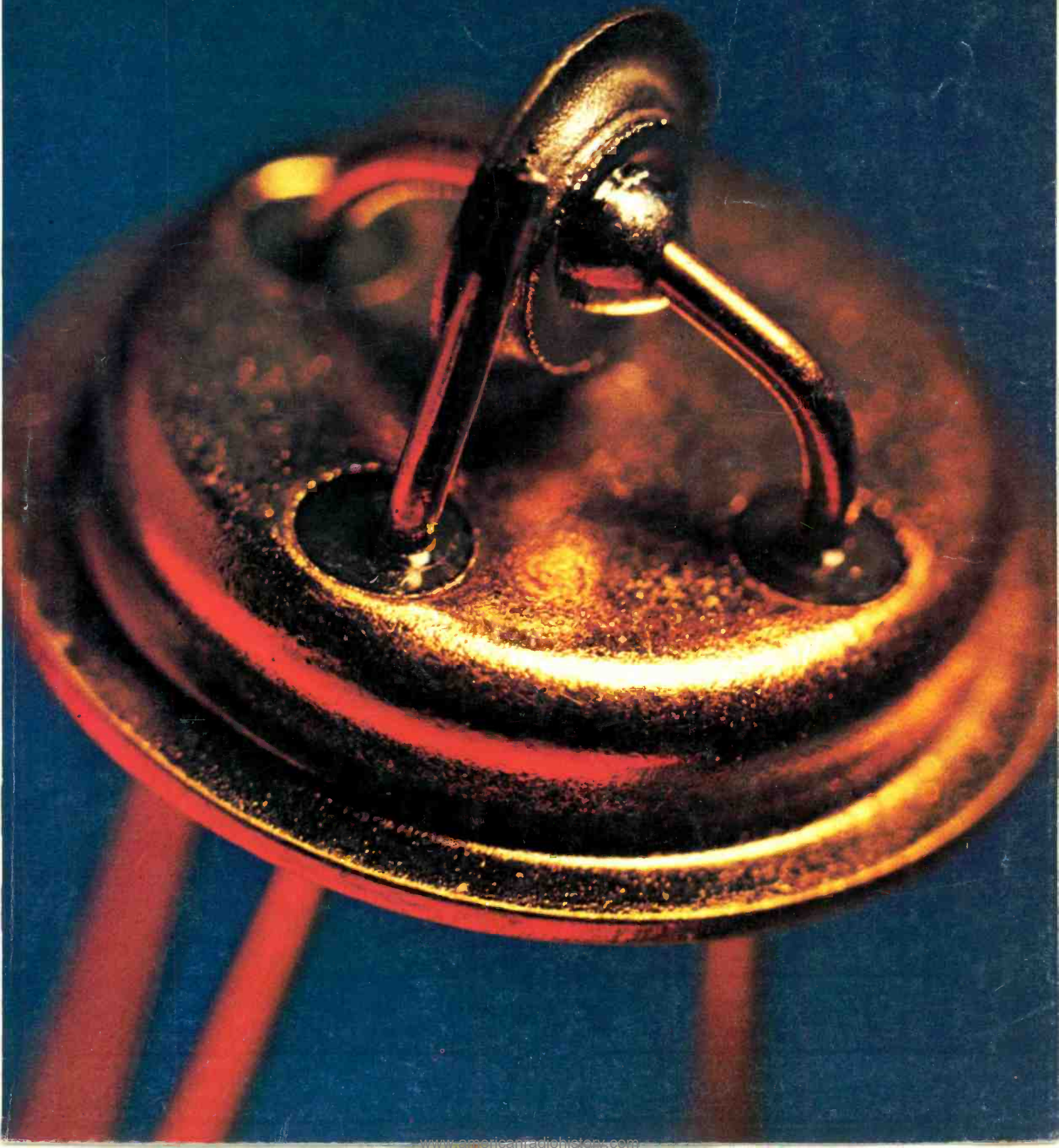


# Wireless World

January 1973 20p

The semiconductor story

Accurate I.f. source



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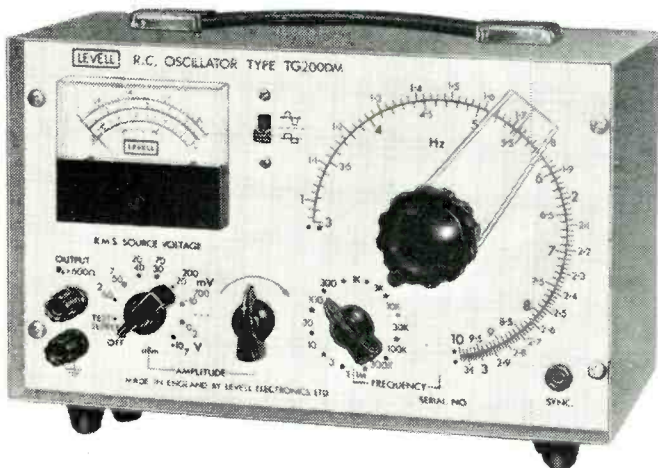


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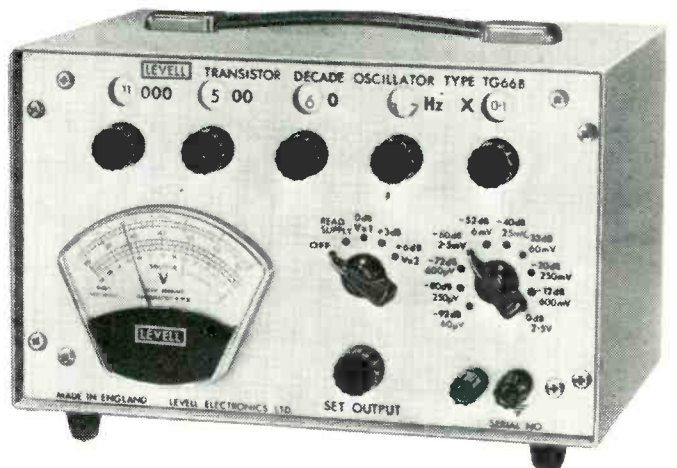
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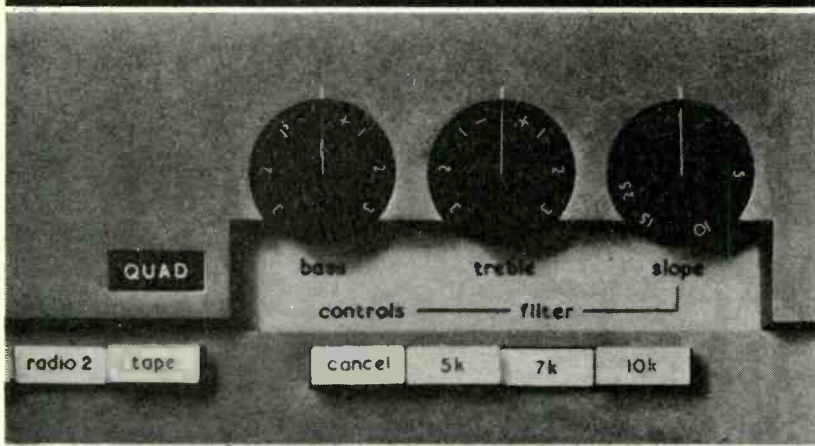
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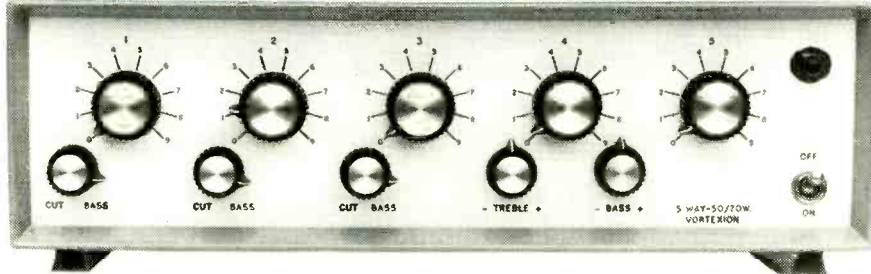
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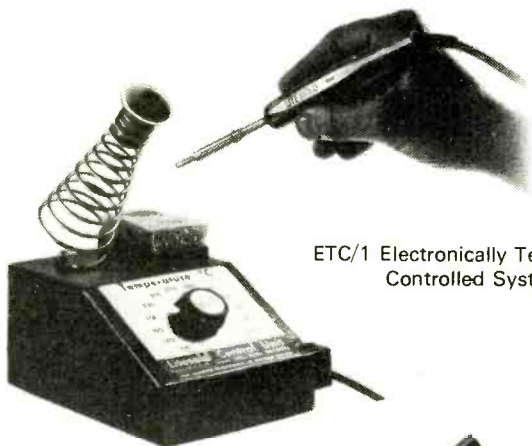
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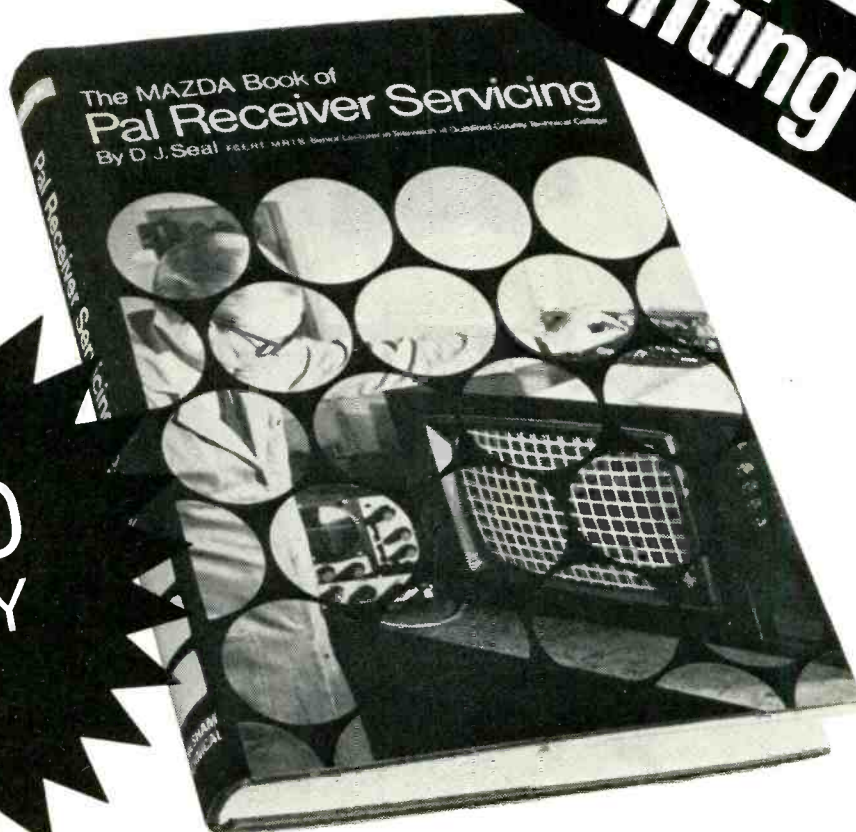
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#### The Author

David Seal, FSERT, MRTS is a Senior Lecturer in charge of the Television unit at Guildford County Technical College, Surrey. His practical grasp of television servicing problems derives, not only from his theoretical qualifications, but is firmly based on several years servicing experience updated by daily contact with his technician students.



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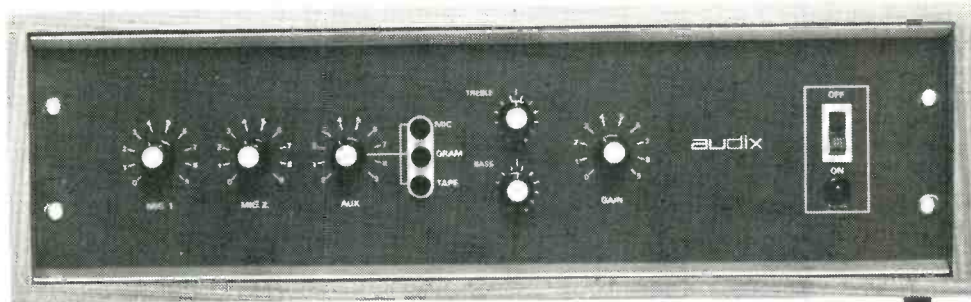




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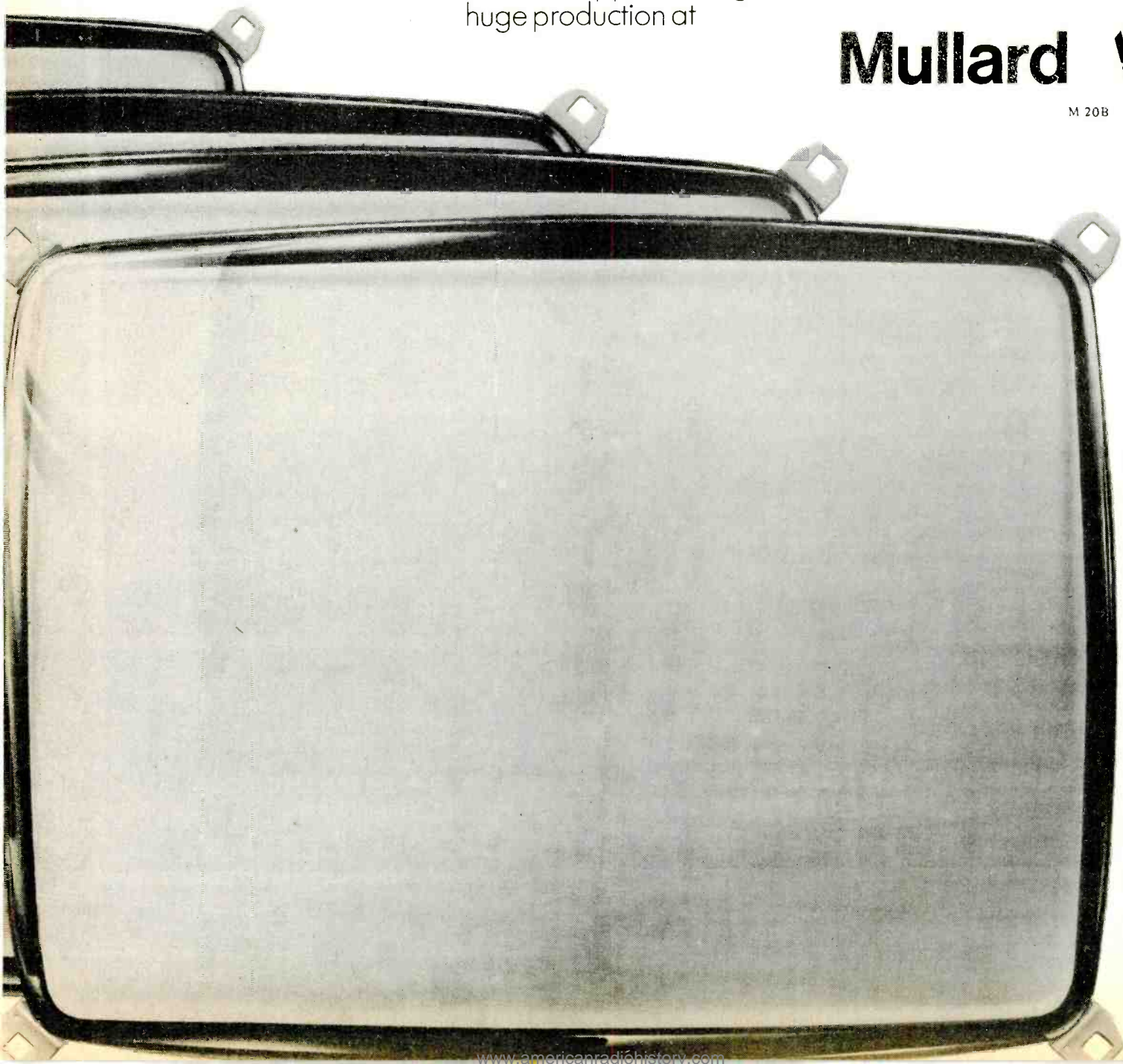
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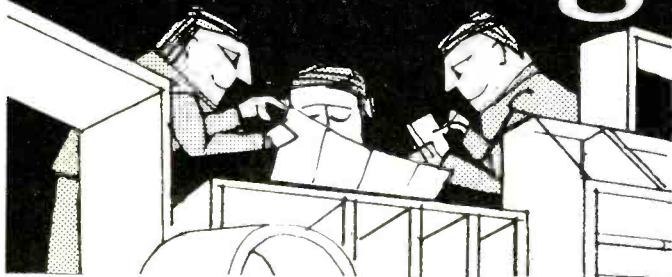
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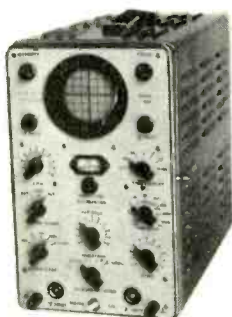


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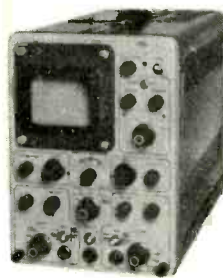
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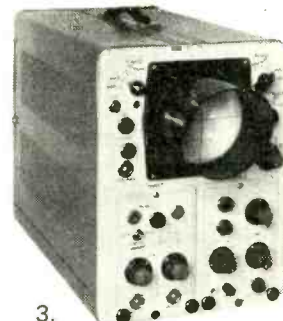
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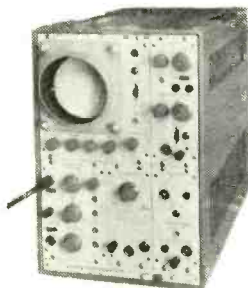
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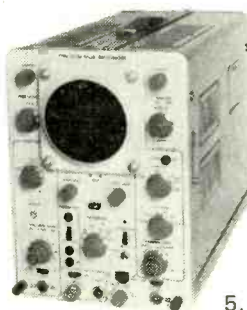
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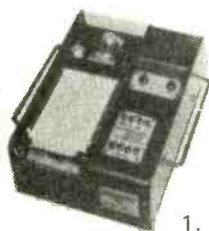


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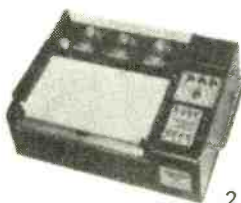


6.

## PEN RECORDERS



1.



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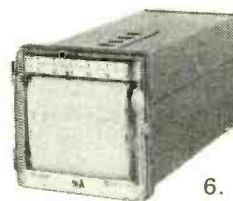
3.



4.



5.



6.

1. H320-1 High speed single channel

2. H320-3 High speed three channel

3. H390 Multi-range AC/DC Recorder

4. H352 Portable single channel 1mA.

5. H30 10-channel event recorder

6. H3100 single channel miniature 1mA recorder



### SUB-STANDARD MULTI-RANGE AC/DC VOLTMETER

Mirror scale 175mm long.  
Knife edge pointer.  
48 ranges from 75mV to 750V and from 300µA to 7.5A.  
Accuracy 0.5% DC; 1% AC.  
Transistorized relay protects movement and circuits.  
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6 decades 0.1-1-10-100-1000-10,000Ω

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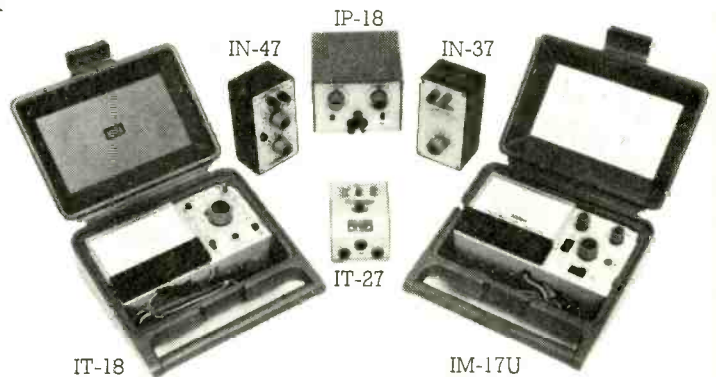
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## So advanced it's not yet made.

Years of experimental design have gone into this unique direct-coupled Stereo pre-amp and power amplifier. And contrary to usual practice the circuit and component layout (critical for low hum levels) has been made public instead of being sold to one of the commercial companies.

So if you are serious about Hi-Fi and want the best amplifier in the world you're going to have to build it yourself. And obviously the components you use must be the best available. Manufacturers rejects, seconds, or anything bought from a dubious source are just not good enough.

We are offering all the semiconductors (inc. power supply), glass fibre p.c. boards ready drilled (all same size and stackable), all the capacitors including the new tantalum types and electrolytics, all to true Hi-Fi standards and all fully-approved by the designer for £29.75 for the 30 watt version and £36.30 for the 50 watt version.

**Specification**

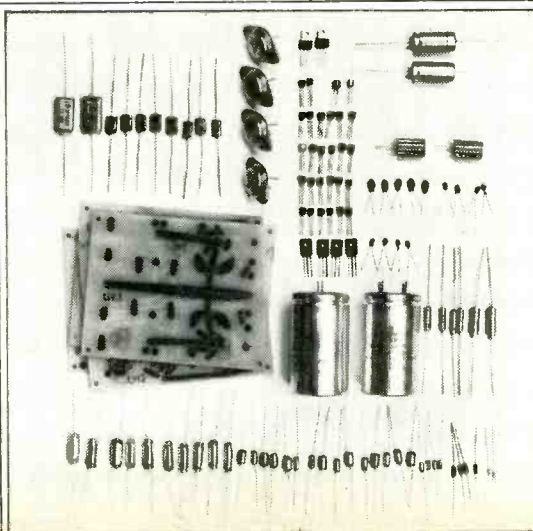
**Pre-amplifier**

Input selector:  
Mag p.u. Ceramic p.u.  
100KΩ 470KΩ  
Mode selector:  
Stereo. Reversed  
Stereo. Mono LH only.  
Mono RH only. Mono  
both channels.  
Filter selector:  
7KHz 10KHz 14KHz  
Twin volume controls  
Filter 'slope' control  
Treble  
Bass  
Balance  
Separate outputs for  
amplifier or tape  
recorder

**Amplifier**

Low distortion, wide  
bandwidth, DC coupled.  
Max power:  
30 or 50 watts per  
channel  
T.H.D :  
<0.01% at all power  
levels below clipping  
Bandwidth:  
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50W)  
Unconditionally stable,  
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I enclose cheque/postal order for £ for  Kits  watt output

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WW2



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# NOW IT'S THE AMCRON DC 300

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£360

## AMCRON DC.300 TWO CHANNEL POWER AMPLIFIER

Eminently suitable for P.A. operation, laboratory and other precision controlled applications. There are other power amplifiers in the Amcron (formerly Crown International) range from two channel 60 watts RMS output to 1000 watts RMS single channel models as well as pre-amp I.C. 150.

*Requests for fuller information invited*

In the Amcron DC.300 you will recognise what was formerly the Crown International DC.300. No other power amplifier in the world has such remarkable specifications. The change to Amcron was simply to avoid possible confusion of name identification. Nothing else has been altered. It might be that the DC.300 you order still shows 'Crown' on the front. It is of no significance. The Amcron remains the same thoroughbred in electronic engineering. Only the name has been changed and if you value perfection, it won't take long to remember.

● BRIEF SPECIFICATIONS

POWER	At clip point 340 watts RMS per channel into 4 ohms. 190 watts into 8 ohms per ch. Mono — more than 500 watts RMS into 8 ohms.
POWER RESPONSE	± 1dB from zero to 20 KHz at 150 watts RMS into 8 ohms per ch.
THD	0.02% at 300 watts RMS per ch. into 4 ohms.
I.M. DISTORTION	less than 0.1% from 0.01 watts to 150 watts RMS into 8 ohms per ch.
HUM & NOISE	100 dB below 150 watts RMS into 8 ohms per ch.
DAMPING FACTOR	Greater than 200 up to 1KHz.
PROTECTION	against short or open circuit and mis-matching.
INPUT SENSITIVITY	1.7V ± 2% at 10 KHz for 150 watts RMS into 8 ohms.
SIZE	19" x 7" high x 9½" deep with front panel, suitable for rack mounting.

LEAFLET WITH FULLER DETAILS ON APPLICATION



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WW—022 FOR FURTHER DETAILS

# SHIBADEN'S NEW COLOUR VIDEO TAPE RECORDER

**For Clear and Sharp Colour  
Reproduction with Variable  
Slow and Still Capability**



This new unit conforming to the new E.I.A.J. standard the SV-620 produces really beautiful high fidelity colour pictures using a very efficient video head with a newly developed HPC ferrite.

This new unit offers a pre-eminent stability and functional performance: it has a horizontal resolution of 240

lines and video signal-to-noise ratio of 40dB minimum (black and white) and has facilities for variable slow motion and still picture in full colour. Switchable PAL-SECAM and also fully compatible with the SV-610 black and white recorder. The SV-620 is ideal for any application where top level

information and education are essential with a playing time of 76 minutes.

**Full colour edit version now available.**  
This new unit allows insert and assembly edits with no loss of colour. Simple automatic tracking ensures trouble free edits. Designated the SV-620D, specifications are identical to the SV-620.

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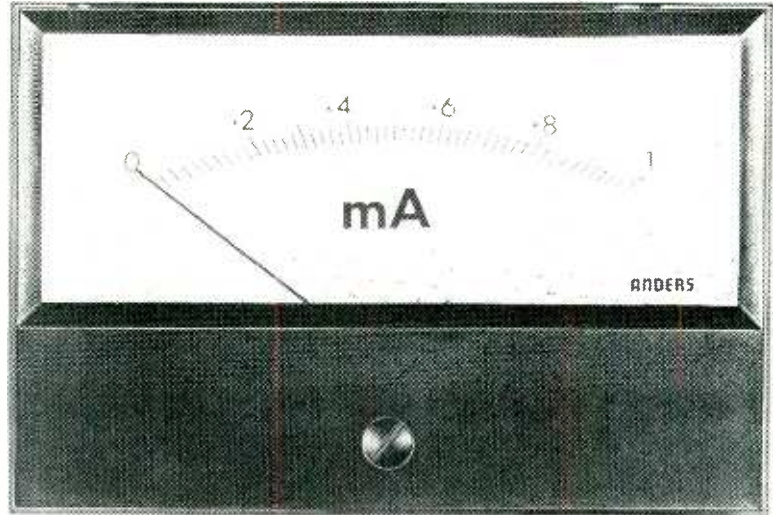
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# ANDERS MEANS METERS...

## REGAL RANGE

- New 100° arc high quality meters at low prices.
- Rugged taut band construction — pivot and jewel available to order
- Sensitivities to 10  $\mu$ A
- Very competitively priced for OEM quantities
- Modern styled meters in matt black plastic cases with flattened arc giving long scale.

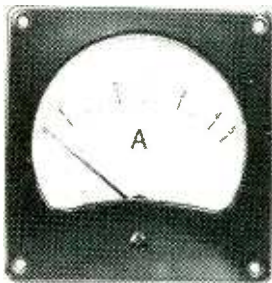


### TWO MODELS

- R55 2.5in (63.5mm) Scale length
- R65 3.2in (81.3mm) Scale length

Anders provide what is probably the largest range of meters available from a single source in Europe: MC/MI, dynamometer, vibrating reed, electrostatic, etc. in over 100 case styles and sizes, a few of which are shown below.

Popular models and ranges are stocked in depth while a specially equipped instrument department enables swift production of non-standard ranges and scales, to suit individual customer requirements, in large or small quantities.



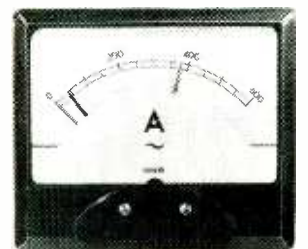
Vulcan Moving Iron. 4 models, 1.5", 1.8", 2.7", 3.7" scales. Voltmeters, ammeters and motor starting meters.



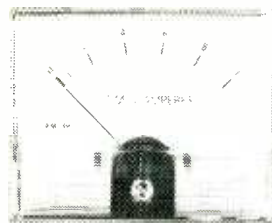
Profile 350 edgewise 4.3" scale. DC moving coil and AC moving coil rectified. Horizontal or vertical mounting.



Crescent Long Scale 180°. 3 models, 4", 5", 6.25" scales. DC moving coil and AC moving coil rectified. Clear plastic.



Soliconroller Moving Coil Relay. DC moving coil and AC moving coil rectified. 1 or 2 adjustable alarm controls.



Kestrel Clear Front. 7 models, 1.3"—5.25" scales. DC moving coil, AC moving coil rectified, AC moving iron.



Stafford Long Scale 240 6 models, 3.5"—11.5" scales. DC moving coil, AC moving coil rectified, AC moving iron. Also 98 scale.



Lancaster Long Scale 240 . 2 models, 4", 5.5" scales. DC moving coil and AC moving coil rectified.

**ANDERS ELECTRONICS LIMITED** 48/56 Bayham Place, Bayham Street, London, N.W.1. Telephone 01-387 9092.

Manufacturers and distributors of Electrical Measuring Instruments. Sole U.K. distributors of FRAHM Resonant Reed Frequency Meters and Tachometers. Manufacturers of purpose built electrical and electronic equipment to customers requirements.

WW-024 FOR FURTHER DETAILS

# Go Hi-Fi yourself!

## New Goodmans Din 20 loudspeaker kit — specially designed to give the D.I.Y. enthusiast excellent hi-fi reproduction at moderate cost.

This system has been thoroughly tested to Goodmans high standards. It will provide extremely satisfactory listening levels from amplifiers rated at 10 watts (per channel, in the case of stereo equipment) but it may also be operated from amplifiers of higher power.

The kit contains all parts needed to complete the system (except timber and other material for the cabinet itself) and has detailed, illustrated assembly instructions.

### Contents

1. Bass unit 204 mm (8ins) diameter.
1. Dome HF radiator 25.4 mm (1 in) diameter.
1. Port tube.
1. Crossover panel with colour coded leads.
1. Terminal board.
1. Foam gasket.
1. Input lead complete with DIN plug and spade terminals.
- Acoustic wadding foam pad.
- Fixing screws and hardware.
- Cabinet template (on bottom of box).

### Specification:

20 watts DIN, 4 ohms impedance, 8 ins bass unit, dome HF radiator, crossover frequency 4,000 Hz

For further details and the name of your Goodmans dealer, send the coupon now



# Goodmans

Sound reasoning.

To: Goodmans Loudspeakers Ltd.,  
Downley Rd., Havant, Hampshire.  
Please send me free leaflets on Constructors' equipment and the name of my Goodmans dealer.

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Address \_\_\_\_\_

WW6

WW—026 FOR FURTHER DETAILS

# “NO



## I'D RATHER HAVE A MINITEST™

The SEI MINITEST has made a remarkable impact in the pocket-sized multi-range meter market, by making itself a firm favourite with discerning people in the industry. Let's look into the reasons why.

First, the appearance. Diminutive, neat, wipe-clean cyclac case with shock and magnetic field proof steel liner. Controls are simple and easy to use.

Second, the range. The Minitest measures a.c. and d.c. voltages d.c. current and resistance over 20 ranges to a sensitivity of 20,000 and 2,000 ohms per volt d.c. and a.c. respectively. Third, high voltage probes. These extend the range to 25 or 30kV d.c. Little wonder the Minitest is preferred!



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WW—027 FOR FURTHER DETAILS



# Amplivox Minilite. Untouched by human ear.

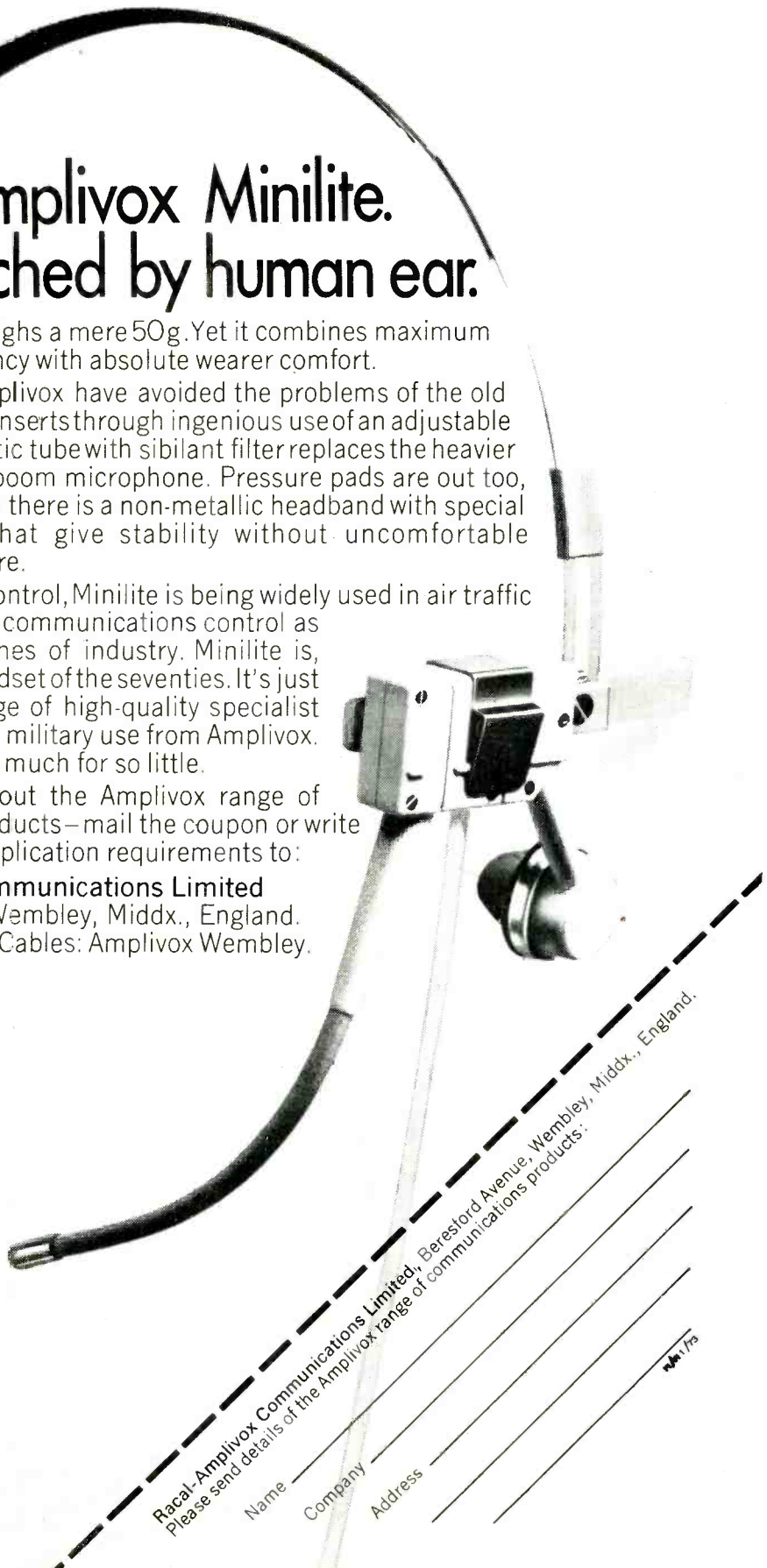
New Minilite weighs a mere 50g. Yet it combines maximum operating efficiency with absolute wearer comfort.

With Minilite, Amplivox have avoided the problems of the old fashioned earplug inserts through ingenious use of an adjustable earpiece. An acoustic tube with sibilant filter replaces the heavier and more familiar boom microphone. Pressure pads are out too, instead there is a non-metallic headband with special bars that give stability without uncomfortable pressure.

Specified for Eurocontrol, Minilite is being widely used in air traffic control, aviation and communications control as well as other branches of industry. Minilite is, undoubtedly, the headset of the seventies. It's just one of the wide range of high-quality specialist products for civil and military use from Amplivox. No-one else offers so much for so little.

To find out more about the Amplivox range of communications products—mail the coupon or write today stating your application requirements to:

**Racal-Amplivox Communications Limited**  
Beresford Avenue, Wembley, Middx., England.  
Tel: 01-902 8991. Cables: Amplivox Wembley.

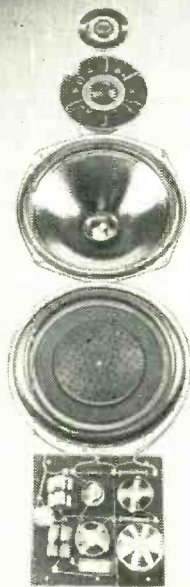
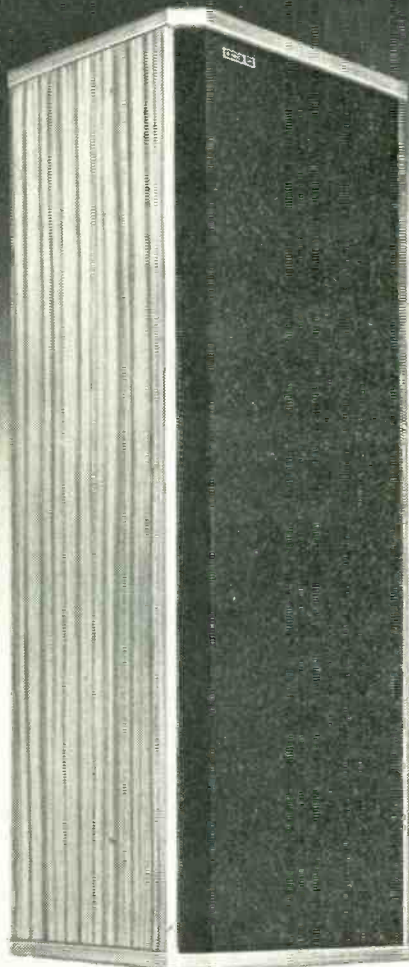


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# Ditton 66 Studio Monitor



- 1.) Celestion's new super tweeter.
- 2.) New design 'pressure' mid-range unit.
- 3.) Ultra Linear 12" Bass drive unit.
- 4.) A.B.R. ensures controlled bass down to 16Hz.
- 5.) Precision crossover for perfect system intergration.

A new Loudspeaker of advanced design suitable for studio use and for home installations of the highest quality.  
UNITS: HF 2000 (dome 'pressure' type) MF 500 (Mid-range Dome 'pressure' type) Ultra linear 12" bass driver and 12" ABR. The crossover has resulted from considerable research and crossover points are at 500 Hz and 5000 Hz 80 Watts Maximum, 4-8 ohm. This monitor loudspeaker system has an exceptionally wide and flat frequency response. Very low order harmonic and inter-modulation distortion. Precise response to transients. Beautifully maintained polar response ensures absence of unwanted directional effects and provides a highly satisfactory stereo image throughout the listening area. Matched pairs.  
SIZE 40 x 15 x 11½ Natural Teak or Walnut Cabinet

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10MHz sine wave output at IV RMS  
Long term stability better than  $1 \cdot 10^{-10}$  per month  
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Warm up: less than 10 minutes to reach  $2 \cdot 10^{-10}$   
Power consumption: only 13 Watts at 25° C ambient from a 24V supply

Dimensions: 4 x 4 x 4.5 inches

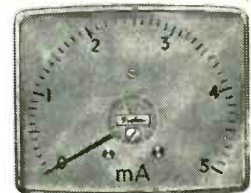
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## 240° of shadowless readings. That's the Taylor Fyneline 'Wide Angle' range.



Meet Taylor's new range of 'Wide Angle' panel meters. The 240° circular scale offers scale lengths of approximately twice that of similar 90° movements.

Model 38, illustrated here, is the smallest in the range with the scale length of  $4\frac{3}{8}$  in. and a panel width of little more than  $2\frac{1}{2}$  in. Find out more about the complete Fyneline range including our 'Standard' and 'Picture Frame' models. Write for data sheet now.

**Taylor**

Taylor Electrical Instruments Ltd.,  
Archcliffe Road, Dover, Kent.  
Telephone: Dover 2634 Telex: 96283

Thorn Measurement Control and Automation Division.

THORN

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Because the chances are they'll have our TT21 already fitted.

Because it's the best beam tetrode you can buy. Best in its class. Best for the money.

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# The new Linstead Millivoltmeter.



**Wide range, 5" scale length,  
5"x5" bench space.**

**M2B** This instrument is based on our popular M2A and has been completely redesigned mechanically for convenience in operating and attractive appearance.

The Panel layout has been designed to give maximum utilization without waste of area. By using a vertical styling valuable bench space is reduced. The case extends to protect the meter and terminals without affecting accessibility. The carrying handle will either sit neatly on top of the instrument when vertical or be used as a rest to allow operation in a sloping position. The battery (the readily available PP9) is accessible from behind a rear plate held by a single retaining screw.

Specification: A.C. 1.2mV FSD to 400V  
D.C. 120mV FSD to 400V

in 20 ranges.

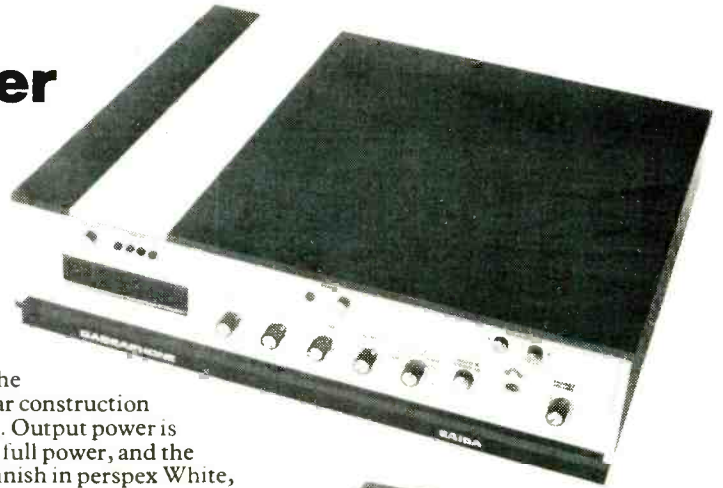
Further details about the new Linstead Millivoltmeter available on request.

**Linstead**  
means a good deal  
in electronics

Linstead Electronics, Roslyn Works, Roslyn Rd., London N15 5JB  
Telephone: 01-802 5144

WW-034 FOR FURTHER DETAILS

# GABRAPHONE Integrated Amplifier -Tape Players



**Saida de Luxe** A stereo amplifier of the highest quality performance with built-in 8-track cartridge player, housed in 18" cabinet. A unique feature is the electronic switching between signal sources, completely eliminating switch-contact noise and unwanted coupling between signal circuits. Input connection facilities for magnetic pick-up, radio tuner or other auxiliary signal source, together with a record replay socket for external tape-deck. Dual loudspeaker circuits, with front-panel switching. The headphone socket has its own, independent, volume control. Modular construction is employed throughout, providing ready interchangeability of units. Output power is 12 watts RMS per channel into 8 ohms distortion less than 0.02% at full power, and the frequency response 25 Hz to 25 kHz ± 1 db. Outstanding styling - finish in perspex White, Black or Grey.

**Saida Minor de Luxe** Multi-input stereo amplifier with built-in 8-track stereo cartridge player for continuous entertainment. Large performance in small size - only 14" x 12" x 5". Inputs for magnetic pick-up and auxiliary signal source. Electronic switching between inputs, output 12 watts RMS per channel into 8 ohms. Available in perspex White, Black or Grey. Modular construction ensures ready interchangeability of units.

**Amelia de Luxe** Tape player - add-on unit. Provides playing facilities for 8-track stereo cartridges when combined with any stereo amplifier. Incorporates equalisation for tape replay characteristic and front-panel attenuator control to adjust output to suit amplifier used. Individual volume and tone control. Elegantly styled in Black, White or Grey perspex - matching the amplifiers and other units in Gabraphone range. Output 750 mVmax into 2,000 ohms. Also available without tone control. Write for full information.



Modern Engineering & Technology Ltd., 4 Station Road West, Canterbury, Kent. Tel: 0227 60431/2.

WW-035 FOR FURTHER DETAILS

## Valradio

The Marine Valradio range of Transvertor are designed for operating low voltage DC battery equipment. Models are also available for AC equipment. Dual 110v and 220v DC available as standard as well as single voltage units.

Type	Input	Output	Price
CR110/220/60RT	110/220	12v 5A smoothed or 24v 2.5A DC	£66.00
CR110/220/12T	110/220	12v 10A Smoothed DC	£88.00
C110/220/60S	110/220	115 & 230v sine wave 60 watts	£70.40
C220/200S	220	115 & 230v sine wave 200 watts	£101.20

Other similar units available to operate from 12, 24, 32 & 50V DC and outputs of from 30W to 750W in square, sine wave or DC.



Send for information leaflet WC13.

**VALRADIO LIMITED**  
BROWELLS LANE, FELTHAM, MIDDX. TW13 7EN  
TEL: 01 890 4242/4837

WW-036 FOR FURTHER DETAILS

## Audio Connectors

Broadcast pattern jackfields, jackcords, plugs and jacks  
Quick disconnect microphone connectors  
Amphenol (Tuchel) miniature connectors with coupling nut  
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XLR compatible in-line attenuators and reversers  
Low cost slider faders by Ruf

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London W1V 3LE  
01- 437 1892/3

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## SANWA MULTI TESTERS



MODEL U-50DX

USED THROUGHOUT THE WORLD. SANWA'S EXPERIENCE OF 30 YEARS ENSURES ACCURACY, RELIABILITY, VERSATILITY, UNSURPASSED TESTER PERFORMANCE COMES WITH EVERY SANWA 6 Months' Guarantee Excellent Repair Service

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Model U-50DX	£9.00	Model 460-ED	£23.40
Model A-303TRD	£11.85	Model EM-700	£45.96
Model K-30THD	£13.55	Model R-1000CB	£59.25
Model E-80TRD	£14.75		

Cases extra, available for most meters, but not sold separately. Please write for illustrated leaflet of these and other specialised Sanwa meters

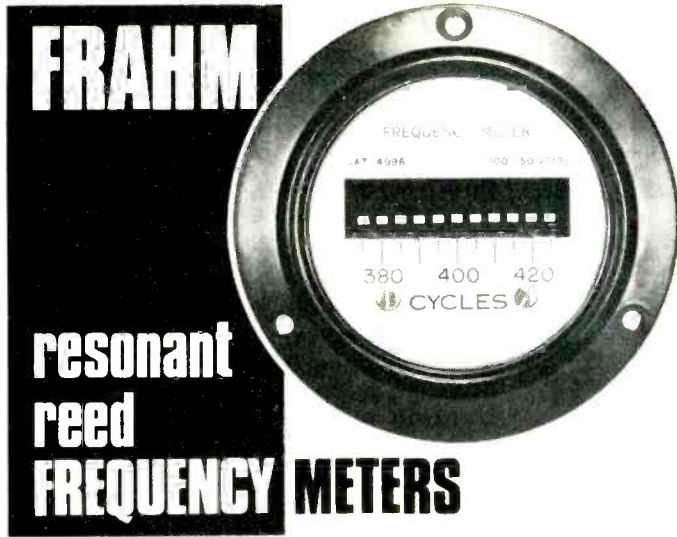
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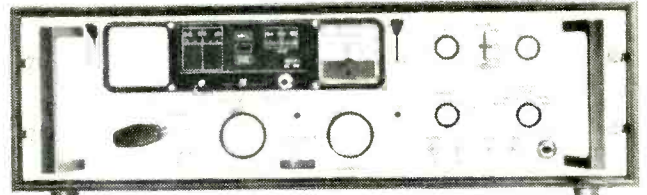
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**EC958  
series of receivers  
10kHz to 30MHz  
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Low cost, compact units extremely simple to operate and protected against overloads the

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are the ideal choice for general purpose bench use. They have good regulation against load or line variation and low ripple content at the output.

Each unit offers two operating ranges, expanding its usefulness at the touch of a button to that of two units.

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WW—042 FOR FURTHER DETAILS

## For high accuracy get Hatfield in your sights



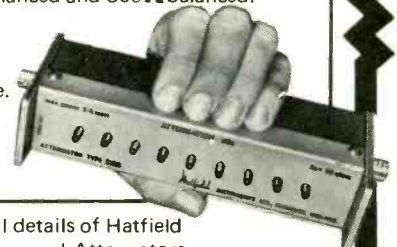
High accuracy over 4, 5 and 6 decades is provided by the full range of Hatfield's Resistance Decade Boxes. (Housed in robust Bondene construction cases). Alternative models with 0.1% or 1% accuracy steps range from  $1\Omega$  to  $100\text{ k}\Omega$ .

Prices from only £10 ex works for 4 decades 1% to £23 for 6 decades 0.1%.

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Another hit in design laboratories is the 2100 Series of Switched Attenuators. They're in similar styling to the Decade boxes with a full range of 8 models covering impedances of  $50\Omega$ ,  $75\Omega$ ,  $600\Omega$ , unbalanced and  $600\Omega$  balanced. A choice of silver or gold switch contacts for each impedance. Only £28 for silver contacts or £36 for gold ex works.



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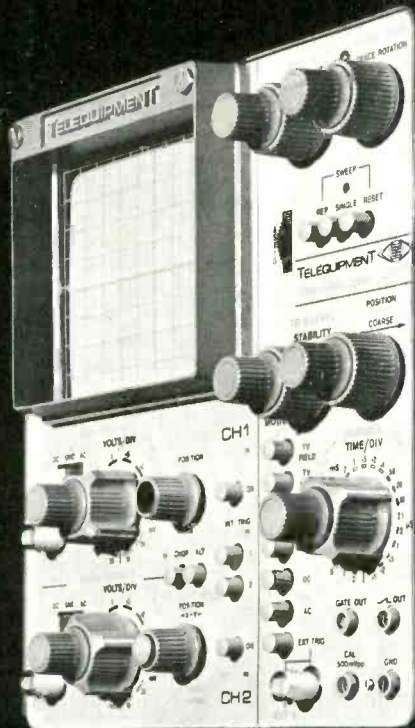
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Telex: 45592 South-East Asia: *for prompt service and deliveries, contact: Hatfield Instruments (NZ) Ltd.*  
P.O. Box 561, Napier, New Zealand.

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# two new dual-trace oscilloscopes



## from Telequipment

- \* D65 for DC-15 MHz operation
- \* D66 for DC-25 MHz operation

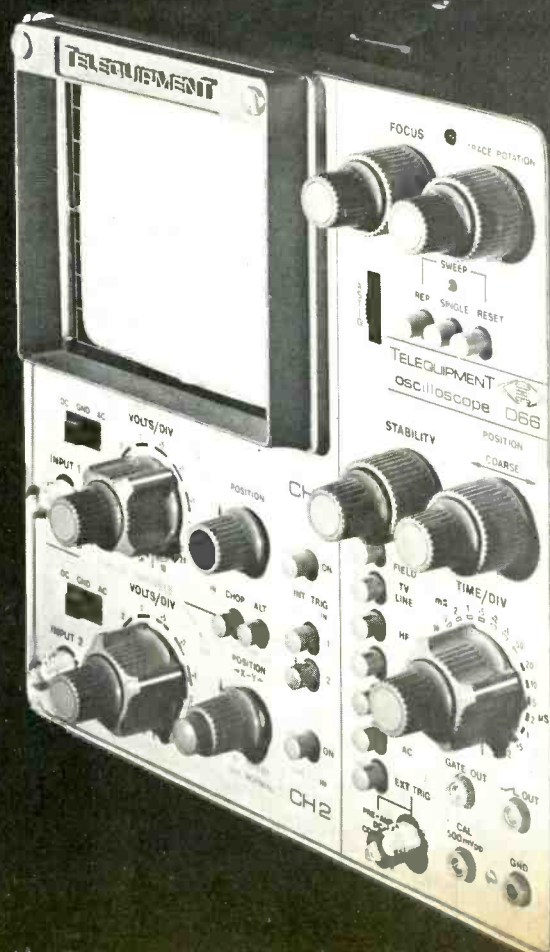
- Large, bright 8 × 10cm display
- Switched X-Y operation
- Signal Delay
- Lightweight, fully portable

## the D65 and the D66

Embodying all the features required for general purpose laboratory measurements, TV servicing and production testing applications; including wide timebase range — 100 ns/div to 2s/div — and broad bandwidth characteristics. Dual-trace allows channels to be displayed separately, added algebraically, alternated or chopped. All solid-state construction plus Telequipment expertise give you choice of two superb instruments at realistic prices —

D65, 15 MHz for £195 (UK)

D66, 25 MHz for £225 (UK)

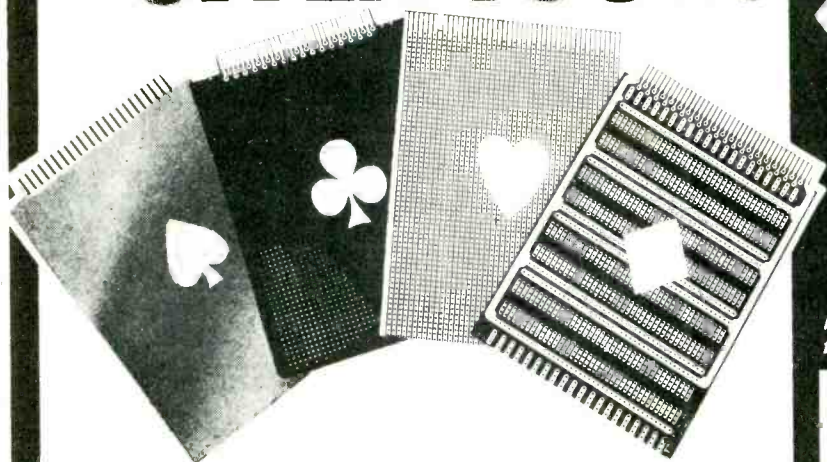


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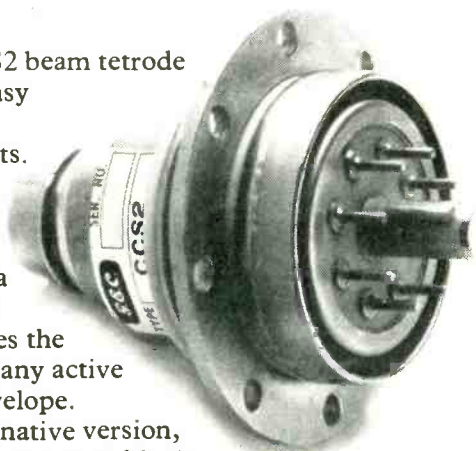
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Our CCS2 beam tetrode is especially easy to design into co-axial circuits.

That's because we've designed a special beryllia ceramic flange which separates the heatsink from any active part of the envelope.

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... and moving iron and rectifier movements too. For any application, there's a high quality Ferranti panel instrument available in a wide variety of presentations.

And they are reliable, accurate, stylish and competitive.

### President

Two styles with scale lengths 3.8 in., 2.8 in. and 2.2 in.

### Classic

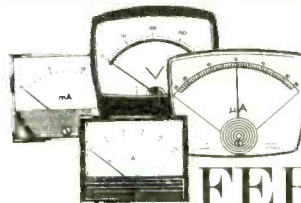
To BS 89. Scale lengths 4.5 in., 3.2 in. and 2.2 in.

### Style A

Front and rear projection a minimum. Scale lengths 2.5 in. and 3.5 in.

Send for illustrated literature.

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Instrumentation Division,  
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Tel: 061-681 2071 Telex: 667857



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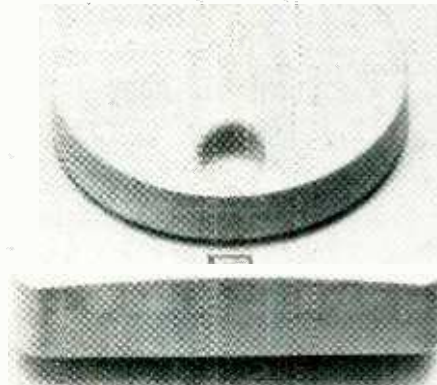
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Velvet dim to full brightness at a touch of the finger. Off/on and infinitely variable.

Beta light glow makes switch easy to find in the dark and consumes no current.



Economical too!

As the light is progressively dimmed, so the current consumption drops – think of it as an electric tap. 300 watt capacity, straight replacement for standard light switch.

Complete kit of parts £2.80 or made up £2.90



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The Jermyn capacitor discharge ignition system.

Instant starting in all weathers. Even with a near flat battery, the unit will produce a full sized spark.

Just one of the many advantages of an electronic ignition system, the others are:

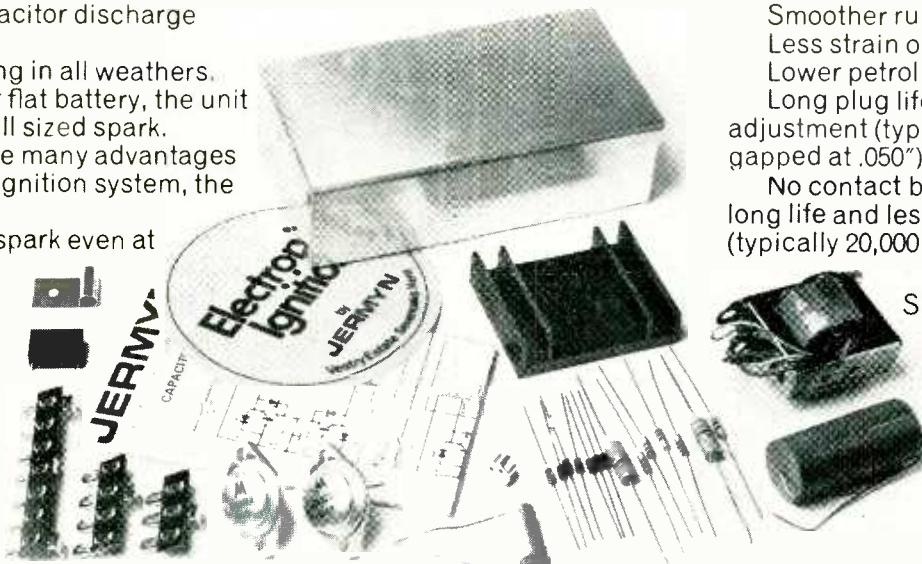
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Smoother running.

Less strain on battery and starter. Lower petrol consumption.

Long plug life with infrequent adjustment (typically 20,000 miles, gapped at .050").

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STATE + or – earth when ordering.

Complete set of parts to build it yourself for only £7.75, as described in Practical Wireless and fully approved by the author.

**Save 55p**  
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Please despatch return of post ..... light dimmer kit ..... light dimmer .....  
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# JERMYN



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### DL905 Transient Recorder

Single voltage transients, repetitive waveforms, or very slowly changing signals can all be recorded by the DL905 in its digital memory. The captured signal may be viewed on an oscilloscope, a permanent record produced on a chart recorder and a digital readout obtained to feed a digital recording device or general purpose computer.

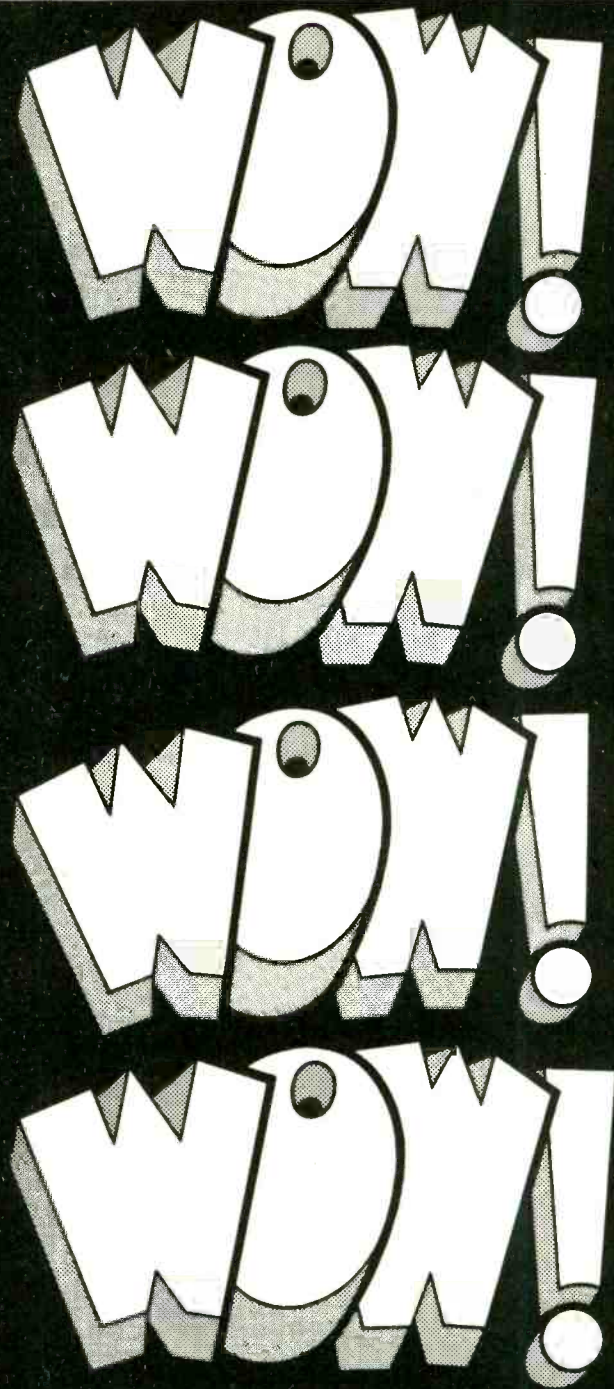
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# TIMERS SWITCHES TRANSFORMERS VOLTAGE CONTROLS FOR IMMEDIATE DELIVERY

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 \*Panel Mounting. \*Low Price.  
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OMRON brand Synchronous Motor driven timer with single instantaneous and two timed change-over contacts.  
**MINIMUM** guaranteed electrical and mechanical 10,000,000 operations.

\*Stocked in 110VAC 240VAC up to twenty eight hours time range;  $\pm 3\%$  repeat accuracy.  
 £14.90 "one off" £10 in quantity.

## PNEUMATIC OMRON TIMER UP TO 200 SECS DELAY—"ATS"



Easily adjustable from delay on energise to delay on de-energise. The OMRON ATS works on an air damped principle and can be adjusted between 0.200 secs with screwdriver adjustment. A precision snap action switch provides a 6A contact and minimum 1,000,000 ops life.  
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Plug-in timer for panel mounting. Synchronous Motor driven with auto-reset facility. Instantaneous and time limit contacts rated at 5A. This timer has fixed and moving pointers.  
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Genuine 1% repeat accuracy with solid timing. Life 50 million operations minimum, instantaneous & time limit contacts. Full time scales 0-1sec; 0-2sec, 0-5sec, 0-10sec; 0-30 sec; 0-60 sec; 0-180sec.

Dual Voltage 110/240VAC £18.50 to £13 each.

## EXCLUSIVE SOCKETS FOR OMRON TIMERS & FLOATLESS SWITCHES



Screw terminals, with clips to hold the timer or switch firmly in place where mounted.  
 Type 8PF for STPNH, TDS, DTS  
 Type 8PFI for 61FGP & TDA

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## PANEL MOUNTING "NSY" SYNCHRONOUS TIMER



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Stock range 110/240 VAC up to 28 hrs £12.50 "one off" to £8 in quantity

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\*Interchangeable with all British & Continental Manufacturers

\*Approvals from: CSA; MIL; UL; SEVC; SAA; DEMKO ETC



**VIC WITH AMP TERMINALS**  
 Single Pole Changeover 15amp switch O.F. 400gm R.F. 114gm M.D.O. 4mm. £19 per 100; £150 per 100; £700 per 5000.



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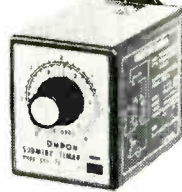
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 Low cost microswitch for coin operated or air vane applications. O.T. 10gm. R.T. 13gm. M.D. 15°. £31 per 100; £190 per 1000; £900 per 5000.



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Only OMRON could provide a timer of such unrivalled superiority over all its competitors, anywhere in the world. The STPNH is a synchronous motor driven timer with automatic reset function. Both instantaneous and time limit contacts are fitted and the timer is mounted on an international 8 pin octal base. Time ranges start 0.6 secs and finish 0-28hrs with operating voltage at 110VAC or 240VAC.

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## PFQ3 SUBMINIATURE PUSHBUTTON SWITCH.

"Push to make" switch with black button 3amps @ 240VAC 15p each per 1000.

## 1SAT4 SUBMINIATURE TOGGLE MICROSWITCH.

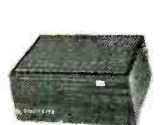
CSA approved toggle switch rated 5A @ 240V 50p ea. in small quantities.

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Full range available with 15amp switching capacity. Approved by CSA Authorities & guaranteed for twelve months. Interchangeable with other British and Continental manufacturers typical price is around £3.50 for the coil spring type.

## VOLTAGE STABILISER



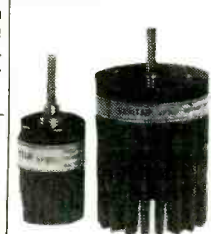
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 \*Input 240VAC  $\pm 20\%$   
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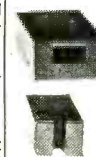
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Full solid state control over AC voltages. Input of 230VAC variable on output to 25-230VAC. Miniature and lightweight with finned aluminium housing these units can truly replace wirewound transformers.

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WORK DIRECT FROM 24VAC SUPPLY.  
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## TECHNICAL LITERATURE

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## ALL THE PRODUCTS ILLUSTRATED HERE ARE ALSO AVAILABLE FROM THE FOLLOWING I.M.O. FRANCHISED DISTRIBUTORS.

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WW—052 FOR FURTHER DETAILS

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Illustrated the Si452 Distortion Measuring Unit — low cost distortion measurement down to .01% **£30.00**

Si451	<b>£35.00</b>	i453	<b>£40.00</b>
Comprehensive Millivoltmeter		Low distortion Oscillator	
350μ Volts	20 range	sine Square RIAA	

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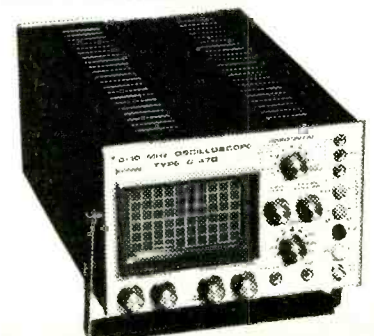
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### MANUFACTURER OF ELECTRONIC MEASURING INSTRUMENTS



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bandwidth: from DC to 10 MHz  
sensitivity: 10mV/cm, 9 compensated ranges attenuator  
calibrator: 10 V ± 3% voltage reference  
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The world's  
most universal  
audio bridges

# Wayne Kerr's B224 and B642



**The B224 is a manually operated bridge,** the resistive and reactive terms being independently set to a null indicated on the meter. A rechargeable battery is fitted in order to make the instrument portable.



**The B642 balances itself automatically.** The meters read real and quadrature terms and highly stable analogue outputs are provided which are directly proportional to capacitance and conductance above 10Ω impedance and also to inductance and resistance below 10Ω. One or two decades can be set to provide the first significant figures of the measurement, thereby increasing the meter sensitivity by 10 or 100 times. If a chart recorder is connected to the output of either term, drifts in component values to at least four significant figures can be observed.

For more information, write to the address below or phone Bognor Regis (02433) 4501

## WAYNE KERR

Durban Road Bognor Regis  
Sussex PO22 9RL

A member of the Wilmot Breedon group

### SPECIFICATION

	B224 (Manual balance)		B642 (Autobalance)	
Frequency	1592Hz (internal) 200Hz - 50kHz (external)		1592Hz (internal) 200Hz - 20kHz* (external)	
Ranges for specified accuracy				
	0.1%	0.3%	0.1%	0.3%
C	100pF - 10μF	10μF - 10mF	1pF - 10μF	10μF - 10mF
G	1nS - 100mS	100mS - 1kS	10nS - 100mS	100mS - 100S
L	1mH - 10kH	100nH - 1mH	1mH - 10kH	1μH - 1mH
R	10Ω - 1GΩ	1mΩ - 10Ω	10Ω - 100MΩ	10mΩ - 10Ω

NOTE: 0.1% accuracy relates to parallel component measurements above 10Ω impedance. 0.3% accuracy relates to series component measurements below 10Ω impedance.

\*Manual operation only.

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The 'Mastatic' whip-type vertical rod aerial is made to be fixed high above electrical interference.

When it's used with the 'Antistatic' system it returns superb performance in difficult reception areas.

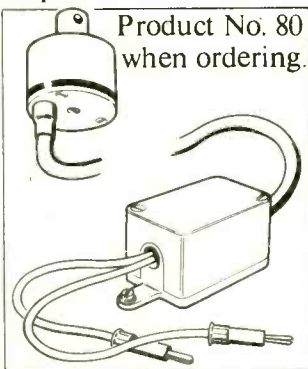
The 'Antistatic' (AM) has a frequency range covering all popular broadcast and short wave bands. It consists of a weatherproofed aerial transformer connected by 60 ft. of screened downlead to a compact receiver transformer.

The 'Mastatic' (AM) comes in three configurations:

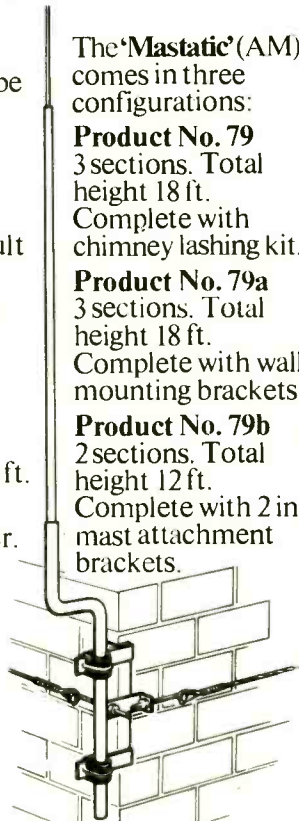
**Product No. 79**  
3 sections. Total height 18 ft. Complete with chimney lashing kit.

**Product No. 79a**  
3 sections. Total height 18 ft. Complete with wall mounting brackets.

**Product No. 79b**  
2 sections. Total height 12 ft. Complete with 2 in. mast attachment brackets.



Product No. 80 when ordering.



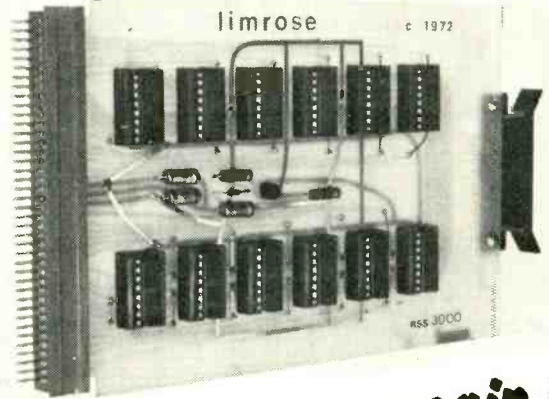
For full information please contact your local Aerialite Distribution Depot or write to:

## Aerialite Aerials Ltd

Radnor Park Trading Estate, West Heath, Congleton, Cheshire CW12 4PX. Telephone: Congleton 3892/8  
Telegrams: Aerialheat, Congleton. Telex: 669640.

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WA14 1PJ, England. Tel. 061-928 8063

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## PORTABLE VHF TRANSCEIVER

# MODEL: TTR-21

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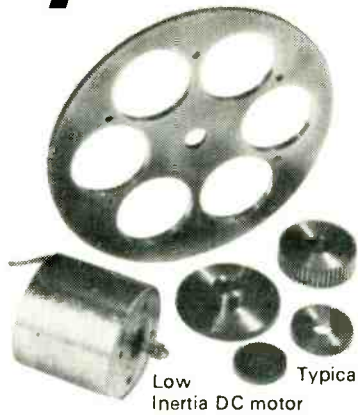
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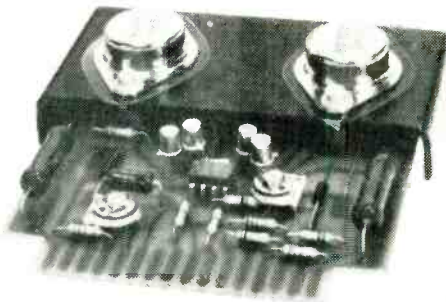


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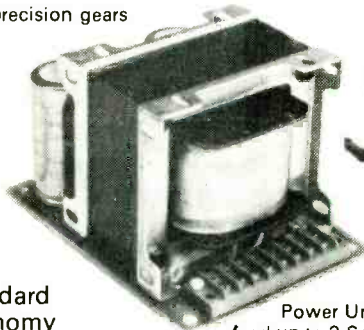


Low Inertia DC motor

Typical precision gears



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Power Unit to feed up to 3 Servos



Gearhead with integral feed-back Potentiometer



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Such a system could be complete in itself or form part of your own design.

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- Camera positioning:
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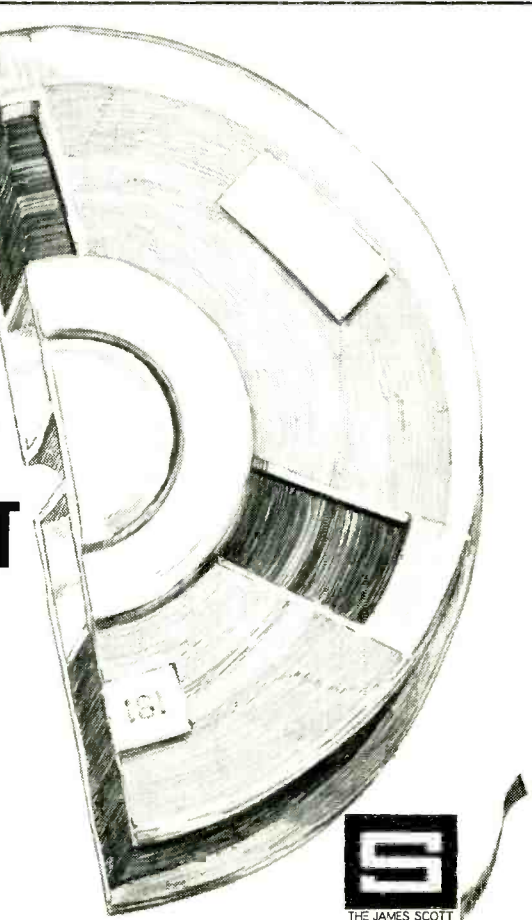
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Pye 7568 range 0.1-1.8V resolution 1 microvolt.	£55
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Tinsley 5205B precision	£65
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+4-18		Ediswan	R2030	£15
0-80C	5	Ediswan	R2030	£29.50
0-8AC	250MA	Ediswan		
2-8.5	500MA	Roband	T98	£12
8.7	10	IE	OS389	£19.50
29	500MA	Roband	T98	£12
9	10	Farnell	S128	£24
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12Twin	1 twin	Constant	K0100	£25
-12	3	Plessey	V3174	£22.50
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-10	4	Lower Elect	SP110	£25
20	4.5	Lower Elect	SP110	£25
+10	300MA	Lower Elect	SP110	£25

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3350C		Farnell	PU335	£10
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0-500	350MA	APT	508	£49
0-500	500MA	APT	512	£49
1000	250MA	APT	7249	£42
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-28V	2			£26
12	2			£26
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28	2.5	Roband	P198	£35
±12	5	Roband	P198	£35
-18	20	Roband	P198	£35
±30	100MA	Roband	P198	£37
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0-30	1	APT	5894	£35
0-30	1	Advantec	PP5	£45
0-30	1	Advantec	PP3	£45
0-30	2	Constant		£38
0-30	3	Solatron	As870	£38
30	7	I.B.M.	210080	£19
37	2	APT	10458/14	£23
25-33	1	Roband	T109	£27
40	6	Advantec	DC188	£27.50
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55-60	1	Roband		£25
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0-500	250MA	APT	505	£35
200-500	350MA	APT	507	£47.50
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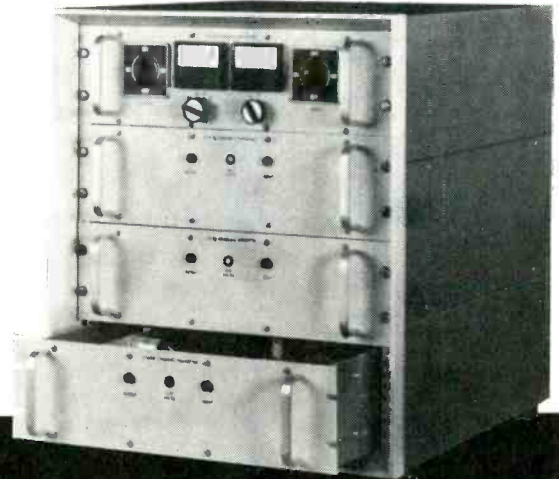
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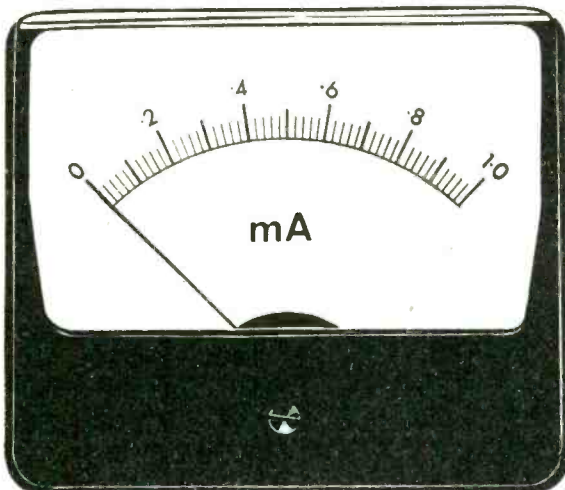
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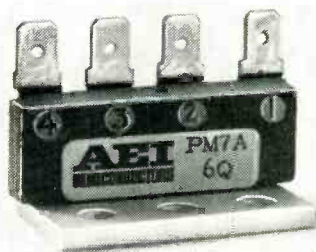
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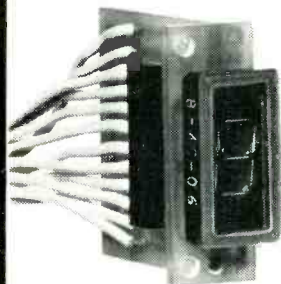
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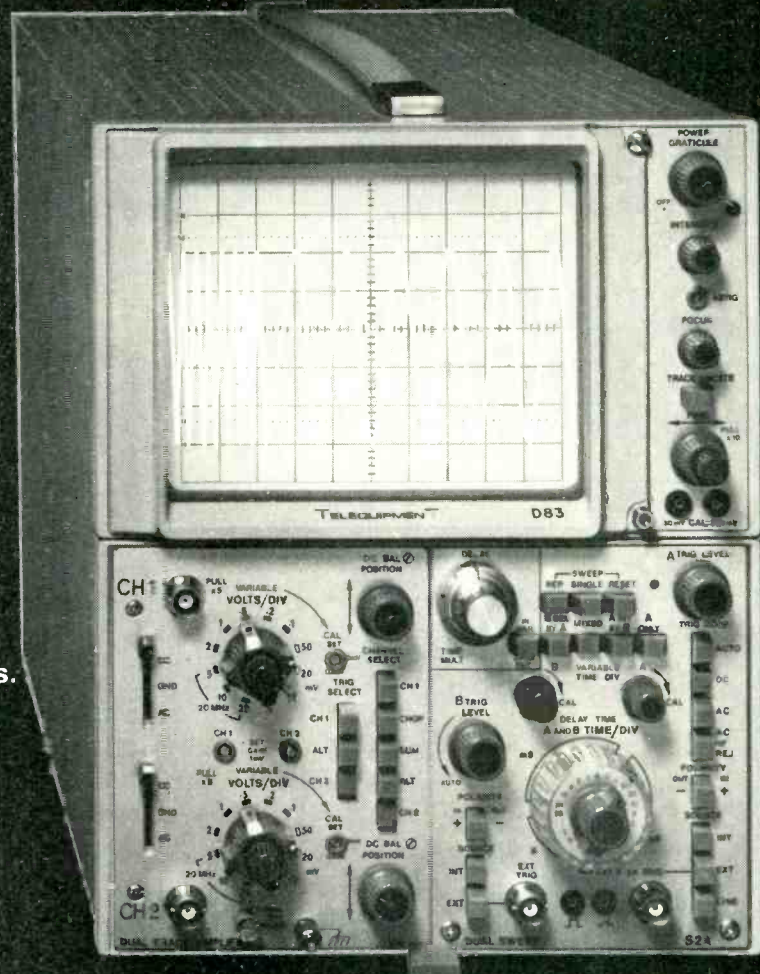
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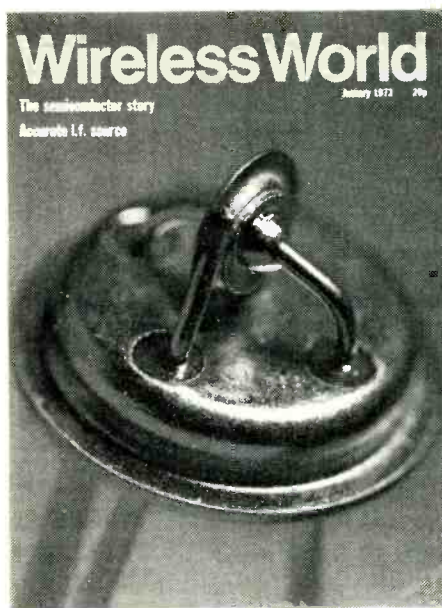
# Wireless World

Electronics, Television, Radio, Audio

Sixty-third year of publication

January 1973

Volume 79 Number 1447



The Newmarket transistor shown on our front cover symbolizes the opening of the semiconductor story which begins in this issue. (photographer Paul Brierley)

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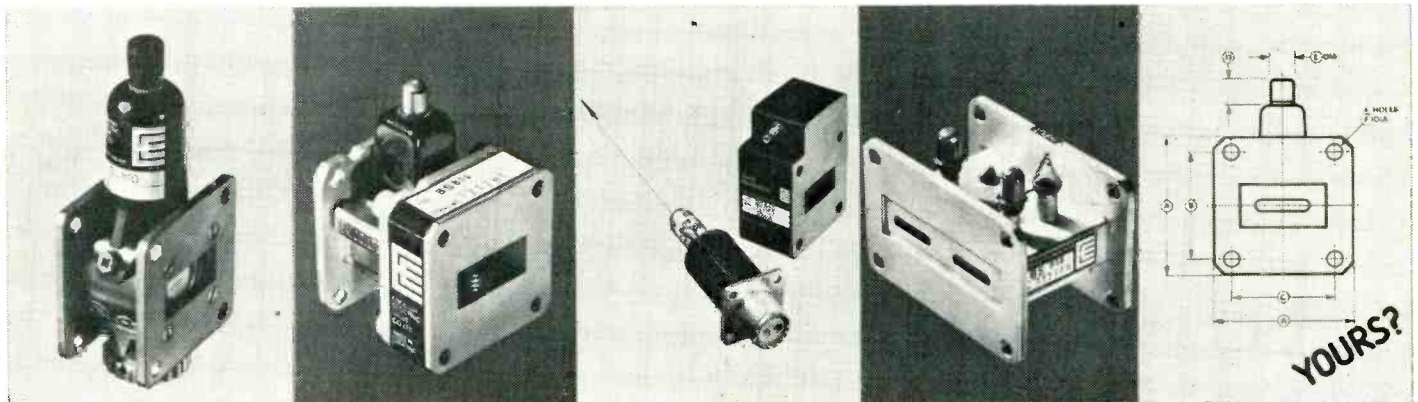
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By the time this issue appears Britain will be a member of the European Economic Community. Inevitably there are misgivings in the minds of many businessmen, engineers and laymen as to the so-called benefits entry into the common market will produce. We have been asked what effect it will have on the contents of *Wireless World*. The simple answer is — editorially, little, if any. We deal with new technologies as and when they are announced irrespective of the place of origin. Moreover, as we write for the individual engineer or technician it matters not whether he is in Asia, Africa, America or Europe. This fact is borne out by our overseas circulation which is in round figures 15,000, of which about 25% is on the Continent.

While entry into the Common Market may not directly affect the contents of the journal it could have major repercussions on this country's electronics industry. With tariff barriers removed, the door for imports into Great Britain will be wide open but the traffic could be two-way if we are ready and prepared to meet the challenge. In a recent contribution on "The future for the British electrical and electronics industry inside the E.E.C." at the I.E.E., Dr F. E. Jones, of Mullard, took a somewhat pessimistic view. This was not entirely because of the Continental threat but in view of the general influx of electronic products. He instanced that during 1972 more colour television sets came into the U.K. from Japan than from the whole Continent — E.E.C. and E.F.T.A.

Dr Jones quoted figures in support of his contention that during the 15 years of the E.E.C. there has not been any major increase in the flow of goods across the frontiers of "the seven". It would appear, therefore, that the British electronics industry has got to go into the market place and sell its wares — entry into the Common Market will not herald the millennium. Our goods must not only be competitive in price but readily available. Here surely is the nub. One of the reasons for the present influx of colour television receivers is because the British radio industry has been unable to meet the demand. The long delay in deliveries has meant that many customers bought imported receivers to ensure having their sets installed for Christmas. A similar story can be told of other sections of the industry.

"It would seem", said Dr Jones "that not much has happened in the 15 years since the formation of the E.E.C. that has been of great benefit to the electrical or electronic industries of Europe in putting them on a more competitive basis with the rest of the world. It would also seem that the full benefits . . . will not be felt until there is a federal government of Europe with a common currency and harmonization of taxes and social systems . . . but this is not in the foreseeable future, if at all."

Another aspect of our entry into the E.E.C. was highlighted by Mr J. E. Engels, chairman of Philips Electrical Industries, in a lecture at the I.E.R.E., incidentally, on the same evening as Dr Jones' I.E.E. lecture (lack of inter-institution consultation?). Mr Engels dealt with the subject of the electronic and radio engineer in the E.E.C., for the treaty of Rome states that member countries will not impede the flow of capital, goods or *people* across national boundaries. He set the scene, as it were, by saying "Universal brotherhood has not suddenly emerged; nor have all national struggles and competition suddenly evaporated. On the contrary, the rules of the game may have changed, but in essence the game is still the same. Within the rules of the Common Market agreements a great struggle is still going on to protect national and industrial interests. In many respects this industrial competitive struggle is more severe than it was before, because there are fewer tariff barriers".

One of the problems involved in the movement of people between countries is the differing standards of technical qualification. It is interesting therefore to learn that a new "super institution" for electrical/electronics engineers in Europe is proposed as a result of a recent convention of the National Electrotechnical Societies of Western Europe held in Zurich. Both the I.E.E. and the I.E.R.E. were represented and we await an official announcement on the outcome.

# The Semiconductor Story

## 1: The new crystal triode

by K. J. Dean\*, M.Sc., Ph.D., and G. White†, M.Phil., B.Sc.

The paper which first announced the discovery of the transistor appeared in the *Physical Review* in July 1948. To commemorate the 25th anniversary of this event, *Wireless World* is publishing a series of four articles presenting a critical survey of the semiconductor industry, past and present, from the U.K. point of view. Part 1 describes the early development of germanium diodes and transistors, while parts 2 and 3 describe respectively the exploitation of the transistor and the integrated circuit to the present day. The final part discusses some of the problems, both technical and commercial, which have faced the industry in recent years. The roles of careful research, happy chance, technical skill and industrial pressure make a fascinating story of our times.

The new crystal triode, as the transistor was first called, seemed in 1948 to be poor competition for the Goliath sized valve manufacturing industry. But a veritable David it turned out to be! *Wireless World* reported the discovery in an article in October 1948, entitled "The Amplifying Crystal". How many people reading that report then realized its implications for the future? The transistor was the end result of research which started 140 years ago in 1833 with Michael Faraday. He noted that while most conductors have a positive temperature coefficient of resistance, a substance called silver sulphide had a negative coefficient. Thus a substance later to be classed as a semiconductor was identified. Rectification, photoconductivity and photo-e.m.f. effects were all observed before 1900. Theoretical work on semiconductors after Faraday's original discovery gathered momentum, so that, by the early 1930s, quantum mechanics was applied to the theory of conduction. Energy band diagrams, electrons and holes then started to be discussed. The stage was set for the discovery in America by J. Bardeen and W. H. Brattain of the transistor—a semiconductor triode. This was the first three-terminal semiconductor device which could amplify, and that was only 25 years ago. Now the impact of the transistor is universal, it has applications ranging from aviation and broadcasting to washing machines and Xerography.

### Cat's whiskers

Semiconductor crystals were used in the early days of radio communications, the crystal rectifier being used as the detector in radio receivers. A typical detector was made by soldering or clamping a minute

piece of the crystal in a small brass cup and the point contact made with a flexible wire called the cat's whisker, which was held in light contact with the crystal. The discovery of the thermionic triode by de Forest in 1907, and its subsequent developments, made the crystal rectifier obsolete in radio receivers. However, the point contact crystal could not be replaced for detecting and monitoring u.h.f. power. At the other end of the scale, at low frequencies, the copper oxide rectifier and selenium rectifier have been commercially successful, but they are however not point contact rectifiers. The rectification property of these is obtained by the contact of a thin film of semiconductor with the metal on which it is deposited. They are therefore termed contact rectifiers.

### Wartime research

The second World War, like all military ventures, provided the cash to oil the wheels of research, so important at times of national emergency. It saw the development of radar, which gave a great impetus to u.h.f. crystal rectifier design. Research was concentrated on using silicon, germanium and boron. Boron prepared with selected impurities, i.e. "doped", showed sufficient conductivity to be of interest, but its typical characteristic curve was S shaped and symmetrical about the origin, thus the project was then dropped. Silicon showed great promise, being used for most of the commercially available devices. At this time the importance of starting with extremely pure silicon was appreciated. The "red-dot" crystal diode developed by the General Electric Company, for example, was derived from silicon crystals prepared from melts made from highly purified silicon powder, to which was added a fraction of a per cent of aluminium and beryllium. The resulting crystal could dissipate relatively large amounts of power without appreciably

impairing its performance as a mixer. These were therefore known as "high-burnout" crystals.

The method of adjusting the cat's whisker at this time is interesting to note. The contact pressure was increased until a pre-determined characteristic was obtained, and the cartridge was then tapped with a light mallet. Careful tapping caused the forward resistance to drop and the reverse resistance to rise. The cartridge was then impregnated with wax to provide mechanical stability and to make it impervious to water. Further work in 1943 led to high purity silicon, doped with only 0.001% boron, which produced an extremely good device and made prolonged tapping unnecessary. The small amount of the impurity needed indicates how material technology had to keep pace with the demands of the semiconductor device manufacturer. At this time, work on germanium led to the high-inverse voltage rectifier; so called because it could withstand up to 100V applied in the reverse direction. The doping agent used was tin, although it was found that similar effects could be obtained with some other elements. Germanium, however, could not compete with silicon above 30MHz. These methods of preparing the germanium crystal and polishing its surface were to be used later in the manufacture of the first transistor.

In 1946 H. Q. North showed that the point-contact used in these devices could be welded to the crystal surface, by passing a high density current (in the order of  $10^7$  amps/sq. in) for a short time through the contact point. Although this did not improve their performance, little was lost either. This technique too was later to be of value in three-terminal point contact devices.

### Post war development

After World War II the immediate problems of survival gave place to the interests of commercial enterprise, and researchers were able to return to more general semiconductor problems, although under industrial patronage. Silicon and germanium were chosen for the research effort, because they are simpler to understand than most other semiconductors. A lot of expertise on these materials had been accumulated during the war, particularly in America. Fig. 1 shows the structure of silicon or germanium crystals. Each atom has four neighbours, all

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at the same distance from it, and all at equal distance from each other. Each atom and one of its neighbours is attached by an electron pair bond, which consists of sharing two electrons to form a stable bond. Each atom has four electrons available to form bonds (valence electrons), therefore the conditions are exactly right for the diamond structure of Fig. 1.

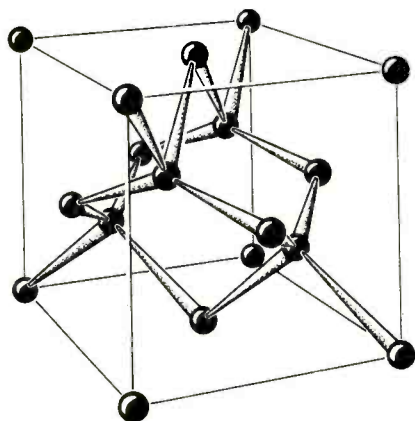


Fig. 1. The crystal structure of germanium and silicon.

The electronic properties are also dependent upon the electrons present in the bonding. By introducing impurities into the crystal the bonding can be modified. Therefore, the electronic properties can be tailored as required by the controlled addition of impurities. The unoccupied bonds on the extreme edge of a perfect crystal cannot be used by internal atoms, but they are capable of accepting electrons. These are called acceptor or surface states. Crystal defects and absorbed foreign atoms will have similar effects and also create surface states. It was the thorough investigation of these states that led to the somewhat accidental discovery of the transistor effect. It is strange that surface states are now something to be avoided in transistor manufacture, because they would provide a low impedance path to current flow that is controlled inside the material.

Amplification using semiconductors was first achieved by using the negative resistance characteristic of thermistors. As the current through the thermistor increased, the heat generated caused a reduction in the resistance, and hence a drop in the voltage. The frequency of operation is limited by the temperature which has to follow the current changes. However, by making the physical dimensions small and the thermal conductivities high, oscillations of up to 100kHz have been produced. Bell Telephone Laboratories' aim after the war was to produce a purely electronic, rather than thermal, semiconductor amplifier. The work was initiated by W. Shockley who directed work on investigating the modulation of the conductance of a thin film of semiconductor. The conductance was controlled by an electric field applied by an electrode insulated from the film. It was hoped that the conductance would be modified by changes

in the surface states caused by the applied field. The experiment gave disappointing results, since only about 10% of the expected change in conductance occurred. The effect was explained by J. Bardeen who in 1947 proposed a double layer at the surface, formed by the charge in the surface states and the induced space charge. Further research was carried out to measure the characteristics of the surface states.

### The transistor discovered

The effect of having the crystal surface immersed in a liquid was studied. The characteristics of a high-inverse voltage germanium rectifier with a field applied by an electrolyte were investigated by J. Bardeen and W. H. Brattain. They proposed that a portion of the current was being carried by holes flowing near the surface. When the electrolyte was replaced with a metal object, transistor action was discovered. The discovery was first published as a short letter to the editor of the *Physical Review* journal in July 1948. This marked the beginning of the transistor era. A more detailed paper was published in the following year.

The transistor is a semiconductor triode amplifier. The prefix "trans" designates the translational property of the device, while the root "istor" classifies it as a circuit element in the same general family with resistor, varistor, and thermistor. The transistor was commercially made in a similar form to the point contact diode, except for a second cat's whisker mounted very close to the first. The device is shown schematically in Fig. 2. A germanium ingot was

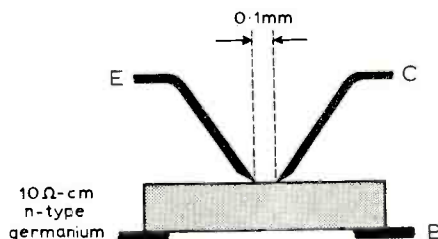


Fig. 2. Schematic of the point contact transistor.

prepared in the same manner as that used for the high inverse voltage diodes, and then a slice of this ingot was ground flat on both sides. The slice was copper-plated and tinned on one side, and diced into small squares with a diamond wheel. One of these squares was then sweated onto the brass base plug and the germanium surface treated. The unit was force fitted into a cylindrical cartridge, which had been shaped to accept the contact assembly. The contacts consisted of two 0.005in phosphor bronze wires, which had been bevelled and polished.

The characteristics of the thermionic diode and the semiconductor diode are fairly similar, and methods of adding a "grid" to control the current in the forward direction as had been achieved with the

triode, were looked at. The transistor, however, is not operated in this quadrant, because the output is reverse biased in the high resistance direction. The current is enhanced and controlled by the forward biased emitter contact. This device was designated the type A transistor to distinguish it from possible future varieties. The transistor effect is the injection of holes into the n-type material by the emitter, which are collected as an increment of the collector current. The common terminal called the base electrode is physically the base of the crystal. Devices which operate on different principles, such as the field effect, have since been called transistors. Therefore, transistor electronics is used generally to describe the art of controlling electron movements in a solid, hence is sometimes called solid state electronics. One of the first point contact transistors to be manufactured in the United Kingdom is illustrated. The patent numbers



The G.E.C. crystal triode type GET 1, one of the earliest point contact transistors to be made in the U.K. The reverse of the packet, shown here with the transistor, carried a warning "To prevent permanent damage to the triode, it is recommended that whenever possible d.c. limiter resistors be placed in series with both emitter and collector . . . Great care should always be taken to connect supplies of the correct polarity to the electrodes."

show the advantage of a strong development facility, by using experience gained in the construction of point contact diodes to help in the manufacture of transistors. Patent number 591092, which was applied for in 1945, describes a method for holding the contact in place after construction. This is achieved by filling the cartridge with a wax-like substance which will harden on heating. The other patent number, 592659, was applied for in 1941, and deals with the preparation of the crystal and the subsequent treatment of its surface. The germanium had to have a spectroscopic purity of 99.95% for good results.

### Transistor amplifiers

The journal *Audio Engineering* published an article in August 1948 entitled "Experimental Germanium Crystal Amplifier", only one month after Bardeen and Brattain's original letter. This described how to construct a germanium crystal amplifier—such was the rate of progress even in 1948. The

article highlights the similarity between point contact diodes and the type A transistor because the construction starts with two diodes. They are dismantled and the crystal used, with the two whisks carefully adjusted on the surface. Difficulty was experienced in finding active spots, due to the relatively impure crystals being used at that time. Manufacturers were aware of the need for high quality germanium. In 1946 the first extraction plant in the United Kingdom was built at Brimsdown for Johnson Matthey for the bulk production of germanium and other semiconductor materials.

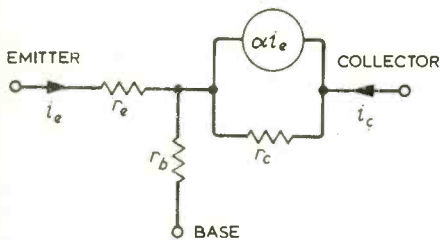


Fig. 3. Equivalent Tee circuit of a transistor.

The type A transistor can be represented by the equivalent circuit shown in Fig. 3, with the following average values for its parameters:

emitter resistance	$r_e = 240\Omega$
base resistance	$r_b = 290\Omega$
collector resistance	$r_c = 19,000\Omega$
amplification factor	$\alpha = 1.8$

Unfortunately the active area of the device is very small and hence the collector dissipation is only about 0.2W, although a power gain of 17dB with a power output of 5mW was achieved. The small size of the device, however, gives it a wide frequency response, with an upper limit of approximately 10MHz. It was soon noted that the transistor could be greatly improved by passing large reverse currents through the collector point. This technique, called forming, resulted in amplification factors as high as 5. This process was explained by the formation of a p-n hook at the collector which reduced the height of the potential energy hill at the collector, so allowing a considerable increase in the number of electrons diffusing from the collector into the floating p region.

The movement of holes was thought to be mainly confined to the surface region but in 1949 J. N. Shive proved that the flow of charges could be through the bulk of the material. This was shown by constructing the double surface transistor, which was produced with germanium in the shape of an acutely tapered wedge, the two contacts being opposite each other near the thin edge. This transistor was developed into the coaxial transistor which was much easier to manufacture. Here the germanium was cut into a pill shaped cylindrical wafer with a dimple ground into the centre of both sides, so that the thickness of the centre was only a few thousandths of an inch. The emitter

and collector contacts then bear on opposite sides of the semiconductor in the dimples, and are arranged coaxially to fit into a cartridge. This method of construction avoided the problem of placing two spring contacts within a few thousandths of an inch of one another. The components used were similar to the parts used in the manufacture of point-contact rectifiers.

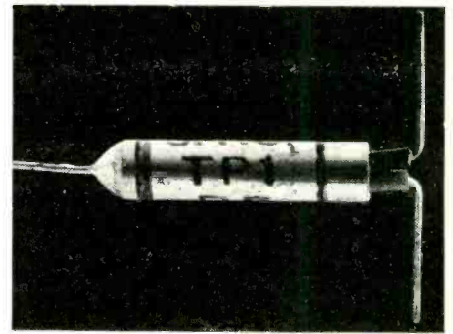
### Junction transistors

In 1949 W. Shockley proposed that transistor action could be achieved with p-n junctions within a single crystal, thus breaking away completely from the surface effects of point contact devices. The device was therefore called a junction transistor. In principle it consisted of a bar of single crystal n-type germanium, for an n-p-n device. In the centre of the bar was formed a thin layer of p type germanium as part of the single crystal. Ohmic non-rectifying contacts were attached to each of the three regions, the outer two being the collector and emitter and the centre the base. The method of operation is essentially the same as the point contact, hence the electrodes have the same names, although the base is now in the middle. The equivalent circuit chosen for comparison is the same one as used for the point contact i.e. Fig 3; the new values for the parameters are:

$r_e = 25\Omega$
$r_b = 250\Omega$
$r_c = 5 \times 10^6\Omega$
$\alpha = 0.95$

The amplification factor  $\alpha$  for junction transistors is less than unity, hence the amplification in common-base operation is due to the difference in impedance levels. A junction transistor was developed with a p-n hook collector, which acted similarly to the point contact transistor as far as the gain was concerned. This was achieved by a four-layer p-n-p-n device, but the transistor had a poor high-frequency response. Little further work was carried out, even though high amplification factors were obtained.

The first junction transistors were a great improvement over the point contact devices. Power gains of 40dB, with class A operation of 49% efficiency were achieved against 23dB gain and an efficiency of 30% for point contact transistors. The higher power gain is due to the increase in the output impedance, and the almost ideal characteristics show that the junction transistor can operate close to the 50% maximum for a class A amplifier. Junction transistors will operate with extremely low input power of around  $0.6\mu\text{W}$ . This is about one thousandth of the power required to operate the point contact transistor, or one millionth of the power to heat the cathode of a typical thermionic valve. Unfortunately the frequency of operation at that time was limited to about 1MHz. This was due to the time taken for the charge carriers to diffuse across the base. The equivalent effect in thermionic valves is the transit time, that is, the time taken by the electrons to travel from the cathode to the anode. The type of case used by S.T.C. for an early junction



The S.T.C. point contact transistor TP1 appeared about the same time as the G.E.C. GET 1. It was soon withdrawn and replaced by the TS 1, a junction transistor.

transistor is shown in the photograph. Although the TP1 device shown was a point contact transistor, it was made at the same time, and externally looks identical to the TS1 junction transistor.

Several methods have been used to improve the high-frequency response of junction transistors. The most obvious answer is to reduce the base width; this is limited, however, by the problem of punch through. A second contact added to the base by Wallace *et al* in 1952 effectively reduced the base area and the base resistance. This increased the cut-off frequency to about 50MHz. Further improvements were realized by advances in material technology, in particular by the diffusion process which started in 1952, and by the production of extremely pure silicon. The purification was achieved by zone refining. This process is based upon the relatively high rate of diffusion of impurities in the molten zone of a crystal, compared with the much slower rate in the solidification zone. The raw single crystal is passed slowly through a localized radio-frequency heating coil. The crystal within the coil is in the molten state, and on passing through the coil re-solidifies into a single crystal again. The impurities tend to remain in the molten region and therefore are swept to the end of the crystal. The process is repeated several times. The end with the impurities is discarded and the concentration of impurities in the main section can be reduced to about  $10^{17}$  atoms/cu.m.

### Field effect

The field effect transistor experiments that failed were the beginning for the point contact and junction transistors. In 1952 W. Shockley proposed a unipolar field effect transistor which overcame the earlier problems of surface states. The point contact and junction transistors are called bipolar because charge carriers of both signs are involved. In the field effect the controlled conductance between input and output terminals results from changes in the number of carriers of one type, hence the name unipolar. The field effect transistor has several advantages, the most important being the high input impedance. The input is a reverse biased p-n junction, and the depletion layers created control the conductance through the channel. The difference in operation is reflected in the

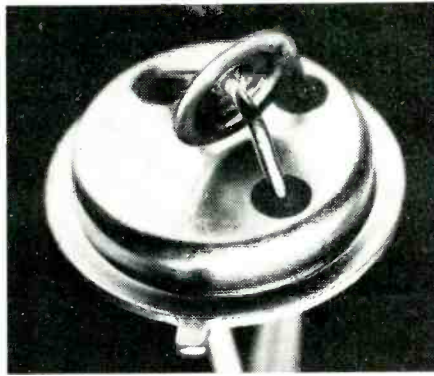


names for the electrodes, the emitter and collector being called the source and drain respectively. The controlling electrode is now called the gate instead of the base. It was not until fairly recently that the technology needed to be able to mass produce these devices has been developed. In the meantime the junction transistor has built up a commanding lead.

### Circuit design

Early work on transistor circuit design tended to start with a well tried thermionic valve circuit, and then modify it for use with transistors, even though the parameters are radically different. The grounded cathode triode is a voltage amplifying device with a high input impedance and a relatively low output impedance. Conversely the grounded base transistor is a current amplifier with a low input impedance and a relatively high output impedance. The early papers on transistor circuit design referred to the transistor's characteristics as peculiar, because they were different to those of a valve. On looking further at the parameters, it was noted that, if the roles of current and voltage were changed over, the devices were similar enough for quantitative designs starting from the valve circuits. This background led to the circuit performance of transistors being less than they might have been, until designers began to take account of the transistor's peculiarities and use them to advantage. One of the major advantages which would be unheard of with valves is the use of complementary circuitry, allowed by having n-p-n and p-n-p transistors.

The small size and ruggedness of transistors opened new fields and their small power requirements meant that the components used with them could be miniaturized also. The type A transistor of 1949 occupied one-fiftieth of a cubic inch, with a collector voltage of 30V. In 1952 the junction transistor could be fitted into one five-hundredth of a cubic inch with a collector voltage of 2V. Bell Telephone Laboratories studied the problem of manufacturing complete circuit packages under an American Signal Corps contract in 1952. At that time the package of a laboratory circuit model required about one-tenth the space



*A modern germanium alloy junction transistor still in production at Newmarket Transistors. The emitter lead is in the foreground and the base lead at the right connects to a metal disc in which the semiconductor pellet is held.*

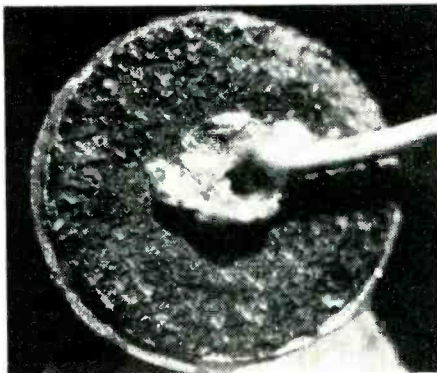
and power of an equivalent package built with thermionic valves. The importance of designing sub-sections of a system, which would be used in quantity, and manufacturing them as packages was realized from the beginning of the transistor's development, and has been a goal ever since.

The general manufacture of transistors began in 1952, after Bell Telephone Labs. held a symposium, where they offered know-how to all who wanted it for the price of an admission ticket (\$25,000). The era of the practical transistor had now begun. Photographs show the construction of an early alloy junction and the progress achieved since then by comparison with a modern alloy junction transistor. The successive developments to improve the parameters and to find transistor structures, which lend themselves to easier manufacture are related in part 2 "The search for the best transistor". The originators of transistor electronics, J. Bardeen, W. H. Brattain and W. Shockley were awarded the Nobel prize for physics in 1956 in recognition of their work in the theory of semiconductors, when it was beginning to be recognized that they had not just invented the transistor, but had laid the foundations of the world-wide multi-million pound microelectronics industry.

(To be continued)

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*A photomicrograph of an early medium power germanium alloy junction transistor. The pellet of impurity and the emitter lead connected to it are clearly shown in the centre of the picture.*

## Sixty Years Ago

An uneasiness in the Marconi Company when share prices fell considerably is reflected in a statement issued by the company and reproduced in the January 1913 issue of *The Marconigraph*. It referred to opinions which had been expressed suggesting that "continuous waves would in the future supersede the spark system". The announcement from the secretary of the company continued "As these statements and opinions are liable to mislead shareholders and cause them some uneasiness, I am instructed to inform you that Mr. Marconi himself tested continuous wave systems many years ago, and experimented with them during the greater part of 1907 at the Poldhu station. As a result of these experiments he learned the advantages and disadvantages pertaining to continuous waves, and eventually arrived at a compromise between the continuous wave and spark systems, combining the best points of both. This resulted in material changes in his system for long distance work, and new and important improvements were patented by him in 1907, which are mainly responsible for the progress since made in long-distance wireless telegraphy. These inventions, which materially modify the spark system, seem to be surprisingly little known, notwithstanding the lectures delivered by Mr. Marconi . . . . . when he made statements relating to the use he was making of continuous waves, semi-continuous waves and the elimination of the spark."

### Corrections

L. Nelson Jones, author of the article "I.C. Peak Programme Meter" in the November 1972 issue, has informed us of an error in the specification of the meter. The scale marking division seven represents a level of +12dBm (not 14dBm) with a peak input voltage of 4.38V. The undefined f.s.d. reading usually corresponds to around 5.37V peak. This calibration fault is easily corrected by changing the value of  $R_{14}$  to 100k $\Omega$ , and Key Electronics, suppliers of the kit, are sending all those who have kits, a replacement resistor together with a copy of the amended handbook.

We regret an error exists in the circuit diagram (Fig. 1) of the "Mobile/Portable Power Unit for H.F. Transceiver" published in our December issue. The conductor between the base terminal of transistor  $Tr_2$  and ground should be omitted otherwise the catastrophic failure of this device will occur.



# News of the Month

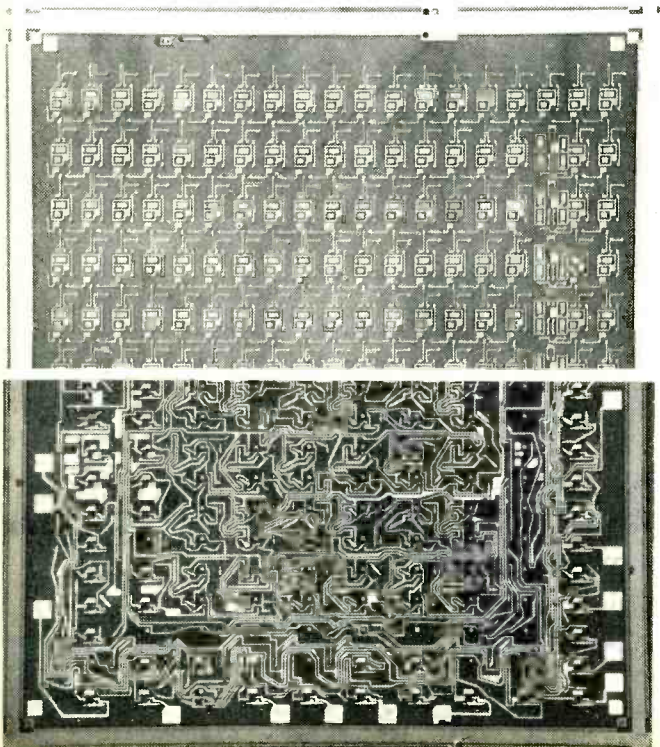
## New i.c. concept

The development of integrated circuits from the first small devices to the latest l.s.i. techniques has been recorded in the pages of this journal over the past few years, and now Ferranti have added to the extensive range of application techniques available to the designer. In 1969 an announcement was made concerning a new process called collector diffusion isolation (c.d.i.), a technique using bipolar devices and an isolation technique based on the diffusion of isolation areas in a p-type substrate. First discovered by Murphy and Glinski of Bell Laboratories and reported in *Wireless World*, Nov. '71 issue, it has significant advantages over m.o.s. since only five masking operations are required. A typical cross-section of a c.d.i. structure reveals two more significant features. First the power and earth connections are made through the semiconductor material itself, thus eliminating the need for multi-layer aluminization to provide for these connections, and second, all signal connections can be made in the single final layer of metal.

Such a structure lends itself ideally to

the new concept from Ferranti; that of an "uncommitted" logic array (u.l.a.) which is illustrated in the top half of the accompanying split photograph. The u.l.a. consists of 200 bipolar devices without the final metal connecting layer. From this a custom-built i.c. can be produced quickly and cheaply by adding an aluminium connecting layer to suit any logic design requirement. By standardizing the type and number of resistive elements and leaving these also in an uncommitted state, simple linear circuits can be additionally devised, thus giving greater versatility. An example of the appearance of the u.l.a. after the metal layer is applied is shown in the bottom section of the photograph. The technique is very much cheaper for short production runs than l.s.i., though if the demand should rise unexpectedly for any particular unit, it becomes a very simple matter to convert to conventional l.s.i. techniques. For about £1250 Ferranti can undertake to produce five tested prototype samples to a customer's own logic requirements, full production prices being from £12 to £20 dependent upon quantity. The value of this system lies in the fact

*Logic array shown in an uncommitted format (top) and after the final metal array has been added.*



that u.l.a. slices can be stockpiled and small quantity runs below 100 readily produced at economical prices. Applications are seen in coin vending machines and automatic machine control among a variety of others. The final package can be made available in 24, 28 or 40 pin moulded or ceramic d.i.l.

## Etching solution controls i.c. windows

A solution to control the etching angle and depth of deeply etched areas in silicon wafers, has been developed by Bell-Northern, of Ottawa, Canada. Silicon wafers form the base material for most integrated circuits and normally the etched bottom is flat or slightly concave and the cross-section is often enlarged or cut away by lateral undercutting of the mask. With the new etching solution the sides of the etched "window" or "well" are substantially straight and normal to the surface of the main body of material. In addition, the profile of the bottom of the etched area can be varied from slightly convex to a situation in which the edges are etched into deep grooves, while limited etching occurs in the central portion, depending on the etchant composition. By varying the amount of arsenic trioxide in the etching solution (refluxing orthophosphoric acid), the preferential etching can be varied considerably. Increasing slightly the quantity of trioxide will change the profile from concave to a centre "island" surrounded by deep grooves. At a certain point of concentration, the solution starts to leave the surface pitted and preferential etching substantially disappears.

The deep grooving effect would lend itself to electrical isolation since grooves can be etched down to a p-type layer through an n-type epitaxial silicon layer. One of the advantages is that the wall goes down straight regardless of the crystal orientation of the silicon. Oxidation of the silicon wafer after the preferential edge etch results in the grooves being completely filled with silicon dioxide and hence provides dielectric isolation of adjacent devices.

## Components Board reorganized

The Electronic Components Board is being reorganized and, with effect from 1st January, the constituent associations responsible for active electronic components cease to exist as separate entities. The two Groups of VASCA,\* covering professional valves and tubes and semiconductor devices, become product groups of the new organization, and a

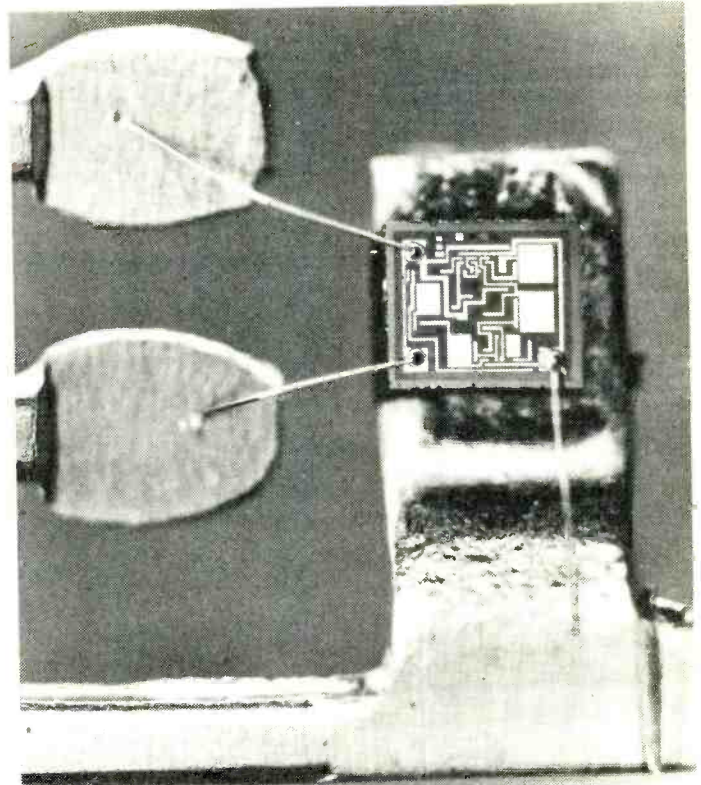


third product group will be responsible for domestic valves and television tubes, taking over the function of the B.V.A.† There will be two categories of members, (a) direct members, being companies engaged in the U.K. in the manufacture and sale of electronic components, and who are approved by the council of the Board, who will pay a subscription direct to the E.C.B. and (b) corporate members, who will be members of the Radio and Electronic Component Manufacturers' Federation, which will pay a block subscription to the E.C.B. on their behalf. The R.E.C.M.F. will therefore continue as a separate autonomous but affiliated, organization. The recently appointed chairman of the E.C.B. is Sir Ronald Melville.

·Electronic Valve & Semi-conductor Manufacturers' Association.

†British Radio Valve Manufacturers' Association.

*Latest Ferranti c.d.i. chip, type ZN414 pictured here can be used as the basis for a simple t.r.f. receiver. Circuit shown provides 70dB of power gain, consumes 1mA and with 30% modulation has a distortion of 2%. The collector diffusion isolation process developed by Ferranti is a bipolar technique, which also has the low-cost production advantage of m.o.s. i.c.s — see page 526 November 1971 issue.*



## London Component Show

Space applied for at the London Electronic Component Show to be held at Olympia, for four days from 22-25 May this year, already accounts for two-thirds of the total space available. The number of companies from whom applications have been received to date is approximately 300. Providing an indication of the wide appeal of the show is the number of exhibitors, at present totalling over 60, who will be making their first appearance at the show. Overseas representation to date, approximately 20% of all intending participants, includes exhibitors from Austria, Canada, France, West Germany, Holland, Hungary, Italy, Switzerland and U.S.A. and the U.S.S.R.

The 1973 show will be the 23rd in the series and the third since it went international. As the first major United Kingdom professional electronics exhibition to be held after the formation of the expanded European Economic Community, this event should play a major part in stimulating and consolidating overseas trade. The London Electronic Component

Show is sponsored by the Radio and Electronic Component Manufacturers' Federation and is organized by Industrial Exhibitions Ltd.

## Thin film laser switch

A light switch for use with lasers has been devised by Bell Laboratories scientists. The switch may be useful in future tiny optical circuits for placing phone calls and other information on a laser beam, capable of carrying many times more information than the present transmission media, such as wire conductors, coaxial cable and microwave radio links.

The magnetically controlled switch, which can modulate light passing through a thin, single-crystal garnet film, could form the heart of a miniature circuit in an

optical communication system. The light switch measures about  $\frac{1}{4}$ in across in its present experimental form, but could be made even smaller. The main components of the switch are a magnetic thin film of single crystal garnet through which the light is guided, and a tiny electric circuit used to impose the required information on the light beam. When a minute current is passed through the circuit a magnetic field is produced which causes the light beam in the film to change its polarization and hence the direction in which the light is refracted as it is coupled out of the film by means of a prism. Information can be impressed or coded on the light beam by switching the beam in or out of its original path in a controlled pattern of light pulses.

*Two videophones have been incorporated in the communal aerial television system installed at the Teleng factory in South Ockendon.*



## Super heat conductors for i.c.s

The principle of heat pipe operation has been known for a long time but only recently have production problems been overcome, resulting in a variety of forms and applications. Jermyn Manufacturing have introduced a range of super heat pipes, plates and strips all working on the heat pipe principle. When one end of the pipe is heated, a fluid in the pipe evaporates and travels along the tube to its cooler end. There it condenses (giving up its heat to a suitable heat dissipator, such as a heat sink attached to the pipe) and the condensate returns to the hot end of the pipe by capillary action. A cyclic process is thus set-up, which will continue as long as there is a small temperature gradient between the ends of the pipe. This process

is efficient, with a temperature gradient down the pipe of 2.5°C per foot. The main manufacturing problem has been the extreme cleanliness necessary in fitting an internal fine mesh "wick" to produce the capillary action. Super heat plates, strips, sinks etc, all operate in exactly the same way. A heat plate for example may be considered as a heat pipe squashed flat. The result of this is a tendency to equalize the temperature of the whole area of the plate (the temperature gradient across its surface not exceeding 0.5°C). An interesting application of this high-efficiency heat radiator has been made by Jermyn, who are producing flat, thin strips of heat conductors on which arrays of integrated circuits can lie to ensure uniform operating temperature of all the devices.

## Europe's first geostationary satellite

A group of major European companies, the Star Consortium, led by British Aircraft Corporation Electronic and Space Systems, has been awarded a new satellite contract by the European Space Research Organization following two years of competitive studies. The contract, worth £254,000, is for the detailed definition study of GEOS, Europe's first geostationary satellite. The study will last three months, and lead to the award of the main development contract to the Star Consortium. B.A.C. is the prime contractor. GEOS is programmed for launch in 1976, when it will carry scientific experiments into geostationary

Earth orbit 22,300 miles above the equator to measure d.c. and a.c. electric and magnetic fields and also particle densities and distributions.

## Giant mobile transmitting and receiving mast

One of the problems associated with outside broadcasting is beaming signals clear of local obstructions. To cope with this problem, Eagle Engineering, of Warwick, have designed two 100ft masts to meet requirements made by the B.B.C. The masts are for use mainly in the London region and are the tallest mobile units in the U.K. suitable for microwave link. Each mast is in four telescoping sections. The lower pair are extended by the action of a hydraulic ram, the upper pair by means of a system of differential cables and pulleys. With two 4ft diameter microwave dish aeriels and associated transmitters mounted on the masts — without the use of guy cables — the maximum safe operational wind speed has been shown to be in the order of 35-40 m.p.h.

## Transmitters for independent radio stations

The first group of independent local radio stations recently announced by the Independent Broadcasting Authority is to

go on the air with transmitters of standard design. The order, placed with Marconi's, is for the supply of a total of .47 transmitters; eight pairs of 1kW v.h.f./f.m. and 21 1kW m.f. units, two 125W v.h.f./f.m. pairs and six 10kW m.f. equipments. All the transmitters are standard Marconi units and those operating in pairs will have automatic changeover facilities. From the first consideration of the commercial broadcasting network, both m.f. and v.h.f. coverage were considered essential, and all five of the designated new stations will broadcast simultaneously on v.h.f. and medium frequencies. An eventual total of 60 independent radio stations will cover an estimated 75% of the population of the country.

## International Apprentice Competition

The United Kingdom will be sending a team of craft apprentices to the International Apprentice Competition in Munich during August 1973. Among the crafts represented in the British team will be industrial electronics and television servicing. The U.K. Steering Committee is now accepting entries for the initial selection competitions. Enquiries and application forms for entry may be obtained from Mr. C. A. Thompson, City of Bath Technical College, James Street West, Bath BA1 1UP. There is a £10 entrance fee for each initial selection competitor.

## A.P.A.E. annual exhibition

The annual exhibition of the Association of Public Address Engineers is to be held at the Bloomsbury Centre Hotel from 13-15th March. It opens on the Tuesday morning at 12.30 and closes at 6.00 p.m. On subsequent days the doors open at 10.00 a.m. This year is the 25th anniversary of the A.P.A.E. and a number of historical exhibits will be shown from the Association's collection. Lectures will be given at intervals in the City room. Tickets are available free of charge from exhibitors or the secretariat, 6 Conduit St., London W1R 9TG.

## B.B.C. exhibition

A final "news-worthy" note is that well over 65,000 people visited the technical exhibition staged at Mullard House, London, to commemorate the B.B.C.'s 50th anniversary.

## B.B.C. local radio transmitting stations

The following table lists transmitting frequencies, radiated power and polarization of the B.B.C. m.f. and v.h.f. local radio transmitting stations. Powers marked with an asterisk are to be increased at a later date and the carriers of several v.h.f. stations will change during the next few months, as indicated in the last column. In addition, the m.f. services at Derby and Nottingham will open later, as will the v.h.f. and m.f. service of Radio Carlisle.

Station	Metres	m.f.		v.h.f.			
		MHz	kW	MHz	kW	Poln.	MHz (later)
Birmingham	206	1.457	1*	95.6	5.5	H	
Blackburn	351	0.854	1*	96.4	1.5	S	
Brighton	202	1.484	1	95.8	0.5	H	95.3
Bristol	194	1.546	2	95.4	5.0	H	95.5
Carlisle	397	0.755	—	95.6	5.0	H	
Derby	271	1.115	—	96.5	5.5	S	
Humberside	202	1.484	2	95.3	4.5	H	96.9
Leeds	271	1.106	1	94.6	0.14	H	92.4
Leicester	188	1.594	0.5	95.2	0.3	S	95.1
London	206	1.457	20	95.3	16.5	H	94.9
Manchester	206	1.457	1*	95.1	4.0	S	
Medway	290	1.034	1	97.0	5.5	H	96.7
Merseyside	202	1.484	2	95.8	5.0	H	
Newcastle	206	1.457	2	95.4	3.5	H	
Nottingham	197	1.520	0.5	94.8	0.3	S	95.4
Oxford	202	1.484	0.5*	95.0	4.5	H	95.2
Rotherham	—	—	—	95.05	0.01	H	
Sheffield	290	1.034	1	88.6	0.03	H	97.4
Solent	301	0.998	1	96.1	5.0	H	
Stoke-on-Trent	200	1.502	1	94.6	2.5	H	96.1
Teesside	194	1.546	0.25	96.6	5.0	H	

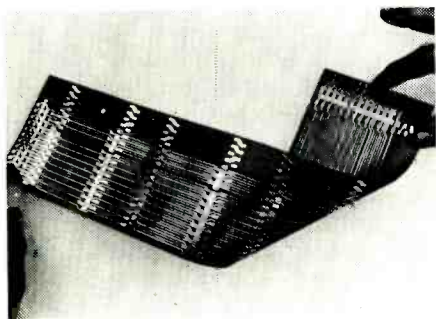


# Electronica in Retrospect

## An impression of this biennial exhibition

After 63,000 visitors had visited the seven-day exhibition of the international electronic components industry, held at Munich in November, it closed and was voted a great success by most who participated. Held biennially, each event has been a little larger, a little better. The variety of products shown makes it difficult to select any particular aspect, but probably one of the most visually striking was the increasingly important part that light is playing in all areas of electronics. Evidence of this was seen on such stands as Jena Glaswerk Schott & Gen and Corning Glass, who were displaying a range of optical glasses and, more importantly, several examples of fibre optic applications. Light-emitting diodes were very much in the forefront of many of the semiconductor manufacturers' product displays and these appeared in a variety of colours from the commonly available red to yellow and green.

Plessey, who were strongly represented in a large and elegant stand, were demonstrating a high brightness yellow l.e.d. generating  $34,000 \text{ cd/m}^2$  at a current of 250mA. Ferranti, showing products in two of the halls, were demonstrating their own expertise in producing green and red emitting GaP material ready for packaging into individual lamps or segment displays. Other examples of the use of l.e.ds were to be found on the Siemens and Texas Instruments stands where a range of opto-electronic couplers, consisting of an l.e.d. and a photo-transistor sealed in a



Typical of a large number of printed circuit types was this flexible version produced by Schoeller & Co. Elektronik GmbH.

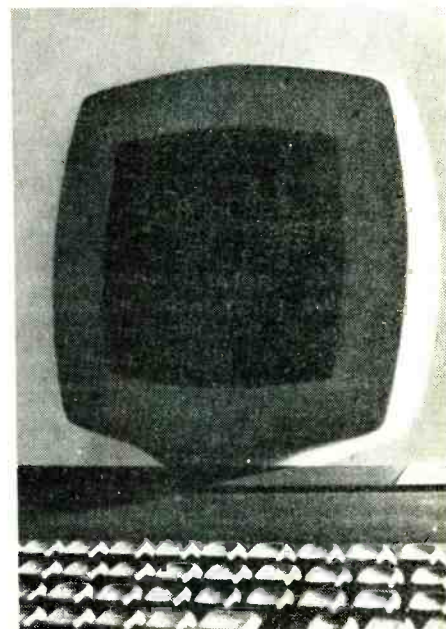
common package, were shown. These devices find common application where a degree of isolation is required between t.t.l. systems and the ground potentials, or to drive s.c.r.s controlling power machinery. Another interesting application is inclusion of opto-isolators in the feedback elements of a switching mode power supply, where error signals can be safely returned to the early stages of the control unit which may be affected by fluctuations originating in the mains supply.

Several stands featured displays of laser equipment, much being designed for educational experimental purposes. An interesting application demonstrated by Spindler and Hoyer KG was the use of an optical laser measuring bench for improving the definition of electron microscope photographs. This idea involves the illumination of a transparency by a coherent light beam from a laser; the transmitted light then undergoes an optical Fourier transform followed by spot frequency filtering and a second transform to reconstitute the image. By selection of the spot frequency filters, definition of any particular aspect of the original picture can be improved.

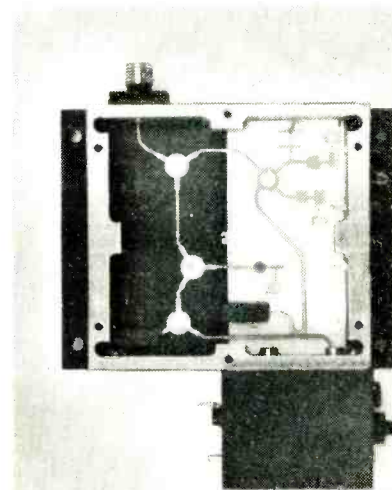
### Larger display units

A flat panel display unit shown on the Thomson-CSF stand attracted considerable interest, as did several other products from this company. Called the Pavane panel, it is available in three principal forms – as a high resolution display with 400 points per square centimetre (illustrated) and suitable to accommodate from 200 to 2000 characters, or in a semi-transparent form with a rear face available for the superimposition of projected images, or in a two- or three-colour unit of medium resolution. Having a high writing speed and digital X-Y access, the panel is also suitable for two-way computer "dialogue" with a light or electric pen.

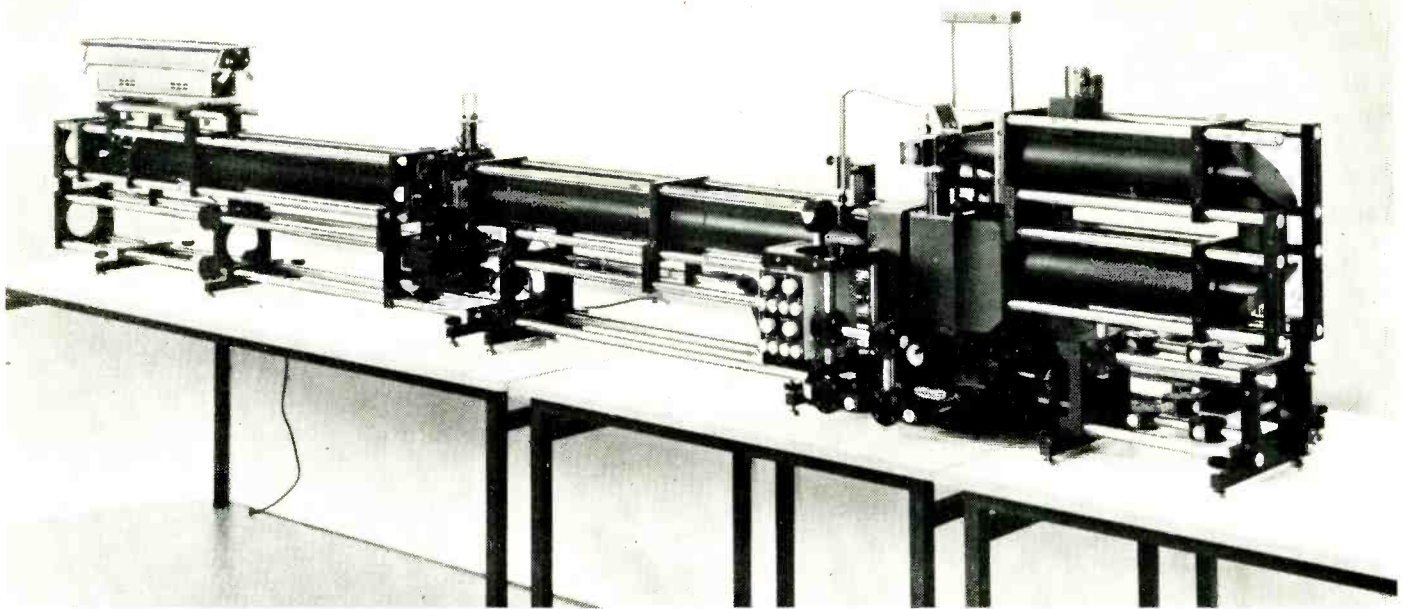
Also shown on the stand was a novel display tube with what is called a multi-colour penetration screen. Since the resolution and brilliance of conventional shadow mask tubes are somewhat limited for instrumentation applications, a new technique has been developed where three layers of material are coated on the inside of the tube face. These consist of two



An example of the Pavane panel used as a computer terminal readout device.



Typical of the new ideas in microwave integrated circuits shown at the Fair was this example from MESL.



*The laser optical measuring bench made by Spindler & Hoyer*

separate fluorescing phosphors of either a different colour or different persistence, separated by a barrier layer. Low energy electrons of about 9keV excite the first phosphor but are prevented from further penetration by the barrier. Higher energy electrons (17keV) will penetrate the barrier to excite the second phosphor. Using red and green phosphors, a range of colours including orange and yellow can be produced with intermediate beam energy. Tubes of this type are now being made up to a 19in size in a variety of screen coatings. A similar product was exhibited by the M-O Valve Company on the joint EEV and M-OV stand.

#### **Liquid crystal display**

Finally on the subject of visual display, liquid crystals appeared in several units shown around the exhibition. Notable examples were those manufactured by the joint company of Swarowski-AMI and also by Electrovac. The last-mentioned company markets the cells under the brand name Nemocell and provides two versions enabling transmitted or reflected light to be utilized. With an operating voltage of 15 to 50V and a digit height of 12mm, applications can be seen in channel number displays for television sets, digital clocks and other units where large alpha-numeric displays are desirable.

Although test instruments were not considered to be part of the components exhibition, at least one complete oscilloscope, of rather novel design, was exhibited. Made by the American company Nicolet Instrument Corporation, it is called a digital oscilloscope. Essentially it is a low-frequency storage oscilloscope making use of a non-volatile digital memory. The advantage of this form of storage is that it eliminates the danger of difficult focus or brightness settings causing potential phosphor burning, and the signal resolution is extended to one part in 4096. An X-Y plotter output is available, giving the extra



*The Ferranti Feedraft used to automatically generate p.c. masters, i.c. masks and other drawings.*

facility of a permanent trace of the stored signal and an additional alpha numeric display on the screen together with a crosshair marker gives the time and voltage co-ordinates at the intersection.

Applications for integrated photodiodes were to be seen on two stands, those of the British company IPL Ltd and Ing. Erich Sommer, a distributor for Reticon Corporation of America. On both the diode arrays were being used to meet a number of needs including component measurement to fine limits and also a possible use in facsimile transmission. The IPL unit was made up as a line scan camera system consisting of a self scanned diode array mounted behind a custom lens assembly. A second unit called

the driver and recharge signal processor unit couples to the camera and the only other requirement is for a d.c. supply. Arrays of 50 to 256 photodiodes can be arranged in any specified length. Reticon were also displaying linear arrays, but had extended their product range to include area arrays of up to 1024 diodes.

A useful feature of the Reticon line scanner is that the i.c. includes the shift register used to operate m.o.s. switches which connect diodes to the video line.

This report covers only a fraction of the interesting range of products at the 1972 Electronica exhibition, which, surely, now ranks in importance with the Hanover Fair.



# Letters to the Editor

*The Editor does not necessarily endorse opinions expressed by his correspondents*

## Doppler effect in loudspeakers

Perhaps I might be permitted to sum up the recent correspondence on Doppler effect in loudspeakers.

The fact that distortion due to the Doppler effect exists in loudspeakers was clearly demonstrated nearly thirty years ago by Beers and Belar, who measured objectively the distortion from various loudspeakers when radiating pure tones, and showed that the distortion obeyed the laws they had predicted. Doppler distortion from loudspeakers has also been assessed subjectively by Moir, again using pure tones, this time in a live room, and he has shown that very small orders of distortion are audible, a figure of 0.001% being quoted for the most critical carrier and modulating frequency used. What then do we make of the statement in my previous letter that Doppler distortion from three differing types of B.B.C. monitoring loudspeaker is inaudible, even at their maximum rated powers, in spite of the fact that the distortion figures exceed that given by Moir? The difference is that I was speaking of distortion under programme conditions, not when using pure tones. It has been shown by Stott and Axon<sup>1</sup> that for flutter, which is just another form of Doppler distortion, the ear can be no less than 38dB more sensitive to the most critical combination of tone and flutter frequency than it is to the corresponding distortion of the most critical type of programme at the same flutter frequency (5Hz), both being listened to on a wide-range loudspeaker in a live room. This difference reduces somewhat to 29dB for a flutter rate of 50Hz which would represent roughly the lower frequency limit of most loudspeakers. These figures are enormous, but in fact they can be confirmed qualitatively by every-day experience. If we take a tape machine whose flutter is *completely inaudible* on programme, record on it a continuous tone of 2kHz and play it back, the resulting frequency modulation is not only just audible, it is *gross*, thus confirming that there is a very large difference in the sensitivity of the ear to this form of distortion for the two types of signal.

One other point should be made. In a given size of loudspeaker unit careful design will reduce the amplitude non-linearity due

to the spider-surround combination or the magnetic field. No such cure is available for Doppler distortion. If the size of the cone, the frequency limits and the sound power are fixed, the level of Doppler distortion follows automatically. Curves showing the minimum sound levels for various size radiators before Doppler distortion is audible in a 2000 ft<sup>3</sup> room are given in a paper to be published, in the *Journal of the Audio Engineering Society*.

H. D. Harwood,  
B.B.C. Research Dept.,  
Kingswood Warren,  
Surrey.

1. Stott, A. and Axon, P. E., *Proc. I.E.E.* Pt. B, No. 5, September 1955, 0. 643.

## Feedback amplifiers

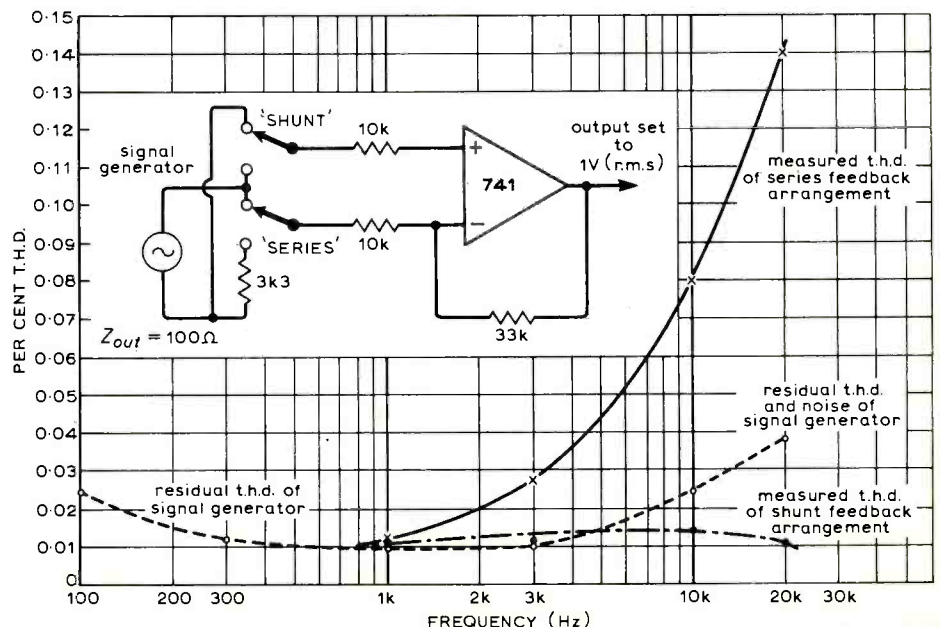
I have read with great interest the further letter from Mr Walker in your November issue (p. 520) and I would like to express my gratitude to him for the light which his analyses have cast upon the noise characteristics of feedback amplifiers, and for the several obscurities which he has resolved.

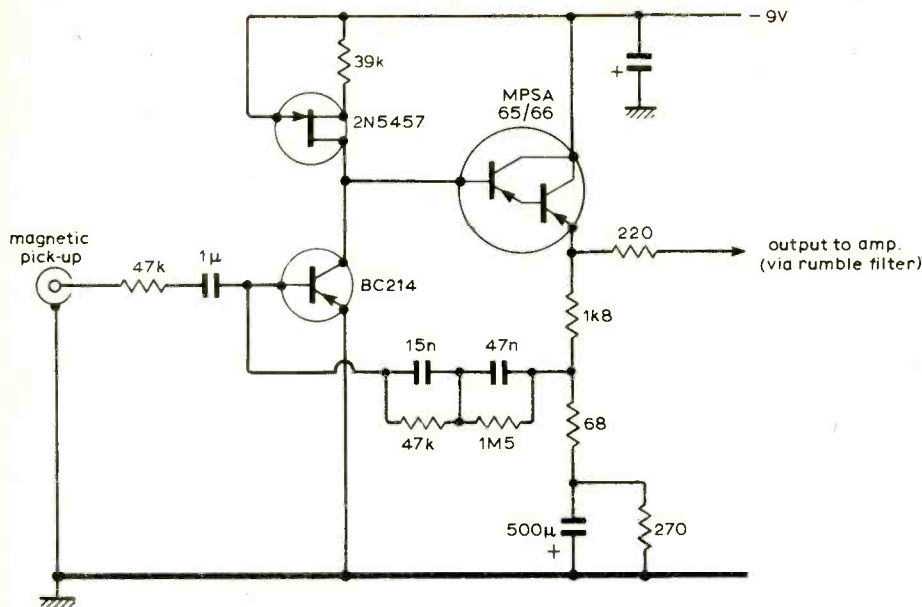
It is not in dispute that the series negative feedback configuration offers the lower noise—this is evident in practice, and is the reason why it is (almost) universally adopted in commercial 'hi-fi' equipment. The normal transistor circuit of commerce has however some snags, as pointed out by Dr A. R. Bailey<sup>1</sup>, myself<sup>2</sup> and others. Since it is not in the nature of human experience that one ever gets anything entirely for nothing, even when these snags are removed by careful engineering there will still be some ways in which the series feedback arrangement (which is better in respect of input noise figure) is less good than the shunt feedback configuration (which is worse in this respect). I contend that these aspects are harmonic distortion and input (common mode) over-load.

As a demonstration of the first of these points, to which I referred in my letter in the August issue as 'transfer non-linearity' between the two inputs of an operational amplifier, I have shown in Fig. 1 the performance of a 741 type operational amplifier (which has a very high—90dB—common mode rejection ratio, and an extremely high—100dB—low frequency open loop gain) as a simple  $\approx \times 3$  feedback amplifier in the series and shunt feedback configurations, at 1 volt r.m.s. output. It is clear that if one set a target t.h.d. figure of 0.02%, the series feedback system would not meet this specification at frequencies above 2kHz because of common mode failure, in spite of the massive amount of negative feedback supposedly available.

By contrast, in the shunt feedback arrangement, the measured t.h.d. does not worsen at h.f. because the whole of the amplifier element is within the feedback loop. The apparent fall of t.h.d. beyond 5kHz is due to the limited h.f. response of the 741 acting to filter out some of the predominantly third harmonic distortion originating in the generator.

In the case of the input R.I.A.A. equalizing circuit using a shunt feedback arrangement, which I described in my preamplifier (July 1969) and was analysed by Mr Walker in





his May 1972 article, the characteristics for which this was optimized were low harmonic distortion (of the order of 0.01%) and effective rumble filtration, these being qualities which I judged then, and now, to be valuable. However, as an example of what can be done in getting both low noise and low distortion with a shunt feedback system, the p-n-p 'Liniac' shown in Fig. 2 (and Fig. 6b, *Wireless World* Sept. 1971, p. 439) has a measured input noise of  $0.6\mu\text{V}$ , a t.h.d.  $< 0.02\%$ , and an effective noise figure of  $-72\text{dB}$  with respect to  $5\text{mV}$  input.

J. L. Linsley Hood,  
Taunton,  
Somerset.

1. Bailey, A. R., *Wireless World*, December 1966.

2. Linsley Hood, J. L., *Gramophone*, February 1971, p. 1383.

## Peak programme meter

One welcomes the Nelson-Jones design for a PPM (November issue)—for in these days of universal meters on tape machines (rather than the old magic eye level indicators, which could be made to behave like a PPM) one is often in doubt as to the meaning of wildly twitching pointers. However, the design could have been made even more useful.

I would have thought it would have been comparatively easy to make the electronics play the part of the special ballistics of the specified meter. At first sight, it seems unreasonable to ask the electronics to control the overshoot of a meter point—but, in fact, there is no need. Why not slow the rate of rise of the pointer to the point where overshoot is not significant? After all, even with the correct movement—or the inertia-less magic eye—it was not possible to take any remedial action once the device had indicated 'overload'. Really the level indicator is of the 'oops sorry' variety, rather than the

'if you don't turn it down a bit it'll overload'. This latter function is an interpretive one provided by the brain. So it matters not if, say, the pointer takes half a second to reach its indication provided it gives a correct indication of what happened half a second ago.

Armed with such a circuit, one could then modify most of the flickering nasties fitted to tape machines today, to give an indication that would be useful, repeatable, and even interpretable. Back to the bench please Mr Nelson-Jones! More power to your elbow (soldering iron?).

Richard Oliver,  
Denmark Hill,  
SE5 8ED.

### The author replies:

First, I would not entirely agree that the PPM is an 'oops sorry' device, since certainly in many recording applications the recording engineer will know what is coming either from previous rehearsal or the score, or both, and it was originally for this purpose that the new circuit was designed. I do, however, agree with you about the nasty little twitching pointers of the VU meters fitted to so many tape recorders, they make my eyes ache.

While I agree with you that because a thing is well established it is not a good reason for continuing with it if something better or simpler comes up, I would point out that the present PPM meter movement is the result of many years of practical experience both on the part of Ernest Turner Instruments and the B.B.C. and has passed the test of time and much experiment. I would point out that when monitoring with a PPM, one is not necessarily hearing the sound also, and a very slow meter movement would I think give a false impression of the sound being monitored. To make use of your idea for using normal meter movements it would be necessary to modify the circuit of my PPM unit to enable the circuit to retain the charge put into the capacitor for a period of some tens of milliseconds

(irrespective of peak level), so that sufficient time would elapse before the circuit started to discharge in order that the meter could catch up. I think that the circuit complication added by this extra would probably outweigh any cost saving coming from using a cheaper standard movement. I have not so far worked out the circuit modifications needed but an initial look leads me to estimate that the circuit complexity would probably be at least doubled.

Finally I would point out that I developed the circuit given in the November article specifically to update the standard PPM, and not to attempt to improve the art as such. So sorry Mr Oliver but I shall not be going back to the bench to radically change the design just yet, as I really cannot see any advantage in doing what you suggest. To sum it up *I do believe* the meter needs a fast dynamic response to meet the needs of the recording and broadcasting engineer, just because the instrument is more than an 'oops sorry' device—at any rate it is to the engineers I know.

Sorry we don't agree on this, but please do not be put off trying the idea; it will certainly be better than the wildly twitching pointers to which you refer, and for applications where you genuinely do not know what is coming it may help a lot.

L. Nelson-Jones.

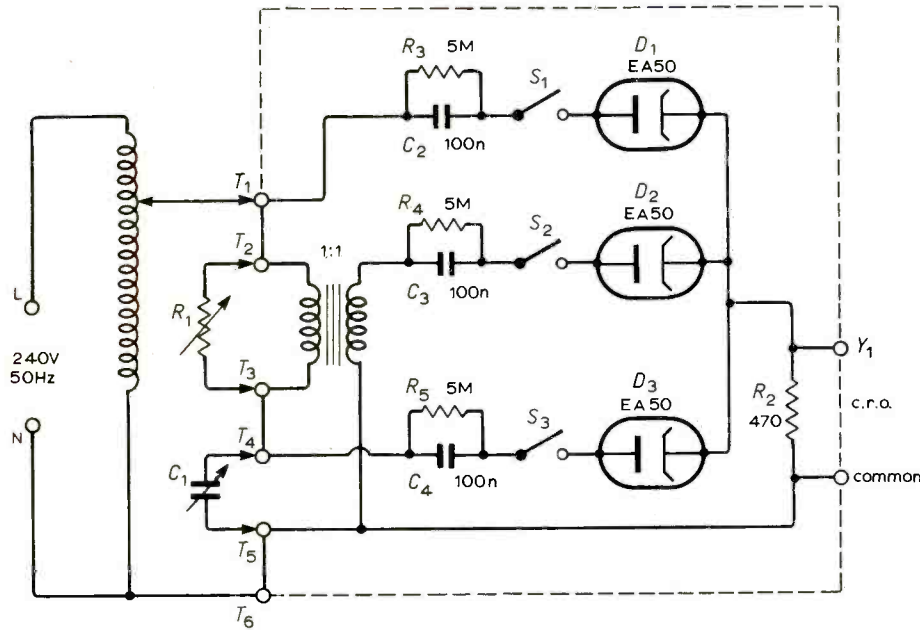
## Displaying phasor diagrams

I was interested to read the article 'Displaying Phasor Diagrams' (August issue) by A. R. Carruthers and J. H. Evans. As the author of the first article quoted in their references, I congratulate them on their design. Their article reminded me of another scheme I tried after writing the article they mention. It did not attempt to display a phasor diagram on a c.r.o. but to suggest the idea of phase difference by showing changes in the displacement between pips on a horizontal timebase when the values of  $R$  or  $C$  were changed in a series  $RC$  circuit. The simplicity of the scheme might appeal to some teachers.

In Fig. 1, the output of a variac is applied to terminals  $T_1$  and  $T_6$ . The components of the  $RC$  circuit are connected to appropriate terminals. We are concerned with three alternating voltages;  $V_{supply}$ ,  $V_R$  and  $V_C$ . So that we can work with reference to a common point, we use a 1:1 isolating transformer. Each voltage is applied to a diode and an  $RC$  circuit; current flows through the diode only when the voltage in question reaches its positive peak value. Whenever current flows through a diode, a positive spike is developed across  $R_2$ , which is common to the three diode circuits. The timebase of the c.r.o. thus shows three spikes, the one on the left corresponding to the voltage which leads the other two. Fig. 2 shows the timebase.

When  $R_1$  is reduced (and the output of the variac is kept constant) the amplitude of the central pip remains constant; the left



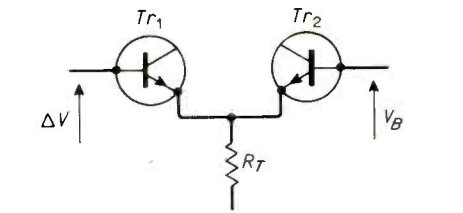


the diagrams. The amended form of Fig. 3 is shown below. In the circuit of the master bistable we used a 2S745 rather than the 'overpowering' 2N1210.  
A. R. Carruthers  
and J. H. Evans.

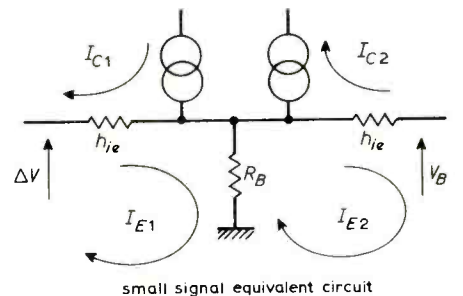
### Special-purpose amplifier

Mr Cocking's interesting article on the 'long tailed pair' amplifier (June 1972 issue), raised some points on deriving the input resistance of such an amplifier.

There are two main approaches to the problem. The first is to derive an expression from basic principles utilizing the diagrams shown in Fig. 1, and summing around the two emitter loops.



$$I_E - I_C = I_B \approx I_E / h_{FE}$$



If  $V_B = 0$ , there is no feedback and  $R_{in} = \frac{\Delta V}{I_{B1}}$  is given by  $h_{ie} + (h_{ie}/h_{fe}R_E) \approx 2h_{ie}$ . If  $V_B = \Delta V$  then the open loop gain is infinite. This gives  $R_{in} = h_{ie} + 2h_{fe}R_T$ , which is approximately the value given by Mr Cocking. For the case of a finite open loop voltage gain of  $A_{OL}$  we put  $V_B = \Delta V \left( \frac{1}{1 - A_{OL}\beta} \right)$  where  $\beta$  is the feedback factor (this means that the input difference voltage is  $\frac{\Delta V}{1 - A_{OL}\beta}$  giving the usual output of  $\frac{\Delta V A_{OL}}{1 - A_{OL}\beta}$ ). This gives us

$$R_{in} = \frac{h_{ie1}^2 + 2h_{ie}R_T}{h_{fe} + \left( \frac{1}{1 - A_{OL}\beta} \right) R_T}$$

Taking the values quoted in the article with  $h_{ie1typ} = 50k\Omega$ ,  $h_{fe1typ} = 200$  both for the BC107 at  $100\mu A$  we derive  $A_{OL} = 375$  by the usual simplified  $h$ -parameter analysis. As  $\beta = -1/10$  we have  $R_{in} = 2.84M\Omega$ .

A much simpler approach which gives



pip is reduced and the right increased. But a more important feature is that the displacement between pips changes in accordance with the changes in the phase angles in the phasor diagram.

When the equipment was made many years ago, it was convenient to use EA50 diode valves, which were plentiful just after the war. I suppose nowadays it would be more convenient to use semiconductors. As far as I remember, I used a 1-10μF decade capacitor box for  $C_1$ ; and a 500-Ω variable resistor for  $R_1$ . To identify the spikes, each diode had a switch. With all switches closed, there were three spikes. If  $S_1$  (in the circuit for  $V_{supply}$ ) was opened, a spike disappeared. We could thus relate the central spike to  $V_{supply}$ .

The simplicity of the scheme might appeal to some, but a warning should be given about its use and the method I described in *Electronic Engineering* in 1951. I must confess that in the long run I was disappointed at the lack of effect of these visual aids. For my students, they did not open gates of perception previously closed: there was a mysterious black box, mysteriously drawing diagrams on a c.r.o. which had some resemblance to the mysterious diagrams in their textbooks. Two mysterious diagrams resembling one another were still mysterious. I started experimenting with v.l.f. oscillators and with coils rotating at 6 rev/min in magnetic fields, in attempts to teach a.c. theory by slow-motion demonstrations (some of which have been described in *W.W.*)

The Carruthers-Evans circuit would seem to be valuable basis for a laboratory measuring instrument and for a teaching aid in a

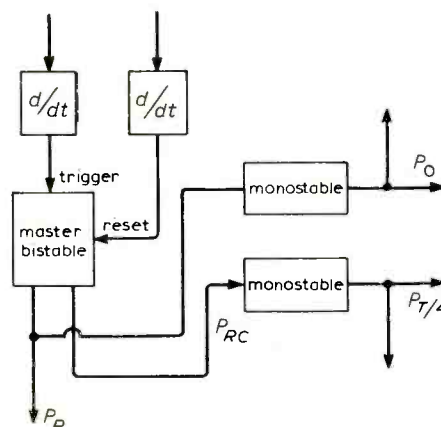
College of Technology. My experience, in teaching a.c. theory to elementary students in a technical college, suggests that schemes for drawing phasor diagrams on a c.r.o. are not as effective as slow-motion demonstrations. But of course the two techniques are not exclusive; there is no reason why we should not start with slow-motion (using centre-zero meters) and go on to phasor diagrams on a c.r.o.

T. Palmer,  
Kew,  
Surrey.

#### The authors reply:

We thank Mr Palmer for his comments, which are clearly based on some considerable experience in teaching circuit theory. The unit described was not intended to be used as the means of teaching a.c. theory, but as a method of reinforcing what had already been taught. It was used to provide short video-tape recording inserts in lectures to demonstrate (with the aid of a black box) the 'dynamic' behaviour of real engineering circuits by variation of component values as opposed to the 'static' descriptions provided with a blackboard or overhead projector.

Regrettably two errors have occurred in





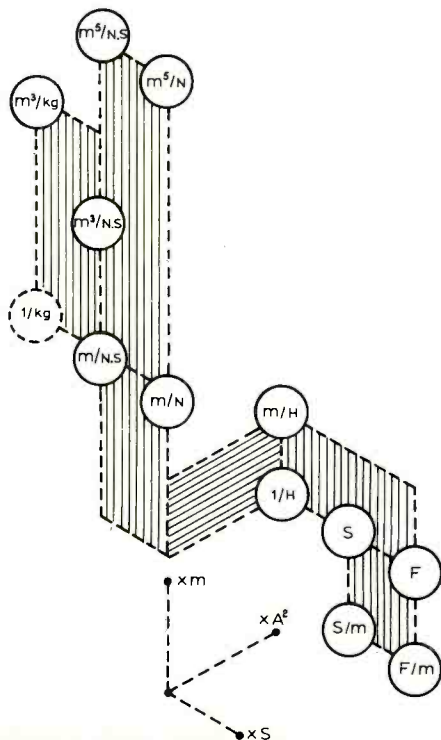


Concerning Mr Clay's difficulties as regards the incorporation of 'heat' within his periodic pattern, I am not clear as to the meaning he attaches to the term. In B.S. 3763:1970, *quantity of heat* is equated with energy and work, whereas *heat capacity* is defined as quantity of heat divided by thermodynamic temperature, the latter being taken as a base quantity. As for charge, in academic circles this is regarded as analogous to mass.

Some quantities may have the same dimensional description, but differ completely in *character*. A familiar case in the mechanical field is the disparity between work and moment of force, or torque. Work has the joule as its unit, given by a force of 1 newton acting through a distance of 1 metre along its direction of application. The unit of torque arises when 1 newton of force acts at right angles to a 1 metre radius of application, but its unit is the newton metre. This conflict can be resolved by regarding torque as work per unit angle. Unfortunately, angles (plane or solid), according to B.S. 3763, may be regarded either as dimensionally independent quantities or mere ratios, whichever is most convenient!

While discussing dimensional displays, it is notable that with the admittance field, named quantities\* (depicted in reciprocal form in Figs. 2 and 5 of the March 1972 article) are relatively sparse as compared with those used in the impedance field. In fact, the latter has 30 dimensional positions directly associated with named quantities, as against only 12 of admittance form. As far as I am aware, the reciprocal of mass has not been given a generally accepted appellation, although the term 'reciprocal mass' is used in the semiconductor field. So, in Fig. 5 of my display, it would presumably be

\*Note. The quantities admittance, conductance and susceptance now have the unit siemens, symbol S, instead of the unit mho.



acceptable to replace '1/permittivity' by the description 'reciprocal permittivity'.

Some doubts have been raised as to the value of exploring dimensional relationships. Many are of negligible interest, but it is salutary to put oneself in the place of a scientist in, say, 1841, ten years after Faraday's fundamental discoveries concerning electromagnetic induction. Given the dimensional equality [permeability] × [permittivity] = [(slowness)<sup>2</sup>], where slowness = 1/velocity, it would have appeared meaningless, yet later became of outstanding significance following Maxwell's mathematical prediction of the feasibility of electromagnetic wave propagation over a wide spectrum.

Returning to the present, is it not possible that a relationship shown by my display such as [mass] × [elastance] = [(magnetic vector potential)<sup>2</sup>] may also hint as to the existence of some form of field so far unobserved?

R. N. Baldock.

### Noise

As a final comment on the colour connotations associated with random noise of various spectra, so clearly expounded by Mr H. D. Harwood in the November issue in reply to my earlier letter, may I now be credited with the origination of the term 'black noise'? I hope this will be accepted as implying equal absence of integrated energy per cycle bandwidth!

R. N. Baldock,  
Harrow,  
Middlesex.

### Seeing in the dark

I should be most grateful if I might be allowed some space in your columns over which I might trail my coat to see if some of the broadcasters and/or television camera manufacturers will jump onto it.

Let me first make some relevant statements which I believe to be accepted universally.

1. The human eye operates over a luminance range of about 10<sup>10</sup>, but at any instant its operating range is much smaller, being well satisfied with a contrast range of about 10<sup>2</sup>, a range which the broadcasters can satisfy when the operating conditions are very favourable. The 10<sup>2</sup> range can thus slide over a range of about 10<sup>8</sup>.

2. Television cameras are available which can operate to provide this 10<sup>2</sup> range anywhere within the 10<sup>10</sup> range over which the eye can operate, but whereas the gain of the camera can be adjusted almost instantaneously, the 'gain-control' of the eye has a time-constant of many minutes.

3. Conditions of flicker, tube design and ambient lighting in the home fix the position in the 10<sup>10</sup> range of the eye where the 10<sup>2</sup> range of reproduction must be located. This means that the 'gain-control' of the eye

operates only over a very small range when viewing television, but the gain control of the camera operates over a very wide range from shot to shot. For instance when cutting from say a shot of a brilliantly lit interior to one of a dark alleyway the two peak brightnesses of the reproductions are similar, in the latter case the peak brightness typically being provided by a street lamp and occupying only a small proportion of the picture area.

4. The human eye possesses a high degree of acuity to luminance changes under conditions of high luminance but a low degree of acuity under conditions of low luminance.

5. The human eye is colour conscious only under conditions of high luminance, everyone being colour-blind under conditions of low luminance.

Having stated the premise upon which my queries are based, I would now like to ask the broadcasters/manufacturers two questions. The first is based upon 4 above. Should there not be a succession of low-pass filters of successively lower cut-off frequency brought into circuit as the camera gain control is advanced? The second is based upon 5 above. As the gain control is advanced should not the gain of the chrominance channel be reduced relative to that of the luminance channel?

If these conditions are not met, then it would appear that when viewing scenes which are shot under conditions of low luminance the viewer will be presented via the television channel with information which he would not see under conditions of direct viewing of the scene, and thus the reproduction appears to be unnatural.

I should be pleased to hear or read of any fallacy in my argument.

Roy C. Whitehead,  
Polytechnic of North London,  
London N7.

### Power supply units—a plea

May I please make via your columns an appeal to the manufacturers of stabilized power units?

The normal commercial unit carries a moving-coil meter and a meter switch which is marked VOLTS/AMPS. The switch is nearly always used in the VOLTS position but occasionally someone moves it to the AMPS position and leaves it there. On the next occasion that the unit is used, the user, accustomed to having the meter set to the VOLTS position, turns up the amplitude control in an endeavour to produce the expected meter deflection. If the load impedance is high he will probably destroy the load before realising his error. (No, I have not blown up any i.c.s, yet!).

The solution would appear to be the use of a switch which has a locking action in the VOLTS position and is nonlocking in the AMPS position.

Roy C. Whitehead,  
Polytechnic of North London,  
London, N7.

# An Electronic Turntable

The London Audio Fair can usually be reckoned to produce one or two innovations. Unique among those shown this year was an electronically controlled parallel tracking turntable produced by Bang and Olufsen, of Denmark.

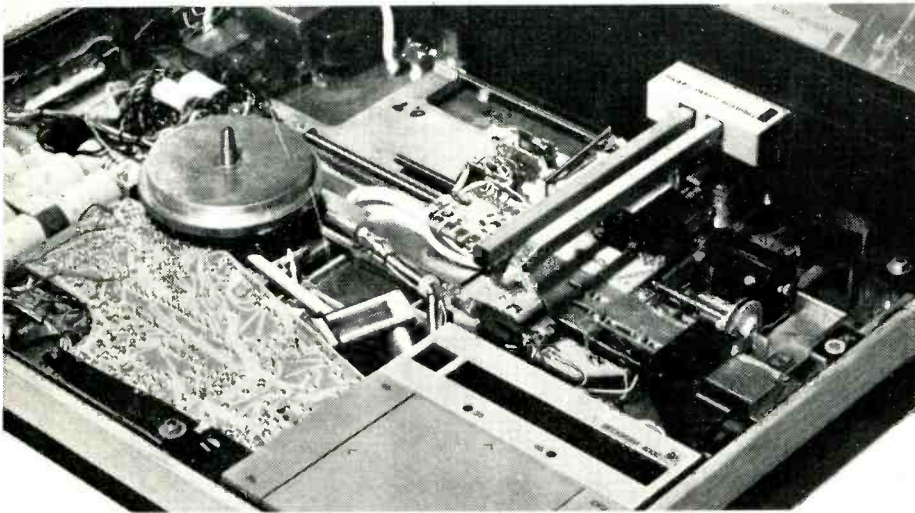
The photograph, which shows the Beogram 4000 with its top covers removed, illustrates some of the more basic details of the deck itself. Most significant is the use of a tangential arm which moves the pickup cartridge in a straight line from the edge to the centre of the record. Using such a system—not new in itself—has produced a number of advantages which have not only permitted the use of a semi-automated electronic control unit, but also improved the potential reproducing performance of

the unit. Inherent in the design of a conventional arm is the difference in tracking angles with respect to the groove tangent, made by the reproducing and recording styli. In an effort to reduce this error to a minimum, the conventional reproducing arm is bent at an angle; however, this gives rise to a mechanical reaction producing a force which drives the stylus against the inner face of the record groove. Some form of compensation, known as bias, is applied to balance out this force but it is an ex-

tremely difficult factor to accurately nullify and thus most systems are somewhat of a compromise. In adopting the tangential arm, the need for bias compensation is eliminated since the arm can be made straight and thus does not produce any side thrust. In addition, because the reproducing stylus is made to track in precisely the same fashion as the cutter, distortion can be reduced.

Two arms are carried on a "slide" which runs on two rails and is driven through a worm gear by a small servo motor. One of the two arms contains a lamp and photocell which serve to detect the edge of the record as the slide moves across the turntable. Since the turntable itself consists of a polished metal surface broken with radial black plastic spokes, the detected reflection produces a varying output from the photocell rather than the steady signal resulting from the reflection off a disc surface. In this way there is no chance of the stylus being lowered onto the turntable platter itself, in the event of the machine being started without a record being loaded. Two states can thus be generated by the detector arm sensor: an alternate shift of level indicating no record, and a d.c. level indicating the presence of a record.

A second sensing system is fitted to the pickup arm. This provides an output indicating angular errors in the position of the arm. As the stylus is carried across the record by the groove, of necessity the slide must be moved in sympathy to keep the arm at an exact tangent to the groove. Attached to the horizontal arm pivot is a



The interior of the B & O 4000 showing the parallel tracking arm and its slide carriage.

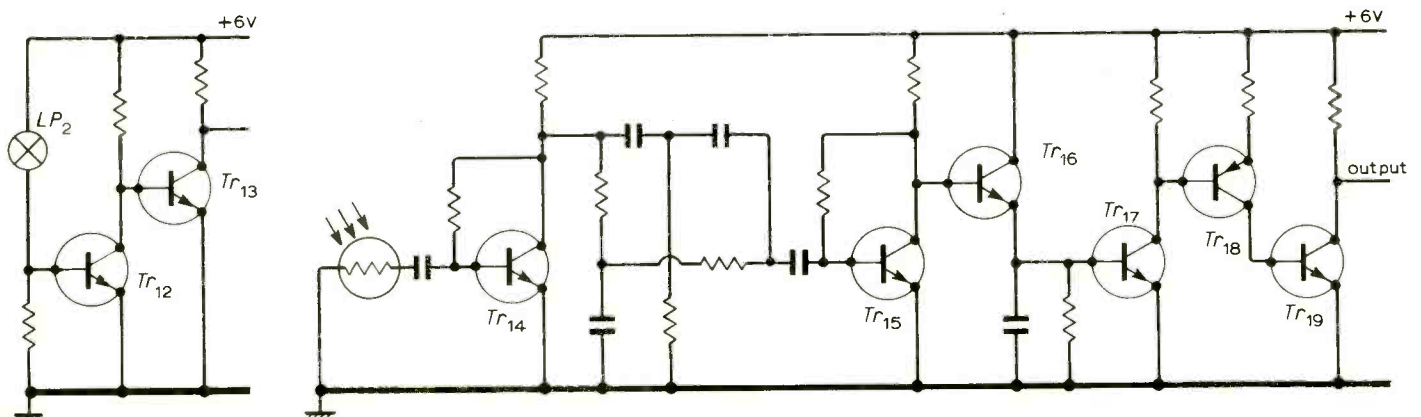


Fig. 1. Detector arm servo amplifier. This circuit produces a two-state output to drive the control switching logic.



small shutter above which is fitted a small lamp and below, to each side, a photocell. Any deviation of the arm from its correct tangential position will partially obscure one or other of the photocells, producing an unbalanced output from the sense system which can then be used to operate the servo control and the motor to correct the situation. Using such an arrangement ensures that angular error in the arm is less than  $0.04^\circ$ .

### Servo control circuits

The output of the photocell sensor in the detector arm is fed via a capacitor to the base of transistor  $Tr_{14}$  (Fig. 1) which is d.c. biased. Since the output from the photocell has a frequency of 13-18Hz with no record present, it is easy to differentiate between this and a spurious signal generated by, say, the flicker of a mains driven room light. Such a selection is in fact achieved by the use of a notch filter between  $Tr_{14}$  and  $Tr_{15}$ , tuned to 100Hz. After integration of the signal from  $Tr_{15}$  by the emitter resistor and capacitor of  $Tr_{16}$ , the level obtained is applied to the base of  $Tr_{17}$ , turning it on and drawing its collector voltage down to near 0V. This in turn switches on both  $Tr_{18}$  and  $Tr_{19}$  giving a low (0V) output from the sensor amplifier. Since the presence of a record beneath the detector arm produces a d.c. level from the detector, the capacitor at the base of  $Tr_{14}$  prevents any change of level at the first transistor and the circuit remains inactive, thus giving a high (6V) output.

In the event that the lamp becomes defective in the detector arm, two additional transistors,  $Tr_{12}$  and  $Tr_{13}$  are used to provide a logic output which is dependent upon current flow in the lamp. If the lamp fails, the control logic circuits prevent the arm being lowered.

The servo control of the arm slide is equally sophisticated and is described with reference to Fig. 2. By using a d.c. servo motor, a differential drive circuit can be used throughout, and although the motor can be driven at high speed with the pickup raised, this description of the circuit operation will be confined to the normal groove tracking mode. When the arm is in the lowered position the 24V supply is connected via contacts to the two photocells; these in turn operate the two servo power amplifiers and a voltage of about 12V appears at each side of the motor. If the pickup arm moves towards the centre of

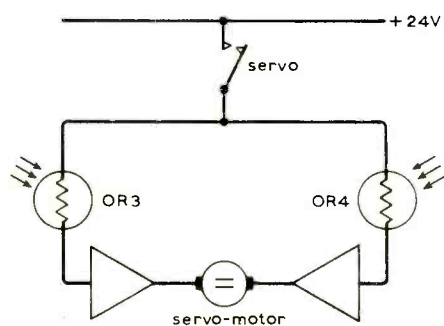
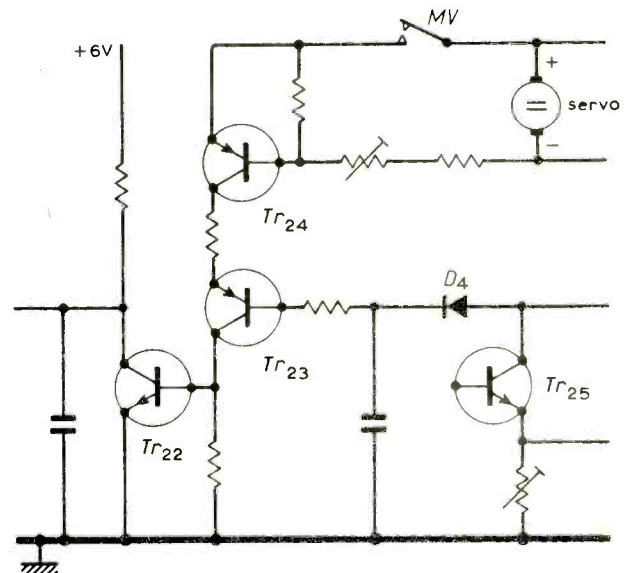


Fig. 2. Block diagram of the servo control from the photo-detectors used to sense angular errors in the arm.

Fig. 3. The circuit used to generate the logic signals for end-of-record operation.



the record photocell  $OR_3$  receives a greater light level than  $OR_4$ , throwing the circuit out of balance and causing the servo to drive the slide until the balanced condition is reached. Additional circuitry provides for automatic arm raising should manual tracking be required by the operation of one of the turntable controls.

End-of-record sensing is also tied in with the servo motor control since in the original design concept it was felt that mechanical techniques would have placed a strain on the stylus. In addition, since there is no recognized standard for the diameter of the last groove on a record, some method was needed which did not rely upon this parameter to signal the restoration of the slide to start position. Fig. 3 shows how this was achieved. When the stylus tracks the last groove of the record, the mechanical contact  $MV$  will have been operated by the slide position to connect the servo motor to the sense transistor  $Tr_{24}$ . Due to the rapid increase of pitch in the run-off grooves of the record, the voltage driving the servo will be unusually high, thus turning on  $Tr_{24}$  and  $Tr_{23}$ . Transistor  $Tr_{22}$  is in turn operated by the increase in voltage across its bias resistor and thus a logic low is produced to operate the "arm raise" system. In the event of a manual "fast inward track" being ordered by the operation of one of the turntable controls, the collector of  $Tr_{25}$  is held high and thus diode  $D_4$  blocks the base current of  $Tr_{23}$  to prevent premature setting of the restoration logic control.

### Logic control system

Devising the logic control for the turntable must start with an analysis of the various operations required to operate the deck. Since a certain amount of manual control can be exercised from switches actuated by pressure plates on the top panel, the commands issued by these will be listed first.

**1. Turntable speed.** The turntable will revolve at  $33\frac{1}{3}$  r.p.m. in the absence of any commands to the contrary being issued by either a speed selector switch, or an automatic decision based on record diameter being taken by the detector arm logic. The higher speed of 45 r.p.m. can also be

selected from a manual switch. In the event that  $33\frac{1}{3}$  r.p.m. is selected by manual control and the record is intended to be played at 45 r.p.m., the unit will not automatically correct, but will remain at the lower speed until a second manual command is made to alter speed.

**2. Arm lift.** This can be initiated at any point during the playing of a disc.

**3. Arm lower.** Used when lowering the stylus into a preselected groove. The logic circuits bar lowering the arm onto anything but a disc.

**4. Fast and slow track in.** These commands are initiated by a two-pressure switch, light pressure for a slow tracking motion, heavier pressure for a faster tracking. In the event that this command is initiated when the arm is lowered, the arm raising control is operated first.

**5. Fast and slow track out.** A similar two-pressure switch is used here and also provision is made for automatic arm raising before the tracking commences. In addition if the arm is tracked out to the normal rest position, the turntable is automatically turned off.

The next consideration is the automatic commands that need to be generated. These are:

**1. Track in (fast).** When the turntable is started by pressing the "on" switch, the arm slide will track in until the edge of a record is found by the detector.

**2. Arm tracking stop, arm lower.** This command is initiated by the detector logic on finding the edge of the record.

**3. Groove tracking mode.** The servo is driven under the command of the servo amplifier and logic commands are not used.

**4. End of record, arm lift, fast track to rest position, turnoff.** This sequence is started by the voltage sensor connected to the servo motor.

These control functions are all undertaken by a number of i.c.s connected to provide six flip-flops, a wired-OR and three single wired gates. Unfortunately lack of space precludes describing the switching techniques employed in this novel turntable, suffice it to say that this is probably the most complex to appear on the market.

# Circards — 4

## A.C. Measurements

### Introducing the fourth set of Circards on peak, mean and precision rectification

by J. Carruthers, J.H. Evans, J. Kinsler and P. Williams\*

Measurement of direct voltages is straightforward. A moving-coil meter has good linearity of deflection against direct current in the meter, and the use of parallel and series resistors (shunts and multipliers) allows such meters to give full-scale readings to cope with a wide range of voltages and currents. For very small direct voltages and currents, d.c. amplifiers may be interposed between source and meter, and such amplifiers may also be used to optimize the input

resistance of the system, i.e. to minimize loading effects.

For a.c. signals the biggest difficulty can be deciding which parameters of the signal to measure—mean, peak or r.m.s. for example. The issue is further complicated by the need to cope with a range of frequencies so broad that, for example, techniques suitable for high-frequencies result in impossibly long measurement times at very low frequencies.

There is a dearth of sensitive, accurate and low-cost types of meter movement capable of responding directly to a.c.;

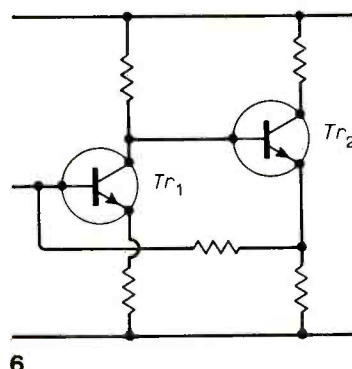
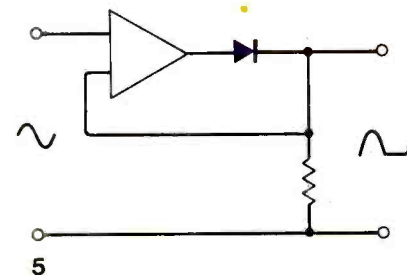
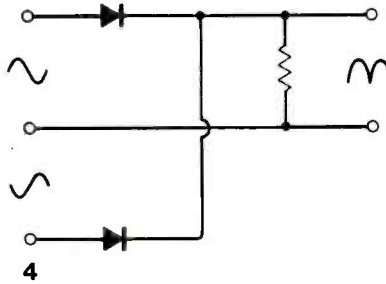
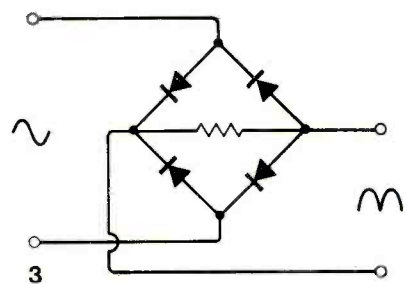
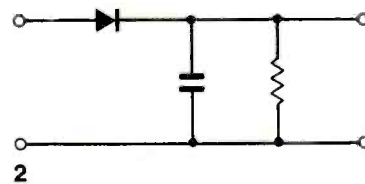
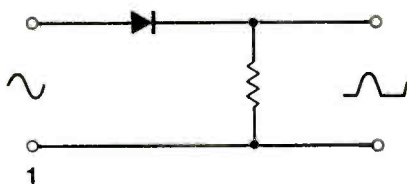
moving-iron instruments for example require much higher power for a given deflection than moving-coil instruments of comparable quality, while the deflection is a non-linear function of the current being measured. Hence in most cases the a.c. waveform is first processed in such a way that a reading may be obtained on a d.c. meter, which reading is proportional to a desired parameter of the waveform. A basic process employed is that of rectification, where the output voltage (or current) is limited to one polarity regardless of the input.

Half-wave rectification (Fig. 1) gives an output which is ideally equal to the input when the latter is positive, and an output which is zero when the input is negative. The ideal diode would pass zero current for all conditions when the anode is negative with respect to the cathode, and have zero p.d. when the polarity is reversed. In practical circuits, while the former ideal is closely approximated to by modern silicon diodes, the diode p.d. in conduction is around 0.5 to 0.8V. The output waveform becomes progressively more distorted as the amplitude of the input voltage is reduced, and for inputs below one volt the output is negligible, i.e. accurate rectification is particularly difficult at low amplitudes. Some improvement is possible by the addition of a second diode biased in such a way that the rectifying diode is brought to the edge of conduction prior to the appearance of a signal.

If a moving-coil milliammeter is placed in series with the load resistance, then the meter current becomes proportional to the average value of the half-wave rectified voltage, provided the frequency is high enough to overcome needle vibration. Such a reading is half that due to a full-wave rectified voltage for symmetrical waveforms such as sine, square and triangular waves. An average reading may also be obtained by feeding the rectified voltage through a low-pass filter to eliminate the a.c. component. Such a modification is necessary where the direct voltage is to be monitored by a digital voltmeter, to provide a digital reading of the mean value of the rectified input.

A direct voltage may be obtained directly as in Fig. 2. The capacitor charges on each positive peak of the input, losing some of that charge between peaks into the resistance of any load. To minimize such losses and make the output a more accurate

\*All with Paisley College of Technology.



Fourth set of Circards illustrates techniques of peak, mean and precision rectification. Half-wave, 1 and 2, and full-wave circuits, 3 and 4, can be used to give either mean or peak measurements. Errors due to diode voltage drops can be reduced by putting the diode in a feedback loop, 5, but use of an amplifier limits h.f. accuracy, avoided by using a simple amplifier, 6, with bridge rectifier/meter in the feedback path.



measure of the repetitive peak input voltage, the time-constant is made much longer than the period of the input signal. Too great a ratio will not allow the capacitor voltage to decay sufficiently rapidly to observe any decay in input peak voltage that may occur during the measurement. Again real diodes introduce a forward-voltage drop that mitigates against accuracy for small inputs.

Full-wave rectification is necessary where the negative and positive portions of the wave may be different. A secondary advantage can be that for symmetrical waves, a full-wave peak detector has its capacitor charge restored twice per cycle, i.e. the time for discharge and hence the ripple is approximately halved. As for half-wave rectifiers, the full-wave circuits could be used for indicating mean or peak values. (The latter would indicate only the largest peaks for an unsymmetrical signal.)

Two methods are available. Bridge rectification as in Fig. 3 requires four diodes to channel current through a load in a given direction regardless of the polarity of the applied potential. Alternatively, the provision of equal but anti-phase drives to a pair of diodes again gives single polarity to the load with each diode contributing on alternate half cycles—Fig. 4. The anti-phase voltage may be provided by a transformer or by an inverting amplifier.

In the above the assumption has been that the rectified waveform would be applied to a measuring device such as a moving-coil meter. Waveform distortion short of that causing significant meter reading error is then unimportant. Where it is required to retain full information on the rectified waveform then a precision rectifier has to be devised, i.e. one in which the rectification process is not burdened by the large errors due to diode voltage drops. Placing the diode(s) in the feedback path of an amplifier allows the effect of the diode p.d. on the output to be reduced by any desired amount.

Fig. 5 shows one version of a precision half-wave rectifier in which, for positive going inputs, the amplifier output is driven positive until it causes the diode to conduct and forces the output voltage to equal the input (or rather to differ from it by a very small p.d. which includes the amplifier offset voltage and a small contribution given by the diode p.d. divided by the amplifier open-loop gain).

The basic circuit shown meets the precision requirements, and in addition minimizes source loading while being capable of supplying normal operational amplifier currents to the load. Many variations are possible leading to: precision half- and full-wave circuits, alternatively known as absolute-value circuits; precision peak detectors and mean-reading circuits.

The use of amplifiers imposes a limit to the upper frequency of operation, which limit is accentuated by the non-linear nature of the circuitry, e.g. the amplifier slew-rate limitation defines the minimum time taken to switch the diode from its non-conducting to conducting state. The precision of the rectification process is more difficult to achieve at higher frequencies and many circuits accurate to a few millivolts at

100Hz are seriously in error at 10kHz. Similar limitations are apparent in any negative feedback system having non-linear elements in the feedback path.

For very high-frequency applications one solution is to construct suitable high-frequency amplifiers of standard design and incorporate a bridge rectifier/meter combination in the feedback path. The simpler designs using the minimum number of transistors are based on circuits such as the d.c. feedback pair of Fig. 6 with the meter circuitry either between  $Tr_2$  collector and  $Tr_1$  emitter, or between  $Tr_2$  emitter and  $Tr_1$  base. Alternating-current coupling of the input signal is then necessary as the direct input voltage cannot be zero in this circuit. The method can be extended to multi-transistor circuits and the feedback network can be located to increase or decrease the input impedance. The lowest frequency of operation is dictated by the largest value of capacitors used, and by the degree of damping of the meter movement.

To extend the frequency downwards, peak detection is usually used, i.e. with a large capacitor to store the peak voltage and minimal discharge current for the period between peaks.

At very low frequencies ( $\ll 1$ Hz) an alternative method is the use of an integrator during a single complete half-cycle or cycle with separate measurement of the time to allow determination of the mean value of the waveform during that cycle.

The amplitude of an a.c. waveform is most frequently quoted in r.m.s. (root mean square) terms, i.e. the instantaneous voltage or current value is squared, the mean value over a complete cycle (or half-cycle) is taken and the square root of that mean value is obtained. It is the r.m.s. value of a voltage that allows calculation of the mean power dissipated in a resistive load, as the power in a resistive load due to an a.c. waveform of  $V$  in r.m.s. terms is identical to that due to a direct voltage of  $V$ .

It is common for instruments which truly measure the mean rectified or peak values of waveforms to have scales calibrated in terms of the corresponding r.m.s. value for a sine-wave. Hence for non-sinusoidal waveforms the readings fail to give a correct measure of either r.m.s., mean or peak, except where power measurements are concerned, e.g. power fed to a loudspeaker. There is considerable advantage in calibrating the instrument directly in terms of the parameter measured, though this set of Circards includes examples of instruments which incorporate such form factors. True r.m.s. meters are a very different matter. Three common classes depend on

- thermocouples generating an e.m.f. dependent on the power dissipated in a load
- non-linear amplifiers approximating to square-law characteristics where the output can be averaged to give a mean-square reading. A second squaring circuit in the feedback path of a following amplifier gives a square-root action

- multipliers in which the output is proportional to the product of two inputs; if the voltage to be measured is simultaneously fed to both inputs, the output is again proportional to the square of the input.

The first method is applied to r.f. signals where the power available is sufficient, and where the use of amplifier/rectifier combinations would introduce errors because of frequency limitations. It is a specialized field and depending as it does largely on the transducer is not covered in this series. The second method requires careful control of the non-linear characteristics for high accuracy to minimize all terms other than second-order; the networks are often obtained as ready-made units from the makers of instrumentation amplifiers. Methods using the square law characteristics of f.e.t.s belong to this general class.

The third method can be achieved by using the logarithmic characteristics of semiconductor p-n junctions and by combining several junctions so that their p.d.s may be added and/or subtracted functions of the form  $(\log V_1 + \log V_2 - \log V_3 - \log V_4)$  may be obtained, i.e. outputs dependent on  $V_1 V_2 / V_3 V_4$ . These circuits can be made the basis of multipliers, or for  $V_1 = V_2 = V_{in}$  and  $V_3 = V_4 = \text{constant}$ , a square-law circuit results. A practical example is included that allows a meter reading proportional to the mean square of an alternating voltage, i.e. a meter that can be calibrated linearly in terms of the power delivered by that voltage to a given load.

#### How to obtain Circards

Order Circards by sending remittance (£1 per set, postage included) to "Circards" *Wireless World*, Dorset House, Stamford Street, London SE1 9LU, indicating which sets you are buying: No. 1, "Basic active filter"; No. 2, Comparators and Schmitts"; No. 3, Waveform generators"; or No. 4.

The Circard concept was outlined in the October 1972 issue. Introductory articles to Circards are published each month in *Wireless World*.

# High-standard Low-frequency Source

## A portable instrument incorporating an i.c. phase-locked loop and utilizing the B.B.C. 200kHz Droitwich transmission

by J. M. Osborne\*

The instrument described here was built as an exercise to evaluate the potentialities of the phase-locked loop for the reception of a frequency standard. The instrument consists of a phase-locked loop i.c. stage followed by a chain of i.c. dividers as shown in Fig. 1. The p.l.l. stage is locked to the 200kHz carrier of the B.B.C. Radio 2 transmitter at Droitwich. The carrier frequency is maintained to an accuracy of  $\pm 5$  in  $10^{10}$ . So long as lock is held, this sets the standard for the instrument.

The main use for this instrument would be the calibration and standardizing of audio oscillators, signal generators and as a source of clocking pulses. The pulses could be used for timing watches; ticks picked up by a microphone on one trace of a c.r.o. display compared with pulses from the instrument on another trace would enable a watch to be set precisely and quickly. With a little modification this type of instrument could operate the gate on a frequency meter. In this application, with a digital counter, the accuracy should be better than with an instrument using a crystal oven.

### Circuit

A block diagram of the phase-locked loop system<sup>1,2</sup> is shown in Fig. 2. The 200kHz signal is fed from a ferrite rod aerial to a phase comparator together with the output of a local voltage controlled oscillator (v.c.o.). The comparator output voltage, which depends in magnitude and polarity on the relative phase of the inputs, is filtered, amplified, limited and used to control the v.c.o. frequency in such a sense as to bring it into lock with the signal from the aerial. Thus the v.c.o., whose output is a square

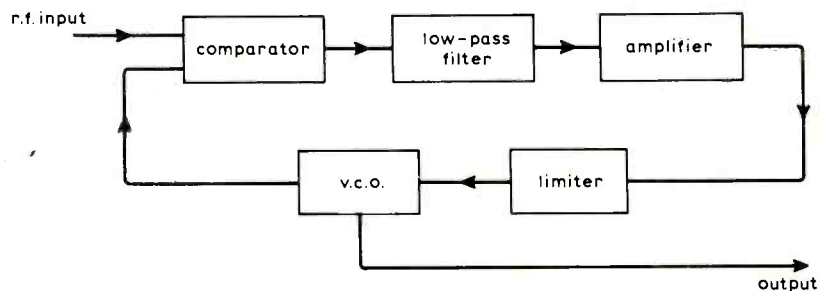


Fig. 2. The main functions of the NE561B phase locked loop i.c.

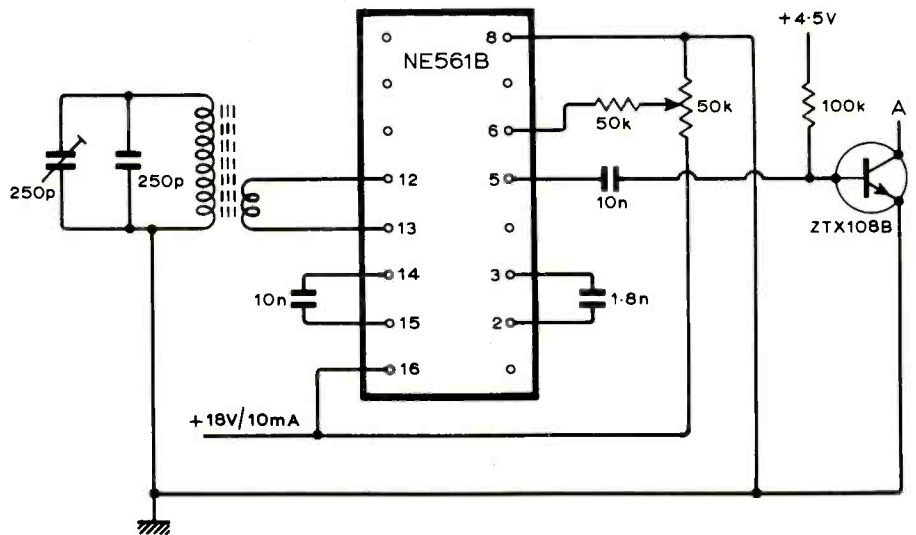


Fig. 3. The circuit of the p.l.l. stage.

\*Westminster School, London.

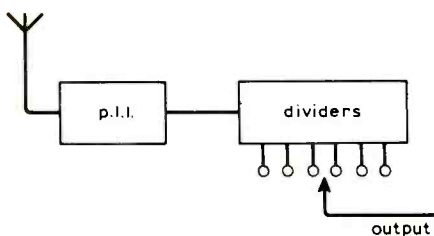


Fig. 1. Block diagram of the low frequency source.

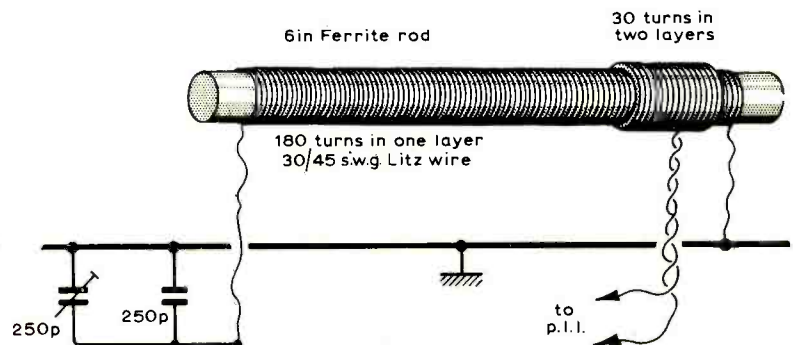


Fig. 4. Coil winding for the ferrite rod aerial.



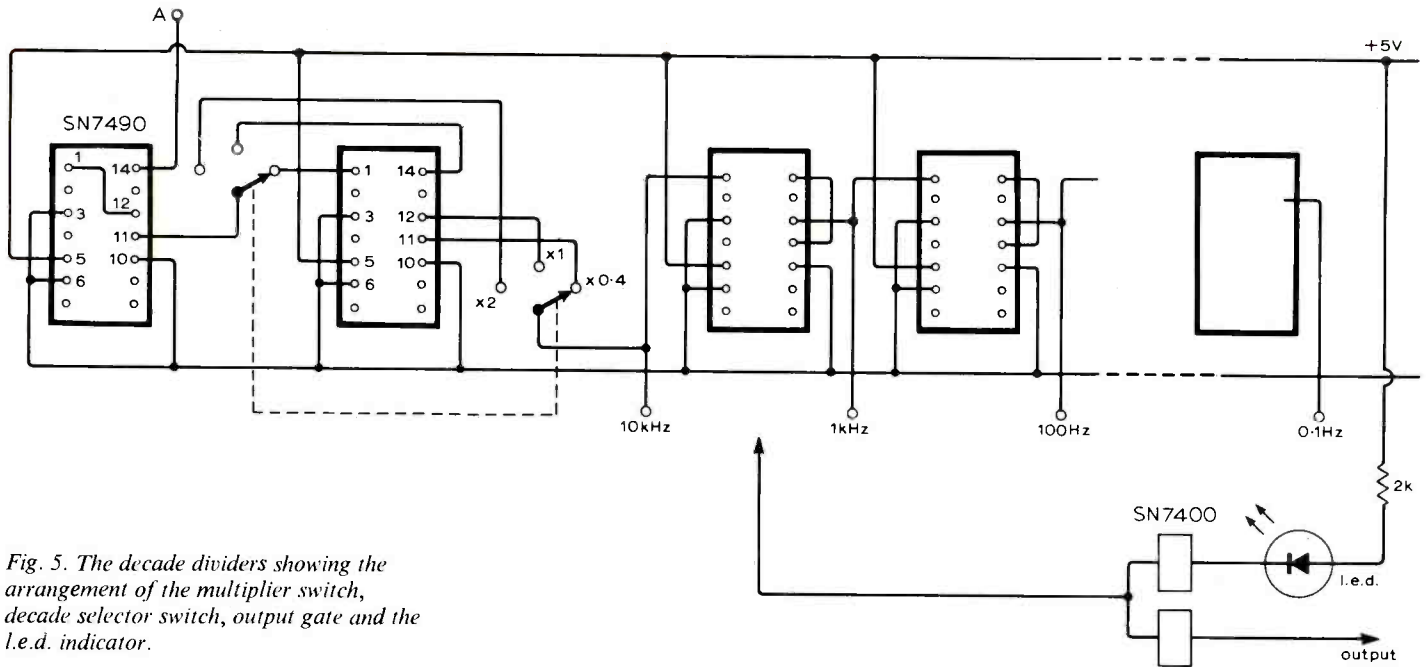


Fig. 5. The decade dividers showing the arrangement of the multiplier switch, decade selector switch, output gate and the i.e.d. indicator.

wave, ideal for operating t.t.l., runs at exactly 200kHz.

As the required r.f. input is small, 1 to 10mV being suitable, no amplification is needed in areas receiving a large signal from Droitwich. The pick-up by the ferrite aerial under typical conditions in London is adequate to provide lock, but an amplifier might be needed at distances over 150 miles from the Droitwich transmitter. A domestic transistor radio tuned to the l.w. Radio 2 programme gives a rough indication of signal strength in a building.

The p.l.l. i.c. used (Fig. 3), a Signetics NE561B, has a balanced input of about 4k $\Omega$  impedance. This would be an unsatisfactory load for the aerial and so a coupling coil is used to match it to the p.l.l. The coil, being free of earth, does not interfere with the internal bias arrangements of the integrated circuit. Litz wire is used in the final version of the aerial coil, the dimensions being given in Fig. 4. Winding over the whole length of the ferrite rod gives the maximum pick-up. The complete aerial is contained in a 1-inch Paxolin tube which also serves as a handle. It is retained by Paxolin sheet about 2 inches above the aluminium box which contains the rest of the instrument. The coupling coil leads and earthy end of the tuning coil enter one end of the box while the live lead from the coil enters from the other. The trimmer and fixed tuning capacitor are just inside the box at this end remote from the p.l.l. This minimizes stray pick-up from the v.c.o. which could interfere with the lock.

The other components associated with the p.l.l. are a 0.01 $\mu$ F low-pass filter, a 1.8nF timing capacitor of the v.c.o. which sets the free running frequency at approximately 200kHz, and a potentiometer for fine tuning of the v.c.o. by adjusting the potential of pin 6. The v.c.o. output from pin 5 is about 0.6V pk-pk and 6.5V above chassis. For interfacing with t.t.l., it is convenient to use capacitor coupling to a transistor switch. The transistor is a Ferranti ZTX108B.

### Setting up the p.l.l.

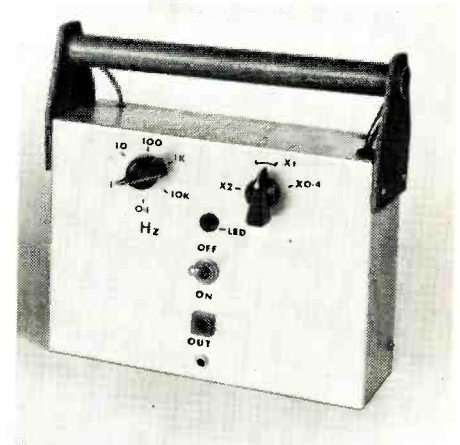
There are two preset controls, an aerial trimmer and the v.c.o. fine tune potentiometer. A transistor radio near the instrument will pick up stray radiation from the v.c.o. If the aerial coil is disconnected or substantially detuned to avoid locking, the free running frequency can be made to beat with Radio 2 by adjusting the potentiometer. This is set for a low audio beat note. Next, with the aerial connected, the trimmer is adjusted until the loop locks, as evidenced by the abrupt change to zero beat. The aerial should now be turned until the lock is just lost. Further adjustment of the trimmer may result in the lock being regained. By repeating this process, optimum tuning can be obtained.

### The dividers

The phase-locked loop is followed by a chain of SN7490 decade dividers. Switches, which should be break-before-make types, then select the required output. The first switch (Fig. 5) operates on the second divider to select  $\times 1$  (straight through),  $\div 2$ , or  $\div 5$ . As the first i.c. divides by ten, the switch selects 20kHz, 10kHz and 4kHz. The switch positions are marked  $\times 2$ ,  $\times 1$  and  $\times 0.4$ . The other switch selects successively from the rest of the chain and is marked 10kHz (straight through), 1kHz, 100Hz and so on. To square up the output of the dividers a simple gate is incorporated (part of an SN7400) before the output terminal. Another gate in parallel drives an i.e.d. as an indicator lamp. This can be seen to flash at 10Hz and less. While this indicates that the dividers are functioning it does not necessarily imply that the p.l.l. is locked.

### Construction notes

A 16-pin d.i.l. socket for the p.l.l. and all other i.cs and components may be soldered to two strips of Veroboard, which are supported on the switch and battery wires. The circuits and batteries are contained in an aluminium box, and the 18V at 10mA



The prototype low frequency source, showing controls and ferrite rod aerial used as a handle.

supply comes from two PP7 batteries on one side of the box while the t.t.l. i.cs are provided with 4.5V at 150mA by a single 126 battery. Strictly the t.t.l. requirement is 5V but they work happily on 4.5V provided the battery is replaced before the voltage on load drops to 4V.

### References

1. J. M. Osborne, 'The Phase Locked Loop', *Short Wave Magazine*, Vol. XXX, No. 1, March 1972.
2. T. D. Towers, 'Elements of Linear Microcircuits', *Wireless World*, August 1971, p. 397.

# 1973 Conferences & Exhibitions

Further details are obtainable from the addresses in parentheses

## LONDON

Feb. 26-Mar. 2 Bloomsbury Centre  
**Seminex**  
 (Evan Steadman and Partners, 4 Lyewood Common, Withyham, Hartfield, Sussex)

Mar. 13-15 Savoy Place  
**Satellite Systems for Mobile Communications and Surveillance**  
 (I.E.E., Savoy Place, London WC2R 0BL)

Mar. 13-15 Bloomsbury Centre Hotel  
**Sound 73**  
 (Assoc. of Public Address Engineers, 6 Conduit St, London W1R 9TG)

Mar. 22 & 23 Royal Garden Hotel  
**Man Made Memories**  
 (Mrs. Rosemary Willson, Mercury House, Waterloo Road, London SE1)

Mar. 27-29 Imperial College  
**Ultrasonics International**  
 (Ultrasonics, 32 High Street, Guildford, Surrey)

Mar. 28-Apr. 1 Excelsior Hotel  
**Sonex Audio Exhibition**  
 (Federation of British Audio, 31 Soho Sq., London W1V 5DG)

Apr. 9-13 Earls Court  
**Physics Exhibition**  
 (Inst. Physics, 47 Belgrave Sq., London SW1X 8QX)

Apr. 9-13 Earls Court  
**LABEX International**  
 (U.T.P. Exhibitions, 36-37 Fumival St., London EC4A 1JH)

Apr. 25-27 Chelsea College  
**B.A.S. Spring Meeting**  
 (British Acoustical Society, 1 Birdcage Walk, London SW1H 9JJ)

May 22-25 Olympia  
**London Electronic Component Show**  
 (Industrial Exhibitions, Commonwealth House, New Oxford St, London WC1A 1PB)

June 5-8 Earls Court  
**International Marine Exhibition (IMEX)**  
 (Brintex Exhibitions, 3 Clements Inn, London WC2A 2DB)

June 5-8 Earls Court  
**International Marine and Shipping Conference (IMAS)**  
 (Institute of Marine Engineers, 76 Mark Lane, London EC3R 7JN)

June 25-29 Royal Lancaster Hotel  
**Film '73**  
 (Paul D. McGurk, B.K.S.T.S., 110-112 Victoria House, Vernon Place, London WC1B 4DJ)

Oct. 1-3 Savoy Place  
**Organization and Management of Computer Based Control and Automation Projects**  
 (I.E.E., Savoy Place, London WC2R 0BL)

Oct. 22-27 Olympia  
**Audio Fair**  
 (International Audio Festival & Fair, Dorset House, Stamford St, London SE1 9LU)

Oct. 23-25 Savoy Place  
**Radar — Present and Future**  
 (I.E.E., Savoy Place, London WC2R 0BL)

Nov. 12-14 Savoy Place  
**Digital Instrumentation**  
 (I.E.E., Savoy Place, London WC2R 0BL)

## BIRMINGHAM

July 10-12 University of Birmingham  
**Video and Data Recording**  
 (I.E.R.E., 9 Bedford Sq, London WC1B 3RG)

Sept. 16-22 University of Aston  
**Switching and Signalling in Telecommunications**  
 (I.E.E., Savoy Place, London WC2R 0BL)

## BOURNEMOUTH

Apr. 11-14 The Pavilion  
**Marketing Communications Tomorrow**  
 (Electromation Exhibitions Ltd., Cleveland House, 344A Holdenhurst Road, Bournemouth)

## BRIGHTON

Jan. 9-11 The Metropole  
**Componex**  
 (Evan Steadman and Partners, 4 Lyewood Common, Withyham, Hartfield, Sussex)

Apr. 5 & 6 University of Sussex  
**European Co-operation in Research and Technology**  
 (Research and Development Society, 47 Belgrave Sq, London SW1X 8QX)

June 19-21 The Metropole  
**Microwave 73**  
 (Microwave Exhibitions and Publishers Ltd., 21 Victoria Rd, Surbiton, Surrey)

## CAMBRIDGE

Apr. 2-4 The University  
**Computer Aided Control System Design**  
 (I.E.E., Savoy Place, London WC2R 0BL)

Sept. 6-9 King's College  
**Royal Television Society Convention**  
 (RTS, 166 Shaftesbury Avenue, London WC2H 8JH)

## CARDIFF

Sept. 12-14 Traherne Hall, UWIST  
**Physics of Semimetals and Narrow-Gap Semiconductors**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## COLCHESTER

Apr. 2-5 University of Essex  
**Software Engineering for Telecommunication Switching Systems**  
 (I.E.E., Savoy Place, London WC2R 0BL)

## HULL

Apr. 11-13 The University  
**Teaching of Electronic Engineering in Degree Courses**  
 (Dr. F. W. Stephenson, Department of Electronic Engineering, The University, Hull HU6 7RX)

## LANCASTER

Apr. 9-11 The University  
**Thin Films**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## LIVERPOOL

Apr. 15-18 The University  
**To be Continued — Education and Training**  
 (I.E.E.T.E., 2 Savoy Hill, London WC2R 0BS)

## MANCHESTER

Jan. 3-5 The University  
**Solid State Physics**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## NEWCASTLE UPON TYNE

Apr. 10-13 The University  
**Atomic and Molecular Physics**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

July 3-5 The University  
**Scanning Electron Microscopy Systems and Applications**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## NOTTINGHAM

Apr. 10-12 The University  
**Datafair 73**  
 (British Computer Society, 29 Portland Place, London W1)

July 9-12 The University  
**Maintenance Management**  
 (Society of Electronic and Radio Technicians, 8-10 Charing Cross Road, London WC2H 0HP)

Sept. 10 & 11 The University  
**Solid State Devices**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## SOUTHAMPTON

Sept. 23-26 The University  
**Optical Properties of Thin Films**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## TEDDINGTON

Feb. 20 & 21 National Physical Lab.  
**Precision and Accuracy in Pressure and Force Measurement**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## UXBRIDGE

Apr. 30-May 2 Brunel University  
**Instrumentation in Vacuum Processes**  
 (Inst. Physics, 47 Belgrave Sq, London SW1X 8QX)

## WARWICK

July 16-19 The University  
**Software for Control**  
 (I.E.E., Savoy Place, London WC2R 0BL)

## OVERSEAS (JAN.-APR.)

Feb. 14-16 Philadelphia  
**International Solid-State Circuits**  
 (I.E.E.E., 345 East 47th St, New York, N.Y. 10017)

Feb. 20-22 Rotterdam  
**A.E.S. Convention**  
 (Herma A. O. Wilms, Zevenbunderslaan 109, B-1190 Vorst-Brussels)

Mar. 6-10 Basle  
**Medical Electronics and Bio-engineering**  
 (Sekretariat MEDEX 73, CH-4021 Basle)

Mar. 6-10 Basle  
**INEL 73 — Industrial Electronics**  
 (Sekretariat INEL 73, CH-4021 Basle)

Mar. 20-Apr. 5 Peking  
**British Industrial Technology Exhibition**  
 (Tek Translation & International Print, 11 Uxbridge Rd, London W12 8LH)

Apr. 2-7 Paris  
**Audiovisual and Communication Exhibition**  
 (Société pour la Diffusion des Sciences et des Arts, 14, rue de Presles, 75740 Paris)

Apr. 2-7 Paris  
**Electronic Components Exhibition**  
 (Société pour la Diffusion des Sciences et des Arts, 14 rue de Presles, Paris-15eme.)

Apr. 3-5 Dayton  
**Military Airborne Video Recording**  
 (Society of Photo-optical Instrumentation Engineers, P.O. Box 288, Redondo Beach, Calif. 90277)



# Magnetism and Magnetic Units

## Understanding the basic relationships, with special reference to SI units

by "Cathode Ray"

The other day I saw—on 'Nationwide', I believe—something about a shopkeeper who persisted in doing business in £sd. (Even he admitted that he wouldn't actually refuse decimal coins. What he thought of paint by the litre and timber by the metre, assuming he was a DIY man, wasn't revealed, probably because his opinion of them wouldn't have been unusual enough to rank as news.)

SI\* units, or at least those included in the mksA system, have been with us far longer than decimal coinage. The mks (metre-kilogram-second) system was proposed by Prof. G. Giorgi as long ago as 1901, and although more than 30 years passed before much notice was taken of it, when the break came (as it did in electrical engineering—after the addition of the ampere—more than 20 years ago) the change-over was much faster than the most optimistic had expected. Yet there is still a pocket of resistance that goes on using cgs units though all others have stopped. I mean the people concerned with magnets and magnetism.

Practically everybody uses magnets, in such things as loudspeakers, magnetic pickups and microphones, tape heads and television receivers for example, but not many are so much involved with them as to have to use magnetic units, or, more correctly perhaps, units of magnetism. May be it is because these are a relatively small group, confined largely to Sheffield†, completely single-minded in their devotion to the task of producing ever better magnets, that they are out of touch with the rest of the technological world in this (to them) unimportant matter. Like the Japanese sergeant found in some remote spot in Indonesia, they don't know that the (units) war has been over for 20 years. To be fair, one must admit that there are other possible reasons for this backwardness. It is all very well for the rest of the technological world to be self-righteous about their own acceptance of SI units; their volts and amps and watts and even henries were completely unaffected by the change. In so far as magnetic magni-

tudes have to be considered by some, this was usually a small part of their whole world and the new units could be accepted without too much upheaval. But for specialists in magnetism, cgs units were part of their tradition, and much greater mental adjustment was required. And even now, when challenged they can claim more than mere mental inertia as an excuse: with some justification they can retort that reckoning flux density per square metre is not strikingly appropriate in this day and age of microelectronics. Square centimetres are much nearer the mark, especially in the loudspeaker magnet trade. Their reasonableness in pleading against the inconvenience of having to specify a typical magnet flux as, say, 0.0015 webers may at this point be adulterated by a certain amount of low commercial cunning, since 150,000 maxwells is much better calculated to impress potential customers. Another argument that will undoubtedly be raised is the convenience of the cgs permeability of air being equal to 1, instead of  $4\pi/10^7$  as in SI.

So the magnet trade at least may be hard to convince. Perhaps a better line to take with them than extolling the virtues of SI (which they will have difficulty in seeing, even if they want to see them, which is unlikely) is the negative approach—to point out that there is no more future for cgs units than for £sd coinage. Their sons—and daughters—are being brought up on SI, and most fathers don't like to be seen as squares in their own business. And even their hi-fi customers, looking up the current loudspeaker lists as I am just now, may soon be wondering what these gauss and maxwells—and even 'lines'—are. When the magnet men realize they are talking an archaic language to the new generation of big money spenders they will change.

The readers I have in mind are not the members of the magnet trade, nor the young who know only SI, but those who were brought up on cgs and are not yet too handy with SI, together with all who are hazy about magnetic quantities of any kind and their relationships to the familiar amps and volts and ohms.

So first of all I will show how magnetic circuits correspond to electric circuits. I know that this is an extremely unoriginal procedure, found in nearly all the elementary books. I used it myself in the September 1947 issue, but even if you had been born by

then you would hardly remember it. And I know that superior persons, looking for a chance to demonstrate their superiority, will point out that this is a false analogy, since magnetic flux corresponds to electric flux, not current. But practically nobody outside the classroom, and few of those inside it, are really familiar with electric flux and elastance. It is a basic principle of teaching that the obscure should not be explained in terms of the more obscure. So I'm going to liken magnetic flux to electric current, with the warning that there is a more perfect analogy to come later.

I hopefully assume that everyone who is still with us understands Ohm's Law. No; I'm not thinking of the pedantic aspects of it that were my subject in the August 1953 issue and can be seen to this day in "Second Thoughts on Radio Theory". All I mean is the relationship between volts, ohms and amps ( $I = E/R$ ), and how resistance depends on the dimensions and resistivity of the circuit or part of a circuit concerned. So, in Fig. 1, the resistance of the bit of wire is

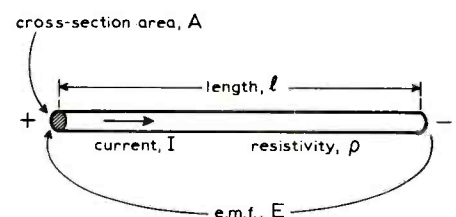


Fig. 1. Ohm's law applied to a piece of wire to find the current flowing through it, given the dimensions and resistivity of the wire and the e.m.f. applied to it.

directly proportional to its length  $l$  and to the resistivity  $\rho$  of the metal, and inversely proportional to the cross-sectional area  $A$ :

$$R = \frac{\rho l}{A} \quad (1)$$

This is true whatever the units of  $R$ ,  $l$  and  $A$ . But the value of  $\rho$  depends on those units. In SI the basic unit of length is the metre, so  $\rho$  is the resistance between two opposite faces of a metre cube of the material, and in the equation  $l$  must be in metres and  $A$  in square metres, or metres<sup>2</sup> as we are encouraged to write it. There is nothing to stop

\*Système Internationale d'Unités.

†To forestall indignant retorts, or even physical assault, from citizens of Sheffield, I would assure them that I have no wish to bring their city into contempt. By all accounts it is an admirably progressive one, not least in the reduction of atmospheric pollution.

us reckoning  $A$  in square millimetres ( $\text{mm}^2$ ) if we prefer, so long as we allow for this deviation by dividing by  $10^6$ . For ordinary circuit materials  $\rho$  is a constant at any one temperature, which is more or less what Ohm was on about. (He didn't know anything about volts, amps, or even ohms.) For metals  $\rho$  increases slightly as the temperature rises. For a lot of other things it falls. And for electronic devices it depends mainly on  $V$  or  $I$ , but of course Ohm knew nothing about them.

One must admit that this resistance formula (1) is not very often used in practice. The resistance of wire is given in tables, and the resistance of resistors is shown by the colour code they bear. If in doubt one can easily measure the resistance with the usual multirange meter. The resistances of electronic devices cannot be calculated by the formula, because  $\rho$  is unknown; anyway, one is not usually interested in their resistances as such so much as in the varying relationship between  $E$  and  $I$ , given by characteristic curves. The main purpose of eqn. 1 is to provide a clear picture of how units of resistance depend on circuit dimensions.

So much for the recapitulation. Now for the analogy. To change over to a magnetic circuit, for electromotive force  $E$  volts put magnetomotive force  $F$  amps (yes!), for current  $I$  amps put magnetic flux  $\Phi$  webers (Wb), for resistivity  $\rho$  put reluctivity  $\nu$ , and for resistance  $R$  ohms put reluctance  $S$  amps per weber (A/Wb). (Note: ohms could be called volts/amp, which would make the resemblance of form still closer. Incidentally, in specifying the full-scale current drain of voltmeters, their manufacturers call amps ohms per volt, but in this case the reason is unknown.)

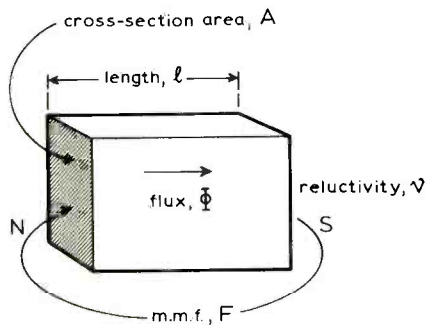


Fig. 2. This is a magnetic analogue of Fig. 1, showing how the magnetic flux in a block of (say) iron can be calculated.

In Fig. 2 we have, say, a piece of iron such as a pole-piece forming part of a magnetic circuit. Following the same reasoning as for Fig. 1 we get

$$S = \frac{\nu l}{A} \quad (2)$$

In both diagrams  $A$  has deliberately been made constant throughout the length  $l$  to avoid bringing in mathematical complications that would distract attention from the main principle. Although for our theoretical purposes  $A$  and  $l$  could have been made the same sizes in Fig. 2 as in Fig. 1, in practice magnetic circuits are generally made short

and fat because (1) the object is usually to make  $\Phi$  as large as possible, and (2) whereas the resistivity of the space surrounding an electric circuit is usually high enough for practically no current to leak into it, reluctivity is never very low so leakage of magnetic flux could be considerable in a long narrow circuit. There is no such thing as a magnetic insulator.

In case anyone is puzzled by reluctivity it might be helpful to reveal that it is the reciprocal of the better known permeability,  $\mu$ ; i.e.,  $\nu = 1/\mu$ . If you prefer you can put permeability in Fig. 2 and substitute the corresponding quantity conductivity,  $\gamma$ , in Fig. 1. But I thought we might make a bad start if we encountered this rather unfamiliar quantity so soon.

Permeabilities or reluctivities, take your choice, are almost the same for all materials—including empty space—other than those called ferromagnetic, for which  $\mu$  can be many thousands of times greater and varies enormously according to the degree of magnetization. In fact, such materials correspond very much to electronic devices in electric circuits; characteristic curves are needed, and electronic current and magnetic flux are both limited by saturation.

Before we can tackle magnetic units we have to consider how  $\Phi$  and  $F$ , and other magnetic quantities not shown in Fig. 2, are related to current and voltage. We must make perfectly sure we don't confuse these relationships with the analogy we have just been considering. It would have been better if we could have illuminated magnetic quantities in Fig. 2 by some analogy with totally unrelated quantities, say the flow of tomato chutney along a pipeline on its way to the bottling department; but chutney-motive force is not a sufficiently familiar concept to come within our basic principle of education, and there are other flaws in the analogy. It happens that Ohm's Law is clearer and simpler and better known than any other valid analogy I could call to mind. But now, having I hope got a clear picture of Fig. 2, let us forget about Fig. 1.

We all know that when an electric current flows it sets up a magnetic field around itself (Fig. 3). And that the strength of this field is directionally proportional to the current. Does it depend on anything else? As a one-time famous broadcaster would so rightly have said, it all depends on what you mean by a magnetic field. I've used the term as vaguely as I suspect many people, even some readers of *Wireless World*, think about it. That is exactly why I'm trying to clarify the matter. There are various approaches, but as we have already established a magnetic 'Ohm's Law' let us begin there, without stopping yet to explain exactly what is meant by a magnetic field.

Whatever it is it can be supposed to be caused by what we already know as a magnetomotive force, hereafter to be abbreviated to m.m.f. in line with e.m.f. It in turn is caused by electric current, and depends on nothing else. That is, if you follow the modern practice and count the total current around which the m.m.f. is considered. So if there are 50 wires close together, each carrying 0.1A (usually because the wire is wound into a 50-turn coil) the effective

current is 5A. Formerly one would have said 5 ampere-turns. The main object of SI being to exclude all illogical constants in the relationships between the basic units, the SI unit of m.m.f. has been so chosen that it is numerically equal to the current that creates it. That is why the name of the unit of m.m.f. is the same as that for the basic unit of current—the ampere.

M.m.f. is not directly useful, but only as a cause of magnetic flux; just as e.m.f. is not directly useful for creating magnetism, but only as a means of making the current flow. And just as the amount of current a given e.m.f. will cause to flow in a circuit is decided by the resistance of the circuit, so

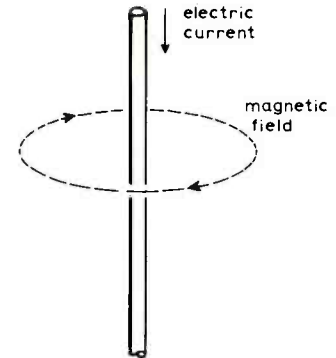


Fig. 3. The basic relationship between an electric current and a resulting magnetic field

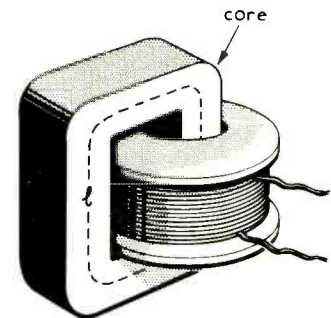


Fig. 4. Here the magnetic circuit linked with a current-carrying coil is assumed (for simplicity) to be confined to a high-permeability core of uniform cross-sectional area  $A$  and mean length  $l$ .

the amount of flux a given m.m.f. will cause in a magnetic circuit is decided by the reluctance of that circuit. In practice one usually looks at it from the other end: knowing that a certain amount of flux has to be provided, how much m.m.f.—in terms of current and number of turns—is needed?

This can be quite difficult. The shape of a magnetic circuit is usually decided by what it is for. In any case the whole circuit around the current cannot be of the ideal rectangular shape shown in Fig. 2. Assuming that one wants to produce the maximum flux for the minimum m.m.f.—in other words to have as little reluctance as possible—eqn. 2 shows that we would choose one of the special alloys with a very low  $\nu$ , or high  $\mu$ . Makers of these alloys supply data showing the values of  $\mu$  under various conditions. One



of the many forms of core made of such materials is shown in Fig. 4. It is quite possible to make  $A$  constant throughout, or nearly so; and although  $l$  varies according to distance from the centre an average figure can be used, and so the reluctance of the whole circuit can be calculated reasonably well.

It is seldom as simple as this. Very often, as in electric motors and generators, loudspeakers and moving-coil meters, the flux has to pass through an air gap to be of any use. When the gap is of such a shape that  $A$  and  $l$  are constant, its reluctance can easily be calculated,  $\mu$  for air being known very accurately, though one has to allow for edge effects. Because  $\mu$  for the core is usually so enormous in comparison, the core reluctance can sometimes be neglected, so letting one off the problem of ascertaining it. Another help is to remember that just as resistances in series add up, so do reluctances, and one can split up the magnetic circuit into separate parts, each needing a certain m.m.f. to carry a given flux. (This is analogous to Kirchhoff's voltage law.)

You may be bursting to tell me that most of the magnets in which *Wireless World* readers are likely to be interested are permanent magnets, for which no current is needed. Actually they too require current to cause the required m.m.f., but the molecules of the magnet material itself are so aligned that the electrons circulating in them constitute the necessary current. (In all other materials the alignment is random or in direct opposition, so the magnetic effects of these tiny currents cancel out.) One would have to be rather unusually bright at physics to predict the effective m.m.f., but fortunately the suppliers of permanent magnets also provide all the necessary data. The units used are (or should be) the same as for electromagnets; the theory is too much to push in here and now, and in any case can be understood more easily when we have covered magnetism generally. I may get around to it later, but meanwhile if you can see the March 1961 issue you will find it all there.

If you look up magnet or magnet core data you are likely to find most of it in terms of  $B$  and  $H$ , with  $\Phi$  and  $F$  and  $S$  hardly mentioned, if at all. Even  $\mu$  may not be specified directly, although it seems to be the most important factor in reluctance. To understand these omissions, let us take a look at a curve of  $\Phi$  against  $F$  for some magnetic material such as iron (Fig. 5). The slope of this curve will be  $\Phi/F$ . Our magnetic 'Ohm's Law' is

$$\Phi = \frac{F}{S} = \frac{F\mu A}{l}$$

So 
$$\frac{\Phi}{F} = \frac{\mu A}{l} \quad (3)$$

The dimensions of the piece of iron,  $A$  and  $l$ , being fixed, we see that the slope is proportional to  $\mu$ . To find the actual value of  $\mu$  we would have to multiply the slope by  $l$  and divide by  $A$ . This way of presenting the data is silly, because we are not interested in the figures for the piece of iron that the manufacturer's lab people happened to use for their tests, but in the properties of that par-

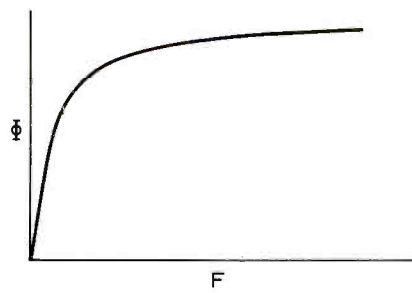


Fig. 5. A graph of flux against m.m.f. for a ferromagnetic material would apply to only one particular size and shape. But by suitable choice of scales of flux density against magnetic field strength the same graph is made to apply to that material in any size and shape.

ticular material, which we can then use to tell us about a piece of the size and shape we might want to use. One way would be to measure a unit cube of the material, so that  $l$  and  $A$  were both =1. But this would restrict the method of measurement very inconveniently, especially with SI units, for a metre cube of iron weighs about 8 tons.

A better idea is to have units that will refer to unit dimensions of the material. So instead of  $\Phi$ , the total flux, we use the flux passing through unit cross-sectional area: the flux density, denoted by  $B$ , in  $\text{Wb/m}^2$ , called teslas (T); and what is called magnetizing force or magnetic field strength,  $H$ , in  $\text{A/m}$ . Rearranging eqn. 3 we get

$$\frac{\Phi}{A} \cdot \frac{l}{F} = \mu$$

So 
$$\mu = \frac{B}{H} \quad \text{or} \quad B = \mu H$$

For the reason just explained I didn't bother to provide Fig. 5 with scales, but if  $B$  is written in place of  $\Phi$  and  $H$  in place of  $F$  then numerical scales would apply to that material in general, regardless of size or shape. (There are exceptions, called anisotropic materials, 'anisotropic' meaning that their properties are not the same in all directions, like wood having different properties along and across the grain.)

Sometimes one comes across data curves showing  $\mu$  directly in terms of  $H$  or  $B$ . From the typical  $B/H$  curve shape in Fig. 5 we can see that the permeability (=slope) begins high and continues so over a range, beyond which it falls off rapidly towards a certain flux density, called saturation, which is not much more than for air. Under these conditions there would be a lot of leakage flux outside the iron.

Since most magnetic data and calculations are in terms of  $B$  and  $H$ , referring back to Fig. 1 we may wonder why the same policy is not adopted there, replacing current by current density and e.m.f. by electric field strength. Well, if I had started from the more strictly appropriate analogy, comparing magnetic fields with electric fields, that is just what one would do. Because one is interested in electric fields mainly in non-conducting spaces (inside a cathode-ray tube, for example) current is replaced by electric flux, which is treated like magnetic

flux and reduced to flux density or displacement. For an overall grasp of electric and magnetic theory it is very helpful to consider this analogy in detail, but I assumed that from a more practical standpoint most people are familiar with electric circuits and would like to be clearer about magnetic circuits and fields.

While we are on about fields we might look again at Fig. 3. If the current flowing through the wire (or group of wires) is called  $I$ , we now know that the m.m.f.  $F$  encircling the wire—at any distance from it—is equal to  $I$ , both  $I$  and  $F$  being reckoned in amps. But because the path length around—call it  $l$  again—is proportional to the distance  $r$  from the axis of the wire, being in fact equal to  $2\pi r$ , the m.m.f. is spread over a greater circular length as the distance from the current is increased. So the magnetic field strength

$$H = \frac{F}{l} = \frac{I}{2\pi r}$$

In words, it is inversely proportional to the distance from the current that causes it. We are assuming—in case you didn't know—that the whole of the space around the wire has the same permeability and contains no currents or magnets to upset the cylindrical distribution of field around the wire.

If your information on magnetism was obtained some time ago you may have been wondering why I've about come to the end of this exposition without having ever mentioned 'unit magnetic pole'. Most of the books used to base their treatment of magnetism on it. The more honest of them admitted that no such things exist, which is why I've ignored them. It is rather different with the analogous electrical concept, unit electric charge at a point, because electrons and protons are as near as you like mobile point charges. Another item that has been perhaps conspicuous here by its absence is the 'line of magnetic force', so much used in 'explaining' magnetic fields. They don't exist either, and can be actually misleading if they are allowed to convey the impression that the spaces between are any less magnetic than the lines themselves. But, like the lines cartoonists draw radiating from persons experiencing intense emotion, they at least help one to visualize something that does exist. In particular, they show on a diagram the directions along which a magnetic field acts; for example, in Fig. 3, in circular paths around the current. If there were such things as mobile magnetic poles of negligible size, these are the paths along which they would be moved.

No; I haven't forgotten that I set out to enlighten any who are still groping in cgs twilight. The fact that cgs units don't fit in with the familiar electrical units such as volts and amps has already been mentioned as one of their disadvantages. Another is the fact that there are two cgs systems of units, one based on unit electric charge and the other on unit magnetic pole, and their units differ from one another and from the practical units by factors usually of many millions. Another snag is that unit charge and unit pole were each said to give rise to a flux of  $4\pi$  units. The reason for this apparently odd choice was that unit flux density

was defined to exist at unit distance from the unit point source of flux. The surface area of the sphere of unit radius is  $4\pi$  units, so if the flux emerging through unit area of the surface is 1 the total flux must be  $4\pi$ . By starting on this basis, the originators of the cgs systems eliminated the factor  $4\pi$  precisely where one ought to find it—in a situation of spherical geometry. The result was that the factor  $4\pi$ , expelled from where it rightly belonged, broke out in places where its presence could not be justified by the geometry; for example, in the formula for a parallel-plate capacitor.

And in the relationship between current and m.m.f. My electrical engineering tutor, whenever a student was stuck at a problem, sat down opposite him, scribbled on a sheet of paper with a circular motion to represent a current-carrying coil; then repeatedly smiting its interior with the point of the pencil to represent end views of lines of force, hissed 'Magnetomotive force is point four pi times the current enclosed!' This relationship took into account the irrational  $4\pi$  and the fact that the electromagnetic cgs unit of current was 10A. Nowadays even the densest student should be able to retain the SI relationship 'Magnetomotive force is equal to the current enclosed' without having to be constantly reminded of it.

Fig. 4 shows that interrelated current and magnetic flux are like adjacent links of a chain. We have considered how current in the coil causes an m.m.f. linking the current path. Faraday's greatest discovery was that a change in magnetic flux causes an e.m.f. linking the flux path. The electromagnetic unit of e.m.f. was quite logically defined as that induced when interlinked flux was changing at unit rate (1 maxwell) per second. But unfortunately this turned out to be  $1/10^8$ V, or  $0.01\mu$ V, which is small even by circuit noise standards. The electrostatic cgs unit of e.m.f., by contrast, is about 300V, because the ratio between the units of e.m.f. in the two systems is equal to the speed of light in centimetres per second. To the uninitiated this might seem as irrelevant as the diameter of the earth or the price of beer. The connection lies in the fact that in both cgs systems the permeability and permittivity of empty space ( $\mu_0$  and  $\epsilon_0$ ) are both fixed as 1. Now one just can't have it both ways like this. The reason is that the speed of light ( $c$ ) is equal to  $1/\sqrt{\mu\epsilon}$  for the medium in which it is travelling, so in space is  $1/\sqrt{\mu_0\epsilon_0}$ . The only way to make  $\mu_0$  and  $\epsilon_0$  both 1 is to choose units of length and time such that  $c = 1$ . If the second is retained as the unit of time, then the unit of length must be 299,792,800 metres. Anyone who proposed this as the standard would have no political future.

The inevitable result of making unit length 1cm at the same time as  $\mu_0 = \epsilon_0 = 1$  was the emergence of two cgs systems, depending on whether  $\mu_0$  or  $\epsilon_0$  was chosen as basic, in which units of the same quantities differed by factors of  $c$  or  $c^2$ . And the real values of  $\mu_0$  and  $\epsilon_0$ , which actually are related to  $c$ , had to be hidden away in the sizes of the various units. So most of them are wildly impractical. The emcgs unit of resistance, for example, is 0.001 microhm,

Quantity	Symbol for quantity	Unit	Abbrevn. for unit		emcgs equivt.
Magnetomotive force	$F$	Ampere	A	In practice, the ampere-turn	$0.4\pi$ gilberts
Magnetic field strength	$H$	Amp. per metre	A/m	$= F/l$	$4\pi 10^{-3}$ oersteds
Magnetic flux	$\Phi$	Weber	Wb	$= AB$	$10^8$ maxwells
Flux density	$B$	Tesla	T	$= \mu H$	$10^4$ gauss
Permeability	$\mu$	Henry per metre	H/m	$= B/H$	$10^7/4\pi$ greater
Permeability of space	$\mu_0$	Henry per metre	H/m	$= 4\pi 10^{-7}$	ditto (=1)

while the escgs unit is about a million megohms. SI works on a different principle. By changing over to the metre and kilogram for length and mass, and using the ampere as the unit of current, all the 'practical' electrical units became parts of it, and new magnetic units emerged from them on the same principles. And so the SI unit of m.m.f. is equal to the current enclosed instead of  $0.4\pi$  times it. And when the magnetic flux is changing at unit rate per second the e.m.f. induced along a linked path is 1 volt.

Does this mean that  $\pi$  no longer appears in electromagnetic equations? Not at all; it means it appears where it logically ought to —as  $2\pi$  in cylindrical geometry and  $4\pi$  in spherical geometry, but not in rectangular geometry. The cgs systems were as confusing as a system of measures would be in which the unit of length was such as to make the surface area of a sphere one unit of length-squared.

Of course there is always a snag. Instead of the convenient values of 1 for space permeability and permittivity we have  $4\pi/10^7$  and approximately  $1/(36\pi \times 10^9)$  respectively. So  $\pi$  and large powers of 10 get back in by the rear entrance! However, it is easier to remember these two values than to have to remember the correct constants for innumerable formulae. If dirt has to be swept under carpets, it is better to have it swept under two already dirty ones if we can rely on there being none anywhere else. There is even something to be said for  $\mu_0$  and  $\epsilon_0$  not being 1. When they were, students were often led to suppose that  $H$  and  $B$  were more or less the same thing and  $\mu$  just a multiplier to take account of the properties of magnetic materials. Then they got into difficulties with the dimensions of equations.

What, then, are the dimensions of  $\mu$  and  $\epsilon$ ? The best clue to  $\epsilon$  is the way the capacitance between two parallel plates is calculated. It is proportional to  $A$ , the area of the space between the plates, and to  $\epsilon$ , the permittivity of whatever occupies that space. And it is inversely proportional to  $l$ , the (uniform) distance between the plates. (Edge effects are neglected, or counteracted in some way.) So in any regular system of units

$$C = \frac{A\epsilon}{l}$$

Therefore

$$\epsilon = \frac{Cl}{A}$$

In SI units,  $C$  is in farads,  $l$  in metres and  $A$  in metres<sup>2</sup>. So  $\epsilon$  is farads  $\times$  metres  $\div$  metres<sup>2</sup>, or farads per metre. Going back to the electrical circuit analogy, we would find in the same way that conductivity ( $\gamma$ ) was in siemens (formerly mhos) per metre, and  $1/\gamma$  (=resistivity,  $\rho$ ) was ohm-metres. An alternative that used to be used was ohms per metre cube, and similarly for the other things; but this looks as if it restricted the measurement to a piece of a particular shape and size of the material tested.

As the analogue for capacitance is inductance we start to get at  $\mu$  from there. The inductance ( $L$ ) of a coil—say the one in Fig. 4—is equal to the flux linked with it when unit current flows through it. If we neglect flux in the surrounding air, and use eqn. 3 we have, when  $F$  is one unit and  $\Phi$  is therefore equal to  $L$ ,

$$\mu = \frac{Ll}{A}$$

So  $\mu$  is in henries per metre.

To sum up, here is a table of the SI magnetic units:

## PUBLICATION DATE

We regret it has not yet been possible for us to get back to publishing on the third Monday of the preceding month. The February issue will not, therefore, appear until February 2nd.



# A 200-MHz Counter Prescaler

## An add-on unit to extend frequency measurement

by D. J. Taylor,\* B.A., G8ARV/G6SDB/T

Direct digital frequency measurement has come well within the amateur's price range this last year due to the introduction of ultra fast logic intended for high volume computer applications. As these circuits are produced by several manufacturers, price competition has resulted in savings for the amateur too. With only £5 worth of integrated circuits, it is possible to build a prescaler which combines 2mV low-frequency sensitivity with a 200MHz measurement ability. Here such a prescaler is described and there are three possibilities for its use:

- As an add-on unit for heterodyne or similar frequency meters, where the indicated readings are multiplied by four to obtain the true frequency.
- As an additional unit for a home-built frequency counter, where the timebase can be modified to include a scaling factor of four.<sup>1</sup>
- With an additional divide-by 25 circuit (not described here) so that the net frequency division is by 100 times. As the output frequency does not exceed 2MHz, this would be suitable for direct reading with an older vintage of counter.

The range of i.c.s which form the basis of the described design, is the Motorola MECL 10000. This is an e.c.l. (emitter coupled logic) family introduced in 1971 which uses current steering rather than

saturated transistor switching. This technique avoids the delays normally associated with transistor charge-storage mechanisms.<sup>2</sup>

Current steering logic has various advantages:

- It can drive 50Ω lines directly.
- It generates fewer supply line transients because of the balanced nature of the circuit.
- Each gate consists of a differential amplifier, which makes interfacing to analogue signals easier than with t.t.l.

The price to be paid for these advantages is a higher power consumption noticeably in the "pull-down" resistors required on the emitter follower outputs.<sup>3</sup> However, the basic gate has a power-speed product (a parameter used by semiconductor manufacturers to sell their devices) second only to that of low-power Schottky t.t.l. which is very much more expensive at this time and availability is poor. Practical advantages of the MECL 10000 series are, the fastest operating speed per pound, ease of electrical operation, and good availability.

Using only two i.c.s this prescaler simply takes a low-level sinewave signal, amplifies it to the levels required by the logic circuit which then divides the frequency by four.

### Pre-amplifier, limiter and divider

The MC10116 (*IC*<sub>1</sub>, Fig. 1) is a triple line-receiver which consists of three wideband differential amplifiers, each having a voltage

gain of 16 (differential input to output). A possible way to use this device is as a pre-amplifier (two stages) and a Schmitt trigger. However, this results in a poorer low-frequency sensitivity and a lower high-frequency limit than can be achieved. A better way to use this i.c. is as a broad-band limiting amplifier, using differential interconnection between the stages. In this way a sensitivity of a few millivolts at 10MHz and about 100mV at 200MHz can be achieved.

The MC10131 (*IC*<sub>2</sub>, Fig. 1) is a dual D-type flip-flop which in this circuit is used as a toggle-bistable to give a frequency division of four times. It can drive loads directly and is guaranteed to toggle at 150MHz.

At the time of writing the following one-off prices were quoted MC10116 - £1.12, MC10131 - £3.93, making the total semiconductor cost £5.05.

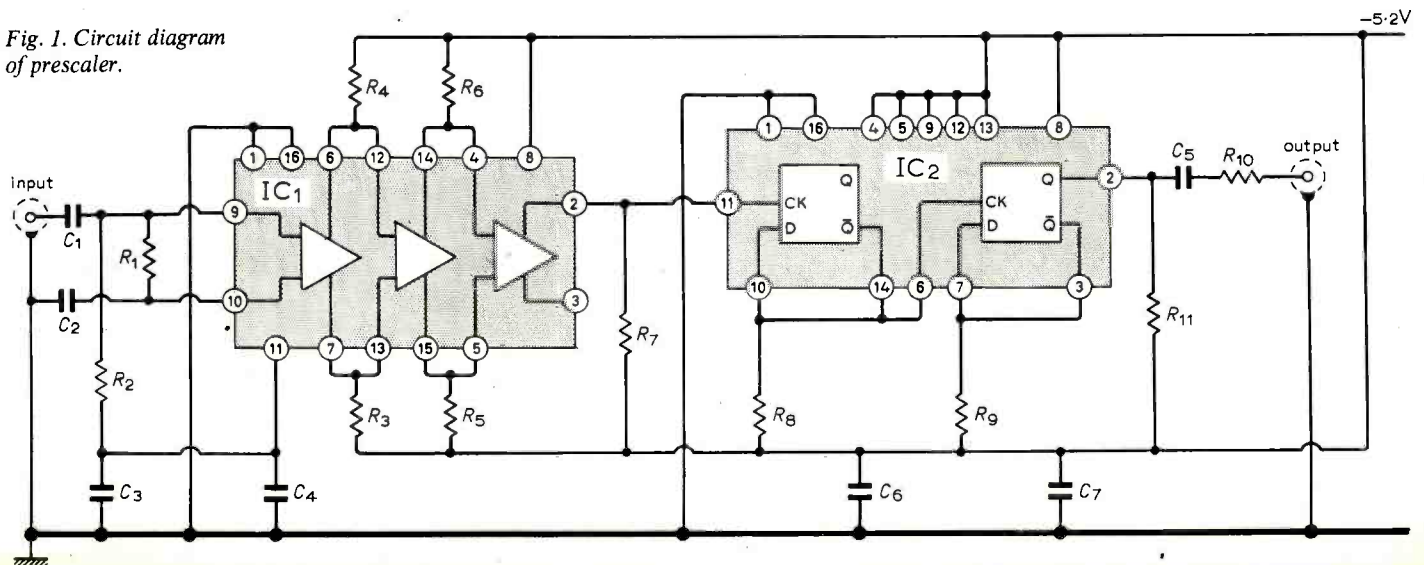
### Circuit details

The input has been designed to match either 50 or 75Ω, the expected source being a small search coil which can couple to the apparatus under test. As will be seen from the circuit diagram this is achieved by altering one resistor *R*<sub>1</sub>, which is 82Ω for 75Ω input and 56Ω for 50Ω input. The off-set voltage produced across this resistor serves to prevent the prescaler being too sensitive at low frequencies, where noise and external signal pick-up may become a problem.

The intermediate amplifiers are termin-

\*Jesus College, Cambridge.

Fig. 1. Circuit diagram of prescaler.



ated by 680Ω resistors to the negative supply, this value of resistor giving adequate bandwidth. The final stage uses a lower value resistor ( $R_7$ ), as experiments have shown that this triggers the divider more satisfactorily and makes the waveform at that point easier to monitor.

The toggle speed is limited by the first bistable and not the bandwidth of the pre-amplifier which only determines the input sensitivity. The bistable itself uses a similar low value of termination resistor ( $R_8$ ) for the first stage which is speed critical. Note that the complementary output  $\bar{Q}$ , does not need a terminating resistor for bistable operation as an extra emitter follower is included inside the device for feedback.

The output can feed either terminated or unterminated lines. If a terminated line is used, the matching resistor  $R_{10}$  should not be included and  $R_{11}$  should be decreased to 220Ω. The output will be about 800mV peak-to-peak. For unterminated lines,  $R_{10}$  absorbs the reflection produced by the open circuit, and the voltage at the open circuit is also about 800mV peak-to-peak. However, this voltage level will no longer be suitable for driving further e.c.l. circuits, as it consists of both forward and reflected waves.

The input stage of the prescaler is not protected against transients, but back-to-back Schottky-barrier diodes, MBD101 or similar, could be connected across  $R_1$  if required.

**Components List**

$R_1$	56Ω	$C_1$	10nF
$R_2$	1k	$C_2$	10nF
$R_3$	680Ω	$C_3$	47nF
$R_4$	680Ω	$C_4$	100pF
$R_5$	680Ω	$C_5$	10nF
$R_6$	680Ω	$C_6$	47nF
$R_7$	270Ω	$C_7$	100pF
$R_8$	270Ω		
$R_9$	1.5k	$IC_1$	MC10116
$R_{10}$	43	$IC_2$	MC10131
$R_{11}$	680 or 220Ω		

**Construction**

As with any circuit operating at 200MHz, lead lengths should be kept as short as possible. In the prototype this was achieved by using the lid of a tobacco tin as a ground plane and mounting the devices, pins uppermost, directly against the metal surface. This also gave some degree of heat-sinking. A photograph of this prototype is shown in Fig. 2. The layout was kept as simple as possible, with the decoupling capacitors having as short a lead length as could be reasonably achieved.

The MECL 10000 series are designed to work with positive earth and have two  $V_{CC}$  pins, 1 and 16 in this case. These are grounded as close to the package as possible. The prescaler is envisaged as a small accessory unit and the use of an insulated case in

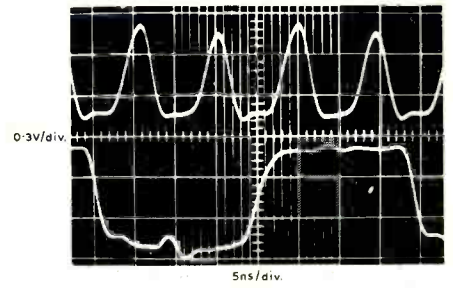


Fig. 4. 100MHz oscilloscope traces: top, pin 2,  $IC_1$ ; bottom, pin 2,  $IC_2$ . Input level 16mV, h.t. 5V.

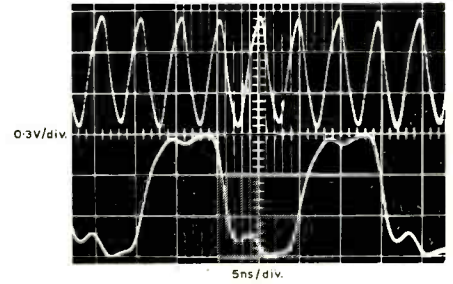


Fig. 5. 200MHz oscilloscope traces: top, pin 2,  $IC_1$ ; bottom, pin 2,  $IC_2$ . Input level 125mV, h.t. 5.5V.

which the unit will fit, will remove any problems of earth polarity incompatibility.

**Performance**

An r.f. signal generator, Marconi TF995A/2M, was fed into the input, providing excitation between 10 and 200MHz. Voltages at pin 2 of each i.c. were monitored with a Tektronix sampling oscilloscope, model 661, with a  $\times 10$ , type P6032 probe.

Fig. 3 shows the minimum voltage to provide satisfactory triggering against frequency over the range 100 to 200MHz with various d.c. supply voltages as a parameter. Signal input voltages are source e.m.f, so that 100mV plotted means 50mV p.d. or 140mV peak-to-peak. Over the range covered, higher supply voltages produced slightly faster toggling but reduced the sensitivity slightly. However, performance is largely independent of supply voltage. At 145MHz, between 28 and 45mV were required, an e.m.f. easily bled-off even a low power transmitter (45mV e.m.f. corresponds to a power requirement of 10μW when referred to 50Ω).

Waveforms for operation at 100MHz and 200MHz, are shown in Fig. 4 and Fig. 5 respectively with horizontal scale of 5ns/div and vertical scale of 0.3V/div. The sub-harmonic is clearly visible on the 100MHz trace, this being a generator imperfection. The distortion on the output waveforms is due to coupling between the two halves of the dual flip-flop package.

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3. 'General Information MECL 10000 Series', Motorola Inc., 1971, sheet O.3-4.
4. 'A 5V Logic Power supply', D. J. Taylor, *Wireless World*, March 1972.

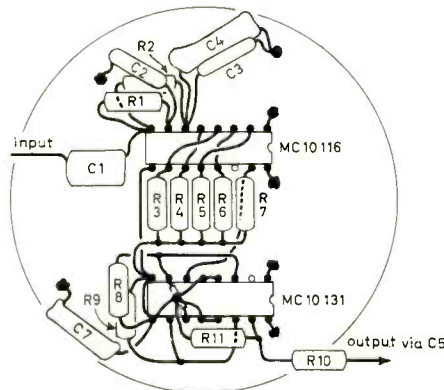
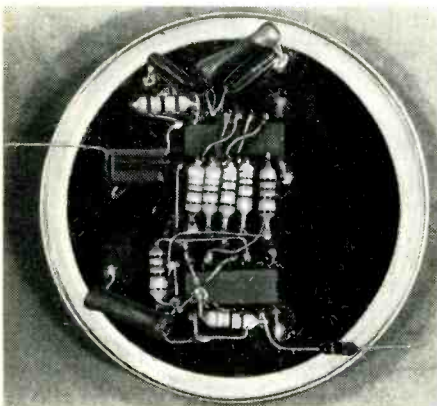


Fig. 2. Prototype construction technique showing component positions.

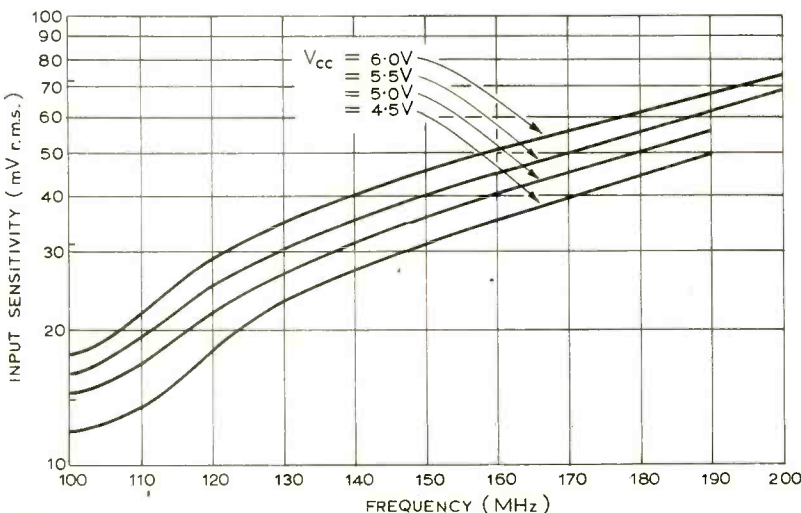


Fig. 3. Measured sensitivity for input frequency.



# Twin-ribbon Speaker

by A. E. Falkus\*, B.Sc.(Eng), F.I.E.E.

The large majority of domestic loudspeaker assemblies use moving-coil units for the bass and mid-range. For the higher audio frequencies however, a number of different types are employed.

- An ideal high-frequency unit would have:
1. A linear response between 1.5 and 20kHz.
  2. A polar distribution of 90° in a horizontal plane throughout the range.
  3. No resonances, colourations and other forms of distortion throughout the range.
  4. Efficiency equal to the average mid-range and bass speaker.
  5. Power handling ability of 30 watts.
  6. A uniform input impedance at all working frequencies.
  7. A reasonable cost comparable with mid-range and bass units.
  8. No external power supply.

The first three of these requirements are essential. For a practical system the parameters outlined in sections 4, 5 and 6 are important, whereas those of sections 7 and 8 are desirable. In many ways the ionophone principle is the most attractive. Unfortunately, to produce an ionic unit to meet the first six of our requirements, although technically possible, is too expensive to be a commercial proposition. The electrostatic principle has many adherents but fails on its inability to meet the requirement of a linear response over the desired range, having a uniform impedance—and, of course, a power supply is required.

By far the commonest form of high-frequency speaker in use at present has some form of dome-shaped diaphragm with moving-coil drive. This dome may be of a hard material, in which case it will fail our third requirement. Alternatively, the dome may be of a comparatively soft material with high internal losses. Here efficiency is sacrificed for reduced resonances but this can be recovered by the use of a more powerful magnet. Nevertheless, residual resonances are always present. It is also difficult to meet our first requirement in a single unit.

## Ribbon loudspeakers re-examined

When recently considering a replacement for the Ionofane, the above considerations led to a re-examination of the ribbon principle. The main drawback that has been associated with ribbon speakers is lack of sensitivity. Experimental models soon showed however, that provided the flux

density is high enough, the efficiency and power handling capacity can be realized by a 1/4in ribbon with horn loading.

The first ribbon speaker we built which gave the required performance had a large block built up from slabs of anisotropic ferrite magnet material with suitable pole pieces as shown in Fig. 1. The ribbon had an exponential horn with a cut off at 575Hz. This unit met all our requirements except that it was expensive. At low sound levels the quality was indistinguishable from the Ionofane while the maximum output was 20dB higher than that at which the Ionofane became overloaded. Further, improved performance at the low-frequency end of the range permitted the cross-over frequency to be reduced to 1500Hz enabling a mid-range speaker to be dispensed with.

The problem thus resolved itself into one of a magnet design to produce a comparatively high flux density in a 9/32in wide gap at a reasonable cost.

The magnet system shown in Fig. 1 suffers from the defects of being too expensive, is heavy and clumsy and the volume of the air space below the ribbon is insufficient to permit the speaker to reproduce satisfactorily the lower end of its frequency range.

The big problem in designing an economic magnet system for a ribbon speaker is that the total leakage flux between the pole pieces near the actual air gap will be many times the useful flux in the gap itself.

For example, if we apply the formula for magnet efficiency (*W.W. Jan. 1960, p. 41*)

$$E = \frac{T}{T + 3.5G} \times 100\%$$

For a 1/4in wide ribbon, *T*, the depth of gap, may be 3/32in and *G*, the width, 9/32. The efficiency thus becomes:

$$E = \frac{\frac{3}{32}}{\frac{3}{32} + 3.5 \times \frac{9}{32}} \times 100\% = 8.7\%$$

Any configuration of the magnet parts that would increase the proportion of the useful flux to the leakage flux is therefore well worth exploring.

It occurred to the writer that an improved magnet efficiency could be obtained by using a central magnet pole of square cross-section and mounting four ribbons around it, one parallel to each face, thus, in effect, using as much as possible of the inevitable leakage. This arrangement is shown in Fig. 2. A sample unit was built but the assembly of the ribbons proved very difficult. A simplified design using two ribbons,

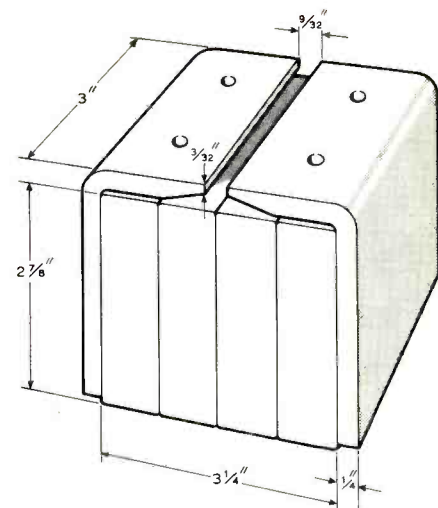


Fig. 1. The ceramic block magnet used in the prototype ribbon speaker.

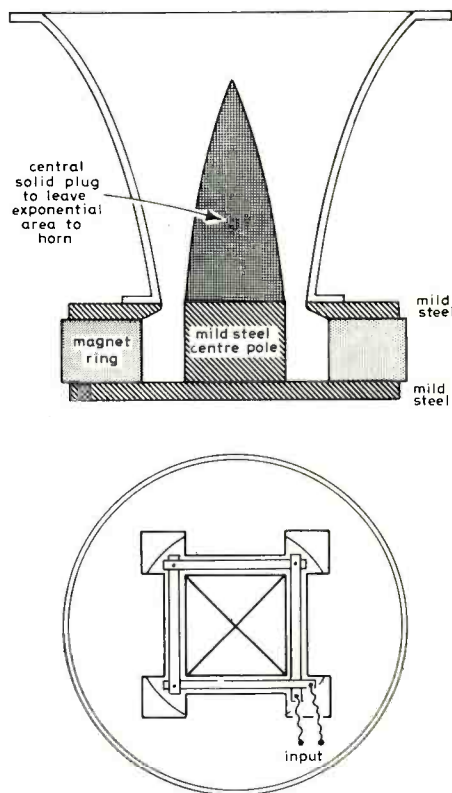


Fig. 2. A cross-section of the twin-ribbon unit and a plan view with the horn removed.

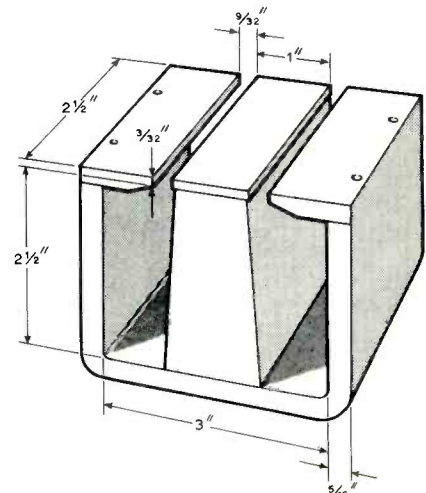


Fig. 3. The final design for the twin-ribbon magnet, which weighs 3.25lb.

\*Fane Acoustics Ltd.

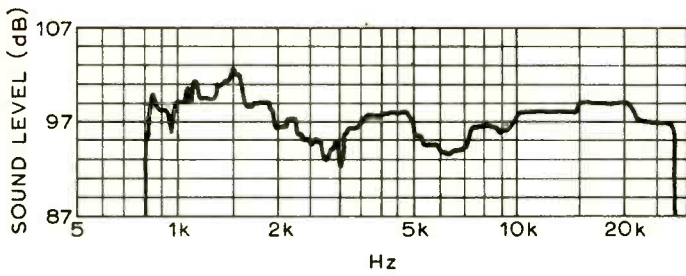


Fig. 4. Response of the unit under 'living room' conditions. Mic 1m on axis, input 4V to transformer, level relative to 0.0002 dynes/cm<sup>2</sup>.

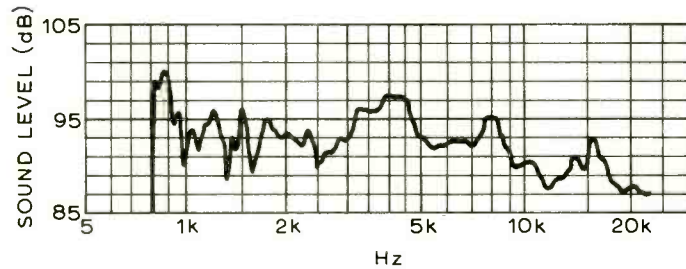


Fig. 5. Response of unit taken under same conditions as for Fig. 4 but with microphone at 0.5m and 45° off axis.

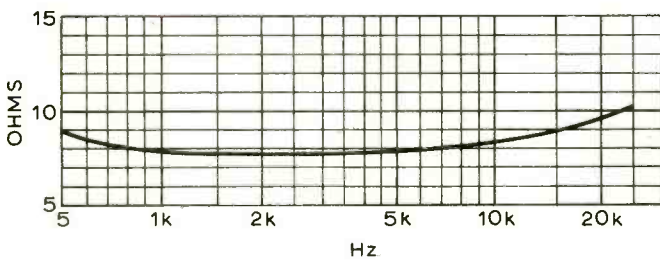


Fig. 6. Input impedance of the unit measured across the transformer primary with cross-over unit disconnected.

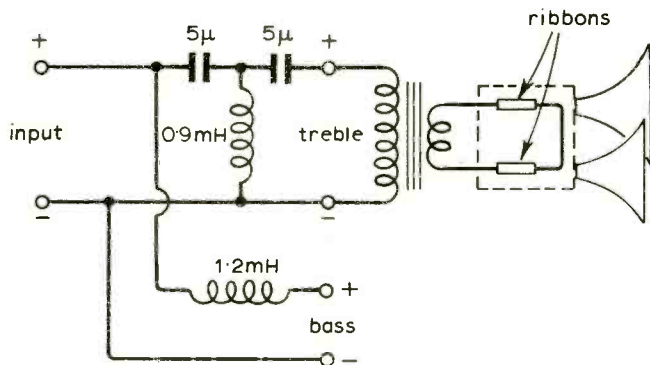


Fig. 7. The cross-over network.



Fig. 8. A view of the completed commercial unit showing the layout of the ribbons.

one to each side of the longer faces of a rectangular section metal alloy magnet, was satisfactory, however, and this forms the basis of the twin-ribbon speaker.\*

**Twin-ribbon design**

The twin-ribbon magnet is shown in Fig. 3. A central block of fully columnar magnet alloy is mounted in a 5/16in thick mild steel yoke. The magnet block is capped with a 3/32in mild steel pole tip 2½ × 1in and the magnet system is completed by two chamfered top plates. The tapering section of the magnet block is desirable since leakage flux is leaving it all the way up and reduction of the section keeps the magnet material working near its BH max point.

The two ribbons are mounted on a bakelite panel so that they are located in the air gaps, one each side of the central magnet. Each has an effective length of 2½in and they work in phase so that the total working length of ribbon is 5in. The ribbons are ¼in wide and 0.0003in thick and transversely corrugated. They are acoustically loaded with twin horns formed in a single casting and have an exponential law with a cut-off frequency of 550Hz. The ribbons are fed from a double-wound transformer at one end of the magnet, their further extremities being connected together.

This speaker will handle an input of 30W r.m.s. and produce a sound level at the mouth of the horn of 115dB. A response curve measured under living-room conditions is given in Fig. 4, and it will be seen that on the axis it is within ±3dB from 800Hz to 21kHz. At 45° from the axis in a horizontal plane there is a small fall off above 10kHz which reaches 4dB at 20kHz (see Fig. 5). The ribbon presents an entirely resistive load to the transformer but there is a small leakage inductance in the transformer of about 0.06mH causing a slight impedance rise with frequency. It will be seen however from Fig. 6 that between 500Hz and 17kHz the impedance is between 7.8 and 9.0Ω.

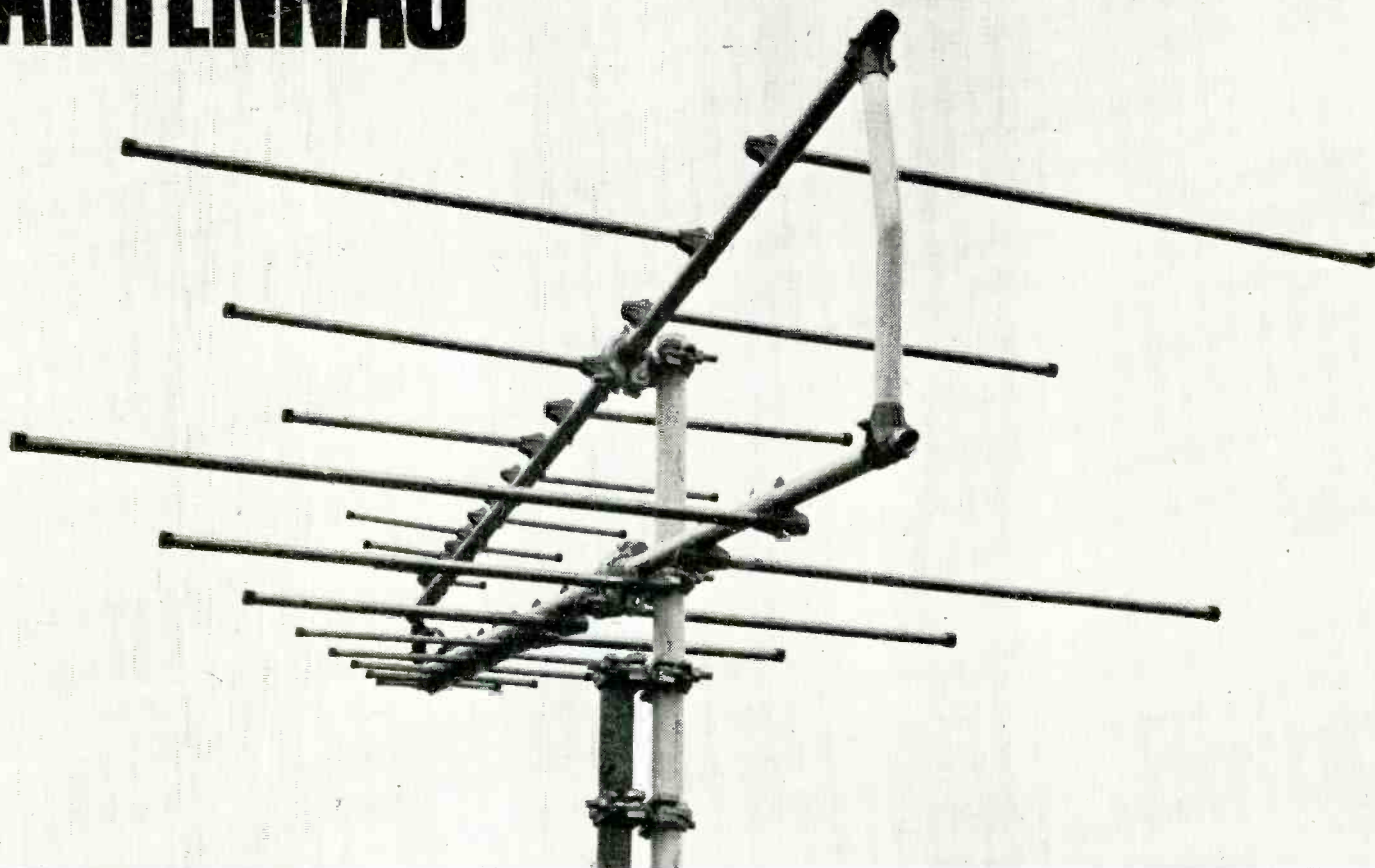
For normal use the speaker is mounted with the ribbons side by side which results in a good horizontal dispersion of the higher frequencies. As with all ribbon loudspeakers care must be exercised to prevent low-frequency signals reaching the ribbons. A small fraction of a watt at 100 or 200Hz can cause large movements, which may cause permanent stretching of the ribbon. For this reason the twin-ribbon speaker has a built-in network crossing over at 1700Hz. The circuit of this is shown in Fig. 7. The components are mounted on a printed circuit board carried on brackets from the ribbon transformer. The spaces behind the ribbons, inside the magnet assembly, are filled with sound absorbent material and sealed with plates at each end of the magnet yoke. The twin-ribbon speaker may thus be mounted in the same enclosure as a bass unit.

A photograph of the complete speaker is shown in Fig. 8. The overall dimensions are width 13in, height 6in, depth 10in, and the weight is 10lb.

\*Patent applied for.

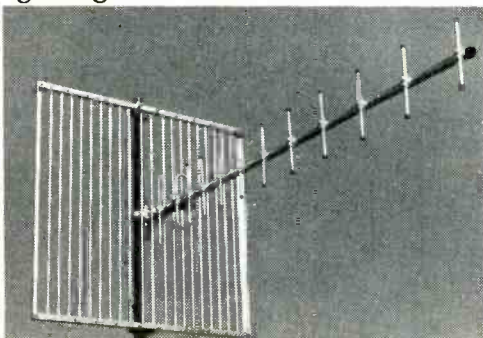
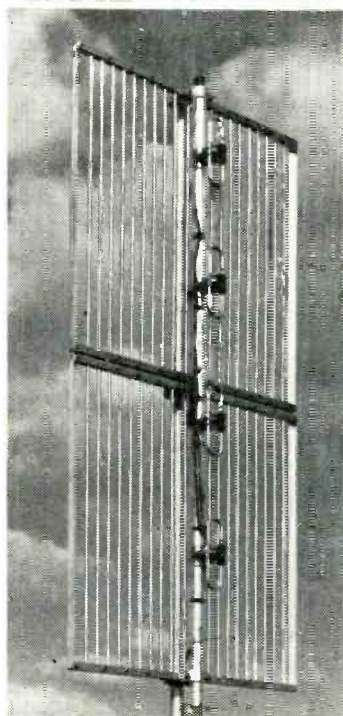


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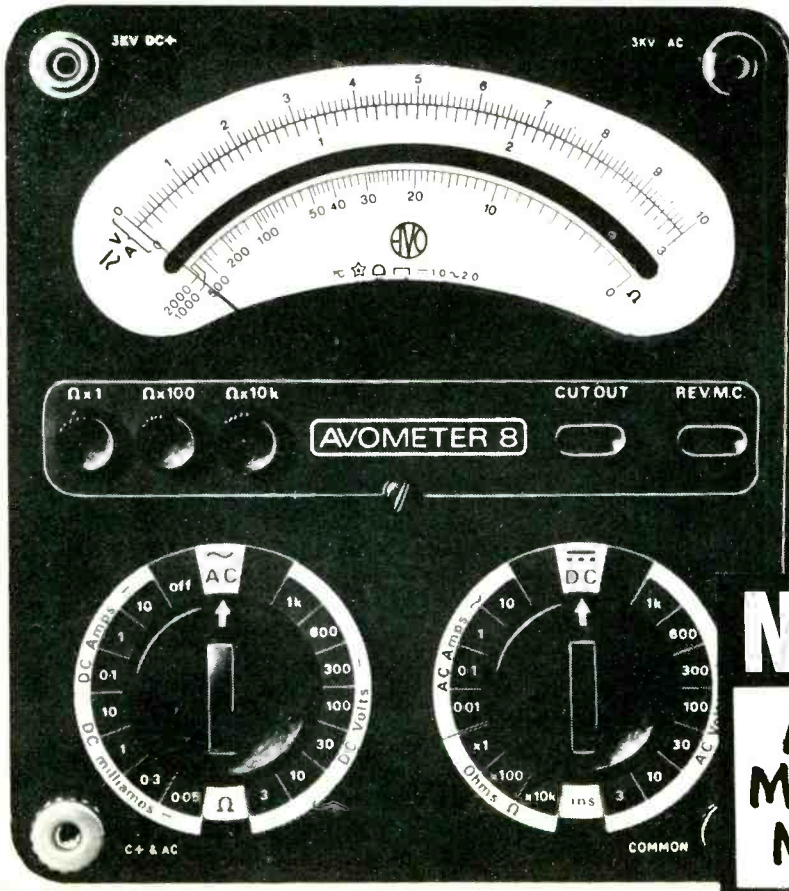
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# Circuit Ideas

## Faster slewing rate with 741 op-amp

The circuits shown enable slewing rates in excess of that offered by a standard 741 operational amplifier to be achieved. A single transistor amplifying stage is fed from the output of the operational amplifier. If the transistor stage provides a gain of  $G$ , then to achieve a given output voltage swing,  $V$ , the operational amplifier output voltage swing must be  $V/G$ . Both voltage swings occupy the same time, but the swing from the transistor stage is  $G$  times that from the operational amplifier. Therefore the slewing rate at the transistor stage output is  $G$  times that at the operational amplifier output.

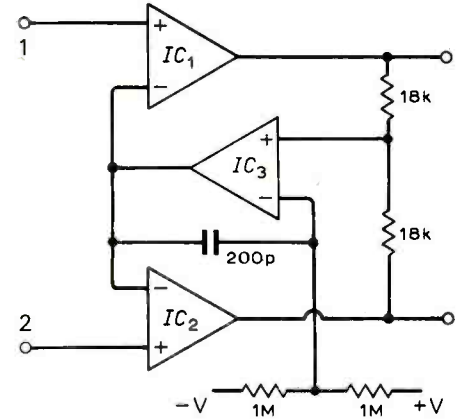
Resistor  $R_1$  must be chosen with regard to the desired output impedance and the current available from the supply. Resistor  $R_2$  is then made equal to  $R_1/G$ , where  $G$  is the desired stage gain. To utilize the available voltage swing the design should be such that the collector of  $Tr_1$  is at

zero volts when the output of the i.c. is at zero volts, assuming the loop is not closed by  $R_f$ . If the collector and emitter currents of  $Tr_1$  are assumed to be equal, then the current through the transistor is  $V_{cc}/R_1$ . Therefore the drop across  $R_2$  and  $Tr_1$  base-emitter is  $V_{be} + (V_{cc}R_2/R_1)$ . Hence the voltage to be dropped by the zener diode is  $V_{cc} - (V_{be} + V_{cc}R_2/R_1)$ .

These calculations need only be approximate because any errors are virtually eliminated when the loop is closed. Resistor  $R_3$  is required to provide sufficient current for the zener diode to operate correctly. Output impedance may be reduced further by the addition of an emitter follower but  $R_f$  must then be taken to its emitter (second circuit). Note that  $R_f$  is returned to the non-inverting input because of the additional inversion due to  $Tr_1$ . Component values given in the circuit increase the slewing rate by a factor of five. Gains of up to 20 have been used.

L. Short,  
Wokingham.

input 1, in both cases via a suitable resistor. If it is more convenient, the connections to the inputs of each op-amp could be reversed, in which case the feedback connections would be output 1 to input 1, and output 2 to input 2.



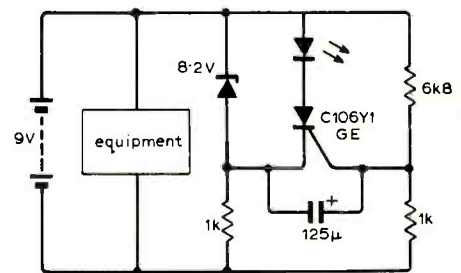
If  $IC_1$  and  $IC_2$  are combined in a dual op-amp, then p.c. board space will be saved, and differential temperature drift reduced. I used a 741 for  $IC_3$  and a 747 (dual 741) for i.c.s 1 and 2.

A. D. Monstall,  
Edinburgh.

## Low battery voltage indicator

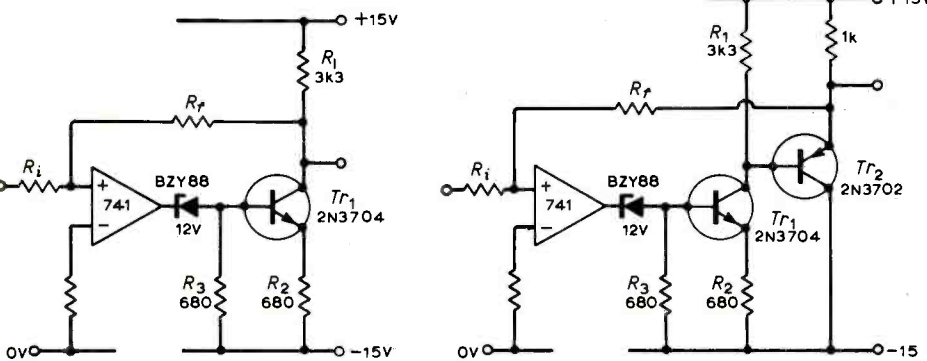
This circuit was devised to indicate when the voltage of the battery fell below a minimum acceptable value during a long period of use.

The design is for a 9-volt version, but can easily be adapted to suit any supply voltage. In this particular case the l.e.d. lights up when the supply voltage falls to 8.3V — this minimum voltage is determined by choice of circuit components. The l.e.d. used is a Hewlett-Packard 5082-4440 available from Integrex. The zener diode is a BZY85 C8V2 400mW, but in this circuit its avalanche point is only 7.7V due to the low current drawn. The circuit draws about 2.5mA normally, and 7mA when the thyristor conducts. The 125- $\mu$ F capacitor



is included to prevent pulses triggering the thyristor as capacitors charged.

P. C. J. Parsonage,  
Whangarei,  
New Zealand.



## Differential input and output with op-amps

This circuit uses three op-amps to provide an amplifier with differential output as well as differential input. It was designed to drive a meter with a signal of either polarity when a centre-tapped power supply was not available, but could have other uses.

The 18-k $\Omega$  resistors form a potential divider across the outputs of the complete amplifier. The voltage at the non-inverting

input of  $IC_3$  is therefore the average of the two output potentials. The divider consisting of the two 1-M $\Omega$  resistors maintains the inverting input of  $IC_3$  at a fixed potential;  $IC_3$  acts to keep its inputs nearly equal, as it forms part of a negative feedback loop, and therefore the average of the two output potentials, i.e. the common mode output, is determined by the resistor values.

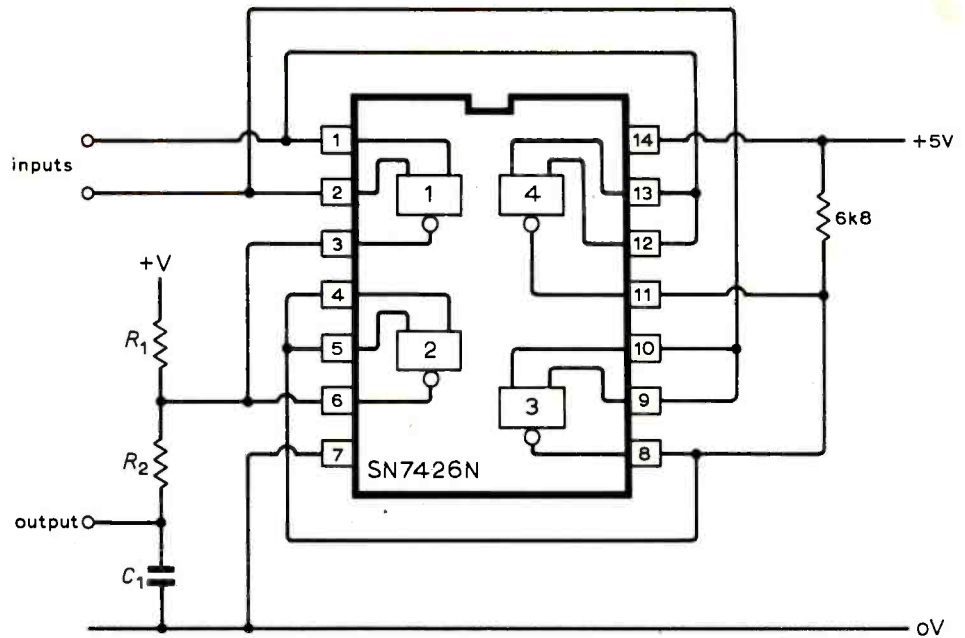
To obtain negative differential feedback with the circuit as shown, output 1 should be connected to input 2 and output 2 to

### Inexpensive p.s.d.

A digital phase-sensitive detector with an output swing of up to 15 volts can be constructed for as little as 40p, using one SN7426N quadruple two-input nand-gate i.c. and a few passive components. The relationship between phase difference and d.c. output level is absolutely linear, so the circuit may find application in the construction of low-cost phase-lock loops and in phase-shift keyed demodulation.

The required logic function for phase detection is that of exclusive-or, i.e. '0' output for similar input levels and '1' output for dissimilar inputs, achieved by connecting the SN7426N as shown. Gate 1 gives the 'nand' function, while gates 3 and 4 act as inverters with their outputs combined by sharing a common load resistor. This combined output is fed to gate 2, inverted, and combined with that of gate 1, again by sharing a common load resistor.

The waveform produced by the detector is a rectangular wave whose mark-space ratio is proportional to the phase difference between the input square waves. This rectangular wave is applied to a low-pass filter formed by  $R_2$  and  $C_1$ , whose values should be chosen to suit the operating frequency and required output resistance. As the SN7426N has high-voltage open-collector outputs, the voltage for the



common load resistor  $R_1$  may be chosen to give the required output swing, to a maximum of 15 volts. Note that the open-collector outputs are rated to sink a maximum current of 16mA.

This whole circuit function could, of course, be achieved by using one circuit

of a SN7486N quadruple two-input exclusive-or, but this would require the use of an external transistor to achieve an output swing of greater than 2.5 volts, as well as being more expensive.

R. A. Harrold,  
Leicester.

### Reducing distortion by 'error add-on'

The conventional virtual earth amplifier must by its nature have an error at its output,  $V_A$  (upper part of first circuit). The basis of this new circuit is to recognize that a measure of this error appears at the input of  $A_1$ , and when fed to  $A_2$  an error 'add-on' signal is produced. The output between  $V_A$  and  $V_B$  is then composed of the error in the output signal  $V_B$  added to the distorted original signal  $V_A$  to produce an output very much closer to the ratio  $R_2/R_1$  than in the conventional case. What error add-on does for amplifiers is to use the second load terminal, normally earthed, to do something useful.

Gain is  $(V_A + V_B)/V_{in} = G_1 + G_2G_1/A_1$ , where

$$G_1 = \frac{A_1 R_2}{R_2 + R_1(1 + A_1)}$$

and 
$$G_2 = \frac{A_2}{1 + A_2 R_3/(R_3 + R_4)}$$

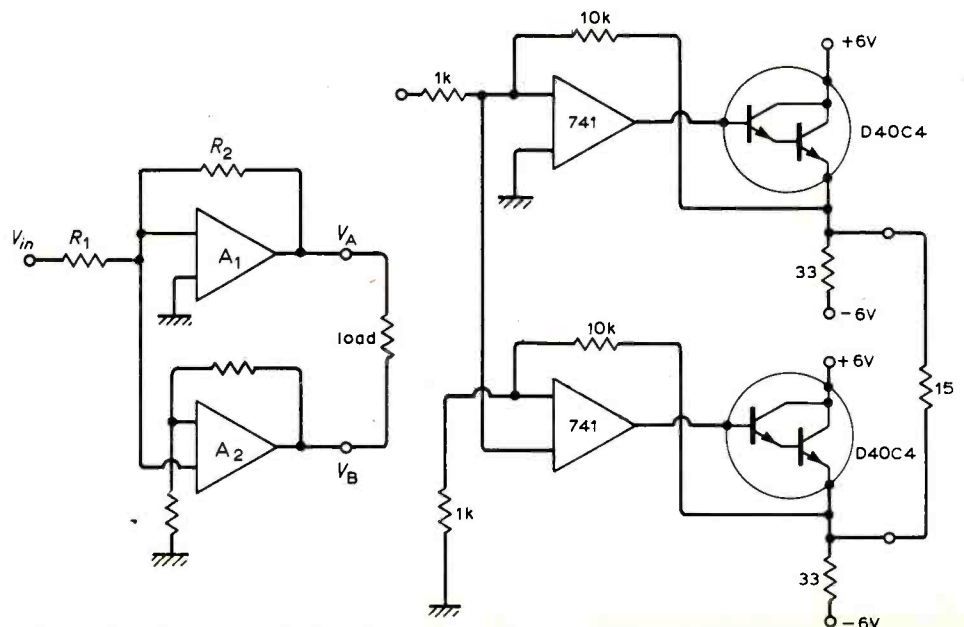
The circuit has been built and demonstrated using the values shown. When slightly overloaded the results show very clearly how the principle works. Resistor  $R_2$  was adjusted but in practice a 1% resistor could be used. It is hoped to publish more details later, but

intuitively I feel that the open-loop gain improves at 12dB/octave compared with 6dB for the conventional case. Of interest is the hope of solving problems such as loudspeaker distortion which negative feedback fails to cope with adequately. A microphone might be placed in front of the main loudspeaker to produce an error add-on signal

for a separate error add-on loudspeaker.

Indeed in principle a chain of microphones and speakers could be employed to reduce distortion to any amount although in practice this might be difficult to achieve.

A. Sandman,  
Lincoln's Inn Fields,  
London, WC2.





# Experiments with operational amplifiers

## 7. Using transistors for logarithmic conversion

by G. B. Clayton,\* B.Sc., F.Inst.P.

Bipolar transistors, operated under appropriate conditions, behave logarithmically. An operational amplifier transistor feedback circuit may be used to perform logarithmic conversion. Converters using this principle assume a transistor characteristic described by the equation

$$V_{EB} = -E_o \log_{10} \frac{I_c}{I_o} \quad (7.1)$$

where  $I_c$  is the collector current in amps,  $I_o$  is a constant at constant temperature, its value is typically  $10^{-12}$ A,  $E_o$  is a constant at constant temperature, its value approximately 60mV at 27°C, and  $V_{EB}$  is the emitter base voltage.

The equation holds for a wide range of collector current values provided that the collector base voltage of the transistor is held at zero.

Because of the temperature dependence of the terms  $I_o$  and  $E_o$  simple logarithmic converters using single transistors give accurate logarithmic conversion only if the temperature is held constant. The effect of temperature changes may be considerably reduced by balancing the temperature variation of one transistor against that of a second transistor; such temperature compensation requires the use of an extra operational amplifier. Experimental circuits for investigating the action of simple log converters and temperature compensated converters are suggested in what follows.

A circuit suitable for investigating the performance of a simple logarithmic converter is illustrated in Fig. 7.1. Negative feedback is applied to the operational amplifier through a diode connected transistor  $T_{R1}$ . The circuit is suitable for positive input voltages. Diode  $D$  is connected in parallel with the logging transistor to protect the transistor against the excessive inverse voltage which would arise if an input signal of wrong polarity were inadvertently applied. Negative input signals may be logged by reversing connections on both transistor and diode. Resistor  $R_E$  is connected in series with the logging transistor to reduce the effective loading on the amplifier output at the higher values of feedback current.

If we assume that the base current of the transistor is negligibly small compared with the collector current, the feedback current

may be equated to the collector current. The output voltage of the amplifier provides the transistor emitter base voltage and we may write:

$$e_o = V_{EB} = -E_o \log_{10} \frac{I_c}{I_o} \quad (7.2)$$

where  $I_c = I_f = \frac{e_i}{R}$ .

Note that the output voltage from the circuit is taken from the emitter of the logging transistor and not from the output terminal of the amplifier, pin 6.

The response equation for the circuit may be verified by applying a range of input voltages and measuring and recording input and output signals. If the widest logging range possible with the circuit is to be realized it is necessary to separately balance both the input voltage offset and the bias current of the amplifier. In making these adjustments the transistor with its protective diode are disconnected from the circuit and a large value resistor (say 1MΩ) is connected in their place.

Input offset voltage is balanced first. This is done by shorting pin 2 to earth and adjusting the offset voltage balance potentiometer

for zero amplifier output. Once input offset voltage has been balanced the short on pin 2 is removed. The input voltage to the circuit is set to zero and the bias current potentiometer is adjusted so that the amplifier output is again zero. The logging transistor with its protective diode should now be connected back into the circuit.

In investigating the logging range of the circuit input voltages in the range, say, 0.1mV to 10V will be found suitable. A typical set of experimental results is given in the table below.

Output voltage $e_o$	Input voltage $e_i$	Log <sub>10</sub> $e_i$
0.32V	$10^{-4}$ V	-4
0.35V	$8.8 \times 10^{-4}$ V	$4.95 = -3.05$
0.4V	$4.7 \times 10^{-3}$ V	$3.66 = -2.34$
0.45V	$3 \times 10^{-2}$ V	$2.48 = -1.52$
0.5V	0.21V	$1.32 = -0.68$
0.55V	1.6V	0.20
0.6V	10V	1

Results may be plotted graphically as in Fig. 7.2 in order to show the logging range. The graph should be used to deduce values for the constants  $E_o$  and  $I_o$  of eq. (7.2).

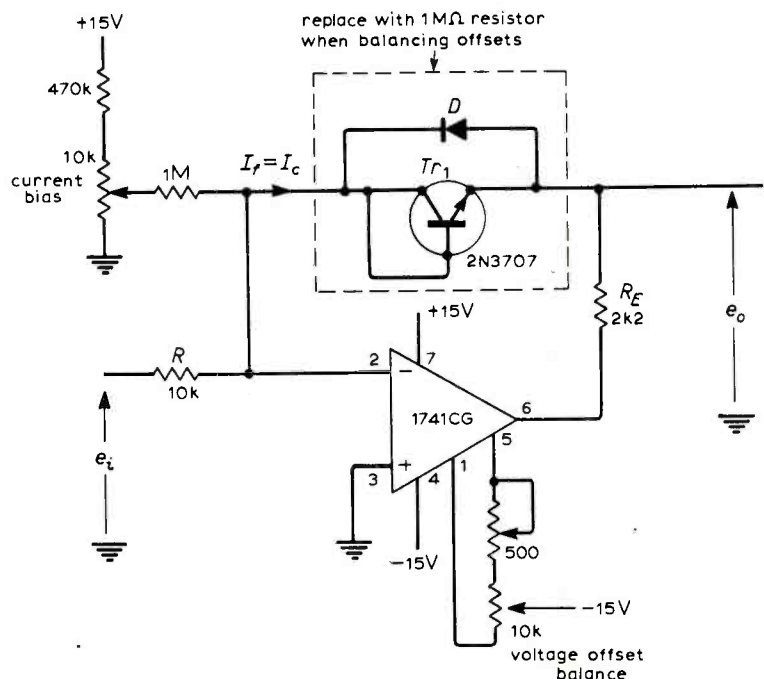


Fig. 7.1. A simple logarithmic converter.

\*Department of Physics, Liverpool Polytechnic.

Interchanging the position of the input resistor and logging element in the circuit of Fig. 7.1 gives the circuit shown in Fig. 7.3. This circuit may be used to perform an anti-log conversion. The circuit accepts positive input signals. Diode connection of the transistor allows the same transistor to be used for either positive or negative input signals, by connecting the transistor into the circuit in the appropriate direction.

It is not necessary to separately balance input offset voltage and bias current; an adjustment of the 10kΩ balance potentiometer for zero output with zero input is sufficient.

Input voltages in the range say 200mV to 600mV should be applied and values of input voltage and output voltage should be recorded. A graph of the input voltage against the log of the output voltage should be drawn.

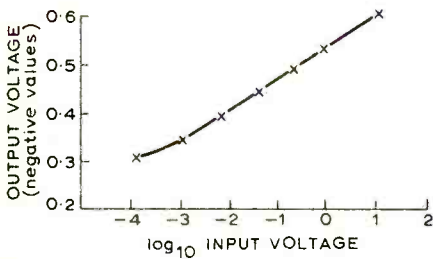


Fig. 7.2. Plot of experimental results from Fig. 7.1 converter.

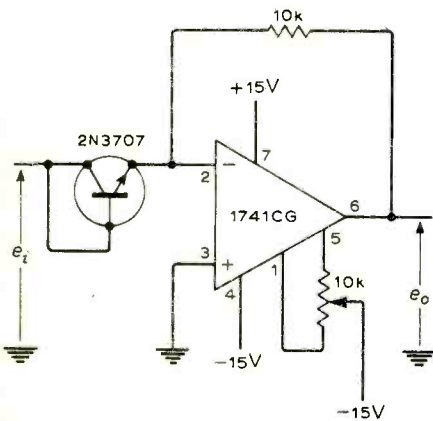


Fig. 7.3. A simple antilog converter.

A circuit for a temperature compensated log converter is given in Fig. 7.4. The circuit uses two operational amplifiers and two logging transistors. The output voltage of amplifier  $A_1$ , attenuated by the resistive divider  $R_3, R_4$  provides the emitter base differential voltage between transistors  $Tr_1$  and  $Tr_2$  and

$$e_o \frac{R_3}{R_3 + R_4} = V_{EB} - V_{EB2} \quad (7.3)$$

$V_{EB2}$  is controlled by the negative feedback round amplifier  $A_2$ . The feedback forces it to take on that value which will cause the collector current  $I_{c2} = I_2$  to flow in transistor  $Tr_2$ . Negative feedback round amplifier  $A_1$  forces  $V_{EB1}$  to take on that value which will cause the collector current  $I_{c1} = I_1$  to flow in transistor  $Tr_1$ .

Substituting  $V_{EB}$  values from eq. (7.1) into eq. (7.3) and rearranging gives

$$e_o = -\frac{R_3 + R_4}{R_3} E_o \log_{10} \frac{I_{c1} I_{o2}}{I_{c2} I_{o1}} \quad (7.4)$$

where

$$I_{c1} = I_1 = \frac{e_1}{R_1} \text{ and } I_{c2} = I_2 = \frac{e_2}{R_2}$$

The output is compensated against the marked temperature dependence of the transistor  $I_o$  terms, since for matched transistors the  $I_o$  terms cancel. Even if the transistors are not perfectly matched it is found that for transistors of the same type the ratio  $I_{o2}/I_{o1}$  remains fairly constant with change in temperature. The linear temperature dependence of the term  $E_o$ , which, together with resistors  $R_3$  and  $R_4$  determines the scaling factor, may be compensated by using a temperature sensitive resistor for  $R_3$ .

If the greatest possible logging range is required the input offset voltage and bias current of amplifier  $A_1$  should be balanced, using the procedure outlined for the simple log converter of Fig. 7.1.

The input signal to be logged is applied at  $e_1$  and a fixed collector current  $I_{c2}$  set by  $e_2$  and  $R_2$  is passed through transistor  $Tr_2$ .

In a practical temperature compensated log converter it is usual to return the  $e_2$  input to the positive supply and to choose the value of  $R_2$  so as to give a required value of  $I_{c2}$ . The value used for  $I_{c2}$  determines the

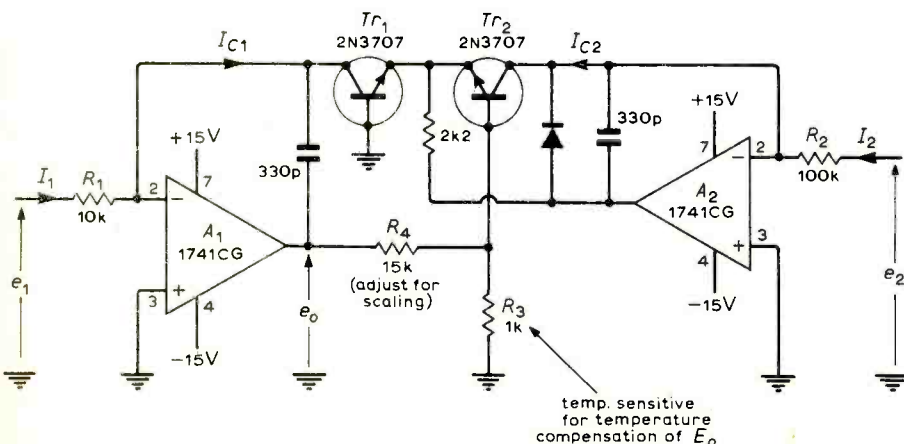


Fig. 7.4. Temperature compensated logarithmic converter.

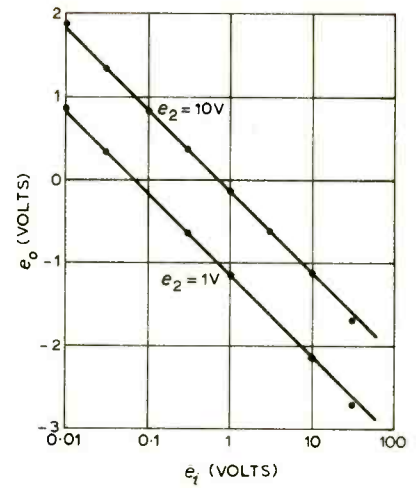


Fig. 7.5. Plot of experimental results from Fig. 7.4. circuit.

value of  $I_{c1}$  and hence  $e_1$  required for zero crossing of the output of amplifier  $A_1$ .

If very small input signals are not to be used and one merely wants to take measurements in order to explore the action of the circuit it is not necessary to balance amplifier  $A_1$  offsets. The output voltage should be measured for a range of values of  $e_1$ . This should be done for several fixed values of the reference current  $I_{c2}$ . Results are conveniently displayed by plotting the output voltage against the log of the input voltage (or input current). The slope of these graphs is equal to  $\frac{R_3 + R_4}{R_3} E_o$ . Values of  $R_3$  and  $R_4$  are normally chosen to give an output voltage change of 1V per decade of input current change.

Experimental results obtained with the circuit of Fig. 7.4 are shown graphically in Fig. 7.5. The results were obtained with two settings of  $e_2$ , 1 volt and 10 volts, corresponding to  $I_{c2} = 10^{-5}A$  and  $10^{-4}A$  respectively. Note that zero crossing of the output occurs in each case when  $I_{c1}$  is slightly less than  $I_{c2}$ . This is because of a mismatch in transistor  $I_o$  terms. The results indicate a value  $I_{o1}/I_{o2} \approx 0.8$  for the two transistors used. In both sets of results accuracy of log conversion falls off for values of the input voltage less than 10mV. The range of the circuit can be extended by balancing the offsets of amplifier  $A_1$ .

The effect of fixing the current  $I_1 = I_c$  at some reference value and applying a varying input signal to the  $e_2$  terminal should be tried. This gives log conversion without sign inversion, but the  $e_2$  input is not suitable for very small signals. Transistor  $Tr_2$  does not give accurate logarithmic conversion for very small currents because its collector base voltage is not zero.

Note that all op-amp transistor feedback log converters will accept only single-polarity input signals. The circuit of Fig. 7.4 is suitable for positive input signals. If one wishes to perform a logarithmic operation on a negative input signal the n-p-n transistors  $Tr_1$  and  $Tr_2$  should be replaced by a suitable p-n-p type (say 2N 4058).

The circuitry in Fig. 7.4 may be rearranged to give a circuit which will per-



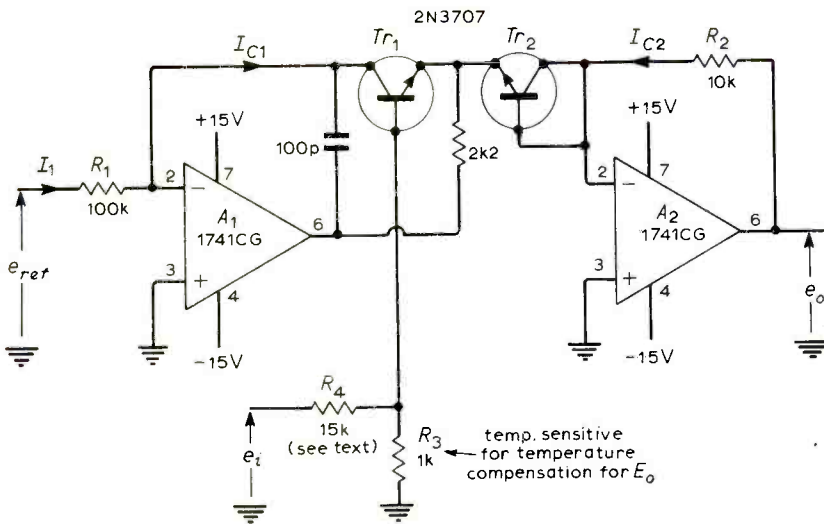


Fig. 7.6. Temperature compensated antilog converter.

form an antilog conversion, as illustrated in Fig. 7.6.

The input signal to the circuit, attenuated by the resistive divider,  $R_3, R_4$ , provides the emitter base differential voltage between transistors  $Tr_1$  and  $Tr_2$  and

$$e_i \frac{R_3}{R_3 + R_4} = V_{EB2} - V_{EB1} \quad (7.5)$$

Negative feedback round amplifier  $A_1$  forces  $V_{EB1}$  to take on that value which will cause the current  $I_1 = I_{c1}$  to flow as a collector current in transistor  $Tr_1$ . If  $I_1$  is held constant as a reference current  $V_{EB1}$  is constant and  $V_{EB2}$  varies directly with  $e_i$ . Voltage  $V_{EB2}$  determines the collector current,  $I_{c2}$ , of transistor  $Tr_2$ . Negative feedback round amplifier  $A_2$  forces  $I_{c2}$  to flow through resistor  $R_2$  and amplifier  $A_2$  gives an output voltage  $e_o = I_{c2}R_2$ .

Substitution of  $V_{EB}$  values from eq. (7.1) into eq. (7.5) gives

$$e_i \frac{R_3}{R_3 + R_4} = E_o \log_{10} \frac{I_{c1} I_{o2}}{I_{c2} I_{o1}}$$

Where  $I_{c1} = I_1 e_{ref}/R_1$  and  $I_{c2} = e_o/R_2$

$$\text{Thus } I_{c1} \frac{I_{o2} R_2}{I_{o1} e_o} = 10^{e_i \frac{R_3}{R_3 + R_4} \frac{1}{E_o}}$$

Values of  $R_3$  and  $R_4$  are normally chosen so that

$$\frac{R_3}{R_3 + R_4} \frac{1}{E_o} = 1.$$

$R_3$  may be made temperature dependent in order to compensate for the temperature dependence of  $E_o$ . With these values of  $R_3$  and  $R_4$

$$e_o = I_{c1} \frac{I_{o2}}{I_{o1}} R_2 10^{-e_i}$$

If  $I_{o1} = I_{o2}$  the multiplying factor

$$I_{c1} \frac{I_{o2}}{I_{o1}} R_2$$

may be made equal to a desired constant  $c$  by choosing  $e_{ref}, R_1$  and  $R_2$  so that  $e_{ref}(R_2/R_1) = c$ . This makes  $e_o = c 10^{-e_i}$ .

The value of the constant  $c$  must, of course, not be made greater than the output

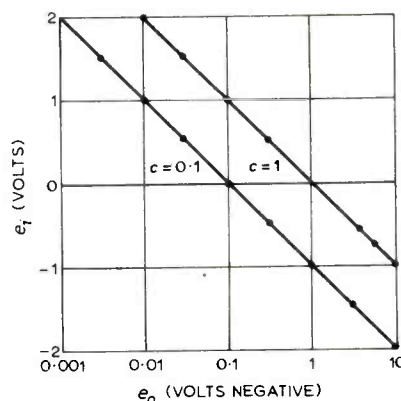


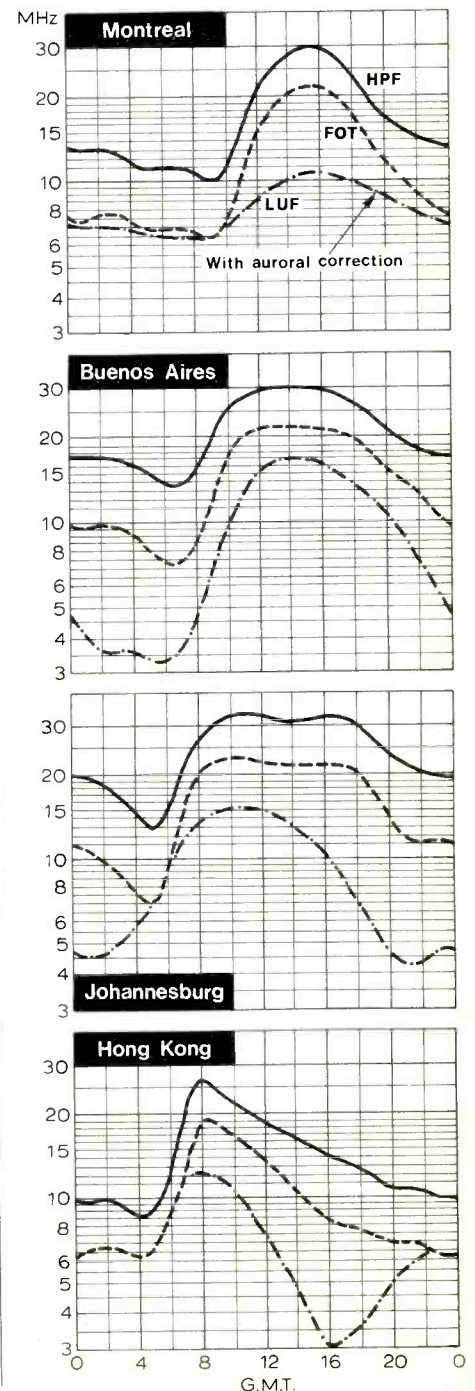
Fig. 7.7. Plot of experimental results from Fig. 7.6 circuit.

voltage capability of the amplifier. To allow for transistor mismatch and to avoid the use of close tolerance resistors the following experimental setting-up procedure may be adopted. Set  $e_i$  to zero and adjust  $e_{ref}$  or  $R_1$  to make the output of amplifier  $A_2$  exactly  $c$  volts. Apply an input signal of minus one volt and trim the value of resistor  $R_4$  to make the output of amplifier  $A_2$  exactly  $10c$  volts. Experimental results obtained with the circuit are shown graphically in Fig. 7.7. The two sets of results are for  $c = 1$  and  $c = 0.1$ . No offset balance was employed. Balancing amplifier  $A_2$  offsets may be expected to extend the range of the circuit. (To be continued)

Op-amp log and antilog converters may be combined in order to generate many non-linear functions. The circuits are connected together in such a way that they perform the operations normally involved in logarithmic computation. The remainder of Experiment 7 will deal with log circuits for multiplication, division and the generation of powers.

## H.F. Predictions — January

HPF (highest probable frequency) is the frequency above which the probability of a skywave path existing is less than 10% and FOT (from the French, optimum traffic frequency) is the frequency below which the probability is greater than 90%. LUF (lowest usable frequency) is the frequency above which the probability of exceeding the desired signal-to-noise ratio is greater than 90%. FOT is an old established term but something of a misnomer as the true optimum, at which the product of skywave and signal probabilities is a maximum, is found to be the geometric mean of FOT and LUF. As the charts, which are prepared by Cable & Wireless, have a logarithmic frequency scale this optimum is easily placed by eye at midway between the FOT and LUF curves.



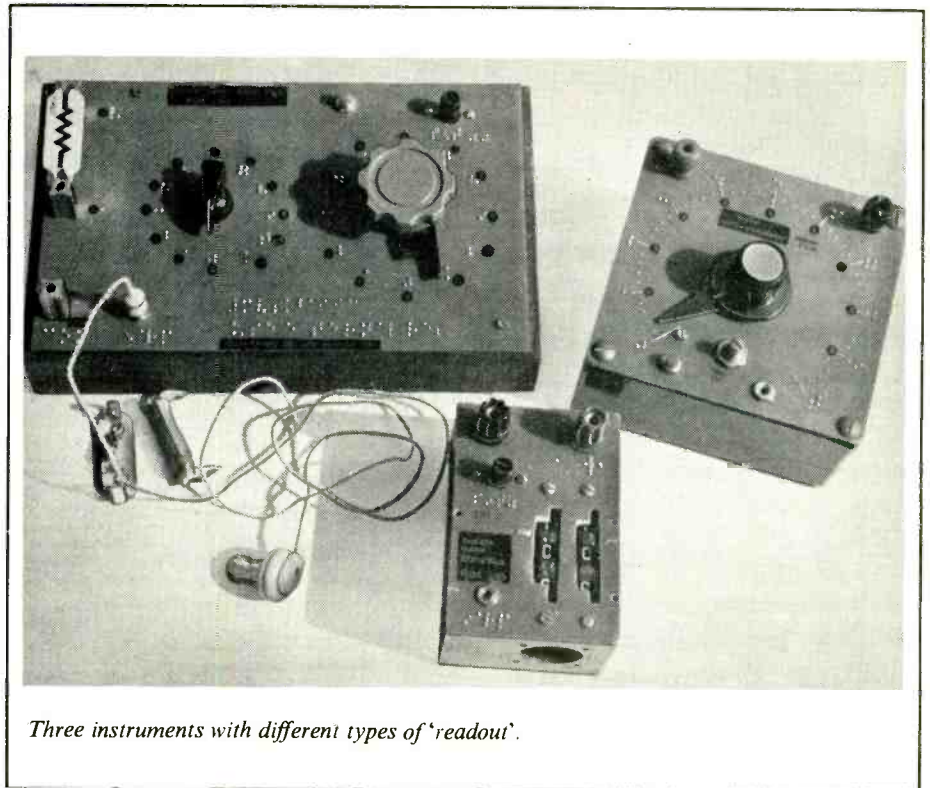
# Meter for Blind Students

## Aural-tactual indication for d.c. measurements

by R. S. Maddever\*, M.A., D.Phil.

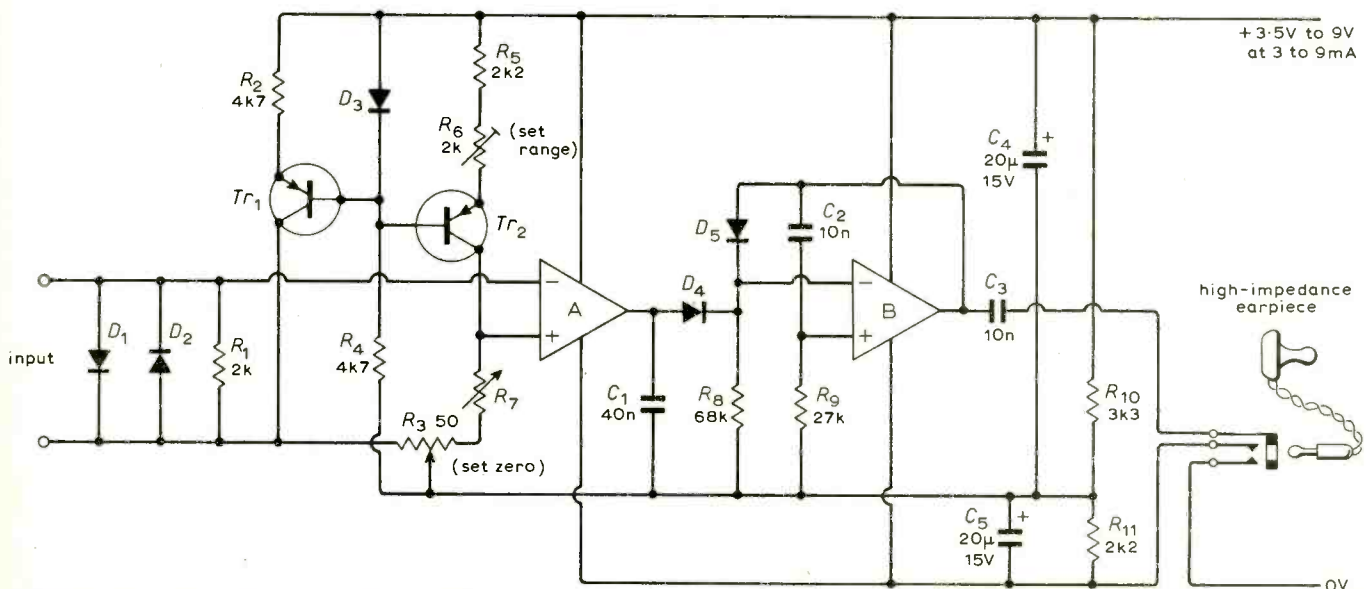
This instrument for blind students is designed to convert an electrical input into an audible indication, as a direct replacement for a moving-coil meter. With a designed range of 0 to 100mV and an input resistance of 2k $\Omega$ , a 10°C change in temperature or a 30% change in battery voltage produces an output change of less than 3%. Tactual 'readout' can be by pointer on a circular scale or by decade switches. With the last-mentioned the reading precision is 1% of full scale.

A variable reference voltage is produced by changing the resistance  $R_7$  in series with the constant current generator  $Tr_2$ . An operational amplifier,  $A$ , compares this reference voltage with the voltage to be measured across  $R_1$ . If the reference voltage is greater than the input voltage the amplifier output is positive and thus allows a second operational amplifier,  $B$ , connected as a free running multivibrator, to function and produce sound in an earpiece. If the reference voltage is lower than the input voltage, amplifier  $A$  output is negative and the multivibrator inoperative. By merely reversing the input leads to the first op-amp the audio output can be obtained when the



Three instruments with different types of 'readout'.

\*Geelong Grammar School, Corio, Australia.



Circuit of the aural-tactual meter. Transistors are germanium types, e.g. OC45, OC71; op-amps Motorola 1435; diodes silicon types, e.g. BA100, OA200, IN914.



reference is below the input, if this is preferred.

Thus, in use,  $R_7$  is adjusted, either by potentiometer or by switches, until oscillations are about to begin, and the input voltage is then known to be practically the same as that read off the variable reference voltage scale. The input terminals will be similar to those of a 50 microamp, 100mV moving-coil meter, so that conventional shunts and series resistors may be switched in to form an 'audible multimeter'.

The Motorola 1435 dual op-amp requires a centre-tapped voltage supply. To achieve this and still allow the supply to be switched on by the insertion of the earpiece, resistors  $R_{10}$  and  $R_{11}$  are used, with decoupling capacitors  $C_4$  and  $C_5$ . The value of  $R_{11}$  is smaller than  $R_{10}$  because the current from the positive supply is greater than that from the negative supply due to the constant current generator. Silicon diodes  $D_4$  and  $D_5$  isolate the functions of the two op-amps. The multivibrator frequency may be altered by changing  $C_2$  or  $R_9$ .

The base of  $Tr_2$ , a germanium transistor, is held at about 700mV below the positive supply line by the silicon diode  $D_3$ . Since the emitter-base voltage is about 300mV, the current through it stabilizes so that a further 400mV is dropped across the emitter load,  $R_5$  and  $R_6$ . Thus by varying  $R_6$  the collector current is adjusted to produce the required maximum reference voltage across  $R_7$  at its full scale value. Temperature compensation is afforded by the fact that the temperature coefficients of the voltage across the diode and  $V_{BE}$  for  $Tr_2$  are similar and thus tend to cancel each other out.  $R_4$  is chosen so that even at the lowest supply voltage the bias current through  $D_3$  is several times the currents in the bases of  $Tr_1$  and  $Tr_2$ . To allow zero setting with no input,  $Tr_1$ ,  $R_2$  and  $R_3$  are added. Silicon diodes  $D_1$  and  $D_2$  are for input protection.

$R_7$  can be either a wire-wound potentiometer or a series of switched resistors. In each case the maximum resistance is made 1k $\Omega$ , and hence  $R_6$  is adjusted to produce a current of 100  $\mu$ A in the collector of  $Tr_2$ .

Instruments using both methods of varying  $R_7$  are shown in the photograph. Front panels are made from copper clad board. Braille figures and letters were put in with resist paint or dots from pressure sensitive sheets such as Letraset. Ordinary lettering was also put in to aid sighted instructors. After etching, the Braille dots were further raised with solder. Before removing the pressure sensitive ordinary letters to expose the copper, the areas around the letters were painted black with a cellulose lacquer. This provides excellent contrast for the copper lettering. The largest instrument uses Locktronic posts and resistors (A. M. Lock & Co. Ltd.) so that blind students may easily insert shunts and series resistors.

The author is grateful to Churchill College, Cambridge, for the award of a Schoolmaster Fellow Commonership during the holding of which these instruments were developed, and to Mr. S. Stephenson, of Worcester College for the Blind, who brought the need of such instruments to his attention and arranged for several to be tested.

## “B.B.C. Engineering — 1922-1972”

We consider that this monumental work\* by Edward Pawley demands more than our normal notice under “Books Received”. This 570-page volume, which incidentally weighs some 3½ lb, contains well over 300,000 words and so much information that it would be invidious to highlight any one section.

As the history of broadcasting in the U.K. falls fairly naturally into the following six periods the book has been divided into these six chapters:

1. The experimental era preceding the formation of the British Broadcasting Company in 1922.
2. The lifetime of the British Broadcasting Company: 1922-6.
3. The formative period of the British Broadcasting Corporation, from its foundation in 1927 until the outbreak of war.
4. The war years: 1939-45.
5. The period of post-war reconstruction: 1946-55.
6. The years of expansion, from 1956 onwards.

Although, inevitably, names (many of which became household words) are prominent in the story, Mr Pawley has dealt with the developments of broadcast engineering rather than the personalities concerned.

A complete picture (“warts and all”) of British broadcasting from the earliest experiments before the setting up of the original British Broadcasting Company to the latest colour television techniques is painted. The work is extremely well documented with something like 550 references.

One aspect of broadcasting in the U.K. which may not be generally known becomes obvious on reading the book. It is that the B.B.C. has played a major part in the international field of broadcasting. Another little known contribution is the part played by B.B.C. engineers in the 1939-45 war effort. In the section covering the war years one learns

what technical juggling was concealed by such code names as “washtub”, “dartboard”, and “domino”. The first of these names was given to the medium-wave transmissions to guide home-ward bound bombers after raids. Dartboard created a strong jamming signal used on the medium-wave band to confuse enemy night fighters who were being given information in a Forces programme broadcast from Stuttgart. The Alexandra Palace television transmitter was used, under the code name domino, to disable the navigational system developed by the Luftwaffe and known as Y-Gerat.

An interesting aspect of broadcast engineering is emphasized by the author in his foreword. He points out that many of the techniques used in broadcasting are common to other branches of electronics and other forms of radio communication but “broadcasting differs from them in one way that has had a profound effect upon its development: the receiving part of a broadcasting system — a vitally important part — is not under the control of the broadcasters”. One result of this peculiarity is that the problem of obsolescence imposes a severe restraint on development as no improvement can be made at the transmitter unless either it is planned and announced so far ahead that existing receivers are worn out before the change takes place or that it is made in such a way that there is no deterioration in reception using existing receivers.

The many and varied achievements of the B.B.C. engineers are well documented in this volume and is in itself a tribute to their work over the past 50 years.

\* “BBC engineering” 1922-1972, by Edward Pawley, BBC Publications, 35 Marylebone High St., London, W1M 4AA. Price £7

## Announcements

Racal-Mobilcal Ltd, Reading, Berkshire, have announced a contract for military radio equipment valued at £1.8M. The equipment includes the “Synical”, “Squadcal” and “Comcal” h.f. mobile radiotelephones.

A customer service laboratory for thick-film materials has been opened by the Du Pont Company (U.K.) Ltd, at Hemel Hempstead, Herts. The service is intended for European customers and possesses equipment for the manufacture and testing of thick-film components.

The consortium of AEG-Telefunken, Aeritalia and the British Aircraft Corporation has been awarded the contract for design, development and manufacture of the Radome (radar transparent nose cone) requirement for the Panavia multi-role combat aircraft.

Jermyn Distribution, Vestry Estate, Sevenoaks, Kent, have been awarded a franchise to handle the range of Siferit pot cores manufactured by Siemens.

EMI Electronics and Industrial Operations, Blyth Road, Hayes, Middlesex, has introduced a computerized spectral calibration service for users of its photomultiplier tubes.

A vacation school intended to familiarize engineers and scientists in industry and education with modern methods and philosophies in the measurement of physical quantities will be held at the

University College of North Wales, Bangor, from 8th to 13th April 1973. The school on Electronic instrumentation will be organized by the Electronics Division of the Institution of Electrical Engineers, Savoy Place, London, WC1.

New Zealand Broadcasting Corporation has ordered two complete mobile sets of outside broadcast colour TV equipment, including Mark VIII automatic colour cameras, from Marconi Communication Systems Ltd, Marconi House, Chelmsford CM1 1PL.

Ultra Electronics (Components) Ltd, Fassetts Road, Loudwater, Bucks, have signed an agreement to represent Ouest Electronic Connecteurs, of France, in the distribution of connectors and related components.

A contract to provide a new telecommunications link with France is included in a transmission equipment order placed by the British Post Office with GEC Telecommunications Ltd, P.O. Box No. 53, Coventry CV3 1HJ.

Two short courses entitled “Video recording” and “Time sharing computer systems” are to be held at Norwood Technical College, Knight’s Hill, London, SE27 OTX. Video recording is a seven-week course from 18.30 to 20.30 each Monday commencing 12th February; fee £3.00. Time sharing is a six-week course from 18.30 to 20.30 each Tuesday commencing 13th February; fee £2.25.

# Books Received

**Semiconductor Diode Lasers**, by Ralph W. Campbell and Forrest M. Mims, is written for experimenters and engineers as a broad introduction to the semiconductor laser and its applications. It simplifies the theory of laser action and deals briefly with the historic development of lasing materials and methods of excitation and discusses the relationship between non-coherent light emissions, as from LEDs, and coherent light emissions which characterize the semiconductor injection laser diode. The book continues with an informative section showing commercial device manufacturing techniques, covering the geometry of single diode construction and high-power, multi-element arrays. The remaining chapters are devoted to the practical applications and circuitry used with these devices, demonstrating the simplicity of pulse generators, modulators, power supplies, detectors and receiving systems. Pp.192. Price £1.90. W. Foulsham & Co. Ltd, Yeovil Road, Slough, Bucks.

**Compatibility and Testing of Electronic Components**, written by C. E. Jowett, is designed to meet the needs of engineers and technologists working in the fields of component reliability, quality control, production and test development. It covers this vast subject in a clear, concise manner, providing detailed information on manufacturing and testing methods and generating an understanding of compatibility between materials, processes and differing environmental conditions. The subject matter deals with practically all aspects of integrated circuits, thick- and thin-film devices, capacitor and deposited resistor technology, hybrid microelectronics, miniature encapsulated relays and flexible film wiring. The remaining chapters are concerned with techniques involved in reliability screening, environmental and life testing, component stress testing and detection of incompatibilities. Pp.345. Price £6.00. Butterworth & Co. Ltd, 88 Kingsway, London WC2B 6AB.

**Field Effect Transistors** has been edited by N. R. Bijlsma and P. Burwell of Elcoma Publications in conjunction with E. G. Evans of Mullard's Central Technical Service. It is designed to familiarize the potential user of f.e.t.s with the operating principles, characteristics and terminology of these devices in such a way that the special properties offered, can be recognized and utilized to advantage. This is achieved by discussion of the relative structures and principles involved in both junction and insulated-gate, field-effect transistors. Development is from triode technology, enhancement and depletion modes of

operation, to tetrode or dual-gate forms of construction. Electrical properties are dealt with and the closing chapter describes circuit configurations and typical applications. Pp.131. Price £1.80. Mullard Ltd, Mullard House, Torrington Place, London WC1E 7HD.

**Dielectrics**, by P. J. Harrop, is the title of a work on a topic which has been neglected to a certain extent even though great advances have been made on the subject of material science. The author has attempted to bring up to date the subject of dielectric materials used in electrical/electronic engineering, using a minimum of the large amount of tedious mathematical analysis normally associated with material physics. The book develops from a section of background information, which summarizes the classic capacitive properties of dielectrics, into the nature of matter which effect classification of the numerous types of material media. The text continues with an extensive survey dealing with the modern forms of dielectric and discusses the relative merits of forms and techniques employed in the fabrication of components. Finally, testing and measurement techniques are reviewed dealing with the basic parameter evaluation of both solid and liquid dielectrics. Pp.155. Price £3.50. Butterworth & Co. Ltd, 88 Kingsway, London WC2B 6AB.

**Techniques of Circuit Analysis**, by G. W. Carter and A. Richardson, is written primarily for undergraduate students of electrical and electronic engineering, though it will also be found useful to physicists. It provides instruction and practice in the methods of analysis which are essential in solving electrical circuit problems. A notable inclusion is the analysis of distributed circuits and transmission lines under transient as well as steady state conditions. Laplace transforms, matrix algebra, Fourier integrals and the complex plane are explained with worked examples used to illustrate the methods described. Each chapter concludes with a set of exercises. Pp.548. Price £5.00. Cambridge University Press, Bentley House, 200 Euston Road, London NW1 2DB.

**Thick Film Circuits**, by G. V. Planer and L. S. Phillips, aims to assemble the basic ideas and data required to enable the reader to understand and assess the capabilities of thick film technology in relation to his own particular requirements. It is also designed as a reference book for those already involved in this area, or who have a more general interest in electronic packaging developments. A selection of the chapter headings are: applications, substrates, conductor and resistor patterns, printed capacitor and insulating layers, printing and

firing procedures, hybrid circuits, trimming and test procedures, environmental protection, and circuit design concepts. Pp.152. Price £4.00. Butterworth & Co. Ltd, 88 Kingsway, London WC2B 6AB.

**Transistor Audio and Radio Circuits**, for radio receivers, record players, tape recorders and hi-fi equipment, is the second edition of a publication by Mullard. This edition incorporates many new circuits that take advantage of developments which have occurred since the first edition was published. These include new audio amplifiers, a radio receiver and amplifiers using integrated circuits. In addition to the designs for 10W and 25W audio amplifiers, there are now three new circuits for 15W, 35W and 50W amplifiers. A pre-amplifier for these new circuits is also included. Methods of protecting these amplifiers from short circuits are discussed and suitable circuits given. Another addition to the book is a chapter on loudspeakers. This considers the choice of speaker for a particular application and the characteristics of the speaker required. Enclosures for speakers and some general rules for construction are discussed. Pp.281. Price £1.80. Mullard Ltd, Mullard House, Torrington Place, London WC1E 7HD.

**Broadcasting in Britain 1922-1972**, by Keith Geddes, is an illustrated, brief account of the engineering aspects of broadcasting from the formation of the British Broadcasting Company to the present era of television broadcasting and digital and stereophony techniques. Pp.63. Price 45p. Her Majesty's Stationery Office (Science Museum Publications), 49 High Holborn, London WC1V 6HB.

**Hi-Fi Year Book 1973** is a complete directory for pickups, motor units, tuners, amplifiers, microphones, recorders, speakers and cabinets. Brief specifications and prices of each product are provided. A section giving manufacturers' and dealers' addresses is also included and introductory articles cover the subjects of specifications, cassettes, loudspeakers and four-channel stereo techniques. Pp.464. Price £1.50. IPC Electrical-Electronic Year Books Ltd, Dorset House, Stamford Street, London SE1 9LU.

**BBC Engineering** is published approximately four times a year and is a record of B.B.C. technical experience and developments in radio and television broadcasting. The October 1972 edition, number 92, is centred around a history of B.B.C. engineering 1922-1972 and an article covering the first five years. A further principal article is entitled "Acoustic Modelling of Studios and Concert Halls". Pp.36. Price 40p (post free). Annual subscription £1.50. B.B.C. Publications, 35 Marylebone High Street, London W1M 4AA.

**Transistor Circuit Design**, by Laurence G. Cowles, is a reference manual of practical transistor circuits with design procedures and formulae covering d.c. to microwaves, small signals to high-power circuits related to discrete components and integrated circuits. Pp.344. Price £6. Prentice-Hall International Publisher, Durrants Hill Road, Hemel Hempstead, Herts.

**Beginner's Guide to Television** (5th edition), by Gordon J. King, deals with basic principles, TV transmission and reception, test cards and receiver controls, relay TV and communal aerials, colour and closed-circuit TV and video-tape recording. Pp.211. Price £1.60. Butterworth & Co. Ltd, 88 Kingsway, London WC2B 6AB.



# A Simple Transistor D.C. Multimeter

by J. D. Pahomoff\*

## A meter for high impedance measurements in transistor circuits

This short, but interesting article was received from one of our Russian readers and was inspired by the Linsley-Hood design we published in June 1972. A certain small amount of editing was undertaken but every effort has been made to preserve the original character of the author's manuscript which we feel adds to the interest of the article.

In spite of its principal simplicity, the final circuit diagram of the multimeter as suggested by Mr. Linsley Hood is too complicated especially for the beginner, because of many switches. I think that the simpler variant of this multimeter, described later, will find popularity among the readers of the magazine. Such a multimeter can be wired up during one week-end. To make the construction of the multimeter more simple all the switches are omitted and substituted for small sockets ( $\frac{1}{8}$  in. diameter or less).

### Circuit

The suggested revised circuit of the d.c. transistor multimeter is shown in Fig. 1. First of all the voltage multiplier is changed so that all the voltage ranges have single individual separate resistors from  $R_1$  to  $R_6$  inclusive. It's more convenient both for wiring and calibration.

The current multiplier is also slightly changed, the first and the last ranges being omitted. All the ranges for measurements of voltage and current are the same: 100-30-10-3-1-0.3-0.1. Only two ranges for measurements of resistance are left unchanged, as it is quite enough for most of the practical purposes. Each ohms range has its individual potentiometer ( $R_{16}$ ,  $R_{18}$ ). The variable resistor  $R_{21}$  in the tail load of  $Tr_1$  and  $Tr_2$  serves as a 'set zero' adjustment. The variable resistor  $R_{23}$  serves to set full scale deflection.

In order to switch off the multimeter there is a switch  $S_1$ . In the position 'OFF' transistor bases of  $Tr_1$  and  $Tr_2$  acquire the zero potential, that's why the current could not flow.

### Construction

Construction of the d.c. multimeter is not critical and it can be made in every way possible. It is suggested that the instrument case may be made of Paxolin. The construction of the voltage multiplier is shown in Fig. 2 and current multiplier in Fig. 3. Part of the current multiplier, for example  $R_{11}-R_{14}$ , may be wire wound. Each of these wire resistors must be correctly checked with Wheatstone bridge. Resistors from  $R_{10}$  to  $R_7$  can be selected among the preferred value series. For example, in the case of the  $67\Omega$  resistor  $R_{10}$ , in the current chain

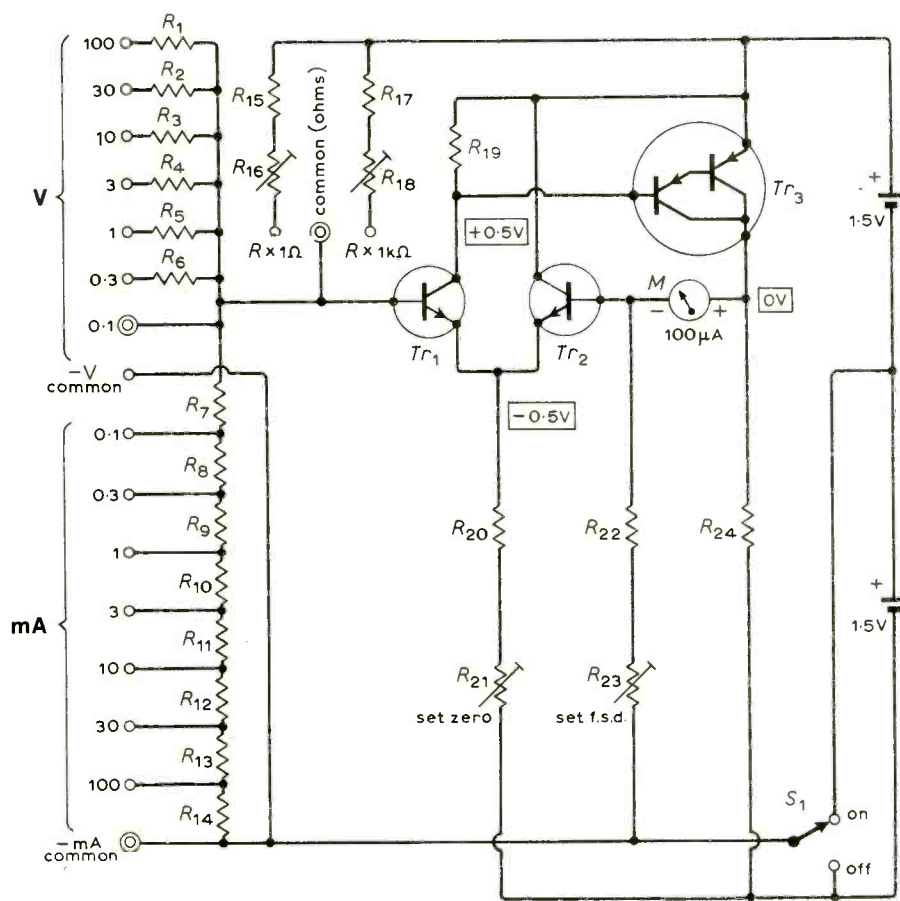


Fig. 1. Complete circuit diagram of the simple transistor d.c. multimeter.

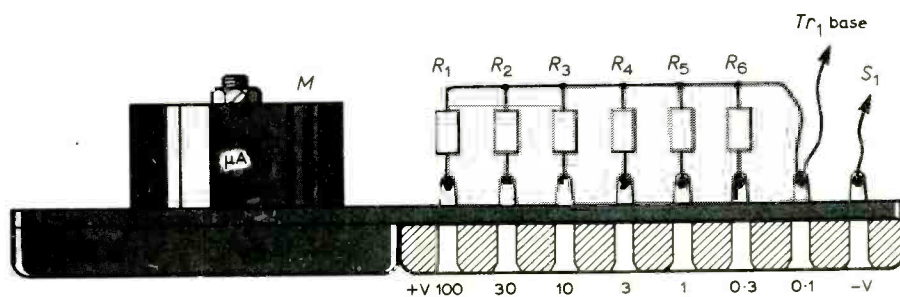


Fig. 2. Construction of the voltage multiplier.

\* Moscow, U.S.S.R.

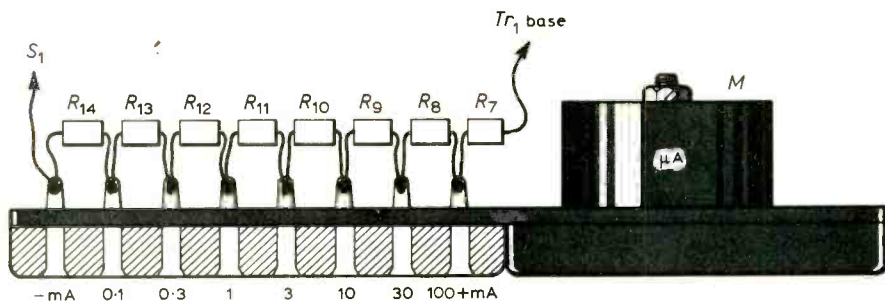


Fig. 3. Construction of the current multiplier.

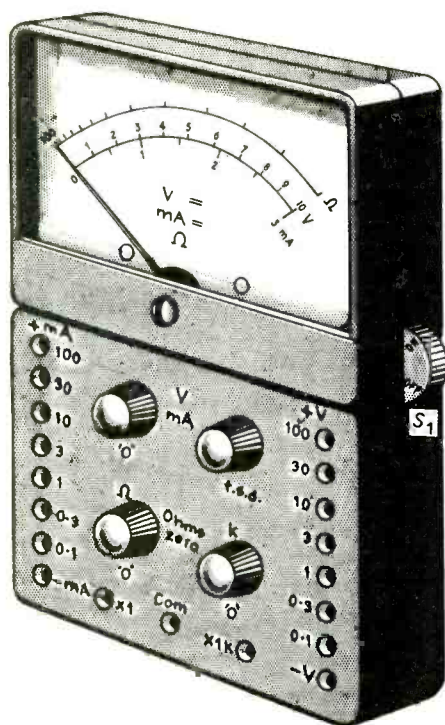


Fig. 4. Position of the main parts of the multimeter.

(multiplier), it can be selected as  $68\Omega-1\%$ ;  $R_9$ ,  $220\Omega-5\%$ , 230 ohm, etc.

The position of the main parts of the multimeter is shown in Fig. 4. All the additional information can be found in the previous article by Mr. Linsley Hood, *Wireless World*, June 1972, pp. 279-280.

#### Components list

##### Resistors

$R_1$	50M	$R_{13}$	2.3
$R_2$	15M	$R_{14}$	1
$R_3$	5M	$R_{15}$	100
$R_4$	1.5M	$R_{16}$	100 preset
$R_5$	450k	$R_{17}$	120k
$R_6$	100k	$R_{18}$	50k preset
$R_7$	49k	$R_{19}$	47k
$R_8$	670	$R_{20}$	18k
$R_9$	230	$R_{21}$	10k preset
$R_{10}$	67	$R_{22}$	680
$R_{11}$	23	$R_{23}$	500 preset
$R_{12}$	6.7	$R_{24}$	3.3k

##### Transistors

$Tr_1, Tr_2$	BC184L
$Tr_3$	MPSA65

content can be accurately preserved, and in addition the transduction is reciprocal so the same finger pattern will regenerate an electric signal from the s.a.w. Bandwidth of the finger array can be simply adjusted by alteration of the number of finger pairs, and electrical impedance determined by the choice of radiating aperture.

In addition to making use of the delay properties by selection of the material used for the piezoelectric substrate — and, of course, the separation of the transducer arrays, the designer can use the same type of element array to make bandpass filters with very small changes in the techniques employed. Tapped delay lines can also be readily devised, and a recent new application has been found for surface acoustic wave devices in f.m. pulse compression filters.

With such a variety of applications already realized for the s.a.w. device, it is small wonder to find that even more advanced projects are planned for the future. Several companies are experimenting with the s.a.w. devices, Microwave and Electronic Systems Ltd, in a recent statement, outlined some future products.

#### Future development prospects

An example of one of the devices predicted is the linear frequency discriminator. This consists of two filters having triangular insertion loss characteristics of equal width, but offset by a frequency difference equal to half the separation of stop band. Positive or negative slope discrimination over bandwidths and frequencies difficult to deal with using conventional design techniques may be easily accommodated using the s.a.w.

Adaptive non-linear convolvers may not be familiar to too many. They use the non-linear interaction of the s.a.w. signal with a reference signal propagating in the opposite direction. The resultant signal at the sum frequency has a very low or even zero velocity (comparable to a standing wave) and can thus be integrated over considerable time periods using a capacitor. The basic mathematical process offered is that of convolution, but correlation is achieved by making the reference signal the reverse of the incident signal.

Finally, the s.a.w. device offers excellent possibilities for the synthesis of highly stable oscillations at v.h.f. and beyond. In practice the actual stability is not as good as conventional quartz crystal oscillators, but there is the advantage of being able to operate at fundamentals of 400MHz and provide the additional facility of electronic tuning over a range of up to 1 part in  $10^3$  with small sacrifice in stability.

Currently, principal substrate materials employed in the production of s.a.w. devices are bismuth germanium oxide, with a surface wave velocity of  $1.6 \times 10^3$  m/s, lithium niobate having a velocity of propagation  $3.5 \times 10^3$  m/s, aluminium nitride,  $5.8 \times 10^3$  m/s and finally the more familiar ST-cut X propagating quartz having a s.a.w. velocity of  $3.1 \times 10^3$  m/s.

## Developments in Surface Acoustic Wave Technology

Eighty-six years ago, Lord Rayleigh discovered the surface acoustic wave effect by which a signal can be propagated and remain on the surface of a material. Instantaneous examination of the propagating waveform in spatial terms gives access to a real time signal which can be sampled or modified. Such a facility extends the designer's armoury where conventional electronic or electro-magnetic circuits are unsuitable. Perhaps the most important of the applications for this type of phenomenon is in practical delay circuits for frequencies from 10 to 400MHz

and delays up to  $50\mu\text{s}$ .

Conversion of electrical to acoustic energy, and the reverse, is achieved by using interdigital transducers consisting of two sets of interleaved metal fingers spaced one-half of an acoustic wavelength apart. The resonant frequency of this electro-mechanical pattern is obtained from dividing the s.a.w. (surface acoustic wave) velocity by the finger spacing, and if a signal of such a frequency is applied across the fingers, then a surface wave will be launched down the piezoelectric substrate. Since the s.a.w. is non-dispersive, the information



# Design Criteria for Logic Power Supplies

by R.B.D. Knight,\* M.A., D. Phil, M.I.E.E.

The features required from a power supply intended for integrated circuit logic are examined. Criteria are stated which, applied to the design or selection of supplies, will improve both economy and reliability of equipment.

Since their introduction in the late fifties, power supply modules have become considerably more refined. Ever smaller variations in output voltages are quoted for changes in load, temperature, time and mains input. Current limiting and protection against voltage transients are often offered as integral parts of the design or as optional extras. It was natural that the designers of logic systems should seek supplies for their circuits from the wide range of standard units available from a large number of manufacturers. The choice made was more important than it appeared at first sight because a unit misguidedly selected on the basis of price, size or an irrelevant technical feature may well have had subtle snags which caused apparently inexplicable i.c. failures and so gave poor equipment reliability.

For reasons of low cost and the wide variety of circuit functions available, 74 series t.t.l. logic working from a nominal 5V supply is very popular. It is generally known from manufacturers' data sheets and applications information that for correct operation:

- The supply voltage must be between 4.75 and 5.25V (industrial) or 4.50 and 5.50V (military grade),
- The supply voltage must not exceed 7.0V,
- No voltage exceeding 5.5V may be applied to a logic input, and
- Every 5 to 10 packages must be decoupled by a capacitor of 0.01 to 0.1 $\mu$ F having good r.f. properties.

It is less easy to find out that:

- Voltage transients exceeding the stated maxima even for a fraction of a microsecond can cause degradation even if catastrophic damage does not ensue.
- Slow changes in supply voltage, e.g. 1V/ms, within the normal limits, are tolerable.
- When the "totem-pole" output stage (see Fig. 1) switches, a heavy current pulse results from the non-conducting transistor switching on before the conducting transistor switches off. This pulse has a duration of the order of a

nanosecond and is the reason for decoupling groups of i.c.s.

- The supply must be free from fast transients and these must not be induced by the current pulses through the totem-pole.
- Conductors longer than 25cm or so behave as transmission lines and not as short circuits to pulses having the rise times to which t.t.l. circuits are sensitive.

## Properties of stabilized supplies

The arrangement generally used in the design of stabilized power supplies is shown in Fig. 2. An amplifier compares the output voltage with a zener reference and develops a control signal which is applied to a series element. The higher the gain of

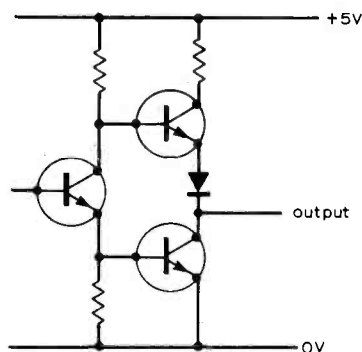


Fig. 1. "Totem-pole" output stage.

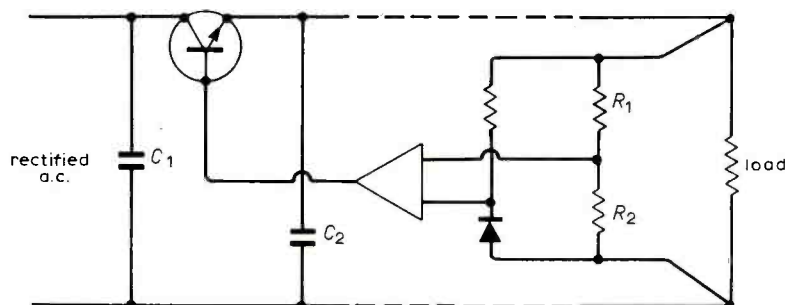


Fig. 2. Series stabilized power supply.

the loop the lower is the output impedance at d.c. and the greater the immunity from changes in mains input. The use of remote sensing connections as shown, enables a low output impedance to appear at a point physically distant from the supply. However, this low impedance is only demonstrated at d.c. and low frequencies. In order to be stable the supply must be designed so that the loop gain of its control system must fall with frequency in a controlled manner. This results in an output impedance which rises with frequency. This rise is controlled by the capacitor  $C_2$  in Fig. 2.

The higher the loop gain of the system the more difficult it becomes to control its frequency response. A low gain design giving modest performance can be stabilized by a single time constant, but high gain designs require two or even more shaping circuits. Inescapably associated with these is a relatively high phase shift at certain frequencies which results in ringing in response to sudden changes in load current. Even worse, transient response is likely if remote sensing is employed as a further time constant is added, as shown in Fig. 3. Resistors  $R_3$  and  $R_4$  represent the resistances of the leads between the power unit and the load;  $C_3$  is the total capacitance at the load end and is largely made up by the decoupling capacitors distributed amongst the i.c. packages. The inductances of the leads,  $L_1$  and  $L_2$ , may also be significant. All these parameters are outside the control of the power supply designer, but an inescapable part of the loop which he is trying to design to be stable! The selection of a supply module having an outstanding performance in the conventional sense in

\*Measurement consultant to Semitron Ltd.

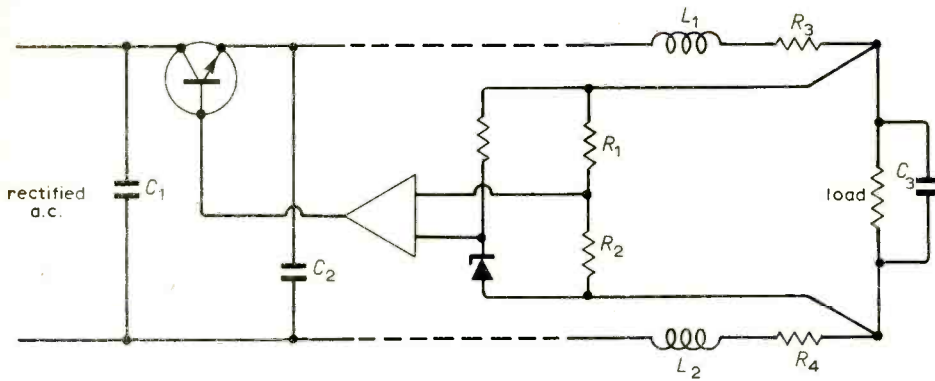


Fig. 3. Supply with long output leads.

the belief that this will ensure that there are no problems in this area is therefore a serious mistake. If anything, the reverse is likely to be true.

**Voltage transient protection.** A small rise in voltage at the output of a supply based on Fig. 2 causes the series element to be cut off, giving the unit a very high output impedance. If, for example, the 5V rail is accidentally shorted to one at a higher voltage or touched by a charged object such as an unearthed soldering iron there is nothing to prevent an excessive potential reaching the logic circuits. If the series device should fail and become a short circuit the output voltage will rise dangerously and cause extensive damage to the logic devices. To reduce these weaknesses, thyristor "crowbar" circuits are often added. The principle of these is shown in Fig. 4. These do not give such satisfactory protection as is often imagined. The switch-on time of most thyristors is of the order of microseconds and the firing circuit adds more delay between the appearance of an excessive voltage and the thyristor becoming effective.

When the mains supply is switched on unpredictable voltage conditions exist throughout the stabilizer and crowbar circuits. These also vary with the exact instant during the supply waveform when the switch is closed. Any bounce in the switch further complicates the situation. Under these conditions it is possible for an even larger and longer voltage transient to occur at the output and not be restrained by the "protection" circuit.

**Current limiting.** If an excessive current is drawn from a power supply its output voltage will fall. This fall may be related to the current in various ways, as shown in Fig. 5. Curve 1 shows considerable foldback, i.e. the output current falls greatly when the supply is overloaded. This brings the danger of lockout states if the load line representing all the logic elements intersects the characteristic at three points. A typical t.t.l. load line is shown dotted in Fig. 5 as curve 2. Much less favourable load lines, such as curve 3, have been reported by Kalb.† However, such extreme cases as he reports were con-

cerned in circuit studies and should not be observed among devices from reputable manufacturers' production runs.

Curve 4 in Fig. 5 shows a modest amount of foldback which would be unlikely to permit lockout conditions to arise. Curve 5 demonstrates the characteristic of a supply which transfers from a constant voltage to a constant current mode. For comparison, the relationship for a simple shunt zener regulator (Fig. 6) is shown in the figure as curve 6. The use of foldback current limiting is attractive to the power supply designer as this leads to a reduction

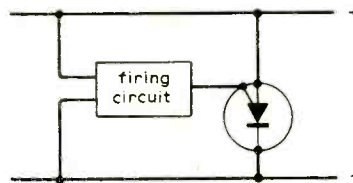


Fig. 4. Thyristor "crowbar" protection circuit.

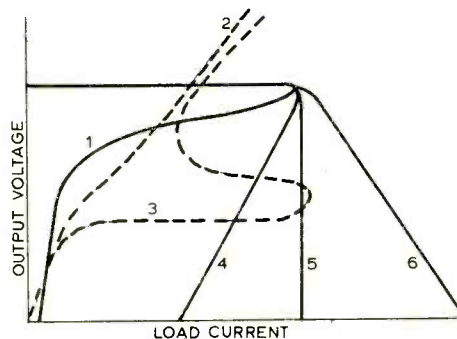


Fig. 5. Characteristics of supplies and loads. 1. Supply with considerable foldback 2 & 3. t.t.l. load lines. 4. Supply with slight foldback 5. Supply having constant current characteristic. 6. Shunt zener stabilizer.

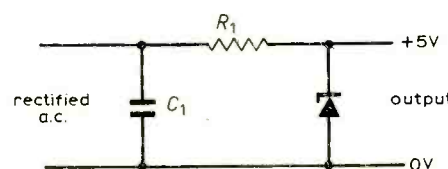


Fig. 6. Shunt regulator using zener diode.

of the dissipation in the series element under conditions of short-circuits and other heavy loads on the output. This can make possible the use of a smaller heat sink or fewer series transistors. However, it is obvious from Fig. 5 that the more re-entrant is the overload characteristic the more probable it is that equipment will fail to function due to having fallen into a lockout condition. At best it may be necessary to use a power module rated at a current significantly higher than the useful load to ensure that there is only one crossing of the load line and limiting characteristic. The supply least likely to give this problem is the simple shunt zener regulator.

**Recommended design approach**

Obviously a supply must always provide an output voltage between the required limits. This is not, however, a stringent design feature. It is essential for a power supply intended for logic circuits to have a controlled transient response in order to be free from significant ringing or overshoot. These are more important than the transient response time itself. The transient performance must not be degraded by the addition of unspecified amounts of additional capacitance across the supply terminals, even at the end of long leads. These requirements are best met by a simple design. The resulting regulation against mains input and output load changes, though poor by power supply industry standards, can readily be arranged to be tolerable by logic elements, allowing in addition for ripple and voltage drop in wiring. Remote sensing is not needed for relatively low currents and is indeed a disadvantage owing to the extra difficulty of obtaining the required transient response. However, when the voltage drop in the cables between the supply module and the load is likely to exceed 100mV, the advantage of eliminating this outweighs the problems which result.

The current limiting characteristic is not too critical although it is essential to ensure that this is crossed only once by the load line of the circuits being driven by the supply. Undoubtedly the less re-entrant this is the more certainly the supply is compatible with any logic elements. Over-voltage protection is very desirable, but to be truly effective must operate very much faster than any thyristor circuit. A zener diode, being a single sharp junction device, gives far superior limiting. Devices having the essential sharp knee, well defined breakdown voltage, very low slope resistance and high surge power ratings have been designed for this application and are now readily available. These devices provide, for the first time, the possibility of effective protection of integrated circuits from damage due to voltage transients. To avoid delays in the operation of the protection due to transmission line effects the device should be installed close to the logic elements. A large heat sink is not mandatory, since the dissipation is negligible under normal conditions. If a sustained excess voltage

†"Design Considerations for a t.t.l. Gate", Jeff Kalb, National Semiconductor Corp. publication TP-6.



occurs, due to a short circuit to a higher voltage rail or a short-circuited series element in the power supply, the dissipation in the protecting device may be excessive. If the device then fails it will almost certainly become a short circuit, continuing to protect the integrated circuits. Repairs are therefore limited to the power supply area and costly searches through the logic circuits for elements which may be only slightly damaged are still avoided. The shunt stabilizer of Fig. 6 inherently provides fast protection against voltage spikes.

**Other logic families.** The demands which 74 series t.t.l. makes from its power supplies apply to the high speed 74H versions, with somewhat greater emphasis. Slower families give less of a current pulse problem but m.o.s. in particular, is very prone to damage by voltage transients. All widely used logic integrated circuits are able to tolerate  $\pm 5\%$  total voltage excursions. Many are unaffected by  $\pm 10\%$ . The same general principles should therefore be applied in the provision of power supplies for all current types of digital integrated circuits.

### Conclusions

Comparison of the properties of standard stabilized power modules and the requirements of logic elements reveal that the supplies give a very well defined voltage, which the integrated circuits do not need, and no protection from voltage transients. Even power supplies with thyristor crowbar circuits may allow, or even cause, dangerous transients.

The specification of sophisticated power supply units for integrated circuit logic is not only uneconomic but also unsatisfactory. Local decoupling of devices, in accordance with device manufacturers' recommendations, should be provided to supply pulse currents without delay due to transmission line effects. The supply module must not oscillate and must have a suitable response to transient currents whatever the total value of capacitance connected at the remote end of the supply leads. The regulation and ripple are not critical, but the total voltage excursions must be within the limits specified for the logic family. A simple shunt zener regulator meets all the requirements and is a practical solution for all currents for which suitably specified zener diodes with the required power rating are available. Overvoltage protection is strongly advised, particularly where series stabilization is utilized in the supply design. This should be obtained by the use of the special zener diodes now available for this purpose. Zener protection can also be added to existing system designs with advantage.

## British participation in ESRO-4

The latest spacecraft from the European Space Research Organization is that of ESRO-4 which was launched by a four-stage, solid-propellant Scout rocket on 21st November, at NASA's Western Test Range in California. There are five experiments on board, one of which was mounted by the Mullard Space Science Laboratory, Dorking, Surrey, and supported by the Science Research Council. The prime function of this British experiment is to measure ion (charged atom) density, temperature and composition of the Appleton or F-layer of the ionosphere.

On the satellite structure three sensors are used for measurement, one of which is a gridded, spherical, ion-collecting probe 20cm in diameter fitted to the end of one of three, 1.3 metre folding booms. The booms perform two functions, one of which is to de-spin the craft after orbit insertion, and the other to position the ion probe clear of the space-charge which will surround the vehicle.

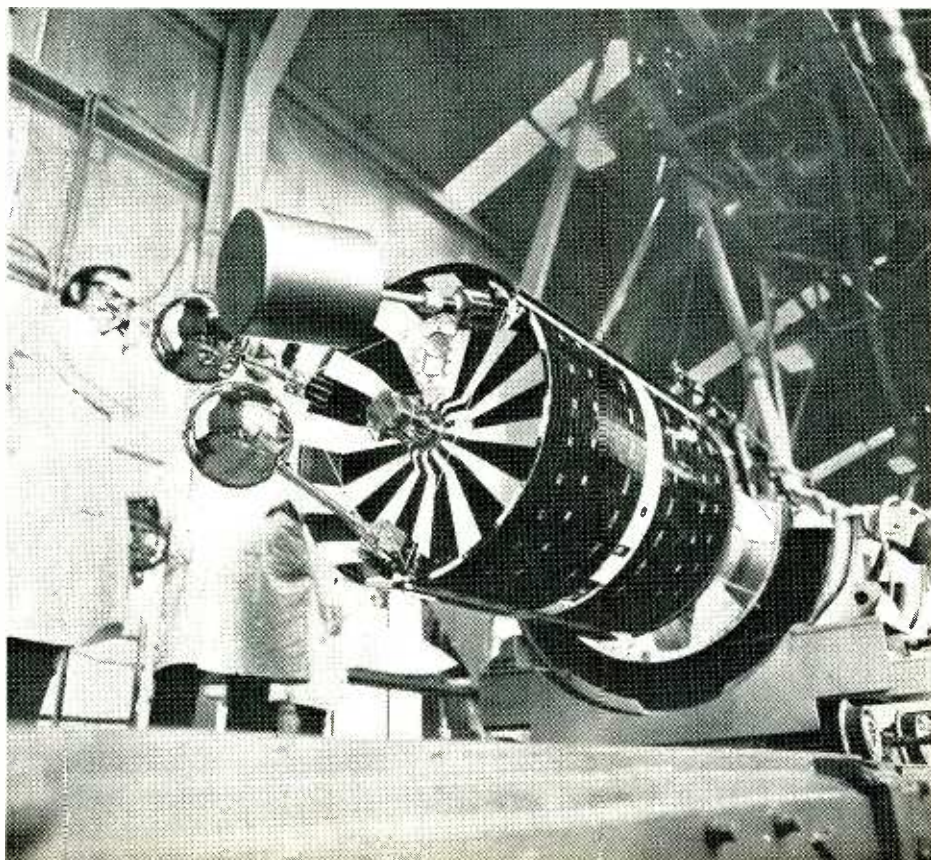
The electrical potential of the probe is swept repeatedly from positive to negative enabling it to act as an ion mass spectrometer. On the same boom as this probe, but very close to the craft, is a smaller sphere of 1cm diameter designed to collect residual electrons and, therefore, to define

the spacecraft's absolute potential in space. This feature allows the correct interpretation of the mass spectrometer readings to be obtained.

A third probe, 10cm in diameter, carried on a boom 0.35 metre in length and mounted axially at the base of the satellite, has a constant charge applied with respect to the spacecraft, which serves as a type of calibrator against which the apparent ion density can be continually checked. The charge is adjusted to represent the mid-range value at the beginning of each potential sweep of the spectrometer probes, so that short period fluctuations in ion current can be detected down to the order of 2%, whatever the residual ion density.

The spacecraft was planned to have a nearly polar orbit with altitudes varying from an apogee of 1100km to a perigee of 280km. Spin rate before orbit insertion was about 150 r.p.m. and after the operation of the de-spin booms it would have been reduced to 65-70 r.p.m. There are five different attitudes planned for the various experiments which are acquired by a command operated magnetic torquer. The prime contractor for this scientific satellite was Hawker Siddeley Dynamics under contract from the European Space Research Organization.

*Spacecraft ESRO-4 on a test rig in California*





# World of Amateur Radio

## Hobby for the well-heeled?

Is amateur radio becoming a high-cost hobby demanding little from its adherents other than a willingness to pay out hundreds of pounds for factory-built equipment? This is a question which can be guaranteed to rouse strong feelings. But certainly the number of amateur "shacks" containing equipment costing £500 or even well over £1000 is now quite high. Amateur communication receivers range up to more than £250; many transceivers are around this figure (though de luxe models such as the CX7A are about £1000); linear amplifiers around the £150 mark; r.f. speech clipping units possibly £50; electronic keyer say £25; beam aerials and towers, virtually no limit; and so on. All this seems a long way from the 0-v-1 ("straight") receivers and the two-band, 10-watt transmitters of the 'thirties, or the surplus HRO and home-built a.m./c.w. transmitter of 20 years ago.

Undoubtedly many amateurs are concerned at this transition from a do-it-yourself and self-training activity to what is increasingly a cheque-book hobby, though some of us continue to find much interest in what are virtually "junk-box" stations. It is still possible to put an amateur station — particularly a c.w. station — on the air for under £25.

## Easier licences?

A similar, and related, debate in amateur circles is about the constant pressure in many countries to make it simpler to obtain amateur licences. To quote a guest editorial in *Break-In* (New Zealand): "At the present time there seems to be a great hue and cry to lower the requirements to become an amateur radio operator . . . we feel that quality will always count more than quantity". The writer notes the outcry against having to learn the "archaic" Morse code and the arguments against formal radio theory examinations, and the feeling that amateurs form an "exclusive club" without regard for the many who wish to participate in the hobby.

The writer quotes an amateur in Japan (where it has been made very easy to obtain a first licence) as suggesting that "many now get a licence after a short

course, buy equipment, send off application for station licence, get on the bands for enjoying long chats with girl friends . . . and then sell their equipment".

The editorial points to the value of c.w. and theory examinations, not only for their own use, but also as a way of ensuring that a licence is valued as something which requires effort to obtain. Certainly most of us who struggled (against our wishes) to learn c.w. operation have subsequently never regretted making the effort.

Yet the following comments were received on 3.5 MHz from a Chesterfield amateur: "I find most days not one c.w. station using the band — often day after day it is the same until the evening, no c.w. but tons of s.s.b. proving the band is open . . . I tested Top Band (1.8 MHz) to find out how much it is used in daytime for c.w. I gave a series of CQ calls across eight hours per day for five days. Not one c.w. station came back".

## Amateurs and BBC-50

The amateur's role in the early days of broadcasting received at least partial recognition during the recent BBC-50 celebrations, though one missed any account of the broadcasting by amateurs in the period 1920 to 1923 or what was virtually the start of Empire broadcasting by the late Gerald Marcuse, G2NM.\* The successful joint I.E.E.-R.S.G.B. lecture by G. R. M. Garratt, G5CS, though full of fascinating detail of the historic events between 1896 and 1901 was placed well before the more controversial love-hate relationship between amateurs and the early B.B.C.

One historic document, the 1921 petition presented to the P.M.G. by the Wireless Society of London and signed by 65 local societies, appears to have been lost for ever, despite the efforts in the early 1940s by Arthur Milne, G2MI, to preserve the petition which he found in Post Office archives marked for destruction. Fortunately he made a photocopy of the document though the original now seems to have vanished for ever. The petition addressed to the Rt. Hon. F. G. Kellaway asked that regular "wireless telephony" transmissions be made, and foresaw the educational value of wireless as well as its use for entertainment.

## Contest Notes

A well-known call-sign appears at the top of the list in the recent 1.8 MHz contest: G6UW, call of the Cambridge University Wireless Society (operated by D. I. Field, G3XTT). Leading scorer in a recently introduced "under 18" section was A. McHale, G4AMH. Revised dates for a number of 1973 contests have been announced by the R.S.G.B.: National Field Day June 2-3; S.S.B. National Field Day July 14-15; Diamond Jubilee h.f. contest, May 12-13 (telephony) and May 19-20 (c.w.). But one must query the action of the R.S.G.B. in organizing for its Diamond Jubilee h.f. events (covering 1.8 to 30 MHz) a contest in which "only contacts between stations in the British Isles will count" in view of the efforts over many years to discourage the use of such bands as 14 and 21 MHz for semi-local contacts. A most curious way of marking 60 years of service to the amateur movement!

The A.R.R.L. continues to issue large numbers of Worked All Continents awards: of 1846 certificates issued in one year, 881 were endorsed for s.s.b., 12 for r.t.t.y., 51 for 3.5 MHz operation and four for 1.8 MHz. A number of these awards have recently been issued for slow-scan television.

Of the 31 awards for 1.8 MHz operation issued up to November 1972, Stew Perry, W1BB, reports that seven were to amateurs in England (G6GM, G3PU, G30QT, G3PQA, G3BBP, G3FPQ and G3LIQ), two to Scottish amateurs (GM3YCB, GM3WDF) and one in Northern Ireland (GI6TK).

\*Recognition is given by Edward Pawley in his recent book "BBC Engineering 1922-1972" — Ed.

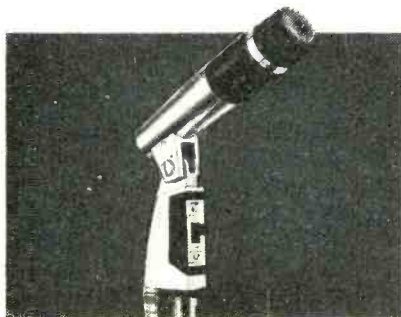
## In brief

Three American organizations and the Cornish Amateur Radio Club are to mark the 70th anniversary of the opening of "CC", the original Marconi transatlantic station in the United States at Cape Cod on January 19, 1903. Special amateur stations will operate from the original sites at Cape Cod and Poldhu. . . . Efforts are being made to establish a new society in the Denby Dale district of Yorkshire and a meeting will be held on January 24 at the local Pie Hall (details J. Clegg, G3FQH, 8 Hillside, Leak Hall Lane, Denby Dale, Huddersfield). . . . Sound advice on the cure of TV and audio breakthrough is given in a new 100-page "Television Interference Manual" by Barry Priestley, G3JGO (published by R.S.G.B. at 90p including postage) which emphasizes that the main problems are those arising from the social difficulties created between the amateur and the viewer. . . . "The Amateur is balanced" — so runs the A.R.R.L.'s amateur's code — but a recent enquiry to the League makes one wonder: "I am going on a honeymoon to Florida and would appreciate advice on what 2-metre f.m. frequencies would be most practical to operate"! Pat Hawker, G3VA





## Microphones matter most.

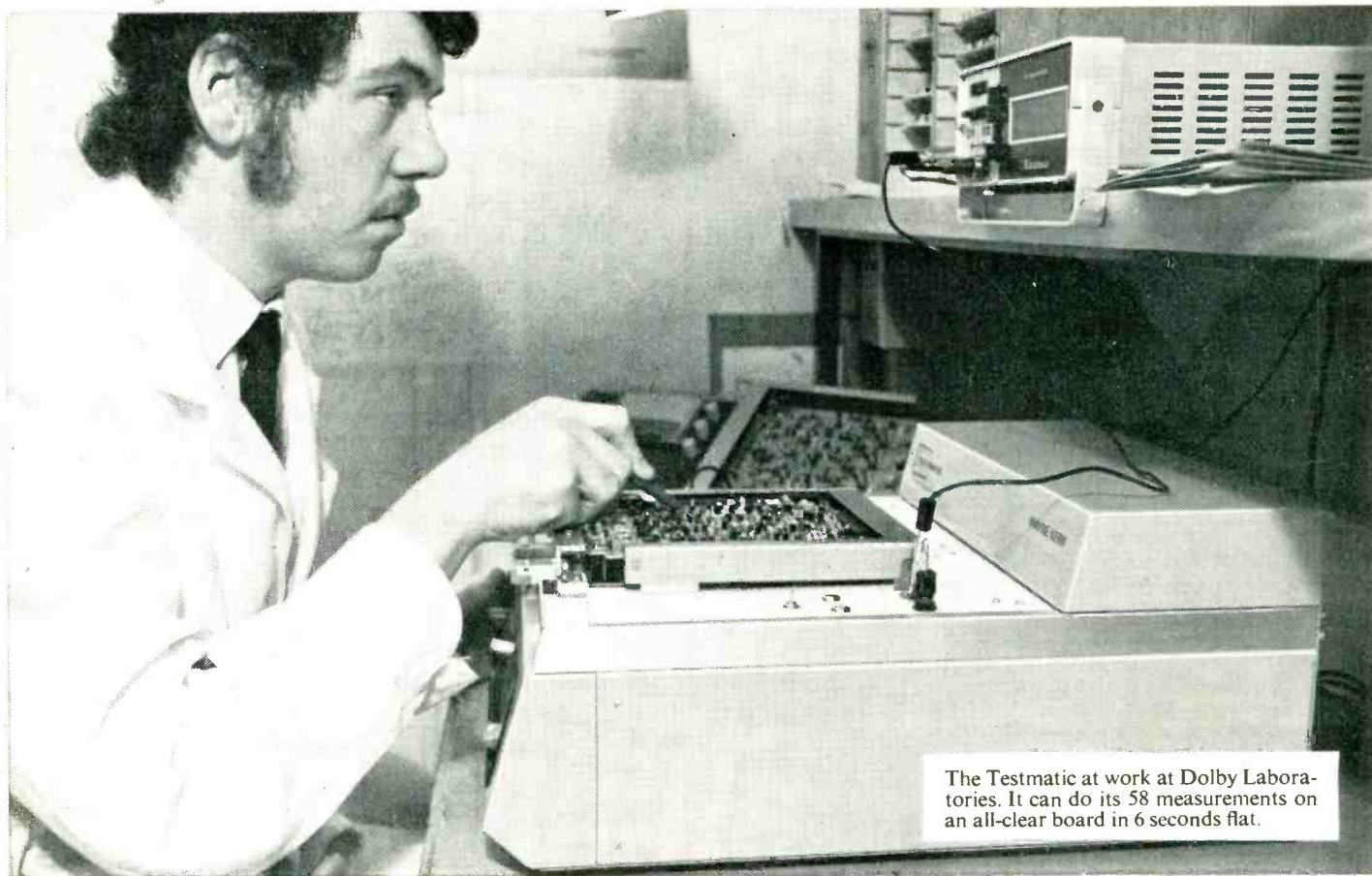


Never have so few words said so much about sound system installations. The truth is that a carefully chosen, top-quality microphone makes a measurable difference in sound system quality—regardless of the other components in the system. It is false economy at its worst to be a microphone miser. Install *Shure Unidyne* or *Unisphere* microphones—for installations with a marked superiority in voice intelligibility (and fewer service calls due to microphone problems).

Shure Electronics Limited  
84 Blackfriars Road  
London SE1, 8HA Telephone (01) 928 3424



WW-081 FOR FURTHER DETAILS



The Testmatic at work at Dolby Laboratories. It can do its 58 measurements on an all-clear board in 6 seconds flat.

# 'If the Wayne Kerr Testmatic did not exist, it would have been necessary for us to invent it'

*Dave Peacock, Head of the Test Department, Dolby Laboratories Inc.*

The heart of a Dolby System noise reduction unit is a small but complex circuit board. In six-by-seven inches are assembled no fewer than 507 resistors, capacitors, diodes and transistors.

On that score alone, fault-finding is a major operation. And as Dolby's policy is to make all processors interchangeable, they have to guarantee the stability of every part of the circuit. So their electronic checkout procedure entails 58 separate DC measurements.

Said Dave Peacock, head of the Test Department: 'An interesting thing about our board is that it is specifically designed to suit the Testmatic. We began by making a thorough search of the market to see if there was a testing machine that would suit us. Had the Testmatic not existed, we should have had to invent something very like it ourselves.'

'How has it done? Well, on average we get about 2.5 faults a board. Half of these are DC

faults. Thanks to Testmatic, finding and correcting them take only 10 percent of our electronic checkout effort.

*'We've costed it, and we know it has saved us more than £1,000 in a year — using the TM60 for a mere 2½ hours a day. But we're stepping up output, so next year the saving should be even more impressive.'*

'Any teething troubles? . . . I wouldn't say so. We hit a small snag about a year ago but the Wayne Kerr service was so prompt that the whole thing was really a non-problem . . .'

The Wayne Kerr Testmatic TM60 — for testing circuit boards, cableforms, sub-assemblies. For more information call Bognor Regis (02433) 4501 or write to the address below.

**WAYNE KERR**

Durban Road, Bognor Regis, Sussex PO22 9RL

A member of the Wilmot Breeden group

WW—082 FOR FURTHER DETAILS



# New Products

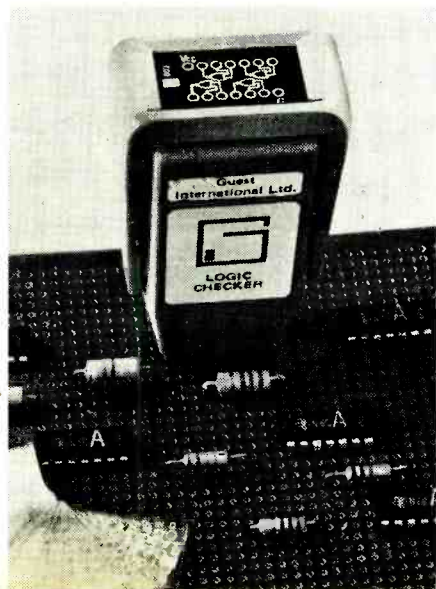
## Tester for transistors and diodes

An addition to the Semitest family of i.c. testers is the Semitest V. Manufactured by Rohde & Schwarz, it is battery-operated and permits measurement of the static characteristics of transistors (current gain, leakage current, break-down voltage up to 15V), diodes (leakage current, forward voltage) and zener diodes. The Semitest V may also be used for function tests on thyristors, resistance measurements and insulation checking in the range of 100 to  $10^{10} \Omega$ . The instrument contains two voltage generators ( $\pm 0$  to 10V and  $\pm 0.5$  to 15V, error  $\pm 3\% \pm 15\text{mV}$ ,  $I_{max}$  10mA), a constant-current generator (10 $\mu\text{A}$  to 10mA, error  $\pm 3\% \pm 1\mu\text{A}$ ). Error limits on meter amp.  $\pm 3\% \pm 0.2\text{nA}$  and 10mV to 30V ( $\pm 3\% \pm 10\text{mV}$ ). U.K. agents. Aveley Electric Ltd, Roebuck Rd., Chessington, Surrey.

**WW302 for further details**

## I.C. logic checker

Manufactured by the Industrial Components Division of Guest International Ltd, a new logic checker features an l.e.d. display. The unit is suitable for use with all d.i.l. integrated circuits having 16 leads or



fewer. It can check t.t.l. or d.t.l. gates, flip-flops, counters, shift registers, decoders, adders, etc. Input impedance corresponds to a single t.t.l. load and there is no interference with the circuit under test.

The logic checker automatically takes its power supply from the i.c. terminals and requires no other external power connection. A particularly useful feature is the clip-on plate showing the logic circuit connection within the i.c. which is placed over the display in order to establish both the circuit and the operating conditions. All logic states can thus be quickly assessed. Price is £23.50. Guest International Ltd, Nicholas House, Brigstock Road, Thornton Heath, Surrey CR4 7JA. **WW309 for further details**

## Interface logic AND driver

An 8-pin, d.i.l., i.c. device, for high-current, high-speed switching operation, is a dual peripheral position AND driver manufactured by SGS/ATES. Designated T75451A, it can be used in systems that employ t.t.l. and d.t.l. logic, and is designed to meet requirements such as high-speed logic buffer, power driver, relay driver, lamp driver, m.o.s. driver and memory driver. The T75451A is said to be free from latch-up and has diode-clamped inputs to simplify system design. Maximum output sinking current is 300mA at a guaranteed output low voltage of 0.7V, and 100 $\mu\text{A}$  of leakage current is guaranteed at 30V output. SGS/ATES, 20041 Agrate Brianza, Milan, Italy.

**WW313 for further details**

## Transistor Arrays

Five transistor arrays are now available from the Semiconductor Division of the Sprague Electric Co. These devices are of monolithic construction and combine the attributes of silicon integrated circuits with the design flexibility and accessibility of discrete devices. Designated the ULS-2045H, ULN-2046A, ULN-2054A, ULN-2081A and ULN-2082A, the arrays are especially useful in applications requir-

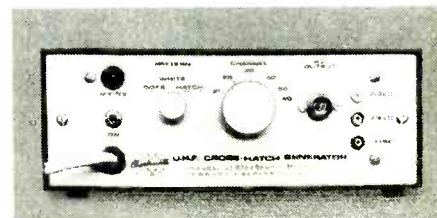
ing matched thermal and electrical parameters.

The first two types consist of five n-p-n transistors, with two connected as a differential pair; type ULN-2054A of six n-p-n transistors connected to form two independent differential amplifiers; and the last two types, each of seven n-p-n transistors connected in the common-emitter and common-collector configuration respectively. All types are well suited for a variety of applications in low-power systems in the d.c. to v.h.f. range. Sprague Electric (UK) Ltd, 159 High Street, Yiewsley, West Drayton, Middx. **WW311 for further details**

## Crosshatch generator

The Checkmate crosshatch generator, made by Industrial Electronic Products Ltd, is available from Manor Engineering. Its "test card" chequered border permits rapid TV picture adjustment of linearity,

crystal controlled crosshatch, dot and white field patterns are obtained by use of digital i.c. logic. Complete synchronizing

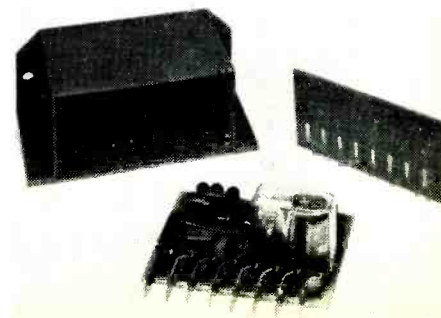


and blanking waveforms are provided, with 2:1 interlace. The generator's r.f. output tunes continuously over u.h.f. TV channels 21 to 65, obviating the need to disturb receiver push button settings. A stabilized power supply is included. Manor Engineering, The School House, Crookham Common, Newbury, Berks. RG15 8EJ.

**WW 305 for further details**

## Component housing

A small, compact and inexpensive electronic component housing is announced by Logikontrol Ltd. Made of high impact polystyrene, it measures 90 x 50 x 37mm including mounting flanges and has an internal volume of 10cc. Among various features, it can accommodate two printed circuit boards on which miniature mains transformers and relays may be mounted. Printed circuit fast-



on connectors and the snap-fit lid eliminate the need for a special plug and socket. Available in five different colours from Logikontrol Ltd., 17 Little Edward Street, London NW1 4AT.

**WW319 for further details**

### Wide-angle viewing l.e.d.

The Litronix RL 21 light-emitting diode announced by Guest International features an extra large radiating area and high luminance at a current of just 20mA.

This l.e.d. is i.c. compatible and designed for front-panel mounting, using either matt black or clear plastic clips which are supplied free. The terminations are rectangular section making them suitable for either soldering or wire-wrapping. It is suitable for wide-angle viewing and the standard device is available in a diffused red moulded package. Clear red, diffused white, or clear packages are also available. Power dissipation at 25°C is 200mW and recurrent forward current is 1A max. Continuous forward current is 100mA max. Guest International Ltd, Nicholas House, Brigstock Road, Thornton Heath, Surrey CR4 7JA.

**WW321 for further details**

### A.C. voltmeter

The new TM4 voltmeter from Farnell measures a.c. from 300 $\mu$ V to 100V f.s.d. at frequencies up to 33MHz. The instrument has a high input impedance minimizing test circuit loading. Loading can be reduced still further by using a passive or active oscilloscope probe. Probe compensation facilities are provided and an output



is available on the front panel to power the active probe. A switched filter is provided to remove unwanted and irrelevant high-frequency signals and noise when making low-frequency measurements. An output capable of driving a pen recorder is provided. The instrument is housed in a grey case with satin-chrome handles and has a retractable tilt stand. The U.K. price is £80. Farnell Instruments Ltd, Sandbeck Way, Wetherby, Yorks, LS22 4DH.

**WW328 for further details**

### A.F. filter system

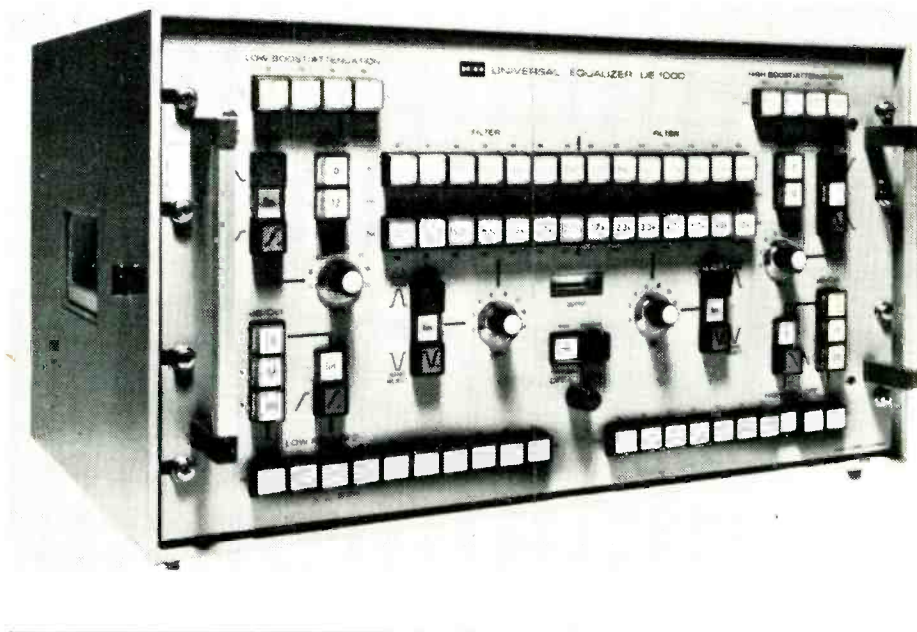
The Universal Equalizer UE 1000, now available from F.W.O. Bauch Ltd., contains eight a.f. filters, combined in six logically arranged equalizer modules. Corresponding to separate functions, these modules permit, through simple control adjustment, the introduction of one, all or groups of filters into the audio signal path.

Features of the UE 1000 include extended cross-over, limiting and cut-off frequencies, as well as improved roll-off slopes of 12, 24 and 36dB/octave, previously only available as 12 or 24dB/octave. The UE 1000 provides distortion-free processing of high signal a.f.-input levels up to a maximum of +22dBm corresponding to 10V, with in-built over-

load indication and protection. Frequency range is from 20Hz to 20kHz, while distortion is less than 0.3% even at +22dBm.

Operation of the "linear" or "equalizer" switches permits the audio signal to be fed unchanged to the audio input, or through the equalizer stages, respectively. The equalizer switch can also be operated during use, for subjective comparison of the reproduction quality in both "linear" and "equalizer" positions. The UE 1000 is self-contained in a standard 19in assembly for rack or surface mounting. F.W.O. Bauch Ltd., 49 Theobald Street, Boreham Wood, Herts. WD6 4RZ.

**WW317 for further details**



### Touch tuning i.cs

Siemens have now introduced in the U.K. their touch sensitive tuning i.cs which replace the mechanical push-buttons on TV tuners. With a mere touch of a finger, channels can be selected and indicated. For even greater convenience a low-cost remote control unit could be used for channel changing, using only a single wire. The new i.c. is also applicable in any similar electronic equipment, i.e. test stations in factories or electronic push-button control in lifts etc. The new unit should improve the reliability of TV and radio channel selection systems where varicap tuners are used, for it has been found that the main failure occurs with the mechanical push-button unit, due mainly to oxidation of the switch contacts.

Only a low-voltage supply is required permitting either the use of inexpensive filament lamps for channel indication or opening up possibilities for future designs with gallium-arsenide diodes, or perhaps even liquid crystals. Because of the low voltage concept, it is also unnecessary to isolate the touch-system from the mains supply or use rectified mains, thus saving additional expensive high ohmic value resistors with high voltage capability.

But perhaps even more important, it permits the circuit to meet the safety requirements of BS 9000, which is in preparation.

Two types are available — the SAS 560 and the SAS 570. Each consists of four similar stages, and up to twelve channels are possible for television use. The SAS 560, a basic 4-stage unit, features an internal memory, which ensures that when the receiver is switched on, channel one is always selected. This could be tuned to the viewer's preferred station. The price of one circuit in production quantities is around 35p.

The input of the i.c. is very sensitive and still works when the resistance of the finger is more than 100M $\Omega$ . There are two independent outputs for each channel — one to switch the varicap supply, the other to switch the indicator lamps, and on export sets, the u.h.f./v.h.f. band switch.

A remote control system for channel switching could be connected to the i.c. Selection would be performed by stepping through the channels and stopping on the one required. Siemens Ltd, Great West House, Great West Road, Brentford, Middx.

**WW304 for further details**



## Thick-film potentiometer

Coutant Electronics Ltd are manufacturing a thick-film focus potentiometer, complete with resistive divider chain, for use in colour television sets. The potentiometer is claimed to offer many advantages over the conventional component employed at present, such as improved reliability, smaller size, better resistance to environmental extremes and superior long-term stability.

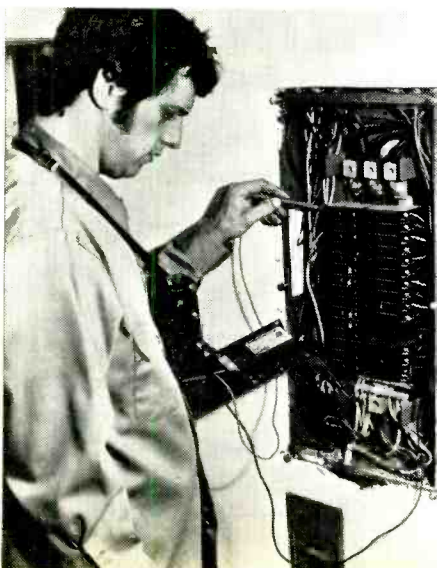
The unit is designed for o.e.m. use and consists of two high-value printed resistors and a central printed potentiometer track all connected in series. Resistor values are  $19.7M\Omega \pm 5\%$  (h.t. end),  $29.4M\Omega$  tracking to within  $\pm 5\%$  (potentiometer) and  $20.1M\Omega \pm 15\%$  (earthy end). Although the normal operating voltage is 9kV it will withstand 15kV across the complete chain, or 9kV across any two terminals with the control knob in any position, without damage or flashover occurring. It is claimed that resistance will stay within 2% of the nominal value for a minimum of 100 rotational cycles or for changes due to temperature.

The values of resistance have been chosen to make the unit compatible with any current production colour television tubes. Most important for domestic equipment, the moulded polypropylene case (measuring 65mm long  $\times$  42.8mm wide) not only protects the printed resistors from the ingress of atmospheric impurities but also is said to have an extremely good resistance to flame. Coutant Electronics Ltd., 3 Trafford Road, Reading, Berks.

**WW315 for further details**

## Circuit tracing device

A simple device for identifying electrical circuits and tracing wires has been introduced by Thomas & Betts. It is claimed that the method makes it possible for a single operator to identify and mark circuits safely in less time than it usually takes two men to do the same job by conventional means. The instrument, called the E-Z-Coder circuit tracer, con-



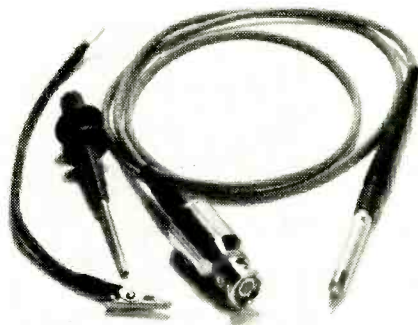
sists of a meter unit, a test block with 12 leads, and a carrying case designed to leave the operator's hands free. Circuits are identified by comparing the resistances of the individual leads connected through the test block, readings being taken off a 90° ohms scale.

Accurate readings are ensured by calibration of the meter prior to use. The adjustment screw is recessed to prevent accidental movement, and the clarity of the scale reduces the possibility of error. Power for the instrument is supplied by a 1.4V mercury cell with a life of about two years. The circuit tracer is fitted with a 'hot line' indicating light to warn the user of any live circuit. Protective insulation shrouds the 36in long test leads in case of contact with a live wire. By using more test blocks wired in series it is possible to check up to 156 wires in groups of twelve. Thomas & Betts Ltd., Greenhill House, 90-93 Cowcross Street, London EC1M 6JR.

**WW 308 for further details**

## Passive probe kit

Electroplan Ltd have introduced a passive probe kit to their accessories range. Known as the GE81600, the kit consists of 10:1 and 1:1 attenuator heads, a compensating lead assembly, a spring plunger body with hook tip and a detachable earth lead.



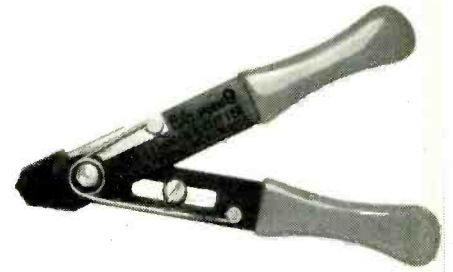
Using the 10:1 attenuator head, the probe may be used from d.c. to 70MHz and can be compensated for use with instruments having an input impedance of  $1M\Omega$  in parallel with 20 to 60pF.

For low-level signals, the 1:1 attenuator head can be used from d.c. to 5MHz and no compensation adjustments are necessary. The GE81600 passive probe kit is available from Electroplan Ltd, P.O. Box 19, Orchard Road, Royston, Herts. Price £9.00, quoting ordering code 15-44.

**WW312 for further details**

## Wire stripper and cutter

Bib Sales Division of Multicore Solders Ltd. have introduced a new wire stripper and cutter. Case hardened, with ground cutting surfaces, the wire stripper adjusts to most standard sizes of wire and is fitted with a handle opening spring to facilitate repetitive wire stripping. A handle locking catch is fitted at the top of the wire



stripper to keep the jaws closed when not in use. Recommended retail price of 75p. Bib Sales Division, Multicore Solders Ltd., Hemel Hempstead, Herts.

**WW 307 for further details**

## Low-cost digital multimeter

Fluke International Corporation have announced the 8000A, a low-priced multimeter which is guaranteed over the temperature range 15-35°C. It will measure a.c. and d.c. volts to 1200V, a.c. and d.c. current to 2A and resistance 20M $\Omega$ .

The following is a brief specification:

d.c. voltage  $\pm(0.1\% + 1 \text{ digit})$   
 a.c. voltage  $\pm(0.5\% + 2 \text{ digits})$   
 d.c. current  $\pm(0.3\% + 1 \text{ digit})$   
 a.c. current  $\pm 1.0\% + 2 \text{ digits}$   
 ohms  $\pm(0.2\% + 1 \text{ digit})$

Overload protection on the various functions: voltage ranges to 1200V r.m.s., current ranges to 2A r.m.s. (fused) and ohms to 230 volts. Size: 2.5  $\times$  8.5  $\times$  10.0in. Weight: 7lb with battery pack (optional). Fluke International Corporation, Garnett Close, Watford WD2 4TT.

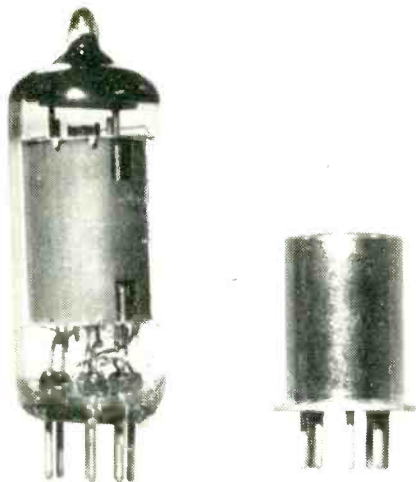
**WW314 for further details**

## Semiconductor valve

Tens of millions of valves are still in use outside the consumer industry. In radar and communications, broadcasting and instrumentation, regular replacement of these valves is essential due to their limited life and characteristic degradation during service. Now a solid state valve replacement, called the Fetron, has been introduced which, in many applications, can be plugged directly into the valve socket without the need for major circuit modification.

GDS Sales, who are stocking the first Fetrons to be marketed in the U.K., say that the advantages of the new device include extremely long life (estimated by Teledyne Semiconductor, the manufacturers, at over 1,000,000 hours), no microphony, zero warm-up time, reduced heat dissipation due to the absence of the valve's heater, no degradation of transconductance, and built-in internal shielding.

First Fetrons to be available are the TS12AT7 and TS6AK5. These are intended to replace the 12AT7 and 6AK5 respectively in most amplifier circuits. The TS12AT7 consists of two high-voltage f.e.t.s and the TS6AK5 a cascode



connected f.e.t. pair. Amongst the valves which it is claimed can be replaced by the TS6AK5 are the EF90, EF95, and EF95F.

At this stage, GDS say that the pentode Fetron should not be considered a plug-in replacement for the valve in oscillator circuits because of the absence of a screen grid. For specific oscillator service, the screen can be simulated by the inclusion of a RC network in the package, but such devices are not yet standard products.

Fetrons are extremely rugged. The case of the current devices is a deep-drawn steel cap welded to a large header. Before welding, the case is evacuated and back-filled with dry nitrogen.

Both the TS12AT7 and TS6AK5 are available from GDS stocks and cost, in quantities of 100 and above, £5.25 and £4.75 respectively. GDS (Sales) Ltd., Michaelmas House, Salt Hill, Bath Road, Slough, Bucks.

**WW 306 for further details**

### Corrosion inhibitor

'Vapor-Strip', which prevents the formation of rust, salt corrosion, mildew and mould, is now available overseas through the manufacturer's (Northern Instruments) exclusive export distributor, Singer Products Company Inc., New York.

'Vapor-Strip' looks and feels like a piece of grey sponge rubber with an easily removable adhesive backing. When this backing is removed and the strip is applied to a clean surface, chemicals are released, which prevent corrosion, reduce acid damage and prevent gum and varnish formation while helping to remove old deposits. One small Vapor-Strip will protect 2500 cubic inches (41000 cc) for over two years of normal use. It has no deleterious effect on commonly used plastics, rubbers, paints and adhesives, while preventing fungus growth.

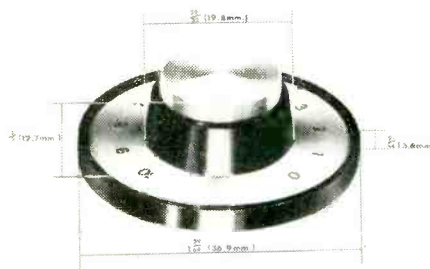
Leather, cloth, engine gaskets and similar materials were incubated under extreme fungus-producing conditions for 16 weeks at 70°F (21°C). With 'Vapor-Strip' protection, there was no

evidence of any damage; untreated samples were almost covered with mould and mildew and frequently rotted away. The product is practically odourless. Normal packaging consists of two  $\frac{3}{8} \times 2\frac{1}{2}$ in 'Vapor-Strips' in a blister type card, with suggested uses and complete directions. Custom sized strips, for special applications, are available to order. Singer Products Company Inc., One World Trade Centre, Suite 2365, New York, N.Y.10048, U.S.A.

**WW322 for further details**

### Knob assembly

A new knob, dial and escutcheon assembly with an alternative plain or customer designed legend dial has been introduced by Bulgin. Designed for push fitting to  $\frac{1}{16}$ in flattened shafts, the knob and



escutcheon are polished black with smooth sides. The decor cap and dial are spin finished alloy. A. F. Bulgin & Co. Ltd., Bye-Pass Road, Barking, Essex.

**WW326 for further details**

### V.H.F. signal generators

Low-noise, broad-frequency coverage and precision modulation are claimed as the foremost attributes of two new a.m./f.m. signal generators from Hewlett-Packard. Covering 450kHz to 550MHz with calibrated modulation and +19 to -145dBm output levels, they can perform complete r.f. and i.f. tests on virtually any kind of v.h.f. receiver.

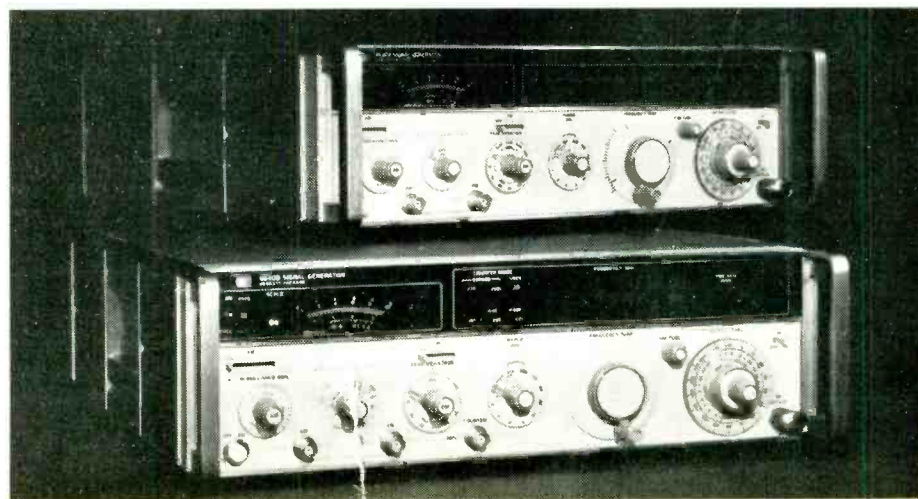
Both units deliver low-noise signals with a wideband signal/noise ratio better than

140dB/Hz and non-harmonic and sub-harmonic outputs that are down more than 100dB. Close-in noise, critical in mobile radio adjacent-channel selectivity tests, is specified at -130dB/Hz at 20kHz offset.

One version of the new signal generator, model 8640A, has a slide-rule tuning dial with 0.5% frequency accuracy and drift of less than 10 p.p.m. per 10 minutes. The other, model 8640B, has a six-digit i.e.d. display (useful separately as a 550MHz frequency counter) and a built-in phase-lock synchronizer to achieve output stability of better than  $5 \times 10^{-8}$  per hour; i.e. synthesizer stability.

Even when the 8640B is locked, the spectral purity and same precision f.m. of the unlocked mode is preserved. This permits meaningful tests on narrowband and crystal-controlled receivers. Provision is also made for locking to an externally applied 5MHz standard for even higher stability, or for locking two 8640Bs together for various two-tone tests. In the unlocked mode, the built-in counter can display the generator's frequency to a resolution of 100Hz at 500MHz and 0.1Hz at 500kHz. The counter can also measure external signals between 20Hz and 550MHz, eliminating the need for separate frequency measuring equipment in many test applications.

Except for the counter and lock features, the overall performance of the 8640A and 8640B signal generators is identical. Power output is calibrated from +19 to -145dBm (2V to .013V) and levelled to  $\pm 0.5$ dB. The maximum output of +19dBm permits high level tests on receiver i.f. strips, amplifiers, and mixers without additional power amplification. Accurate low level measurements down to -145dBm have been assured through r.f.i. shielding and use of an accurately calibrated step attenuator. The output level is displayed on both a direct reading dial and a built-in meter that autoranges for high resolution. Other facilities available are modulation of the c.w. with independent a.m. and f.m. sources that are metered and calibrated for all r.f. output frequencies and levels. The a.m. is adjustable from 0 to 100% with the bandwidth, accuracy and low incidental f.m. required for the most stringent a.m. measurement applications. Distortion is





1% at the 50% modulation setting and 3% at 70% a.m. Provision is also made for external pulse modulation with pulse widths down to 1 sec.

The f.m. mode provides calibrated and metered deviation that remains constant with frequency or band changes. Peak deviations to at least 0.5% of carrier frequency are available. Important for accurate narrowband f.m. measurements, there is negligible frequency shift from the c.w. to f.m. mode and no degradation in spectral purity. With the 8640B in the phase-locked mode, full f.m. capability is preserved at modulating rates from 50Hz to 250kHz, producing accurate f.m. with the carrier stability of a crystal oscillator. The standard internal modulating tones are 400 and 1000Hz for both a.m. and f.m. Hewlett-Packard Ltd., 224 Bath Road, Slough, Bucks. SL1 4DS.

**WW325 for further details**



### Ultrasonic air transducers

Two piezo-electric ultrasonic transducers made by H. D. A. MacDonald and designated type UT40T and UT40R, are designed for 40-kHz transmitting and receiving applications, respectively. Obtainable as matched pairs, with the matching achieved to within 100Hz, the specifications quoted are:

#### UT40T

Sensitivity (0dB = 1 $\mu$ bar/V/m) > 3dB  
 Frequency 40  $\pm$  0.9kHz  
 Impedance 200 $\Omega$   
 Capacitance 1400  $\pm$  20%pF  
 Selectivity 70  
 Max. applied voltage 7V  
 Temperature range -15 to +65°C

#### UT40R

Sensitivity (0dB = 1V/ $\mu$ bar) > -64dB  
 Frequency 40  $\pm$  0.9kHz  
 Impedance 70k $\Omega$   
 Capacitance 1400  $\pm$  20%pF  
 Selectivity 60  
 Temperature range -15 to +65°C

Priced at £3.95 for a single pair, discounts are offered for quantity orders. H. D. A. MacDonald, 100 Clarendon Road, Ashford Middlesex TW15 2QD.

**WW301 for further details**

### V.H.F./U.H.F. amplifier

Microwave International (U.K.) Ltd, have announced a range of solid-state broad-band power amplifiers, covering 225-400MHz, which have been developed for use in transceivers. One, the Model WA2240, finds application as a power amplifier for sweepers and many test set-up applications. These units have been used successfully as drivers for the testing of high-power r.f. circuitry in network analyzer systems.

The modules are designed with 50 $\Omega$  to 50 $\Omega$  input/output impedance, and are factory aligned. The Model WA2240 is available in power output ranges from 5 to 100 watts and may be ordered with signal

gain from 10 to 50dB. It is also available with electronic output protection against poor and varying load v.s.w.r.s. Specifications for the Model WA2240 wide-band amplifier are:

Frequency	225-400MHz
Instantaneous bandwidth	175MHz
Power output	5W at 1A 20W at 2A 60W at 6A 100W at 12A
Power input	1 or 10mW
Second harmonic	-30dB minimum
Input v.s.w.r.	2:1 max. 1.5:1 typical
Load v.s.w.r.	2:1 maximum
Spurious output	-50dB minimum
Supply voltage	+28V d.c.

Microwave International (U.K.) Ltd, 33-37 Cowleaze Road, Kingston upon Thames, Surrey.

**WW329 for further details**

### V.H.F.-A.M. radiotelephone

Dymar Electronics have introduced a rugged, weatherproof amplitude-modulated v.h.f. personal portable radiotelephone (type 980) for general purpose short-range land communications. Single- or two-frequency simplex service is provided with three channels spaced within a bandwidth of 1.0MHz. Channel spacing is either 12.5 or 25kHz and the frequency range is 68 to 174MHz.

Transmitter characteristics include: r.f. power output, 500mW into 50 ohms; up to 100% modulation; modulation response, with +1dB and -3dB relative to 1kHz between 300Hz and 2.5kHz; and modulation distortion, less than 10% at 1kHz and 5% modulation (typically 5%). Receiver characteristics include:

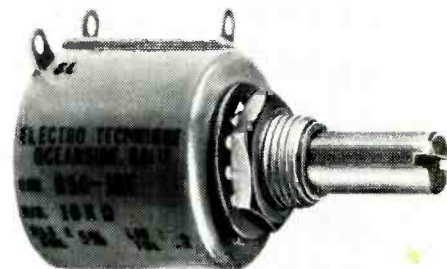
sensitivity, 1.6 $\mu$ V e.m.f.; selectivity, not less than 70dB adjacent channel rejection; spurious responses, attenuated at least 60dB relative to wanted signal; a.g.c., less than 10dB increase in a.f. output for an increase in signal from 1.6 $\mu$ V to 100mV e.m.f.; a.f. output, 100mW. A choice of aerials is available — helical, whip or trailing wire.

Depending on the battery used, the type 980 weighs between 0.6kg and 0.75kg (approximately 1lb 5oz and 1lb 10oz). Dimensions are 208  $\times$  84  $\times$  39mm (approximately 8  $\times$  3 $\frac{1}{4}$   $\times$  1 $\frac{1}{2}$ in). Dymar Electronics Ltd, Colonial Way, Radlett Road, Watford, Herts.

**WW316 for further details**

### 10-turn potentiometer

A miniature precision 10-turn potentiometer, only  $\frac{3}{8}$ in long, and  $\frac{7}{8}$ in diameter, is now available from Kynmore Engineering Co. Ltd. The new model is known as the ET-850. The case is made of high-temperature moulded plastic and the internal slip-rings and the external solder terminals are of heat-treated beryllium copper with gold plating.



Standard linearity is 0.25% and temperature stability 70 p.p.m./°C. Standard resistance values are: 100, 200, 500, 1000, 2000, 5000, 10k, 20k, 50k and 100k ohms. End resistance is 0.25% or 1 ohm, whichever is the larger. Kynmore Engineering Co. Ltd., 19 Buckingham Street, London WC2N 6EQ.

**WW 303 for further details**

### H.V. Darlington hybrid

A new high-gain, high-voltage, dual Darlington hybrid circuit has been announced by RCA Solid State-Europe. The HC3100 contains two Darlington circuits, both of which are electrically isolated from the package so that the unit can be mounted directly on a chassis. It incorporates protective diodes for the logic drive circuit, diodes for commutating inductive loads and operates from power supplies up to 120V. The HC3100 can be used in regulators as well as such applications as hammer, solenoid, and stepper motor drivers. The case is an 8-pin variant of the TO-3 hermetic package. RCA Ltd., Sunbury-on-Thames, Middx.

**WW320 for further details**

# About People

**Dr. Frank E. Jones, M.B.E., F.R.S.**, managing director of Mullard Ltd. has retired but joined the board of Philips Industries Ltd on January 1st. Dr. Jones, who is 58, joined the Mullard board in 1956 as technical director and was appointed managing director in 1962. He graduated at King's College, London, and entered the scientific civil service in 1940 and was at one time head of experimental physics research at the Telecommunications Research Establishment of which he later became deputy chief scientific officer. He left T.R.E. in 1952 to become deputy director of the Royal Aircraft Establishment, Farnborough. In 1967 he was elected a Fellow of the Royal Society for his work on radar and infra-red technology and "his outstanding technological leadership in an advanced industry". Dr. Jones is succeeded as managing director of Mullard by **Jack C. Akerman** who has been with Mullard since 1936. In 1967 he was appointed a director of Associated Semiconductor Manufacturers Ltd., an associated company of Mullard Ltd. He took over as head of Mullard's Consumer Electronics Division in 1969. He has been commercial director and a member of the Mullard board since 1970.

**Peter Rainger, B.Sc., F.I.E.E.**, head of the Research Department of the B.B.C., has received the David Sarnoff Gold Medal Award for 1972 from the Society of Motion Picture and Television Engineers. He was given the award "for his pioneering development of all-electronic television standards conversion techniques together with numerous other important contributions to television technology". Mr. Rainger, a graduate of London University, was head of the B.B.C. Designs Department from 1968 to 1971, and since November 1971 has been head of the B.B.C. Research Department.

**Dr. William Shockley** who with Drs. W. H. Brattain and J. Bardeen received the 1956 Nobel Prize in Physics for the invention of the junction transistor, is to visit

the U.K. in February to deliver a lecture at the Institution of Electrical Engineers. Dr. Shockley's lecture on 14th February will be the highlight of a week of celebrations to commemorate the 25th anniversary of the discovery of the transistor. Dr. Shockley, who was born in London in 1910, joined Bell Telephone Laboratories in 1936 where he was director of transistor physics when he left in 1956. He was with Beckman Instruments for a few years before occupying the chair of engineering sciences in the Department of Electrical Engineering at Stamford University. He rejoined Bell Labs in 1965.

Among the recent recipients of Royal Society Medals are **Sir Nevill Mott, F.R.S.**, emeritus professor of physics in the University of Cambridge and senior research fellow, Imperial College of Science and Technology, London, who receives the Copley Medal "for his original contributions over a long period to atomic and solid state physics". The Hughes Medal has been awarded to **Dr. B. D. Josephson, F.R.S.**, reader in physics, University of Cambridge, "for his discovery of the remarkable properties of junctions between superconducting materials." Readers may recall that Dr. Josephson, wrote on superconducting devices in our October 1966 issue. Except for a short time spent in the Physics Dept. of the University of Illinois as research assistant professor, Dr. Josephson has been at Trinity College, Cambridge, since 1957. He graduated in 1960.

**David Hawkins, 33**, has been appointed sales manager of Blueline Electronic Components. Previously he was an account executive with ITT Components Group, having joined ITT from Telcon Magnetic Cores Ltd in 1970.

**David Griffin, M.I.E.R.E.**, marketing manager of Motorola Semiconductors Ltd, has been appointed director of product

promotion and planning. Europe. He moves to Geneva in January. Mr. Griffin, who is 38, was with Texas Instruments, Bedford, from 1957-62 and with Celdis immediately prior to joining Motorola in 1964. He is succeeded as marketing manager, U.K., by **Mike Ward**, who is 36 and has been with Motorola for the past six years.

**John Bishop, M.I.E.R.E.**, has joined GEC-Elliott Process Automation Ltd as manager of its Telemetry and Supervisory Systems Division at Leicester. Mr. Bishop graduated from the University College of Southampton where he studied electronics. In the mid fifties he spent three years with GEC in Coventry and for the past ten years has been sales manager with Serck Controls Ltd.

**Geoff Gamble**, who joined Brookdeal nearly four years ago and earlier this year was promoted to chief applications engineer, has become marketing manager. Prior to joining Brookdeal, Mr. Gamble was for three years an engineer in the Radio Systems Division of Plessey.

**David Letheren, B.Sc.**, a graduate of University College, London, has joined the m.o.s. applications team at Emihus Microcomponents Ltd, at Weybridge, Surrey. Mr. Letheren, who is 32, joins Emihus from Bell Punch Company, where he was an m.o.s. design engineer. Previously, he was with Decca Radar Ltd, working at the Hershram research laboratory on analogue and digital radar systems.

Orbit Controls Ltd, of Cheltenham, have appointed **Michael E. Cosens** to the new post of field sales manager. He joined Orbit from The Plessey Company where he was European sales manager of the Memories Division. Previously Mr. Cosens, who is 36, was general sales manager of Fabritek Inc., responsible, from London, for world marketing and sales outside the U.S.A.

**Tom Ivall, M.I.E.R.E.**, technical editor of *Wireless World* since 1965, will become editor on the retirement of **Harold Barnard** in April.

**Geoff Hammond, B.Sc.**, recently became applications engineer with Brookdeal Electronics Ltd, the signal recovery instrumentation manufacturers of Bracknell. His post carries the responsibilities of providing a technical back-up service for the sales engineers, dealing with customers' technical and experimental enquiries and the writing of application notes. Immediately prior to his appointment Mr Hammond was a

research student at the City of London Polytechnic preparatory to writing a thesis for his Ph.D.

**Ian Clinksales**, who has joined GDS Sales Ltd as sales manager, has over thirteen years' experience in the semiconductor industry, both in the United Kingdom and Scandinavia. He was latterly with Motorola Semiconductors Ltd where he held the position of industrial sales manager. From 1962 to 1971 he was with SGS-Fairchild, having previously been with Texas Instruments.

**Alan Smith** has been appointed sales manager of Best Electronics (Slough) Ltd, the recently launched subsidiary of GDS Sales Ltd. He has been with GDS since 1969.

**Tom E. Zombory-Moldovan, M.Sc., F.I.E.E.**, has become technical director of GEC-Elliott Industrial Controls Ltd. Mr Zombory-Moldovan, a British citizen aged 45, was educated in Hungary and served an engineering apprenticeship with Standard Telephone Company in Budapest. After leaving Hungary in 1956 he joined the staff of Manchester University and was awarded his M.Sc. degree in 1960. This was followed by five years as head of advanced electronics in the Power Protection and Meter Department of Associated Electrical Industries Ltd (now part of the GEC organization). Immediately prior to his new appointment Mr Zombory-Moldovan was technical manager of the Plessey Numerical Control Co. Ltd.

On the retirement of **R. A. H. Penney**, the Marconi International Marine Co. has appointed **K. Pope** as London manager (sales). Mr Penney was a seagoing radio officer from 1927, when he joined the company, until 1945 when he was transferred to the shore technical staff. His shore appointments include contracts representative based on Newcastle, manager, northern area (contracts division), and London sales manager since 1968. Mr Pope, the new London manager (sales), joined the seagoing staff of Marconi Marine as a radio officer at the end of the war. Since 1962 he has been joint manager of the London Office.

Marconi International Marine Co. have also announced the appointment of **David Bowker** as its representative in North America. He succeeds **John Older** who has returned to the United Kingdom. Mr Bowker began his career with Marconi Marine as a seagoing radio officer in 1960. He served at sea until 1964 when he transferred to the company's shore staff as a technical sales assistant in the export sales division. He served from 1969 to 1971 as the company's U.S.A. representative and has recently been marine director of the Norsk Marconikompani.



# January Meetings

*Tickets are required for some meetings: readers are advised therefore, to communicate with the society concerned*

## LONDON

3rd. I.Phys. — One-day meeting on "On-line computers for laboratory experiments" at 9.45 at Imperial College, SW7.

4th. IEE — Kelvin lecture "Conduction in amorphous materials — theory and applications" by Prof. Sir Nevill Mott at 17.30 at Savoy Pl., WC2.

9th AES — "Monitoring in multi-track recording" by R. W. Swettenham at 19.15 at the IEE, Savoy Pl., WC2.

10th. IEE/IERE — Colloquium on "Microcomputers and electronic calculating aids" at 14.30 at the IERE, 9 Bedford Sq., WC1.

10th. IEE — Discussion on "Active antennas and steerable arrays for communications" at 17.30 at Savoy Pl., WC2.

15th. IEE — "Cold cathode electron emission" by R. Brander at 17.30 at Savoy Pl., WC2.

17th. R. I. Navigation — "Situation display: marine radar" by P. O. Prior at 17.00 at Royal Inst. of Naval Architects, 10 Upper Belgrave St., SW1.

17th. IEE — "Traffic control and surveillance on motorways" by K. W. Huddart and J. T. Duff at 17.30 at Savoy Pl., WC2.

17th. IEE — "Solid-state displays devices" by Dr. C. Hilsom at 17.30 at Savoy Pl., WC2.

18th. IEE — "The relationship between research, development and marketing" by I. Barron at 17.30 at Savoy Pl., WC2.

18th. RTS — Panel discussion on "Why digital?" at 19.00 at I.B.A., 70 Brompton Rd., SW3.

23rd. SERT — "The introduction of flight data recording systems" at 19.00 at the IBA Conference Room, 70 Brompton Rd., SW3.

24th. R. I. Navigation — Discussion on "The use of Omega for air and sea navigation" at 15.00 at Royal Aeronautical Soc., 4 Hamilton Pl., W1.

24th. IERE — "Media: A continuous digital process control system" by J. R. Halsall and I. J. Kirby at 18.00 at the IERE, 9 Bedford Sq., WC1.

25th. IEE — Colloquium on "The properties of evaporated semiconductor films" at 10.00 at Savoy Pl., WC2.

30th. IERE — Colloquium on "Fixed and variable resistors" at 10.00 at Harkness Hall, Birkbeck College, Malet St., WC1.

## AYLESBURY

11th. IEE/RAeS — "The Skynet satellite communication system" by Air Commodore F. C. Padfield at 19.30 at Kermode Hall, R.A.F., Halton.

## BATH

17th. IERE — "Medical electronics" by K. Riley at 19.00 at Bath University, Room 2E.3.1.

## BELFAST

16th. IERE — "Practical aspects of air traffic control" by W. J. Eames at 19.00 at Cregagh Technical College, Montgomery Rd.

## BIRMINGHAM

8th. IEE — "50 years of B.B.C. engineering" by J. Redmond at 18.00 at the MEB Offices, Summer Lane.

10th. RTS — "The development of u.h.f. television" by L. G. Dive at 19.00 at B.B.C. Broadcasting Centre, Pebble Mill Rd.

24th. IERE — "Some recent developments in

v.h.f. mobile radio by J. D. Parsons at 19.15 at City of Birmingham Polytechnic, North Centre, Franchise St., Perry Bar.

## BRADFORD

11th. IERE — "The 8500 colour television receiver concept" by A. Martinez at 19.00 at the Technical College.

## BRIGHTON

30th. IEE Grads. — "The engineer in Parliament" by A. Palmer at 19.30 the University of Sussex, Falmer.

## CAMBRIDGE

11th. IEE — "Electronic aids to night vision" by Dr. P. Schagen at 18.30 at the University Engineering Department, Trumpington Street.

25th. IERE/IEE — "Vocoder techniques" at 18.30 at the University Engineering Laboratories, Trumpington St.

25th. IEE/IERE — "Future advances in h.f. communications systems" by M. H. Gross at 18.30 at The University Engineering Laboratories, Trumpington St.

## CARDIFF

10th. IERE — "Man-computer interface for process control" by K. E. Morgan at 18.30 at U.W.I.S.T.

## CHATHAM

31st. IERE — "High-fidelity sound reproduction" by R. West at 19.00 at the Medway College of Technology.

## CHELMSFORD

17th. IEE/IERE — "Beam indexing colour television systems" by Dr. J. A. Turner at 18.30 at King Edward VI Grammar School, Broomfield Rd.

## GUILDFORD

24th. IERE — "Review of solid-state microwave devices" by J. G. Summers at 18.30 at University of Surrey.

## KINGSTON UPON THAMES

16th. IEE Grads. — "Making electronic music" by G. Rodgers at 18.30 at Kingston Polytechnic, Penrhyn Rd.

## LEICESTER

17th. IERE — "Application of integrated circuits" by A. Potton at 18.45 at the Lecture Theatre "A", Physics Block, Leicester University.

## LETCWORTH

16th. IEE — "The Open University and technological education" by Dr. D. I. Crecroft at 19.45 at the College of Technology.

## LIVERPOOL

22nd. IEE — "Computer-aided design of integrated circuits" by A. Cranswick at 18.30 at the Lecture Theatre, Dept. of Electrical Engineering, University of Liverpool.

## MALVERN

8th. IEE — "Tomorrow's world in telecommunications" by W. J. Bray at 19.30 at the Abbey Hotel.

17th. IERE — "Electronics education and the Open University" by J. A. Myers at 19.30 at Abbey Hotel.

## MANCHESTER

18th. IERE — "Electronic control of small a.c. motors" by P. Bowler at 18.15 at Renold Building, UMIST.

22nd. IEE — Faraday lecture "Navigating — land, sea, air and space" by A. Stratton at 19.30 at the Free Trade Hall.

23rd. IEE — Faraday lecture "Navigating — land, sea, air and space" by A. Stratton at 14.30 and 18.30 at the Free Trade Hall.

## NEWCASTLE-UPON-TYNE

10th. IERE — "Recent developments in nucleonics and scanning systems as applied to medicine" by J. W. Haggith at 18.00 at Ellison Building, the University.

## NEWPORT, Mon.

17th. IEETE — "Electronics in the modern car" by C. S. Rayner at 19.30 at Newport & Monmouthshire College of Technology, Allt-yr-yn Avenue.

## PORTSMOUTH

30th. IEE Grads — "Angels, birds and radar" by Dr. E. Eastwood at 19.00 at Portsmouth Polytechnic.

## READING

18th. IERE — "Visual telecommunications systems — a review of some technical problems" by I. Macdiarmid at 19.30 at the J. J. Thomson Laboratory, University of Reading, Whiteknights Park.

## SOUTHAMPTON

17th. IEETE — "Hi-Fi" by R. West at 19.30 at the Polygon Hotel, Cumberland Pl.

31st. IERE — Colloquium on "Electrons in cars" at 16.00 at the University.

## STAFFORD

23rd. IEE — "Military applications of electronics" by D. Cawsey and T. K. Garland-Collins at 19.00 at N. Staffs Polytechnic, Beaconside.

## Sunderland

18th. IEETE — "Computers — techniques and applications" by R. A. Selby, B. Meech and M. Todd at 19.30 at Priestman Building, Sunderland Polytechnic, New Durham Rd.

## TAUNTON

17th. IEE — "Micro-electronic logic circuits" by Dr. A. T. Johns at 19.45 at the County Hotel.

## WORTHING

16th. IEE — "Electronic performance testing of motor vehicles" by C. D. Freeman at 18.30 at Worthing College of Further Education.

# Literature Received

*For further information on any item include the WW number on the reader reply card*

## ACTIVE DEVICES

A new range of Passivated, Assembled, Circuit Elements (PACE-packs) manufactured by International Rectifier, Hurst Green, Oxted, Surrey, is described in leaflet E2716. The modules described, utilize passivated diode and thyristor junctions in various configurations to form isolated power controllers rated for 250V r.m.s. at 25 and 42.5 amperes .....WW401

A 12-page technical booklet describing a complete range of encapsulated, thick film, voltage regulators and over-protection units is available from Coutant Electronics Ltd, 3 Trafford Road, Richfield Estate, Reading, Berks .....WW402

Data sheets on the Q400A and Q400B series of photo-conductive cells having spectral responses of 570nm and 690nm, respectively, are:

Sheet 3290 (Q400A) .....WW403  
Sheet 3291 (Q400B) .....WW404

Joseph Lucas (Electrical) Ltd, Electronic Products Group, Mere Green Road, Sutton Coldfield, Warwickshire.

"Thyristors and Diode Stacks" is the subject of a 28-page brochure which provides information on aluminium fabricated cooling-fins and semiconductors covering the range 10-700 amperes. AEI Semiconductors Ltd, Carholme Road, Lincoln LN1 1SG .....WW405

Modular, universal active filter elements is the subject of a brochure containing nomographs and filter response curves for the design of bandpass, highpass and lowpass responses, maximally-flat and elliptical function forms. Kinetic Technology Inc., 3393 De La Cruz Boulevard, Santa Clara, California 95050 .....WW406

A catalogue of electronic components entitled "Sensors" providing electrical data on optoelectronic devices and temperature and magnetically sensitive resistors has been received from Siemens Ltd, Great West House, Great West Road, Brentford, Middlesex, TW8 9DG .....WW407

"Buyers Guide to Integrated Circuits" lists the type numbers and nearest equivalents of m.o.s., linear and digital integrated circuits from Texas Instruments, Signetics, General Instrument Microelectronics and Plessey stocked by S.D.S. Components Ltd, Gunstore Road, Hilsa Trading Estate, Portsmouth, Hants. PO3 5JW .....WW408

## PASSIVE DEVICES

Data about Elcor Isoformers, which are isolation transformers intended for use in low-noise and medical electronics where maximum interference and leakage protection is required, is available from Aveley Electronics Ltd, Roebuck Road, Chessington, Surrey KT9 1LP .....WW409

Five technical bulletins describing models TP-101, 102, 103, 104 and 105 wide band (0.5-1500MHz), fast rise-time (0.18ns), low-loss (0.4dB) r.f./pulse transformers in flat-pack form, were received from

Anzac Electronics, 39 Green Street, Waltham, Massachusetts 02154 .....WW410

A leaflet contains a full specification and description of a new type of miniature, p.t.f.e. covered, probe and socket from Sealectro Ltd, Walton Road, Farlington, Portsmouth, Hants. PO6 1TB .....WW411

A short-form catalogue describing precision coaxial and waveguide components covering the range d.c. to 18GHz manufactured by Maury Microwave Corporation was sent to us by Tony Chapman Electronics Ltd., 3 Cecil Court, London Road, Enfield, Middlesex .....WW412

New miniature servo-controlled a.c. voltage stabilizers for laboratory or industrial application providing distortionless control at power ratings between 180VA and 720VA, are described in a leaflet from Claud Lyons Ltd, Valley Works, Hoddesdon, Herts .....WW413

Data on types "VK", ceramic capacitors (1pF to 1 F), "VY", porcelain capacitors (0.24pF to 10nF), "Vee Jem", chip capacitors (1pF to 470nF) and a new low-cost Phenolic dipped range, is available in a condensed catalogue from Vitramon Europe, Wooburn Green, Bucks .....WW414

Type 3W1, precision decade capacitor having direct in-line readout over the range 0.001 to 1.099 F, with an accuracy of  $\pm 0.5\%$  in 0.001 F steps, is the subject of engineering bulletin 90,606 from Sprague Electric Company, North Adams, Massachusetts 01247 .....WW415

## APPLICATION NOTES

Two application notes received concerning power transistors discuss:

The basic performance characteristics and specific circuit design detail related to the application of transistors 2N6104/2N6105 in broadband u.h.f. power amplifiers. AN6010 .....WW416

A testing programme used to determine the capability of the 2N3055 power transistor design to withstand thermal cycling over a wide range of operating conditions. AN4783 .....WW417

RCA/Solid State Europe, Sunbury-on-Thames, Middlesex.

An application report on Motorola's new emitter-coupled logic family, MECL 10,000 series, which features non-saturated switching functions for very high-speed operation with load driving capability, has been produced by GDS (Sales) Ltd., Michaelmas House, Salt Hill, Bath Road, Slough, Bucks .....WW418

"1N821 and B2X90 series of high-stability reference diodes" is the title of application note TP1339 which compares the performance of standard-cell reference sources against that of semiconductor diodes. Formulae are given for the calculation of stabilization factor and curves show the performance of a number of circuits described. Instrument and Control Electronics Division, Mullard Ltd., Mullard House, Torrington Place, London WC1E 7HD .....WW419

## EQUIPMENT

A remotely controlled, digitally tuned, microwave-receiving system (model 3600) covering 0.5 to 18GHz and developed by American Electronics Laboratories Inc., is described in a brochure from C.T. (London) Electronics Ltd., Sutherland House, Sutherland Road, Walthamstow, London E17 6BU .....WW420

A brochure summarizing, the characteristics of autobalanced component measuring bridges with diagrams explaining the principles for both manual and automatic operation, was received. It provides brief specifications of the five different types of bridge manufactured by Wayne Kerr Company Ltd, Durban Road, Bognor Regis, Sussex PO22 9RL .....WW421

A loose-leaf binder received, contains numerous information sheets dealing with "Data and Telegraph Equipment". It covers signal test equipment, message generators, code converters/regenerators, receiver/demodulators, tonekeyers and selectors, tape readers and message storage equipment. Plessey Company Ltd, Sopers Lane, Poole, Dorset BH17 7ER .....WW422

Leaflets describing trip amplifiers, with input sensitivities ranging from 10mV to 300V and 10 A to 1A intended for industrial control systems also, low-cost miniature power supplies with output voltages in the range 4V to 24V d.c. are:

ICD2 (amplifiers) .....WW423  
PS8 (power supplies) .....WW424

Farnell Instruments Ltd., Sandbeck Way, Wetherby, Yorks LS22 4DH.

## COMMUNICATIONS

A booklet, containing technical descriptions and specifications of the various v.h.f. and u.h.f. transmitter-receivers available for mobile radiotelephone service, is entitled "Over 70 years of mobile radio" and is available from Marconi Communications Systems Ltd, Marrable House, Great Baddow, Chelmsford, CM2 7QW .....WW425

Information sheets about the various aspects of business radio including features such as telephone answering and personal paging services, are available in a wallet form from Air Call Ltd, 176/184 Vauxhall Bridge Road, London S.W.1 .....WW426

## GENERAL INFORMATION

A complete list of production tools to metric standards (mm) suitable for the manufacture of solder washers, discs and rings, has been received from Enthoven Solders Ltd, Dominion Buildings, South Place, London EC2M 2RE .....WW427

Automation system architecture and its involvement in the electronics/automation industry is the subject of a booklet from Warren Point Ltd., Prospect Place, Welwyn, Herts. ....WW428

Tefzel insulated wire, said to have excellent mechanical and high temperature properties combined with high chemical resistance and light weight, is specified in a data sheet from Permoid Ltd., Manchester M4 7JX .....WW429

A catalogue dealing with all the necessary component parts needed by the enthusiast for a build-it-yourself electronic organ, was received from Elvins Electronic Musical Instruments, 8 Putney Bridge Road, London S.W.18 .....WW430

The 500-page 1973 catalogue and price list including diodes, thyristors, transistors, i.c.s, resistors, relays, switches, potentiometers, r.f. connectors and accessories, is available from G.D.S. (Sales) Ltd., Michaelmas House, Salt Hill, Bath Road, Slough Bucks .....WW 431

Nearly 8000 components and accessories are listed in a 240-page catalogue and price list from Home Radio (Components) Ltd, 234-240 London Road, Mitcham, Surrey CR4 3HD. Price 50p plus 20p postage.



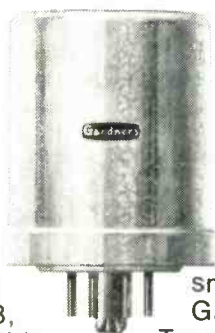
# Gardners line up

## Line Matching Transformers from Standard to Super Fidelity

It's easy to choose the right Line Matching Transformer from the five Gardners ranges.

The Super Fidelity Series, with a frequency response of 10Hz to 80kHz - 0.5dB, gives the widest possible bandwidth for high accuracy instrumentation and recording applications.

Then there's the Wide and Extra Wide-band ranges. Outstanding performers with a frequency range 30Hz - 20kHz or more - for the 0.5dB points. Used a lot by broadcasting and recording companies throughout the world.



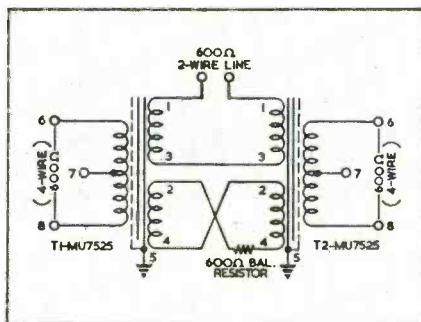
The Miniature and Standard ranges provide excellent bandwidth for most purposes, 30Hz - 22kHz for the 1.0dB points.

Except for the very smallest in the range, all Gardners Line Matching Transformers are fully magneti-

cally shielded, giving very high hum rejection ratios.

Prices start from £2.61 (recommended retail price) and all types are usually available from stock.

Complete technical information is given in brochure GT.5 'Audio Frequency Transformers' which we'll be glad to send on request.



*So accurate is the balancing of the windings on some of these transformers that, when used as pairs in a hybrid circuit (as illustrated) we can guarantee a rejection of better than -55dB over the frequency range 50Hz to 10kHz and normal rejection of up to -75dB may be expected.*



Specialists in Electronic Transformers

# GARDNERS

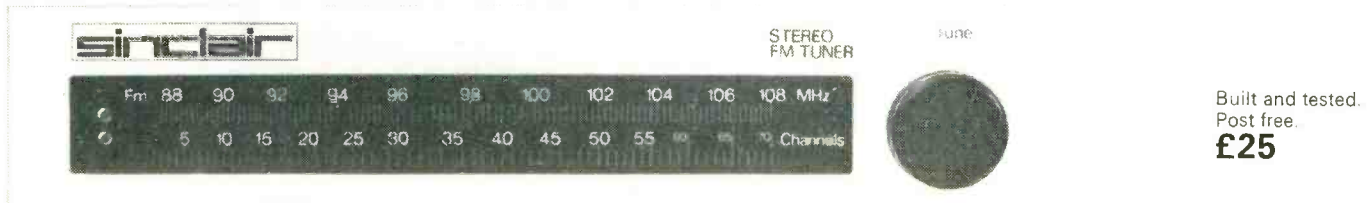
TRANSFORMERS LIMITED

Gardners Transformers Limited, Christchurch, Hampshire, BH23 3PN  
Tel: Christchurch 2284 (STD 0201 5 2284) Telex: 41276 GARDNERS XCH.

WW-083 FOR FURTHER DETAILS

# Sinclair Project 60

## Project 60 Stereo FM Tuner



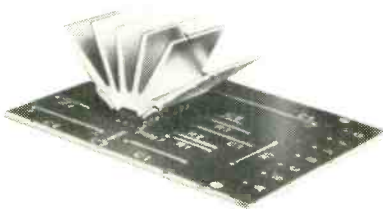
### with phase lock-loop principle

Amongst the many advanced electronic features to be found in this remarkable stereo tuner, use of the phase lock loop principle ensures standards of audio quality better than from any other method of detection yet used. Varicap diode tuning, accurately formed printed circuit coils, an I.C. in the special stereo decoder section and switchable squelch circuit for silent tuning between stations contribute to the unsurpassed performance of this tuner, irrespective of price consideration. But the Project 60 FM Stereo Tuner is far from expensive – indeed, it offers fantastic value for money and will bring the thrill of stereo radio to many who previously may not have been able to afford it. The tuner may be used with any good system as well as Project 60, but if you use it with other Project 60 modules, you will find the matching front panels particularly impressive in appearance as well as function.

#### SPECIFICATIONS

**Number of transistors:** 16 plus 20 in I.C.  
**Tuning range:** 87.5 to 108MHz.  
**Sensitivity:** 7µV for lock-in over full deviation.  
**Squelch level:** typically 20µV.  
**Signal to noise ratio:** ±65dB.  
**Audio frequency response:** 10Hz–15KHz (±1dB).  
**Total harmonic distortion:** 0.15% for 30% modulation.  
**Stereo decoder operating level:** 2µV.  
**Cross talk:** 40dB.  
**Output voltage:** 2 × 150mV R.M.S. max. (typically 2 × 50mV stereo).  
**Operating voltage:** 25–30V DC at 100mA  
**Indicators:** Stereo on; tuning.  
**Size:** 93 × 40 × 207mm.

### Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-fi constructors with the IC.10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC.12, a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up, F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC. make possible. It is the equivalent of a 22 tran-

sistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

#### SPECIFICATIONS

**Output power:** 6 watts RMS continuous (12 watts peak). 6–8Ω. **Frequency Response:** 5Hz to 100KHz ±1dB. **Total Harmonic Distortion:** Less than 1%. (Typical 0.1%) at all output powers and frequencies in the audio band (28V). **Load Impedance:** 3 to 15 ohms. **Input Impedance:** 250 Kohms nominal. **Power Gain:** 90dB (1,000,000,000 times) after feedback. **Supply Voltage:** 6 to 28V. **Quiescent current:** 8mA at 28V. **Size:** 22 × 45 × 28mm including pins and heat sink.

Manual available separately 15p post free.

With FREE printed circuit board and 40 page manual.

**£2.98** Post free

### Project 605



The easy way to buy and build Project 60

Project 605 is one pack containing one P25, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free **£29.95**

Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having to solder.

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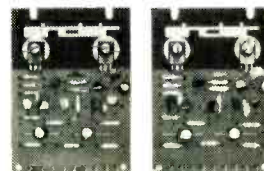


# the world's most advanced high fidelity modules

## Z.30 & Z.50 power amplifiers *Built, tested and guaranteed with circuits and instructions manual. z.30 £4.48 z.50 £5.48*

The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8Ω) and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may be used in a far wider range of applications.

**SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications).—Power Outputs:**  
**Z.30** 15 watts R.M.S. into 8 ohms using 35 volts. 20 watts R.M.S. into 3 ohms using 30 volts.  
**Z.50** 40 watts R.M.S. into 3 ohms using 40 volts. 30 watts R.M.S. into 8 ohms using 50 volts.  
**Frequency response:** 30 to 300,000Hz ±1dB. **Distortion:** 0.02% into 8 ohms. **Signal to noise ratio:** better than 70dB unweighted. **Input sensitivity:** 250mV into 100 Kohms (for 15w into 8Ω). For speakers from 3 to 15 ohms impedance. **Size:** 14 x 80 x 57mm.



## Stereo 60 Pre-amp/control unit

*Built, tested and guaranteed. £9.98*

Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly easy to mount.

**SPECIFICATIONS—Input sensitivities:** Radio – up to 3mV. Mag. p.u. 3mV. correct to R.I.A.A. curve ±1dB. 20 to 25,000 Hz. Ceramic p.u. – up to 3mV. Aux – up to 3mV. **Output:** 250mV. **Signal to noise ratio:** better than 70dB. **Channel matching:** within 1dB. **Tone controls:** TREBLE +12 to –12dB at 10KHz. BASS +12 to –12dB at 100Hz. **Front panel:** brushed aluminium with black knobs and controls. **Size:** 66 x 40 x 207mm.



## A.F.U. High & Low Pass Filter Unit

*Built, tested and guaranteed. £5.98*

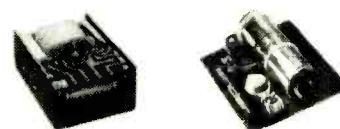
For use between Stereo 60 unit and two Z.30s or Z.50s. The unit is very easily mounted and is unique in that the cut-off frequencies are continuously variable. As attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. There are two filter sections – rumble (high pass) and scratch (low pass). H.F. cut-off (–3dB) variable from 28KHz to 5KHz. L.F. cut-off (–3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply) 0.02% at rated output. Operating voltage from 15 to 35V. Current 3mA. **Size:** 66 x 40 x 90mm.



## Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 or PZ.8 where a stabilised supply is essential.

- PZ.5** 30 volts un stabilised **£4.98**
- PZ.6** 35 volts stabilised **£7.98**
- PZ.8** 45 volts stabilised (less mains transformer) **£7.98**
- PZ.8** mains transformer **£5.98**



### Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	<b>Z.30</b>	Crystal P.U., 12V battery volume control, etc.	<b>£4.48</b>
Mains powered record player	<b>Z.30, PZ.5</b>	Crystal or ceramic P.U. volume control, etc.	<b>£9.45</b>
12W. RMS continuous sine wave stereo amp. for average needs	<b>2 x Z.30s, Stereo 60; PZ.5</b>	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	<b>£23.90</b>
25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	<b>2 x Z.30s, Stereo 60; PZ.6</b>	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	<b>£26.90</b>
80W. (3 ohms) RMS continuous sine wave deluxe stereo amplifier. (60W. RMS into 8 ohms)	<b>2 x Z.50s, Stereo 60; PZ.8, mains transformer</b>	As above	<b>£34.88</b>
Indoor P.A.	<b>Z.50, PZ.8, mains transformer</b>	Mic., guitar, speakers, etc., controls	<b>£19.43</b>

F.M. Stereo Tuner (£25) & A.F.U. (£5.98) may be added as required.

## Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in 'normal' use, we will service it at once and, without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

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**Type SW.100 100 x 80mm**


50µA	£3 80
50-0-50µA	£3 80
100µA	£3 80
100-0-100µA	£3 70
500µA	£3 50
1mA	£3 40
20V. D.C.	£3 40
50V. D.C.	£3 40
300V. D.C.	£3 40
1 amp. D.C.	£3 40
5 amp. D.C.	£3 40



300V. A.C. £3 40  
VU Meter £4 15

**Type SD.830 82.5mm x 110mm Fronts**

10µA	£2 50
50µA	£2 50
100µA	£2 50
500µA	£2 50
1mA	£2 50
1 amp.	£2 50
5 amp.	£2 50
10 amp.	£2 50
5V. D.C.	£2 50
10V. D.C.	£2 50
20V. D.C.	£2 50
50V. D.C.	£2 50
300V. D.C.	£2 50
1 amp. A.C.	£2 75
300V. A.C.	£2 75
VU Meter	£3 00



**Type SD.640 83.5mm x 85mm Fronts**

50µA	£2 80
50-0-50µA	£2 55
100µA	£2 55
100-0-100µA	£2 55
200µA	£2 55
500µA	£2 35
1mA	£2 35
3mA	£2 35
10µA	£2 35
50µA	£2 35
100µA	£2 35

500µA ..... £2 35  
1 amp. .... £2 35  
5 amp. .... £2 35  
10 amp. .... £2 35  
5V. D.C. .... £2 35  
10V. D.C. .... £2 35  
20V. D.C. .... £2 35  
50V. D.C. .... £2 35  
300V. D.C. .... £2 35  
1 amp. A.C. .... £2 40  
300V. A.C. .... £2 40  
VU Meter .... £2 70

**Type SD.460 46mm x 59.5mm Fronts**

50µA	£2 40
50-0-50µA	£2 35
100µA	£2 35
100-0-100µA	£2 35
200µA	£2 35
500µA	£2 20
1mA	£2 15
5µA	£2 15
10µA	£2 15
50µA	£2 15
100µA	£2 15

500µA ..... £2 15  
1 amp. .... £2 15  
5 amp. .... £2 15  
10 amp. .... £2 15  
5V. D.C. .... £2 15  
10V. D.C. .... £2 15  
20V. D.C. .... £2 15  
50V. D.C. .... £2 15  
300V. D.C. .... £2 30  
1 amp. A.C. .... £2 30  
VU Meter .... £2 55

**\* MOVING IRON—**  
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**Type MR.85P. 4 1/4in. x 4 1/4in. fronts.**

10µA	£3 10
50µA	£3 10
100µA	£3 10
500µA	£3 10
1 amp.	£3 10
5 amp.	£3 10
15 amp.	£3 10
30 amp.	£3 20
20V. D.C.	£3 10
50V. D.C.	£3 10
150V. D.C.	£3 10
300V. D.C.	£3 10
15V. A.C.	£3 10
15V. A.C.	£3 10
30V. A.C.	£3 10
150V. A.C.	£3 10
8 Meter 1mA	£3 15
VU Meter	£3 95
1 amp. A.C.*	£3 10
5 amp. A.C.*	£3 10
10 amp. A.C.*	£3 10
15 amp. A.C.*	£3 10
20 amp. A.C.*	£3 10
30 amp. A.C.*	£3 10

50µA ..... £3 95  
50-0-50µA ..... £3 40  
100µA ..... £3 40  
100-0-100µA ..... £3 30  
200µA ..... £3 30  
500µA ..... £3 20  
5000-500µA ..... £3 10  
1mA ..... £3 10  
1-1mA ..... £3 10  
5mA ..... £3 10

**Type MR.52P 2 1/2in. square fronts**

50µA	£3 40
50-0-50µA	£2 85
100µA	£2 85
100-0-100µA	£2 75
500µA	£2 55
1mA	£2 20
5mA	£2 20
10µA	£2 20
50µA	£2 20
100µA	£2 20
500µA	£2 20
1mA	£2 20
5 amp.	£2 20

500µA ..... £2 20  
1 amp. A.C.\* ..... £2 20  
5 amp. A.C.\* ..... £2 20  
10 amp. A.C.\* ..... £2 20  
20 amp. A.C.\* ..... £2 20  
30 amp. A.C.\* ..... £2 20

**Type MR.65P. 3 1/4in. x 3 1/4in. fronts**

50µA	£3 70
50-0-50µA	£3 00
100µA	£3 00
100-0-100µA	£2 90
200µA	£2 90
500µA	£2 85
5000-500µA	£2 40
1mA	£2 40
5mA	£2 40
10µA	£2 40
50µA	£2 40
100µA	£2 40
500µA	£2 40
1mA	£2 40
5 amp.	£2 40
10 amp.	£2 40
15 amp.	£2 40
20 amp.	£2 40
30 amp.	£2 55
50 amp.	£2 75
5V. D.C.	£2 40

10V. D.C. .... £2 40  
20V. D.C. .... £2 40  
50V. D.C. .... £2 40  
150V. D.C. .... £2 40  
300V. D.C. .... £2 40  
15V. A.C. .... £2 55  
50V. A.C. .... £2 55  
300V. A.C. .... £2 55  
8 Meter 1mA ..... £2 60  
VU Meter ..... £3 70  
1 amp. A.C.\* ..... £2 40  
100µA A.C.\* ..... £2 40  
200µA A.C.\* ..... £2 40  
500µA A.C.\* ..... £2 40  
1 amp. A.C.\* ..... £2 40  
5 amp. A.C.\* ..... £2 40  
10 amp. A.C.\* ..... £2 40  
20 amp. A.C.\* ..... £2 40  
30 amp. A.C.\* ..... £2 40

Send for illustrated brochure on SEW Panel Meters. Discounts for quantities.

**Type MR.38P. 1 21/32in. square fronts.**

50µA	£2 30
50-0-50µA	£2 10
100µA	£2 10
100-0-100µA	£1 95
200µA	£1 95
500µA	£1 80
500-0-500µA	£1 75
1mA	£1 75
1-0-1mA	£1 75
2mA	£1 75
3mA	£1 75
20µA	£1 75
20µA	£1 75
50µA	£1 75
100µA	£1 75

150µA ..... £1 75  
200µA ..... £1 75  
300µA ..... £1 75  
500µA ..... £1 75  
750µA ..... £1 75  
1 amp. .... £1 75  
2 amp. .... £1 75  
5 amp. .... £1 75  
10 amp. .... £1 75  
3V. D.C. .... £1 75  
10V. D.C. .... £1 75  
15V. D.C. .... £1 75  
20V. D.C. .... £1 75  
50V. D.C. .... £1 75  
100V. D.C. .... £1 75  
150V. D.C. .... £1 75  
300V. D.C. .... £1 75  
500V. D.C. .... £1 75  
750V. D.C. .... £1 75  
15V. A.C. .... £1 85  
50V. A.C. .... £1 85  
150V. A.C. .... £1 85  
300V. A.C. .... £1 85  
500V. A.C. .... £1 85  
8 Meter 1mA ..... £1 85  
VU Meter ..... £2 30

**Type MR.45P. 2in. square fronts.**

50µA	£2 50
50-0-50µA	£2 30
100µA	£2 30
100-0-100µA	£2 05
200µA	£2 05
500µA	£1 85
500-0-500µA	£1 85
1mA	£1 85
5mA	£1 85
10µA	£1 85
50µA	£1 85
100µA	£1 85
500µA	£1 85
1 amp.	£1 85

5 amp. .... £1 85  
10V. D.C. .... £1 85  
20V. D.C. .... £1 85  
50V. D.C. .... £1 85  
300V. D.C. .... £1 85  
15V. D.C. .... £2 00  
500V. D.C. .... £2 00  
8 Meter 1mA ..... £2 05  
VU Meter ..... £2 50  
1 amp. A.C.\* ..... £2 20  
5 amp. A.C.\* ..... £2 20  
10 amp. A.C.\* ..... £2 20  
20 amp. A.C.\* ..... £2 20  
30 amp. A.C.\* ..... £2 20

## EDGWISE METERS



**Type P.E.70. 3 1/2x3 1/2in. x 1 1/2x3 1/2in. x 2 1/2in. deep.**


50µA	£3 40
50-0-50µA	£3 30
100µA	£3 30
100-0-100µA	£3 20
200µA	£3 20

500µA ..... £3 05  
1mA ..... £2 70  
10µA ..... £2 70  
300V. A.C. .... £2 70  
VU Meter ..... £3 75

## "SEW" BAKELITE PANEL METERS

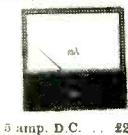
**Type MR.65. 3 1/4in. square fronts.**

1 amp.	£2 15
5 amp.	£2 15
15 amp.	£2 15
30 amp.	£2 15
60 amp.	£2 15
5V. D.C.	£2 15
10V. D.C.	£2 15
20V. D.C.	£2 15
50V. D.C.	£2 15
150V. D.C.	£2 15
300V. D.C.	£2 15
30V. A.C.*	£2 20
150V. A.C.*	£2 20
300V. A.C.*	£2 20
500µA A.C.*	£2 15
1 amp. A.C.*	£2 15
5 amp. A.C.*	£2 15
10 amp. A.C.*	£2 15
20 amp. A.C.*	£2 15
30 amp. A.C.*	£2 15
50 amp. A.C.*	£2 15
VU Meter	£3 40
50 amp. D.C.	£2 40
100µV D.C.	£2 40



**Type S.80 80mm Square Fronts**

50µA	£3 50
50-0-50µA	£3 40
100µA	£3 40
100-0-100µA	£3 30
500µA	£3 05
1mA	£2 85
20V. D.C.	£2 85
50V. D.C.	£2 85
300V. D.C.	£2 85
1 amp. D.C.	£2 85
300V. A.C.	£2 85
VU Meter	£3 70



5 amp. D.C. .... £2 85  
300V. A.C. .... £2 85  
VU Meter ..... £3 70

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**Type ED.107**


Size overall 100mm x 90mm x 108mm.

A new range of high quality moving coil instruments ideal for school experiments and other bench applications. 3 1/4in. mirror scale. The meter movement is easily accessible to demonstrate internal working.

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100µA	£5 10
1mA	£4 85
50µA	£5 10
100-0-100µA	£4 85
1-0-1mA	£4 85
1A D.C.	£4 85
5A D.C.	£4 85

10V D.C. .... £4 85  
20V D.C. .... £4 85  
50V D.C. .... £4 85  
300V D.C. .... £4 85  
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5V/50 V.D.C. £5 10



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20 Amp	£29 00
25 Amp	£38 00
40 Amp	£52 50

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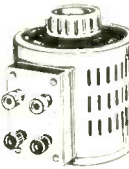
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1000 W	£7 50	P. & P. 38p
1500 W	£10 20	P. & P. 43p
2250 W	£17 25	P. & P. 50p
5000 W	£35 00	P. & P. 61




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Moving coil. Ideal for language teaching, communications. Headphone imp. 16 ohms. Microphone imp. 200 ohms. £4 62. Post 13p.



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Built-in gearbox. All brand new and boxed. 30 RPH CW; 2 RPH CW; 20 RPH CW; 2 RPH ACW; 30 RPH CW. 50p each. Post 12p.



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Solid state. Variable output 0-24V DC up to 1 amp. Dual scale meter to monitor voltage and current. Input 220/240V AC. Size 185 x 85 x 105mm. £8 97. Post 25p.




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**LB4 TRANSISTOR TESTER**

Tests PNP or NPN transistors. Audio indication. Operates on two 1.5v batteries. Complete with all instructions etc. £4 50. Post 20p.



**LB3 TRANSISTOR TESTER**

Tests IC0 and B. PNP/NPN. Operates from 9v battery. Complete with all instructions etc. £3 95. Post 20p.



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Industrial quality in robust metal cases. Battery operation. Volume and squelch controls. Call button and press to talk button. Telescopic aerial. Complete with carrying cases.

2 channel 300 mW.	£52 50	Pair. Post 50p.
3 channel 2 watt.	£79 50	Pair. Post 50p.



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Ideal for home, office, stores, factories, etc. Supplied complete with batteries, cable and free instructions.

2 Station	£2 97.	Post 15p.
3 Station	£5 25.	Post 15p.
4 Station	£6 62.	Post 17p.



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**G. W. SMITH & Co. (Radio) Ltd.**

Also see next three pages





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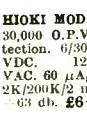


**T560 POCKET MULTIMETER**  
High-precision at low-cost.  
Ranges: D.C. 15V, 150V, 1,000V. (10,000 opv). A.C. 15V, 150V, 100V. (1,000 opv).  
D.C. Current 150mA. Resistance 100k/ohms. £1.85. Post 15p.

**MODEL 1092 Testmeter.**  
5,000 O.P.V.  
0/3/15/150/300/1200 V. D.C.  
0/30/300/600 V. A.C.  
0/300μA/300 mA  
0/10K/1 meg Ω  
Decibels -10 to +16 db.  
£2.75 each. Post 15p.



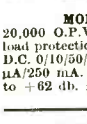
**HIOKI MODEL 720X**  
20,000 O.P.V. Overload protection.  
5/25/100/500/1000 VDC.  
10/50/250/1000 VAC. 50μA/250 mA.  
20K/2 meg ohm. -5 to +62db. £4.97. Post 15p.



**HIOKI MODEL 730X**  
30,000 O.P.V. Overload protection.  
6/30/60/300/600/1200 VDC.  
12/60/120/600/1200 VAC.  
60 μA/30 mA/300 mA.  
2K/200K/2 megohm. -10 to +63 db. £6.50. Post 15p.



**MODEL TE-12**  
20,000 O.P.V. 0/0.6/30/120/600/1200/3,000/6,000V. D.C.  
0/6/30/120/600/1200V. A.C.  
0/60μA/6/60/600mA. 0/6K/600K/6 meg. 60 Meg. Ω 50pF.  
0.2mFd. £5.97. Post 17p.



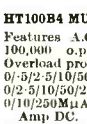
**MODEL TE-200**  
20,000 O.P.V. Mirror scale, overload protection. 0/5/25/125/1,000V. D.C. 0/10/50/250/1,000V. A.C. 0/50 μA/250 mA. 0/60K/6 meg Ω. -20 to +62 db. £3.95. Post 15p.



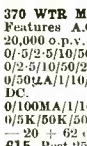
**MODEL 500** 30,000 O.P.V. with overload protection, mirror scale. 0/5/25/10/25/100/250/500/1,000 V. D.C. 0/2/5/10/25/100/250/500/1,000 V. A.C. 0/50μA/5/50/500 mA. 12 amp. D.C. 0/60K/6 meg/60 meg Ω. £8.87. Post paid.



**HIOKI MODEL 750X**  
50,000 o.p.v. 43 ranges 0-0.3 to 1,200V. D.C. 0-3 to 1,200 V. A.C. 0-30μA/300mA. 0-3K/30 meg. ohms. -10 to +17 db. £78.97. Post 20p.



**HT100B4 MULTIMETER**  
Features A.C. current ranges, 10,000 o.p.v. Mirror Scale, Overload protection.  
0/5/2.5/10/50/250/500/1000 V D.C.  
0/2.5/10/50/250/1000 V A.C.  
0/10/250μA/2.5/25/250 mA/10 Amp DC.  
10 Amp AC.  
0/20K/200K/2MEG/20MEG. -20 + 62 db.  
£12.50. Post 25p.



**370 WTR MULTI METER**  
Features A.C. current ranges, 20,000 o.p.v.  
0/5/2.5/10/50/250/500/1000 V D.C.  
0/2.5/10/50/250/500/1000 V A.C.  
0/50μA/1/10/100mA/1/10 Amp DC.  
0/100mA/1/10 Amp AC.  
0/5K/50K/500K/5MΩ/50MEG. -20 + 62 db.  
£15. Post 25p.

**RUSSIAN 22 RANGE MULTIMETER**

Model U437 10,000 o.p.v. A first class variable instrument manufactured in U.S.S.R. to the highest standards. Ranges: 2/5/10/50/250/500/1000V D.C. 2/5/10/50/250/500/1000V A.C. D.C. Current 100 μA/1/10/100 mA/1A. Resistance 300 ohms/3/30/300K/3M Ω. Complete with batteries, test leads, instructions and sturdy steel carrying case. Our Price £5.97. Post 25p.



**ROUND SCALE TYPE PENCIL TESTER MODEL TS.68**



Completely portable, simple to use pocket sized tester. Ranges: 0/3/30/300V. A.C. and D.C. at 2,000 o.p.v. Resistance 0-20K ohms. Only £1.97. Post 13p.

**LT901 MULTIMETER**  
New style 20,000 o.p.v. pocket multimeter.  
5/25/50/250/2500V. D.C.  
10/50/100/500/1000V. A.C.  
50μA/250mA. 6K/6 meg ohms. -20 to +22db. £3.75. Post 20p.



**MODEL TR-12**  
20,000 o.p.v. Overload protection. Slide switch selector. 0/1/25/2.5/10/50/250/1000V. D.C.  
0/10/50/250/1000V. A.C.  
0/50μA/25/250mA D.C.  
0/3K/30K/300K/3 meg. -20 to +50db. £4.97. Post 15p.



**MODEL TE-300** 30,000 O.P.V. Mirror scale, overload protection 0/6/3/15/60/300/1,200 V.D.C.  
0/6/30/120/600/1,200 V.A.C.  
0/300μA/60mA/60mA/600mA/600mA.  
0/8K/80K/800K/8 meg. -20 to +63 db. £5.97. Post 15p.



**MODEL PL436.** 20kΩ/Volt D.C. 8kΩ/Volt A.C. Mirror scale. 0/3/12/30/120/600V D.C. 3/30/120/600V A.C. 50/600μA/30/600mA. 10/100K/1 Meg/10 meg Ω. -20 to +40db. £6.97. Post 12p.



**TMK MODEL TW-50K**  
46 ranges, mirror scale, 50K/Volt. D.C. 5K Volt A.C. D.C. Volts: 125, 25, 2.5, 5, 10, 25, 50, 125, 250, 500, 1,000V. A.C. Volts: 1.5, 3, 5, 10, 25, 50, 100, 250, 500, 1,000V. D.C. Current: 25, 50μA, 2.5, 5, 25, 50, 250, 500mA, 5, 10 amp. Resistance: 10K, 100K, 1 MEG, 10 MEGΩ. Decibels: -20 to -81.5 db. £8.50. Post 17p.



**MODEL K228A**  
Taut band suspension. Overload protection. Polarity reversing switch. 30,000 o.p.v.  
0/5/2.5/15/250/500/1000/2500V D.C.  
0/15/50/150/500/1000V. A.C.  
0/50μA/5/50/150/500mA/5A D.C.  
0/3K/300K/3 meg. £8.95. Post 20p.



**HIOKI MODEL 700X**  
100,000 O.P.V. Overload protection. Mirror scale. 3/4/12/1/5/3/6/12/30/60/150/300/600/1200 V.D.C.  
1.5/3/6/12/30/60/150/300/600/1200 V.A.C.  
15/30V/3/6/30/60/150/300 mA. 6/12 AMP DC. 2K/200 K/2 Meg/20 megohm. -20 to +63db. £13.50. Post 20p.



**MODEL C-7080 EN**  
Giant 6in. mirror scale. 20,000 o.p.v.  
0/25/1/2.5/10/50/250/1000/5000V. D.C.  
0/2.5/10/50/250/1000/3000V. A.C.  
0/50μA/1/10/100/500mA/10 amp. D.C.  
0/2K/200K/20 meg. -20 to +50 db. £13.95. Post 35p.



**U4312 MULTIMETER**  
Extremely sturdy instrument for general electrical use. 667 o.p.v. 0/3/15/75/30/60/150/300/600/900 VDC and 75mV. 0/3/15/75/30/60/150/300/600/900 VAC. 0/300μA/1.5/6/15/60/150/600mA/1.5A. D.C. 0/1.5/6/15/60/150/600mA/1.5A. A.C. 0/200/2/3K/30K Ω. Accuracy DC 1%. AC 1.5%. Knife edge pointer, mirror scale. Complete with sturdy metal carrying case. Leads and instructions. £9.50. Post 25p.



# Selected TEST EQUIPMENT

**FTC-401 TRANSISTOR TESTER**

Full capabilities for measuring A, B and 100. NPN or PNP. Equally adaptable for checking diodes. Supplied complete with instructions, battery and leads. £7.50. Post 20p.



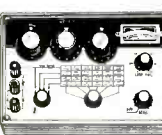
**TE-16A** Transistorised Signal generator. 5 ranges 300KHz-30MHz. An inexpensive instrument for the handyman. Operates on 9v battery. Wide easy to read scale. 800kHz modulation. 51 x 51 x 31in. Complete with instructions and leads. £7.97. Post 25p.

**Model S-100TR MULTI-METER/TRANSISTOR TESTER 100,000 o.p.v. MIRROR SCALE/OVERLOAD PROTECTION**

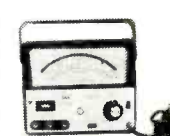
0/12-0/3/12/30/120/600 V DC.  
0/6/30/120/600 V. A.C.  
0/12/600μA/12/300MA/12 Amp. DC.  
0/10K/1 MEG/10 MEG. -20 to +50 db. 0-01 -2 mfd. Transistor tester measures Alpha, beta and Ico. Complete with batteries, instructions and leads. £13.50. Post 25p.



**TRANSISTORISED L.C.R. A.C. MEASURING BRIDGE.**



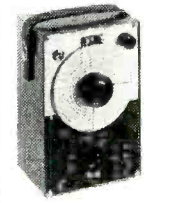
A new portable bridge offering excellent range and accuracy at low cost. Ranges: R. 1Ω-111 MEG Ω. 6 Ranges ± 1%. L. 1μH-111 HENRIES. 6 Ranges ± 2%. C. 10pF-1110MFD. 6 Ranges ± 2%. TURNS RATIO 1:1/1000-1:1/1100 6 Ranges ± 1%. Bridge voltage at 1,000 CFS. Operated from 9 volts, 100μA. Meter indication. Attractive 2 tone metal case. Size 7 1/2" x 5" x 2" £20. Post 25p.



**MODEL 449A IN CIRCUIT TRANSISTOR TESTER**  
Checks true A.C. beta in/out. Checks Ico. Checks diodes in/out. Checks SCR etc. Beta HI 10-500. LO2-50. £17.50. Post 25p.

Icho 0-5000μA. 220/240V. A.C. operation. £17.50. Post 25p.

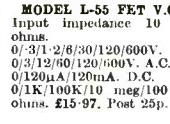
**RF-300 AF/RF SIGNAL GENERATOR**



All transistorised, compact, fully portable. AF sine wave 18Hz. to 220KHz. AF square wave 18Hz. to 100KHz. Output sine/square 10V. P.P. RF 100KHz. to 200 MHz. Output 1v. maximum. Operation 220/240V. A.C. Complete with instructions and leads. £29.95. Post 50p.



**TE-20 D RF SIGNAL GENERATOR**  
Accurate wide range signal generator covering 120 Kc/s-500 Mc/s on 6 bands. Directly calibrated Variable R.F. attenuator, audio output. Xtal socket for calibration 220/240V. A.C. Brand new with instructions. £15. Carr. 37d. Size 140 x 215 x 170 mm.



**MODEL L-55 FET V.O.M.**  
Input impedance 10 meg. ohms. 0/3/1-2/6/30/120/600V. D.C. 0/3/12/60/120/600V. A.C. 0/120μA/120mA. D.C. 0/1K/100K/10 meg/100 meg ohms. £15.97. Post 25p.



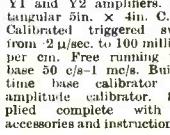
**CI-5 PULSE OSCILLOSCOPE**  
For display of pulsed and periodic waveforms in electronic circuits. VERT. AMP. Bandwidth 10MHz. Sensitivity at 100KHz VRMS/mm. 1-25; HOH. AMP. Bandwidth 500KHz. Sensitivity at 100KHz. V RMS/mm. 3-25; Preset triggered sweep 1-3,000μsec.; free running 20-200,000Hz in nine ranges. Calibrator pipe. 220 x 360 x 430mm. 115-230V. A.C. operation. £39.00. Carr. paid.

**TO-3 PORTABLE OSCILLOSCOPE, 3" TUBE**



Y amp. Sensitivity. 1v p-p/CM. Bandwidth 1.5 cps -1.5 MHz. Input imp. 2 meg Ω. 25 PF. X amp sensitivity. 9v p-p/CM. bandwidth 1.5 cps-800 KHz. Input imp. 2 meg Ω. 20 PF. Time base. 5 ranges 10 cps-300 KHz. Synchronization. Internal/external. Illuminated scale. 140 x 215 x 330 mm. Weight 15lbs. 220/240 V. A.C. Supplied brand new with handbook £40.00. Carr. 50p.

**RUSSIAN CI-16 DOUBLE BEAM OSCILLOSCOPE**



5 mcs Pass Band. Separate Y1 and Y2 amplifiers. Rectangular 5in. x 4in. CRT. Calibrated triggered sweep from 2μsec. to 100 milli-sec. per cm. Free running time base 50 c/s-1 mcs. Built-in time base calibrator and amplitude calibrator. Supplied complete with all accessories and instruction manual. £87 Carr. paid.

**MODEL TE.15 GRID DIP METER**

Transistorised. Operates as Grid Dip, Oscillator, Absorption Wave Meter and Oscillating Detector. Frequency range 440Kc/s-280Mc/s in 6 coils. 500μA Meter. 9V. battery operation. Size 180 x 80 x 40mm. £12.50. Post 20p.



**BELCO AF-5A SOLID STATE SINE SQUARE WAVE C.R. OSCILLATOR**



Sine 18-200,000 Hz; Square 18-500,000 Hz. Output max. +10 dB (10 K ohms). Operation internal batteries. Attractive 2-tone case 7 1/2in. x 5in. x 2in. Price £17.50 Carr. 17p.



**MODEL MG-100 SINE SQUARE WAVE AUDIO GENERATOR**  
Range: 19-220,000 Hz. Sine Wave 19-100,000 Hz. Square Wave. Output Sine or Square wave 10v. P. to P. Size 180 x 90 x 90mm. Operation 220/240V. A.C. £17.50. Post 37p.



**MODEL AT201 DECADE ATTENUATOR**  
Frequency range: 0-200KHz. Attenuator: 0-111db. 0.1db. step. Impedance 600 ohms. Max. input power 30dbm. Size 180 x 90 x 55mm. £12.50. Post 37p.

**TE-65 VALVE VOLTMETER**

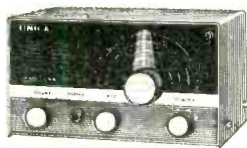
High quality instrument with 28 ranges. D.C. volts 1.5-1,500 v. A.C. volts 1.5-1,500 v. Resistance up to 1,000 megohms. 220/240V. A.C. operation. Complete with probe and instructions. £17.50. Post 30p. Additional Probes available: R.P. £2.12 H.V. £2.50.



**MODEL U4311 SUB-STANDARD MULTI-RANGE VOLT AMMETER**  
Sensitivity 330 ohms/Volt A.C. and D.C. Accuracy 5% D.C. 1% A.C. Scale length 165mm. 0/300/750μA/1.5/3/7.5/15/30/75/150/300/750mA/1.5/3/7.5/15/30/75/150/300/750V. D.C. 0/750mV/1.5/3/7.5/15/30/75/150/300/650V. A.C. Automatic cut out. Supplied complete with test leads, manual and test certificates. £49. Post 50p.

**G. W. SMITH & Co. (Radio) Ltd.**  
Also see opposite page and next two pages





**UNR 30 RECEIVER**  
4 Bands covering 550kc/s - 30mc/s. B.F.O. Built in Speaker 220/240v AC. Brand new with instructions. £15.75. Carr. 37p.



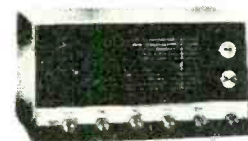
**UR-1A SOLID STATE COMMUNICATION RECEIVER**  
4 Bands covering 550kc/s-30mc/s. FET, 8 Meter. Variable BFO for SSB. Built-in Speaker. Bandspread. Aerobic tuning. BFO. A.V.C. N.L. 'R' meter. AM/CW/SS B. Integrated speaker and phone socket. Operation 220/240v AC or 12v. D.C. 12 1/2" x 4 1/2" x 7". Brand new with instructions. £25. Carr. 37p.

**SKYWOOD CX203 COMMUNICATION RECEIVER**



Solid state. Coverage on 5 bands, 200-420 KHz and 55 to 30 MHz. Illuminated slide rule dial. Bandspread. Aerobic tuning. BFO. A.V.C. N.L. 'R' meter. AM/CW/SS B. Integrated speaker and phone socket. Operation 220/240v AC or 12v DC. Size 325 x 266 x 150 mm. Complete with instructions and circuit. £28.50. Carr. 50p.

**LAFAYETTE HA-600 SOLID STATE RECEIVER**



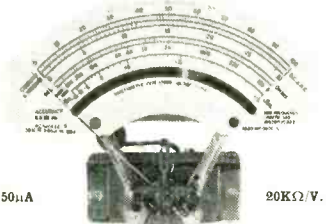
General coverage 150-400 Kc/s, 550kc/s-30 mc/s. FET front end. 2 mech. filters. product detector, variable B.F.O., noise limiter, 8 Meter, Bandspread. RF gain. 15" x 9 1/2" x 8 1/2". 18 lb. 220/240v AC. or 12V D.C. Brand new with instructions. £50. Carr. 50p.

**TRIO 9R59DS COMMUNICATION RECEIVER**



4 band covering 550 Kc/s to 30 Mc/s. continuous and electrical bandspread on 10, 15, 20, 40 and 80 metres. 8 valve plus 7 diode circuit. 4/8 ohm output and phone jack. SSB-CW. A.N.L. Variable BFO. 8 meter. Sep. bandspread dial. 1F frequency 445 Kc/s. audio output 1.5v. Variable RF and PA gain controls 115/950v A.C. Size: 7in. x 13in. x 10in. with instruction manual. £49.50. Carr. paid.

**AVOMETER MOVEMENTS**



Spare movements for Model 8 or 9. (Fitted with Model 9 scale) or basis for any multimeter. Brand new and boxed. £3.50. Post 25p.

**HONEYWELL DIGITAL VOLTMETER VT.100**



Can be panel or bench mounted. Basic meter measures 1 volt DC, but can be used to measure a wide range of AC and DC volt, current and ohms with optional plug in cards. Specification: Accuracy: ± 0.2, ± 1 digit. Resolution: 1 mV. Number of digits: 3 plus fourth overrange digit. Overrange: 100% (up to 1.999). Input impedance: 1000 Meg ohms. Measuring cycle: 1 sec. Adjustment: Automatic zeroing, full scale adjustment against an internal reference voltage. Overload: to 100v. D.C. Input: Fully floating (3 poles). Input power: 110-230v. A.C. 50/60 cycles. Overall size: 5 1/2in. x 2 13/16in. x 8 3/16in. AVAILABLE BRAND NEW AND FULLY GUARANTEED. £35.50 Carr. 50p.

**SINCLAIR IC-12**



List price £2.98  
**OUR PRICE**  
**£1.80**  
Post 10p.

**SINCLAIR EQUIPMENT Project 60. Package Offers**



2 x Z30 amplifier, stereo 60 pre-amp, P25 power supply. £15.95. Carr. 37p. Or with P26 power supply. £18.00. Carr. 37p. 2 x Z50 amplifier stereo 60 pre-amp, P28 power supply. £20.25. Carr. 37p. Transformer for P28. £2.97 extra. Add to any of the above £4.45 for active filter unit and £13.00 for a pair of Q18 speakers. All other Sinclair products in stock. IC12 £1.80. Post 10p. 2,000 amp £21.95. Carr. 37p. 3,000 amp £28.50. Carr. 37p. Neoteric amp £43.95. Carr. 37p. NEW PROJECT 605 £20.97. Carr. 37p.

**WHARFEDALE MID-RANGE HI-FI UNITS**

As used in world famous system. 5in. dia. Impedance 4/8 ohms. High flux ceramic magnet. 20 watts rms. Brand new £15.00. Carr. 37p.



**SPECIAL OFFER GOODMANS AXIOM 301**

Hi Fi 12in. 20 watt twin cone full range speaker. 30-18,000 Hz. 16,500 gauss. 8 ohm impedance. Brand new and boxed. (List price £21.72) OUR PRICE £12.50 each. Carr. 50p.



**EMI LOUSPEAKERS**

Model 350. 13" x 8" with single tweeter/crossover. 20-20,000 Hz. 15 watt RMS. Available 8 or 15 ohms. £7.25 each. Post 37p. Model 450. 13" x 8" with twin tweeters/crossover. 55-13,000 Hz. 8 watt RMS. Available 8 or 15 ohms. £3.62 each. Post 25p.



**EA-41 REVERBERATION AMPLIFIER**

Self contained, transistorised. battery operated. Simply plug in microphone, guitar, etc. and output into your amplifier. Volume control, depth of reverberation control. Beautiful walnut cabinet. 7 1/2 x 3 1/4 in. £5.97. Post 15p.



**SPECIAL OFFER! STEREO SPEAKERS**

Matched pair of stereo bookshelf speakers. De-luxe teak veneered finish. Size 14 1/2in. x 9in. x 7 1/2in. 8 ohms 8 watt RMS. 16 watt peak. Complete with 12V lead. £12.95 pr. Carr. 50p.



**MW/LW CAR RADIO**

Fully transistorised, dual waveband. Size 6 1/2in. x 4 1/2in. x 2 1/2in. 12v. D.C. Neg. or Pos. earth. Complete with fixing kit, speaker and leads. ONLY £7.50. Post 20p.



**SUPER BARGAIN!**

**8-TRACK CAR STEREO TAPE PLAYER**

Tone, volume and balance controls. Track selector. Complete with matched pair of stereo speakers, connections and fittings. ONLY £15.95. Post 30p.



**B.S.R. TD8S 8-TRACK STEREO TAPE PLAYER DECK**

Integrated preamps (output 125 mV) to feed into any stereo amplifier. Automatic and manual programme selector. 4 pole synchronous motor. 210/240 V. A.C. OUR PRICE £16.25 Carr. 37p.



**AKAI BARGAINS**

**SUPER MONEY-SAVING OFFERS—BUY NOW WHILE STOCKS LAST! ALL BRAND NEW AND FULLY GUARANTEED**



- 1721 Tape Rec. . . . . £73.95
- X5000 Tape Rec. . . . . £99.95
- GX370 Tape Rec. . . . . £259.95
- 4000D Tape Deck . . . . . £61.50
- X201D Tape Deck . . . . . £73.95
- X221D Tape Deck . . . . . £189.95
- GX220D Tape Deck . . . . . £184.95
- GX280D Tape Deck . . . . . £249.40
- X1810SD Tape/8 track Deck . . . . . £189.95
- GX1900D Tape/Cas. Deck . . . . . £177.95
- X20081D Tape/Cas./8 Rec. . . . . £223.50
- CR81 8 track Rec. . . . . £50.95
- CR81D 8 track Rec. . . . . £65.95
- CR81T 8 track Receiver . . . . . £118.90
- CR808S 8 track system . . . . . £145.00
- CS60 Cassette Rec. . . . . £79.00
- CS50D Cassette Deck . . . . . £74.95

- GXC40 Cassette Rec. . . . . £82.95
- GXC40D Cassette Deck . . . . . £86.95
- GXC40T Cassette Receiver . . . . . £123.95
- GXC45D Cassette Deck . . . . . £95.95
- GXC48D Cassette Deck . . . . . £103.50
- GXC60D Cassette Deck . . . . . £111.25
- GXC65D Cassette Deck . . . . . £119.25
- CS35D Cassette Deck . . . . . £59.50
- AA6200 Receiver . . . . . £74.95
- AA6300 Receiver . . . . . £82.50
- AA6800 Receiver . . . . . £109.00
- AA6900 Receiver . . . . . £175.00
- ADM11 Microphones (Pair) . . . . . £7.50

Carriage 50p. extra. (Recorders & Decks 75p.)

**GENUINE BARGAIN!**



**KOSS SP.3XC STEREO HEADPHONES**  
Response 10-15,000 Hz. Impedance 4-6 ohms. Brand new, boxed and fully guaranteed. (List £9.50). OUR PRICE £6.50. Post 25p.

**1021 STEREO LISTENING STATION**

For balancing and gain selection of loudspeakers with additional facility for stereo headphone switching. 2 gain controls, speaker on-off slide switch, stereo headphone sockets. 6" x 4" x 2 1/2". £2.25. Post 15p.



**MP7 MIXER PREAMPLIFIER**

5 microphone inputs each with individual gain controls enabling complete mixing facilities. Battery operated. 9 1/2" x 5" x 3". Inputs Mics: 3 x 3mV 50K; 2 x 3mV 600 ohm. Phono meg. 4 mV 50K. Phono ceramic 100mV 1 meg. Output 250mV 100K. £8.97. Post 20p.



**TE-1035 STEREO HEADPHONES**

Low cost high performance stereo headphones. Foam rubber ear cups. Adjustable headband. 8 ohm impedance. 25-18,000 Hz. With lead and stereo jack plug. ONLY £1.97. Post 12p.

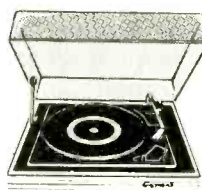


**HA-10 STEREO HEADPHONE AMPLIFIER**

All silicon transistor amplifier operates from magnetic ceramic or tuner inputs with twin stereo headphone outputs and separate volume controls for each channel. Operates from 9v. battery. Inputs 5mV/100mV. Output 50mV. £5.97. Post 15p.



**NEW GARRARD MODULES**



Popular range of Garrard decks with Shure cartridge fitted in de-luxe plinth with hinged lid. SP25 Hi Module/M75-6 . . . . . £33.50  
AP76 Module/M75-6 . . . . . £33.80  
AP96 Module/M75-6 . . . . . £38.75  
Zero 1008 Module/M93E . . . . . £52.60  
Carr. 50p extra any item.

**DOLBY SYSTEM NOISE REDUCTION UNIT**



Improves the performance of cassette and semi-professional recorders. Reduces tape hiss by 3dB at 600 Hz, 6 dB at 1200 Hz and 10 dB for all frequencies above 300 Hz. Controls for input levels and noise reduction on record and replay. 2 meters for Dolby level. Off tape monitoring. Frequency response: 20 Hz to 15kHz ± 1 dB 19 kHz - 35 dB. Size 15 1/2" x 9" x 3 1/2". A.C. 200/250 V.

OUR PRICE £32.50 Carr. 50p.

**HOSIDEN DH-02S STEREO HEADPHONES**

Wonderful value and excellent performance combined. Adjustable head band. 8 ohm impedance. 20-12,000 cps. Complete with lead and stereo jack plug. ONLY £2.37. Post 12p.



**TAPE CASSETTES**

Top quality Hi-Fi Low Noise in Library cases.



C80 . . . . . 3 for 75p 10 for £2.35  
C90 . . . . . 3 for £1.05 10 for £3.30  
C120 . . . . . 3 for £1.35 10 for £4.20

Tape Head Cleaner 30p each. Post 10p extra.

**SPECIAL OFFER! ROTEL RH700 STEREO HEADPHONES**



20-20,000Hz. 8-16 ohm. (List £9.95). OUR PRICE £6.75. Post 25p.

**SPECIAL PURCHASE! LEAK MINI-SANDWICH SPEAKERS**



Brand new and fully guaranteed. 8 watts. 8 ohm. Teak finish. (Rec. list £59.50 pr.) OUR PRICE £39.50 pr. Carr. £1.00

**TRANSISTORISED FM TUNER**



6 TRANSISTOR HIGH QUALITY TUNER SIZE ONLY 6in. x 4in. x 2 1/2in. 3 I.F. stages. Double tuned discriminator. Ample output to feed most amplifiers. Operates on 9 volt battery. Coverage 88-108 Mc/s. Ready built ready for use. Fantastic value for money. £6.37. Post 12p. STEREO MULTIPLEX ADAPTORS. £4.97.

**TE 1018 DE-LUXE MONO HIGH IMPEDANCE HEADSET**



Sensitive, soft earpads, adjustable headband. Magnetic impedance 2,600 ohms. £1.97. Post 15p.

**G. W. SMITH & Co. (Radio) Ltd.**  
Also see previous pages and opposite page.



**FANTASTIC OFFER!**

**NIKKO TRM 50 STEREO AMPLIFIER**



17 + 17 watts rms stereo amplifier with inputs for Magnetic and Crystal phono, Tuner, Tape, AUX. and Tape Monitor. Outputs for two pairs of stereo speakers and Tape. Stereo headphone socket. Full range of controls including loudness control, scratch filter etc. Size 13in. x 9 1/2in. x 3 1/2in. Unrepeatable offer—limited stocks!

List price £59.50  
**OUR PRICE £39.95**  
Carriage 50p.

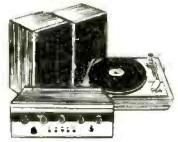
**NIKKO TRM 50 SYSTEM**



Nikko TRM50 17+17 watt stereo amplifier, BSR MP60, plinth and cover, Goldring G800 cartridge, pair of Linton 2 speakers and all leads.

**OUR PRICE £104.90** Carr. & Ins. £1.50

**LEAK DELTA 30 SYSTEM**



Leak Delta 30 stereo amplifier, Goldring GL75, plinth, cover and G800 cartridge. Pair of Leak 150 speakers and all leads.

**OUR PRICE £121.50** Carr. & Ins. £1.50

**AMSTRAD 8000 II SYSTEM**



Amstrad 8000 II 7 + 7 watt amplifier, BSR MP60, plinth and cover, Goldring G800 cartridge, pair of Apollo speakers and all leads. Amplifier only, £14.50. Carr. 50p.

**OUR PRICE £48.25** Carr. £1.00

**AUDIOTRONIC LA.1700 SYSTEM**



17 + 17 watt stereo amplifier, Garrard AP76 with Goldring G800 cartridge, teak veneered plinth with cover and a pair of Wharfedale Linton 2 speakers in matching teak.

**OUR PRICE £92.95** Carr. & Ins. £1.50

Matching LT1700 AM/FM Stereo Tuner £39.00 if purchased with above system.

**SUPER MONEY SAVING OFFER!**

**TELETON R.4300L**



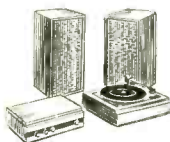
3 waveband stereo tuner amp. 2 x 5W Medium/Long/Stereo FM. Full range of controls. Input for tape or ceramic cartridge.

List over £50.00 **OUR PRICE £27.50** Post 50p

**CREDIT TERMS AVAILABLE FOR CALLERS**



**WHARFEDALE LINTON SYSTEM**



Wharfedale Linton Amplifier, Linton Turntable, pair of Linton 2 speakers and all leads.

**OUR PRICE £105.00** Carr. & Ins. £1.25

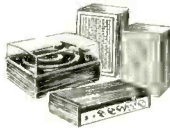
**TELETON CRIOT/RG42 SYSTEM**



Teleton AM/FM 4 + 4 watt stereo tuner amplifier, Garrard 2025 T/C, plinth and cover, stereo cartridge, pair of matching speakers and all leads.

**OUR PRICE £35.50** Carr. £1.00

**TELETON SAQ206B SYSTEM**



Teleton SAQ206B 8 + 8 watt amplifier, BSR MP60, plinth and cover, Goldring G800 cartridge, pair of Apollo speakers and all leads.

**OUR PRICE £55.95** Carr. £1.50

Amplifier only, £22.95. Post 50p.

**TRIO KA 2000A SYSTEM**



Trio KA 2000A 16 + 16 watt amplifier, BSR MP60, plinth and cover, Goldring G800 cartridge, pair of Denton 2 speakers and all leads.

**OUR PRICE £79.95** Carr. £1.25

Matching Trio KT 1000A AM/FM stereo tuner, £50.95 extra if required.

**SPECIAL PURCHASE!**

**FERGUSON 3414 STEREO TUNER AMPLIFIER TURNTABLE UNIT**

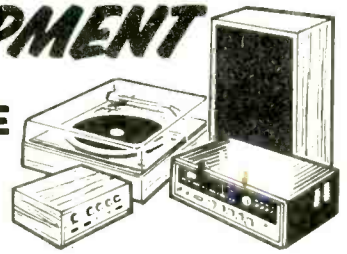


10+10 watts rms. Five push buttons with separate scales for pre-tuning to desired FM station. Housed in a handsome walnut finished cabinet with BSR M128/MP60 record deck with Goldring G800H stereo magnetic cartridge. Offered complete with cover and a pair of matching Medway speakers, size 18" x 11" x 8".

TODAY'S VALUE AT LEAST **OUR PRICE £75** Carr. & Ins. £1.50

**HI-FI EQUIPMENT SAVE UP TO 33 1/3% OR MORE**

SEND S.A.E. FOR FULL DISCOUNT PRICE LISTS AND PACKAGE OFFERS



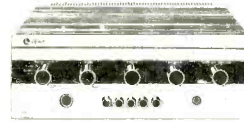
**SAVE £££**

**PHILIPS GA308 TRANSCRIPTION TURNTABLE**

2 speeds 33 1/3 and 45 r.p.m. Light weight tubular counter-balanced arm. Belt driven low speed synchronous motor. Viscous damped pick up fit/low device. Complete with teak plinth and hinged cover. GA308 less cartridge (List £36.55) **OUR PRICE £24.50**. Post 50p. GA308 PU with GP400 stereo magnetic cartridge (List £47.95) **OUR PRICE £29.95**. Post 50p. LIMITED NUMBER ONLY!



**LEAK BARGAINS**



**LIMITED OFFER! ALL STOCKS BRAND NEW AND GUARANTEED**

Delta 30	£45.95
Delta 70	£55.95
Delta FM	£55.95
Delta AM/FM	£67.95
Delta 75	£127.50
Leak 150, pair	£37.50
Leak 250, pair	£47.95
Leak 600, each	£33.95

Post 50p extra each item.

**ROTEL BARGAINS!**

ALL BRAND NEW AND GUARANTEED



RA210 Amp.	£29.95
RA310 Amp.	£35.95
RA610 Amp.	£48.25
RX150 Receiver	£48.95
RX200 Receiver	£60.95
RX400 Receiver	£70.95

Post 50p extra any item.

**EAGLE TSA.150 STEREO AMPLIFIER**



Housed in attractive Teak cabinet 7.5 x 7.5 watts rms. Switched input for Max. Car tape, tuner, bass, treble, volume balance controls. Headphone socket. Output for main or remote speakers. List Price £29.60.

**OUR PRICE £16.50**. Post 50p.

**AKAI BARGAINS!**



**MODEL AA6300 AM/FM STEREO TUNER AMPLIFIER**

20+20 watts rms. Inputs for magnetic and ceramic cartridge and tape. Frequency response 20-20,000Hz. Bass, treble, volume and loudness controls. Frequency range FM 88-108MHz. AM 535-1605kHz. Headphone socket. Output for two pairs of speakers. 17 1/2" x 5 1/2" x 13 1/2". List Price £123.85.

**OUR PRICE £82.50** Post 50p

**RECORD DECKS**

(Post 50p.)

B.S.R. McDONALD C129 Mono.	£6.50
C137	£8.35
MP60	£9.75
610	£12.65
810	£31.25
210/TP13	£8.75
MP60/G800	£12.95
MP60/TPD1	£16.95
MP60/TPD1/G800	£19.50
MP60/TPD2	£14.35
610/TPD1	£18.95
510/TPD1	£17.95
HT70	£19.99
HT70/G800	£17.25
HT70/TPD1	£20.35
HT70/TPD1/G800	£23.90
810 Plinth/Cover	£9.25



<b>GOLDRING</b> GL69/2	£18.50
GL72	£20.95
GL72/P	£27.50
Plinth 69/72	£7.02
Lit 72	£3.25
GL75	£28.95
GL75/P	£35.25
Plinth 75	£7.35
LID 75	£3.80
G99	£19.25
GL85P/C	£58.95
LID 85	£4.95
G101P/C	£20.50

**LEAK Delta T table**

£52.50

**MICRO-SEIKI MR111**

£29.50

MR111 Plinth & Cover. £9.50

**PHILIPS GA105**

£16.65

GA105 Teak. £27.00

GA308 Teak. £24.50

GA308 P.U. Teak. £28.95

GA212. £25.75

**PIONEER PL120**

£34.50

PL15C. £51.35

PLA35. £82.65

PL50. £111.95

PL11D. £118.50

PL61. £119.95

**THORENS TD125 II**

£66.50

TD125AB II. £99.95

TX25. £6.95

TD160C. £56.95

TD150. £28.95

TD160A II. £35.95

TD150AB II. £39.95

TD150 Plinth. £3.80

TX11. £3.60

**WHARFEDALE Linton Turntable**

£28.95

**PLINTHS & COVERS (Post 50p)**

Budget SP25 etc.	£3.20
Budget SP25 Play on	£4.80
Budget AP76/Zero 100s	£4.50
Budget B.S.R.	£3.25
SME 2000 System	£34.50

**RECORD DECK PACKAGES (Post 50p.)**

Decks supplied with stereo cartridge ready wired in plinth with cover.



Garrard 2025TC/9TAHCD	£12.75
Garrard SP25 III/9TAHCD	£15.95
Garrard SP25 III/G800	£18.50
Garrard SP25 III/M75-6	£18.50
Garrard SP25 III/H41-7	£19.75
Garrard SP25 III/H41-E	£20.95
Garrard SP25 III/M55E	£22.40
Garrard AP76/G800	£27.95
Garrard AP76/M75-6	£30.25
Garrard AP76/M55E	£30.50
Garrard AP76/M75EJ	£32.50
Garrard AP76/G800E	£30.75
Garrard AP76/M44E	£30.50
Garrard AP76/M75ED	£38.95
B.S.R. McDonald MP60/G800	£17.50
B.S.R. McDonald MP60/M44-7	£19.50
B.S.R. McDonald MP60/M44-E	£20.25
Goldring GL72/G800E	£34.50
Goldring GL75/G800	£39.50
Goldring GL75/G800E	£42.50

**SPECIAL PURCHASE! NEAT G30J STATIC BALANCE PICK-UP ARMS**



Identical specification to NEAT G30 arm but with two-tone chrome and black finish. Complete with head shell, pick up rest and plug in phono leads. BRAND NEW—FULLY GUARANTEED. ONLY £8.95. Post 25p.

**G.W. SMITH & CO (Radio) LTD**

Personal Callers Welcome—All Branches Open 9-6 Mon. to Sat.

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# FM TUNER

NELSON-JONES

Approved parts for this outstanding design (W.W. April 1971/2).  
Featuring 0.75  $\mu$ V sensitivity. Mosfet front end.  
Ceramic I.F. strip. Triple gang tuning.  $\frac{1}{2}$ V r.m.s. output level, suitable for phase locked decoder, as below. Designer's own P.C.B.

THOUSANDS  
NOW IN USE

### FURTHER PRICE REDUCTIONS

Basic Tuner Parts with Screening Box.  
NOW LESS THAN £11.50. Please send S.A.E. lists.

### NEW ALIGNMENT SERVICE

Details on request.

### SOLID STATE TUNING INDICATOR

(W.W. April '72). Tuning is indicated by the balance of two light emitting diodes. The kit includes, LED's, high gain transistors, P.C.B., resistors, mounting kit and instruction booklet. Order T041. Price £1.72 plus P. & P. 10p. with two LED's (or £1.98 with extra LED for "stereo" lamp-see decoder).

### DIAL CHASSIS KIT

Now available—includes all dial drive components, dial plate, decoder mounting bracket, tuning scales, decoder-tuner tagstrips, etc., 4-way 2/3 pole rotary switch and instruction booklet. Price £2.15 plus P. & P. 17p (Note: may be purchased without dial drive components.)

### PHASE-LOCKED STEREO DECODER KIT

Now with free LED "stereo on" light—complementing this superb decoder (W.W. Sept. '70). Suitable for wide variety of tuners including the NELSON-JONES TUNER.  
Complete kit ONLY £7.68. P. & P. 16p.

NEW 1C Stabilised PSU. S/C, overload protected, low ripple. £3.55. P. & P. 19p.

### LIGHT EMITTING DIODES (Red)

Improved efficiency type, mech. identical to HP LED, panel or PCB mounting with free mounting clip—clear or black—please state. Order LED1A. Please add postage. Monsanto miniature PCB mounting with radial leads. Order LED2. Please add postage.  
NOW ONLY 35p each with connection dsta.

### 7 SEGMENT LED Displays. Lowest cost.

0.325" characters with RH dec. point.

ONLY £2.46 each

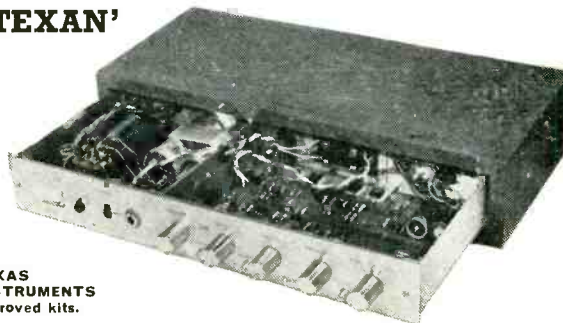
### AERIALS—3 ELEMENT VHF/FM (Outdoor)

A good aerial is essential for optimum Stereo Radio reception.

ONLY £2.60. P. & P. 40p.

Coax 5p/metre. (Masts and Fixing kits available).

## 'TEXAN'



TEXAS  
INSTRUMENTS  
approved kits.

20+20 watts (8 ohms) INTEGRATED STEREO AMPLIFIER. Distortion less than 0.1%. Kit is complete with all metalwork, front panel, knobs, preformed cable/leads. Free TEAK CASE. Chassis size 14 1/2 in. x 6 in. x 2 in. high. (Further details in our lists. S.A.E. please).

ONLY £28.50. Post (U.K.) 45p.

## ELECTRONIC CALCULATORS

Both of our Pocket size calculators feature—

MOS LSI Calculating Chip with 8 Digit Led Display, Overflow and Negative Number Indicators. Leading Zero Suppression.

Full 4 Function—will perform Addition, Subtraction, Multiplication and Division including Chain or Mixed Multiplication or Division as well as true credit balance.

**RAPIDMAN 800.** Calculates in 10 digits and displays to two decimal places. Carrying case £1.45. Mains adaptor £2. Size 5.4 in. x 3.1 in. x 0.9 in. Weight: 7 ozs.

PRICE on application

**MODEL BC806.** Calculates in 12 digits. Decimal point may be either 2, 4, or 6 places or Fully Floating. Last entry cancel. In addition there is a CONSTANT KEY for Input conversion. Size: 6 in. x 3 1/2 in. x 1 1/2 in. Weight 8 ozs. Supplied complete with leather carr. case. Rec. Ret. £59. OUR PRICE £46.00. P. & P. 25p.

Mains adaptor available shortly.

All calculators are fully guaranteed and complete with batteries.

INTEGREX LIMITED, P.O. Box 45, Derby, DE1 1TW

Phone 0283 89 3580

## Contil INSTRUMENT CASES

Type	1 off	5 off	10 off	P&P
755	3.05	2.95	2.90	30p
867/975	3.20	3.15	3.10	30p
1277 white or black panel	3.60	3.45	3.40	40p
1277 unpainted	2.95	2.90	2.80	40p
16127	6.60	6.50	6.40	60p
191010	8.90	8.75	8.60	75p
191010D	12.20	12.10	12.00	120p

Available in a range of seven sizes in 21 gauge Zintec steel with electric blue hammer finish. Front panels are 18 gauge Zintec in white or PVC coated aluminium. Cases supplied with non-slip feet, ex stock by return of post. Please consult catalogue or ask for quote for larger quantities.

WEST HYDE

WEST HYDE DEVELOPMENTS LIMITED, RYEFIELD CRESCENT, NORTHWOOD HILLS, NORTHWOOD, MIDDX. HA6 1NN. Telephone: Northwood 24941/26732. Telex: 923231

WW—086 FOR FURTHER DETAILS

## 'Brightcase'

BRIGHTCASE	1 off	5 off	10 off	P & P
BC21 (3 1/2" Whole Rack)	8.40	8.30	8.20	45p
BC22 (3 1/2" Half Rack)	6.80	6.70	6.60	45p
BC31 (5 1/2" Whole Rack)	10.20	10.10	9.90	45p
BC32 (5 1/2" Half Rack)	8.40	8.30	8.20	45p

Rack Brackets 3 1/2" = 60p per pair. 5 1/2" = 85p per pair. Add "L" for louvres 0.50

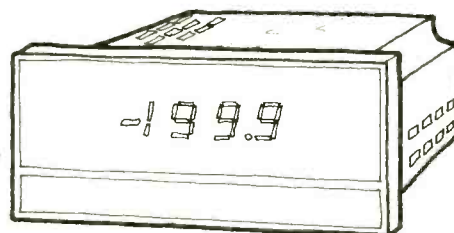
West Hyde present four new instrument cases which can be used as free standing, or as 19 inch rack mounting cases. The cases are constructed from anodised aluminium with contrasting black PVC covered steel panels. Black button headed screws also provide the means of attaching 19 inch mounting brackets and louvred top and bottom panels can be supplied for extra ventilation. Cases are supplied ex stock by return of post.

fully assembled with front and rear panels in anodised aluminium fixed with stainless steel posidriv screws.

WEST HYDE

WEST HYDE DEVELOPMENTS LTD. RYEFIELD CRESCENT, NORTHWOOD HILLS, MIDDX. HA6 1NN. Telephone: Northwood 24941/26732. Telex: 923231 Code: West Hyde Nthwd.

WW—087 FOR FURTHER DETAILS



## I've got a chip on my shoulder

A single 24-pin MOS LSI plug in chip, to be exact.

Which not only contains all the digital logic, polarity sensing logic, over range sensing logic, the comparator to sense threshold crossing, synchronization of the display strobing, storage register, but also replaces up to 16 standard 14-pin TTL packages, giving good reliability and easy servicing. Some chip!

That's not all. I've also got an LED plug-in readout which makes me extremely long-lived though low on power consumption. I only use 2 1/2 watts (mains operated). I'm very strong. My larger upright components are compression mounted, so I can withstand great shock with no damage to my circuit board. You can have me in 3 standard full scale voltage values — and you can change the range on my main printed circuit board. When you order me from Electroplan, they'll send you a handbook with full instructions on how to change my range. If you want a special version of me, just ask for their Application Department and they'll fix you up. So this is the Daystrom 1295 Digital Panel Meter signing off now, and leaving you free to write or ring Electroplan Limited, P O Box 19, Orchard Road, Royston, Herts SG8 5HH. Telephone Royston 41171. At only £77.00 I'm a snip.

Electroplan Ltd is an Electrocomponents Associated Group Company

WW—088 FOR FURTHER DETAILS



Type No.	ADVANCE	Price	Ref. No.
—	Constant Voltage Transformer 3000VA.	£98	385
D/D	R.F. Signal Generator	£45	192/191
P.P.3	Dual Stabilized Power Supply	£55	139/140
<b>AIRMEC</b>			
201	Signal Generator	£98	304
252	Signal Generator	£70	187
775	Bridge Heterodyne Detector	£68	132
761	Frequency Standard	£60	—
C	Ohmmeter	£10	317/8
<b>AVO</b>			
FP 5K	Oscilloscope Camera with Polaroid attachment—suits all Tektronix Scopes.	£160	302
CT38	Electronic Multimeter	£18	—
—	Valve Characteristic Tester	£68	321
<b>BIRTCHEER CORPORATION</b>			
70A	Semiconductor Test Set	£75	322
<b>BROOKDEAL TELESEC</b>			
CR811	Laboratory Chart Recorder 10-0-10mV. Sensitivity; 10 Speeds	£70	324/5/6
<b>CAWKELL</b>			
SO.1	Storage Oscilloscope	£180	49
SO.1	Storage Oscilloscope	£130	50
321	D.C. Voltage Standard. Standard d.c. output from 10uV. to 1000V. in 6 decades. As new condition.	£525	134
<b>CONTROL ELECTRONICS LTD.</b>			
ME-63/U	Phase Monitor 20Hz-20KHz.	£50	319
<b>CINTEL</b>			
36601	Electrolytic Capacitance and Incremental Inductance Bridge 0.1uF-1000uF; 0.01H-100H.	£80	339
<b>COSSOR</b>			
CG.200	Millimicrosecond Pulse Generator	£45	179
CDU 110	Double Beam Oscilloscope DC-20MHz. Brand new, complete with manual.	£300	327
CDU 120	Double Beam Oscilloscope DC-60MHz. Brand new, complete with manual.	£450	332
CDU 130	Mains/Battery Portable Oscilloscope DC-15MHz. Brand new, complete with manual and accessories.	£140	337
CDU 150	Double Beam Oscilloscope DC-35MHz. Brand new complete with manual.	£400	387
1463	Sine/Square Wave Generator	£55	178
<b>DECCA</b>			
MW.14/10	Waveguide to Co-axial line Transformer (Tuneable)	£60	67
MW.40/S	S-Band Oscillator.	£80	252
<b>D.M.A.C.</b>			
ADE2243	X-Y. Plotter	£150	—
<b>EDISWAN</b>			
R.666	L.F. Oscillator	£30	125/126
<b>E.E.V.</b>			
U1000/3/40A	Variable Vacuum Capacitor	£72	—
<b>EDDYSTONE</b>			
770U	Communication receiver	£240	200
<b>E.I.L.</b>			
22B	Micovac Electronic Testmeter	£35	59
33B	Vibron Electrometer	£45	94
44	Multimeter	£20	77/78
<b>ELLIOTT</b>			
P.P.	Voltmeter (Dynamometer) 0-300V, 600V	£25	210
<b>FOSTER</b>			
VRECV	Constant Voltage Transformer 1000V A. 0.25%	£43	358
<b>HEWLETT-PACKARD</b>			
140A	Sampling Oscilloscope complete with Time Base unit type 1425A plus V Amplifier type 1410A. 1Ghz. 1mV/cm. Dual trace	£800	372
684B	Sweep Generator 4-8 Ghz.	P.o.A.	379
940B	Transfer Oscillator	P.o.A.	176
612A	UHF Signal Generator	P.o.A.	177
1780A	Auxiliary Plug-in All brand	£295	—
1782A	Display Scanner new	£295	—
1783A	Plug-in and	£296	—
1783A	Time-Mark generator unused	P.o.A.	297
H05-1751A	Vertical Amp. and Scanner Plug-in unit	£55	182
<b>MARCONI</b>			
TF338A/B	Variable Attenuator	£10	402/11
TF240	Output Power Meter	£25	412
TF801A/1	A.M. Signal Generator 10-310MHz	£65	419
TF887A	Valve Voltmmeter	£30	414
TF1041B	Valve Voltmeter	£35	421
TF1078	UHF Signal Generator	P.o.A.	422
TF1152A	R.F. Power Meter 25W, 500MHz	£35	424/5
TF1245	Circuit Magnification Meter	£65	426
TF1289	V.S.W.R. Indicator	£50	427
TF1291	V.S.W.R. Indicator	£50	428
TF1371	Wideband Millivoltmeter	£45	433
TF1374/1	Crystal Calibrator 100kHz-1500MHz.	£50	434/7
F.M. No. 3	Test Sets Deviation	£130	110
TF.142E	Distortion Factor Meter	£30	98
TF.142F	Distortion Factor Meter	£55	115/148
TF.144G	Standard Signal Generator Mini	£75	251
TF.195M	Beat Frequency Oscillator	£30	46
TF.428C	Valve Voltmeter	£36	15
TF.562/B1	Oscillator-Detector Unit	P.o.A.	281
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TF868/1	Universal Bridge	£60	309/10
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AC126	0-17	AF115	0-24	BC154	0-30	BD176	0-80
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AC128	0-17	AF117	0-24	BC158	0-12	BD178	0-65
AC132	0-14	AF118	0-36	BC159	0-12	BD179	0-70
AC134	0-14	AF124	0-30	BC160	0-45	BD180	0-70
AC137	0-14	AF125	0-25	BC161	0-50	BD185	0-85
AC141	0-14	AF126	0-28	BC167	0-12	BD186	0-65
AC143K	0-17	AF127	0-28	BC168	0-12	BD187	0-70
AC142	0-14	AF159	0-30	BC169	0-12	BD188	0-70
AC142K	0-17	AF178	0-30	BC170	0-12	BD189	0-75
AC151	0-15	AF179	0-50	BC171	0-14	BD190	0-75
AC154	0-20	AF180	0-50	BC172	0-14	BD195	0-85
AC156	0-20	AF181	0-45	BC173	0-14	BD196	0-85
AC166	0-20	AF186	0-45	BC174	0-14	BD198	0-90
AC167	0-24	AF239	0-37	BC175	0-22	BD198	0-90
AC168	0-24	AF102	0-45	BC177	0-19	BD199	0-95
AC168	0-20	AL103	0-65	BC178	0-19	BD200	0-95
AC167	0-20	ASY26	0-25	BC179	0-19	BD205	0-80
AC168	0-24	ASY27	0-30	BC180	0-24	BD206	0-80
AC169	0-14	ASY28	0-25	BC181	0-24	BD207	0-85
AC176	0-20	ASY29	0-25	BC182	0-10	BD208	0-85
AC177	0-24	ASY30	0-25	BC183	0-10	BD210	0-80
AC178	0-28	ASY61	0-25	BC183	0-10	BF115	0-24
AC179	0-28	ASY92	0-25	BC183L	0-10	BF117	0-45
AC180	0-17	ASY94	0-25	BC184	0-12	BF118	0-70
AC180K	0-20	ASY95	0-25	BC184L	0-12	BF119	0-70
AC181	0-17	ASY96	0-25	BC186	0-28	BF121	0-45
AC181K	0-20	ASY97	0-25	BC187	0-28	BF123	0-50
AC187	0-28	ASY98	0-25	BC207	0-11	BF125	0-45
AC187K	0-20	ASZ21	0-40	BC208	0-11	BF127	0-50
AC188	0-22	BC107	0-09	BC209	0-12	BF152	0-55
AC188K	0-20	BC108	0-09	BC212	0-11	BF153	0-45
ACY17	0-25	BC109	0-10	BC213L	0-11	BF154	0-45
ACY18	0-20	BC113	0-10	BC214L	0-14	BF155	0-70
ACY19	0-20	BC114	0-15	BC215	0-10	BF156	0-60
ACY20	0-20	BC115	0-15	BC226	0-35	BF157	0-55
ACY21	0-20	BC116	0-15	BCY30	0-24	BF158	0-55
ACY22	0-16	BC117	0-15	BCY31	0-26	BF159	0-60
ACY27	0-18	BC118	0-10	BCY32	0-30	BF160	0-40
ACY28	0-19	BC119	0-30	BCY33	0-22	BF162	0-40
ACY29	0-55	BC120	0-50	BC121	0-25	BF163	0-45
ACY30	0-28	BC125	0-12	BCY70	0-14	BF164	0-40
ACY31	0-28	BC126	0-18	BCY71	0-18	BF165	0-40
ACY34	0-21	BC132	0-12	BOY72	0-14	BF167	0-22
ACY35	0-21	BC134	0-18	BCZ10	0-20	BF173	0-22
ACY36	0-28	BC135	0-12	BCZ11	0-25	BF176	0-25
ACY40	0-16	BC136	0-15	BC137	0-15	BF177	0-35
ACY41	0-18	BC137	0-15	BD121	0-60	BF178	0-30
ACY44	0-35	BC139	0-40	BD123	0-65	BF179	0-30
AD180	0-38	BO140	0-30	BD124	0-60	BF180	0-30
AD140	0-48	BC141	0-30	BD131	0-50	BF181	0-30
AD142	0-48	BC142	0-30	BD132	0-60	BF182	0-40
AD143	0-30	BC143	0-30	BD133	0-60	BF183	0-40
AD149	0-60	BC145	0-45	BD135	0-40	BF184	0-25
AD181	0-33	BC147	0-10	BD136	0-40	BF185	0-30

BF188	0-40	OC19	0-35	2G371	0-18	2N3219	0-30	2N3054	0-46	2N4059	0-10
BF190	0-40	OC20	0-43	2G373B	0-18	2N3220	0-30	2N3055	0-50	2N4060	0-12
BF195	0-12	OC22	0-38	2G373	0-17	2N3221	0-20	2N3091	0-14	2N4061	0-12
BF196	0-14	OC23	0-42	2G374	0-17	2N3222	0-20	2N3091A	0-16	2N4062	0-12
BF197	0-14	OC24	0-56	2G377	0-30	2N3266	0-17	2N3892	0-14	2N4284	0-17
BF200	0-45	OC25	0-38	2G378	0-18	2N3269	0-14	2N3893	0-14	2N4285	0-17
BF222	0-95	OC26	0-25	2G381	0-16	2N3269A	0-14	2N3894	0-14	2N4286	0-17
BF257	0-45	OC28	0-50	2G382	0-18	2N3241	0-24	2N3895	0-17	2N4287	0-17
BF258	0-60	OC29	0-50	2G401	0-30	2N3242	0-24	2N3896	0-21	2N4288	0-17
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BF262	0-55	OC36	0-50	2G417	0-25	2N2711	0-21	2N3404	0-28	2N4290	0-17
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BF270	0-35	OC42	0-24	2N388A	0-55	2N2714	0-21	2N3414	0-15	2N4292	0-17
BF271	0-30	OC44	0-15	2N404	0-20	2N2904	0-17	2N3415	0-15	2N4293	0-17
BF272	0-50	OC45	0-12	2N404A	0-25	2N2904A	0-22	2N3416	0-28	2N4294	0-12
BF273	0-35	OC70	0-10	2N824	0-42	2N2905	0-21	2N3417	0-28	2N4295	0-12
BF274	0-35	OC71	0-10	2N827	0-42	2N2905A	0-21	2N3425	0-75	2N4568	0-32
BF275	0-60	OC72	0-14	2N598	0-49	2N2906	0-16	2N3426	0-09	2N5459	0-40
BF276	0-27	OC74	0-14	2N599	0-45	2N2906A	0-18	2N3702	0-10	28301	0-40
BF277	0-22	OC75	0-15	2N599A	0-12	2N2907	0-20	2N3703	0-10	28302A	0-40
BF278	0-50	OC76	0-15	2N599B	0-12	2N2907A	0-22	2N3704	0-11	28302B	0-42
BF279	0-22	OC77	0-25	2N599C	0-24	2N2922	0-14	2N3705	0-10	28303	0-55
BF282	0-24	OC81	0-15	2N599D	0-35	2N2924	0-14	2N3706	0-09	28304	0-70
BF283	0-22	OC82	0-15	2N706	0-08	2N2925	0-14	2N3707	0-11	28305	0-84
BF284	0-22	OC82D	0-15	2N706A	0-09	2N2926	0-10	2N3708	0-07	28306	0-84
BF285	0-20	OC83	0-20	2N708	0-12	2N2926 (Y)	0-12	2N3709	0-09	28307	0-84
BF286	0-20	OC84	0-20	2N711	0-30	2N2926 (V)	0-11	2N3710	0-09	28321	0-86
BF287	0-20	OC85	0-20	2N717	0-35	2N2926 (O)	0-10	2N3711	0-09	28322	0-86
BF288	0-22	OC86	0-20	2N718	0-24	2N2926 (R)	0-10	2N3712	0-08	28323	0-86
BF289	0-15	OC87	0-20	2N718A	0-24	2N2926 (B)	0-10	2N3713	0-08	28324	0-86
BF290	0-15	OC88	0-20	2N718B	0-24	2N3010	0-10	2N3714	0-09	28325	0-86
BF291	0-15	OC89	0-20	2N718C	0-24	2N3011	0-14	2N3715	0-07	40361	0-40
BF292	0-15	OC90	0-20	2N718D	0-24	2N3053	0-17	2N4058	0-12	40362	0-40
BF293	0-18	OC92	0-25	2N819	0-21						
BF294	0-18	OC93	0-25	2N819A	0-21						
BF295	0-18	OC94	0-25	2N819B	0-21						
BF296	0-18	OC95	0-25	2N819C	0-21						
BF297	0-18	OC96	0-25	2N819D	0-21						
BF298	0-18	OC97	0-25	2N819E	0-21						
BF299	0-18	OC98	0-25	2N819F	0-21						
BF300	0-18	OC99	0-25	2N819G	0-21						
BF301	0-18	OC100	0-25	2N819H	0-21						
BF302	0-18	OC101	0-25	2N819I	0-21						
BF303	0-18	OC102	0-25	2N819J	0-21						
BF304	0-18	OC103	0-25	2N819K	0-21						
BF305	0-18	OC104	0-25	2N819L	0-21						
BF306	0-18	OC105	0-25	2N819M	0-21						
BF307	0-18	OC106	0-25	2N819N	0-21						
BF308	0-18	OC107	0-25	2N819O	0-21						
BF309	0-18	OC108	0-25	2N819P	0-21						
BF310	0-18	OC109	0-25	2N819Q	0-21						
BF311	0-18	OC110	0-25	2N819R	0-21						
BF312	0-18	OC111	0-25	2N819S	0-21						
BF313	0-18	OC112	0-25	2N819T	0-21						
BF314	0-18	OC113	0-25	2N819U	0-21						
BF315	0-18	OC114	0-25	2N819V	0-21						
BF316	0-18	OC115	0-25	2N819W	0-21						
BF317	0-18	OC116	0-25	2N819X	0-21						
BF318	0-18	OC117	0-25	2N819Y	0-21						
BF319	0-18	OC118	0-25	2N819Z	0-21						
BF320	0-18	OC119	0-25	2N819AA	0-21						
BF321	0-18	OC120	0-25	2N819AB	0-21						
BF322	0-18	OC121	0-25	2N819AC	0-21						
BF323	0-18	OC122	0-25	2N819AD	0-21						
BF324	0-18	OC123	0-25	2N819AE	0-21						
BF325	0-18	OC124	0-25	2N819AF	0-21						
BF326	0-18	OC125	0-25	2N819AG	0-21						
BF327	0-18	OC126	0-25	2N819AH	0-21						
BF328	0-18	OC127	0-25	2N819AI	0-21						
BF329	0-18	OC128	0-25	2N819AJ	0-21						
BF330	0-18	OC129	0-25	2N819AK	0-21						
BF331	0-18	OC130	0-25	2N819AL	0-21						
BF332	0-18	OC131	0-25	2N819AM	0-21						
BF333	0-18	OC132	0-25	2N819AN	0-21						
BF334	0-18	OC133	0-25	2N819AO	0-						



# -the lowest prices!

## 74 Series T.T.L. I.C.'S

BI-PAK STILL LOWEST IN PRICE FULL SPECIFICATION GUARANTEED. ALL FAMOUS MANUFACTURERS



1			25			100+			1			25			100+		
SN7400	0.15	0.14	0.12	SN7450	0.15	0.14	0.12	SN74123	£2.80	£2.70	£2.60	SN74123	£2.80	£2.70	£2.60		
SN7401	0.15	0.14	0.12	SN7451	0.15	0.14	0.12	SN74141	0.67	0.64	0.58	SN74141	0.67	0.64	0.58		
SN7402	0.15	0.14	0.12	SN7453	0.15	0.14	0.12	SN74145	£1.50	£1.40	£1.30	SN74145	£1.50	£1.40	£1.30		
SN7403	0.15	0.14	0.12	SN7454	0.15	0.14	0.12	SN74160	£3.00	£2.70	£2.50	SN74160	£3.00	£2.70	£2.50		
SN7404	0.15	0.14	0.12	SN7460	0.15	0.14	0.12	SN74131	£1.00	0.95	0.90	SN74131	£1.00	0.95	0.90		
SN7405	0.15	0.14	0.12	SN7470	0.29	0.28	0.24	SN74135	£1.20	£1.10	£1.00	SN74135	£1.20	£1.10	£1.00		
SN7406	0.35	0.31	0.28	SN7472	0.29	0.28	0.24	SN74134	£1.80	£1.70	£1.60	SN74134	£1.80	£1.70	£1.60		
SN7407	0.35	0.31	0.28	SN7473	0.37	0.35	0.32	SN74155	£1.40	£1.30	£1.20	SN74155	£1.40	£1.30	£1.20		
SN7408	0.18	0.17	0.16	SN7474	0.37	0.35	0.32	SN74156	£1.40	£1.30	£1.20	SN74156	£1.40	£1.30	£1.20		
SN7409	0.18	0.17	0.16	SN7475	0.45	0.43	0.42	SN74157	£1.90	£1.80	£1.70	SN74157	£1.90	£1.80	£1.70		
SN7410	0.15	0.14	0.12	SN7476	0.40	0.39	0.38	SN74160	£1.80	£1.70	£1.60	SN74160	£1.80	£1.70	£1.60		
SN7411	0.25	0.24	0.23	SN7480	0.67	0.64	0.58	SN74161	£1.60	£1.50	£1.40	SN74161	£1.60	£1.50	£1.40		
SN7412	0.35	0.31	0.28	SN7481	£1.20	£1.15	£1.10	SN74182	£4.00	£3.75	£3.50	SN74182	£4.00	£3.75	£3.50		
SN7413	0.29	0.28	0.24	SN7482	0.87	0.86	0.85	SN74163	£4.00	£3.75	£3.50	SN74163	£4.00	£3.75	£3.50		
SN7414	0.43	0.40	0.38	SN7483	£1.10	£1.05	0.95	SN74164	£2.20	£2.15	£2.10	SN74164	£2.20	£2.15	£2.10		
SN7417	0.43	0.40	0.38	SN7484	£1.00	0.95	0.90	SN74165	£2.25	£2.20	£2.15	SN74165	£2.25	£2.20	£2.15		
SN7420	0.15	0.14	0.12	SN7485	£3.00	£3.00	£3.00	SN74166	£3.50	£3.25	£3.00	SN74166	£3.50	£3.25	£3.00		
SN7422	0.50	0.48	0.45	SN7486	0.32	0.31	0.30	SN74174	£2.30	£2.20	£2.10	SN74174	£2.30	£2.20	£2.10		
SN7423	0.50	0.48	0.45	SN7489	£5.00	£5.00	£5.00	SN74175	£1.60	£1.50	£1.40	SN74175	£1.60	£1.50	£1.40		
SN7425	0.50	0.48	0.45	SN7490	0.67	0.64	0.58	SN74178	£2.50	£2.40	£2.30	SN74178	£2.50	£2.40	£2.30		
SN7427	0.45	0.42	0.40	SN7491	£1.00	0.95	0.90	SN74177	£2.50	£2.40	£2.30	SN74177	£2.50	£2.40	£2.30		
SN7428	0.70	0.65	0.60	SN7492	0.67	0.64	0.58	SN74180	£2.00	£1.80	£1.60	SN74180	£2.00	£1.80	£1.60		
SN7430	0.15	0.14	0.12	SN7493	0.67	0.64	0.58	SN74181	£5.50	£5.00	£4.75	SN74181	£5.50	£5.00	£4.75		
SN7432	0.45	0.42	0.40	SN7494	0.77	0.74	0.68	SN74182	£2.00	£1.80	£1.60	SN74182	£2.00	£1.80	£1.60		
SN7433	0.80	0.75	0.70	SN7495	0.77	0.74	0.68	SN74184	£2.50	£2.25	£2.00	SN74184	£2.50	£2.25	£2.00		
SN7437	0.64	0.62	0.60	SN7496	£2.00	£1.95	£1.90	SN74185	£1.95	£1.90	£1.85	SN74185	£1.95	£1.90	£1.85		
SN7438	0.84	0.82	0.80	SN74100	£1.65	£1.60	£1.55	SN74191	£1.90	£1.85	£1.80	SN74191	£1.90	£1.85	£1.80		
SN7440	0.15	0.14	0.12	SN74104	0.97	0.94	0.88	SN74192	£1.95	£1.90	£1.85	SN74192	£1.95	£1.90	£1.85		
SN7441	0.67	0.64	0.58	SN74105	0.97	0.94	0.88	SN74193	£2.00	£1.80	£1.75	SN74193	£2.00	£1.80	£1.75		
SN7442	0.67	0.64	0.58	SN74107	0.40	0.38	0.36	SN74194	£2.70	£2.60	£2.50	SN74194	£2.70	£2.60	£2.50		
SN7443	£1.30	£1.25	£1.20	SN74110	0.55	0.53	0.50	SN74195	£2.00	£1.90	£1.80	SN74195	£2.00	£1.90	£1.80		
SN7444	£1.30	£1.25	£1.20	SN74111	0.95	£1.15	£1.10	SN74196	£1.90	£1.70	£1.60	SN74196	£1.90	£1.70	£1.60		
SN7445	£1.80	£1.77	£1.75	SN74118	£1.00	0.95	0.90	SN74197	£1.80	£1.70	£1.60	SN74197	£1.80	£1.70	£1.60		
SN7446	0.97	0.94	0.88	SN74119	£1.35	£1.25	£1.10	SN74198	£5.50	£5.00	£4.50	SN74198	£5.50	£5.00	£4.50		
SN7447	£1.00	0.97	0.95	SN74121	0.40	0.37	0.34	SN74199	£5.50	£5.00	£4.50	SN74199	£5.50	£5.00	£4.50		
SN7448	£1.00	0.97	0.95	SN74122	£1.40	£1.30	£1.10										

## The AL50 HI-FI AUDIO AMPL 50W pk 25w (RMS)

0.1% DISTORTION! HI-FI AUDIO AMPLIFIER

- Frequency Response 15Hz to 100,000—1dB.
- Load—3, 4, 8 or 16 ohms. • Supply voltage 10-35 Volts.
- Distortion—better than 0.1% at 1kHz.
- Signal to noise ratio 80dB.
- Overall size 63 mm x 105 mm x 13 mm.

Tailor made to the most stringent specifications using top quality components and incorporating the latest solid state circuitry conceived to fill the need for all your A.F. amplification needs. FULLY BUILT—TESTED—GUARANTEED.

BRITISH MADE. only £3.25 each



## STABILISED POWER MODULE SPM80

£2.95

AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (r.m.s.) per channel simultaneously. This module embodies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer MT80, the unit will provide outputs of up to 1.5 amps at 55 volts. Size: 63 mm x 105 mm x 20 mm. These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including: Discos Systems, Public Address, Intercom Units, etc. Handbook available, 10p.

TRANSFORMER BMT80 £1.95 p. & p. 25p

## NUMERICAL INDICATOR TUBES



MODEL	CD66	GR114	3015F Mhiltrom
Anode voltage (Vdc)	170min	175min	3
Cathode Current (mA)	2-3	14	8
Numerical Height (mm)	18	13	9
Tube Height (mm)	47	32	22
Tube Diameter (mm)	19	13	12 wide
I.C. Driver Rec.	BP41/14 141	BP41 or 141	BP47
PRICE EACH	£1.70	£1.55	£1.90

All indicators 0-9 - Decimal point. All side viewing. Full data for all types available on request.

## STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO MONO switch, volume, balance and continuously variable bass and treble controls.

### SPECIFICATION:

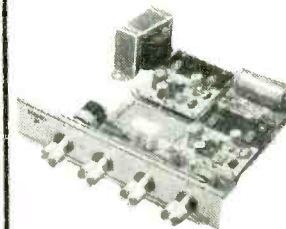
Frequency response	20Hz—20kHz ±1dB	Bass control	±15dB at 20Hz
Harmonic distortion	better than 0.1%	Treble control	±15dB at 20kHz
Inputs: 1. Tape head	1.25mV into 50KΩ	Filters: Rumble (high pass)	100 Hz
2. Radio, Tuner	35mV into 50KΩ	Scratch (low pass)	8kHz
3. Magnetic P.U.	1.5mV into 50KΩ	Signal/noise ratio	better than +65dB
All input voltages are for an output of 250mV.		Input overload	+26dB
Tape and P.U. inputs equalised to RIAA curve within ±1dB from 20Hz to 20kHz.		Supply	+35 volts at 20mA
		Dimensions	292 x 82 x 25 mm

SPECIAL COMPLETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT80 & 1 PA100 ONLY £23.00 FREE p. & p

only £11.95

## The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm x 14 cm x 5.5 cm. This compact unit comes complete with on/off switch, volume control, balance, bass and treble controls. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet.



Output power 20w peak  
Freq. res. 20Hz-25kHz  
Harmonic distortion typically 0.25% at 1 watt  
Input 1 (Cer.) 300mV into 1M  
Input 2 (Aux.) 4mV into 30K  
Bass control ±12dB at 60Hz  
Treble control ±14dB at 14kHz

£12.25 free p. & p.

## NEW COMPONENT PAK BARGAINS

Pack No.	Qty.	Description	Price
C 1	250	Resistors mixed values approx. count by weight	0.50
C 2	200	Capacitors mixed values approx. count by weight	0.50
C 3	50	Precision Resistors 1%, mixed values	0.50
C 4	75	1/4 W Resistors mixed preferred values	0.50
C 5	5	Pieces assorted Ferrite Rods	0.50
C 6	2	Tuning Gangs, MW/LW/VHF	0.50
C 7	1	Pack Wire 50 metres assorted colours	0.50
C 8	10	Reed Switches	0.50
C 9	3	Micro Switches	0.50
C 10	15	Assorted Pots & Pre-sets	0.50
C 11	5	Jack Sockets 3 x 3.5mm 2 x Standard Switch Types	0.50
C 12	40	Paper Condensers preferred types mixed values	0.50
C 13	20	Electrolytics Trans. types	0.50
C 14	1	Pack assorted Hardware—Nuts/Bolts, Grommets etc.	0.50
C 15	4	Main Toggle Switches, 2 Amp D/P	0.50
C 16	20	Assorted Tag Strips & Panels	0.50
C 17	10	Assorted Control Knobs	0.50
C 18	4	Rotary Wave Change Switches	0.50
C 19	3	Relays 6—24V Operating	0.50
C 20	4	Sheets Copper Laminate approx. 10" x 7"	0.50

Please add 10p post and packing on all component packs, plus a further 10p on pack Nos. C1, C2, C19, C20.

## LINEAR I.C.'S—FULL SPEC.

Type No.	Price	1-24	25-99	100 up
BP 201C	81.201C	83p	53p	45p
BP 701C	81.701C	83p	50p	45p
BP 702C	81.702C	83p	50p	45p
BP 709	72.709	38p	34p	30p
BP 709P	72.709P	36p	34p	30p
BP 710	72.710	42p	42p	40p
BP 711	72.711	45p	43p	40p
BP 712	72.712	75p	60p	50p
BP 703C	74.703C	28p	26p	24p
TAA 293		70p	60p	55p
TAA 298		90p	75p	70p
TAA 350		170p	158p	150p

## ROCK BOTTOM PRICES LOGIC DTL 930 Series I.C.'s

Type No.	Price	1-24	25-99	100 up
BP930		12p	11p	10p
BP932		13p	12p	11p
BP933		13p	12p	11p
BP935		13p	12p	11p
BP936		13p	12p	11p
BP944		13p	12p	11p
BP945		25p	24p	22p
BP946		12p	11p	10p
BP948		25p	24p	22p
BP951		65p	60p	55p
BP982		12p	11p	10p
BP993		40p	38p	35p
BP994		40p	38p	35p
BP997		40p	38p	35p
BP999		40p	38p	35p

Devices may be mixed to quantity or price. Larger quantities on application. (DTL 930 Series only).

## SYSTEM 12 STEREO

Each Kit contains two Amplifier Modules, 3 watts RMS, two loudspeakers, 15 ohms, the pre-amplifier, transformer, power supply module, front panel and other accessories, as well as an illustrated stage-by-stage instruction booklet designed for the beginner.

ONLY £16.95 FREE p. & p.

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P.O. BOX



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### 20 + 20 WATT INTEGRATED I.C. STEREO AMPLIFIER

★ FREE TEAK CABINET with complete kits!

**FEATURES.** New sllm design with 6 - IC's, IC sockets, 10 silicon transistors, 4 rectifiers, 2 zeners. Special Gardeners low field sllm line transformer. Fibre glass PC panel. Complete chassis work.

**HIGH QUALITY & STABILITY ARE PREDOMINATE FEATURES** - DEVELOPED BY TEXAS ENGINEERS FOR PERFORMANCE, RELIABILITY AND EASE OF CONSTRUCTION.

**FACILITIES.** On/off switch indicator, headphone socket, separate treble, bass, volume and balance controls, scratch-removable filters, mono/stereo switch, input selector, Mag. P.U. Radio Tuner, Aux. Can be altered for Mic. Tape, Tape-head, etc. (Parts list Ref. 20 on request). Constructional details (ref no 21) 30p.



SPECIAL KIT PRICE

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(As featured in "Practical Wireless" May to August 1972)

★ SLIM DESIGN WITH SILVER TRIM Overall chassis size 14 1/2" x 6" x 2" high

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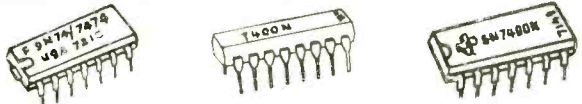
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SN7402	20p	18p	16p	SN7454	20p	18p	16p	SN74162	22-80	22-40	22-25
SN7403	20p	18p	16p	SN7455	20p	18p	16p	SN74163	22-80	22-40	22-25
SN7404	20p	18p	16p	SN7456	20p	18p	16p	SN74164	22-80	22-40	22-25
SN7405	20p	18p	16p	SN7457	20p	18p	16p	SN74165	22-80	22-40	22-25
SN7406	20p	18p	16p	SN7458	20p	18p	16p	SN74166	22-80	22-40	22-25
SN7407	20p	18p	16p	SN7459	20p	18p	16p	SN74167	22-80	22-40	22-25
SN7408	20p	18p	16p	SN7460	20p	18p	16p	SN74168	22-80	22-40	22-25
SN7409	20p	18p	16p	SN7461	20p	18p	16p	SN74169	22-80	22-40	22-25
SN7410	20p	18p	16p	SN7462	20p	18p	16p	SN74170	22-80	22-40	22-25
SN7411	20p	18p	16p	SN7463	20p	18p	16p	SN74171	22-80	22-40	22-25
SN7412	20p	18p	16p	SN7464	20p	18p	16p	SN74172	22-80	22-40	22-25
SN7413	20p	18p	16p	SN7465	20p	18p	16p	SN74173	22-80	22-40	22-25
SN7414	20p	18p	16p	SN7466	20p	18p	16p	SN74174	22-80	22-40	22-25
SN7415	20p	18p	16p	SN7467	20p	18p	16p	SN74175	22-80	22-40	22-25
SN7416	20p	18p	16p	SN7468	20p	18p	16p	SN74176	22-80	22-40	22-25
SN7417	20p	18p	16p	SN7469	20p	18p	16p	SN74177	22-80	22-40	22-25
SN7418	20p	18p	16p	SN7470	20p	18p	16p	SN74178	22-80	22-40	22-25
SN7419	20p	18p	16p	SN7471	20p	18p	16p	SN74179	22-80	22-40	22-25
SN7420	20p	18p	16p	SN7472	20p	18p	16p	SN74180	22-80	22-40	22-25
SN7421	20p	18p	16p	SN7473	20p	18p	16p	SN74181	22-80	22-40	22-25
SN7422	20p	18p	16p	SN7474	20p	18p	16p	SN74182	22-80	22-40	22-25
SN7423	20p	18p	16p	SN7475	20p	18p	16p	SN74183	22-80	22-40	22-25
SN7424	20p	18p	16p	SN7476	20p	18p	16p	SN74184	22-80	22-40	22-25
SN7425	20p	18p	16p	SN7477	20p	18p	16p	SN74185	22-80	22-40	22-25
SN7426	20p	18p	16p	SN7478	20p	18p	16p	SN74186	22-80	22-40	22-25
SN7427	20p	18p	16p	SN7479	20p	18p	16p	SN74187	22-80	22-40	22-25
SN7428	20p	18p	16p	SN7480	20p	18p	16p	SN74188	22-80	22-40	22-25
SN7429	20p	18p	16p	SN7481	20p	18p	16p	SN74189	22-80	22-40	22-25
SN7430	20p	18p	16p	SN7482	20p	18p	16p	SN74190	22-80	22-40	22-25
SN7431	20p	18p	16p	SN7483	20p	18p	16p	SN74191	22-80	22-40	22-25
SN7432	20p	18p	16p	SN7484	20p	18p	16p	SN74192	22-80	22-40	22-25
SN7433	20p	18p	16p	SN7485	20p	18p	16p	SN74193	22-80	22-40	22-25
SN7434	20p	18p	16p	SN7486	20p	18p	16p	SN74194	22-80	22-40	22-25
SN7435	20p	18p	16p	SN7487	20p	18p	16p	SN74195	22-80	22-40	22-25
SN7436	20p	18p	16p	SN7488	20p	18p	16p	SN74196	22-80	22-40	22-25
SN7437	20p	18p	16p	SN7489	20p	18p	16p	SN74197	22-80	22-40	22-25
SN7438	20p	18p	16p	SN7490	20p	18p	16p	SN74198	22-80	22-40	22-25
SN7439	20p	18p	16p	SN7491	20p	18p	16p	SN74199	22-80	22-40	22-25
SN7440	20p	18p	16p	SN7492	20p	18p	16p				
SN7441	20p	18p	16p	SN7493	20p	18p	16p				
SN7442	20p	18p	16p	SN7494	20p	18p	16p				
SN7443	20p	18p	16p	SN7495	20p	18p	16p				
SN7444	20p	18p	16p	SN7496	20p	18p	16p				
SN7445	20p	18p	16p	SN7497	20p	18p	16p				
SN7446	20p	18p	16p	SN7498	20p	18p	16p				
SN7447	20p	18p	16p	SN7499	20p	18p	16p				
SN7448	20p	18p	16p	SN7500	20p	18p	16p				
SN7449	20p	18p	16p								
SN7450	20p	18p	16p								
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SN7460	20p	18p	16p								
SN7461	20p	18p	16p								
SN7462	20p	18p	16p								
SN7463	20p	18p	16p								
SN7464	20p	18p	16p								
SN7465	20p	18p	16p								
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SN7498	20p	18p	16p								
SN7499	20p	18p	16p								
SN7500	20p	18p	16p								

PRICES OF 7400 SERIES ARE CALCULATED ON THE TOTAL NUMBER ORDERED REGARDLESS OF MIX. LARGER QUANTITY PRICES PHONE 01-402 4891. TEXAS HANDBOOK No. 21C. 700 PAGES DATA 60p. POST 20p.

IC SOCKETS 16 lead 17p 14 lead 15p 8 lead 15p

## TEST EQUIPMENT

- SE250B Pocket Pencil Signal Injector £1.90
- SE500 Pocket Pencil Signal Tracer £1.50
- THL33D Robust 2K/Volt £4.55. With case £4.95
- TE15 Grid Dip Meter 440 KHz-230 MHz £13.45
- 500 30 K/V Multimeter £9.25
- 200H With leather case £10.50
- 20 K/V Multimeter £4.20. With case £9.50
- AF105 50 K/V Multimeter £8.50.
- U4341 A.C.D.C. Multimeter with transistor tester. Steel case £10.50
- TE20D RF Generator 120KHz-500MHz £15.95 Carr. 35p
- TE22D Audio Generator 20Hz-200KHz £17.50 Carr. 35p
- C1-5 3" Pulse Scope 10Hz-10MHz £39.00 Carr. 50p
- TE65 Valve Voltmeter 28 ranges £17.50 Carr. 40p.

ALL NONBREAD MODELS IN STOCK

**"BANDSPREAD" PORTABLE MW/LW TUNER**

To build MW/LW Superhet Radio using Mullard RF/IF Module, 600mW o/p. Fibre glass cabinet. All parts £7.98. P. & P. 82p. (Battery 22p extra.)

ML3 - Superhet MW/LW radio Tuner to build S/M Tuning. Mullard Module etc. ALL PARTS £4.85. P. & P. 15p.

ALL PARTS SOLD SEPARATELY

VISIT OUR NEW ELECTRONICS STORE, 404-406 EDGWARE ROAD, W.2.

## 7 SEG & NIXIE TUBES

(Post 15p per 1 to 6)

XN3, XN13, GN6 0-9 side view with data. 85p.

GNP-7, GNP-8 0-9 side view with decimal points and data. 95p.

3015F 7 seg. £2 each. £7 per 4 with data.

12 and 24 hour clock circuits. Ref. No. 31 15p.

## ULTRASONIC TRANSDUCERS

Operate at 40Kc/s up to 100 yds. Ideal remote switching and signalling. Complete with data and circuits. PRICE PER PAIR £5-90. Post 10p.

## QUALITY SLIDER CONTROLS

60mm stroke singles and ganged. Complete with knobs. 5kΩ, 10kΩ, 25kΩ, 100kΩ, 250kΩ, 500kΩ, 1 meg. Log and n. 40p each. 10kΩ, 25kΩ, 50kΩ, 100kΩ, 250kΩ, Log and Lin ganged. 60p each.

## MARRIOTT TAPE HEADS

4 TRACK MONO or 2 TRACK STEREO

- "117" High Impedance £2-00
- "118" Med. Impedance £2-00
- "36" Med.-Low Imp. £3-50

Erase Heads for above 75p

- "63" 2 track mono-High Impedance £1-75
- "43" Erase Head for above 75p.





**MINIATURE WAFER SWITCHES**

2 pole, 2 way—4 pole, 2 way—2 pole, 3 way—4 pole, 3 way—2 pole, 4 way—3 pole, 4 way—2 pole, 6 way, 1 pole, 12 way. All at 20p each; ten for £1.80, your assortment.

**TOGGLE SWITCHES**

Metal, all standard types with metal dolly 240v, 3 amp. ST, ST 15p SP, DT, 20p DP, ST 20p DP, DT, 25p less 10% for ten of same type.

**ROCKER SWITCH**

13 amp self-fixing into an oblong hole. Size approximately 1in. x 1/2in., 8p each, 10 for 72p.



**SLIDE SWITCHES**

Slide Switch, 2 pole change over pane mounting by two 6 BA screws. Size approx. 1" x 3/4" rated 250v lamp. 7p each, 10 for 65p. Ditto as above but for printed circuit 8p each, 10 for 54p. Sub Miniature Slide Switch, DPDT 10mm (1/2" approx.) between fixing centres, 12p each or 10 for £1.08.



**DOUBLE LEAF CONTACT**

Very slight pressure closes both contacts. 7p each, 10 for 65p. Plastic push-rod suitable for operating. 5p each, 45p for 10

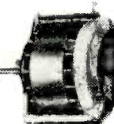
**LIGHT CELL**

Almost zero resistant in sunlight increases to 10 K. Ohms in dark or dull light. epoxy resin sealed. Size approx. 1 in. dia. by 1/4 in. thick. Rated at 500 MW. wire ended. 55p. Suit most circuits.



**PAPST MOTORS**

Est. 1/20th h.p. Made for 110-120 volt working, but two of these work ideally together or a larger quantity may be packed into a square solenoid. Rating 1A 200V. Price 80p each, £3 per dozen. Small ceramic magnets to operate these reed switches 9p each, 90p dozen. Flat, flat type, 2" long, just over 1/8" thick, flattened out, so that it can be fitted into a smaller space or a larger quantity may be packed into a square solenoid. Rating 1A 200V. Price 80p each, £3 per dozen. Small ceramic magnets to operate these reed switches 9p each, 90p dozen. Dry Reed Relays. Solenoids on moulded bobbins within magnetic shields—printed circuit or panel mounting.



**LUMINOUS CORD SWITCHES**

Double pole with neon led into side so luminous in dark. Ideal for dark room light or for use with waterproof element—new plastic case. 25p, 10 for £2.25 3 heat model 38p 10 for £3.42.



**REED SWITCHES**

Glass encased, switches operated by external magnet—gold welded contacts. We can now offer 3 types: Miniature, 1" long x approximately 1/8" diameter. Will make and break up to 300V. Price 13p each, £1.20 doz. Standard, 2" long x 1/4" diameter. This will break currents of up to 1A, voltage up to 250V. Price 10p each, 90p per dozen. Flat, flat type, 2" long, just over 1/8" thick, flattened out, so that it can be fitted into a smaller space or a larger quantity may be packed into a square solenoid. Rating 1A 200V. Price 80p each, £3 per dozen. Small ceramic magnets to operate these reed switches 9p each, 90p dozen. Dry Reed Relays. Solenoids on moulded bobbins within magnetic shields—printed circuit or panel mounting.

Ref.	Coil Resistance	Normally open	Reed Switches	Price
71005	2 K	1 normally open		25p
81916	5 K	1 normally open, 1 normally closed		75p
05003	4 K	1 normally open		25p
62040	1500 & 500 ohms	1 normally open		35p



**DRILL CONTROLLER**

New 1kW model. Electronically changes speed from approximately 10 revs. to maximum. Full power at all speeds by finger-rip control. Kit includes all parts, case, everything and full instructions £1.50, plus 13p post and insurance. Made up model also available £2.25 plus 13p p. & p.

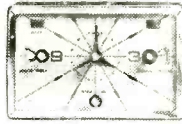
**BAKELITE INSTRUMENT CASE**

Size approx. 6 1/2" x 3 1/2" x 2" deep with brass inserts in four corners and bakelite panel. This is a very strong case suitable to house instruments and special rigs, etc. Price 45p each.



**15A ELECTRICAL PROGRAMMER**

Learn in your sleep! Have radio playing and kettle boiling as you awake—switch on lights to warn off intruders—have warm house to come home to. All these and many other things you can do if you invest in an electrical programmer. Clock by famous maker with 15 amp, on/off switch. Switch on time can be set anywhere to stay on up to 6 hours. Independent 60 minute memory logger. A beautiful unit. Price £1.95 + 20p p. & p. or with glass front chrome bezel 75p extra.



**WATERPROOF HEATING ELEMENT**

26 yards length 70W. Self-regulating temperature control. 50p post free.



**0-8 AMMETER**

2 in. square full vision for flush mounting. Moving iron instrument. Ideal for charger. Price 60p each, 10 for £5.40.

**HIGH ACCURACY THERMISTAT**

Uses differential comparator I.C. with thermistor as probe. Designer claims temperature control to within 1/7th of a degree. Complete kit with power pack £5.50.



**TREASURE TRACER**

Complete kit (except wooden battery) to make the metal detector as the circuit in Practical Wireless August issue. £2.95 plus 20p post and insurance.

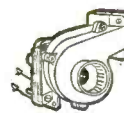


**NUMICATOR TUBES**

For digital instruments, counters, timers clocks, etc. Hi-vac XN. 3. Price 99p each 10 for 99.

**CENTRIFUGAL BLOWER**

Miniature mains driven blower centrifugal type blower unit by Woods, powerful but specially built for quiet running—driven by cushioned induction motor with specially built low noise bearings. Overall size of blower is approx. 4 1/2" x 4 1/2" x 4". When mounted by its flange air is blown into the equipment but to suck air out mount it from the centre using a clamp, ideal for cooling electrical equipment, or fitting into a cooker hood, film drying cabinet or for removing fume smoke when soldering etc., etc. A real bargain at £1.85.



**MULLARD I.F. MODULE**

This is a fully screened intermediate frequency module for amplification and detection of f.m. signals at 10.7MHz and a.m. signals at 470KHz. The first stage is used as an i.f. amplifier for f.m. and a self-oscillating mixer for a.m. operation, in conjunction with an external oscillator coil. 85p each, 10 for £7.85, 100 for £62.50. With connection dig.



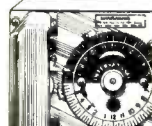
**TANGENTIAL HEATER UNIT**

This heater unit is the very latest type, most efficient and quiet running. Is as fitted in Hoover and blower heaters costing £14 and more. We have a few only. Comprises motor, impeller, 2kW. element and 1kW. element allowing switching 1, 2 and 3kW. and with thermal safety cut-out. Can be fitted into any metal line case or cabinet. Only needs control switch. £3.50, 2kW. Model as above except 2kW. £2.50. Don't miss this. Control Switch 35p. P. & P. 10p.



**ELECTRIC TIME SWITCH**

Made by Smiths these are A.C. mains operated. NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be built into box with 13A socket. 2 completely adjustable time periods per 24 hours, 5 amp changeover contacts will switch circuit on or off during these periods. £2.50 post and ins., 23p. Additional time contacts 50p pair.



**COMPUTER TAPE**

2,400ft. of the Best Magnetic Tape money can buy—users claim good results with Video and sound. 1in. wide £1.00 plus 33p post and insurance. With cassette. 1/2in. wide £1.00 plus 30p post and insurance with cassette. 1/4in. wide 85p plus 25p post and insurance with cassette. Spare spools and cassettes—1in. 75p, 1/2in. 75p each plus 20p post and insurance.



**THIS MONTH'S SNIP**

**MULLARD 4 WATT AMPLIFIER EP 9000**  
Suitable for mono or stereo systems. Its output approx. 4w. speech or music into a 12-15 ohm speaker. Power requirements 24 volts 10 watts. Harmonic distortion at typical listening level is less than 2%. Frequency response at typical listening level 50hz. to 10kHz, totally enclosed in moulded case size 3 1/4 x 2 1/4 x 1 1/4in. with screw terminal connections—a fantastic bargain at only £1.45 while stocks last. Don't miss this—it's one of our best bargains ever.

**FREE DO-IT-YOURSELF STEREO HANDBOOK**

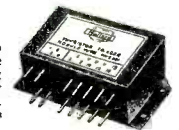
**ERGOTROL UNITS**

These units made by the Mullard Group are for operating and controlling d.c. Motors and equipment from A.C. mains. Thyristors are used and these supply a variable d.c. resulting in motor speed control and operating efficiency far superior to most other methods. The units are contained in wall mounting cabinets with front control panel on which are fuses—push buttons for on/off and the variable thyristor firing control. 4 models are available—all are brand new in makers cases:  
Model 2410 for up to 5 amps £17.50  
Model 2411 for up to 10 amps £27.50



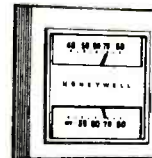
**MULLARD THYRISTOR TRIGGER MODULE**

This produces pulses for phase control triggering. It has two isolated out-puts, so one thyristor or two thyristors (in separate arms of bridge) can be controlled by one module. The timing circuit is synchronised to the mains frequency and control is by an external variable resistor or from a voltage or current source. Provision is made for feedback where automatic control is required. Price £4.50 each or 10 for £40.00.



**THERMOSTAT WITH THERMOMETER**

Made by Honeywell for normal air temperatures 40°-80°F. (5-25°C). This is a precision instrument with a differential which can be adjusted to better than 1.5°F. A mercury switch breaks on temp. rise—the switch is operated by coiled bi-metal element and an adjustable heater is incorporated for heat anticipation. Elegantly styled and e-cased in an ivory plastic case with clear plastic windows, thermometer above and switch setting scale below. Size approx. 3 3/8" x 3 1/2" x 1 1/4" deep. Can be mounted on conduit box or directly on wall. Price £1.25 each or 10 for £11.25.



**HORSTMANN "TIME & SET" SWITCH**

(A 30 Amp Switch.) Just the thing if you want to come home to a warm house without it costing you a fortune. You can delay the switch on time of your electric fires, etc., up to 14 hours from setting time or you can use the switch to give a boost on period of up to 3 hours. Equally suitable to control processing. Regular price probably around £5. Special snip price £1.50. Post and ins. 23p.



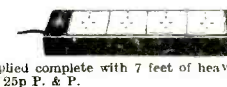
**RADIO STETHOSCOPE**

Easiest way to fault find—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio, TV, amplifier, anything—complete kit comprises two special transistors and all parts including probe tube and crystal earpiece. £2. twin stethoscopes instead of earpiece 75p extra—post and ins. 20p.



**DISTRIBUTION PANELS**

Just what you need for work bench or lab, 4 x 13 amp sockets in metal box to take standard 13 amp fused plugs and on/off switch with neon warning light. Supplied complete with 7 feet of heavy cable. Wired up ready to work. £2.25 less plug; plus 25p P. & P.



**MULLARD AUDIO AMPLIFIERS**

All in module form, each ready built complete with heat sinks and connection tabs, data supplied.  
Model 1153 500mW power output 65p.  
Model 1172 750mW power output 85p.  
Model 124000 4 watt power output £1.45.  
EP9001 1/2in. channel or stereo per amp. £1.80.  
10% discount if 10 or more ordered.



**NEW ITEMS THIS MONTH**

**CAR PANEL SWITCH.** Our Ref. No. 901. Arcos made. Has long flat ended toggle black and chrome finish. Rated 2A. at 250v. and is double pole on/off. Listed at 45p. Our price 22p each.

**CAR PANEL AUTO. SWITCH.** Ref. No. 903. Again a flat ended toggle. Made by Arrow. A 3 position double pole change over switch centre off for auto aerials, reversing motors etc. 30p each.

**3 PIN PLUG AND SOCKET.** Our Ref. No. PS01. Flat pins, American style rated at 10A. 250v. Socket panel mounting. Plug is white and intended for flex. Useful where non standard power outlet is required. Also suitable for speaker leads, etc., etc. Price 25p per pair.

**3 PIN REVERSE PLUG AND SOCKET.** Our Ref. PS02. For bringing live leads to equipment. All brown bakelite construction, rated 10A. 250v. Price 35p per pair.

**1 R.P.M. MOTOR.** Smiths. 240v. 50 cycle mains working. Ideal motor to drive clock mechanisms. Price £1 each or 10 for £9.

**LIGHT DIMMERS.** We regret that through increased costs our 1kW. model has now to be increased to £2.95.

**LIGHT DIMMER BOX.** Another feature we can supply is box and 13 amp socket. This makes dimmer suitable for control of portable lights and equipment. This price is 45p extra.

**13 AMP JUNCTION BOXES.** Made to take 7029 cables so ideal for ring mains. Price 8p each or 10 for 72p.

**PORCELAIN FUSE AND CARRIER.** 20A. 250v. MEM Ref. No. 151BB 15LR11W. Make your own fuse board. Price 20p per pair.

**AUTO TRANSFORMER.** Primary 220-240v. Secondary 110-120v. Well built and varnish impregnated. 250 watt intermittent rating. 150v. continuous rating. Size approx. 3 1/4 x 3 x 3in. £1 plus 20p post and insurance.

**30KV EBT UNIT.** This unit is self contained and on wheels. It stands approx. 6ft. high and 3ft. square. On the front panel is a Variac, Voltmeter, a 60 second timer as well as the normal overload trip on/off switch and cut outs etc. The transformer itself is oil filled and rated at 7 kVA 30 kV. The Variac is in the primary so all voltages up to 30kV are available. We believe the normal use for such a unit would be a breakdown and flash tester. 1 only—not new but in good order. Price £150. Carriage extra at cost.

**INSTANT START UNITS.** 2in. tubes, Philips or Smart & Brown in a tray complete with tube clips and tube ends. Price £1.50 each or 10 for £13.50.

**SPLIT MOTOR.** 200-250v. Induction Motor. Driving a carter gear box with 1 1/2in. of output drive shaft running at 5 revs. per minute. Intended for roasting chickens etc. suitable for driving models, miniature, coloured disc lighting effect, etc., etc. £1.85 plus 20p post and insurance.

**WIRE ENDED FUSES.** Useful where you want a quick solder-in fuse. Rated 2A. 250v. These are about the size of a resistor. Price 5p each.

**PANEL NEON INDICATOR.** Our Ref. No. P101. Oblong type, self-fixing in oblong hole, suitable for 200/250v. Price 13p each.

**THERMOSTAT WITH PROBE.** Our Ref. No. TH01. Made by Ranco. Range 0-107°C. 16A. 250v. switch. Joined to a 10in. probe by approx. 40in. of capillary tubing. 1 hole fixing. Normal control spindle. 85p each.

**THERMOSTAT WITH PROBE.** Our Ref. No. TH02. As TH01 but the range is 0-120°C and the capillary tube is approx. 46in. long. Price 95p each.

**FLOURESCENT TUBES.** Standard types—Bi pin ends, ideal pelmet lighting as well as for standard replacements—18in. 15 watt. 24in. 40 watt. 36in. 40 watt. 39in. 40 watt. All first grade tubes offered at one price—£3.50 per box of 24—i.e. less than 15p each. If not collecting then please add 50p per box per 200 miles.

**DIGITAL DISPLAY.** Panel mounting unit measuring approx. 3 1/4 x 1 x 1 1/4in. deep. Size of the display aperture is approx. 1 1/4 x 1in. Light up to 0-9. Ex equipment but unused and in perfect order. Price £1 each.

**DIGITAL SWITCHES.** Small 10 type S.T.C. number SW211 or SW212. These are a snap in 6 hole approx. 1 1/4 x 1 1/4in. Knob engraved 0-9. Gold plated contacts 1 pole 10 way. Thumb wheel operation. These are designed so that they may be stacked in rows. Price 75p each.

**6 DIGIT COUNTER.** Operated by 240v. A.C. mains through resistor or direct from 115v. A.C. from 80v. D.C. Made in Westley-Rook at America. Metal encased for surface mounting. Size approx. 3 1/4 x 1 1/4 x 2 1/4in. Price £1 each, 10 for £9.

**COLOURED 13 AMP SOCKETS.** Standard Flush mounting available in the following colours—Yellow, green, grey and red. Use any good quality plastic with porcelain interior made by Ward and Goldstone. Useful on control panels. Price 20p each, 10 for £1.90.

**THROAT MICROPHONES.** Dynamic type. Made for government contract. Many uses: i.e. motor cyclists talking to pillion passengers, under guitar strings, vibration amplifiers etc., etc. Price 30p each, 10 for £2.70.

**REED SWITCH COILS.** These are solenoids wound on moulded formers of the correct shape and dimensions to take standard reed switches. They have printed circuit board mounting. Six types available—RC1 takes 1 reed—Operates 10-15v. 600 ohms. 30p. RC2 takes 2 reeds—Operates 10-15v. 180 ohms. 25p. RC3 takes 1 reed—Operates 15-30v. 1K ohms 32p. RC4 takes 2 reeds—Operates 15-30v. 300 ohms. 45p. RC5 takes 1 reed—Operates 45-70v. 6000 ohms. 35p. RC6 takes 2 reeds—Operates 45-70v. 3500 ohms. 40p. Standard reed switches available 10p each or 10 for 90p 100 for £8.00.

**MINIATURE ROCKER SWITCH.** Our Ref. RS01, 10 amp. 240v. Self-fixing into hole size approx. 1in. x 3/4in. by famous French maker Ruesenburgh. Price 10p each.

**ROCKER SWITCH.** Our Ref. RS02, 13 amp. self fixing into hole approx. 1in. x 3/4in. Made by the Carr Fastener Co. Very reliable. Price 8p.

**PHOTO TRANSISTOR.** OCPT70—ideal for burglar alarms and similar applications. Price 65p each.

**EXIT SIGNS.** One of our customers has pointed out how easily our box signs can be converted to exit signs. These are illuminated having a 20w. fluorescent lamp with associated control gear. The front is very thick, clear plastic. Directly onto this you can stick down the letters available at most stationers. There is room inside the box for a battery and low volt lamp in the case of power failure. Size of sign is 2ft. high x 14in. wide x 5in. deep. Solidly made from sheet steel and hammer finished in enamel. Price £3.50 + 50p carriage per 200 miles.

**MUTUAL INDUCTANCE COIL.** Laboratory type. M-0-0011H. Inductance of coils 0.00221H and 0.0021H. Coil resistance 0.53 ohms and 0.51 ohms respectively. Maximum current through coils—3 amps. Completely encased with 4 screw down terminals. Overall size 6in. diameter by 3in. deep. Price £4 each.

Where postage is not stated then orders over £5 are post free. Below £5 add 20p. S.A.E. with enquiries please.

**J. BULL (ELECTRICAL) LTD.**  
(Dept. W.W.) 7, Park Street, Croydon, CRO 1YD  
Callers to 102/3, Tamworth Road, Croydon



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**COMPLETE TELEPHONES**  
 NORMAL HOUSEHOLD TYPE  
 AS SUPPLIED TO THE POST OFFICE  
 EX. G.P.O.  
**ONLY 95p**

P & P 35P EACH



**TELEPHONE DIALS**  
 Standard Post Office type  
 Guaranteed in working order  
**ONLY 25p**  
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**TESTED AND GUARANTEED PAKS**

B2	4	Photo Cells, Sun Batteries, 0.3 to 0.5V. 0.5 to 2mA	50p
B79	4	IN4007 Sil. Rec. diodes, 1,000 PIV lamp plastic	50p
B81	10	Reed switches Reed Relay Inserts 1 1/2" long	50p
B99	200	Mixed Capacitors. Approx. quantity, counted by weight	50p
H4	250	Mixed Resistors. Approx. quantity, counted by weight	50p
H7	40	Wirewound Resistors. Mixed types and values	50p
H40	20	BFY50/2, 2N696, 2N1613 NPN Silicon uncodded TO-5	50p
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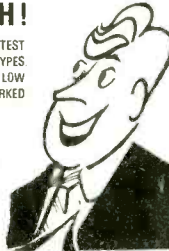
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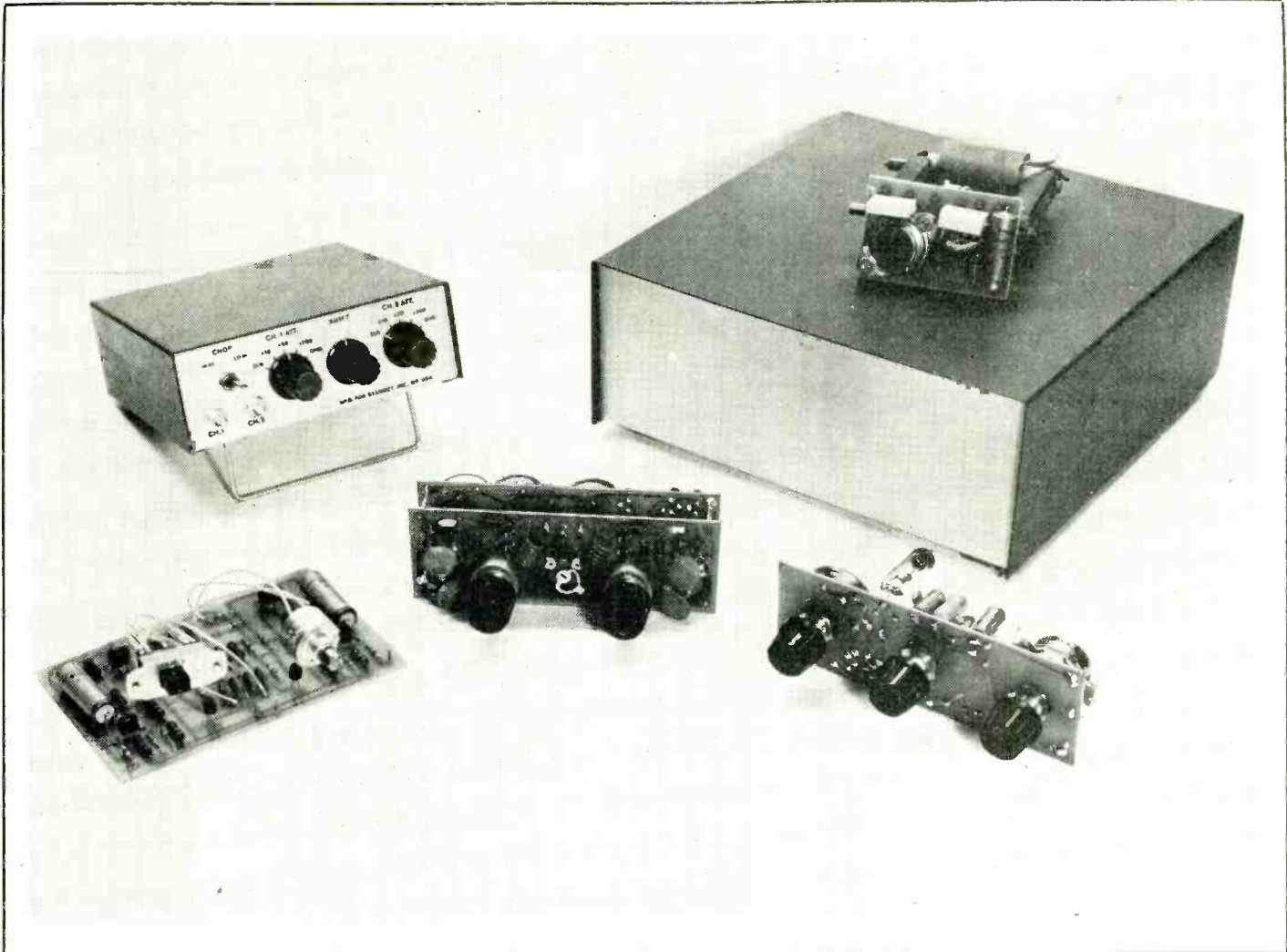
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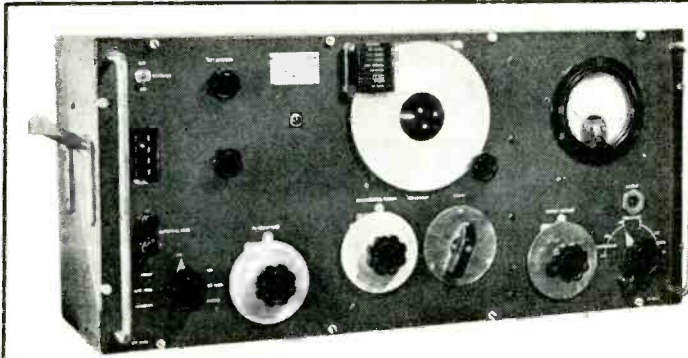
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- TM-6156 Attenuator 40DB. £20.00 each. Post 60p.
- TM-6183 Decoding Unit. £30.00 each. Carr. £1.
- TM-6184 Numerical Display Unit. £15.00 each. Post 60p.
- TM-5691 Pre-amplifier. 3Hz-100KHz. £15.00 each. Post 60p.
- TM-6600 Secondary Pulse Generator. £15.00 each. Post 60p.
- TM-6629 Signal Compressor. £25.00 each. Carr. £1.
- TM-6899/1 Assembly Unit. £6.00 each. Post 60p.
- 6076A Deviation Test Set. 65-75MHz. £75.00 each. Carr. £1.

**CT.52 MINIATURE OSCILLOSCOPE:** Portable. Operates from 115V or 250V 50-60c/s; or 180V 50c/s. A small compact tropicalised instrument designed to meet requirements of radar and communication engineers and general electronic service. Measures 9 in. x 8 in. x 6 1/2 in. Time base 10c/s-40Kc/s. Y plate sensitivity 40V per cm. Tube 2 1/2 in. Frequency compensated amplifier up to 38dB gain. Bandwidth up to 1 Mc/s. Single sweep facilities. Complete with test leads, metal transit case. As new £27.50 each. Carr. £1.

**POLARAD MSG-3 MICROWAVE SIGNAL GENERATOR:** 4.5-8GHz. Internal pulse and squarewave modulation. £185 each, carr. £1.50.

**POLARAD MSG MICROWAVE SIGNAL GENERATOR:** 12.4-17.5GHz. £225 each, carr. £1.50.

**POLARAD KLYSTRON POWER SUPPLY Model KXB:** Input 240V a.c. 50-60c/s. £55 each. Carr. £2.

**TS-45/APM3 "X" BAND SIGNAL GENERATOR (and transmitter output power and frequency meter):** 8.7-9.5GHz. Accuracy ± 2MHz. 115V a.c. £25 each, carr. £1.

**USM-24C OSCILLOSCOPE:** 3 in. oscilloscope with 2c/s to 10Mc/s vertical response, and 8c/s to 800Kc/s horizontal response. Sensitivity 50 mv. rms/inch. Triggered sweep, built-in trigger pulses and markers. Mains input 115V, 50c/s. Complete with all leads, probes and circuit diagram. £42.50 each, carr. £2.

**SIGNAL GENERATOR TS-497B/URR:** (Boonton). Freq. 2-400 Mc/s in 6 bands. Internal Mod. 400 or 1000 c/s per sec. External Mod. 50 to 10,000 c/s per sec. External PM. Percent Mod. 0-30 for sine wave. Am or Pulse Carrier. Output Voltage 0.1-100,000 microvolts cont. variable. Impedance 50 Ω. Price: £85 each + £1.50 carr.

**FREQUENCY METER TS-74 (same TS-174):** Heterodyne crystal controlled. Freq. 20-280 Mc/s. Accuracy .05%. Sensitivity 20 mV. Internal Mod. at 1000 c/s. Power Supply—batteries 6V and 135V. Complete with calibration book. (Manufactured for M.O.D. by Telemax. "As new" in cartons.) £75 each. Fully stabilised Power Supply available at extra cost £7.50 each. Carr. £1.50.

**CT.54 VALVE VOLTMETER:** Portable battery operated. In strong metal case with full operating instructions. 2.4V-480V. A.C. or D.C. in 6 Ranges, 1Ω to 10MegΩ in 5 Ranges. Indicated on 4in. scale meter. Complete with probe, excellent condition. £12.50, carr. 75p.

**CT.381 FREQUENCY SWEEP SIGNAL GENERATOR:** 85Kc/s-30Mc/s and response curve indicator with 6in. CRT tube and separate power supply. Fully stabilised. Price on request.

**TRANSFORMER HV:** 228V input 19,500-0-19,500 4.5KVA, Wt. 220 lbs. £30 each. Carr. £4.

**MODULATOR UNIT:** complete with transformer and 2x807 valves mounted in 19 in. chassis x 8 in. high x 8 in. deep. £4.50 secondhand cond., or £6.50 new cond. Carriage £1.

**RF UNIT:** suitable for use with the above unit. Complete with 2x3E29 valves. Ideal for conversion to 4 metres. £5 secondhand cond., or £7.50 new cond. Carriage £1.

**CONDENSERS:** 30 mfd 600 v wkg. d.c., £3.50 each, post 50p. 15 mfd 330 v a.c., wkg., 75p each, post 25p. 10 mfd 600 v. 43p each, 25p post. 8 mfd 2500 v. £5 each, carr. 63p. 8 mfd 600 v. 43p each, post 15p. 8 mfd. 1% 300 v. D.C. £1.25, post 25p. 4 mfd 3000 v. wkg. £3 each, post 37p. 4 mfd 2000 v. £2 each, post 25p. 4 mfd 600 v., 2 for £1. 0.25 mfd. 2Kv, 20p each, post 10p. 0.01 mfd MICA 2-5Kv, £1 for 5, post 10p. Capacitor 0.125 mfd, 27,000 v. wkg. £3.75 each, 50p post. 2.25 mfd 25 Kv. wkg. £20 each, £3 carr.

**CONTROL PANEL:** 230 v. A.C., 24 v. D.C. @ 2 amps, £2.50 each, carr. 75p.

**OHMITE VARIABLE RESISTOR:** 5 ohms, 5 1/2 amps; or 40 ohms at 2-6 amps; 500 ohms, 0.55 amps. Price (either type) £2 each, 30p post each.

**TX DRIVER UNIT:** Freq. 100-156 Mc/s. Valves 3 x 3C24's; complete with filament transformer 230 v. A.C. Mounted in 19in. panel, £4.50 each, carr. 75p.

**POWER SUPPLY UNIT PN-12A:** 230V a.c. input 50-60 c/s. 513V and 1025V @ 420 mA output. With 2 smoothing chokes 9H, 2 Capacitors, 10Mfd 1500V and 10Mfd 600V. Filament Transformer 230V a.c. input. 4 Rectifying Valves type 5Z3. 2 x 5V windings @ 3 Amps each, and 5V @ 6 Amp and 4V @ 0.25 Amp. Mounted on steel base 19"wx11"Hx14"D. (All connections at the rear.) Excellent condition £6.50 each, carr. £1.

**AUTO TRANSFORMER:** 230-115V, 50-60c/s, 1000 watts, mounted in a strong steel case 5" x 6 1/2" x 7". Bitumen impregnated. £7 each, Carr. 75p. 230-115V, 50-60c/s, 500 watts. 7" x 5" x 5". Mounted in steel ventilated case. £4.00 each, Carr. 75p.

**MODULATOR UNIT:** 50 watt. part of BC-640, complete with 2 x 811 valves, microphone and modulator transformers etc. £7.50 each, 75p carr.

**CATHODE RAY TUBE UNIT:** With 3in. tube, Type 3EG1 (CV1526) colour green, medium persistence complete with nu-metal screen, £3.50 each, post 50p.

**TS 622/URM 44 SIGNAL GENERATOR:** Freq. range—7 to 11 GHz. Output -10 to -127 dbm; CW, FM, Pulse. Direct reading. 115V, 50 c/s. £185.00 each plus £2.00 carriage.

**APN-1 INDICATOR METER, 270° Movement.** Ideal for making rev. counter. £1.25, post 30p.

**VARIABLE POWER UNIT:** Complete with Zenith variac 0-230V. 9 amps. 2 1/2 in. scale meter reading 0-250V. Unit is mounted in 19 in. rack. £15 each, £1.50p carr.

**AIRCRAFT SOLENOID UNIT S.P.S.T.:** 24V, 200 Amps, £2 each, 30p post.

**DECADE RESISTOR SWITCH:** 0.1 ohm per step. 10 positions. 3 Gang, each, 0.9 ohms. Tolerance ± 1% £3 each, 25p post. 30 ohms per step. 10 positions, total value 900 ohms. 3 Gang. Tolerance ± 1%. £3.50 each, post 30p.

**CRYSTAL TEST SET TYPE 193:** Used for checking crystals in freq. range 3000-10,000Kc/s. Mains 230V, 50c/s. Measures crystal current under oscillatory conditions and the equivalent parallel resistance. Crystal freq. can be tested in conjunction with a freq. meter. £12.50 each, £1 carr.

**VARIAC TRANSFORMERS:** Input 115V, output 0-135V at 2 Amps. £3 each 75p post. Input 115V, output 135V at 5 Amps. £5 each, 75p post.

**RACK CABINETS:** (totally enclosed) for Std. 19 in. Panels. Size 6 ft. high x 21 in. wide x 16 in. deep, with rear door. £12 each, £2.50 Carr. OR 4 ft. high x 23 in. wide x 19 in. deep, with rear door. £8.50 each, £2 Carr.

**FUEL INDICATOR Type 113R:** 24V complete with 2 magnetic counters 0-9999, with locking and reset controls mounted in 3in. diameter case. Price £2 each, 30p post.

**MARCONI DERIVATIVE TEST SET OA-1259:** This unit has been designed primarily for testing the linearity of modulator/demodulator equipment used in UHF radio links. The unit mainly consists of a Sweep Generator Unit (TF-1260), a Cathode-Ray-Tube Unit (TF-1261) and associated stabilised power supplies. Further details on request. Secondhand, excellent cond. £225 each. Carr. £2.

**MARCONI TF-1234 UHF RECEIVER:** Suitable for testing the RF stages of radio link equipment. A superheterodyne receiver tunable from 1700-2300MHz. Complete with power supply. Secondhand, excellent cond. £175 each. Carr. £2.

**TS-418/URM49 SIGNAL GENERATOR:** Covers 400-1000MHz range. CW Pulse or AM emission. Power Range 0-120 dbm. £125 each. Carr. £1.50.

**TN/130/APR.9 UHF TUNING UNIT:** Freq. 4300-7350MHz. IF Output 160MHz with bandwidth of 20MHz and is electrically tuned by a d.c. reversible motor. £27.50 each. Carr. £1.

**APR-4 AM RADIO RECEIVER:** 90-1000MHz. This receiver is suitable for monitoring and measuring frequencies as well as relative signal strength. Power Supply 115V 50c/s. £100 each. Carr. £2.

**R-361 RECEIVER:** 225-400MHz. 1 preset channel crystal controlled. Superheterodyne, voice and CW. 230V 50c/s input. £35 each. Carr. £1.50.

**TS-130 TEST SET:** Complete with RF Probe type 1019 Freq. 0.9-12.5KHz, and RF Probe type 1020 Freq. 0.3-1KHz. Also slotted line attenuator 1M-34/U. Freq. 0.3-4KHz; and connectors. £45 each. £1 carr.

**CLASS "D" WAVEMETER NO. 2:** Crystal controlled heterodyne frequency meter covering 2-8MHz. Power supply 6V d.c. Good secondhand cond. £7.50 each. Post 60p.

**RCA TE-149 HETERODYNE WAVEMETER:** V-cut, 1MHz crystal (0.005%). Accuracy better than 0.02%. Dial directly calibrated every 1KHz from 2.5-5MHz. Useful harmonics up to 20MHz. Provision for fitting internal dry batteries. "As new" complete with Manual and Spares. £14 each. Carr. 75p.

**POWER UNIT TYPE 24:** (for R.216 Receiver) A.C. operated 100-125V or 200-250V, 50c/s. "As new" £10 each. Carr. 75p.

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**ROTARY INVERTERS: TYPE PE.218E—**input 24-28V d.c., 80 Amps. 4,800 rpm. Output 115V a.c. 13 Amp 400 c/s. 1 Ph. P.F.9. £17.50 each. Carr. £1.50. **TYPE 8A—**Input 24V d.c., Output 115V a.c. 3 Ph. 1.8 Amps. 400 c/s. £7.50 each. 75p post.

**POWER SUPPLY:** 230V a.c. input; 3000V @ 2.5mA; 4v @ 1 Amp, 300-0-300 200mA; 6V @ 7 Amp; 6V @ 3 Amp. With smoothing capacitors etc. £10.00 each. £1.50p carr.

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CL 8370	7400	12p
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CL 8390	7410	12p
CL 8470	7420	12p
	7440	12p
	7453	12p
	7470	24p
	7472	24p
	7473	32p
	7474	32p
	7482	88p
	7483	95p
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AZ41 0-60	EAB080	ECH42 1-00	EF183 0-30	EZ31 0-29	OH2 0-35	PE46D	PV83 0-38	UH81 0-40	354 0-35	6B1W6 0-85	6V8GT 0-40	30C15 0-80	807 0-60
CBL31 1-00	0-35	ECH81 0-30	EF184 0-35	EZ30 0-25	OZ4 0-40	0-75	PY800 1-00	UCL82 0-35	3Y4 0-35	6B1W7 0-80	6X4 0-35	30C17 0-80	6080 1-60
CL33 1-30	EAF42 0-55	ECH83 0-45	EL33 1-75	0-75	PC86 0-60	PL2000-65	PY800 0-40	UCL83 0-60	5R4GY 0-75	6C 0-33	6B1G 0-75	30C18 0-80	6145 1-60
CY31 0-45	EAF61 0-50	ECH84 0-45	EL34 0-50	GY501 0-80	PC89 0-48	PL36 0-60	SP1 3-75	UF41 0-60	5V4G 0-45	6C8H 0-60	7B7 0-50	30FL1 0-75	1CP31 7-00
DAF91 0-30	EAC33 0-50	ECL80 0-45	EL37 0-25	GZ50 0-40	PC94 0-40	PL61 0-50	SP1 3-75	UF89 0-40	5Y3GT 0-40	6E5 1-00	Z87 2-25	30FL14 0-85	2AP1 4-00
DAF96 0-45	EAC41 0-55	ECL82 0-45	EL42 0-65	GZ34 0-60	PC98 0-50	PL82 0-45	T41 1-00	UL41 0-65	5Z4G 0-40	6F23 0-85	Z87 2-25	30FL15 0-85	3BP1 3-00
DC090 1-35	EBC81 0-30	ECL84 0-40	EL48 0-25	H63 0-90	PC98 0-30	PL83 0-45	U41 0-60	UL84 0-40	6AL5 0-20	6G3 0-33	Z87 2-25	30FL17 0-80	3DP1 2-50
DP91 0-30	EHP80 0-40	ECL86 0-40	EL51 0-35	HL41DD	PC98 0-60	PL84 0-40	U41 0-60	UR5 0-40	6AQ3 0-38	6K6GT 0-80	Y4 0-65	30FL18 0-80	3EG1 2-50
DP96 0-45	EHP83 0-40	EF37A 1-20	EL56 0-35	0-88	PCF8010-50	PL304 0-80	U191 0-75	VP1B 1-25	6A87 0-85	6K7GT 0-35	12AC6 0-50	30FL1 0-75	3GP1 2-50
DK91 0-40	EHP89 0-50	EF39 0-50	EL59 0-35	HN309 1-50	PCF8020-50	PL306 0-90	U404 0-60	VR75/30	6AT6 0-35	6K8GT 0-50	12AD6 0-55	30FL13 0-93	5BP1 4-00
DK92 0-55	EHP91 0-50	EF40 0-50	EL60 0-35	KT51 1-50	PCF8050-80	PL309 1-10	U801 1-18	0-45	6AU6 0-25	6P25 1-50	12AE6 0-55	30PL14 0-90	5CP1 5-00
DK96 0-50	ECX40 1-00	EF52 1-25	EM80 0-45	T66 2-05	PCF806 7-0	PL391 0-80	UA080	0-38	6AV6 0-30	6Q7GT 0-43	12AT6 0-50	35L6GT0-50	5FP7 2-00
DL92 0-35	EC081 0-35	EF80 0-25	EM81 0-60	KT91 (7C5)	PCF808 8-5	PL402 0-85	0-40	VR105/30	6B6 0-30	6R7GT 0-40	12AT7 0-55	35L6GT0-50	5P87 2-00
DL94 0-48	EC082 0-30	EF85 0-35	EM84 0-35	1-13	PCF808 8-5	PL4 2-50	0-40	VR150/30	6BA6 0-25	6R7GT 0-40	12AT7 0-55	35L6GT0-50	5P87 2-00
DL96 0-45	EC083 0-30	EF86 0-30	EV31 0-40	KT88 2-00	PCF808 8-5	PL25 2-50	0-35	0-35	6BB6 0-30	6R7GT 0-40	12AU7 0-30	35Z4GT0-60	CV960 5-00
DM70 0-45	EC085 0-40	EF89 0-28	EY86 0-40	KTW611-00	PCF84 0-45	PY32 0-63	0-35	0-35	6BH6 0-75	68L7GT0-85	12AU7 0-30	35Z4GT0-60	CV960 5-00
DT86 0-33	EC088 0-40	EF91 0-33	EZ40 0-50	KTW621-00	PCF85 0-40	PY33 0-63	0-35	0-35	6B1G 0-75	68N7GT	12AU7 0-30	35Z4GT0-60	CV960 5-00
DX67 0-33	ECF80 0-35	EF92 0-35	EZ41 0-50	N78 1-50	PCF86 0-45	PY81 0-30	0-35	0-35	6B36 0-50	6BQ7A 0-45	12BA6 0-40	35Z4GT0-60	CV960 5-00

## TRANSISTORS

IN21 0-17	2N708 0-15	2N3709 0-10	AF116 0-25	BF195 0-15	CR82/40	GJM 0-37	NKT128	0A95 0-07	OC26 0-25	OC71 0-12	OC84 0-25	ORP60 0-40
IN23 0-20	2N1802 0-18	2N3711 0-10	AF117 0-25	BF196 0-15	CR83/40	KS100A0-20	0-35	OA200 0-07	OC28 0-25	OC72 0-20	OC123 0-65	ORP61 0-42
IN4001 0-07	2N1303 0-18	2N3819 0-35	AF121 1-00	BF561 0-28	CV102 0-18	MAT101	0-30	OA202 0-10	OC29 0-40	OC73 0-30	OC139 0-25	8X640 0-50
IN4002 0-08	2N1304 0-22	2N4289 0-15	BC107 0-10	BF598 0-28	CV103 0-18	MAT120	0-30	OC29 0-40	OC30 0-40	OC74 0-30	OC140 0-35	8X642 0-80
IN4003 0-10	2N1305 0-22	2N4290 0-15	BC108 0-10	BF599 0-22	CV223 1-10	MAT121	1-25	OC30 0-40	OC31 0-40	OC75 0-30	OC141 0-35	8X643 0-70
IN4004 0-10	2N1306 0-22	2N4291 0-15	BC109 0-10	BF599 0-22	CV223 1-10	MAT121	1-25	OC31 0-40	OC32 0-40	OC76 0-25	OC142 0-35	8X644 0-70
IN4006 0-15	2N1307 0-25	2N4292 0-15	BC110 0-10	BF599 0-22	CV223 1-10	MAT121	1-25	OC32 0-40	OC33 0-40	OC77 0-40	OC143 0-35	8X645 0-70
IS111 0-13	2N2147 0-75	AC126 0-20	BC115 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC33 0-40	OC34 0-40	OC78 0-20	OC144 0-35	8X646 0-70
IS131 0-13	2N2148 0-75	AC127 0-20	BC116 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC34 0-40	OC35 0-40	OC79 0-20	OC145 0-35	8X647 0-70
IS132 0-13	2N2149 0-75	AC128 0-20	BC117 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC35 0-40	OC36 0-40	OC80 0-20	OC146 0-35	8X648 0-70
IS133 0-13	2N2150 0-75	AC129 0-20	BC118 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC36 0-40	OC37 0-40	OC81 0-20	OC147 0-35	8X649 0-70
IS134 0-13	2N2151 0-75	AC130 0-20	BC119 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC37 0-40	OC38 0-40	OC82 0-20	OC148 0-35	8X650 0-70
IS135 0-13	2N2152 0-75	AC131 0-20	BC120 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC38 0-40	OC39 0-40	OC83 0-20	OC149 0-35	8X651 0-70
IS136 0-13	2N2153 0-75	AC132 0-20	BC121 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC39 0-40	OC40 0-40	OC84 0-20	OC150 0-35	8X652 0-70
IS137 0-13	2N2154 0-75	AC133 0-20	BC122 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC40 0-40	OC41 0-40	OC85 0-20	OC151 0-35	8X653 0-70
IS138 0-13	2N2155 0-75	AC134 0-20	BC123 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC41 0-40	OC42 0-40	OC86 0-20	OC152 0-35	8X654 0-70
IS139 0-13	2N2156 0-75	AC135 0-20	BC124 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC42 0-40	OC43 0-40	OC87 0-20	OC153 0-35	8X655 0-70
IS140 0-13	2N2157 0-75	AC136 0-20	BC125 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC43 0-40	OC44 0-40	OC88 0-20	OC154 0-35	8X656 0-70
IS141 0-13	2N2158 0-75	AC137 0-20	BC126 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC44 0-40	OC45 0-40	OC89 0-20	OC155 0-35	8X657 0-70
IS142 0-13	2N2159 0-75	AC138 0-20	BC127 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC45 0-40	OC46 0-40	OC90 0-20	OC156 0-35	8X658 0-70
IS143 0-13	2N2160 0-75	AC139 0-20	BC128 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC46 0-40	OC47 0-40	OC91 0-20	OC157 0-35	8X659 0-70
IS144 0-13	2N2161 0-75	AC140 0-20	BC129 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC47 0-40	OC48 0-40	OC92 0-20	OC158 0-35	8X660 0-70
IS145 0-13	2N2162 0-75	AC141 0-20	BC130 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC48 0-40	OC49 0-40	OC93 0-20	OC159 0-35	8X661 0-70
IS146 0-13	2N2163 0-75	AC142 0-20	BC131 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC49 0-40	OC50 0-40	OC94 0-20	OC160 0-35	8X662 0-70
IS147 0-13	2N2164 0-75	AC143 0-20	BC132 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC50 0-40	OC51 0-40	OC95 0-20	OC161 0-35	8X663 0-70
IS148 0-13	2N2165 0-75	AC144 0-20	BC133 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC51 0-40	OC52 0-40	OC96 0-20	OC162 0-35	8X664 0-70
IS149 0-13	2N2166 0-75	AC145 0-20	BC134 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC52 0-40	OC53 0-40	OC97 0-20	OC163 0-35	8X665 0-70
IS150 0-13	2N2167 0-75	AC146 0-20	BC135 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC53 0-40	OC54 0-40	OC98 0-20	OC164 0-35	8X666 0-70
IS151 0-13	2N2168 0-75	AC147 0-20	BC136 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC54 0-40	OC55 0-40	OC99 0-20	OC165 0-35	8X667 0-70
IS152 0-13	2N2169 0-75	AC148 0-20	BC137 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC55 0-40	OC56 0-40	OC100 0-20	OC166 0-35	8X668 0-70
IS153 0-13	2N2170 0-75	AC149 0-20	BC138 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC56 0-40	OC57 0-40	OC101 0-20	OC167 0-35	8X669 0-70
IS154 0-13	2N2171 0-75	AC150 0-20	BC139 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC57 0-40	OC58 0-40	OC102 0-20	OC168 0-35	8X670 0-70
IS155 0-13	2N2172 0-75	AC151 0-20	BC140 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC58 0-40	OC59 0-40	OC103 0-20	OC169 0-35	8X671 0-70
IS156 0-13	2N2173 0-75	AC152 0-20	BC141 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC59 0-40	OC60 0-40	OC104 0-20	OC170 0-35	8X672 0-70
IS157 0-13	2N2174 0-75	AC153 0-20	BC142 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC60 0-40	OC61 0-40	OC105 0-20	OC171 0-35	8X673 0-70
IS158 0-13	2N2175 0-75	AC154 0-20	BC143 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC61 0-40	OC62 0-40	OC106 0-20	OC172 0-35	8X674 0-70
IS159 0-13	2N2176 0-75	AC155 0-20	BC144 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC62 0-40	OC63 0-40	OC107 0-20	OC173 0-35	8X675 0-70
IS160 0-13	2N2177 0-75	AC156 0-20	BC145 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC63 0-40	OC64 0-40	OC108 0-20	OC174 0-35	8X676 0-70
IS161 0-13	2N2178 0-75	AC157 0-20	BC146 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC64 0-40	OC65 0-40	OC109 0-20	OC175 0-35	8X677 0-70
IS162 0-13	2N2179 0-75	AC158 0-20	BC147 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC65 0-40	OC66 0-40	OC110 0-20	OC176 0-35	8X678 0-70
IS163 0-13	2N2180 0-75	AC159 0-20	BC148 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC66 0-40	OC67 0-40	OC111 0-20	OC177 0-35	8X679 0-70
IS164 0-13	2N2181 0-75	AC160 0-20	BC149 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC67 0-40	OC68 0-40	OC112 0-20	OC178 0-35	8X680 0-70
IS165 0-13	2N2182 0-75	AC161 0-20	BC150 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC68 0-40	OC69 0-40	OC113 0-20	OC179 0-35	8X681 0-70
IS166 0-13	2N2183 0-75	AC162 0-20	BC151 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC69 0-40	OC70 0-40	OC114 0-20	OC180 0-35	8X682 0-70
IS167 0-13	2N2184 0-75	AC163 0-20	BC152 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC70 0-40	OC71 0-40	OC115 0-20	OC181 0-35	8X683 0-70
IS168 0-13	2N2185 0-75	AC164 0-20	BC153 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC71 0-40	OC72 0-40	OC116 0-20	OC182 0-35	8X684 0-70
IS169 0-13	2N2186 0-75	AC165 0-20	BC154 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC72 0-40	OC73 0-40	OC117 0-20	OC183 0-35	8X685 0-70
IS170 0-13	2N2187 0-75	AC166 0-20	BC155 0-20	BF599 0-22	CV223 1-10	MAT121	1-25	OC73 0-40	OC74 0-40</			



# BENTLEY ACOUSTIC CORPORATION LTD.

7A GLOUCESTER ROAD, LITTLEHAMPTON, SUSSEX. Tel. 6743 THE VALVE SPECIALISTS.

0A2	0.30	6BG6G	1.05	6L1	0.98	12AT7	0.16	30P16	0.28	AZ1	0.40	EC92	0.34
0B2	0.30	6BH6	0.43	6L6GT	0.39	12AU6	0.21	30P19	0.48	AZ1	0.46	EC92	1.50
0Q4	0.25	6BJ6	0.39	6L7M	0.38	12AU7	0.19	30P4	0.55	AZ41	0.53	EC93	1.50
1A3	0.23	6BK7A	0.50	6L12	0.32	12AV6	0.26	30P11	0.57	B919	0.27	EC93	0.95
1A7GT	0.32	6BQ5	0.21	6L1P	0.44	12AX7	0.21	30P12	0.29	CL33	0.90	EC94	0.80
1B3GT	0.35	6BQ7A	0.28	6L1D2	0.28	12AX7	0.68	30P13	0.75	CV6	0.53	EC94	0.16
1C2	0.35	6BR7	0.79	6L2D2	0.48	12BA6	0.30	30P15	0.87	CV8	0.53	EC93	0.21
1G6	0.30	6BR8	0.68	6L2GT	0.40	12BH7	0.27	35A3	0.48	CY1C	0.53	EC94	0.28
1H5GT	0.33	6BS7	1.25	6L2GT	0.40	6P1	1.50	19J5GT	0.30	CY31	0.29	EC93	0.32
1L4	0.13	6BW6	0.72	6P1	0.21	6P13	0.50	35B5	0.70	D63	0.20	EC96	0.40
1LD5	0.30	6BW7	0.50	6P2A	0.59	6S7GT	0.38	35L2GT	0.42	DA9P6	0.33	EC98	0.35
1N3	0.40	6BX6	0.21	6P2B	0.59	12K5	0.50	35V4	0.23	DC90	0.60	EC98	0.50
1N3GT	0.37	6BY7	0.25	6P2GT	0.48	12K5GT	0.34	35Z3	0.50	DD4	0.53	EC94	0.50
1R5	0.27	6BY7	0.21	6Q7(M)	0.43	12L6	0.28	35Z4GT	0.24	DF91	0.14	EC98	1.70
1S4	0.22	6BZ6	0.31	6R7G	0.35	12M7	0.40	35Z5GT	0.30	DF96	0.34	EC98	0.27
1S5	0.20	6C6	0.19	6R7(M)	0.55	12N6	0.35	35Z5GT	0.30	DH76	0.28	EC92	0.25
1U4	0.20	6C9	0.73	6S7A	0.35	12P6GT	0.23	35B5	0.32	DH81	0.58	EC98	0.64
1U5	0.48	6CB6A	0.26	6S7GT	0.38	12R17	0.15	50C19G	0.50	DI12	0.18	EC98	0.64
2D21	0.35	6C12	0.25	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
2K3	0.25	6C17	0.63	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
3A4	0.25	6C17	0.63	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
3B7	0.25	6C8A	0.68	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
3D8	0.19	6C8B	0.38	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
3Q4	0.38	6CL6	0.43	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
3Q5GT	0.37	6CL8A	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
3S4	0.23	6C18A	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
4C6	0.50	6C17	0.63	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
5C4	0.30	6D6	0.15	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
5V4G	0.33	6D7E	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
5Y3GT	0.25	6E7B	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
5Z3	0.45	6I7E	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
5Z4G	0.33	6I7E	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6A5	0.25	6F14	0.40	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6A8G	0.33	6F6	0.25	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AC7	0.15	6F12	0.17	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6A95	0.25	6F14	0.40	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AH6	0.50	6F13	0.33	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AJ3	0.75	6F13	0.33	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AJ8	0.25	6F18	0.65	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AK5	0.25	6F23	0.68	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AK6	0.30	6F24	0.68	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AK8	0.30	6F24	0.68	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AL5	0.10	6F25	0.51	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AM8A	0.50	6F28	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AN8	0.49	6F32	0.15	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AQ3	0.21	6G6G	0.25	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AQ8	0.32	6G8A	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AR3	0.30	6G8K	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AR6	1.00	6G8K	0.50	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AT6	0.18	6H6GT	0.15	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AL6	0.18	6I5G	0.19	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AV6	0.28	6J5GT	0.29	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AV8A	0.54	6J6	0.18	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6AX4	0.39	6J6	0.18	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6B8G	0.13	6J7G	0.24	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6BA6	0.19	6J18A	0.28	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6BC8	0.50	6K7G	0.10	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64
6BE8	0.20	6K8G	0.18	6S7GT	0.38	12R17	0.15	50C19G	0.50	DH81	0.58	EC98	0.64

EL91	0.23	N709	0.21	PM84	0.31	UY41	0.38	2N966	0.53	AF139	0.65	FSV41A	23	OC23	0.38
EL95	0.32	P61	0.44	PY33/2	0.50	UY85	0.23	2N1756	0.50	AF170	0.68	GD4	0.33	OC24	0.38
EL96	0.49	PABCO80		PY80	0.30	UY10	0.43	2N2147	0.50	AF180	0.48	GD5	0.28	OC25	0.38
EL180	0.75	PC86	0.32	PY81	0.24	UY12/14	0.38	2N2297	0.50	AF186	0.55	GD6	0.28	OC28	0.60
EM80	0.37	PC86	0.44	PY81	0.24	UY16	0.75	2N2309A	0.50	AF209	0.35	GD6	0.30	OC42	0.63
EM81	0.37	PC88	0.44	PY83	0.28	UY17	0.35	0.22	ASV27	0.43	GD9	0.20	OC29	0.60	
EM83	0.75	PC95	0.53	PY88	0.31	UY18/20	0.75	2N2613	0.39	ASV28	0.33	GD11	0.20	OC35	0.32
EM84	0.31	PC97	0.36	PY301	0.56	UY19	1.73	2N3053	0.33	ASV29	0.50	GD12	0.20	OC36	0.43
EM85	1.00	PC900	0.29	PY500	0.95	UY22	0.38	2N3121	2.50	BA102	0.45	GD14	0.50	OC38	0.43
EM87	0.34	PC908	0.57	PY800	0.31	UY25	0.62	2N3173	0.19	BA115	0.14	GD16	0.40	OC41	0.50
EM91	0.29	PC928	0.39	PZ30	0.48	UY31	0.30	2N3297	0.90	BA116	0.25	GD16	0.30	OC42	0.63
EM93	0.55	PC939	0.44	PQ21	0.50	UY33	1.50	2N3866	1.90	BA129	0.13	GD18	0.20	OC43	1.18
EM94	0.31	PC97	0.36	PY301	0.56	UY35	0.83	2N3988	0.50	BA130	0.10	GD18	0.40	OC44	0.10
EM95	1.00	PC900	0.29	PY500	0.95	UY37	1.75	2N4223	0.50	BA153	0.15	GD18	0.20	OC45	0.11
EM97	0.34	PC908	0.57	PY800	0.31	UY47	0.62	AA119	0.15	BCV10	0.45	GD19	0.20	OC46	0.15
EM98	0.29	PC928	0.39	PZ30	0.48	UY48	0.78	AA120	0.15	BCV12	0.50	GD19	0.38	OC65	1.13
EM99	0.55	PC939	0.44	PQ21	0.50	UY49	0.53	AA129	0.15	BCV33	0.20	GD19	0.43	OC70	0.13
EM99	0.29	PC928	0.39	PZ30	0.48	UY50	0.25	AA133	0.15	BCV38	0.23	GD19	0.15	OC72	0.11
EM99	0.29	PC928	0.39	PZ30	0.48	UY50	0.25	AA133	0.15	BCV38	0.23	GD19	0.15	OC72	0.11
EM99	0.29	PC928	0.39	PZ30	0.48	UY50	0.25	AA133	0.15	BCV38	0.23	GD19	0.15	OC72	0.11

All goods are unused and subject to the manufacturers' guarantee. We do not handle manufacturers' seconds nor rejects, which are often described as "new and tested" but have a limited and unreliable life. Business hours Mon-Fri 9.30-5.30 p.m.

Terms of business: Cash or cheque with order. Post/packing 3p per item, subject to a minimum of 9p per order. Orders over £5 sent free. All orders cleared same day by first class mail. Any parcel insured against damage in transit for 3p extra per order. Complete catalogue with conditions of sale 7p post paid. No enquiries answered unless S.A.E. is enclosed for reply.

**MARCONI**  
**SIGNAL GENERATOR TF 801B/3/S.** Range 12 Mc/s to 485 Mc/s. P.O.A.  
**TF121 HETERODYNE UNIT.** Frequency range: 2 Kc/s-100 Mc/s in nine ranges. P.O.A.  
**TF34512 COUNTER FREQUENCY METER** with plug-in units up to 220 Mc/s. P.O.A.  
**OA.1094A/3 H.F. SPECTRUM ANALYSER** with trolley and L.F. extension unit type TM6448. Frequency range: 3-30 MHz in nine bands. Selectivity: 6, 30, 150 Hz at 3 dB. Sweep width: 0.3 kHz to 0.30 kHz in two ranges. Sweep duration: 0.1, 0.3, 1, 3, 10 and 30 sec. and manual control.  
**L.F. EXTENSION UNIT TYPE TM6448.** Frequency range up to 3 MHz, approximately from 100 Hz in five bands. Bandwidth: in the tuned ranges, the 3 dB bandwidths at the centre approx.: Range 1: 500 Hz; 2: 80 kHz; 3: 50 kHz. Full spec. — price on app.  
**TF 144H SIGNAL GENERATOR.** Frequency range: 10 kHz-72 MHz. Stability: 0.002%. High discrimination, built-in crystal calibrator. Good r.f. waveforms at all frequencies. Protected thermocouple level monitor. Price and spec. on request.  
**SO1 REMSCOPE Storage Oscilloscope** with Trace Shifter type TS1 (740/3). Full spec. and price upon request.  
**AVO TRANSISTOR ANALYSER CT 448** £70 incl. carr.  
**AVO MULTIMETER MODEL IX.** £24.50 incl. carr.  
**TF 791D CARRIER DEVIATION METER.** Carrier range: 4 to 1024 Mc/s. Deviation range: up to ± 125 Kc/s. Modulating frequency range: up to 35 Kc/s. P.O.A.  
**CT436 OSCILLOSCOPE D.C. 6 Mc/s. £85.00.**  
**CD1220 WIDE-BAND OSCILLOSCOPE** with Dual Trace Pre-Amplifier CX1257. Bandwidth: DC-24 Mc/s (-3 dB); 2.5 c/s-24 Mc/s A.C. coupled. Rise Time: 10 nanosec approx. Sensitivity: 50 mV/cm to 50 V/cm in nine calibrated ranges with fine gain control. A Time Base—Range: 100 nanosec/cm to 5 sec/cm in 24 calibrated ranges, with continuous coverage to 12 sec/cm, 20 nanosec/cm with X5 sweep expansion. B Time Base—Range: 2 usec/cm to 1 sec/cm in 18 calibrated ranges. Max. speed 0.4 usec/cm with 5 expansion. P.O.A.

**RACAL UNIVERSAL COUNTER/TIMER SA550 (CT48)**  
 8 digit in line read-out.  
 Facilities include:  
 - direct frequency measurement up to 100MHz;  
 - pulse, period, ratio, time interval and totalling measurements. Input sensitivity variable from 300mV to 5V, three independent inputs, self-check etc. Full spec. and price on request.

**JOHN CRICHTON**  
*Electronic Equipment*  
 558, Kingston Road, Raynes Park, London, S.W.20  
 Please phone 01-540 9534

**OA 1094A/S H.F. SPECTRUM ANALYSER**  
 Carrier range: 30 Mc/s to 485 Mc/s. P.O.A.  
 Sweep width: up to 30 Mc/s. Sweep width: up to 30 Kc/s. 60 dB amplification. Difference frequency measurement available. P.O.A.

**B.R.A. NEW TRIMPOTS**  
**HELIPOT:** 10, 50, 100, 500, 5K, 10K, 20K, 25K ohm. 70p each. M.E.C.: 100Ω 60p each.  
**PAINTON:** 200, 500, 2Kohm, 60p each.  
**RELANCE:** 1K0-K. 45p each. Discount for quantity.

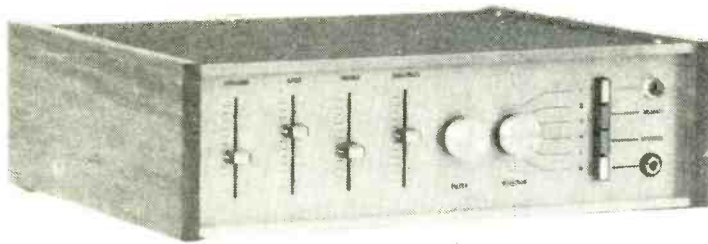
**B.R.A. NEW RELAYS BY "DIAMOND M".** 4 P.D.T. relay. Coil-ohms 150, 265 V. 55p each.

**THERMOCOUPLES.** Mineral Insulated Metal Sheathed. Conductors: Positive Nickel-Chromium. Negative Nickel-Aluminum. Conductor Diameter: 0.11 inch nominal. Tolerance: ± 3°C. up to 400°C. ± 2% between 400°C and 1000°C. Length 3ft. 2in. (96 cm. approx.). £2.25 post paid.

**"WESTON"** clear plastic meters 50.0-50.0uA type S.221.3.150 size 120 x 120 mm. £



# POWERTRAN ELECTRONICS



## METALWORK SYSTEM

Designed to house Bailey, Blomley or Linsley Hood Class AB amplifiers with simple or regulated power supplies and Bailey Burrows pre-amp. Options of standard or hum reducing toroidal mains transformer. Also rotary control version. Details in price list.

## TOROIDAL TRANSFORMER 60 volt 2 amp.

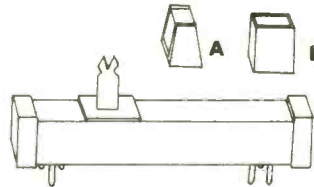
Max. height 2in. Suitable for our regulated power supply. . . £7-40  
 Simple clamp . . . . . 0-20  
 Magnetically screening clamp . . . . . 0-75

## COMPONENTS FOR W.W. AMPLIFIER DESIGNS

<b>100W AMPLIFIER (FEB. 1972)</b>	
Designer approved kit.	
Semiconductor set	15-60
Resistors, capacitors, pots	2-50
F/Glass PCB	1-30
<b>POWER SUPPLY (For 100W Amp.)</b>	
Designer approved kit.	
Semiconductors, Resistors, capacitors, pots, trans-formers, F/Glass PCB	14-70
<b>30W BLOMLEY (New approach to class B)</b>	
Semiconductor set	5-60
Resistors, capacitors, pots	1-85
F/Glass PCB	0-70
<b>30W BAILEY (Single power rail)</b>	
Transistor set	4-60
Resistors, capacitors, pots	1-45
F/Glass PCB	0-65
<b>LINSLEY-HOOD CLASS A (Dec., 1970, circuit)</b>	
Designer approved kit.	
2N3055 pair, BC212L, 2N1711	1-25
Resistors, capacitors, pot	1-80
F/Glass PCB	0-60
<b>LINSLEY-HOOD 20W CLASS AB</b>	
Designer approved kit.	
MJ481/491, MJE521, BC182L, BC212L, zener	3-35
Resistors, capacitors, pots	2-20
F/Glass PCB	0-70
Regulate 8Ω or 15Ω	
<b>REGULATED 60V POWER SUPPLY</b>	
A 5 transistor series stabiliser, suitable for a pair of Bailey or Blomley amplifiers, featuring very effective S/C protection. All Semi/C's, R's, C's, F/Glass PCB	4-85
Power supplies for other amplifiers also available	
<b>PRE-AMPS</b>	
Each component set comprises of all specified resistors, capacitors, transistors, pots, including special balance control for stereo sets.	
<b>BAILEY/BURROWS (Aug., 1971)</b>	
Stereo F/Glass PCB	1-60
Component Set: Mono	2-75
Component set: Stereo	6-35
<b>BURROWS SIMPLE PRE-AMP</b>	
Mono F/Glass PCB	0-80
(suitable for +ve and -ve voltage systems)	
Component set: Mono	2-05
Component set: Stereo	4-90
<b>LINSLEY-HOOD SIMPLE PRE-AMP</b>	
Stereo F/Glass PCB	1-60
(includes accommodation for mag. PU circuit but components for this are not supplied with the sets)	
Component set: Mono	2-50
Component set: Stereo	5-85
<b>STUART TAPE RECORDER</b>	
Set of stereo f/glass PCBs	2-70
Components sets on price list.	

## SLIDER POTENTIOMETERS

LENGTH: 87mm  
 WIDTH: 10mm  
 TRAVEL: 55mm



Single: log or lin 1K, 2K2, 4K7, 10K, 22K, 47K, 100K, 220K, 470K, 1M 35p  
 Dual: log or lin 1K, 2K2, 4K7, 10K, 22K, 47K, 100K, 220K, 470K, 1M 55p  
 Balance: special dual track 10K 60p  
 Black/Chrome knob: type A or B 12p

## THYRISTORS

<b>PIV 1A</b>				<b>3A</b>			<b>7A</b>			<b>16A</b>		
	P	P	P	P	P	P	P	P	P	P	P	
50	25	27	45	60	7	8	19					
100	27	30	50	65	7	9	20					
200	35	37	55	75	8	10	22					
300	40	45	60	85	9	11	25					
400	45	50	65	90	10	12	26					

Zener Diodes 400mW 4V7-30V 12p

## RECTIFIERS

<b>1A</b>			<b>1-5A</b>			<b>3A</b>		
	P	P	P	P	P	P	P	P
	7	8	19					
	7	9	20					
	8	10	22					
	9	11	25					
	10	12	26					

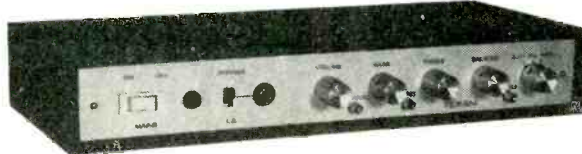
## 23mm CARBON POTENTIOMETERS

Single: lin 1K to 2M2 12p  
 log 4K7 to 2M2 12p  
 Dual: lin or log 4K7 to 2M2 35p  
 Balance: 10K log A log 40p  
 Balance: Purpose designed; better than Log./A Log. No attenuation at mid point. 22K only 45p

## Semi-Conductors

2N699	0-25
2N1613	0-20
2N1711	0-25
2N2926G	0-10
2N3053	0-15
2N3055	0-45
2N3442	1-20
2N3819	0-23
2N3904	0-17
2N3906	0-20
2N4058	0-12
2N4062	0-11
2N4302	0-60
2N5457	0-30
2N5830	0-30
40361	0-40
40362	0-45
BC107	0-08
BC108	0-08
BC109	0-08
BC125	0-15
BC126	0-15
BC182K	0-10
BC212K	0-12
BC182L	0-10
BC184L	0-11
BC212L	0-12
BC214L	0-14
BF257	0-40
BF259	0-47
BFX29	0-30
BFY50	0-20
MJ481	1-20
MJ491	1-30
MJE521	0-60
MPSA05	0-30
MPSA12	0-55
MPSA14	0-35
MPSA55	0-35
MPSA65	0-35
MPSA66	0-40
MPSH05	0-20
MPSU05	0-60
MPSU55	0-70
SN72741P	0-58
SN72748P	0-58
T1B11	1-10
TIP29A	0-50
TIP30A	0-60
TIP31A	0-60
TIP32A	0-70
TIP33A	1-00
TIP34A	1-50
TIP41A	0-74
TIP42A	0-90
TIP3055	0-60
IB08T20	0-50
IB40K20	1-40
IN914	0-07
IN916	0-07
IS44	0-05
IS920	0-10
IS3062	0-25
5805	1-20

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These interesting 27v 0.5A units (will happily provide 700mA indefinitely) are built into an attractive grey-finished instrument case, provision being made for base or side mounting. Cable entry grommets are mounted in the base of the unit. The choke capacity smoothed output is solid state stabilised against variation in input voltage and output current, and input and output fuses with spares are fitted. The output operates a built-in S.P.C.O. relay to switch for instance an alarm circuit, input voltage is 200-250v A.C. in 10v steps, while the transformer secondary carries two taps. All terminations to a Grelco block. There is adequate room for other equipment within the ventilated case, which is 12" x 10" x 6" deep. Our price, brand new in carton with circuit, only £3.75 (P.Pd. U.K.).

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In sizes 08, 11, 15, 16, 18 and 23 for 50, 60 and 400 Hz operation.  
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250-0-250v, 100mA, 6.3v, 4a., 0-5-6.3v, 3a.	£2.20
300-0-300v, 100mA, 6.3v, 4a., 0-5-6.3v, 3a.	£2.20
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**ALSO AVAILABLE WITH 115/120V SECONDARY WINDING**

Ref. No.	VA (Watts)	Weight lb oz	Size cm.	P & P
07	20	1 11	7.0 x 6.0 x 6.5	1.61 30
100	60	3 8	8.9 x 8.0 x 7.7	2.39 36
61	100	5 12	10.2 x 8.9 x 8.3	2.62 52
30	200	9 8	12.0 x 10.3 x 10.0	4.39 52
62	250	12 4	9.5 x 12.7 x 11.4	5.80 67
55	350	15 0	14.0 x 10.8 x 12.4	7.77 82
63	500	27 0	17.1 x 11.4 x 15.9	11.20 **
92	1000	40 0	17.8 x 17.1 x 21.6	20.63 **
128	2000	63 0	24.1 x 21.6 x 15.2	34.10 **
129	3000	84 0	21.6 x 21.6 x 20.3	53.34 **
190	6000	178 0	31.1 x 35.6 x 17.1	87.52 **



**440V 300VA ISOLATOR, Primary 440V Secondary 240V, Centre Tapped Screened and Shrouded, £9.43. P & P 67p.**

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Ref. No.	VA (Watts)	Weight lb oz	Size cm.	Auto Taps	P & P
113	20	1 11	7.3 x 4.3 x 4.4	0-115-210-240	0.85 22
64	75	1 14	7.0 x 6.4 x 6.0	0-115-210-240	1.66 30
4	150	3 0	8.9 x 6.4 x 7.6	0-115-200-220-240	2.00 36
66	300	6 0	10.2 x 10.2 x 9.5	"	3.89 52
67	500	12 8	14.0 x 10.2 x 11.4	"	5.78 67
84	1000	16 0	11.4 x 14.0 x 14.0	"	10.49 82
93	1500	28 9	13.5 x 14.9 x 16.5	"	15.20 **
95	2000	40 0	17.8 x 16.5 x 21.6	"	19.84 **
73	3000	45 8	17.4 x 18.1 x 21.3	"	26.99 **

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Ref. No.	Amps.	Weight lb oz	Size cm.	Secondary Windings	P & P
111	0.5-0.25	1 12	7.6 x 5.7 x 4.4	0-12V at 0.25A x 2	0.85 22
213	1.0-0.5	1 0	8.3 x 5.1 x 5.1	0-12V at 0.5A x 2	1.01 22
71	2	1 9	7.0 x 6.4 x 5.7	0-12V at 1A x 2	1.33 22
18	4	2 4	8.9 x 7.0 x 7.0	0-12V at 2A x 2	1.86 36
70	6	3 12	10.2 x 7.6 x 8.6	0-12V at 3A x 2	2.24 42
108	8	4 5	10.0 x 8.3 x 8.2	0-12V at 4A x 2	2.48 52
72	10	5 6	7.9 x 10.8 x 10.2	0-12V at 5A x 2	2.94 52
17	16	8 7	12.1 x 9.5 x 10.2	0-12V at 8A x 2	4.54 52
115	20	10 13	12.1 x 11.4 x 10.2	0-12V at 10A x 2	5.78 67
107	30	15 12	13.3 x 12.1 x 12.1	0-12V at 15A x 2	10.67 82
226	60	30 34	17.0 x 14.5 x 12.5	0-12V at 30A x 2	19.61 **

**30 VOLT RANGE Secondary Taps**

Ref. No.	Amps.	Weight lb oz	Size cm.	Secondary Taps	P & P
112	0.5	1 4	8.3 x 3.7 x 4.9	0-12-15-20-24-30V	1.01 22
79	1.0	2 0	7.0 x 6.4 x 6.0	"	1.35 36
3	2.0	3 2	8.9 x 7.0 x 7.6	"	2.01 36
21	4.0	4 6	10.2 x 8.9 x 8.6	"	2.48 42
51	6.0	6 8	10.2 x 10.0 x 8.6	"	2.94 52
117	8.0	7 8	12.1 x 10.0 x 10.2	"	3.66 52
88	8.0	10 0	14.0 x 11.7 x 10.0	"	5.64 67
89	10.0	12 2	14.0 x 10.2 x 11.4	"	7.14 67

**50 VOLT RANGE Secondary Taps**

Ref. No.	Amps.	Weight lb oz	Size cm.	Secondary Taps	P & P
102	0.5	1 11	7.0 x 7.0 x 5.7	0-19-25-33-40-50V	1.33 30
103	1.0	2 10	8.9 x 7.3 x 7.0	"	1.94 36
104	2.0	5 0	10.2 x 8.9 x 8.6	"	2.69 42
105	3.0	6 0	10.2 x 10.2 x 8.3	"	3.65 52
106	4.0	9 4	12.1 x 11.4 x 10.2	"	4.83 52
107	6.0	12 4	12.1 x 11.1 x 13.3	"	7.14 67
118	8.0	18 9	13.3 x 13.3 x 12.1	"	9.32 97
119	10.0	19 12	16.5 x 11.4 x 15.9	"	11.68 97

**60 VOLT RANGE**

Ref. No.	Amps.	Weight lb oz	Size cm.	Secondary Taps	P & P
124	0.5	2 4	8.3 x 9.5 x 6.7	0-24-30-40-48-60V	1.35 36
126	1.0	3 0	8.9 x 7.6 x 7.6	"	1.88 36
127	2.0	5 6	10.2 x 8.9 x 8.6	"	2.94 42
125	3.0	8 8	11.9 x 9.5 x 10.0	"	4.48 52
123	4.0	10 6	11.4 x 9.5 x 11.4	"	5.78 67
120	6.0	16 12	13.3 x 12.1 x 12.1	"	8.37 82
122	10.0	23 2	16.5 x 12.7 x 16.5	"	13.85 **

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146	8.0	6 4	8.9 x 10.2 x 10.2	3.49 52
50	12.5	11 14	13.3 x 10.8 x 12.1	5.20 67

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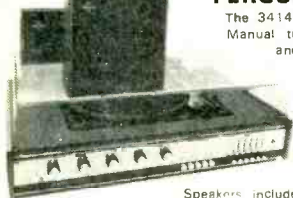
## Audiotronic 6 Pole Quadraphonic Decoder

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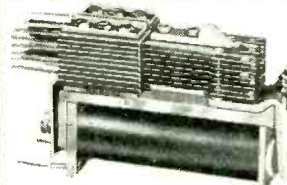
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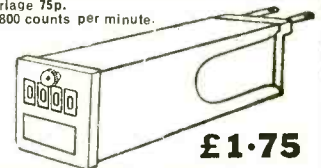
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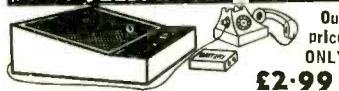
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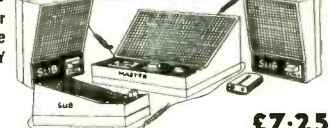


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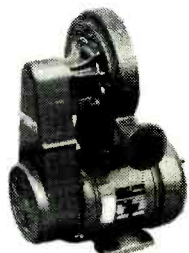
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No.	Sec. Taps	Amps	Price	Carr.
1A	25-33-40-50	15	£12.00	65p
1B	25-33-40-50	10	£9.00	50p
1C	25-33-40-50	6	£7.50	50p
1D	25-33-40-50	3	£5.50	40p
2A	4-16-24-32	12	£7.75	45p
2B	4-16-24-32	8	£6.50	45p
2C	4-16-24-32	4	£3.90	40p
2D	4-16-24-32	2	£2.75	30p
3B*	25-30-35	10	£7.50	60p
3C	25-30-35	5	£5.75	45p
3E	25-30-35	3	£3.25	45p
4A*	12-20-24	20	£13.00	75p
4B	12-20-24	10	£9.00	50p
4C	12-20-24	5	£5.75	50p
4D	12-20-24	2	£4.00	45p
5D	12-20-24	10	£10.50	45p
6A	3-12-18	20	£7.75	50p
5B	3-12-18	10	£4.75	45p
5C	3-12-18	5	£3.75	40p
5D	3-12-18	2	£2.75	40p
6A	48-56-60	1	£2.75	35p
6B	48-56-60	1	£2.75	55p
7A*	6-12	50	£12.50	55p
7B	6-12	20	£6.50	45p
7C	6-12	10	£3.75	35p
7D	6-12	5	£2.50	35p
8A	12-24	1	£1.75	35p
9A	17-32	1	£6.50	35p
10A*	9-15	2	£1.50	35p
11A	6-3	15	£3.75	35p
12A	30-25-0-25-30	2	£3.75	35p
13A*	12-0-12	8	£3.90	35p

Note: By using the intermediate taps many other voltages can be obtained.

Example: No. 1 7-8-10-15-17-25-33-40-50v.  
No. 2 4-8-12-16-20-24-32v.  
No. 5 3-6-9-12-15-18v.

## UNSHROUD TERMINAL BLOCK CONNECTIONS. All Primaries, 240v. Size H 5 x 4 1/2 x 3 1/2 In.

Type	Size	Amps	Price	Carr.
A	6-12	15	£4.00	45p
B	12-0-12	8	£4.00	45p
C	9-17	10	£4.00	45p
D	24	8	£4.00	45p

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Pri. 200-220-240v. Sec. 20-21-22-23-24-25v. 6a., 20-21-22-23-24-25v. 3.5a., 18-19-20-21-22-23v. 2a., 11-12-13-14-15-16v. 0.5a. twice 100-0-100v. 150 m/a 'C' Core. T. Top connections. £8.50 carr. 75p.

Pri. 200-220-240v. Sec. tapped 63-68-74v. 3a. and 6v. 4a. Open frame terminal block connections £2.50 P.P. 50p.

Pri. 200-220-240v. Sec. 37-40-43v. 5a., 105v. 300 m/a. twice. Oil filled potted type. £6.00 carr. 75p.

Pri. 200-220-240v. Sec. 39v. 8.6a., 38v. 2.6a. Oilfilled potted type. £8.50. carr. 75p.

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Pri. 220-240v. Sec. tapped 6-12v. 2a. fully shrouded. £1.75 P.P. 25p.

Pri. 200-220-240v. Sec. tapped 3-10-13v. 7a. Open frame. T. top connections £2.00 P.P. 35p.

Pri. 220-240v. Sec. 24.5-0-24.5v. 0.75a. 'C' Core. T. top connections £1.50 PP 25p.

Pri. 200-220-240v. Sec. 11-0-11v 176m/a. 'C' core. T. top connections 75p. P.P. 25p.

Pri. 220-240v. Sec. 22v. 0.9a. 21v. 0.06a. 'C' core T. top connections 75p. P.P. 25p.

REDCLIFFE Pri. 200-220-240v. Sec. 12-0-12v. 4a. 'C' core T. top connections £3.00 P.P. 40p.

Pri. 220-240v. Sec. 24v. 3a. 'C' core T. top connections £2.00 P.P. 35p.

Pri. 220-220-240v. Sec. 11v. 9a. 'C' core T. top connections £2.50 P.P. 50p.

Pri. 200-220-240v. Sec. 25-0-25v. 154 m/a. 7v. 1.35a. 'C' core T. top connections £1.25 P.P. 25p.

Pri. 240v. Sec. 14v. 6a. open frame. T. top connections £2.00 P.P. 35p.

Pri. 110-240-440v. Sec. tapped 24-26v. 8a. 6v. 1a. open frame type £3.50 carr. 50p.

G.E.C. Pri. 200-240-240v. Sec. tapped 59-61-63-64-67-69v. 10a. Fully tropicalised. Open frame terminal block connections. £5.50 carr. 50p.

Pri. 200-220-240v. Sec. tapped 56-58-60v. 3a open frame. Terminal block connections. £2.75 P.P. 50p.

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Pri. tapped 100-110-200-220-230-240-250v. Sec. 115v. 13.5 amps conservatively rated. Fully shrouded table top Connections. Sizes 13" x 10" x 8 1/2" Price £32.50. Carr. £2.

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1	2	3	4	1	2	3	4
32	3-6	2 c/o	63p*	700	6-12	1c/oHD	50p*
280	9-12	2 c/o	73p*	700	16-24	6 M	63p*
700	16-24	4M/2B	63p*	700	20-30	6 c/o	75p*
700	16-24	4 c/o	78p*	1250	24-36	4 c/o	63p*
700	12-24	2 c/o	63p*	2500	36-45	6 M	63p*
410	10-18	4 c/o	73p*	2400	30-48	4 c/o	50p*
700	15-35	2c/oHD	73p*	9000	40-70	2 c/o	50p*
				15k	85-110	6 M	50p*

(1) Coil ohms; (2) Working d.c. volts; (3) Contacts; (4) Price HD=Heavy Duty. All Post Paid. (\*including Base)

**12 VOLT D.C. RELAY**

Type 1: Three sets c/o contacts 5 amp. 78p incl. P. & P. (Similar to illustration below)

Type 2: One set c/o contacts 60p incl. P. & P.

Type 3: 4-8 volt 3 c/o HD, 67 ohm coil. 78p.

**'DIAMOND H' 230 VOLT A.C. RELAYS (Unused)**

Three sets c/o contacts rated at 5 amps. Price 50p, P. & P. 10p. (100 lots £40.00 incl. P. & P.)

**230 VOLT A.C. RELAYS M.f.g. 'Keyswitch'**

One set c/o contacts rated at 7.5 amps. Boxed. Price 40p, P. & P. 5p. (100 lots £32.00 incl. P. & P.)

**MINIATURE RELAYS**

9-12 volt D.C. operation. 2 c/o 500 M.A. contacts. Size only 1 in. x 1 1/2 in. Price 58p Post paid.

30-36 v. D.C. operation. 2 c/o 500 M.A. contacts. 3,200 ohm coil. Size only 1 1/2 x 1 1/2 in. 43p post paid.

**MINIATURE LATCHING RELAY**

Mfg. by Clare-Elliott Ltd. (Type F) 2 c/o permanent latching in either direction. Coil 1150 ohm. 15-30 v. D.C. New 73p, incl. P. & P.

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Test to I.E.E. Spec. Rugged metal construction, suitable for bench or field work, constant speed clutch. Size L. 8 in., W. 4 in., H. 6 in. weight 6 lb.

**500 VOLTS, 500 megohms £28 carriage paid**

**1,000 VOLTS, 1,000 megohms, £34 carriage paid**

**230V/240V COMPACT SYNCHRONOUS GEARED MOTORS**

Manufactured by either Sangamo, Haydon or Smith. Built-in gearbox.

5 RPM A/cw	3 RPH A/cw	20 RPH cw
1 RPH A/cw	6 RPH cw	
2 RPH cw	12 RPH c/w	

cw = Clockwise, A/cw = Anti-clockwise

Fraction of makers' price. All at 75p incl. P. & P.

**REVERSIBLE SPLIT PHASE MOTOR**

250 r.p.m. 100-115/210-240V A.C. 2 in. x 1 in. Ideal for rim-drive models, display etc. Extremely powerful for size including small capacitor. 75p. post paid.

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230/250V. A.C. 50 r.p.m. 7 lb/ins. Continuously rated. Less base £6.00 P. & P. 30p.

TYPE: SDI.S/89400/OM

230/250V. A.C. 50 r.p.m. 22 lb/ins. Continuously rated. Incl. base £7.00 P. & P. 30p. The above motors are new and unused.

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Speed 9,000 r.p.m. approx. or 3,200 r.p.m. if used with built-in governor, or variable speed over a wide range if used in conjunction with our Dimmer Switch, illustrated below. PRICE: £1.75 P. & P. 25p.

**600 WATT DIMMER SWITCH**

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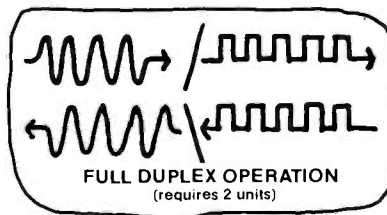
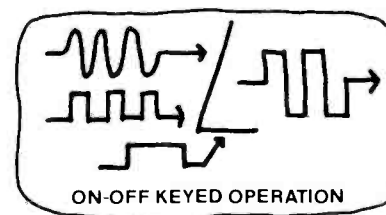
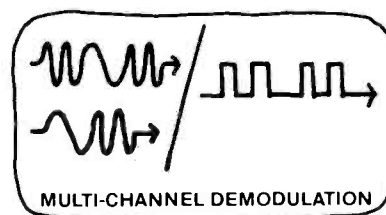
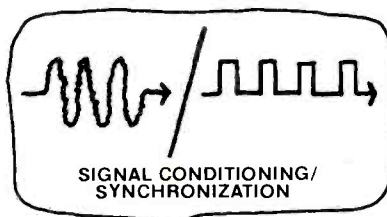
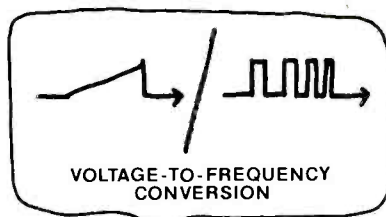
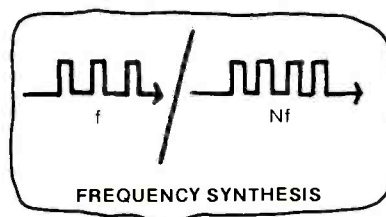
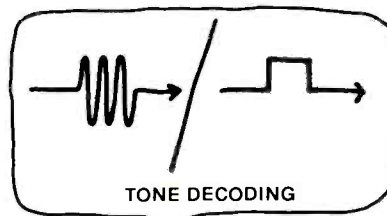
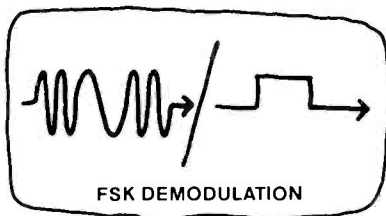
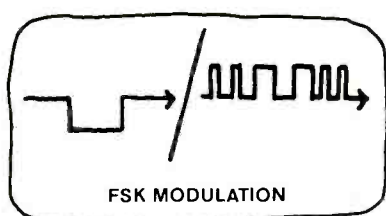
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QUANTITY	1-24	£5.25
	25-99	£4.85
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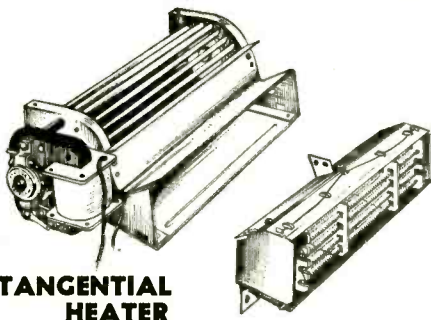


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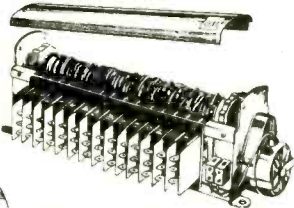


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P. & P. 40p.

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A bank of 15 micro-switches are each independently operated by 15 pairs of cams which in turn are individually adjustable to give switching periods of zero to 12 seconds with infinitely variable combinations. A mains synchronous motor drives the cam shaft at 1 rev. per 12 seconds (5 R.P.M.). Designed originally for vending machines at a cost of £15.00 plus. Many applications where continuous sequence programmes are required, such as lighting effects etc. New in original maker's cartons. First class value at £3.75 plus 25p P. & P.



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**"SORENG" MAINS SOLENOID.** 1" travel, 18 lb. pull (approx.). Size: 2 1/2" long x 2 1/2" x 2" high. Similar in appearance to "SORENG" £1.25. P. & P. 25p.

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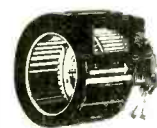
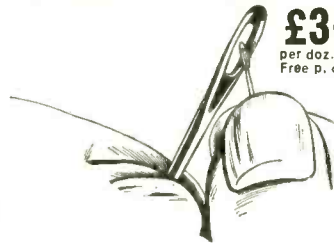
160Ω movement, 2" case, elliptic plastic front. Green-Red-Green uncalibrated scale. £1.50 each. Carriage Paid.

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OUR PRICE **£3.25** per doz. Free p. & p.



**"PRECISION FAN CO." (Smiths Industries) DOUBLE ENTRY CENTRIFUGAL FAN BLOWER.**—This is a beautifully balanced, particularly quiet running unit giving approx. 90 cubic ft./min. The motor is a 2 pole shaded pole 240v. Mycalex, drawing only 240ma. on run. Weight 2 1/2 lb. Sizes: Case dia. 3-1", width (case only) 3-1/25 in., 1-35 in. Offered well below makers price at £2.95 P. & P. 25p.

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95p EACH.  
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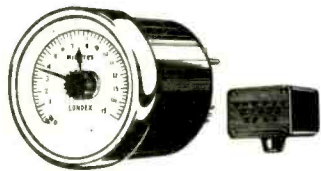
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A magnetically activated switch. Vacuum sealed in a glass envelope. Silver contacts normally closed, rated 3 amp at 120v, 1 1/2 amp at 240v. Size (approx.) 1 1/8" long x 1/2" dia. Ideal for Burglar Alarms, Security systems, etc., and wherever non-mechanical switching is required. New Lower Price. Only £2.10 for 12. £8 for 50 or £15 for 100 complete with magnet.

**NOW OPEN OUR NEW COMPONENTS SHOP 315 EDGWARE ROAD, LONDON W.2.**

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**ATLAS MIDGET PANEL LAMPS** unrivalled for indication purposes requiring a brilliant but tiny light source. Available with flange cap or wire ended in the following ratings: Capped: 6v. -1A. Uncapped: 4v. -25A., 6v. -1A., 6v. -2A. £1.20 per dozen or boxes of 50 at £4 per box.  
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**"HONEYWELL" V3 Series.** Flush micro-switch 10 amp. c/o. The slide panel is insulated. End plate size: 2" x 8". £1.50 per doz. Carr. Paid.



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BRAND NEW RELAYS by "SCHRACK" (Perspex enclosed).

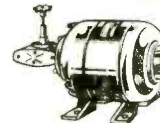
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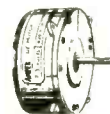
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Table listing various thyristor models and their prices.

VEROBOARD

Table listing Vero Board models and their prices.

RESISTORS

Table listing various resistor models and their prices.

“SCORPIO”

Capacitor discharge ignition system. (as published in Practical Electronics, Nov. 1971).

OPTOELECTRONICS

Table listing optoelectronic components like indicator lamps and diodes.

SLIDER POTENTIOMETERS

Table listing slider potentiometer models and their prices.

THERMISTORS

Table listing various thermistor models and their prices.

PANEL METERS table listing different meter sizes and their prices.

MULLARD C280 M/FOIL CAPACITORS table listing capacitor models and their prices.

Log. or Lin. With switch table listing switch models and their prices.

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1N3754	20p	2N3055	60p	2N5457	30p	AD162	40p	BC109	5	11p	NKT271	18p
1N5399	24p	2N3525	51p	2N5459	30p	*AD161/2	30p	BC110	4	25p	NKT274	19p
1N5402	23p	2N3405	40p	40239	71p	AF114	4	11p	3	11p	NKT275	25p
1N5407	35p	2N3673	55p	40231	89p	AF115	4	11p	3	11p	NKT403	66p
1R441	6p	2N3702	10p	40361	45p	AF116	4	11p	3	11p	NKT404	64p
1R404	5p	2N3703	10p	40362	45p	AF117	4	11p	3	11p	NKT405	83p
2N696	17p	2N3704	10p	40466	53p	AF118	4	11p	3	11p	NKT603F	32p
2N697	18p	2N3705	10p	40408	40p	AF119	4	11p	3	11p	NKT613F	32p
2N706	12p	2N3706	10p	40412	40p	AF120	4	11p	3	11p	NKT674F	28p
2N830	21p	2N3707	10p	40430	40p	AF121	4	11p	3	11p	NKT700	21p
2N1181	25p	2N3708	8p	40431	40p	AF122	4	11p	3	11p	NKT701	21p
2N1192	25p	2N3709	10p	40432	40p	AF123	4	11p	3	11p	NKT702	21p
2N1392	19p	2N3719	10p	40433	40p	AF124	4	11p	3	11p	NKT703	21p
2N1393	19p	2N3711	10p	40434	40p	AF125	4	11p	3	11p	NKT704	21p
2N1394	28p	2N3731	10p	40435	40p	AF126	4	11p	3	11p	NKT705	21p
2N1395	28p	2N3734	10p	40436	40p	AF127	4	11p	3	11p	NKT706	21p
2N1396	33p	2N3735	10p	40437	40p	AF128	4	11p	3	11p	NKT707	21p
2N1397	33p	2N3736	10p	40438	40p	AF129	4	11p	3	11p	NKT708	21p
2N1398	36p	2N3737	10p	40439	40p	AF130	4	11p	3	11p	NKT709	21p
2N1399		2N3738	10p	40440	40p	AF131	4	11p	3	11p	NKT710	21p
2N1400		2N3739	10p	40441	40p	AF132	4	11p	3	11p	NKT711	21p
2N1401		2N3740	10p	40442	40p	AF133	4	11p	3	11p	NKT712	21p
2N1402		2N3741	10p	40443	40p	AF134	4	11p	3	11p	NKT713	21p
2N1403		2N3742	10p	40444	40p	AF135	4	11p	3	11p	NKT714	21p
2N1404		2N3743	10p	40445	40p	AF136	4	11p	3	11p	NKT715	21p
2N1405		2N3744	10p	40446	40p	AF137	4	11p	3	11p	NKT716	21p
2N1406		2N3745	10p	40447	40p	AF138	4	11p	3	11p	NKT717	21p
2N1407		2N3746	10p	40448	40p	AF139	4	11p	3	11p	NKT718	21p
2N1408		2N3747	10p	40449	40p	AF140	4	11p	3	11p	NKT719	21p
2N1409		2N3748	10p	40450	40p	AF141	4	11p	3	11p	NKT720	21p
2N1410		2N3749	10p	40451	40p	AF142	4	11p	3	11p	NKT721	21p
2N1411		2N3750	10p	40452	40p	AF143	4	11p	3	11p	NKT722	21p
2N1412		2N3751	10p	40453	40p	AF144	4	11p	3	11p	NKT723	21p
2N1413		2N3752	10p	40454	40p	AF145	4	11p	3	11p	NKT724	21p
2N1414		2N3753	10p	40455	40p	AF146	4	11p	3	11p	NKT725	21p
2N1415		2N3754	10p	40456	40p	AF147	4	11p	3	11p	NKT726	21p
2N1416		2N3755	10p	40457	40p	AF148	4	11p	3	11p	NKT727	21p
2N1417		2N3756	10p	40458	40p	AF149	4	11p	3	11p	NKT728	21p
2N1418		2N3757	10p	40459	40p	AF150	4	11p	3	11p	NKT729	21p
2N1419		2N3758	10p	40460	40p	AF151	4	11p	3	11p	NKT730	21p
2N1420		2N3759	10p	40461	40p	AF152	4	11p	3	11p	NKT731	21p
2N1421		2N3760	10p	40462	40p	AF153	4	11p	3	11p	NKT732	21p
2N1422		2N3761	10p	40463	40p	AF154	4	11p	3	11p	NKT733	21p
2N1423		2N3762	10p	40464	40p	AF155	4	11p	3	11p	NKT734	21p
2N1424		2N3763	10p	40465	40p	AF156	4	11p	3	11p	NKT735	21p
2N1425		2N3764	10p	40466	40p	AF157	4	11p	3	11p	NKT736	21p
2N1426		2N3765	10p	40467	40p	AF158	4	11p	3	11p	NKT737	21p
2N1427		2N3766	10p	40468	40p	AF159	4	11p	3	11p	NKT738	21p
2N1428		2N3767	10p	40469	40p	AF160	4	11p	3	11p	NKT739	21p
2N1429		2N3768	10p	40470	40p	AF161	4	11p	3	11p	NKT740	21p
2N1430		2N3769	10p	40471	40p	AF162	4	11p	3	11p	NKT741	21p
2N1431		2N3770	10p	40472	40p	AF163	4	11p	3	11p	NKT742	21p
2N1432		2N3771	10p	40473	40p	AF164	4	11p	3	11p	NKT743	21p
2N1433		2N3772	10p	40474	40p	AF165	4	11p	3	11p	NKT744	21p
2N1434		2N3773	10p	40475	40p	AF166	4	11p	3	11p	NKT745	21p
2N1435		2N3774	10p	40476	40p	AF167	4	11p	3	11p	NKT746	21p
2N1436		2N3775	10p	40477	40p	AF168	4	11p	3	11p	NKT747	21p
2N1437		2N3776	10p	40478	40p	AF169	4	11p	3	11p	NKT748	21p
2N1438		2N3777	10p	40479	40p	AF170	4	11p	3	11p	NKT749	21p
2N1439		2N3778	10p	40480	40p	AF171	4	11p	3	11p	NKT750	21p
2N1440		2N3779	10p	40481	40p	AF172	4	11p	3	11p	NKT751	21p
2N1441		2N3780	10p	40482	40p	AF173	4	11p	3	11p	NKT752	21p
2N1442		2N3781	10p	40483	40p	AF174	4	11p	3	11p	NKT753	21p
2N1443		2N3782	10p	40484	40p	AF175	4	11p	3	11p	NKT754	21p
2N1444		2N3783	10p	40485	40p	AF176	4	11p	3	11p	NKT755	21p
2N1445		2N3784	10p	40486	40p	AF177	4	11p	3	11p	NKT756	21p
2N1446		2N3785	10p	40487	40p	AF178	4	11p	3	11p	NKT757	21p
2N1447		2N3786	10p	40488	40p	AF179	4	11p	3	11p	NKT758	21p
2N1448		2N3787	10p	40489	40p	AF180	4	11p	3	11p	NKT759	21p
2N1449		2N3788	10p	40490	40p	AF181	4	11p	3	11p	NKT760	21p
2N1450		2N3789	10p	40491	40p	AF182	4	11p	3	11p	NKT761	21p
2N1451		2N3790	10p	40492	40p	AF183	4	11p	3	11p	NKT762	21p
2N1452		2N3791	10p	40493	40p	AF184	4	11p	3	11p	NKT763	21p
2N1453		2N3792	10p	40494	40p	AF185	4	11p	3	11p	NKT764	21p
2N1454		2N3793	10p	40495	40p	AF186	4	11p	3	11p	NKT765	21p
2N1455		2N3794	10p	40496	40p	AF187	4	11p	3	11p	NKT766	21p
2N1456		2N3795	10p	40497	40p	AF188	4	11p	3	11p	NKT767	21p
2N1457		2N3796	10p	40498	40p	AF189	4	11p	3	11p	NKT768	21p
2N1458		2N3797	10p	40499	40p	AF190	4	11p	3	11p	NKT769	21p
2N1459		2N3798	10p	40500	40p	AF191	4	11p	3	11p	NKT770	21p
2N1460		2N3799	10p	40501	40p	AF192	4	11p	3	11p	NKT771	21p
2N1461		2N3800	10p	40502	40p	AF193	4	11p	3	11p	NKT772	21p
2N1462		2N3801	10p	40503	40p	AF194	4	11p	3	11p	NKT773	21p
2N1463		2N3802	10p	40504	40p	AF195	4	11p	3	11p	NKT774	21p
2N1464		2N3803	10p	40505	40p	AF196	4	11p	3	11p	NKT775	21p
2N1465		2N3804	10p	40506	40p	AF197	4	11p	3	11p	NKT776	21p
2N1466		2N3805	10p	40507	40p	AF198	4	11p	3	11p	NKT777	21p
2N1467		2N3806	10p	40508	40p	AF199	4	11p	3	11p	NKT778	21p
2N1468		2N3807	10p	40509	40p	AF200	4	11p	3	11p	NKT779	21p
2N1469		2N3808	10p	40510	40p	AF201	4	11p	3	11p	NKT780	21p
2N1470		2N3809	10p	40511	40p	AF202	4	11p	3	11p	NKT781	21p
2N1471		2N3810	10p	40512	40p	AF203	4	11p	3	11p	NKT782	21p
2N1472		2N3811	10p	40513	40p	AF204	4	11p	3	11p	NKT783	21p
2N1473		2N3812	10p	40514	40p	AF205	4	11p	3	11p	NKT784	21p
2N1474		2N3813	10p	40515	40p	AF206	4	11p	3	11p	NKT785	21p
2N1475		2N3814	10p	40516	40p	AF207	4	11p	3	11p	NKT786	21p
2N1476		2N3815	10p	40517	40p	AF208	4	11p	3	11p	NKT787	21p
2N1477		2N3816	10p	40518	40p	AF209	4	11p	3	11p	NKT788	21p
2N1478		2N3817	10p	40519	40p	AF210	4	11p	3	11p	NKT789	21p
2N1479		2N3818	10p	40520	40p	AF211	4	11p	3	11p	NKT790	21p
2N1480		2N3819	10p	40521	40p	AF212	4	11p	3	11p	NKT791	21p
2N1481		2N3820	10p	40522	40p	AF213	4	11p	3	11p	NKT792	21p
2N1482		2N3821	10p	40523	40p	AF214	4	11p	3	11p	NKT793	21p
2N1483		2N3822	10p	40524	40p	AF215	4	11p	3	11p	NKT794	21p
2N1484		2N3823	10p	40525	40p	AF216	4	11p	3	11p	NKT795	21p
2N1485		2N3824	10p	40526	4							



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2,500 ohm (okay 24V)—13p ea.

**S.T.C.** Brand New 2 pole c/o 6800 ohm coil—15p ea.

**CARPENTERS** polarised Single pole c/o 20 and 65 ohm coil as new, complete with base 37p ea.  
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Varley VP4 Plastic covers 4 pole c/o 5K—30p ea. 15K—33p ea.

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**COLVERN** 3 watt. Brand new, 5; 10; 25; 500 ohms; 1; 2.5; 5; 10; 25; 50k all at 13p ea.

**MORGANITE** Special Brand new, 2.5; 10; 100; 250; 500K; 2.5 meg. 1 in. sealed, 17p ea.

**BERCO** 2½ Watt. Brand new, 5; 10; 50; 250; 500 ohms; 1; 2.5; 5; 10; 25; 50K at 15p ea.

**STANDARD** 2 meg. log pots. Current type 15p ea.

**INSTRUMENT** 3 in. Colvern 5 ohm 35p ea.; 50k and 100K 50p ea.

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**RELIANCE**: 270; 470; 500 ohms; 10K at 35p ea. ALL BRAND NEW.

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Size 1x2½ ins.	Size 1½x5½ ins.
0.05mfd 2.5kV 50p ea.	0.01mfd 10kV 50p ea.
0.01mfd 5kV 40p ea.	0.002mfd 15kV 65p ea.
0.001mfd 10kV 50p ea.	0.0005mfd 20kV 60p ea.
Size 2½x6½ ins.	0.1mfd 4kV 35p ea.
0.05mfd 8kV 50p ea.	

**DUBILIER** 0.1mfd 5 KV; 0.1mfd 7.5 KV; 0.25mfd 7.5 KV; 0.5mfd 5 KV all at 50p ea. P. & P. 15p.

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OA2	0.85	R17	0.48	UC85	0.40	Z803A	1.25	5B4GY	0.75	6A86	0.37	6CH6	0.55	6K25	0.70
OB2	0.35	R19	0.37	UCF80	0.55	Z900T	0.95	5U4G	0.35	6A87G	0.80	6CL6	0.49	6LM6	1.50
PABC80	0.87	STV		UCH42	0.70	1L4	0.15	3V4G	0.45	6A7G	0.30	6D6	0.20	68A7	0.40
PC97	0.45	280/40	3.40	UCH81	0.33	1B5	0.40	6Y4G	0.30	6B26	0.25	6E8A	0.25	68A7GT	0.32
PC800	0.47	STV		UC183	0.60	1B5	0.40	5V3GT	0.35	6AX4GT	0.60	6F23	0.75	68C7GT	0.25
PC84	0.40	280/80	9.00	UC183	0.60	1B5	0.40	5Z3	0.55	6AX5GT	0.70	6F33	1.50	68G7	0.35
PC88	0.50	STV		UV11	0.50	1T4	0.22	5Z4	0.75	6B7	0.40	6H6M	0.20	68J7	0.37
PC189	0.55	TT21	3.00	UF80	0.38	1X2A	0.40	5Z4GT	0.40	6BK7	0.60	6JAWA	0.75	68J7GT	0.32
PC200	0.75	U25	0.72	UF89	0.40	1X3B	0.50	6AB7	0.30	6B46	0.25	6J6	0.40	68K7	0.46
PCF80	0.30	U26	0.72	U1	0.83	2K25	7.50	6AC7	0.30	6B66	0.50	6J5GT	0.25	68L7GT	0.32
PCF82	0.33	U27	0.50	UL41	0.40	3A4	0.35	6AK5	0.30	6B16	0.45	6J6	0.20	68N7GT	0.32
PCF84	0.40	U191	0.70	UL84	0.40	3A4	0.35	6AK8	0.32	6B47A	0.40	6J7G	0.35	68Q7	0.39
PCF86	0.42	U801	0.80	U15	0.55	3D6	0.15	6AL5	0.15	6B7R	0.85	6J7M	0.40	68Q7GT	0.35
PCF201	0.73	UABC80	0.35	UY41	0.43	3Q4	0.45	6AL5W	0.40	6B8W	0.85	6K8GT	0.58	6V6G	0.17
PCF801	0.45	UAF42	0.55	UY85	0.40	384	0.35	6AM6	0.30	6B9W	0.85	6K8GT	0.58	6V6GT	0.40
PCF802	0.50	UBC41	0.46	VR105/30	0.35	3V4	0.45	6AN8	0.50	6B9W	0.85	6K7	0.32	6X4	0.30
PCF805	0.80													6X5G	0.30
PCF806	0.70													6X5GT	0.37
PC181	0.40													6Y6G	0.60
PC182	0.35													6-30L2	0.80
PC183	0.60													6Z4	0.36
PC184	0.42													7B7	0.45
PC185	0.43													7Y4	0.60
PC186	0.42													9D6	0.37
PC187	0.50													11E2	2.80
PC188	0.48													12A76	0.30
PC189	0.40													12A77	0.30
PC190	0.40													12A78	0.30
PC191	0.40													12A79	0.30
PC192	0.40													12A80	0.30
PC193	0.40													12A81	0.30
PC194	0.40													12A82	0.30
PC195	0.40													12A83	0.30
PC196	0.40													12A84	0.30
PC197	0.40													12A85	0.30
PC198	0.40													12A86	0.30
PC199	0.40													12A87	0.30
PC200	0.40													12A88	0.30
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PC202	0.40													12A90	0.30
PC203	0.40													12A91	0.30
PC204	0.40													12A92	0.30
PC205	0.40													12A93	0.30
PC206	0.40													12A94	0.30
PC207	0.40													12A95	0.30
PC208	0.40													12A96	0.30
PC209	0.40													12A97	0.30
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PC213	0.40													12A101	0.30
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PC216	0.40													12A104	0.30
PC217	0.40													12A105	0.30
PC218	0.40													12A106	0.30
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PC222	0.40													12A110	0.30
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PC225	0.40													12A113	0.30
PC226	0.40													12A114	0.30
PC227	0.40													12A115	0.30
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PC233	0.40													12A121	0.30
PC234	0.40													12A122	0.30
PC235	0.40													12A123	0.30
PC236	0.40													12A124	0.30
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PC239	0.40													12A127	0.30
PC240	0.40													12A128	0.30
PC241	0.40													12A129	0.30
PC242	0.40													12A130	0.30
PC243	0.40													12A131	0.30
PC244	0.40													12A132	0.30
PC245	0.40													12A133	0.30
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PC247	0.40													12A135	0.30
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OA73	0.07	OC76	0.25	12MT10	0.33	6FR3	0.45	IC113	0.10	GET115	0.45
OA74	0.07	OC81	0.20	1ZT5	0.67	12FR60	0.73	BC118	0.20	GET116	0.50
OA79		OC81D	0.20	1ZT10	0.63	40954	1.25	BCY72	0.15	GEX66	1.50
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OA210	0.25	OC84	0.25	2N1307	0.25	AC127	0.25	BB8	0.47	8D928	0.31
OA211	0.30	OC122	0.50	2N1347	0.64	AC128	0.20	BBY29	0.25	8D938	0.25
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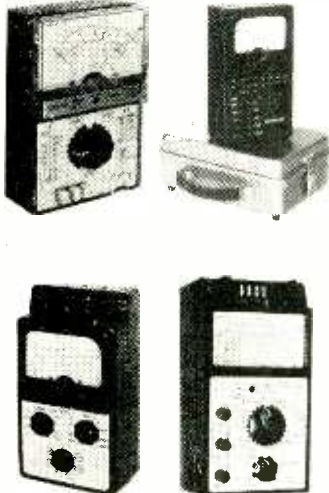


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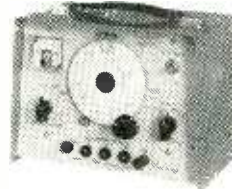
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963	£ 11.00	964	£ 11.00	965	£ 11.00
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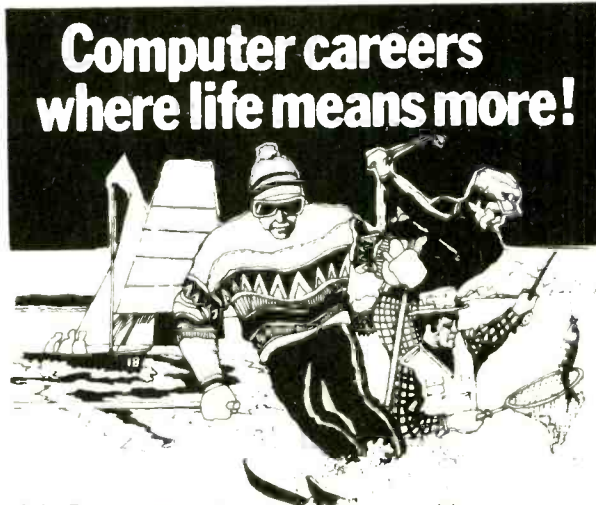
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## Computer careers where life means more!

Join Burroughs and you can have an exciting computer career and live on the threshold of the Scottish Highlands. You can commute from excellent residential areas, enjoy golf, angling, ski-ing and yachting and send your children to excellent schools and universities in the area. You can work on viable research and development programmes in an expanding environment in the computer and peripheral field. Due to expansion we have vacancies for

### SENIOR ELECTRONIC ENGINEERS

Experienced in electronics packaging and the design of digital and M.O.S./L.S.I. circuits and power supplies.

*Applicants should have an Honours degree and experience in the above field.*

*Excellent salaries and relocation expenses will be offered.*

*Apply in writing to:* Engineering Recruitment Officer,  
 Burroughs Machines Limited,  
 Cumbernauld, Scotland.

**Burroughs**   
 CUMBERNAULD SCOTLAND

### H.M. GOVERNMENT COMMUNICATIONS CENTRE

has vacancies for

## COMMUNICATION OPERATORS

Posts are available entailing watchkeeping on a rota basis providing secure employment with superannuation benefits. There are prospects of service abroad. It is essential to be able to drive a car.

**QUALIFICATIONS.** Selected candidates will be invited to interview and test and will be required to:

(a) Send and receive morse at 25 w.p.m.  
 (b) Display knowledge of radio theory, maintenance and repair to the equivalent standard of:

i) PMG—Class 1  
 or ii) The Maritime Radiocommunications General Certificate  
 or iii) City and Guilds Course 49.

The ability to touch-type on a standard teleprinter keyboard is desirable.

**AGE.** Candidates should generally be aged 30 or under.

**SALARY.** Starting salary according to age and experience.

**APPLICATIONS.** With personal details, qualification and experience to:

The Personnel Officer (Communication Operators),  
 H.M.G.C.C.,  
 Hanslope Park, Near Wolverton, Buckinghamshire.

[2272]

## Middlesex Polytechnic

### Enfield Microelectronics Centre

#### Short Practical Courses in 1973

These day and evening courses which have become well-known and popular in previous years are being offered again together with new courses designed to cater for modern technology and industrial trends.

- ★ Integrated Circuit Technology
- ★ Computer Aided Analysis and Design
- ★ Hybrid Microelectronics and Thick Films
- ★ MOS Devices and Technology

In every case emphasis is put on practical experience for the participant.

For full details and application forms contact The Admissions Office, (Enfield Short Courses Dept. W.W.1), Middlesex Polytechnic, P.O. Box 40, Enfield, Middlesex EN3 4SF. Tel: 01-804 8131.

2243

### BROMLEY GROUP HOSPITAL MANAGEMENT COMMITTEE

## ELECTRONICS MAINTENANCE TECHNICIAN

for the acceptance, testing and maintenance of a variety of electronic control and communication equipment and electro-medical apparatus.

Salary £1,896 by increments to £2,448. Applicants must hold, as a minimum, O.N.C. or O.N.D. in Electronics or Light Current Electrical Engineering or the City & Guilds Final Certificate in Telecommunications Engineering. Practical experience in industry or the armed services is essential; hospital experience an advantage but training with manufacturers possible. Own transport, for which mileage is payable, essential.

Applications, with details of training, experience, age, etc., and naming two referees, to reach the Group Engineer "Bassetts", Starts Hill Road, Farnborough, Kent (Tel.: Farnborough 53333) not later than 21st January, 1973. No accommodation available for married applicants.

[2237]



# Shore jobs for Radio Officers.

If you'd like a job ashore, at a United Kingdom Coast Station, the Post Office will start you off on £1,350—£1,710, depending on age, with annual rises up to £2,310 (compulsory pension contributions are included in these amounts). In addition you would receive payments that can be as much as £300 or more a year for attendances during evenings, nights, Saturday afternoons and Sundays. Opportunities also exist for overtime.

There are good prospects for promotion to higher posts.

You will need to be 21 or over, with a 1st Class Certificate of Competence in Radiotelegraphy issued by the Postmaster General, or the Ministry of Posts and Telecommunications, or a

Radiocommunication Operator's General Certificate issued by the Ministry of Posts and Telecommunications, or an equivalent certificate issued by a Commonwealth administration or the Irish Republic.

Find out more by writing to:  
The Inspector of Wireless Telegraphy,  
IMTR, Wireless Telegraph Section,  
Union House, St. Martins-le-Grand,  
London, EC1A 1AR.

## Post Office Telecommunications

L36

### THAMES CONSERVANCY

Applications are invited for the following posts in the Chief Engineer's Department at Reading:—

#### ELECTRONICS ENGINEER

(Salary S.O. Grade 1—2 - £2565 to £3324 p.a.)

who will be required to lead a sub-section applying engineering science in the field of Water Resources. The person appointed should be a corporate member of an appropriate Engineering Institution, and will be involved in the following work:—

- (i) the establishment of a major system of telemetry monitoring hydrological parameters throughout the Thames Basin;
- (ii) the progressive development of electric analogue models of hydrological systems;
- (iii) the development of hydrometric instruments;
- (iv) digital computer application.

Knowledge and experience of telecommunications and telemetry is essential, whilst post graduate qualifications and experience of computer programming would be an advantage.

#### ELECTRONICS TECHNICIAN

(Salary AP 2—3 - £1530 to £2100 p.a.)

required for the maintenance of a system of telemetry throughout the Thames Basin, the repair of Hydrometric instruments and the construction of electric analogue models. O.N.C. in Electrical Engineering or City & Guilds Electronics Technician's Certificate desirable. Previous experience of telemetry would be an advantage.

Applications should be submitted in writing, giving details of age, marital status, qualifications and experience, to the undersigned as soon as possible.

E. J. BRETTELL, Chief Engineer,  
Chief Engineer's Headquarters,  
Thames Conservancy,  
De Bohun Road, READING, Berks.

[2242]

### TELEVISION ENGINEER

required

to join a small but enthusiastic team  
operating a

## Television Unit for Horseracing

If you have an HNC, City & Guilds, or equivalent qualification and have experience in operating and maintaining outside broadcast television equipment and VTRs together with a willingness to travel and to work in a demanding field

THEN

THIS COMPANY OFFERS YOU

- 1 the opportunity to join an organisation that is forward looking and is planning to develop and expand in the field of television and electronics
- 2 a job that is located in varied surroundings on British racecourses
- 3 a basic salary of between £2,500-£2,750 plus expenses when on location.

If you are interested please write or telephone for a Company form to Mr. F.T. Dixon, Racecourse Technical Services Limited, 88 Bushey Road, London SW20: Tel.: 01-947 3333.

[2241]

**REDIFON** is consolidating its resources in Crawley.

**REDIFON**, having recently won some large orders, is enjoying a large expansion programme.

**REDIFON** offers attractive opportunities and competitive salaries.

In particular in our new look Customer Service Department we require:—

### TECHNICAL AUTHORS

Redifon require T.A.'s for its flight simulation projects. This is varied and interesting work in a highly sophisticated industry. Some knowledge of electro-mechanical and electrical systems is necessary; a digital techniques background would be advantageous. Though formal authorship qualifications are not necessary, clarity of expression and a maintenance experience background are desirable.

### CHECKER/PROOF READER

(Air publications and Civil manuals, technical proposals, etc.)

Check laymark camera copy against draft material for errors, layout and general quality of work.

### EDITORIAL ASSISTANT (Paste-up Artist)

Responsible for preparation of material for printing Civil manuals to R.F.S.L. requirements and for printing air publications to prescribed requirements. Involves the recording, preparing of artwork and re-touching of original artwork. The submission of artwork text and illustrations, mounting of negatives on masking sheets and pasting up line illustrations in text as necessary.

### SPARES PROVISIONING CLERK

Responsible for receiving and preparing spares orders, liaising with customers, suppliers, shipping, etc., despatch follow up and organising appropriate records. Good customer approach necessary. Ability to read parts lists and identify electrical electro-mechanical details. Training will be given.

### SPARES SCHEDULING CLERK

To assemble detailed break-down data and associated information from which spares lists and recommendations are produced. Production of documentation to plan and time scale. Knowledge of electrical electro-mechanical parts needed.

Apply Personnel Officer, **REDIFON FLIGHT SIMULATION LIMITED**, Gatwick Road, Crawley, Sussex.  
Telephone Crawley 28811



A Member Company of the Rediffusion Organisation

## OPPORTUNITIES AT DYMAR

Continued expansion at Dymar Electronics has produced the following interesting positions—

### ELECTRONIC ENGINEER

An electronic development engineer is required to join a team of young enthusiasts engaged in the design of a new generation of HF communications and associated equipment. Qualifications should be at least to HNC level, although special consideration will be given to relevant experience. Familiarity with the design of medium power transmitters would be an advantage.

Salaries, which will be commensurate with experience, will be negotiable and there are attractive fringe benefits.

Written applications, giving brief career details, should be sent to:

**G. C. Holden, Chief Engineer HF Division, Dymar Electronics Limited,**  
Colonial Way, Hertfordshire WD2 4LA.

**DYMAR**

the name in radiotelephones

2280

### INSTRUMENT TEST ENGINEER

A test engineer is sought to assume responsibility for final testing of the company's range of instruments. A wide selection of products provides interesting and challenging work for an engineer with experience in this specialist field.

### LEEDS (ST JAMES'S) UNIVERSITY HOSPITAL MANAGEMENT COMMITTEE

A new post has been established for an

### X-Ray Maintenance Technician (Medical Physics Technician III)

at St James's Hospital

The duties of the successful candidate will include maintenance, repair and development of X-Ray, machinery. Opportunities exist for developing knowledge and skills by attending courses, conferences and exhibitions.

A full Medical Physics Department is being set up and prospects may exist in other fields. Salary scale £1,602-£2,076.

Whitley Council Conditions of service. Applications in writing stating age, experience etc. and giving the names of two referees to the Group Personnel Manager, St James's Hospital, Leeds LS9 7TF as soon as possible.

[2239

## RADIO OFFICERS

DO YOU HAVE

PMG 1  
PMG 11  
MPT  
2 YEARS OPERATING EXPERIENCE

POSSESSION OF ONE OF THESE QUALIFIES YOU FOR CONSIDERATION FOR A RADIO OFFICER POST WITH THE COMPOSITE SIGNALS ORGANISATION

On satisfactory completion of a 7-month specialist training course, successful applicants are paid on scale rising to £2,365 p.a.; commencing salary according to age — 25 years and over £1,664 p.a. During training salary also by age, 25 and over £1,238 p.a. with free accommodation.

The future holds good opportunities for established status, service overseas and promotion.

Training courses commence at intervals throughout the year. Earliest possible application advised.

Applications only from British-born UK residents up to 35 years of age (40 years if exceptionally well qualified) will be considered.

Full details from:

**Recruitment Officer (TRO. 2.)**  
**Government Communications Headquarters**  
**Room A/1105**  
**Oakley Priors Road**  
**CHELTENHAM Glos GL52 5AJ**  
**Telephone: Cheltenham 21491 Ext 2270**

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City of London Polytechnic

## TECHNICIAN

A vacancy now exists for a Technician in the Psychology Section of the Sir John Cass School of Science and Technology. Candidates should be suitably qualified, preferably in electronics, and must be able to construct and operate a wide range of apparatus for use in the investigation of Human Behaviour. Experience in the development and fault-tracing of circuits would be an added advantage.

Salary scales:

Junior Technician £666 (at age 18 years) to £1,125.

Technician £1,107 (at age 21 years) to £1,557. Starting salary depending upon age, qualifications and experience.

Plus London Weighting Allowance of £174 per annum.

Apply in writing, giving full details and with the names and addresses of two referees, to Dr. I. N. Balanescu, Principal Lecturer in Charge of Psychology, City of London Polytechnic, Central House Annexe, Whitechapel High Street, London E1 7PF. Telephone 01-283 1030. Extension 486. [2158



## FAULT FINDERS

British Radio Corporation is one of the industry's leading manufacturers of unit/audio equipment for distribution both in this country and to a thriving export market. In order to cope with the continuing expansion it is necessary to engage additional technical staff.

Applicants for these positions must be capable of diagnosing faults in radio, radiogram and hi-fi equipment, and will preferably hold an appropriate Electronics qualification and will already have experience in this field. Successful candidates will be offered an excellent rate of pay and promotion prospects.

Written applications in the first instance to:

**PERSONNEL MANAGER,  
BRITISH RADIO CORPORATION LTD.,  
43/49 FOWLER ROAD,  
HAINAULT,  
ILFORD,  
ESSEX**

2252

## TECHNICAL WRITERS

Do you want an attractive salary and a choice working location in South Germany near Stuttgart? The world's leading manufacturer of precision electronic test and measurement equipment and systems offers these and other outstanding benefits to the Technical Writers who join our technical publications group. You may qualify if you have a sound background in electronics and are an experienced writer, preferably in both service and promotional fields, some knowledge of German would also be advantageous. Please write or phone (reverse charges).

HEWLETT  PACKARD

Hewlett-Packard GmbH, 703 Böblingen,  
Herrenberger Str. 110, Germany,  
Telephone 07031/6671. 2268

## H.F. Development Engineers

International Marine Radio Company is a member of a world-wide organisation, and is a Company leading in the design and manufacture of radio communications equipment for marine applications.

We require development engineers at both senior and junior levels to work on new projects for H.F. single sideband receivers and transmitters.

These positions require a sound knowledge of radio communications circuit design, and some development experience on equipments for the M.F. and H.F. bands would be an advantage.

Candidates should preferably be qualified to either HNC or degree standard, but the ability to demonstrate a professional outlook and to make an immediate contribution to the projects by working independently and accepting the responsibility this entails will be our major requirement.

Apply by telephone or in writing to The Personnel Manager, International Marine Radio Company Limited, 1 Peall Road, Croydon, CR9 3AX. Telephone 01-684 9771.

**ITT** Marine

2244

## Television Engineers

Thames Television has vacancies for Television Engineers to work in the Central Technical area of their Euston Studios in London.

Candidates aged 20 to 30 should have a knowledge of, and an interest in, all aspects of colour television engineering and preferably be educated to HNC standard.

Initial salaries will be related to previous experience and range from £2,058 per annum to £2,890 per annum.

Please apply in writing, giving brief details of age, qualifications and experience.

The Personnel Officer,  
Thames Television Limited,  
Teddington Lock,  
Teddington,  
Middlesex.

**THAMES**

2274

# Magnetic Tape Recording

Not less than £2,700 p.a.

The Central Research Laboratories of EMI Limited are carrying out a study of Magnetic Tape for airborne data recording, and require an engineer who is experienced in tape recording.

The work involves a study of the characteristics and performance of magnetic tape under high environmental conditions.

Candidates preferably aged between 28 and 40, should possess a BSc. degree in Physics or Electronic Engineering or an equivalent qualification. They should be familiar with digital encoding techniques and also be able to design and construct laboratory apparatus suitable for the study of the physical

parameters of magnetic tape.

**Experience in magnetic tape recording is essential.**

Starting salary will not be less than £2,700 and there is a contributory pension scheme. Assistance will be given towards re-location.

Please write giving brief details of experience to: **C. W. T. Mott, Chief Recruitment Officer, EMI Limited, 135 Blyth Road, Hayes, Middlesex.**



International leaders in Electronics, Records and Entertainment.

## TELEVISION SERVICE ENGINEER

We are an expanding Television Rental and Retail Company with a vacancy for an additional qualified service engineer. Suitable applicant will preferably have some colour experience, be responsible to the Service Manager, have a clean driving licence and be eligible for a spacious rent free flat.

Apply:

### Hydes of Chertsey Ltd.

56/60 Guildford Street, Chertsey, Surrey. Phone: Chertsey 63243

[2180]

## SOUTHEND-ON-SEA MUNICIPAL AIRPORT

### RADAR/RADIO ENGINEER

required with experience in maintenance of 3 c.m. and 10 c.m. Radar, VHF communications and recording equipment and navigational aids. Possession of appropriate City & Guilds or National Certificates desirable. Salary according to Technical 4/5 Scales, £1,530-£2,100.

Written applications, giving age, experience and qualifications, to the Airport Commandant, Municipal Airport, Southend-on-Sea, Essex.

[2238]

**MEN!**  
**£50 p.w.**  
**can be yours**

**Jobs galore!** 144,000 new computer personnel needed by 1977. With our revolutionary, direct from-America, course, you train as a Computer Operator in only 4 weeks!

Pay prospects? £2500 + p.a. After training, our exclusive appointments bureau — one of the world's leaders of its kind — introduces you **FREE** to world-wide opportunities. Write or phone **TODAY**, without obligation.

**London Computer Operators Training Centre**  
P13, Oxford House, 9-15, Oxford Street, W.1.  
Telephone: 01-734 2874  
127, The Piazza, Dept. P13, Piccadilly Plaza, Manchester 1.  
Telephone: 061-236 2935

2281

## LEEDS (ST. JAMES'S) UNIVERSITY HOSPITAL MANAGEMENT COMMITTEE ST. JAMES'S HOSPITAL

### MEDICAL PHYSICS TECHNICIAN GRADE 3

Candidates for this post must possess a thorough knowledge of electronics preferably as applied to medicine.

An applicant with adequate industrial experience of several years would be considered.

The salary scale is £1602 increasing by annual increments to a maximum of £2076. Candidates from outside the Health Service will commence at the minimum except in exceptional circumstances. Whitley Council conditions of service.

Applications in writing stating age, qualifications, experience etc. and giving the names of two referees to the Group Personnel Manager, St. James's Hospital, Leeds LS9 7TF.

[2261]

## SENIOR

### DESIGN ENGINEER

Required by PROGRESSIVE LONDON BASED COMPANY IN **ELECTRONIC MUSICAL INSTRUMENT FIELD** with experience and specialised knowledge of Electronic Organs, Semi-Conductors and Synthesiser Techniques. Salary negotiable but commensurate with responsibility of the position.

All replies will be treated in strictest confidence. Box No. WW 2267.

## ARTICLES FOR SALE

### 100KHZ FREQUENCY MARKER OSCILLATOR

Crystal Controlled  
TTL Compatible.  
5V DC Input. £4.25 each.

For details of these or our Quartz Crystal Units send to:—

**Crystal Electronics Ltd.**

Cromwell House, Third Avenue, Millbrook, Southampton, SO10LE.  
Tel: Southampton (0703) 76361.

MANUFACTURERS OF QUARTZ CRYSTALS AND CRYSTAL PRODUCTS

2164

## SURREY COUNTY COUNCIL

### SENIOR TECHNICIAN

Educational Television Unit  
Guildford County Technical College

To be responsible to the Chief Technician for the daily operation and maintenance of black and white and colour television equipment, including cameras, monitors, vision and sound mixers, video tape recorders, etc.

Candidates should preferably have practical experience with vidicon cameras and helical-scan recorders. An interest in photography is desirable, but not essential.

The unit operates a well equipped closed circuit television studio and mobile system producing and distributing educational material for use within the College and else-

where in the County.

Candidates should have reached the Final year of the course in Radio, Television and Electronics Servicing (City and Guilds 172) or have completed Part 1 of the Radio Television and Electronics Technicians Course (City and Guilds 272).

Salary: £1311-£1530, or £1530-£1803, plus qualification allowance where appropriate.

**Application form and further details, on receipt of S.A.E., from The Principal, Guildford County Technical College, Stoke Park, Guildford.**

[2284]



★ ★ **ARTICLES FOR SALE** ★ ★

**1/2 MILLION MUST GO!** **NEW - Guaranteed & boxed TV VALVES** **!PRICE BARRIER SMASHED!**

**Cheapest Available Anywhere**

**25p**

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MANY OTHERS IF NOT LISTED SEND 30p P.O.

**OUR ASSTD. BOX 100 OF TOP TWENTY INCLUDES VALVES FROM A, B, and C.**

SEND PO, CHEQUE or MO to: **SOUTHERN MACHINE SERVICES** 285 MORLAND ROAD, CROYDON, SURREY, CR0 6HE Telephone 01-653 4863 or 01-656 0374

2279

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**ELEKTRON SUPPLIES** 259 CARDINGTON RD., BEDFORD, BEDS.  
Mail Order Only. C.W.O. P. & P. 7p. 10% Discount on 25+.

**PRIMAX Soldering GUN** INSTANT HEAT 6 Seconds! Twin Spotlight

Can also be used To cut and seal P.V.C. Plastics, Nylon Rope etc.:-  
60 Watt Gun @ 108/- p & p 5/  
100 Watt Gun @ 140/- p & p 5/.

**S. KEMPNER LTD 421/3 HIGH RD N12 346-6222**

**ELECTRONIC BARGAINS**

NEW fully electronic voice operated Auto-fade unit.  
NOW with built-in Mic. pre-amp for Auto music fade system.  
**£6-00 per kit. £8-75 ready to use.**

NEW quality stereo pickup Pre-amps with tone controls.  
NOW on 90mm. square fibre glass board (for MAG., CER. or CRY.).  
**£9-00 per kit. £12-00 ready to use.**

NEW expandable audio mixer cabinets.  
NOW offer economical low cost system.

Please add 25p for postage and packing.  
S.A.E. for details.

**PARTRIDGE ELECTRONICS** 23-25 HART ROAD BENFLEET, ESSEX SS7 3PB [2269]

**CUT THE COST OF SERVICING WITH LONG LIFE TOSHIBA VALVES**

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EF.183	29.5	8.5	38.0
EF.184	29.5	8.5	38.0
EH.90	27.0	7.5	34.5
PC.900	22.5	6.5	29.0
PCC.89	31.5	9.0	40.5
PCC.189	33.5	9.5	43.0
PCF.80	27.0	7.5	34.5
PCF.86	33.0	9.5	42.5
PCF.801	34.5	10.0	44.5
PCF.802	33.0	9.5	42.5
PCL.82	30.0	8.5	38.5
PCL.84	26.5	7.5	34.0
PCL.85	30.5	8.5	39.0
PCL.86	30.0	8.5	38.5
PFL.200	41.5	12.0	53.5
PL.36	45.5	13.0	58.5
PL.84	22.0	6.5	28.5
PL.504	45.0	13.0	58.0
PL.508	50.0	14.5	64.5
PL.509	80.0	23.0	103.0
PY.88	25.5	7.5	33.0
PY.500A	50.0	14.5	64.5
PY.800	23.0	6.5	29.5

Valves packed individually in labelled White boxes.  
Subject to settlement discount 5% of "Goods" content 7 days and 2% monthly.

**CPC**

Write or Phone **COMBINED PRECISION COMPONENTS (PRESTON) LTD.** 3 Moor Park Avenue, Preston PR1 6AS, Lancashire Tel: Home Sales Division, Preston, 0772 56347. Export Division, Preston, 0772 54157. Telex 47129.

New Price List from 11th October '72

**REED UNITS**

Contains 31 1 1/4 250V reeds mounted round a drum with magnet inside, also resistors, plugs etc. Only £1 (25p). 2 for £1.65 (35p). Ferric Chloride 1lb 40p (15p). 10lbs £3.50 (40p). BC107-8-9 8p or 14 for £1. 2N3055 35p. 709C 25p. 741C 25p. 723C 40p. 2N1613 12p. 2N3819 26p. CASED AMPLIFIERS. 4 valve, 2 watts orp for 20pV up 7 x 4" 3 ohm speaker, also non-standard single motor solenoid operated tape deck. All in polished oak-faced cabinet. £3 (£1) Resistor packs: 300 5% 60p (15p); 200 5% Hi-stab 60p (12p). 100 1% & 2% 60p (8p); 100 Metal oxide 60p (8p). One of each £2 (25p). 3W 5% R's 270, 470, 6k8, 15k, 27k, 33k, 82k, 100 for 50p (25p). Meters: 2 1/2" 500V dc 40p (10p); 2 1/2" 10V ac 40p (10p). Others available, state requirements. Croton Light guide, 64 lbre £1 per meter. TEST GEAR: TF144g £12; TF142D £10; TF142E £14; BSR Audio Oscillator 0-16kHz £9; Decade Res. 0-11110 ohms £7.50. All post extra.

Post in brackets, small parts 3p; SAE List, details.

**GREENWELD (W9) 24, Goodhart Way, W. Wickham, Kent.**  
Tel 01-777 2001 up to 10.30pm. Shop at 21 Deptford Broadway SE8, open Sats. Tel 01-692 2009.

**UNISELECTOR SWITCHES**

24 volt, 10 position, 3 bank, c/w suppressing condenser and supplied c/w base plug in jacks. Uniselector only, £1-25, p. & p. 25p. C/w base plug in jack, £1-65, p. & p. 25p. Ditto, as above, 12 position, 3 bank. Uniselector only, £1-35, p. & p. 25p. C/w base plug in jack, £1-75, p. & p. 25p.

Ditto, as above, 25 position, 6 bank. This uniselector is fitted to a front panel and has a distribution board fitted in the rear and is wired from the uniselector to the distribution panel. Limited number only. £2-75 each, p. & p. 50p.

24 volt, Radiospares type 22, relays c/w bases, fitted to small panel (2 per panel), 60p per pair, p. & p. 15p.

Glass Fibre plug in digital boards. New. Designed to take divide by 10 I.C.'s and nixi tube IC driver, c/w CCT instructions, 28p each, p. & p. 3p.

New Numerical 0-9 Indicator tubes, c/w data, £1-35 each, p. & p. 6p.

Plastic Holders designed to hold the above tube and will fit to the PCB as above, 8p each, p. & p. 4p.

**G. T. F. ELECTRONICS**  
9 Ernie Road, Calne, Wilts. SN11 9BT.  
Phone: Calne 3360. 2273



**Trampos electronics**

All Brand New. Money Back Guaranteed. Fast Service.  
**DIGITAL INDICATORS** 5V type. 7 segment 0-9 DP socket. & red filter £1.39 LED type £3.  
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**stereo hi-fi**

**QUAD AUDIO:** 4 chan from 2 chan matrixing 1C (not xover) £2.67.  
**AD MAGNETIC CARTRIDGE:** 20-20 KHZ 5mV Diamond £4.19.  
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**Fresh stock — Fully tested**  
 Close tolerance capacitors by well-known manufacturer. Good stability and very low leakage. All 83V d.c.  
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 2.2µF: ±5% 50p; ±2% 60p; ±1% 75p  
 4.7µF: ±5% 70p; ±2% 90p; ±1% 115p  
 6.8µF: ±5% 95p; ±2% 115p; ±1% 150p  
 10µF: ±5% 110p; ±2% 140p; ±1% 180p  
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BC108A	0.07	1.65	3.00	5.10	BFX85	29 19.60
BC108B	0.07	1.65	3.00	5.10	BFX86	24 17.00
BC108C	0.07	1.65	3.00	5.10	BFX87	25 17.20
BC109	0.05	1.50	2.50	4.00	BFX88	20 14.10
BC109B	0.07	1.65	3.00	5.10	BFY60	18 14.00
BC109C	0.07	1.65	3.00	5.10	BFY61	18 13.00
BC113	0.05	2.20	3.50	5.80	BFY62	18 12.50
BC114	0.11	2.40	3.80	5.85	BFY66	34 19.80
BC115	0.12	2.60	3.70	5.90	BFY64	40 26.25
BC116	0.13	2.80	3.90	6.05	BFY78	40 27.50
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BC132	0.15	3.20	6.30	9.00	BSX27	34 25.25
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BC135	0.10	2.35	3.55	5.85	BSX29	47 32.00
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BC137	0.14	3.00	4.00	6.00	BSY27	25 17.50
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BC145	0.20	4.40	7.10	13.00	ME0404-1	15
BC153	0.10	2.10	3.70	6.20	ME0404-2	17
BC154	0.10	2.10	3.70	6.20	ME0411	17
BC182K	0.10	2.10	3.70	6.20	ME0412	18
BCY70	0.15	3.50	5.00	9.00	ME0413	14
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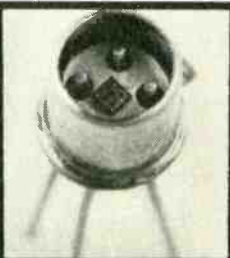
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**TENDERS**

**WARWICKSHIRE COUNTY COUNCIL AMBULANCE SERVICE**  
**Replacement of Mobile Radio Equipment**  
 Enquiries are invited from firms able to supply mobile and base station radio telephone equipment in connection with replacement of the existing equipment in the County Council's Ambulance Service during the financial year 1973/74. Details may be obtained by writing to the County Medical Officer of Health, Health Department, Shire Hall, Warwick.  
 E. CUST Clerk of the Council. [2240]



## SITUATIONS VACANT

**SENIOR ENGINEER** required by Continental Radio, T.V. and Audio manufacturers, experienced in general servicing problems. Location London, N.1. Attractive salary for the right man. Write Mr. A. Massing, Europhon (Radio & Television), 70 Caledonian Road, London, N.1. Tel: 01-837 3045. [2251]

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**FIRST** class Radio and Audio Engineer required for one of Britain's largest photographic and radio importers. Good conditions, excellent prospects, L/Vs. Apply Mr. Vassie, 253 8031. [2246]

**JAPANESE** Radio importers require experienced engineers for servicing transistor radios, etc. Part or Full Time. Tel.: 01-628 6157. [2258]

**MARINE** Radio Installation Engineer to fit and service SSB and VHF Radio Telephones, Radar and Automatic Pilots to yachts of all types anywhere in U.K. Must be based in or near London. Vehicle including personal use provided. The applicant must work on his own initiative and be capable of some mechanical engineering as well as woodwork. Knowledge of boating a great advantage. Telesonic Marine Ltd., 243 Euston Road, London, NW1 2BT. 01-387 7467. [2230]

**MANAGER/SENIOR** Salesman required for busy Television, Radio and all Electrical Appliance Showroom. Must be fully experienced in all leading appliances. Wages from £2,000 p.a. Banstead area. Tel. Victor Towler & Co. Ltd., 399 3476/7/8. [2259]

## SITUATIONS WANTED

**RADIO/ELECTRONICS** technician, 26 years, married, is open to offers of permanent or contract employment in UK or overseas. Living 30m south of London, but willing to travel anywhere. 7 years experience in vhf/uhf communications and industrial electronics, driving licence holder and radio amateur. Distinction C & G Electronics Servicing (Final). Reliable and practical man, capable of working on own initiative on the design, construction, commissioning and maintenance of radio and electronics equipment. Looking for an out of the ordinary situation, incorporating both bench and field work, where abilities will be recognised. prospects are good, and the remuneration £2,000 per annum plus. Box No. WW 2265. [2266]

## ARTICLES FOR SALE

**AARVAK ELECTRONICS**. 3-channel sound-light converters. £17. Strobes, £16. Rainbow Strobes, £132.—74 Bedford Avenue, Barnet, Herts. 01-449 1268. [119]

**A MATEUR** computer constructors' newsletter. S.A.E. M. Lord, 7 Dordells, Basildon, Essex. [2266]

**BUILD IT** in a **DEWBOX** quality plastic cabinet 2 in. x 2½ in. x any length. D.E.W. Ltd. (W.), Ringwood Rd., Fernwood, Dorset. S.A.E. for leaflet. Write now—Right now. [76]

**COMPONENT** Kits for magazine projects, constructor services, components. All at very low prices. Send S.A.E. for lists. Audio and Control Engineering, 30 Baker Street, London, W1M 2DS. [2255]

**FRONT** surface mirrors, 94% reflectance, optically flat, extremely durable. From £2.00 per square foot, ex-stock.—OCLI Optical Coatings Limited, Dunfermline, Fife. Inverkeithing 3631 (038 34 3631). [1955]

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## COLOUR, UHF and TV SERVICE SPARES.

Colour and UHF lists available on request. Varicap/Varactor UHF Tuners ELC1043 £4.50, VHF Varicap Tuners for Band 1 and Band 3 £2.85, Salvaged Varicap Tuners £1.50, incl. Connection Data, P/P 25p. Delay Lines DL20 £3.50, DL1 £1.95, P/P 25p. Lumiance Delay Line 50p. P/P 15p. Philips G6 Decoder Panel incl. DLIE, Crystal, etc., £6.50. P/P 30p. Also quantity Colour TV Camera panels and assid. manufacturers' surplus Colour receiver panels. Plessey Colour scan coils £5.75 P/P 35p. Convergence coils £3.80 P/P 25p, Blue lateral £1.25 P/P 10p (or complete set £10 P/P 50p). Mullard type colour Scan coils plus latest convergence coils for electronic control of static convergence £5.25 P/P 35p. Leading Brit. maker Colour LOPT assy. incl. EHT output and focus control £3.50 P/P 35p. Integrated transistd. decoder unit incl. circuits £1.25 P/P 10p. B9D valve bases for colour valves and PL500 series 10p P/P 5p. UHF tuners transistd. £2.85, incl. slow motion drive, indicator £3.95. Transistd. push button £6.25. Knobs 40p. UHF/VHF basic integrated tuner £3.95. Cyldon UHF valve tuners £1.50; all tuners P/P 25p. Transistd. UHF/VHF IF panels £4.75 (or salvaged £2.50) P/P 25p. MURPHY 600/700 series complete UHF conversion kits incl. tuner, drive assy., 625 IF amplifier, 7 valves, accessories housed in cabinet plinth assembly £7.50 P/P 50p. SOBELL/GEC 405/625 Dual standard switchable IF amplifier and output chassis incl. cct. £1.50 P/P 30p. THORN 850 Dual standard time base panel £1.00 P/P 30p. PHILIPS 625 IF amplifier panel incl. cct. £1.00 P/P 25p. VHF turret tuners AT7650 incl. valves for KB Featherlight, Philips 19TG170, GEC 2010 etc. £2.50. PYE miniature incremental for 110 to 830, Pam and Invicta £1.95. A.B. miniature with UHF injection suitable KB, Baird, Ferguson, 75p, Ekco, Ferranti, Plessey push button with UHF injection £1.00, all tuners P/P 25p. New fireball tuners Ferguson, HMV, Marconi £1.90 P/P 25p. Large selection LOPTs, Scan coils, FOPTs available for most popular makes. PYE/LABGEAR transistd. Masthead UHF Booster £5.25, Power unit £4.25 Labgear "Triset" 3 outlet UHF/VHF distributor amplifier, mains operated £6.50 P/P 25p. MANOR SUPPLIES, 172 WEST END LANE, LONDON, N.W.6 (No. 28, 59, 159 Buses or W. Hampstead Bakerloo and Brit. Rail). MAIL ORDER: 64 GOLDERS MANOR DRIVE, LONDON, N.W.11. Tel. 01-794 8751. [160]

**PRINTED** Circuit Board in 6 widths: 2 in., 2½ in., 3 in., 3½ in., 4 in. and 5 in. x any length; 1/16 in. single-sided fibreglass, 2p per 3 sq. in. Double-sided 1p per sq. in. P & P 5p per order. SAE quotations for other sizes and quantity discounts.—J. Knopp, 11 Connaught Gardens, Braintree, Essex, CM7 6LY. Tel. Braintree 25254. [115]

**STEREO SLIDER POTENTIOMETERS** / tracks matched two better than 2dB—Smooth action. Lengths 88mm, widths 20mm, travel 60 mm. P.C. Mountings. Log 100 K+100k, lin. 50k+50k, 53p. Stereo Balance 10K 55p. U.K. post free, overseas at costs. C.W.O. to Component Suppliers, 3 Kesters Close, Hardwick, Cambs. [2282]

**TELEQUIPMENT** Scopes. Perfect Condition. D51 Double Beam 6MHz Bandwidth Auto-sync £70. S52 3MHz Bandwidth plus X & Y facilities £60. S54 10MHz Bandwidth. Fully Transistorised £70. Carriage £2 extra. Only one each available. Phone: 01-886 3733/9666. [2250]

**TELEQUIPMENT** D53 Oscilloscope for sale, first class condition £150 o.n.o. Phone L. R. Denton 01-202 9824 after 6.30 p.m. [2267]

**TRANSISTORED** UHF Tuners £1.00 inc. P. & P. VHF with valves P.B. or rotary 75p inc. P. & P. C. P. Trading, 15 Cavour Road, Sheerness, Kent. [2175]

**TV** and **RADIO** aluminium mast 2in. x 35 feet high including supporting guys and T.V. and radio aerials. Buyer collects, offers. Henham (near Bishops Stortford) 483. [2130]

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**VHF KIT** 80-180 MHz receiver, tuner, converter. Transistorised, remarkable performance. £4 or s.a.e. for literature Johnsons (Radio), St. Martins Gate, Worcester. WR1 2DT. [113]

**VIDEO TAPE RECORDER**, National NV-1020E, 405/625 £165. National WV-350N Camera, Built in Monitor £150. Rediffusion 23% Video/Audio Monitor £60. Above as new. L. G. Fulcher, 11 Mount Pleasant, Framlingham (723590), Woodbridge, Suffolk. [2254]

**60** KHz MSF Rugby and 75 KHz Neuchatel Radio Receivers. Signal and Audio outputs. Small, compact units. Two available versions £35 and £60. Toolx, Bristol Road, Sherborne (3211), Dorset. [21]

## ARTICLES WANTED

**AVO 8** WANTED. Any condition. Any quantity. Send for packing INS. Huggett's Ltd., 2 Pawsons Road, W. Croydon, SY. [28]

**ENGINEER** requires modern transistorised single or dual trace oscilloscope. Details to P. W. E. Custard, 24 Etchingham Court, Etchingham Park Road, London, N3. Tel. 01-349 1752. [2262]

**REQUIRED** most urgently 30 pieces CV.2422. Ring 01-979 0123 [2249]

**WANTED** urgently Bleepers system preferably with aerial transmitter for minimum one mile radius operation, to handle up to 12 bleepers. Any make considered. Offers with full details to Ogdin, Otley, Yorkshire LS21 1HX. Tel. 094 34 4531. [112]

**WANTED**, all types of communications receivers and test equipment.—Details to R. T. & I. Electronics, Ltd., Ashville Old Hall, Ashville Rd., London, E.11. Ley. 4986. [63]

**WANTED**, televisions, tape recorders, radiograms, new valves, transistors, etc.—Stan Willetts, 37 High St., West Bromwich, Staffs. Tel. Wes. 0186. [73]

**WANTED**, EMI CCTV equipment, any condition. 11 Penn Close, Wells, Somerset. Tel. Wells 78901. [2269]

## BOOKS

**WORLD RADIO TV HANDBOOK** 1973, published December, £2.80, Post (first class) 10p. Order from David McGarva, Box 114F, Edinburgh EH1 1HP. [27]

## BUSINESSES FOR SALE

**OFFERS** for Limited Company known as Radiometrics Ltd.—Dormant—name of interest. Box No. WW 2263.

## BUSINESS OPPORTUNITIES

**R.S.M.C.** Radio Scan Marine Company. This is a firm based in Scotland interested in Sales/Service Agencies for Marine Radio, Radar and Echo Sounding Equipment of Foreign Manufacture aimed at the "Small Boat Market". Box No WW 2248.

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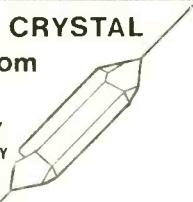
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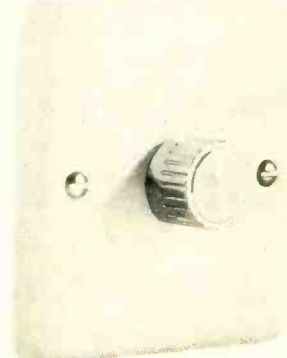
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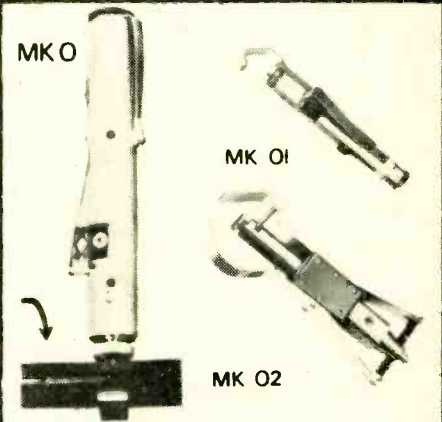
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