to facilitate the observation of fast leading edges. This oscilloscope may also be used on a mains supply. Electroplan Limited, P.O. Box 19, Orchard Road, Royston, Herts SG8 5HH.

WW 315



WW 315

# Sidebands

## by mixer

### Wall of words

Why is it, I wonder, that the average bank clerk, boiler maker or mole exterminator is so quick to claim total and passionate ignorance of anything electronic? Mention, in passing, the fact that you work in electronic engineering and see his face register the "Well, how interesting! But of course all that sort of thing is above my head" expression. But talk to him about his car and he will instantly be away into a discussion of steering geometry, carburation and the advantages of limited-slip differentials.

Next time the company chairman is wheeled round the lab on his annual tour of inspection, just watch the pent-up surge of indifference glaze his eyes as you explain to him what you've been about during the last year. This is not to say he's a fool — anyone who gets to be chairman of a company has to have something upstairs — but it does seem that many such, otherwise rational, people experience this automatic switch off at the mere mention of electronics. I think most of the blame lies with electronic engineers themselves: we have built up this carefully-guarded mystique over the years by cloaking even the most straightforward statements in the most grotesque jargon ever heard outside a marketing and advertising office. We talk about large-scale integrated t.t.l., ceemoss bucket brigades, intelligent terminals and jungle chips without a thought for the hapless individual with a head full of nothing more complicated than running a film-a-year company. No wonder they all think we're too way out to be taken seriously.

### A breath of fresh air

He has a good aim with a bucket of icy water, has Peter Baxandall. If, as is only proper, you turned to this page first, I insist that you must now read his article on fog-dispersal. He doesn't call it that, of course, because it would look peculiar in the index, but that's what it is about.

The writings of some of those who

describe audio equipment for magazines has ascended (or descended, according to your point of view) to the level of the argot used by art and music critics. But while there are reasons for not being able to describe a painting by Lowry or a concerto by Vivaldi in precise language, there can be no excuse for disguising a lack of information in a flurry of adjectives such as "chesty", "forward", "relaxed" or, as in a recent review, "boring". Critics don't, as a rule, talk about indefinable agencies at work in paintings or music; indeed, they are usually only too willing to explain in detail just what it is about the brushwork or the violinists' fingers that gives a work its character. Perhaps now, after Baxandall, we can drop all this pseudo science about amplifiers and stop believing in fairies.

### PR pidgin

*a breakthrough* . . . . the same as all the others except it uses i.c.s.  
*years of research* . . . . three days looking through the competition's catalogues.  
*professional* . . . . has a lot of knobs and it's too dear for most people.  
*sophisticated* . . . . expensive. A recent favourite — "sophisticated genuine wood."  
*computerised* . . . . has a transistor in it.  
*symposium* . . . . marketing managers' jamboree.  
*new low price* . . . . cheaper than it could be, dearer than it should be.  
*indispensable* . . . . dispensable.  
*high-density ABS* . . . . plastic.  
*the ultimate* . . . oh! come now.

### Not cricket

We get some funny letters to these offices. They cover the field from "My radio has gone wrong; can you tell me how to mend it, please?" to requests for an explanation of the workings of computers ". . . if you could spare a few minutes of your time". We had a man who used to write in and say that beings from space were following him around and could we let him have a circuit to jam their 'detection beams', and the number of people who have invented stereoscopic television displays must be well into the double figures.

But we have now received the classic communication. A letter came from an official who is responsible in some way for the welfare of inmates of H.M. prisons, wanting to know the value of a certain type of radio receiver. It appears that the governing body of the chokey in question are being given the runaround by one of their flock who, much to his indignation, has had his radio stolen!

Now, this will not do. It is quite definitely the sort of thing that gives

dishonesty a bad name, and if you can't leave things lying around in a government establishment, well, it's no wonder the country's going to the dogs. Apart from which, there's the question of honour among . . . er . . . wealth redistribution operatives — is there no sense of shame among these people?

What I can't work out — where on earth have they hidden it?

### Sound control

I suppose the knobs, switches, meters and assorted decorations are built on to audio equipment because the makers have found that their customers want them. The nearer in appearance to mission control, the better for the image, so to speak. Indeed, there is even a demand for a "military look" in some portable radios and a "laboratory look" in much recent high-fidelity sound gear. All these controls and indicators presumably have a function, but one wonders whether they are ever used.

I must point out that I'm not being patronising, because I have some equipment like that myself, although the gimmicks did come with the performance, which was why I bought it. It has a loudness button, which serves to ruin the frequency response, no less than three "on" switches and a separate "off" switch, a useless signal level meter, a scratch filter and a rumble filter, neither of which has ever been used in anger, and any amount of satin chrome. It all looks very technical and my wife won't touch it. I think she's a bit puzzled about the red pilot light, which only comes on with certain programmes.

I dare say she isn't alone, either — the days when you could "turn on the wireless" with one flick of the wrist are long gone. There must be thousands of middle-aged and elderly people who are as fastidious about sound quality as anyone else, but who simply do not want to know about bass and treble boost and cut, balance, loudness contours, tape bias and equalisation, noise-reduction controls and peak-programme meters. And yet only one NAIM springs to mind. There may be others (QUAD equipment is not excessively self-conscious) which do not attempt to impress except by way of performance, but most gear that you buy seems to have the young and technically-minded at heart rather than the person who wants to hear music without being reminded that it's all very clever.

Would it not be possible and desirable to market very high quality units with a minimum of controls, especially for people who aren't able, for any reason, to use them to best advantage?



# KEEP YOUR COOL

WITH ANTEX SOLDERING IRONS...

THIS UNIQUE SAFETY STAND - PART OF THE ANTEX SOLDERING KITS SK3 and SK4



**Stand S.T.3** has a chromium plated steel spring and is suitable for all our models. Priced at £1.40 excl. of VAT

With the new Antex soldering stand you have the assurance that with the iron tucked neatly into the strong angled spring coil you have maximum safety when preparing or waiting for the iron to heat. Moulded into this stand is provision for six alternative bits, and two small sponges for cleaning bits.

This sturdy plastic stand is a useful addition to any household or workshop. The SK3 and SK4 kits comprise of a full instruction card mounted with either the CX miniature soldering iron or the larger X25 general purpose iron. Included in both of these kits is the safety stand.

All the range of Antex soldering irons are made on the principle of putting the heating element inside a shaft, then the desired bit is eased over the shaft, giving maximum heat transference, this is why so often a small Antex iron can do the job of a larger conventional iron. The precision made slide on bits are slit to make them easily interchangeable.

Our comprehensive range is sure to meet your need.

**Model CX-17 watts**  
 ... a miniature iron with the element enclosed first in a ceramic shaft, then in stainless steel. Virtually leak-free. Only 7 1/2" long Fitted with a 3/32" bit £3.40 excl. of VAT. Range of 5 other bits available from 1/4" down to 1/64"

**Model X25-25 watts**  
 A general purpose iron also with a ceramic and steel shaft to give you toughness combined with near-perfect insulation. Fitted with 1/8" bit and priced at £3.40 excl. of VAT. Range of 4 other bits available. B.E.A.B.-APPROVED.

**Model SK3 KIT**  
 Contains both the model CX soldering iron and the stand S.T.3 Priced at £4.80 excl. of VAT it makes an excellent present for the radio amateur modelmaker or hobbyist

**Model SK4 KIT**  
 With the model X25 general purpose iron and the ST3 stand and its B.E.A.B. safety label, this kit is a must for every toolkit in the home.

**Model SK1 KIT**  
 This kit contains a 15 watt miniature soldering iron, complete with 2 spare bits, a coil of solder, a heat sink and a booklet. How to solder. Price £5.30 excl. of VAT

**Model MLX KIT**  
 The soldering iron in this kit can be operated from any ordinary car battery. It is fitted with 15 feet flexible cable and battery clips. Packed in a strong plastic envelope it can be left in a car, a boat or a caravan ready for soldering in the field. Price £3.95 excl. of VAT

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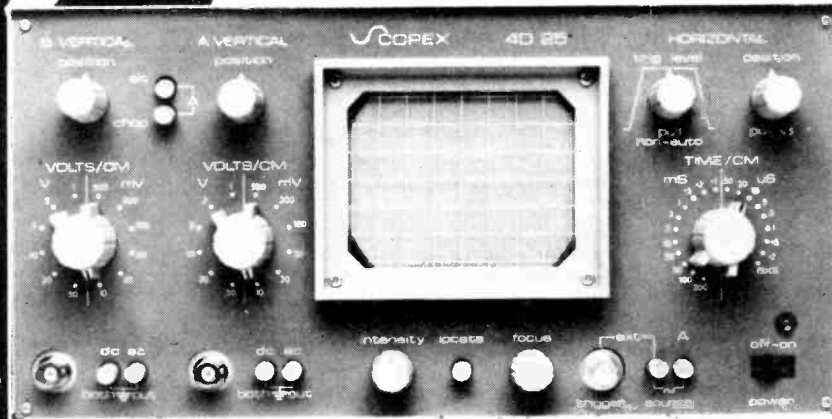
<b>TTLs by TEXAS</b> 7400 16p 7400 28p 7400 63p 74LS00 30p 7401 18p 7402 18p 7403 18p 7404 23p 74H04 36p 7405 25p 7406 43p 7407 43p 7408 25p 7409 27p 7410 18p 74H10 28p 7411 24p 7412 25p 7413 36p 7414 75p 7416 33p 7417 36p 7420 18p 7421 40p 7422 22p 7423 37p 7425 30p 7427 37p 7428 36p 7430 18p 7432 36p 7437 36p 7438 36p 7440 19p 7441 75p 7442 70p 7443 140p 7444 140p 7445 100p 7446 100p 7447 85p 7448 80p 7450 18p 7451 20p 7453 20p 7454 18p 7460 18p 7470 36p 7472 30p 7473 34p 7474 34p 7475 45p 7476 36p 7480 50p 7481 95p 7482 90p 7483 90p 7484 110p 7485 120p 7486 34p 7489 320p 7490 40p 7491 85p 7492 55p 7493 40p 7494 90p 7495 70p 7496 84p 7497 340p 74100 120p 74104 65p 74105 65p 74107 36p		<b>C-MOS I.Cs</b> CD4000AE 20p CD4001AE 20p CD4002AE 20p CD4006AE 95p CD4007AE 20p CD4008AE 107p CD4009AE 61p CD4010AE 60p CD4011AE 20p CD4012AE 20p CD4013AE 55p CD4015AE 90p CD4016AE 50p CD4017AE 100p CD4018AE 110p CD4019AE 52p CD4020AE 120p CD4022AE 100p CD4023AE 82p CD4024AE 20p CD4025AE 22p CD4026AE 170p CD4027AE 65p CD4028AE 90p CD4029AE 120p CD4030AE 55p CD4035AE 131p CD4040AE 120p CD4042AE 90p CD4043AE 100p CD4044AE 104p CD4046AE 140p CD4047AE 100p CD4049AE 63p CD4050AE 57p CD4051AE 104p CD4054AE 120p CD4055AE 140p CD4056AE 135p CD4060AE 130p CD4069AE 27p CD4071AE 27p CD4072AE 27p CD4073AE 30p CD4081AE 21p CD4082AE 27p CD4093AE 95p CD4502AE 138p CD4510AE 130p CD4511AE 160p CD4516AE 112p CD4518AE 130p CD4528AE 120p MC14553 525p		<b>OP. AMPS</b> 1458 Dual Op Amp Int Comp 8 pin DIL 70p 3014 Ext. Comp 8 pin DIL 35p 3130 COSMOS/Bk-Polar MosFet 8 pin DIL 100p CA3140 BIMO. 8 pin DIL 110p CA3160 Int. Comp. 8 pin DIL 100p LM318N High speed 8 pin DIL 200p LM324N Quad Op. Amp. 14 pin DIL 120p NE531V High slew rate 8 pin DIL 140p 9900 Quad Op. Amp. 14 pin DIL 70p 709 Ext. Comp. 8/14 pin DIL 36p 741 Int. Comp. 8/14 pin DIL 22p 747 Dual 741 14 pin DIL 36p 748 Ext. Comp. 8/14 pin DIL 36p 776 Programmable Op. Amp. TO-5 180p		<b>TRANSISTORS</b> AC125 35p AC126 25p AC127 25p AC128 25p AC141 20p AC142 20p AC176 25p AC187 25p AC187K 30p AC188 25p AC189K 30p AD149 49p AD161 45p AD162 45p AF1105 30p AF115 30p AF116 30p AF117 30p AF127 25p AF139 43p AF239 48p BC107/B 9p BC108/B 9p BC109/B 9p BC109C 12p BC117 22p BC125 12p BC148 9p BC149C 10p BC157 11p BC158 10p BC159 11p BC169 12p BC172 11p BC177 18p BC178 17p BC179 18p BC182 12p BC183 12p BC184 13p BC187 30p BC212 11p BC213 10p BC214 14p BC451 16p BC478 30p BC479 30p BCY70 18p BCY71 22p BD124 130p BD131 130p BD132 65p BD133 65p BD136 50p BD139 52p BD140 58p BOY56 20p BF115 22p BF127 23p BF170 23p BF173 25p BF177 26p BF178 28p BF179 33p BF180 33p BF184 22p BF194 10p BF195 9p BF196 14p BF197 15p BF200 32p BF257 32p BF258 36p BF259 45p BF337 30p BF339 30p BF340 30p BF342 20p BF349 30p BF379 30p BF380 30p BF381 30p BF382 30p BF383 30p BF384 30p BF385 30p BF386 30p BF387 30p BF388 30p BF390 22p		<b>DIODES</b> *SIGNAL 9p OA47 9p OA81 20p OA85 20p OA90 7p OA91 7p OA95 7p OA200 8p OA202 10p IN914 4p IN915 4p IN4148 9p		<b>RECTIFIERS</b> *BY100 25p *BY126 12p *BY127 10p IN4001 5p IN4002 5p IN4004 6p IN4005 6p IN4007 7p IN5401 13p IN5404 18p IN5407 23p		<b>ZENER</b> 2.7V to 33V+ 7p *400mW 9p *1W 18p		<b>BRIDGE RECTIFIERS</b> *1A 50V 25p *1A 100V 27p *1A 200V 30p *1A 400V 32p *1A 600V 36p *2A 50V 30p *2A 100V 35p *2A 200V 40p *2A 400V 45p *3A 200V 60p *3A 600V 72p *4A 100V 80p *4A 400V 90p 6A 50V 90p 6A 100V 95p 6A 200V 108p 6A 400V 120p 10A 400V 270p 25A 400V 400p		<b>TRIACS</b> Plastic Amp Volts 3 400 85p 6 400 99p 6 500 107p 10 400 120p 10 500 140p 15 400 160p 15 500 180p 40A30 130p 40669 130p DIAC BR100 30p		<b>HEATSINK</b> For TO-220 Vol Regs and Transistors 17°C/W 25p	
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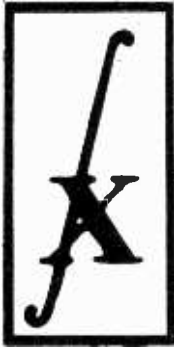
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The unit is designed to decode not only 45J but virtually all other 'quadroponic' systems (Not CD4), including the new BBC Matrix H.10 input selections.

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Complete kit, including licence fee £45.00 + VAT

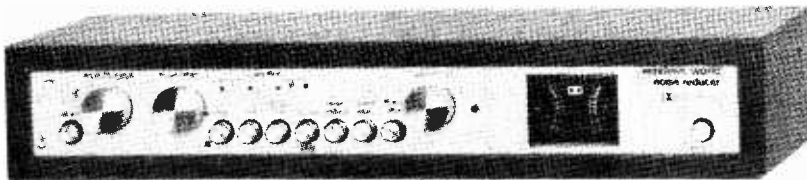
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**With Home Office Type approval.**

As in this issue of "Wireless World", designed by Mike Hosking, 240V ac mains operated and disguised as a hardbacked book. Detection range up to 30 feet. Complete kit. Exclusive designer approved kit £46.00 + VAT, all ready built and tested £54.00 + VAT.

## Wireless World Dolby<sup>TM</sup> noise reducer

Trademark of Dolby Laboratories Inc.



#### Typical performance

Noise reduction better than 9dB weighted.  
Clipping level 16.5dB above Dolby level (measured at 1% third harmonic content)

Harmonic distortion 0.1% at Dolby level typically 0.05% over most of band, rising to a maximum of 0.12%

Signal-to-noise ratio. 75dB (20Hz to 20kHz, signal at Dolby level) at Monitor output

Dynamic Range > 90db

30mV sensitivity.

#### Featuring

- switching for both encoding (low-level h.f. compression) and decoding.
- a switchable f.m. stereo multiplex and bias filter
- provision for decoding Dolby f.m. radio transmissions (as in USA)
- no equipment needed for alignment
- suitability for both open-reel and cassette tape machines
- check tape switch for encoded monitoring in three-head machines

Complete Kit **PRICE: £39.90 + VAT**

Also available ready built and tested ..... **Price £54.00 + VAT**

Calibration tapes are available for open-reel use and for cassette (specify which) ..... **Price £2.20 + VAT \***

Single channel plug-in Dolby<sup>TM</sup> PROCESSOR BOARDS (92 x 87mm) with gold plated contacts are available with all components ..... **Price £8.20 + VAT**

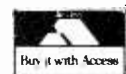
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Gold Plated edge connector ..... **Price £1.50 + VAT \***

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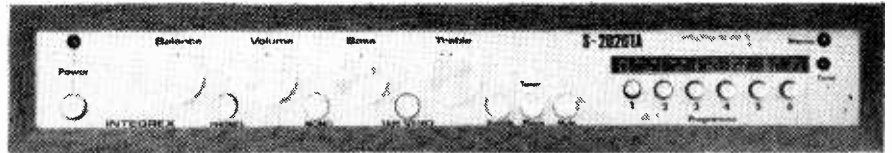
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# INTEGREX

## S-2020TA STEREO TUNER / AMPLIFIER KIT

**SOLID MAHOGANY CABINET**

*A high-quality push-button FM Varicap Stereo Tuner combined with a 24W r.m.s. per channel Stereo Amplifier.*

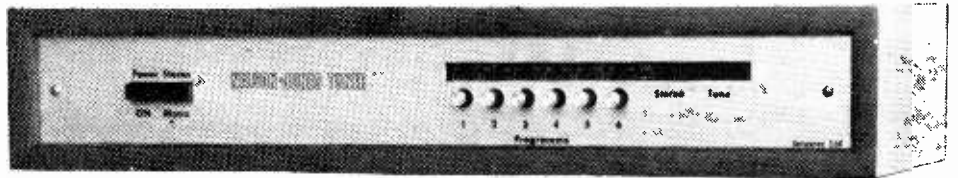


**Brief Spec.** Amplifier Low field Toroidal transformer, Mag. input, Tape In/Out facility (for noise reduction unit, etc.), THD less than 0.1% at 20W into 8 ohms. Power on/off FET transient protection. All sockets, fuses, etc., are PC mounted for ease of assembly. Tuner section uses 3302 FET module requiring no RF alignment, ceramic IF, INTERSTATION MUTE, and phase-locked IC stereo decoder. LED tuning and stereo indicators. Tuning range 88—104MHz. 30dB mono S/N @ 1.2  $\mu$ V. THD 0.3%. Pre-decoder 'birdy' filter.

**PRICE: £58.95 + VAT**

## NELSON-JONES STEREO FM TUNER KIT

*A very high performance tuner with dual gate MOSFET RF and Mixer front end, triple gang varicap tuning, and dual ceramic filter / dual IC IF amp.*



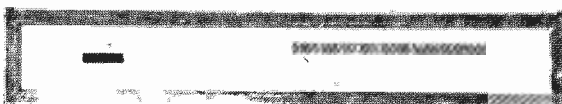
**Brief Spec.** Tuning range 88—104MHz. 20dB mono quieting @ 0.75  $\mu$ V. Image rejection — 70dB. IF rejection — 85dB. THD typically 0.4%. IC stabilized PSU and LED tuning indicators. Push-button tuning and AFC unit. Choice of either mono or stereo with a choice of stereo decoders.

*Compare this spec. with tuners costing twice the price.*

**Mono £32.40 + VAT**

**With ICPL Decoder £36.67 + VAT**

**With Portus-Haywood Decoder  
£39.20 + VAT**



Sens. 30dB S/N mono @ 1.2  $\mu$ V  
THD typically 0.3%  
Tuning range 88—104MHz  
LED sig. strength and stereo indicator

## STEREO MODULE TUNER KIT

*A low-cost Stereo Tuner based on the 3302 FET RF module requiring no alignment. The IF comprises a ceramic filter and high-performance IC Variable INTERSTATION MUTE. PLL stereo decoder IC. Pre-decoder 'birdy' filter Push-button tuning*

**PRICE: Stereo £31.95 + VAT**

## S-2020A AMPLIFIER KIT

*Developed in our laboratories from the highly successful "TEXAN" design. PC mounting potentiometers, switches, sockets and fuses are used for ease of assembly and to minimize wiring*

*Power 'on/off' FET transient protection.*

**Typ Spec.** 24+24W r.m.s. into 8-ohm load at less than 0.1% THD. Mag. PU input S/N 60dB. Radio input S/N 72dB. Headphone output. Tape In/Out facility (for noise reduction unit, etc.). Toroidal mains transformer.

**PRICE: £33.95 + VAT**

**ALL THE ABOVE KITS ARE SUPPLIED COMPLETE WITH ALL METALWORK, SOCKETS, FUSES, NUTS AND BOLTS, KNOBS, FRONT PANELS, SOLID MAHOGANY CABINETS AND COMPREHENSIVE INSTRUCTIONS**

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<b>BASIC MODULE TUNER KIT (stereo)</b>	<b>£16.75 + VAT</b>	<b>PUSH-BUTTON UNIT</b>	<b>£5.00 + VAT</b>
<b>PORTUS-HAYWOOD PHASE-LOCKED STEREO DECODER KIT</b>			<b>£8.00 + VAT</b>

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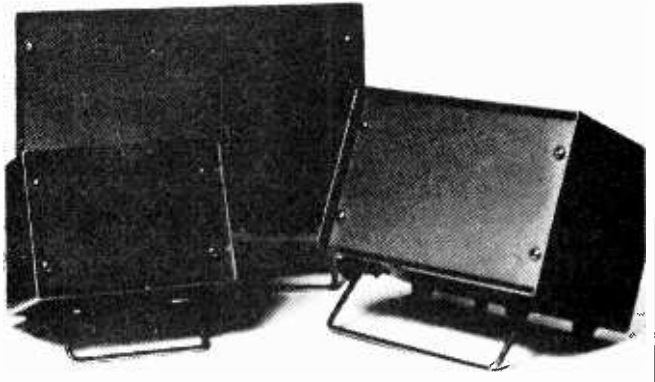
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0.3" DL704/2	65p*	2N5457 FET	
0.3" DL707/2	65p*	INS BUSH SETS, EA	
0.6" DL747/2	£1.00*	MATCHING ADD	
TCS308 GAS DETECTOR	£5.00*		
309pF MED./SHORT TUNER	£1.00*		
<b>AUDIBLE WARNING BLEEPER</b>		<b>FULL SPEC. PAKS</b>	
12V 100mA	£1.49*	PAK A 10 x LEDS	£1.00*
DALO PCB PEN 2 TIPS	74p*	PAK B 4 x 741G	£1.00*
SRBP 6" x 4"	80p*	PAK C 3 x 2N3055	£1.00*
FEC	£1.00*	PAK H 6 x 2N3819E	£1.00*
PCB ETCHING KIT	£2.00*	PAK K 40 x 1N914	£1.00*
		PAK N 25 x OA81/91	£1.00*
		PAK M 3 x 2 AMP, PNP/NPN	£1.00*
		PAIRS 60 VOLT (TOTAL 6)	£1.00*
<b>DIODES</b>		PAK W 20 x MIXED 10V	
OA81/91	5p	ELECTROLYTIC 2-100µf	
IN4148 & IN914 SILICON	4p*		
IN4001 5p*	IN4004 7p*		
B2788 ZENERS 400mW	10p*		
BRIDGE 1A 50V 25p*	6A		
	£1.00*		
		MORE PAKS IN FREE LISTS	

# OLSON

## MINICASES



Type	Overall Dimension			Case no vents	Case with vents	Chrome leg
	Width	Height	Depth			
21	6 1/2"	4 1/2"	4 1/2"	—	4.75	1.00
22	8 1/2"	5 1/2"	5 1/2"	—	5.35	1.00
23	10 1/2"	6 1/2"	6 1/2"	—	6.35	1.05
24	12 1/2"	7 1/2"	7 1/2"	—	6.95	1.05
25A	6 1/2"	4 1/2"	4 1/2"	4.60	5.15	1.05
25B	6 1/2"	4 1/2"	6 1/4"	4.85	5.40	1.05
26A	8 3/4"	5 3/4"	6 1/4"	6.50	7.05	1.05
26B	8 3/4"	5 3/4"	8 1/4"	6.83	7.38	1.05
27A	12 1/4"	7 1/2"	5 1/2"	7.10	7.75	1.05
27B	12 1/4"	7 1/2"	8"	7.70	8.35	1.05
28A	14"	10 1/2"	6 1/2"	8.40	9.05	—
28B	14"	10 1/2"	8 1/2"	9.13	9.78	—
29A	10"	4"	6"	5.88	6.43	1.05
29B	10"	4"	8"	6.20	6.75	1.05
30A	12"	5"	6"	6.40	7.05	1.05
30B	12"	5"	8"	6.70	7.35	1.05
31A	14"	6"	6"	7.00	7.65	1.05
31B	14"	6"	8"	7.35	8.00	1.05
61	15 1/2"	7 1/2"	9 1/2"	—	10.60	—
62	17 1/2"	8 1/2"	9 1/2"	—	12.35	—
63	16 1/2"	9 1/2"	9 1/2"	—	12.35	—
64	15 1/2"	7 1/2"	12 1/2"	—	12.35	—
65	17 1/2"	8 1/2"	12 1/2"	—	14.00	—
66	16 1/2"	9 1/2"	12 1/2"	—	14.00	—



## Better instruments. Better service.

We have established a nationwide network of approved service organisations to deal with the repair and maintenance of our instruments. Every repair is backed by a full 12 month guarantee. Here's where to find them.

**ENGLAND** London Instrument Repair Centre, Acton Lane, Chiswick, London W4 5HJ Trade Reception, Cunnington Street Tel: 01-995 9212  
 London Instrument Repair Centre, Archcliffe Road, Dover, Kent Tel: Dover (0304) 202620  
 Farnell International Instruments Ltd, Sandbeck Way, Wetherby, West Yorkshire LS22 4DH. Tel Wetherby (0937) 3541  
 T.E.R. Instrumentm'ts Ltd, Peel Lane, Astley, Manchester M29 7JH. Tel: Atherton (05234) 2275 or 5611  
 Midlands Instrument Repair Centre, Thorn Automation Ltd., Armitage Road, Rugeley, Staffs Tel: Rugeley (08894) 5151

**SCOTLAND** Falcon Electronics, 92 High Street, Johnstone, Scotland Tel: Johnstone (0505) 23377

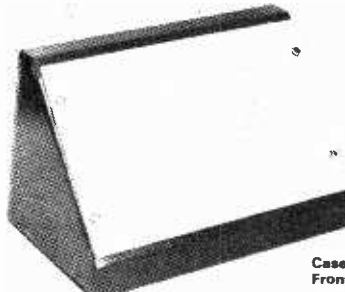
**WALES** Electro Services, 25 Chepstow Road, Newport, Gwent NPT 8BX Tel: Newport (0633) 211243

**LONDON INSTRUMENT REPAIR CENTRE**

The manufacturers' joint service organisation.

**WW-040 FOR FURTHER DETAILS**


## NEW OLSON SLOPING CASES



Cases made from 20G steel  
Front panels made from 20G aluminium

Type	Panel Dim	Depth	Height	Price
1	150 m/m x 100 m/m	95 m/m	95 m/m	£1.95p
2	200 m/m x 100 m/m	95 m/m	95 m/m	£2.25p
3	250 m/m x 100 m/m	95 m/m	95 m/m	£2.75p

### PORTABLE POWER DISTRIBUTION FOR INSTANT MAINS!



COMPLETE WITH 6FT. CABLE AND 13 AMP FUSED PLUG

4 sockets 13A	£9.75
6 sockets 13A	£11.50
4 sockets 13A switched	£11.25
6 sockets 13A switched	£12.50

**ALL DISTRIBUTION PANELS ARE FITTED WITH MK SOCKETS & PLUG**

Send for details of complete range

**OLSON ELECTRONICS LTD., FACTORY NO. 8, 5-7 LONG ST., LONDON E2 8HJ**  
 TEL: 01-739 2343

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# BI-PAK

High quality modules for stereo, mono and other audio equipment.



**NEW**

## PUSH-BUTTON STEREO FM TUNER

OUR PRICE ONLY  
**£20.45**

Fitted with Phase Lock-loop Decoder

The 450 Tuner provides instant program selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, by simply changing the settings of the pre-set controls.

Used with your existing audio equipment or with the BI-KITS STEREO 30 or the MK60 Kit etc. Alternatively the PS12 can be used if no suitable supply is available, together with the Transformer T538.

The S450 is supplied fully built, tested and aligned. The unit is easily installed using the simple instructions supplied.

- ★ FET Input Stage
- ★ VARI-CAP diode tuning
- ★ Switched AFC
- ★ Multi turn pre-sets
- ★ LED Stereo Indicator

**Typical Specification:**  
Sensitivity 3µ volts  
Stereo separation 30db  
Supply required 20-30v at 90 Ma max.

## MPA 30



Enjoy the quality of a magnetic cartridge with your existing ceramic equipment using the new M.P.A. 30, a high quality pre-amplifier enabling magnetic cartridges to be used where facilities exist for the use of ceramic cartridges only. It is provided with a standard DIN input socket for ease of connection. Full instructions supplied.

**£2.85**

## STEREO PRE-AMPLIFIER



## PA 100 OUR PRICE £13.75

A top quality stereo pre-amplifier and tone control unit. The six push-button selector switch provides a choice of inputs together with two really effective filters for high and low frequencies, plus tape output.

**MK. 60 AUDIO KIT:** Comprising 2 x AL60's, 1 x SPM80, 1 x BTM80, 1 x PA100, 1 front panel and knobs. 1 Kit of parts to include on/off switch, neon indicator, stereo headphone sockets plus instruction booklet. **COMPLETE PRICE £34.90** plus 85p postage.

**TEAK 60 AUDIO KIT:** Comprising Teak veneered cabinet size 16 3/4" x 11 1/2" x 3 3/4", other parts include aluminium chassis, heatsink and front panel bracket plus back panel and appropriate sockets. **Kit PRICE £13.25** plus 85p postage

Frequency Response + 1dB 20Hz 20KHz. Sensitivity of inputs  
1. Tape Input 100mV into 100K ohms  
2. Radio Tuner 100mV into 100K ohms  
3. Magnetic P.U. 3mV into 50K ohms  
P.U. Input equalises to R1AA curve with 1dB from 20Hz to 20KHz  
Supply — 20-35V at 20mA

Dimensions —  
299mm x 89mm x 35mm.

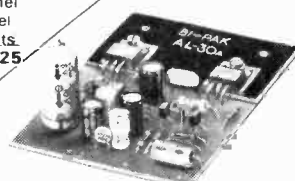
## NEW AL30A 10w R.M.S. AUDIO AMPLIFIER MODULE

The AL30A is a high quality audio amplifier module replacing our AL20 & 30. The versatility of its design makes it ideal for record players, tape recorders, stereo amps, cassette and cartridge players. A power supply is available comprising a PS12 together with a transformer T538, also for stereo, the pre-amp PA12.

**SPECIFICATION:**

- Output Power 10w. R.M.S.
- Load Impedance 8 to 6ohms.
- Sensitivity 90mv for full output.
- Frequency Response 60Hz to 25KHz ± 2db.
- Supply 22 to 32 volts.
- Input Impedance 50K.
- Total Harmonic Distortion Less than .5% (Typically .3%).
- Max. Heat Sink Temp 80 c.

● Dimensions 90 x 64 x 27mm



**ONLY £3.65**

**VAT  
ADD  
12 1/2%**

## POSTAGE & PACKING

Postage & Packing add 25p unless otherwise shown. Add extra for airmail. Min. £1.00

## STEREO 30 COMPLETE AUDIO

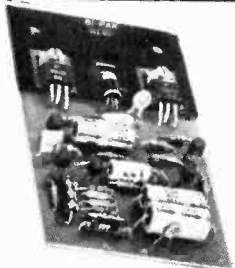
7+7 WATTS  
R.M.S.



**£16.25**

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a wide range of inputs i.e. high quality ceramic pick-up, stereo tuner, stereo tape deck etc. Simple to install, capable of producing really first class results, this unit is supplied with full instructions, black front panel knobs, main switch, fuse and fuse holder and universal mounting brackets enabling it to be installed in a record plinth, cabinets of your own construction or the cabinet available. Ideal for the beginner or the advanced constructor who requires Hi-Fi performance with a minimum of installation difficulty (can be installed in 30 mins).

**TRANSFORMER £3.25** plus 50p p & p  
**TEAK CASE £5.45** plus 70p p & p



## AL 60 25 Watts (RMS)

- ★ Max Heat Sink temp 90C.
- ★ Frequency response 20Hz to 100KHz
- ★ Distortion better than 0.1 at 1KHz
- ★ Supply voltage 15-50v
- ★ Thermal Feedback
- ★ Latest Design Improvements
- ★ Load — 3,4,8, or 16 ohms
- ★ Signal to noise ratio 80db
- ★ Overall size 63mm. 105mm. 13mm.

Especially designed to a strict specification. Only the finest components have been used and the latest solid-state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F. enthusiast.

**£4.35**

## NEW PA12

Frequency Response 20Hz-20KHz (-3dB). Bass and Treble range, 12dB. Input Impedance 1 meg ohm. Input Sensitivity, 300mV. Supply requirements 24V 5mA. Size 152mm x 84mm x 33mm.

**NEW PA12 Stereo Pre-Amplifier completely redesigned for use with AL30A Amplifier Modules.** Features include on/off volume, Balance, Bass and Treble controls. Complete with tape output.

**£6.70**

## PS12

Power supply for AL30A, PA12, SA450, etc.

Input voltage 15-20v A.C. Output voltage 22-30v D.C. Output current 800 mA Max. Size 60mm x 43mm x 26mm. **OUR PRICE £1.30**  
Transformer T538 £3.20

## Stabilised Power Supply Type SPM80

SPM80 is especially designed to power 2 of the AL60 Amplifiers, up to 15 watts (R.M.S.) per channel simultaneously. With the addition of the Mains Transformer BMT80, the unit will provide outputs of up to 1.5A at 35V. Size: 63mm. 105mm. 30mm. Incorporating short circuit protection.

Transformer BMT80  
**£5.30 + 86p postage**


**£3.75**

# BI-PAK

P.O. BOX 6,  
WARE,  
HERTS.

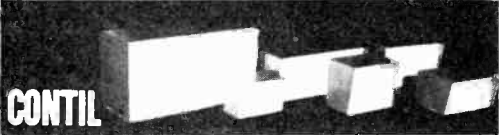
SHOP AT 18 BALDOCK ST., WARE, HERTS  
OPEN 9 to 5.30 Mon. / Sat.

## WEST HYDE Instrument cases



**MOD 3**

Offer instrument manufacturers low-cost cases ex-stock. Blue PVC coated steel strength and rigidity. PVC aluminium grey front and rear panels are removable. PCB and PSU mounting system available. Also available in black.



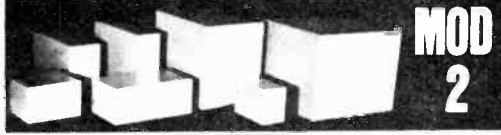
**CONTIL**

A range of eyebrow cases in blue textured acrylic. Front panels normally white zinc or PVC/aluminium, also available unpainted up to 1277 size. Aluminium panels extra.

All dimensions are Width x Height x Depth  
PRICES 1 off inc. P & P but not VAT.

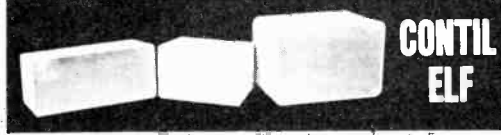
<b>MOD-3 (including chassis)</b>		
301	7x3 x5 1/2"	7.19
302	7x4 1/4 x5 1/4"	7.39
303	7x6 x5 1/4"	8.59
304	11x3 x5 1/4"	7.85
305	11x4 1/4 x5 1/4"	9.19
306	11x6 x5 1/4"	10.99
<b>CONTIL TEXTURED</b>		
755	7x5x5"	8.68
867	8x7x6"	10.30
975	9x5x7"	10.30
1277	12x7x7"	11.86
1277	unpainted	8.83
16127	16x7x12"	16.36
191010	19x10x10"	22.53
<b>ELF CASES Grey (inc. chassis)</b>		
Elf	6x4x4"	3.20
Bare Elf (less ft. ch. pnl)		2.15
Giant Elf	8x5 1/4 x5"	4.50
Long Elf	9x4x3"	3.60
Jumbo Elf	10 1/4 x5 1/4 x5 1/4"	5.40
<b>MOD-2 CASES (including chassis)</b>		
A	4.5 x 3x 6.5"	9.05
B	4.5 x 7x 6.5"	9.70
C	4.5x10x 6.5"	11.34
D	9 x 3x 6.5"	8.72
E	9 x 7x 6.5"	10.80
F	9 x10x 6.5"	12.80
G	13 x 3x 6.5"	10.78
H	13 x 7x 6.5"	12.36
I	13 x10x 6.5"	14.51
J	18 x 3x 6.5"	13.82
K	18 x 7x 6.5"	16.17
L	18 x10x 6.5"	20.00
M	4.5x 3x13"	10.67
N	4.5x 7x13"	11.48
O	4.5x10x13"	13.53
P	9 x 3x13"	11.36
Q	9 x 7x13"	12.98
R	9 x10x13"	15.25
S	13 x 3x13"	13.28
T	13 x 7x13"	15.27
U	13 x10x13"	17.92
V	18 x 3x13"	16.77
W	18 x 7x13"	19.64
X	18 x10x13"	24.10

Mod-2 in Wood-grain or Black finish in sizes A-L & N.



**MOD 2**

Mod-2 cases over 24 sizes. Front and back panels grey PVC. Aluminium chassis included. Packed flat. Outer casing blue PVC steel or up to size L also available in wood-grain and black.




**CONTIL ELF**

These tough little cases add very little to the cost of a job. Front panel aluminium with protective coat. Elf cases are available in 4 sizes, all dough moulded in grey glass polyester, all panels, feet and chassis included.

All West Hyde cases are available with substantial discounts for quantities. Most cases have discounts at 5 off and 25 off with discounts up to 25% at 100 off. Prices include P & P and are less 10% if collected, on first two price breaks on cases only.

**BUY A CASE FROM A SMALL RANGE, YOU GET A CASE—BUY A CASE FROM A BIG RANGE, YOU GET A SOLUTION**

## Instrument cases



**BRIGHTCASE MARK II**

BC212 (3 1/4" Full Rack)	23.01
BC222 (3 1/4" Half Rack)	18.63
BC312 (5 1/4" Full Rack)	25.24
BC322 (5 1/4" Half Rack)	18.61

Rack Brackets available

**MINOS**


M2	85x100x50mm	.73
M3	100x130x50mm	.84
M2	Bare	.48
M3	Bare	.56

**SAMOS**

S1	100x 50x50mm	1.36
S2	100x 100x50mm	1.56
S3	100x 150x50mm	1.74
S4	125x 50x75mm	1.96
S5	125x100x75mm	2.24
S6	125x150x75mm	2.63
S7	125x200x75mm	2.92


**HEAVY DUTY CASE**

8x 8x5"	16.38
10x10x7"	22.95
12x10x7"	25.95



**SAMOS**

Miniature instrument cases in blue and white PVC steel. Assemble in the lower half, clip-in feet. 2 screws allow the cover to hinge off cases. 2 more to fix. PC feet are available to hold up to 4 PC boards horizontally in case.



**HEAVY DUTY**

Available in 3 sizes. Heavily constructed in zinc steel, welded corners with heavy hinges. 2 screw fixings and foam around the door. In the base is a gland plate with gasket and a chassis with screws provided.

**OVER 400 DIFFERENT CASES IN STOCK—SIZE RANGE OVER 5000:1 IN VOLUME**

Prices correct October 1977

Send for catalogue

### WEST HYDE

DEVELOPMENTS LIMITED  
Ryefield Crm., Northwood Hills, Northwood, Middx., HA6 1NN  
Telephone: Northwood 24941/26732/27051  
Telex: 822231 West Hyde Nthwd.

WW—091 FOR FURTHER DETAILS



**TELECRAFT**  
COLOUR ENCOUNTER

**TELECRAFT**  
COLOUR ENCOUNTER

# TELECRAFT

## THESE UNBEATABLE OFFERS CANNOT LAST!

## SAVE YOU MORE POUNDS—

**T.V. GAME MODULES** Colour (as illustrated left) £16.50. Black and white (below) £10.50. Colour Converter for black and white games £6.60.

**T.V. GAME I.C.'s** AY-3-8500 £5.00; AY-3-8550 (gives horizontal and vertical bat movement) £8.50; the SPORTELENT 600 (three games in colour with horizontal and vertical bat movement) £15.00.

**TELETEXT DECODERS** (as illustrated below right) the TIFAX XM11 £99.90 (for a limited period only).

Application drawings supplied with all items and technical assistance available.




### TELECRAFT

53 Warwick Road, New Barnet, Herts EN5 5EQ  
Telephone: 01-440 7033

Personal callers and trade enquiries welcome  
Cheques and Postal Orders to be made payable to "Telecraft"  
Prices include VAT, postage and packing

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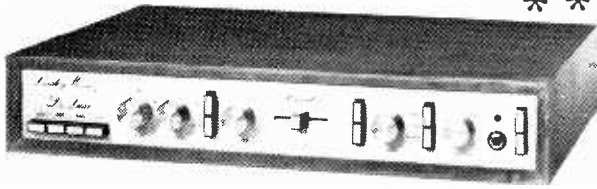


KENYA HOLLAND JAMAICA UNITED ARAB EMIRATES NORWAY SINGAPORE ICELAND SWEDEN MALAYSIA INDONESIA BRAZIL SWITZERLAND ZAMBIA GIBRALTAR CHILE SPAIN

IRENE GRENADA SAUDI ARABIA NEW ZEALAND NORWAY SINGAPORE ICELAND SWEDEN MALAYSIA INDONESIA BRAZIL SWITZERLAND ZAMBIA GIBRALTAR CHILE SPAIN

# POWERTRAN AUDIO KIT SUPPLIERS TO THE WORLD

## NEW! DE LUXE EASY TO BUILD LINSLEY-HOOD 75W AMPLIFIER

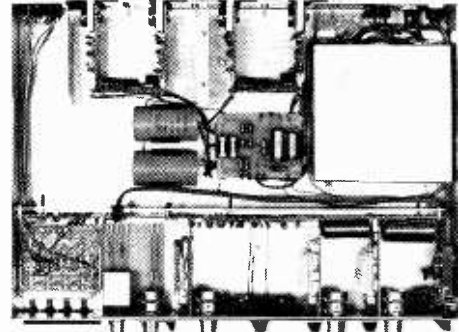


Available as Separate Packs

Details in Free Catalogue

**SPECIAL PRICE FOR COMPLETE KIT £99.30**

The standard model of our kit for Mr. Linsley-Hood's 75 watt design has for a long time offered exceptional performance for a very modest cost (just look at prices for comparable high quality high power ready-built units). Features of the amplifier include very low distortion (less than 0.01%), 75W rms per channel power output, rumble filter, variable slope scratch filter, variable transition frequency tone controls, tape monitoring facilities and individually adjustable inputs. This model is based on 5 circuit boards which not having the controls mounted on them can, if desired, be effectively used separately in high performance audio systems not based on our metalwork. Our new De Luxe model uses 14 boards which interconnect with gold plated contacts and have the potentiometers and switches fitted to them. There are 3 boards for each power amplifier, 1 board for the power supply and 7 boards for the stereo pre amplifier. This system almost eliminates internal wiring, making construction delightfully straightforward and as each board can be easily removed in seconds from the chassis, checking and maintenance is so simple that even newcomers to electronics will be able to cope competently with the kit. Additional features of our new model are inclusion of latest circuit improvements, generously sized heatsinks for heavy duty use, even in tropical climates and metal oxide resistors throughout for long-term stability and reliability.



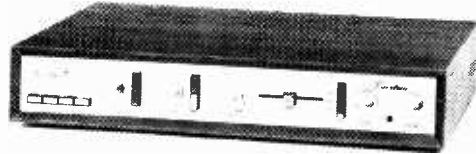
Internal view of De Luxe Kit

There are 3 boards for each power amplifier, 1 board for the power supply and 7 boards for the stereo pre amplifier. This system almost eliminates internal wiring, making construction delightfully straightforward and as each board can be easily removed in seconds from the chassis, checking and maintenance is so simple that even newcomers to electronics will be able to cope competently with the kit. Additional features of our new model are inclusion of latest circuit improvements, generously sized heatsinks for heavy duty use, even in tropical climates and metal oxide resistors throughout for long-term stability and reliability.

### PACK PRICES FOR STANDARD KIT

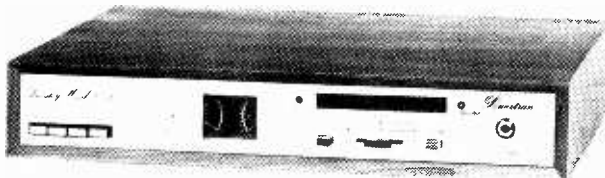
Pack	Price	Pack	Price
1. Fibreglass printed circuit board for power amp	£1.15	11. Fibreglass printed-circuit board for power supply	£0.85
2. Set of resistors, capacitors, pre-sets for power amp	£2.50	12. Set of resistors, capacitors, secondary fuses, semiconductors for power supply	£5.40
3. Set of semiconductors for power amp	£6.50	13. Set of miscellaneous parts including DIN skts., mains input skt., fuse holder, interconnecting cable, control knobs	£6.20
4. Pair of 2 drilled, finned heat sinks	£1.10	14. Set of metalwork parts including silk screen printed fascia panel and all brackets, fixing parts, etc.	£8.20
5. Fibreglass printed-circuit board for pre-amp	£1.90	15. Handbook (free with complete kit)	£0.30
6. Set of low noise resistors, capacitors, pre-sets for pre-amp	£4.10	16. Teak cabinet 18.3" x 12.7" x 3.1"	£10.70
7. Set of low noise, high gain semiconductors for pre-amp	£2.40		
8. Set of potentiometers (including mains switch)	£3.50		
9. Set of 4 push-button switches, rotary mode switch	£5.40	2 each of packs 1-7 inclusive are required for complete stereo amplifier. Total cost of individually purchased packs	£90.80
10. Toroidal transformer complete with magnetic screen/ housing primary: 0 117-234 V; secondaries: 33-0-33 V, 25-0-25 V	£10.95		

### STANDARD LINSLEY-HOOD 75W AMPLIFIER



**SPECIAL PRICE FOR COMPLETE KIT £79.80**

### LINSLEY-HOOD CASSETTE DECK

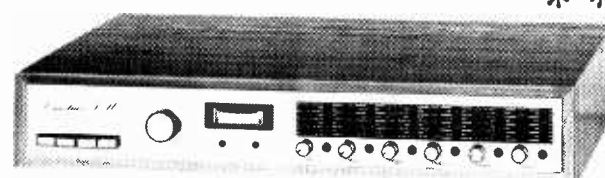


**SPECIAL PRICE FOR COMPLETE KIT £79.60**

Published in Wireless World (May, June, August 1976) by Mr. Linsley-Hood, this design, although straightforward and relatively low cost, nevertheless provides a very high standard of performance. To permit circuit optimization separate record and replay amplifiers are used, the latter using a discrete component front-end designed such that the noise level is below that of the tape background. Push button switches are used to provide a choice of equalization time constants, a choice of bias levels and also an option of using an additional pre-amplifier for microphone use. The mechanism used is the Goldring-Lenco CRV, a unit distinguished in its robustness and ease of operation. Speed control and automatic cassette ejection are both implemented by electronic circuitry. This unit which is powered by a toroidal transformer and uses metal oxide resistors throughout offers an excellent match for the Wireless World Tuner and the Linsley-Hood 75 Watt Amplifier.

Pack	Price	Pack	Price
1. Stereo PCB (accommodates 2 rep. amps, 2 meter amps, bias/erase osc. relay)	£3.35	10. Set of capacitors, rectifiers, I.C. voltage regulator for power supply (Powertran design)	£2.80
2. Stereo set of capacitors, M.D. resistors, potentiometers for above	£7.95	11. Set of miscellaneous parts, including sockets, fuse holder, fuses, interconnecting wire, etc.	£3.40
3. Stereo set of semiconductors for above	£8.50	12. Set of metalwork including silk screened fascia panel, internal screen, fixing parts, etc.	£7.10
4. Miniature relay with socket	£2.90	13. Construction notes	£0.25
5. PCB, all components for solenoid, speed control circuits	£3.80	14. Teak cabinet 18.3" x 12.7" x 3.1"	£10.70
6. Goldring-Lenco mechanism as specified	£18.50		
7. Function switch, knobs	£1.90	One each of packs 1-14 inclusive are required for complete stereo cassette deck. Total cost of individually purchased packs	£83.80
8. Dual VU meter with illuminating lamp	£6.95		
9. Toroidal transformer with E.S. screen prim. 0-117V, 234V, Sec. 15V	£4.90		

### WIRELESS WORLD FM TUNER



**SPECIAL PRICE FOR COMPLETE KIT £70.20**

Designed in response to demand for a tuner to complement the world-wide acclaimed Linsley-Hood 75W Amplifier, this kit provides the perfect match. The Wireless World (Skingley and Thompson) published original circuit has been developed further for inclusion into this outstanding slimline unit and features a pre-aligned front end module, excellent a.m. rejection and temperature compensated varicap tuning, which may be controlled either continuously or by push-button pre-selection. Frequencies are indicated by a frequency meter and sliding LED indicators, attached to each channel selector pre-set. The PLL stereo decoder incorporates active filters for 'birdy' suppression and power is supplied via a toroidal transformer and integrated regulator. For long term stability metal oxide resistors are used throughout.

Pack	Price	Pack	Price
1. Fibreglass printed board for front end IF strip, demodulator, AFC and mute circuits	£2.15	10. Frequency meter, meter drive components, fibreglass printed circuit board	£10.35
2. Set of metal oxide resistors, thermistor, capacitors, cermet preset for mounting on Pack 1	£4.80	11. Toroidal transformer with electrostatic screen. Primary: 0-117V 234V	£4.90
3. Set of transistors, diodes, LED, integrated circuits for mounting on Pack 1	£5.25	12. Set of capacitors, rectifiers, voltage regulator for power supply	£2.10
4. Pre-aligned front end module, cell assembly, three section ceramic filter	£8.50	13. Set of miscellaneous parts, including sockets, fuse holder, fuses, inter-connecting wire, etc.	£2.05
5. Fibreglass printed circuit board for stereo decoder	£1.10	14. Set of metalwork parts including silk screen printed fascia panel, acrylic silk screen printed tuning indicator panel insert, internal screen, fixing parts, etc.	£8.30
6. Set of metal oxide resistors, capacitors, cermet preset for decoder	£2.60	15. Construction notes (free with complete kit)	£0.25
7. Set of transistors LED, integrated circuit for decoder	£2.90	16. Teak cabinet 18.3" x 12.7" x 3.1"	£10.70
8. Set of components for channel selector switch module including fibreglass printed circuit board, push-button switches, knobs, LEDs, preset adjusters, etc.	£9.40	One each of packs 1-16 inclusive are required for complete stereo FM tuner. Total cost of individually purchased packs	£81.15
9. Function switch, 10 turn tuning potentiometer, knobs	£5.80		

## EXPORT A SPECIALITY!

Our Export Department can readily despatch orders of any size to any country in the world. Some of the countries to which we sent kits last year are shown in this advertisement. To assist in estimating postal costs our catalogue gives the weights of all packs and kits. This will be sent free on request, by airmail, together with our 'Export Postal Guide' which gives current postage prices.

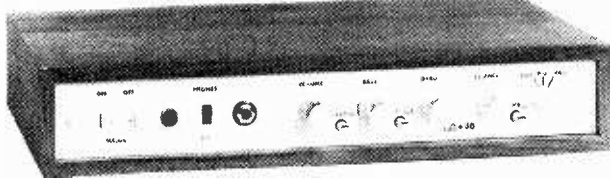
EXPORT ORDERS: No minimum order charge! Prices same as for U.K. customers but no Value Added Tax charged. Postage charged at actual cost plus 50p documentation and handling. Please send payment with order by Bank Draft, Postal Order, International Money Order or cheque drawn on an account in the U.K. Alternatively for orders over £500 we will accept Irrevocable Letter of Credit payable at sight in London.

**OUR CATALOGUE IS FREE**  
JUST SEND YOUR NAME AND ADDRESS TO RECEIVE YOURS



# T20 + 20 AND T30 + 30 20W, 30W AMPLIFIERS

\*\*



Designed by Texas engineers and described in Practical Wireless, the Texan was an immediate success. Now developed further in our laboratories to include a Toroidal transformer and additional improvements, the slimline T20 + 20 delivers 20W rms per channel of true Hi-Fi at exceptionally low cost. The easy to build design is based on a single F/Glass PCB and features all the normal facilities found on quality amplifiers including scratch and fumble filters, adaptable input selector and headphones socket. In a follow-up article in Practical Wireless further modifications were suggested and these have been incorporated into the T30 + 30. These include RF interference filters and a tape monitor facility. Power output of this model is 30W rms per channel.

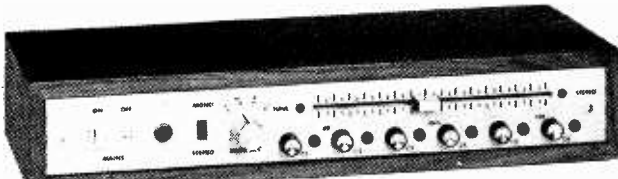
Pack	T20	T30	Pack	T20	T30
1. Set of low noise resistors	£1.60	£1.70	9. Fibreglass PCB	£3.50	£3.90
2. Set of small capacitors	£2.60	£3.40	10. Set of metalwork, fixing parts	£5.20	£6.20
3. Set of power supply capacitors	£2.20	£2.50	11. Set of cables, mains lead	£0.40	£0.40
4. Set of miscellaneous parts	£3.50	£3.50	12. Handbook (free with complete kit)	£0.25	£0.25
5. Set of slide, males, P.B. switches	£1.50	£1.50	13. Teak cabinet 15.4" x 6.7" x 2.8"	£4.50	£4.50
6. Set of pots, selector switch	£2.80	£2.80			
7. Set of semiconductors, ICs, skts.	£7.25	£7.75			
8. Toroidal transformer—240V prim.			One each of Pack 1-13 are required for complete stereo amplifier. Total cost of individually purchased packs T20 + 20 £40.90. T30 + 30 £45.60.		
e.s. screen	£5.60	£7.20			

SPECIAL PRICES FOR COMPLETE KITS

T20 + 20 KIT PRICE **£33.10** T30 + 30 KIT PRICE **£38.40**

## WWII TUNER

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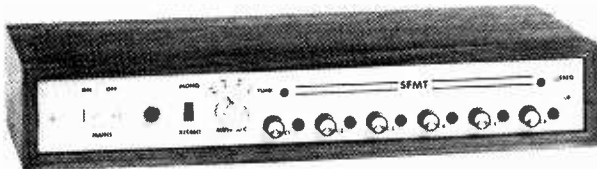


Following the success of our **Wireless World FM Tuner Kit** this cost reduced model was designed to complement the **T20 + 20** and **T30 + 30** amplifiers and the cabinet size, front panel format and electrical characteristics make this tuner compatible with either. The frequency meter of the more advanced model has been omitted and the mechanics simplified, however the circuitry is identical and this kit offers most outstanding value for money. Facilities included are switchable afc, adjustable, switchable muting, LED tuning indication and both continuous and push-button channel selection (readily adjusted by controls on the front panel).

SPECIAL PRICE FOR COMPLETE KIT **£47.70** AVAILABLE AS SEPARATE PACKS — PRICES IN OUR FREE CATALOGUE

## POWERTRAN S.F.M.T. TUNER

\*\*



The requirement was a simple, low cost design which could be constructed easily without special alignment equipment but which still gives a first class output suitable for feeding any of our very popular amplifiers or any other high quality audio equipment. Not finding a suitable published circuit, the requirement was met by design and development work in our own laboratories and this tuner, which uses a pre-aligned front end module can be set up with the aid of nothing more sophisticated than a multi-meter. A phase-locked-loop is used for stereo decoding and controls include switchable afc, switchable muting and push-button channel selection (adjustable by controls on the front panel). This unit matches well with the T20 + 20 and T30 + 30 amplifiers.

PRICE FOR COMPLETE KIT **£35.90** AVAILABLE AS COMPLETE KIT ONLY

**Wireless World Amplifier Designs.** Full kits are not available for these projects but component packs and PCBs are stocked for the highly regarded Bailey and 20W class AB Linsley-Hood designs together with an efficient regulated power supply of our own design. Suitable for driving these amplifiers is the Bailey Burrows pre-amplifier and our circuit board, for the stereo version of it features 6 inputs, scratch and fumble filters and wide range tone controls, which may be either rotary or slider operating. For tape systems a set of three PCBs have been prepared for the integrated circuit based, high performance stereo Stuart design. Details of component packs are in our free Catalogue.

30W Bailey Amplifier	
BAIL Pk 1 F/Glass PCB	£1.00
BAIL Pk 2 Resistors, Capacitors Potentiometer set	£2.35
BAIL Pk 3 Semiconductor set	£4.70
20W Linsley-Hood Class AB	
LHAB Pk 1 F/Glass PCB	£1.05
LHAB Pk 2 Resistor Capacitor Potentiometer set	£3.20
LHAB Pk 3 Semiconductor set	£3.35
Regulator Power Supply	
60VS Pk 1 F/Glass PCB	£0.85
60VS Pk 2 Resistor Capacitor set	£2.20
60VS Pk 3 Semiconductor set	£3.10
60VS Pk 6A Toroidal transformer (for use with Bailey)	£8.80
60VS Pk 6B Toroidal transformer (for use with 20W LH)	£7.25
Bailey Burrows Stereo Pre-Amp	
BBPA Pk 1 F/Glass PCB (stereo)	£2.80
BBPA Pk 2 Resistor Capacitor Semiconductor set (stereo)	£6.70
BBPA Pk 3R Rotary Potentiometer set (stereo)	£2.85
BBPA Pk 3S Slider Potentiometer set with knobs (stereo)	£3.10
Stuart Tape Recorder	
TRRP Pk 1 Replay Amp F/Glass PCB (stereo)	£1.30
TRRC Pk 1 Record Amp F/Glass PCB (stereo)	£1.70
TROS Pk 1 Bias Erase/Stabilizer F/Glass PCB (stereo)	£1.20

## SQ QUADRAPHONIC DECODERS

These state-of-the-art circuits described by CBS are offered as kits of superior quality with close tolerance capacitors, metal oxide resistors and Fibreglass PCBs designed for edge connector insertion. Further information on these kits is given in our FREE CATALOGUE.

M1 Basic matrix decoder	£5.90
L1 Full logic decoder	£17.20
L2A Full logic decoder with variable blend	£22.60
L3A As L2A but with high performance discrete component front end (or with carbon film resistors)	£30.10
SQM1 30 Decoder complete with 30W rear channel amplifiers. Complete kit matches T30 + 30 amplifier	£25.90
	£40.75

**Value Added Tax not included in prices UK Carriage FREE**

**PRICE STABILITY:** Order with confidence! Irrespective of any price changes we will honour all prices in this advertisement until December 31st, 1977, if this month's advertisement is mentioned with your order. Errors and VAT rate changes excluded.

**U.K. ORDERS:** Subject to 12½% surcharge for VAT (i.e. add ½ to the price). No charge is made for carriage, \*or at current rate if changed.

**SECURICOR DELIVERY:** For this optional service (U.K. mainland only) add £2.50 (VAT inclusive) per kit.

**SALES COUNTER:** If you prefer to collect your kit from the factory call at Sales Counter (at rear of factory) Open 1 p.m.-4.30 p.m. Monday-Thursday.

## SEMICONDUCTORS

as used in our range of quality audio equipment

2N699	£0.20	BC107	£0.10	BF257	£0.40	MPSA05	£0.25	TIP30C	£0.60
2N3055	£0.45	BC108	£0.10	BF259	£0.47	MPSA12	£0.35	TIP41A	£0.70
2N3442	£1.20	BC109	£0.10	BFR39	£0.30	MPSA55	£0.25	TIP42A	£0.80
2N3711	£0.09	BC109C	£0.12	BFR79	£0.30	MPSA65	£0.35	TIP41B	£0.75
2N3904	£0.17	BC125	£0.15	BFY51	£0.20	MPSA66	£0.40	TIP42B	£0.80
2N3906	£0.20	BC126	£0.15	BFY52	£0.20	MPSU05	£0.50	1N914	£0.07
2N5087	£0.25	BC182	£0.10	CA3046	£0.70	SBA750A	£1.90	1N916	£0.07
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2N5457	£0.45	BC182L	£0.10	LP1185	£6.80	SL304S	£1.20		
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2N5460	£0.50	BC212L	£0.12	MC1351	£1.05	SN72748P	£0.40		
2N5461	£0.50	BC214L	£0.14	MC1741CG	£0.65	STCR53	£2.40		
2N5830	£0.35	BCY72	£0.13	MFC4010	£0.95	TIL209	£0.20		
40361	£0.40	BD529	£0.65	MJ4B1	£1.20	TIP29A	£0.40		
40362	£0.45	BD530	£0.55	MJ491	£1.45	TIP30A	£0.45	FM4	£1.00
74004	£0.35	BDY56	£1.60	MJE521	£0.60	TIP29C	£0.55	SFJ10 7MA	£1.50

## NEW PROJECTS

### LINSLEY-HOOD LOW DISTORTION OSCILLATOR

A Wien bridge audio oscillator (10Hz-100KHz) with sine or square wave output (1mV-1V) published in Wireless World September, October 1977

Pack 1 Fibreglass PCB	£2.65
Pack 2 Capacitors, 2% metal oxide resistors	£2.60
Pack 3 Transistors, IC, IC socket, thermistor	£3.90
Pack 4 Potentiometers and switches	£2.80

### ERIC F. TAYLOR PRE-AMPLIFIER

A low noise, low distortion (0.005%) stereo pre-amplifier for use with magnetic pick-up (RIAA equalization)

Pack 1 Fibreglass PCB (Stereo)	£1.45
Pack 2 Metal oxide resistors, capacitors (Stereo)	£3.20
Pack 3 Transistors, ICs, IC sockets, zeners (Stereo)	£4.20

For further details of these please ask for our NEW PROJECTS LIST

**QUALITY:** All components are brand new first grade full specification guaranteed devices. All resistors (except where stated as metal oxide) are low noise carbon film types. All printed circuit boards are fibreglass, drilled roller tinned and supplied with circuit diagrams and construction layouts.

**AFTER-SALES BACK-UP:** Servicing facilities (very rarely required for our kits) are available for all \*\* complete kits. Further details will be sent on request.

**FOR FURTHER INFORMATION PLEASE WRITE OR TELEPHONE FOR OUR FREE CATALOGUE**

DEPT WW11

# POWERTRAN ELECTRONICS

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# Electronic Brokers

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★ 78 Station ASCII Keyboard including separate numeric cluster, cursor control keys, and 6 special function keys

★ Standard TTL logic

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★ 8-bit ASCII code (including parity) providing full 96-character set with upper and lower case outputs

★ negative strobe with 4.0 ms delay  
Overall dimensions 16½ x 7¾ x 2", supplied complete with full technical data and circuit diagrams.

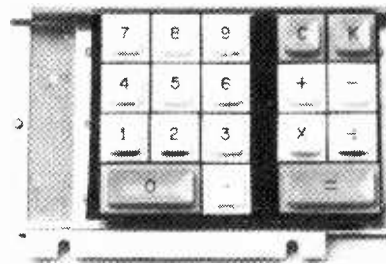
PRICE: £55.00 + £1 25 p&p + 8% VAT (send £60 75)

**DXS-CRT 96** station ASCII11B-coded TTL-compatible 4 bank alphanumeric keyboard 8-bit code upper and lower case alpha output plus separate numeric pad Delayed strobe and 2-key rollover. Mounted in attractive box overall dimensions 20½ x 7¼ x 3½"

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#### 18-KEY PUSH-BUTTON CALCULATOR KEYBOARD

Numerals 0-9 decimal point C K + - × ÷ = Mounted on PCB overall dimensions 5½ x 4¾ x 1½"

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#### ★ ASCII Keyboard

★ Hard copy unit (friction or sprocket paperfeed)

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11" CRT XY input, stored resolution 400 x 300 line pairs

**COSSOR** D10S 401-2A and 402-2A visual display units, 13 lines of 80 characters, 600/1200 baud rate, modified ASCII code.

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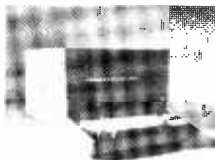
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#### HAZELTINE 1000

Compact terminal providing 12 line by 80 character display (960 chs.), full/half Duplex, MOS-shift register memory with constant refresh Underline cursor

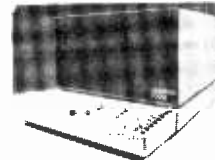
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★ Teletype-compatible ★ 12" Diagonal Screen ★ TTY Format Keyboard ★ 64 ASCII Character Set ★ 5 x 7 Dot Matrix ★ Switch-selectable Transmission Rate up to 9600 baud ★ Switch-selectable Parity ★ Standard CCITT V.24 Interface

**HAZELTINE 1200** All the features of the Model 1000 but with double screen capacity of 1920 characters (24 lines of 80). Reverse block image Cursor

**New List Price £941.**  
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#### HAZELTINE 2000

Superb buffered terminal with full edit facilities, 1998 character capacity (27 lines of 74), detachable ASCII keyboard including 10-key numeric pad and 13-key edit/cursor control cluster Selectable transmission full/half Duplex or batch

**New List Price £1649.**  
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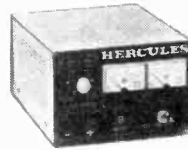
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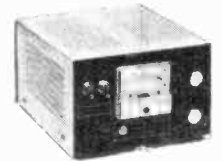
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- ★ **£65.00**



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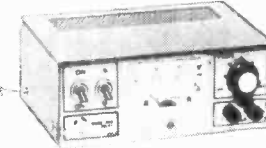
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- ★ 6-14V @ 2.5A.
  - ★ Ripple, less than 3mV.
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  - ★ Short-circuit protection.
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### P.G. 77

- ★ 3-15V @ 2.5A maximum (80% duty cycle).
  - ★ Ripple, less than 10mV.
  - ★ Stability, 0.1%.
  - ★ Short-circuit protection
- ★ **£29.50**



### P.G. 116

- ★ 12.6V @ 2A
  - ★ Ripple, less than 2mV
  - ★ Stability, 1%.
  - ★ Short-circuit protection.
- ★ **£15.95**

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- ★ Output: Sine-wave, 0-10V r.m.s. from 600.
- ★ Square-wave 0-20V p.p. from 600
- ★ 0-60 dB step attenuator.

★ **£95.00**

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- ★ Frequency: 1Hz to 1.1 MHz.
- ★ Sine, square and triangle.
- ★ 5V from 0-60 dB 50 attenuator.
- ★ Also simultaneously 10V from three independent 600 outputs
- ★ D.C. offset.

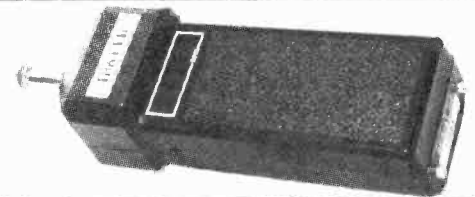
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- ★ 5 digits
- ★ Optional wheels for linear speed-ft/sec or decimetres

Complete with leather carrying case

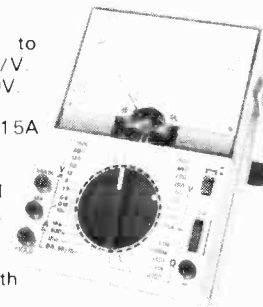
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Features 38 colour-coded ranges with high input impedance

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- ★ D.C. Current, 10μA to 15A f.s.d.
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- ★ Mirror-scale, rugged taut-band suspension, dB scale, diode and fuse protection.
- ★ Supplied complete with test leads and leather carrying-case.

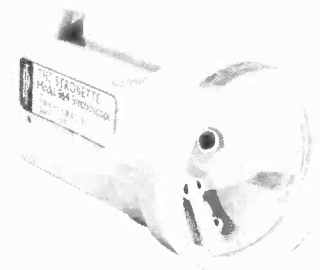


★ **£39.50**

### "STROBETTE" STROBOSCOPE TACHOMETER MODEL 964

- ★ 200-6000 flashes/minute
- ★ Directly calibrated in r.p.m.
- ★ Xenon lamp

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Part of our wide range of "strosbes and tachos"

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WW-107 FOR FURTHER DETAILS

## FREQUENCY COUNTERS

1/10 Hz to 1.2GHz

High performance instruments measuring frequency, period, time, freq./ratio and calibrated output facility. Fast delivery. Specials by arrangement.



TYPE 801B

CRYSTAL OVEN  
OPERATING MANUAL  
TWO TONE BLUE CASE

£280 250 MHz

Sensitivity 10mV. Stability 5 parts 10.<sup>10</sup>

Resolution ± 1 Count

301M	32MHz 5 Digit	£98	401A	32MHz 6 Digit	£135
501	32MHz 8 Digit	£192	701A	80MHz 8 Digit	£210
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SUPPLIERS TO: Ministry of Defence, G.P.O., B.B.C., Government Depts., Crystal  
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**R.C.S. ELECTRONICS**

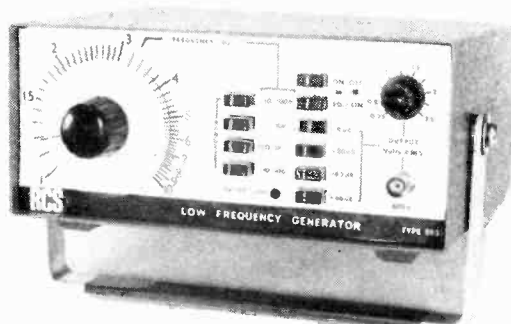
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Telephone: Ashford (Code 69)  
53661/2

WW-085 FOR FURTHER DETAILS

## NEW PRODUCT

PRECISION LOW FREQUENCY  
GENERATOR

SINE AND SQUARE WAVE



TYPE 203

£78

Excl. VAT

### FEATURING

- |                      |   |
|----------------------|---|
| WIDE FREQUENCY RANGE | 10 Hz to 100 KHz IN 4 RANGES                              |
| SINE OUTPUT          | MAX. T.H.D. 0.3%  |
|                      | AMPLITUDE LEVEL TO WITHIN .1% OVER ENTIRE FREQUENCY RANGE |
|                      | MAX. RISE TIME 20 nS                                      |
| SQUARE OUTPUT        | 2.5V R.M.S. SINE AND SQUARE                               |
| OUTPUT LEVEL         | 80 dB RANGE   |
| ATTENUATOR           | 2 PP9s OR OPTIONAL MAINS POWER UNIT                       |
| POWER                | (£12 EXTRA)   |



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## TELECOMMUNICATIONS ANTENNAS

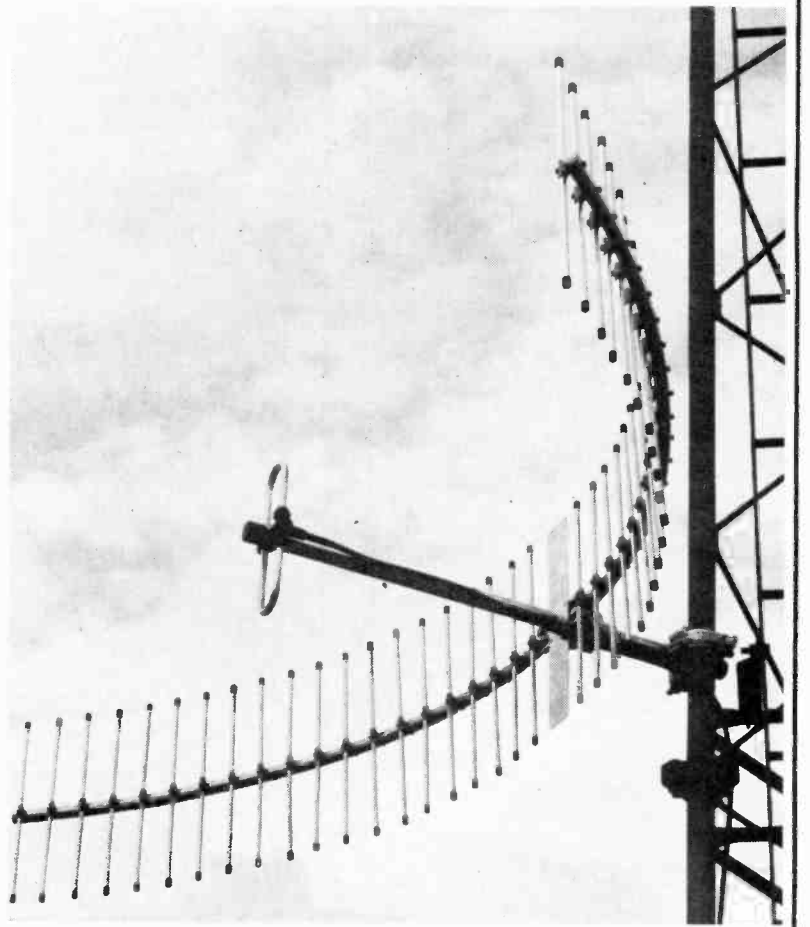
The PU900 is a fixed station broadband antenna with a gain of 15dB over a dipole, front to back ratio average 20dB. In the lower part of the band from 400-700MHz the bandwidth is 150MHz and from 700 to 1500MHz it is 250MHz with a VSWR better than 1.5-1.0 with reference to 50 ohms. The antenna can be operated in either the horizontal or vertical mode.

We not only design and manufacture antennas, but also a wide range of structures, both guyed and self-supporting towers. This enables us to offer a complete package to customers.

You will find our prices are very competitive, and our deliveries are exceptionally fast, including overseas shipments.

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WW-102 FOR FURTHER DETAILS

# NEW PRODUCTS FROM ITA

Here are just some of the products stocked by THE UK's BIGGEST EQUIPMENT CENTRE, ITA:—

**Revox Teac  
 Otari  
 Itam Quad H & H**

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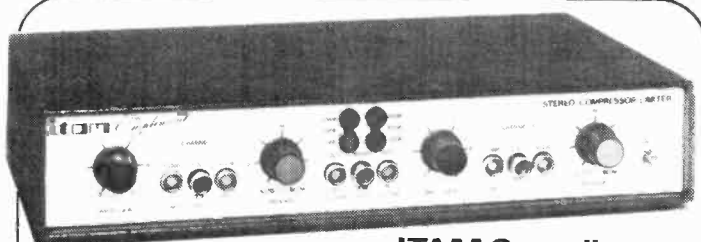


1-7 Harewood Avenue, Marylebone Road  
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**ORBAN PARASOUND from USA**

Dual channel multispring reverb unit. Each channel features four springs — far smoother than single spring systems. "Twang" and "boing" are virtually eliminated by incorporating a floating threshold limiter. Bass, mid-range EQ and bandwidth controls. The best compact reverb unit available.



**ITAM Compliment**

New Stereo compressor limiter. Competitively priced. Free standing self-contained unit, accurate stereo tracking, stepped 1:1, 1:5, 3:1 plus limiting ratio at 20:1. Switchable attack time, variable release time, automatic release time. Input attenuation to accommodate large range of inputs. Pre-set adjustable output. Switched link for stereo tracking. Visual representation of compression. £247 + VAT

WW-112 FOR FURTHER DETAILS

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Registered in England 1179820

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- Pressac Pins, part No's 11/3125 & 11/1893, available in large qty. Phone for details.
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- Telescopic Aerials, 2' 0" chrome swivel **25p**.  
2' 6" chrome swivel **30p**.
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- Erie Can Electrolytic 500 + 50 $\mu$ F 200v D.C. **25p**.
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32 way .15" **40p**.  
40 way .1" BICC Burndy **50p**.
- Microswitches, various styles, i.e. lever pip roller, etc. Callers only (a fraction of the normal price).
- We have very large stocks of** ★  
★ **Ceramics and Polystyrenes in stock, average 1000 off. Price £10/1000. For low values, phone for details. Last stock count 2 million PCS plus.** ★
- ★ **Metal Oxide Resistors by Elettrosil & Welwyn. Last stock count 2½ million pcs. plus. Phone for prices & availability, etc.** ★
- Transformer 18v 2½ amp primary 240v **£1.60**. Size 3" x 1" x 2½".
- Miniature Mains Transformer PRI 240v SEC 12v 100mA. Manuf. Hinchley. Size 36 x 45 x 40mm. Price 1—**65p**, 100—**60p ea.**, 1000—**50p**, 10,000—**35p**.
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- Piher Presets Type PT15 ex-stock. 200,000 pcs. various values, horizontal & vertical, **£20/1000**.
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- 1K $\Omega$  Pot by Egen. Price **£60/1000**.
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100mF 10v Radial **£20/1000**.  
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400mf 30v Axial **£40/1000**.  
470mf 25v Axial **£30/1000**.  
100mf 25v Axial **£80/1000**.  
1000mf 63v Axial **£90/1000**.  
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1 $\mu$ F Polyester 600v Axial **£90/1000**.  
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- Belling Lee Panel Fuseholder, 1¼ size, **£25/100, £20/1000**.
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# 15 — 240 Watts!

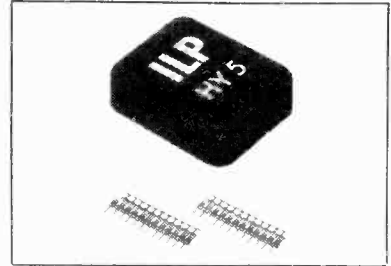
## HY5 Preamplifier

The HY5 is a mono hybrid amplifier ideally suited for all applications. All common input functions (mag Cartridge, tuner, etc.) are catered for internally, the desired function is achieved either by a multi-way switch or direct connection to the appropriate pins. The internal volume and tone circuits merely require connecting to external potentiometers (not included). The HY5 is compatible with all I.L.P. power amplifiers and power supplies. To ease construction and mounting a P.C. connector is supplied with each pre-amplifier.

**FEATURES:** Complete pre-amplifier in single pack — Multi-function equalization — Low noise — Low distortion — High overload — two simply combined for stereo

**APPLICATIONS:** Hi-Fi — Mixers — Disco — Guitar and Organ — Public address

**SPECIFICATIONS:**  
**INPUTS:** Magnetic Pick-up 3mV, Ceramic Pick-up 30mV, Tuner 100mV, Microphone 10mV, Auxiliary 3-100mV, input impedance 47k $\Omega$  at 1kHz  
**OUTPUTS:** Tape 100mV, Main output 500mV R.M.S.  
**ACTIVE TONE CONTROLS:** Treble  $\pm$  12dB at 10kHz, Bass  $\pm$  at 100Hz  
**DISTORTION:** 0.1% at 1kHz, Signal/Noise Ratio 68dB  
**OVERLOAD:** 3dB on Magnetic Pick-up, **SUPPLY VOLTAGE:**  $\pm$  16-50V  
**Price £5.22 + 65p VAT P&P free**  
 HY5 mounting board B1 48p + 6p VAT P&P free



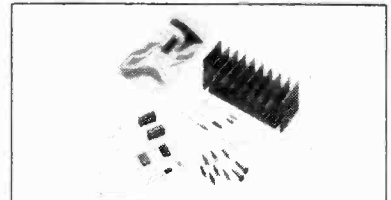
## HY30 15 Watts into 8 $\Omega$

The HY30 is an exciting New kit from I.L.P., it features a virtually indestructible I.C. with short circuit and thermal protection. The kit consists of I.C., heatsink, P.C. board, 4 resistors, 6 capacitors, mounting kit, together with easy to follow construction and operating instructions. This amplifier is ideally suited to the beginner in audio who wishes to use the most up-to-date technology available.

**FEATURES:** Complete kit — Low Distortion — Short, Open and Thermal Protection — Easy to Build

**APPLICATIONS:** Updating audio equipment — Guitar practice amplifier — Test amplifier — Audio oscillator

**SPECIFICATIONS:**  
**OUTPUT POWER:** 15W R.M.S. into 8 $\Omega$ , **DISTORTION:** 0.1% at 15W  
**INPUT SENSITIVITY:** 500mV, **FREQUENCY RESPONSE:** 10Hz-16kHz — 3dB  
**SUPPLY VOLTAGE:**  $\pm$  18V  
**Price £5.22 + 65p VAT P&P free.**



## HY50 25 Watts into 8 $\Omega$

The HY50 leads I.L.P.'s total integration approach to power amplifier design. The amplifier features an integral heatsink together with the simplicity of no external components. During the past three years the amplifier has been refined to the extent that it must be one of the most reliable and robust High Fidelity modules in the World.

**FEATURES:** Low Distortion — Integral Heatsink — Only five connections — 7 Amp output transistors — No external components

**APPLICATIONS:** Medium Power Hi-Fi systems — Low power disco — Guitar amplifier

**SPECIFICATIONS:** **INPUT SENSITIVITY:** 500mV  
**OUTPUT POWER:** 25W RMS in 8 $\Omega$ , **LOAD IMPEDANCE:** 4-16 $\Omega$ , **DISTORTION:** 0.04% at 25W at 1kHz  
**SIGNAL/NOISE RATIO:** 75dB, **FREQUENCY RESPONSE:** 10Hz-45kHz — 3dB  
**SUPPLY VOLTAGE:**  $\pm$  25V, **SIZE:** 105 50 25mm  
**Price £6.82 + 85p VAT P&P free**



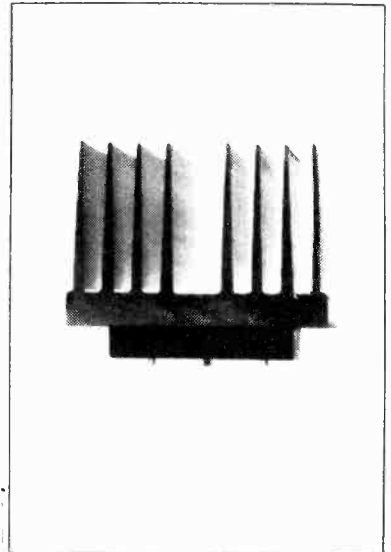
## HY120 60 Watts into 8 $\Omega$

The HY120 is the baby of I.L.P.'s new high power range, designed to meet the most exacting requirements including load line and thermal protection, this amplifier sets a new standard in modular design.

**FEATURES:** Very low distortion — Integral Heatsink — Load line protection — Thermal protection — Five connections — No external components

**APPLICATIONS:** Hi-Fi — High quality disco — Public address — Monitor amplifier — Guitar and organ

**SPECIFICATIONS:** **INPUT SENSITIVITY:** 500mV  
**OUTPUT POWER:** 60W RMS into 8 $\Omega$ , **LOAD IMPEDANCE:** 4-16 $\Omega$ , **DISTORTION:** 0.04% at 60W at 1 kHz  
**SIGNAL/NOISE RATIO:** 90dB, **FREQUENCY RESPONSE:** 10Hz-45kHz — 3dB, **SUPPLY VOLTAGE:**  $\pm$  35V  
**Size:** 114 x 50 x 85mm  
**Price £15.84 + £1.27 VAT P&P free.**



## HY200 120 Watts into 8 $\Omega$

The HY200, now improved to give an output of 120 Watts, has been designed to stand the most rugged conditions, such as disco or group while still retaining true Hi-Fi performance.

**FEATURES:** Thermal shutdown — Very low distortion — Load line protection — Integral Heatsink — No external components

**APPLICATIONS:** Hi-Fi — Disco — Monitor — Power Slave — Industrial — Public address.

**SPECIFICATIONS:** **INPUT SENSITIVITY:** 500mV  
**OUTPUT POWER:** 120W RMS into 8 $\Omega$ , **LOAD IMPEDANCE:** 4-16 $\Omega$ , **DISTORTION:** 0.05% at 100W at 1kHz  
**SIGNAL/NOISE RATIO:** 96dB, **FREQUENCY RESPONSE:** 10Hz-45kHz — 3dB, **SUPPLY VOLTAGE:**  $\pm$  45V  
**SIZE:** 114 x 100 x 85mm  
**Price £23.32 + £1.87 VAT P&P free.**

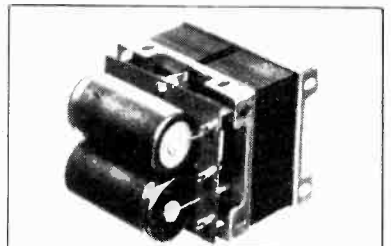
## HY400 240 Watts into 4 $\Omega$

The HY400 is I.L.P.'s "Big Daddy" of the range producing 240W into 4 $\Omega$ ! It has been designed for high power disco or public address applications. If the amplifier is to be used at continuous high power levels a cooling fan is recommended. The amplifier includes all the qualities of the rest of the family to lead the market as a true high power hi-fidelity power module.

**FEATURES:** Thermal shutdown — Very low distortion — Load line protection — No external components

**APPLICATIONS:** Public address — Disco — Power Slave — Industrial

**SPECIFICATIONS:** **OUTPUT POWER:** 240W RMS into 4 $\Omega$ , **LOAD IMPEDANCE:** 4-16 $\Omega$ , **DISTORTION:** 0.1% at 240W at 1 kHz  
**SIGNAL/NOISE RATIO:** 94dB, **FREQUENCY RESPONSE:** 10Hz-45kHz — 3dB, **SUPPLY VOLTAGE:**  $\pm$  45V  
**INPUT SENSITIVITY:** 500mV, **SIZE:** 114 x 100 x 85mm  
**Price £32.17 + £2.57 VAT P&P free.**



### POWER SUPPLIES

PSU36 suitable for two HY30 s £5.22 plus 65p VAT P/P free  
 PSU50 suitable for two HY50 s £6.82 plus 85p VAT P/P free  
 PSU70 suitable for 2 HY120 s £13.75 plus £1.10 VAT P/P free  
 PSU90 suitable for one HY200 £12.65 plus £1.01 VAT P/P free  
 PSU180 suitable for two HY2000 s or one HY400 £23.10 plus £1.85 VAT P/P free  
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# THE DYNAMIC DUO



The C15/15 is a unique Power Amplifier providing Stereo 15 watts per channel or 30 watts Mono and can be used with any car radio/tape unit. It is simply wired in series with the existing speaker leads and in conjunction with our speakers S15 produces a system of incredible performance.

A novel feature is that the amplifier is automatically switched on or off by sensing the power line of the radio/tape unit hence alleviating the need for an on/off switch.

The amplifier is sealed into an integral heatsink and is terminated by screw connectors making installation a very easy process.

The S15 has been specially designed for car use and produces performance equal to domestic speakers yet retaining high power handling and compact size.

**C15/15**  
 15 Watts per channel into 4Ω  
 Distortion 0.2% at 1KHz at 15 watts  
 Frequency response 50Hz - 30KHz  
 Input Impedance 8Ω nominal  
 Input sensitivity 2 volts R.M.S. for 15 watts output  
 Power line 10 - 18 volts  
 Open and Short circuit protection  
 Thermal protection  
 Size 4 × 4 × 1 inches

**Data on S15**  
 6" Diameter  
 5 1/4" Air Suspension  
 2" Active Tweeter  
 20oz Ceramic magnet  
 15 Watts R.M.S. handling  
 50 Hz - 15KHz frequency response  
 4Ω Impedance

C15/15 Price £17.74 + £2.21 VAT P & P free

S15 Price per pair £17.74 + £2.21 VAT P & P free

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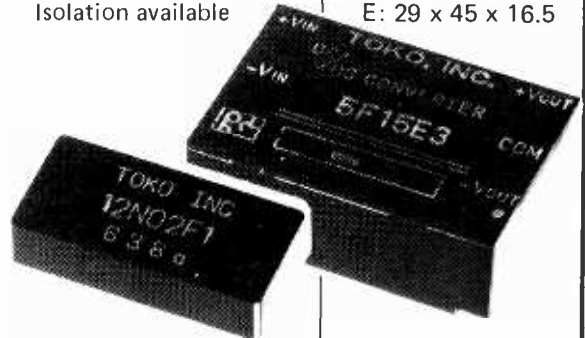
FROM THE WORLD'S LARGEST MANUFACTURER OF QUALITY WOUND COMPONENTS  
A COMPLETE RANGE OF VERY COMPETITIVELY PRICED

# DC-DC CONVERTERS



Quick reference table of TOKO DC-DC converter modules:

Input Voltage V in (V)	Output Voltage V out (V)	Rated Output Po (mW)	Input/Output Isolation	Dimensions (mm)
+5±10%	+6, +9, +12 +15, +20, +24	250, 500, 1000	F, M & K series Not available	F: 17 x 35 x 8 M: 17 x 32.5 x 10 K: 17 x 32.5 x 12
	-5, -6, -9, -12, -15, -20	250, 500, 1000.		
	±6, ±9, ±12, ±15, ±20	250, 500, 1000.		
	+12 or -12 +15 or -15 +24 or -24	1,500	E series Isolation available	
+12±20%	+5 or -5 +15 or -15 ±12 or ±15	1,500 1,500		E: 29 x 45 x 16.5
	+5 or -5 +12 or -12 +15 or -15	1,500 1,500		
+24±20%	+5 or -5 +12 or -12 +15 or -15	1,500 1,500		
	±12, ±15	1,500		



TOKO (UK) Ltd., Ward Royal Parade, Alma Road, Windsor, Berkshire. Windsor (07535) 54057

WW-096 FOR FURTHER DETAILS

## MARCONI TEST EQUIPMENT

- TF329G circuit magnification meter **£125**
- TF455E Wave analyser. New. **£135**
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- TF1099 20MHz sweep generators
- TF1041B & C. VT Voltmeters
- TF1102 Amplitude modulator. 500MHz
- TF1020A Power meter. 100W. 250MHz. **£85**
- TF1152A/1 Power meter. 25W. 500MHz. **£75**
- TF890A/1 RF test set. **£425**
- TF801B/3S Signal generator. **£175**
- TF1417 200MHz counter (imperfect).
- TF1400 Pulse generator
- TF675F Pulse generator
- TF1370 Wide-range RC oscillator **£125**
- TF2163 UHF attenuator DC-1GHz. **£95**
- TF2200 Oscilloscope
- TF2904 Colour gain delay test set
- TF1058 UHF/SHF signal generator

ALL EQUIPMENT IS AVAILABLE FOR HIRE AT VERY REASONABLE RATES. PLEASE TELEPHONE YOUR REQUIREMENTS.

**POLARAD TYPE TSA. SPECTRUM ANALYSER.** C/w type STU/2M plug-in unit covering from 950 to 4500 MHz.

**EVER-READY NICKEL-CADMIUM BATTERIES.**  
Size 'D' (HP2) 1.25V, 3.5 AH. Only small quantity available at **£2 + 10p** post.

**APT POWER SUPPLIES.** Stabilised and regulated. 6V (variable) at 3A. Brand new **£25.**

**BECKMAN TURNS COUNTER DIALS**  
Miniature type (22mm diam.) Counting up to 15 turn 'Helipot's'. Brand new with mounting instructions Only **£2.50 each**

**Wandel & Gottman Equipment**  
Level Meter 0.2-1600KHz  
Level Oscillator 0.2-1600KHz  
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Carrier Frequency Level Meter

## P. F. RALFE ELECTRONICS

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TEL: 01-723 8753

### TEST EQUIPMENT

- ADVANCE SG62B signal gen. 150KHz-220MHz **£65**
- AIRMEC 399 Video oscillator 15Hz-15MHz **£70**
- AIRMEC 254 High-power oscillator/amplifier
- BOONTON 80 Signal generator. 2-400MHz. **£105**
- BOONTON 230A RF Power Amplifier **£325**
- BPL Capacitance decade (5) CD133. 100pf-1uF **£45**
- GERTSCH Frequency meter and deviation meter 20-1000MHz **£250**
- GR Standard sweep generator. 400KHz-230MHz. **£485**
- HEWLETT PACKARD 693D sweep oscillator **£350**
- HEWLETT PACKARD 432A Power meter
- DERRITRON Digital Wheatstone Bridge **£110**
- MUIRHEAD K-134-A Battery op wave analyser
- PYE EHT scalamp voltmeter 0-40KV **£125**



- RADIO CORPUS PB1 pulse & bar generator **£45**
- SIEMENS Level oscillator 12-160KHz
- SCHNEIDER type cf252 100MHz counter (red) **£200**
- SCHOMANDL type FD1 frequency meter **£125**
- SOLARTRON type CD1212 oscilloscope **£145**
- Bruel & Kjoer type 3301 Automatic Frequency Response Recorder 200Hz-20KHz
- Airmec 201A Signal Generator 30KHz-30MHz.
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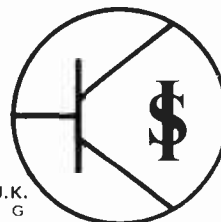
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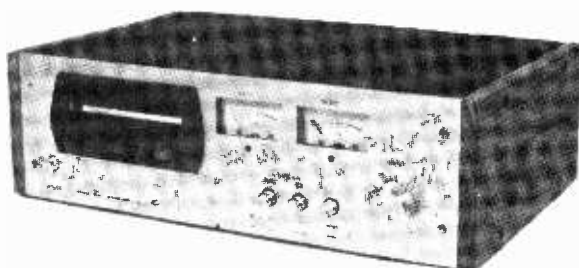
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The successful Engineer will be involved in the detailed planning of the systems and be responsible to the Telecomms. Engineering Manager for the guidance and co-ordination of the planning group. Age is likely to be mid-thirties and membership of an appropriate professional body is expected.

### Planning Engineers

– Radio & Line  
– up to £6,000

These appointments require relevant experience in systems design and planning, field surveys, report writing and path performance estimates. A knowledge of telecomms. power supplies would be a distinct advantage. Age is likely to be late 20s or early thirties and a suitable qualification is expected.

### Planning Engineers

– Data & Telegraphy  
– up to £6,000

The Engineers appointed to these roles will be experienced in the planning, specifying and procurement monitoring of modern telegraph and data facilities such as teleprinters, telex, modems, networks, switching and multiplexing equipment. Age is likely to be late 20s, early thirties, and a suitable qualification is expected.

All these posts may engage the engineers in some limited overseas travel. In addition to the salary, the company provides a number of worthwhile benefits including generous relocation expenses and pension scheme. Attractive long term prospects exist in this progressive and expanding company.

If you want to be considered for these interesting roles then telephone our Engineering Manager for a brief discussion or write with full personal/career details, quoting ref: 407 to John Callow, International Aeradio Limited, Aeradio House, Hayes Road, Southall, Middlesex.

Telephone 01-571 0678 or 01-572 9894

CITY OF LONDON POLYTECHNIC  
DEPARTMENT OF MODERN  
LANGUAGES

### TECHNICIAN GRADE 4

SALARY in the range of £3,024-£3,405 including London Weighting plus Pay Supplement £151 minimum – £208 maximum.

The Modern Languages Department requires for its language laboratories a Technician to be responsible for the maintenance, servicing and setting up of the wide range of equipment used.

Ability to catalogue and organise the loan of cassettes and tapes is desirable. Some knowledge of French or German or Spanish would be an advantage.

For further details and application form please apply in writing to The Assistant Secretary, City of London Polytechnic, 117/119 Houndsditch, London EC3A 7BU, as soon as possible (7598)

## TECHNICAL SALES REPRESENTATIVE

required by long established Radio and Electronic Component Makers dealing direct with manufacturers. The successful applicant should live in the Greater London area preferably north of the Thames and following a period of product familiarisation will be required to operate a large well established area.

This is a permanent position with excellent prospects and a contributory pension scheme. A company car would be provided. Applicants between 25/35 years of age should write, stating age, education and previous experience to – Wingrove and Rogers Limited, Domville Road, Liverpool L13 4AT.

(7619)

LUXMAN DISTRIBUTORS

Require an additional

## HI-FI ENGINEER

Must be experienced and capable of servicing high quality equipment. Good prospects.

Apply **Sales Manager,**  
**HOWLAND-WEST LTD.**  
3/5 Eden Grove  
London N7 8EQ  
Tel: 01-609 0293

7642

# DESIGN/DEVELOPMENT ENGINEERS

**Ferranti wins Army contract.**

**Ferranti land space order.**

**1200 MORE JOBS FOR FERRANTI EXPANSION**

**MoD order goes to Ferranti.**

## Come and make headlines with us.

Headlines like these are only possible when you're acknowledged internationally as one of the world's leaders in avionics. To keep us at the forefront we need highly motivated design/development engineers keen to make their mark. And at Ferranti there's plenty of opportunity to do just that. On projects like the Tornado, Sea Harrier, Jaguar and Lynx.

And headlines like these also mean expansion. Which explains why we're looking for more graduate mechanical and electronic engineers to join our airborne radar and inertial navigation teams. They must have the design/development experience to spearhead the progress of equipment from drawing board through to production.

We are particularly interested in talking to engineers with backgrounds in the design of:-

**Digital/analogue circuitry.**

**Microwave and laser techniques.**

**Small digital computers.**

**Advanced instruments.**

**Optics.**

**Airborne structures and light mechanisms.**

So if you're keen to make your mark on avionics, you'll find you're very much on our wavelength.

Think about it. Then ask the family how they'd like living in Edinburgh, freely acknowledged as one of Europe's finest cities.

Salaries are negotiable and, of course, we operate a contributory pension and life assurance scheme and pay realistic relocation expenses.

For an application form, write to John McPhee at the address below:

**Ferranti Limited  
Ferry Road  
EDINBURGH EH5 2XS  
Tel: 031-332 2411.**

These posts are open to both male and female candidates.

(7000)

**FERRANTI**

## Land a good job

Your  
Radio Officer's  
qualifications  
can mean a lot  
here on shore

If you're thinking of a shore-based job, here's where you'll find interesting work, job security, good money, and the opportunity to enjoy all the comforts of home where you appreciate them most — at home!

The Post Office Maritime Service has vacancies at Portishead Radio and some of its other coast stations for qualified Radio Officers to undertake a wide variety of duties, from Morse and teleprinter operating to traffic circulation and radio telephone operating.

To apply, you must have a United Kingdom Maritime Radio Communication Operator's General Certificate or First Class Certificate of Proficiency in Radio-telegraphy or an equivalent certificate issued by a

Commonwealth Administration or the Irish Republic. And, ideally, you should have some sea-going experience.

The starting pay at 25 or over works out at around £4093; after three years' service this figure rises to around £5093. (If you are between 19 and 24 your pay on entry will vary between approximately £3222 and £3732). Overtime is additional, and there is a good pension scheme, sick-pay benefits, at least 4 weeks' holiday a year, and excellent prospects of promotion to senior management.

For further information, please telephone Andree Trionfi on 01-432 4869 or write to her at the following address: ETE Maritime Radio Services Division (L690), ET 17.1.2, Room 643, Union House, St. Martins-le-Grand, London EC1A 1AR.

Post Office Telecommunications



## Electronic Test Engineers

We manufacture and market professional audio noise reduction equipment which is widely used by major recording companies, recording studios and broadcasting authorities throughout the world and have enjoyed successful growth since incorporation in 1968.

Because of continuing expansion we need to recruit a number of experienced Test Engineers who will be responsible for testing, calibrating and trouble-shooting our sophisticated professional audio electronic equipment.

The successful candidates, probably with degrees or HNC's, will have practical knowledge and experience of electronic testing and must enjoy the challenge of quality and delivery pressures.

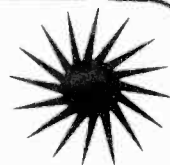
Excellent pay and conditions.



Write or telephone:  
Dan Bleakley  
Dolby Laboratories  
346 Clapham Road  
London SW9. 01-720 1111

7055

## REDIFFUSION



## TEST EQUIPMENT MAINTENANCE ENGINEER

Due to impending retirement, a vacancy has arisen for an experienced engineer to be responsible for the maintenance and calibration of general electronic test equipment used in our research laboratories at Kingston-upon-Thames. This equipment is mostly commercially manufactured but includes some specialized instruments designed for applications associated with cable television distribution systems.

Applicants must have a sound engineering background with previous experience in electrical maintenance work and be qualified to H.N.C. or equivalent level.

A good salary with excellent working conditions will be offered to the successful applicant.

Apply to:

**I. R. Budgen**  
**Head of Test Section**  
**Rediffusion Engineering Limited**  
**187 Coombe Lane West**  
**Kingston-upon-Thames**  
**Surrey KT2 7DJ. Tel. 942 8900**

(7603)



## H. F. Instrument Development

A mature imaginative

### ENGINEER

is required to expand our development activities in high frequency instrumentation.

Our present product line includes automatic modulation meters, frequency synthesisers, scanning receivers, etc. Applicants should have experience or an interest in this type of instrumentation.

A top salary, with other benefits are offered, with eventual progression to board level management.

Applicants should apply in writing, giving brief career history.

**SAYROSA ENGINEERS LTD.**  
Wey River House  
Alton, Hampshire  
Alton 84500

(7570)

## TELEVISION ENGINEER

A vacancy occurs with an old establishment Retailer.

The Post requires someone with a wide range of experience in Television and Audio equipment, a clean driving licence is essential. Large flat available for suitable applicant.

**HYDES OF CHERTSEY LTD.**  
56/60 Guildford Street, Chertsey  
Telephone: Chertsey 63243

(7650)

## CLIVEDEN CONSULTANTS

### CHIEF TEST ENGINEER

up to c £5250

### SENIOR TEST ENGINEERS

up to £4200 + O.T.

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£ neg. + O.T.

For interesting work on computer peripherals and advanced electronic instruments. W. Middx., Surrey, Berks.

Contact R. Howard, C.Eng., Maidenhead (0628) 29709 (7594)

# Engineer Programmers - A Company that will keep you interested

Exciting things are happening to this country's telephone network and STC is, as ever, at the forefront. As leaders in our field we are continually pushing forward the boundaries of electronic switching technology.

Test programming plays a vital part in the on-going development of our systems. The job involves preparing test programs using a high level language and deriving test-generation techniques to control the testing of PCB assemblies on ATE. An experienced Engineer (male or female) will advise designers on the 'testability' of their designs.

If you have a background in testing, fault-finding, commissioning or a similar field using modern electronic techniques, we will broaden your experience. And remember, a Company like ours is big enough to KEEP YOU INTERESTED.

For further information telephone Mike Batsch on 01-235 7030 Ext. 233 or write to

*Mike Randal, Electronic Switching Products Division,  
Standard Telephones and Cables Ltd.,  
Oakleigh Road South,  
New Southgate, London N11 1HB.*

## Standard Telephones and Cables Limited

A British Company of ITT

(7574)

## The Polytechnic of North London

### ELECTRONICS TECHNICIAN

We are looking for a well-qualified electronics technician with a keen interest in video, audio and audio-visual. As a member of the Educational Development Service, the technician would be responsible for:

- \*establishing servicing routines and records
- \*establishing technical standards and assisting production staff in video and audio recordings
- \*training and supervising technical staff
- \*developing and building ancillary equipment

HNC or equivalent qualification required and minimum of nine years' relevant experience.

Salary scale: £3621-£4227 (including London Weighting) plus 5% earnings supplement (minimum £2.50 per week, maximum £4 per week).

Application form from Educational Development Service, Polytechnic of North London, Holloway Road, N7 8DB.

7571

## DEVON AREA HEALTH AUTHORITY Exeter Health Care District

**ROYAL DEVON AND  
EXETER HOSPITAL (WONFORD)**  
Barrack Road, Exeter EX2 5DW

### MEDICAL PHYSICS TECHNICIAN IV

(Salary: £2346-£3267 p.a. plus phase 1 & 2 pay supplements)

Required for general duties in the Physics Department concerned with Radiotherapy, Radioactive Isotopes, Radiation Protection and Instrumentation.

Further information obtainable from the Principal Physicist, Mr. C. F. Walker, tel: Exeter (0392) 77833 ext. 2262.

Application form and job description obtainable from the Personnel Officer, Royal Devon and Exeter Hospital (Wonford), Barrack Road, Exeter EX2 5DW.

(7624)

## REPAIR/ CALIBRATION ENGINEERS

**C****S****L**

We are looking for additional Repair/Calibration Engineers for servicing and calibrating electronic test equipment in our Repair Laboratories.

We welcome DVM, Oscilloscope and RF specialists together with others having a broader background. We would also welcome Engineers with more limited experience who wish to improve their knowledge to cover some of the other equipment that we handle.

We offer salaries in range £3,300 to £4,000 according to grade, with overtime, service awards and profit sharing bonuses in addition. Our working conditions are very good and our staff enjoy the benefit of the friendly atmosphere of a small company.

We are one of the leading repair and calibration companies. We have a B.C.S. Approved Standards Laboratory, hold Ministry Approvals to DEF.STAN. 05/24 and 05/26, and are also Defence Contract and CAA listed.

Having told you about ourselves, why not contact us and discuss where you could fit into our Company.

For more details and application form, write or telephone:

**Technical Manager**  
**CALIBRATION SYSTEMS LIMITED**  
Blackwater Station Estate, Camberley, Surrey  
Telephone Camberley 33922 (7635)

## Closed Circuit Television

### (Video Workshop)

## Engineer

### £3349 - £4910

#### Garnett House

Downshire House, Roehampton Lane SW15 4HR

Applications are invited for this post at Garnett College which trains qualified mature students for teaching careers in Further and Higher Education. Duties will include maintenance of television equipment in use throughout the college, production work and participation in training. Applicants should be qualified and experienced in the use and maintenance of CCTV equipment.

Excellent conditions of employment. Starting salary will be dependent on qualifications and experience. Salary includes London Weighting and pay supplements for 1976 and 1977.

For further details and application forms contact the Chief Technician at the College. Tel. 01-789 6533.

**GLC Mechanical  
& Electrical Engineering** (7652)



## REDIFFUSION REDITUNE LIMITED

the world's leading music service, require the following staff:

### STUDIO MAINTENANCE SUPERVISOR

This position involves the technical and administrative control of a small team of qualified technicians responsible for the maintenance of dubbing and high speed duplicating equipment. A thorough knowledge of studio equipment and techniques, and previous experience of the control of technical staff, is essential.

### STUDIO MAINTENANCE ENGINEER

The successful candidate will carry out maintenance of dubbing and high speed tape duplicating equipment and associated ancillary equipment. A thorough knowledge of studio equipment and two years' experience in a similar capacity is essential. Candidates with academic qualifications to ONC level will be preferred.

### SERVICE WORKSHOPS SUPERVISOR

To assume technical and administrative control of a base workshops concerned with trouble-shooting, repair, and maintenance of tape players and associated public address equipment. A thorough knowledge of audio equipment and previous experience of the control of technical staff is essential.

### SERVICE TECHNICIAN

For trouble-shooting and repair of tape players and associated audio equipment. Some previous experience is essential and on the job training would be given to suitable candidates.

Please apply stating age, qualifications, and previous experience to:

**Chief Engineer**  
**Rediffusion Reditune Ltd.**  
Cray Avenue  
Orpington  
Kent BR5 3QP

(7643)

**MEDICAL PHYSICS  
TECHNICIAN  
GRADE IV**

A vacancy exists in the Electronics Section of the Department of Medical Physics. The work involves the development and manufacture of a wide range of medical and research instruments, using both digital and analogue integrated circuit techniques.

Appointment will be to Medical Physics Technician Scale IV, Scale £3,162-£4,130 (inclusive of all allowances). Minimum qualifications are ONC or equivalent with recognised practical training.

For further details of the post contact Mr D. Ritchie, Chief Technician, Department of Medical Physics, St. George's Hospital SW17 (672-1255 ext. 4058).

Formal application and request for job descriptions should be made to: Miss H. Forsyth, Personnel Department, St. George's Hospital, Blackshaw Road SW17. (7577)

**ROYAL FREE HOSPITAL**

**MEDICAL PHYSICS  
TECHNICIAN  
GRADE III**

required to maintain a range of Radiotherapy and diagnostic equipment, principally a newly installed SL 75 Linear Accelerator, but including a computer-controlled cobalt unit to be installed shortly, dosimeters, etc. Applicants must hold an appropriate science degree HNC/HND, ONC or Final City and Guilds in electronics subjects and have had at least three years' experience preferably in maintenance work.

Salary £3,776 - £4,708 p.a. (including all allowances and according to experience). Application form from Personnel Department, Royal Free Hospital, 21 Pond Street, London, NW3 2PN. Telephone: 01-794 0431. Quote Ref. 1498.

**ELECTRONIC  
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To design equipment for use of the physically handicapped. Knowledge/interest in digital systems, communications, computers, microprocessors preferred. Interesting range of work with small Company in pleasant location.

**GRANGE ELECTRONICS LTD**  
Stone Lane, Wimborne  
Dorset 7629

**CAPITAL APPTS.** **FREE LISTS**  
101 Design/Development and Test Jobs.  
Permanent and Contract  
**To £6,000**  
(7641)  
**637 5551**

30 Windmill St. London, W.1

**TELEVISION BROADCAST** Engineers and Operators. The Rank Video Centre is a major television facilities company providing a wide range of services to broadcasters, advertisers and industry. The Video Centre has vacancies for operational engineers to work in Central London on advanced technology broadcast equipment. Applicants should have broadcast engineering experience in quadruplex videotape recording and telecine. A working knowledge of Ampex AVRI's, RCA TR70C's and CMX time code editing systems would be an advantage. Operational flair is most important. Salary range: £4,043 to £5,755 (under review) according to experience. Please contact: Gary McJannett, Operations Manager, Rank Video Centre, 142 Wardour Street, London, W1V 4BU. Telephone No: 01-734 2235. (7608)

**VERY EXPERIENCED** Electronic Engineer for electronic keyboard and amplification service. Salary negotiable. Phone Maurice Placquet 01-749 3232. (7614)

**Test Technicians**

Do you ever get that feeling .....

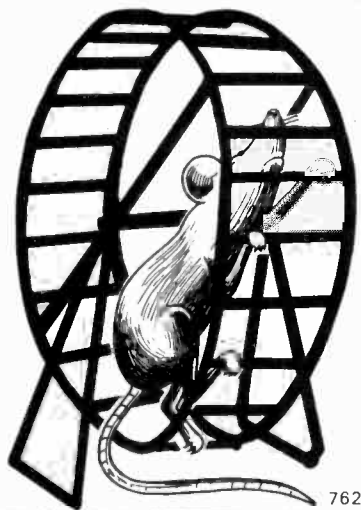
Then why not earn up to £5,000pa with a company who can offer bags of opportunity for promotion and a variety of work?

Can you test/repair digital equipment-VDU's-MINI's-INTERFACES etc?

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Engineering and Technical Recruitment TELEPHONE: 01-229 9239



7622

**Electronics  
Engineers**

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influence in high places

## LINK



## OPPORTUNITIES IN TELEVISION

- We are** Link Electronics Limited, a successful, expanding company with room for individual ability to make itself felt.
- We make** a full range of TV studio broadcast equipment, including colour cameras for studio and O/B applications.
- We need** a **Commissioning Engineer** to work closely with the buyers of our equipment, assisting them in their acceptance checks of our products; training their staff and visiting them as required to see new equipment into service.

a **Senior Test Engineer** to undertake work on advanced and complex TV cameras and associated equipment, including our new multi-mode colour camera recently announced. These appointments are at a senior level and so direct experience of similar equipment is a **must**.

**We offer** salary above average, according to ability and not a rigid grade structure. Benefits, generous holidays, free life and health insurance, pension scheme, staff restaurant, relocation expenses.

**Location** a modern factory in a very pleasant part of Hampshire with no traffic problems and easy access to London, the South Coast and many major towns.

**Housing** a wide choice. Prices from about £10k upwards if you want to buy.

**TO APPLY** either phone **Jean Smith at Andover (0264) 61345** and ask for an application form or write to **Mic Comber** with enough information to make a form unnecessary.

**LINK**  
ELECTRONICS

Walworth Industrial Estate,  
Andover, Hampshire, England Telephone: Andover (0264) 61345

(7597)

# ELECTRICAL/ ELECTRONIC ENGINEERS

*Design unique computer/  
communication systems*

This is an opportunity to design, plan and manage the implementation of a wide range of interesting and unique computer/communication systems. The computer systems range from the use of microprocessors for specific applications, through mini computers to large main frame systems employing the whole range of peripheral devices. The communication systems range from line communications through the full spectrum of radio communications including satellite communications.

Most posts are designated project officer/manager, and involve the interpretation of internal customer requirements, and the preparation of project studies, designs and plans which provide technical solutions and define and cost all resource requirements to implement the solution.

Candidates must have passed, or been exempted from, examinations qualifying them for corporate membership of IEE or IERE, and have an aggregate of at least 5 years' recognised study, professional training and experience. Project management experience in the computer/communication field an advantage.

Starting salary between £3950 and £5240, depending on qualifications and experience. Promotion prospects. Non-contributory pension scheme.

For further details and an application form (to be returned by 10 November 1977) write to Civil Service Commission, Alencon Link, Basingstoke, Hants RG21 1JB, or telephone Basingstoke (0256) 68551 (answering service operates outside office hours). Please quote T(C) 85/1.

(7637)

## GCHQ Cheltenham

## The Polytechnic of North London

Department of Chemistry

## LABORATORY TECHNICIAN

(Grade 5)

is required in the Spectroscopy Laboratory of the Department either to operate the Mass Spectrometer or to be actively involved in the electronic and mechanical maintenance of spectroscopic instruments.

Experience at fault-finding, repair and maintenance of electronic and scientific instruments would be a special advantage.

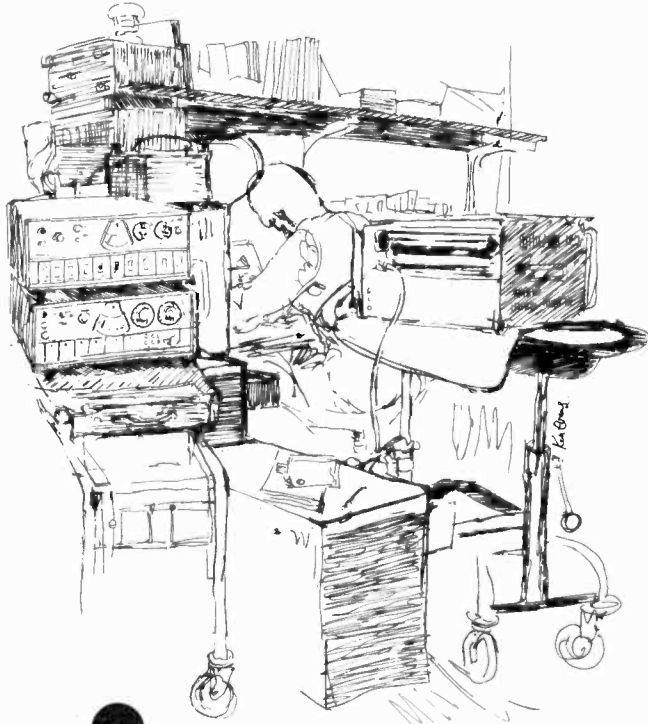
Candidates should normally hold HNC, C and G Advanced certificate and have at least 8 years' experience inclusive of the training period.

Salary scale: £3216-£3672 (inclusive of London Weighting) plus 5% earnings supplement (minimum £2.50 per week, maximum £4 per week).

Apply for further details and application form to the Head of the Department of Chemistry, The Polytechnic of North London, Holloway Road, London N7 8DB.

7572

# Marconi Instruments



## ELECTRONIC TECHNICIANS

**Opportunities for the experienced and sometimes inexperienced in St. Albans and Luton.**

Work situations range from fault finding on PCB's and components, to batch product testing of equipment that utilise very advanced techniques including microprocessors and the repair/calibration of all manner and types of test instruments.

Attractive salaries and, where appropriate, relocation are offered for the right candidates. Further information may be obtained in confidence from John Prodger

**Marconi Instruments Limited,**  
Longacres, St. Albans, Herts. tel: St. Albans, 59292



A GEC-MARCONI ELECTRONICS COMPANY

7613

## TV TRANSMITTER ENGINEERS

If you would like to work on some of the most modern TV Transmitters in the world why not join Pye TVT Limited, the Broadcast Company of Philips?

We are looking for engineers with several years experience of commissioning or maintenance or design of VHF or UHF TV Transmitters.

The job is to commission and carry out per-

formance tests on the equipment at our customers' sites and will involve extensive travel overseas.

HNC or equivalent is desirable, but it is more important that applicants have experience in the setting up and adjustment of TV Transmitters and are conversant with up to date TV colour measurements and techniques.

## STUDIO ENGINEER

We also require an Engineer to commission studio equipment. Several years experience of commissioning, maintenance or design of TV broadcast equipment is essential.

Attractive salaries will be paid plus overseas allowances and expenses where relevant. We

also offer all normal benefits and in approved cases relocation expenses to this pleasant part of East Anglia.

Please write or telephone: Dave Barnicoat, Personnel Officer, Pye TVT Limited, PO Box 41, Coldhams Lane, Cambridge CB1 3JU.  
Telephone: Cambridge (0223) 45115.

7620



## Pye TVT Limited

The Broadcast Company of Philips

# Glaxo

## ELECTRONICS ENGINEER

Our Research Central Services Unit at Greenford requires an Electronics Engineer to strengthen the team involved in the design and development of electronic equipment needed for experimental work in the Research Group. It is anticipated that the post will be filled by a graduate or an engineer with equivalent qualifications and some experience of electronics design. A knowledge of analogue and digital circuiting is essential and some experience in computer applications would be advantageous.

The appointment will be made in our Scientific Officer grade, the scale for which is £3147 p.a. to £5047 p.a. (including supplement and London Allowance). The starting salary will be according to qualifications and experience.

There are pension and bonus schemes and 20 days annual holiday. Assistance with relocation expenses will be paid where appropriate.

Please write or telephone for an application form to: R. E. Nolan, Personnel Officer (Research), Glaxo Research Ltd., Greenford Road, Greenford, Middlesex. Tel. 01-422 3434, quoting reference No. ZH179.

(7590)



We require an experienced

## BROADCAST ENGINEER

who's primary responsibility will be for maintenance, design and construction of equipment, but will also be involved with outside broadcasts.

If you are qualified to at least HNC level, send a written application, with brief details of experience to:

**Derrick Connolly**  
**Chief Engineer**  
**RADIO HALLAM**  
**PO Box 194, Sheffield S1 1GP**

## Electronic Engineers

Decca Radar Limited offer highly interesting career opportunities for Electronic Engineers to work in the Environmental Laboratories.

The work includes component and equipment evaluation and development together with design of special test equipment for Marine Radar and Government Contracts.

Applicants, men or women, with a knowledge of components and analogue/digital circuitry and possessing HNC/HND or equivalent should apply. General conditions of employment are consistent with a large progressive organisation with benefits which include a Pension and Life Assurance Scheme. Please write or telephone **G. A. Betts, Decca Radar Limited, Davis Road, Chessington, Surrey. Telephone 01-397 5281.**

**DECCA**  *The Queen's Award for Export Achievement to Decca Ltd 1976.* (7600)

## MANAGEMENT TRAINEE

A young technically orientated self-starter is required to train for management in Fields, based initially with our Aircraft Instrument and Ancillaries Division at Croydon.

The successful candidate is likely to be in his early to mid-twenties with a basic Engineering knowledge, probably gained in an indentured apprenticeship. A year or two's experience in purchasing or production management in the Engineering Industry would be a distinct advantage.

Prospects are excellent and the starting salary is negotiable in the region of £2,650.00.



Please apply for application form to:

**The Company Personnel Manager**  
**FIELD AVIATION LIMITED**  
**Heathrow Airport - London, Hounslow, Middx. TW6 3AE**  
**Tel: 01-759 2141, ext. 56**

7610

## RADIO ENGINEER/TECHNICIAN FOR THE CARIBBEAN

Needed to work as technical adviser to the Radio Schools in Haiti, a non-governmental literacy development programme. Responsibility for the training of local counterparts.

A British Volunteer Programme Post: Volunteer terms of service include free accommodation, living and other allowances, return air travel, language and orientation courses.

Write with details of curriculum vitae to: **CIIR Overseas Volunteers, 1 Cambridge Terrace, London NW1 4JL.** (7596)

**CIIR** OVERSEAS VOLUNTEERS

**HI-FI — IS IT  
YOUR SUBJECT?**

We are looking for someone young (up to 30), literate and interested enough in Hi-Fi to want to join the technical staff of our Hi-Fi Magazines. A knowledge of models and the market is essential in this post which might suit someone either in the trade or with a technical background. Salary range commences at £3,500.

Apply to Sharon Giles, Haymarket Publishing Ltd., Regent House, 54-62 Regent Street, London W.1.

(7593)

**TELEVISION  
BENCH ENGINEER**

R & L Services (London) Ltd. require a Television Bench Engineer with experience of working on all makes of sets including English, Japanese, continental, etc., to work in the west 10 area. Salary negotiable.

Telephone:  
696 4781 or 960 4239

(7651)

**AVIONICS ENGINEER**

Licensed 12.1 12.2 12.3 required to help organise and run repair workshop at Dublin Airport. Salary negotiable in the £4,000 - £6,000 range.

Apply to:

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(7618)

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30 Windmill Street, London, W1  
01-637 5551

**FIELD & BENCH  
ENGINEER**

required for work on radio  
telephone equipment

573-4541

(7609)

**RADIO - TELEPHONE ENGINEERS**

Experienced in V.H.F. mobile equipment. Top salaries for top ability. We are a young, progressive company currently the busiest, and fastest expanding radio-telephone firm in London. Ring London Communications on 01-328 5344 ask for Mike Rawlings or Bill Clarke. (7356)

**RECORDING STUDIO NEEDS** experienced maintenance engineer. Must be conversant with radio production techniques and equipment as well as all aspects of installation work. £4,250 + bonuses. Telephone Mike Farrell, day 01-437 6422, night 01-385 7451. (7630)

**INSTALLATION  
AND  
SERVICE ENGINEERS**

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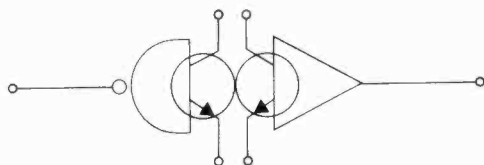
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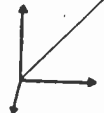
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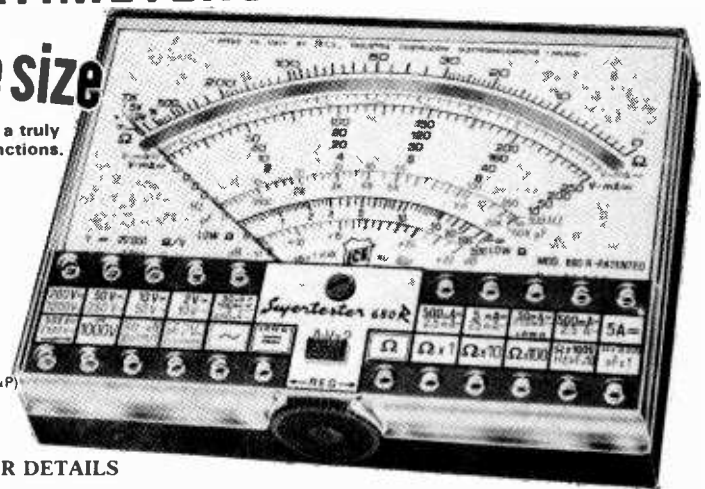
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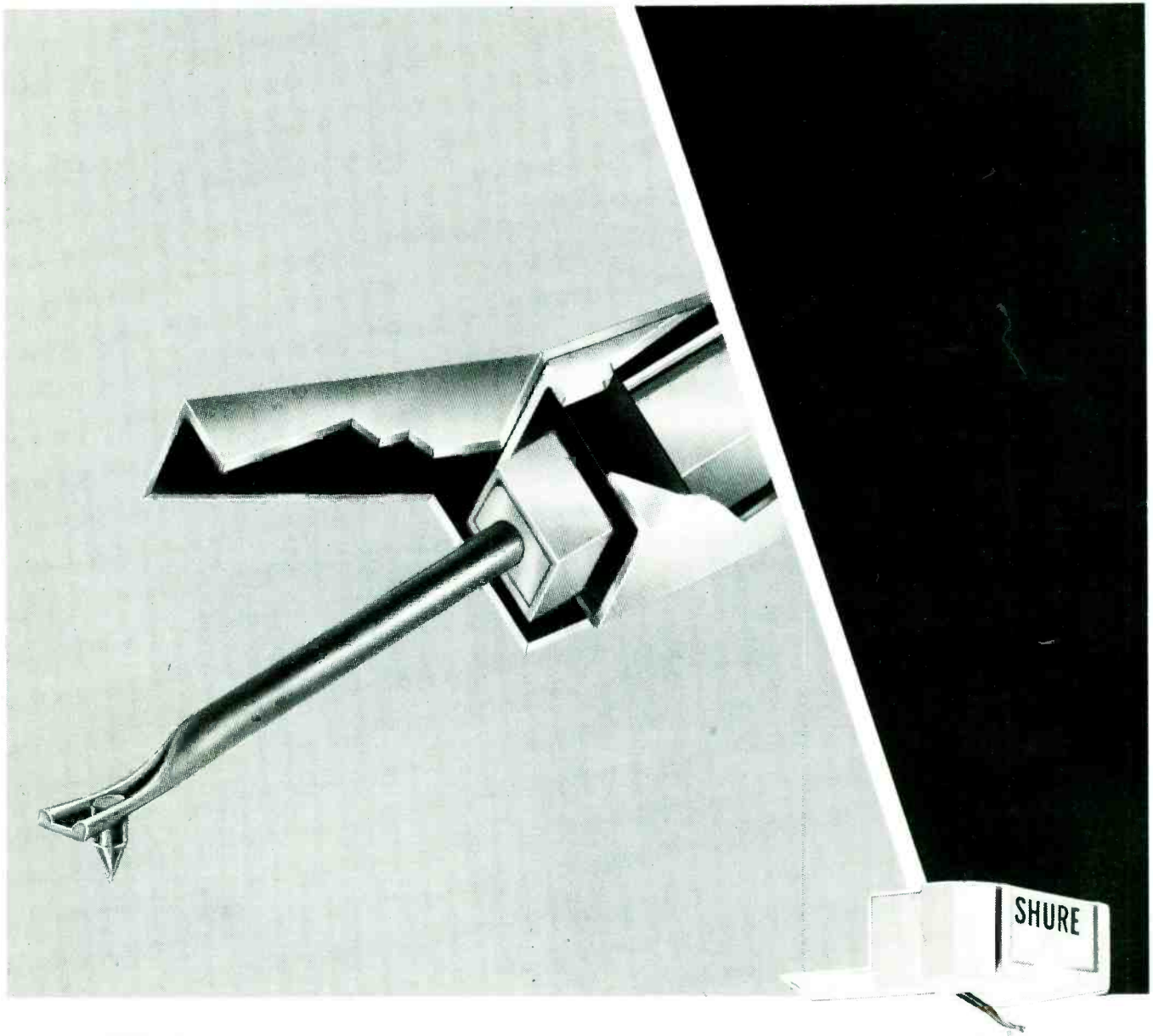
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