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# The RADIO Constructor



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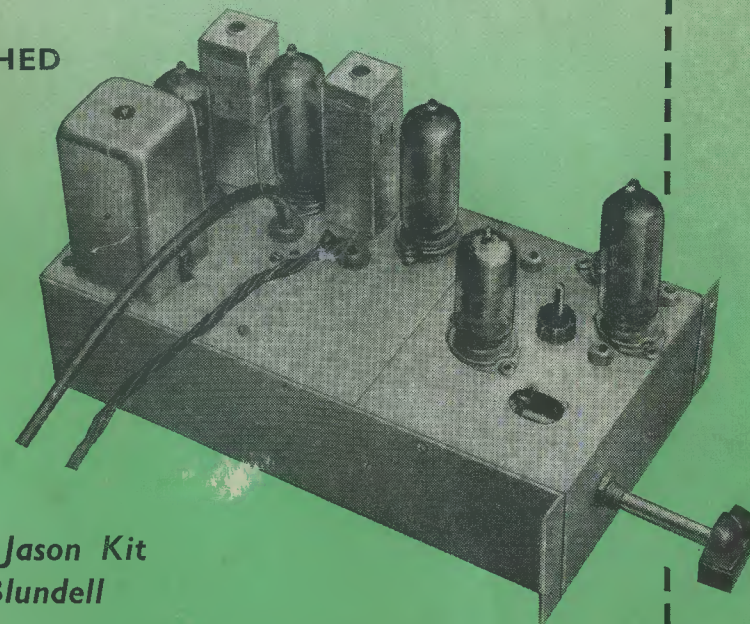
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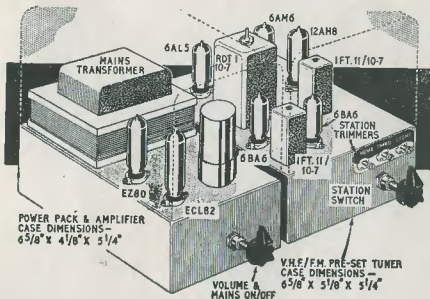
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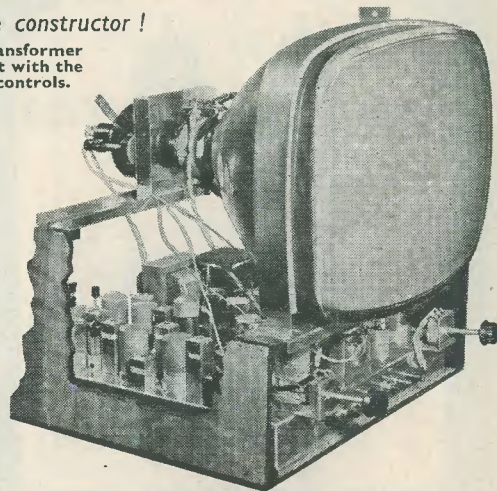
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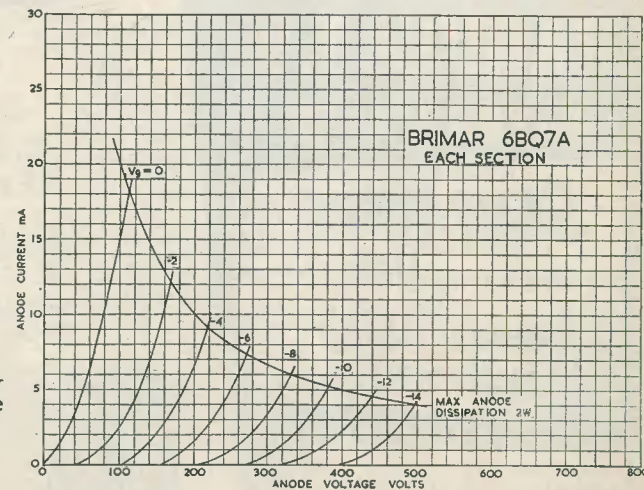
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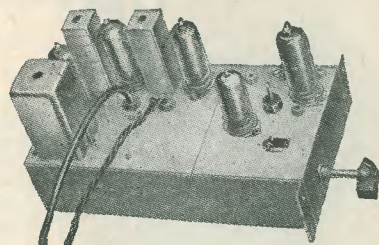
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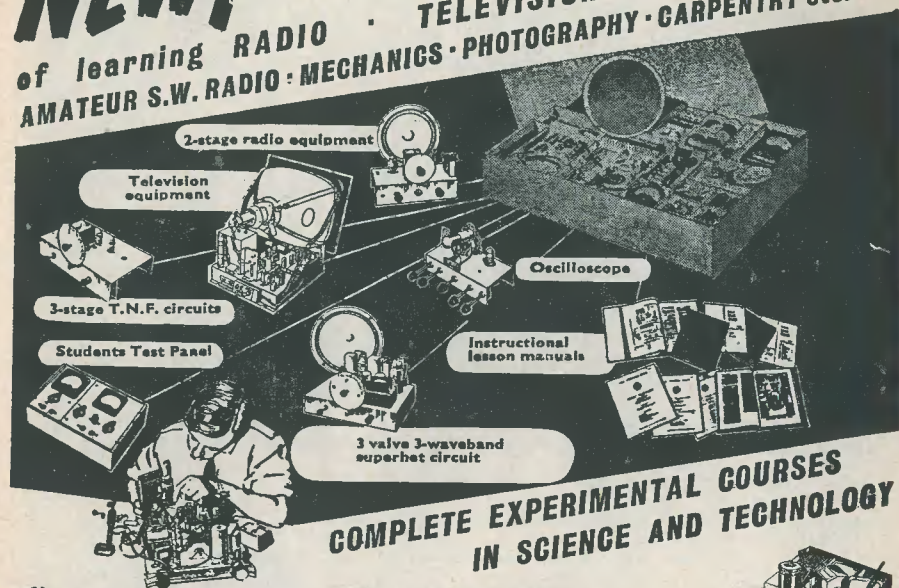
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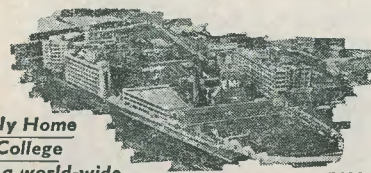
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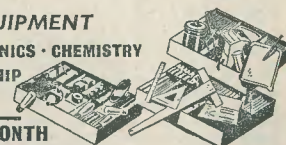
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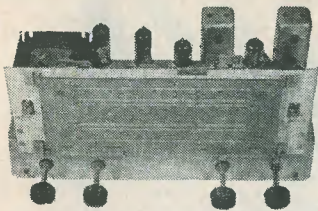
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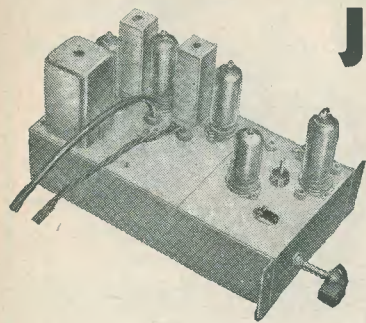
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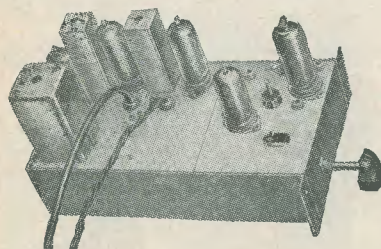
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OCTOBER 1957

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## NOTICES

THE EDITOR invites original contributions on construction of radio subjects. All material used will be paid for. Articles should preferably be typewritten, and photographs should be clear and sharp. Diagrams need not be large or perfectly drawn, as our draughtsmen will redraw in most cases, but all relevant information should be included.

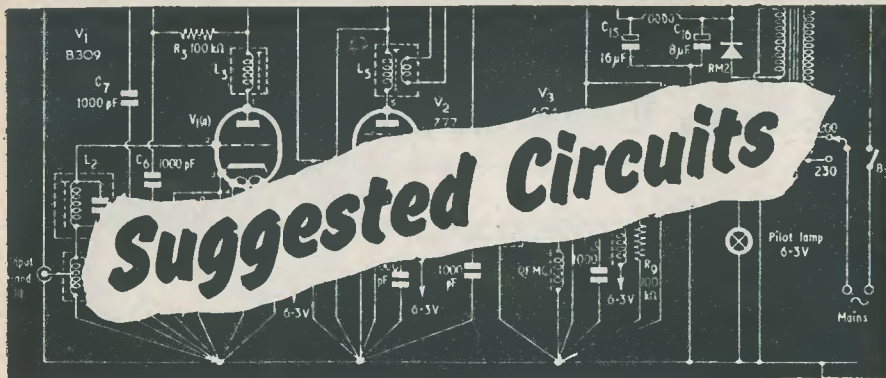
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QUERIES. We regret that we are unable to answer queries, other than those arising from articles appearing in this magazine; nor can we advise on modifications to the equipment described in these articles.

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The circuits presented in this series have been designed by G. A. FRENCH, specially for the enthusiast who needs only the circuit and essential relevant data

### No. 83. A SINGLE VALVE FM TUNER

IT FREQUENTLY HAPPENS, IN THE ALTERING scene which is inevitable in a rapidly advancing science such as that of electronics, that individual developments are liable to become relegated to the background even when they deserve especial attention on their own merits. The circuit which is described this month tends to fall within this class, insofar that it represents an f.m. tuner which caused some noticeable interest in the United States in 1947 to 1949, but which, so far as the writer is aware, has since occasioned very little comment. It is, of course, possible that the particular time when the circuit appeared may have some bearing on the fact that it is now so little-known. In this period, f.m. broadcasting in the States was becoming uneconomic under the conditions of commercial broadcasting which were then applicable. Public interest was swinging towards television, and the demand for high fidelity reproduction—which could have given a fillip to the f.m. medium—was limited. At the same time, f.m. broadcasting in Europe was practically non-existent, and the design received scant publicity outside the States.

Because of these facts, it seems that the one-valve f.m. tuner circuit which forms the basis of this month's contribution has been given

an undeserved lack of attention. To the writer's mind, the tuner employs such ingenious circuitry that it deserves recognition on this score alone, and the fact that it also provides an intriguing field of investigation for the more serious experimenter makes its inclusion in this series all the more desirable.

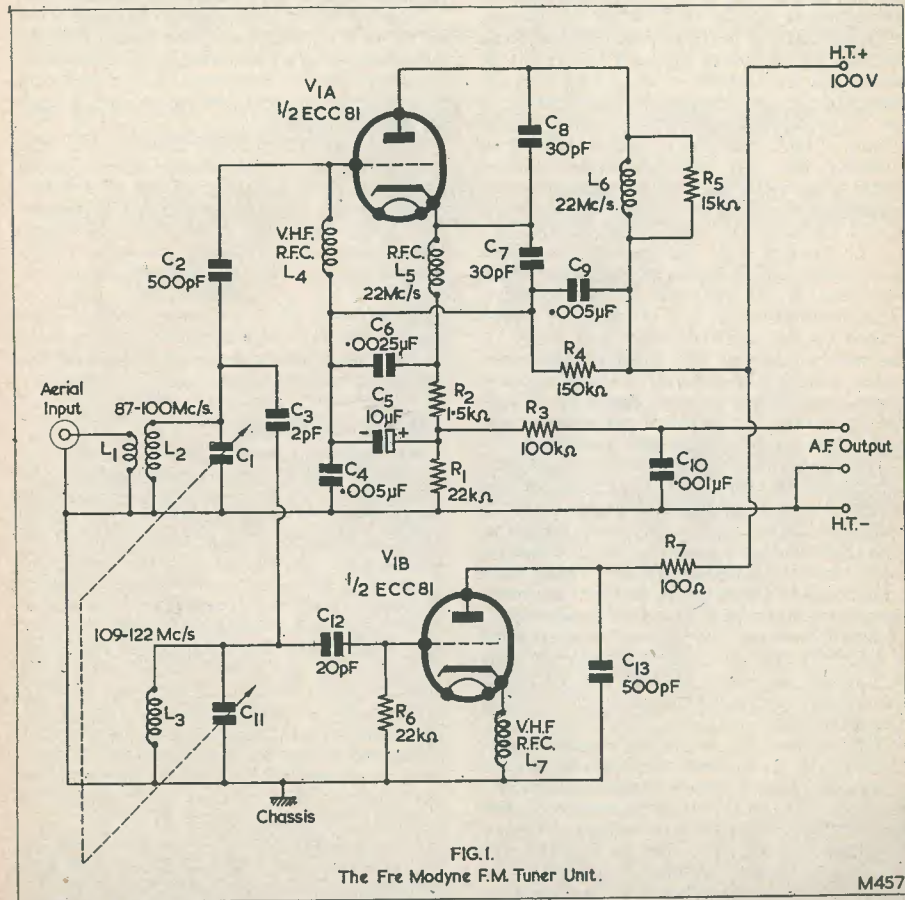
#### The Circuit

Before proceeding to a description of the circuit itself, some details of its source should be given. The circuit is due to B. D. Loughlin, and was produced by the Hazeltine Corporation as the FreModyne receiver. The circuit employs a single ECC81 (12AT7) and provides an audio frequency output at a level normally associated with superhet tuners. There are two references to the design which may be available to readers, and these are quoted at the end of this article.

The circuit accompanying this article is that of the Hazeltine FreModyne receiver in full; with the single exception that the original 300Ω input circuit has been changed to one more suitable for 75Ω operation. In the 300Ω version the coupling coil, L<sub>1</sub>, is not employed. One conductor of the 300Ω aerial feeder connects directly to chassis (at the bottom end of L<sub>2</sub>), whilst the other connects to the top end of L<sub>2</sub> via a 2pF capacitor.

The operation of the circuit is complex, insofar that a number of components perform several functions simultaneously. Unfortunately, the material available to the writer offers no detailed description of all of circuit operation, and he is unable to give quite as much design information as he normally likes to do. He feels also that he should stress, at this stage, that this particular circuit is intended for the advanced and experienced constructor rather than for the beginner. Since the circuit is that of a tuner which has been commercially produced, the major difficulty liable to be encountered is that of layout.

lator and runs at 22 Mc/s above the input signal frequency. If the oscillator circuit is analysed it will be found that it is basically a v.h.f. Colpitts, the only difference to the version normally encountered in such things as television tuners being that the anode of the valve is at chassis potential so far as r.f. is concerned, and not the cathode. Provided that it covered the frequencies required and developed sufficient oscillator amplitude, any other oscillator circuit could be employed in place of that shown. The oscillator voltage is fed to the grid of V<sub>1(a)</sub> via the 2pF condenser C<sub>3</sub>.



Apart from coils and chokes, which are discussed later, all the components are standard.

It is advisable to commence an examination of the circuit by first considering the oscillator, V<sub>1(b)</sub>. This triode, which is half of the ECC81, functions as a superhet local oscil-

lator. A signal voltage, built up across the tuned circuit, L<sub>2</sub>-C<sub>1</sub>, is applied to the grid of V<sub>1(a)</sub> in addition to the oscillator voltage. As will be seen shortly, V<sub>1(a)</sub> is switched on and off at a supersonic frequency, with the result that, for part of the time, the valve operates in a non-linear fashion and mixing between the



oscillator and signal frequencies takes place. The oscillator is off-set from the signal frequency by 22 Mc/s, with the result that an i.f. of this value appears at the anode of  $V_{1(a)}$ .

$V_{1(a)}$  also functions as a self-quenched super-regenerative detector running at 22 Mc/s, and with a quench frequency around 30 kc/s. In this mode of operation the valve employs  $L_6$  and  $C_7$ ,  $C_8$  to form an oscillatory tuned circuit, one end of which connects directly to the anode, whilst the other is applied to the grid via the choke  $L_4$ . This choke offers a high impedance to v.h.f. but has low impedance at 22 Mc/s. The grid of the triode is, so far as 22 Mc/s r.f. is concerned, at chassis potential, the cathode being isolated by means of choke  $L_5$ . It will be noted that the cathode of  $V_{1(a)}$  taps into the centre of the capacity tuning  $L_6$ . Insofar as the super-regenerative action proper of the circuit is concerned, it is rather difficult to visualise the CR network which causes quenching, due to the various capacities connected to the grid of  $V_{1(a)}$ . However, it would probably be valid to consider  $C_9$ - $R_4$  as the quench CR; the quench frequency being considerably increased by reason of the fact that  $R_4$  is returned to h.t. positive. (This connection to h.t. is probably necessitated by the positive cathode of  $V_{1(a)}$ . If  $R_4$  were returned to chassis the super-regenerator would not start.) Working as a super-regenerative detector tuned to 22 kc/s, the i.f. circuit is capable of achieving a very high degree of selectivity and sensitivity.

Discrimination of the 22 Mc/s frequency modulated i.f. signal is achieved by its conversion to a.m. on the side skirts of the i.f. response curve and subsequent detection. The response curve given by the FreModyne circuit has skirts which are very linear when considered in terms of db against frequency deviation, and which have a steepness of the order of 20 db per 100 kc/s. In consequence, a relatively high level of amplitude modulation may be obtained for the frequency deviations normally encountered in v.h.f. transmissions.

The a.f. output of the super-regenerative detector is taken from the cathode of the triode, it being built up across the detector load  $R_1$ . This a.f. is then filtered by  $R_3$  and  $C_{10}$ , and is finally passed on to the subsequent amplifier. A  $0.01\mu\text{F}$  condenser in series with the feed to the a.f. amplifier is desirable if the latter is likely to be affected by the small d.c. component present.

#### Further Details

There are one or two points concerning the circuit which require a little further discussion at this stage. First of all, it will have been noted that conversion to a.m. is achieved by

applying the f.m. signal to the side skirts of an i.f. response curve, and this infers that two tuning positions would be given for each station received. However, in reference 2 it is stated that the double tuning effect is hardly apparent, and that it is possible to miss it without prior knowledge. So far as non-linearity in the conversion of f.m. to a.m. is concerned, it has to be pointed out that a response curve which is linear when considered from the point of view of db versus frequency is not quite the same thing as one which is linear for voltage against frequency. Nevertheless, the fidelity given by the device appears to be of an acceptable nature.

Another factor which has to be considered is that of a.m. rejection. It is stated that the circuit provides a useful degree of rejection to impulsive interference insofar that, employing a super-regenerative detector, it is only "on" for part of the time.

A final point is concerned with sensitivity; and a minimum sensitivity figure would appear to be of the order of  $200\mu\text{V}$  across a  $300\Omega$  input. The limiting factor to sensitivity is the necessity of obtaining an audio signal which satisfactorily overrides background noise. The  $200\mu\text{V}$  input figure corresponds to a signal-to-noise ratio of approximately 30 db. An input level of  $70\mu\text{V}$  (across  $300\Omega$ ) gives a signal-to-noise ratio of 20db, a figure which would be just acceptable for entertainment value.

#### Experimental Details

As was mentioned at the beginning, the Hazeltine FreModyne circuit offers considerable scope for the more experienced constructor. At first sight the coils would appear to present some difficulties, but closer examination shows that this may not be so. Examining the aerial input circuit, it will be noted that all that is required of  $L_1$  and  $L_2$  is that they allow a signal voltage of good amplitude to be built up across the tuned circuit. The input coils could, therefore, very probably consist of reasonably high-grade types already available in the home-constructor market. As was stated above, it is not necessary for the oscillator  $V_{1(b)}$  to take up the exact form shown in the diagram, and alternative oscillators may enable the choke  $L_7$  to be dispensed with.

$L_6$ , the super-regenerator coil, is also not as "awkward" as might be thought at first, this being due to the fact that it is damped in the FreModyne circuit by the fairly low value resistance (for 22 Mc/s) of  $15k\Omega$ . This point infers that the constructor could employ any reasonably high-Q coil at this position, altering the value of  $R_5$ , if necessary, to sharpen up or flatten off the 22 Mc/s response curve.

The two chokes  $L_4$  and  $L_5$  may require a

little experiment. The purpose of  $L_5$  is that of offering a high impedance at 22 Mc/s, and a conventional commercial component should cope here.  $L_4$  is intended to offer a high impedance to v.h.f. and a low impedance to 22 Mc/s, and may require some development work before it is finally satisfactory.

It would probably be advisable, when initially putting the circuit into working order, to concentrate primarily on the 22 Mc/s super-regenerator section. To get this part of the circuit functioning correctly, the local oscillator,  $V_{1(b)}$ , may be ignored, the  $2p\text{F}$  condenser  $C_3$  being left temporarily out of circuit. In addition,  $L_2$  could be tem-

porarily replaced by a resistor of some  $75\Omega$ , and the output of an amplitude modulated signal generator set to 22 Mc/s connected across it. When the super-regenerative circuit was satisfactorily tuned to 22 Mc/s and gave a sufficiently sharp response, the v.h.f. section could then be brought into operation.

#### References

1. *Radio Engineering Handbook*, fourth edition, p. 868. McGraw-Hill.
2. *Radio News*, Feb. 1948. Ziff Davis Publishing Co.

## TUBELESS TYRES

## TUBELESS RADIO

*Our acting-unpaid but otherwise temporarily harmless private eye, who is at large on parole, reports.*

Being unable to find a current-production car radio suitable for the apurtenances of the super-luxury "Eldorado Brougham," body-stylists in the Cadillac Division of General Motors, Detroit, commissioned their colleagues in the Delco Radio Division to devise a quality radio that would be in keeping with the affluent features of this lush automobile. It must, they specified, be something unusual; it must be the goods; nothing but the fantastic is good enough for this dream-car, which only the disgustingly rich shall be able to afford, for it is to be a limited-production jalopy.

The back-room boys went into hibernation, got down to it and evolved a design. True to type, they lacked nothing in imagination or lavishness. They discarded entirely the old-fashioned electron tube, and liberally sprinkled their drawing-boards with semi-conductors. Triumphant they emerged with a *magnum opus* incorporating no fewer than 13 transistors and 4 crystal diodes. This, they declared, is tubeless radio the like of which you have never, but never, seen before.

A discerning scrutineer can detect, by the simple process of ignoring certain embellishments, a superhet circuit embodying an r.f. amplifier, separate oscillator and mixer stages, three i.f. stages at (strangely) 262 kc/s, infinite impedance detector, delayed and amplified a.v.c., an audio driver stage, and push-pull output. Negative feedback is applied to the audio driver stage, but the push-pull stage seems to be left to its own devices, except for a thermistor-controlled circuit which ensures optimum bias for the two power transistors therein. Frequency response of the receiver is said to extend to 18 kc/s, but oddly the two speakers into which it works cut

off at 60 c/s and 9 kc/s, which looks rather peculiar to those who know their hi-fi.

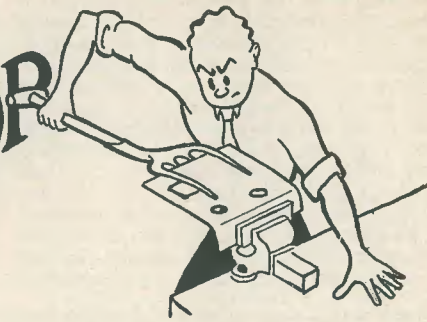
As the helmsman of the car must be given something to do radio-wise, the receiver has push-button station selection. It is here we discover the equivalent of automatic gear-shift applied to a.m. radio, for the desired button having been pushed, electronics take over; two transistors and a crystal diode then twiddle non-existent knobs by operating in a trigger amplifier and relay control circuit designated by the bright boys, "automatic search tuning." It is known to us, no doubt, simply as a.f.c.

Sensitivity, they claim, is better than  $3\mu\text{V}$ , and with only  $1\mu\text{V}$  of aerial signal input you can have 1 watt of audio output. If you can muster energy enough to turn the volume control round to maximum, and assuming your ears will not cave in, you can revel in 10 watts of audio. The car then becomes a small concert hall capable of being trundled round the countryside at speeds in excess of the murder margin.

The receiver has no insatiable appetite for electrical power, for it needs only the 12V car battery to operate it, and demands about 600mA total current therefrom. Of this more than half is consumed by the two pilot lamps.

We have reported on this receiver rather facetiously, but it is really no leg-pull. You can read all about it on pages 60 and 61 in the August issue of the American magazine, *Radio and TV News*. However, we did not notice any particular mention of how 10 watts of audio is derived from a d.c. input to the receiver of about 3 watts. One wonders how it is done. (Ask a silly question like that, and you might get a stupid answer.—ED.)

# IN YOUR WORKSHOP



Aided by his able assistant, Dick, Smythy the Serviceman continues to run the Workshop

"I THINK," REMARKED DICK, AS HE TOOK A receiver off the rack and placed it on the bench in front of him, ready for repair, "that I'll have to give up any ideas I had of becoming a serviceman, and become a compositor instead!"

"What's up?" grunted Smythy, looking up. The morning was half gone, and he and Dick had been working steadily through the sets which filled the "For Repair" shelf.

"It's these printed circuit sets that are coming into the shop these days," replied Dick. "I've had two this morning already. If I ever made a cold joint in one I'd feel like writing 'stet' on it!"

"Well, that's corny enough," commented Smythy. "Anyway, I'm glad you're getting some practice on printed circuits. They are getting more and more common these days."

## Printed Circuits

Dick looked a little glum.

"The future of servicing doesn't seem to be very bright, then," he remarked. "The more printed circuits sets that are made the fewer snags that will occur, and the less work there will consequently be for you and me."

"What on earth makes you think that?" asked Smythy, surprised.

"Well, printed wiring is supposed to be much more reliable than ordinary wiring," said Dick, "and to my mind that means less servicing work."

"Don't you believe it," Smythy replied. "Printed circuits won't cause us any drop in work; in fact they may very probably bring more in. Funnily enough, you're the second person who's made a comment of that nature to me in the last few days. I don't know why it is, but there seems to be a generally

exaggerated feeling that printed circuits are going to completely revolutionise the industry in the next few years. Perhaps my imagination is getting a little blunted in my old age, but I just can't see the point of such an argument. You may remember that it wasn't so long ago when I made some comments on printed circuits, as considered from the manufacturer's point of view.\* At that time I discussed the considerable difficulties facing manufacturers who wanted to change over to printed production. The first thing I pointed out was that the labour cost involved in wiring up, say, a television set represented only a very small proportion of its total cost, a far greater proportion going into the cabinet, tube, valves and components. Thus, if a manufacturer changed over to printed circuits and had operators inserting components individually by hand, the saving in cost would hardly be worth the trouble. In order to get the best out of printed circuits, components would have to be inserted by machinery, and that would involve a very heavy outlay of capital. I didn't mention it at the time, but the thought has since occurred to me that, owing to the speed with which new ideas in commercial electronic production become obsolete, it should not be at all outside the bounds of possibility for a particular automatic insertion machine to fall out of date after only a few years use. The depreciation per year in value of such a machine would then become shockingly high. All these points are liable to deter the set-maker from embarking on printed circuits 100%; and they cause their introduction to the British market to be somewhat slower than you might, at first sight, expect it to be.

\*In Your Workshop, May 1957

"However, once the initial slow introductory period has been overcome, I should imagine that the use of printed circuits will increase with much greater rapidity. We are probably nearing the end of the initial period at the present moment, and I wouldn't be at all surprised to see the second phase come fully into being in 1958. So, although set manufacturers are probably not making much money at present by the introduction of printed circuits, they are still pressing on with them, albeit rather slowly, in the hopes of better things to come.

"Anyway, let's forget the manufacturer for the moment and get down to the service engineer's viewpoint. Now, you have just raised the question that the introduction of printed circuitry may reduce the amount of work coming into the service shop, whilst I said that it would probably bring more in. I think it would be valuable at this point if we were to consider first of all just exactly what a present-day printed circuit *does*. An average contemporary printed circuit consists, quite simply, of an insulating board with a copper foil pattern which replaces the wiring of a conventional chassis. Because of this, the printed circuit board merely obviates conventional wiring, whereupon the only fault condition which has been deleted is that of incorrect connections. It occasionally happens that a conventionally-wired receiver leaves its factory with a component connected to a wrong tag, and yet still manages to give a fairly average performance. Printed circuit boards would prevent wiring mistakes of that type. However, manufacturing faults in this class are very few and far between, and their absence would make very little difference to the total amount of work handled by the serviceman."

"Well, that seems to be a reasonable argument," commented Dick. "What about cold joints and things like that?"

"I can't see printed circuits drastically reducing the number of cold joints in a set," replied Smythy. "And, here again, you have to face the fact that the number of cold joints in a conventionally wired chassis is not, in any event, very high these days. Don't forget that printed circuit components have to be soldered to the copper foil, and I would have thought that the risk of cold joints here is just as high as when the components are soldered to tags. Indeed, the risk may even be higher, as it is not quite as easy to solder to a flat piece of copper as it is to a tag around which the wire has been twisted. Of course, much printed circuit soldering will be done automatically, but this fact is not, to my mind, likely to reduce the number of cold joints encountered.

"So far as the overall reliability of a printed circuit set is concerned, you must also

remember that it employs just the same components and valves as are used in conventionally wired chassis. It is these which cause the majority of failures; whereupon it becomes irrelevant whether any particular component is stuck to a printed board or hung between two tags."

"You said just now," reminded Dick, "that printed circuits might actually increase the work we have to do. How do you justify that?"

"Well, I may have been gazing into the crystal ball rather deeply there," admitted Smythy, "although, on the face of it, events would seem to point that way. First of all, the inevitable result of printed circuits will be an increase in production, although this may not become evident for a number of years. Increased production, when it comes, means more sets in people's homes, more sets to go wrong, and more sets to be passed on to the serviceman. Secondly, printed circuits may introduce one or two snags on their own account, such as leakiness between conductors through the board, and so on—again more jobs for us! Time alone will tell what faults may arise from the use of printed circuits, but I would be very surprised if they introduced none at all. I suppose that I am being rather pessimistic in making such a statement, but then I never have looked only on the bright side of things!"

## Practical Servicing

"I'll keep my fingers crossed for the future, then," Dick said. "In the meantime, have you any hints on printed circuit servicing you could pass on?"

"Well, printed circuit servicing is all very straightforward," replied Smythy, "so long as you pay attention to several common-sense rules. The main thing to avoid is the use of brute force methods on the printed board itself. This applies particularly to soldering operations. Although the copper foil adheres very strongly to the insulated board it *can* come unstuck, and especially so if you apply too much heat. So any soldering operations which are needed have to be carried out quickly and carefully. Sometimes the copper foil is covered with a varnish, and as this may have fluxing properties it does not always need to be scraped away if you intend to make a joint. You can always check the properties of any varnish you may find by making an experimental dab with the iron in the centre of a large earthing section—most boards have large areas of copper at earth potential—to see how quickly tinning occurs. This quick check may save damage to a more intricate part of the circuit elsewhere. Remember, by the way, that the service manual *should* give you information concerning the best method of soldering to the board, and this should be consulted always.

"Whenever you make a joint to a board, it is best to use a miniature iron which is well tinned. In most instances the only time you should ever have to apply an iron to the board is when you suspect a cold joint between a component lead-out wire and the copper foil.

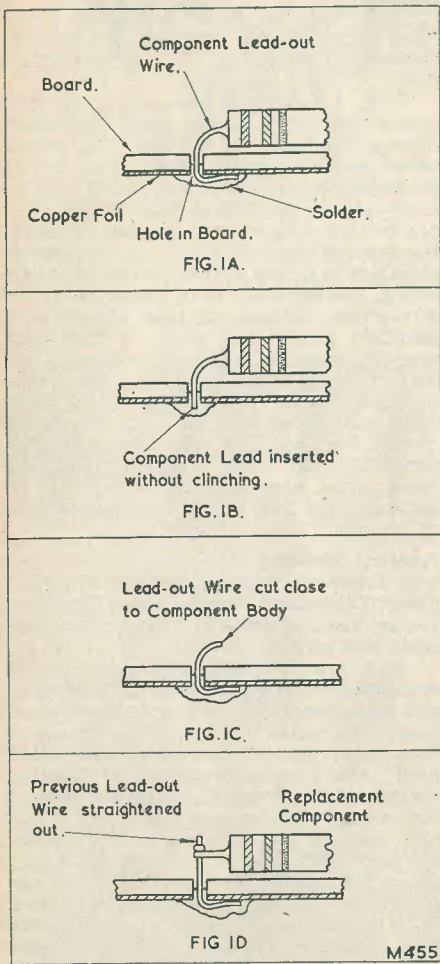


Fig. 1 (a). Cross-sectional view showing a lead-out wire from a resistor clinched to a printed circuit board before soldering  
 (b) A component lead-out wire inserted without clinching  
 (c) For replacement purposes, the lead-out wire of the faulty component should be cut, as illustrated here  
 (d) A replacement component secured to the previous lead-out wire

Nine times out of ten, the mere application of the iron, without any solder or flux, will be enough to make the joint serviceable. A very good idea consists of melting a little cored solder on to the tip of the iron and of shaking this off again just before applying it to the foil. This idea will ensure that the iron tinning has a minimum of oxide, and that a quick thermal connection can be made to the solder in the suspect joint. Cold joints on printed circuit boards are fairly easy to find, by the way, as they frequently have an 'obvious' look about them. Usually, you will find that the solder collects in a blob around the component wire, instead of spreading nicely over the surface of the copper foil; or that, although the solder has spread over the copper, the component lead has the unmistakable appearance of not having 'taken.' Light, repeat light, taps on the components will usually make a cold joint show up as an intermittent. It is inadvisable to check for a cold joint by moving a component bodily back and forth over any great distance unless it happens to have thin lead-out wires. Rough movement of the component can cause the copper foil on the other side of the board to be strained, whereupon it may become torn away from the board. The lead-out wires on almost all resistors and many condensers fall within the 'thick' category; and these components are those which should not be moved around too violently."

"How do you replace faulty components on a printed board?" asked Dick.  
 "The best way," replied Smithy, "is, whenever possible, to cut the existing lead-out wires and solder the new component to these. There is a good reason for this particular policy. In most printed boards, component leads are clinched over in manufacture before soldering. Like this (Fig. 1 (a)), where you can see a cross-sectional view of a lead-out wire from a resistor soldered to the copper foil. Now, if you try to replace the component by simply unsoldering it from the board, you would find that you would have to keep the iron on the joint for quite a long time before you could straighten out the wire and pull it through its hole. This may cause overheating of the board. Sometimes, the lead-out wires aren't clinched over, being merely inserted straight into the holes in the board (Fig. 1 (b)). Even here it is preferable to avoid trying to unsolder the wires at the board; although the risk of overheating is much less in this case, since the wires can be pulled through their holes more quickly. Don't forget that, after unsoldering at the foil, the appropriate holes in the board will be full of solder, and this can be a nuisance at times. As I said just now, therefore, in order to overcome these snags the best plan consists

of clipping the lead-out wires of the faulty component as close to its body as you can (Fig. 1 (c)), and then soldering the new component to those leads (Fig. 1 (d)). Even here

repair of this nature can be made to look quite neat, incidentally, and it gives just as good results as did the previous connections to the copper foil itself."

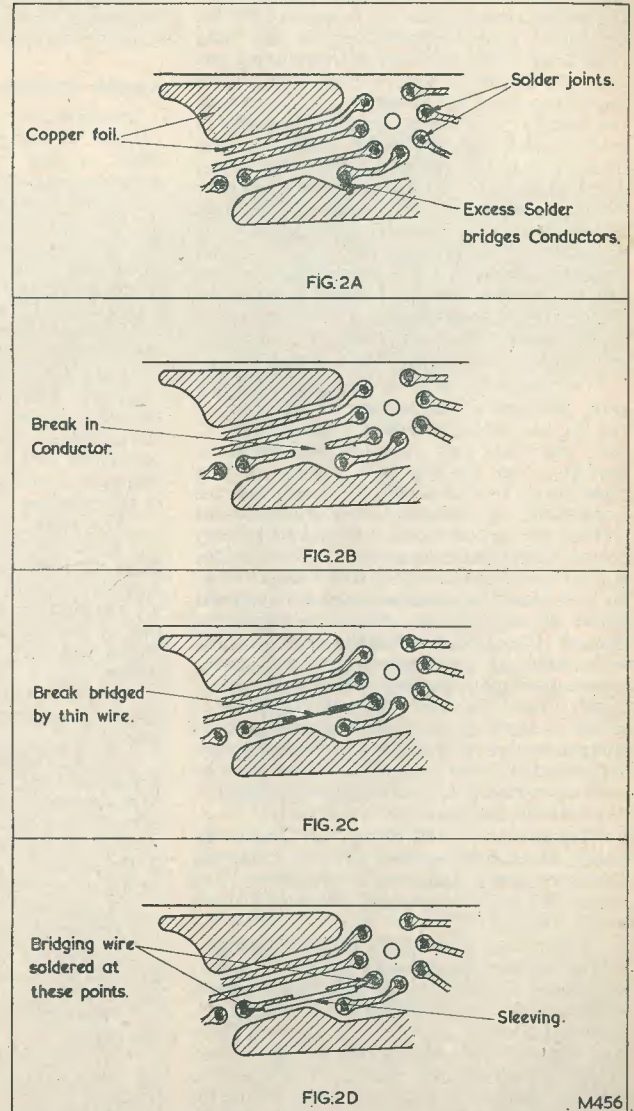


Fig. 2 (a) Whilst servicing printed circuits, excess solder may accidentally bridge adjacent conductors  
 (b) A break in a printed circuit conductor  
 (c) The break of (b) bridged by a thin wire  
 (d) An alternative, and somewhat safer, method of bridging the conductor break

you need to be fairly quick in order to prevent the heat travelling down the cut leads and loosening the joints at the copper foil. A

"It sounds to me," commented Dick, "that the thing to avoid in printed circuit servicing is the printed panel itself!"

"That's true enough," Smithy replied, "and you soon find yourself evolving new techniques for preventing damage. Sometimes, soldering directly to the copper foil becomes inevitable, of course, and there are some errors which you then have to take particular care to avoid. The worst one is that wherein the solder runs outside the boundary of one conductor and bridges over to the next (Fig. 2 (a)). The only way of overcoming this state of affairs, if you're ever unfortunate enough to have it happen to you, is to turn the board upside down—so that the solder is underneath—and, with the soldering iron applied, tap the board so that the excess solder falls off. You should never try to break the solder joining the two conductors by scratching at it with a pen-knife or a screwdriver. If you do this you may pull away the copper foil as well as the solder, and you are almost certain to break the skin of the insulating board as well. The latter could then become water absorbent at that point, and might later become leaky.

"Occasionally, due to careless handling plus, perhaps, a thin section of foil, part of the circuit becomes broken (Fig. 2 (b)). If this happens, you may be successful in bridging over the gap with a piece of thin wire (Fig. 2 (c)). Both the wire and the copper should be tinned before you make the joints. If the conductor happens to be very narrow at the point where the break occurs, or if the conductors on either side are very close to it, it would be more advisable to make the joints at any points where the conductor widens (Fig. 2 (d)). Usually such widening will occur at connections to components, whereupon you already have the copper nicely tinned for you. A further solution is given by the fact that, since the conductor is almost bound to connect to components on either side of the break, you might then be able to connect your bridging wire between their lead-out wires *above* the board."

"Up to now," said Dick, "all your comments have been concerned with soldering and component replacement problems. Are these the major troubles to expect with printed circuits?"

"They are, mainly," replied Smithy. "Most of the other snags you are likely to encounter are those of fault location, which apply equally to conventionally wired chassis. Before I finish I should point out that there are one or two precautions to take when working with printed boards. For instance, you shouldn't take a soldering iron whose bit is heavily laden with solder near the board, as you then run the risk of dropping blobs of solder on to the copper, and they may be quite difficult to get off again. Other undesirable things, such as paste flux—which you shouldn't use on printed boards in any case

—between conductors may also cause a lot of trouble.

"A final point to remember about printed circuit boards is that they are liable to warp somewhat with age and heat. So, if a particular receiver employs a large board, you should keep an eye open just in case severe warping in service has caused any connection to become strained."

#### Another Problem

Smithy finished speaking and left Dick to ponder over the points he had just discussed. After a few moments, the Serviceman addressed his assistant once more.

"Well," he remarked, "I think we've had enough nattering for one day. Even so, though, I cannot help but be tempted to waste just a little more time before returning to the grindstone. So I'm going to set you a little problem."

"Oh no," protested Dick. "Not another 'hocus-pocus'\* effort, please!"

"I'm sorry," continued Smithy mercilessly, "but my mind's made up. Our last problem proved to be very popular, and so I think we should have a repeat performance. This time the whole thing is extremely simple indeed, and you should be able to give me an answer in two minutes. Are you ready?"

"Fire away," said Dick, resignedly.

"Well, the problem concerns a friend of mine who was walking past a Government surplus radio shop one morning, when he saw a large sign in the window which said: 'Buy one of our bargain condenser parcels.' My friend was very intrigued by this and went inside.

"'Could you tell me what condensers there are in your bargain parcels?' he asked the salesman.

"'Well,' replied the salesman, 'each parcel is the same and each has four condensers in it. What is more, the values of all condensers are expressed in whole numbers of microfarads. That is to say, any condenser could be 1 $\mu$ F, 2 $\mu$ F, 3 $\mu$ F or any other number up, there being no fractions or decimals.'

"I see," replied my friend; 'could you give me any more information?'

"'Certainly, sir,' said the salesman. 'The product of the condenser values in each parcel comes to 36.'

"'That still doesn't help me,' commented my friend.

"'Well,' continued the salesman, 'the sum of their values is equal to the date next Tuesday.'

"My friend looked at the number indicated on the calendar by the assistant.

"'I'm sorry, but I'm *still* not satisfied,' he said.

\* In Your Workshop, May, June 1957

"'All I can add, sir,' replied the salesman, 'is that the condenser in each parcel with the largest value is 500V wkg.'

"'Ah, that's what I wanted to know,' said my friend, whereupon he bought a parcel of condensers and walked out of the shop."

"I should jolly well think he *would* walk out of the shop after meeting a salesman like

that," said Dick feelingly. "Anyway, go on with the problem."

"That's it!" grinned Smithy. "Now you tell me the condenser values in each bargain parcel. I'll tell you the answer at our next little session if you haven't already worked it out."



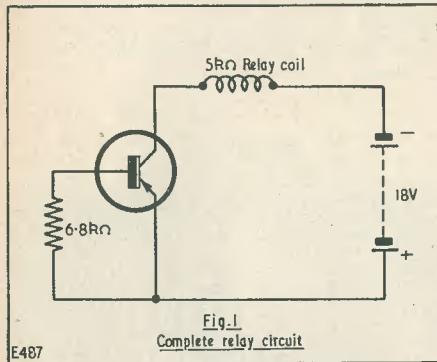
#### A Photo-Sensitive Transistor

IT HAS BEEN KNOWN FOR SOME CONSIDERABLE time that germanium possesses photo-sensitive properties, but not until very recently has any real use been found in its application. The term "photo-electric" is a familiar one and is used in describing a phenomena in which the movement pattern of electrons in a material is changed quite appreciably by the application of light to the material. Usually the amount of energy which the photo device can control is quite small, so that it has to be followed by a valve amplifier or perhaps a gas-filled trigger valve; in either case the purpose is normally to open or close a relay depending upon the intensity of the light falling on the photocell. A new type of photocell has now been introduced and is known as a "phototransistor." It does, in effect, combine the properties of the photocell with those of a transistor amplifier so that a remarkably high order of sensitivity can be achieved. In fact, the sensitivity is such that it can be made to operate a conventional type of relay without any additional form of amplification. Like most types of semiconductor diodes and transistors on the market today, the phototransistor employs a germanium element which has been found to possess excellent photo-sensitive properties. This has in the past led to some rather queer results being obtained by experimenters using transistors, and it is worth digressing for a moment to describe an effect which may have already puzzled some constructors.

In a laboratory, engineers were working to test a new fully transistorised amplifier which differed from the normal run of amplifiers in that it had been developed with special care to give high fidelity reproduction. Now the results obtained were very good, but the performance was marred by a strong 100 c/s hum. It was naturally assumed that the hum was being picked up from adjacent mains wiring; but careful screening, and indeed even shorting the input terminals, did little to help. This was very disappointing, as it had been assumed that one of the advantages of employing transistors was that complete freedom could be obtained from mains hum, a defect which so often haunts the hi-fi constructor. Then one of the engineers switched off the fluorescent lighting in the laboratory and immediately the hum ceased, as it had, in fact, been caused by the photo-sensitivity of one of the transistors in the equipment. All forms of lamp, whether of the filament or discharge type, will flicker at mains frequency, and although persistence of vision renders this invisible to the eye, it does exist.

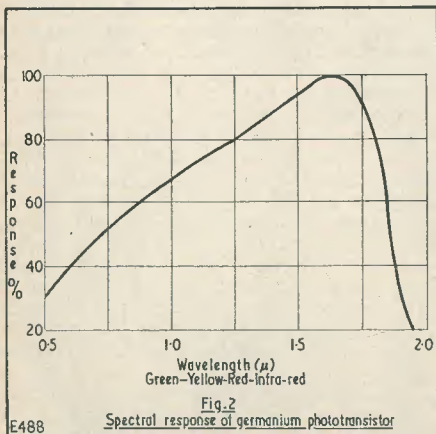
The applications of the phototransistor are very similar to those of any other form of photocell, namely automatic door opening, burglar alarms, counting and batching, machine protection, etc. For all these devices the mode of operation is basically the same—a beam of light is caused to fall on the cell, and when interrupted a relay in the cell circuit is energised. Other applications are

found in sound film reproduction, but it is in the classes already mentioned that the phototransistor excels because of its much greater sensitivity. The first example of this type of



cell to appear in England is that made by the Mullard Company under the type number OCP71. Its physical size is extremely small by comparison with the more conventional type of cell, being only  $15 \times 5.9$ mm. This, coupled with a very simple circuit, enables a high degree of miniaturisation to be achieved.

A typical circuit which is suitable for most of the on/off applications which have been



listed above is shown in Fig. 1. It will be seen that the emitter-collector circuit of the transistor is joined in series with a relay coil and battery. The current which flows in this

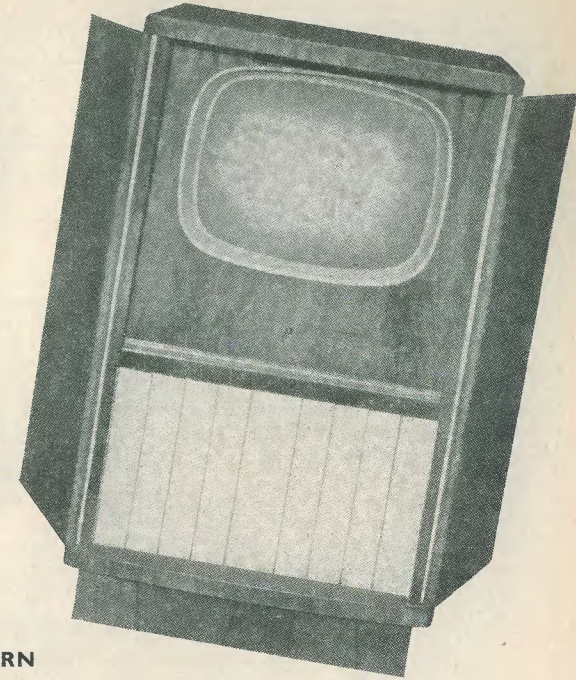
circuit will be dependent upon the light falling on the cell and the ambient temperature in its vicinity. The inclusion of this latter factor may come as a surprise until it is remembered that all germanium devices are temperature sensitive. In the phototransistor the effect of increasing the working temperature is to increase the dark current; this has the effect of reducing the ratio of light to dark current with increasing temperature. The effect can be minimised by connecting a resistor between base and emitter as shown in the diagram, a value of  $6.8k\Omega$  being a good compromise; too low a value will reduce the sensitivity to changes in light level.

One of the advantages of the phototransistor is that its high sensitivity enables a normal type of relay to be employed. A typical 25mW 5,000 ohm relay will be quite suitable for the job, as it will have a pull-in current of some  $1\frac{1}{2}$  to 2mA, whereas the photocell will provide some 4mA under light saturation conditions. If the use of a relay having a coil resistance other than that recommended is contemplated, care should be taken not to exceed the maximum collector dissipation of the phototransistor. To over-heat the germanium pellet can permanently ruin the characteristics of the cell. The maximum dissipation on the collector will occur when the cell is in the half-switched-on condition, that is when the current is midway between the minimum and maximum values. The collector dissipation under this condition is calculated by taking the product of half the total current and half the supply voltage, and this should not exceed 25mW.

Some knowledge of the dark current may be useful, particularly in those applications where a beam of light is used only occasionally to switch on the cell for a short period of time, as under such conditions a low capacity battery may be employed to give an almost indefinite life. At  $25^\circ\text{C}$ . the dark current can be expected to be in the region of  $50\mu\text{A}$ .

The spectral response curve of the phototransistor is shown in Fig. 2, from which it will be seen it is most sensitive to light at the red end of the range. Knowledge of the response curve is useful in those applications where light of a given colour is used to operate the cell to reduce the interference from ambient illumination. Normally, all that is necessary in the way of a light source for normal switching applications is a small torch bulb fitted with a reflector and convex lens focusing a beam of light on to the cell. A good idea of the sensitivity of the system is obtained from the fact that if a 2.5V bulb is under-run at 1.5V, the light from the dimly glowing filament when focused on to the cell will operate it at a distance of several centimetres.

# The MAYFAIR Turret Tuned Band 1-Band 3 Home Constructor TELEVISOR



PART 2

by S. WELBURN

*Our popular contributor on television topics devotes the second article in this present series to the vision i.f. strip of the Mayfair television receiver*

IN LAST MONTH'S ISSUE THE WRITER introduced the Mayfair home-constructor television receiver, and discussed the circuit and functioning of its power pack section. He also gave step-by-step instructions for the construction of this particular unit, these instructions describing in detail the procedure needed for its complete assembly. In this month's article the vision i.f. strip is dealt with and, once again, comprehensive building instructions are given.

## The Vision I.F. Strip

The circuit of the vision i.f. strip and video output stage is given in Fig. 4. As may be seen from this diagram, the circuit design is fairly conventional in character, well-tried basic principles being employed. The intermediate frequencies handled by the strip are 16 Mc/s vision, and 19.5 Mc/s sound. The coils specified are available pre-aligned, incidentally, thus obviating the necessity for adjustments after construction.

Not shown in Fig. 4 is the turret tuner, this being treated in these articles as a separate unit. The turret tuner immediately precedes the vision i.f. strip, its output at i.f. being fed directly to pin 6 of the Input Coil. Pin 1 of the Input Coil connects to the grid of the first i.f. amplifier valve  $V_2$ ; whereupon the coil functions as the inductive element of a pi filter, its tuning capacities on either side being given by the  $C_{gk}$  of the first i.f. amplifier and the capacity to chassis of the lead from the turret tuner. An EF80 is employed as first i.f. amplifier in order to take advantage of the high input resistance which this valve offers.

The anode of the EF80 connects into the first I.F. Coil, thus providing a partial band-pass response by the use of a coupling winding in series with the primary. This coupling winding is fitted close to the secondary, and the overall arrangement has the advantage of providing a more closely controlled coupling factor for different core settings than is given

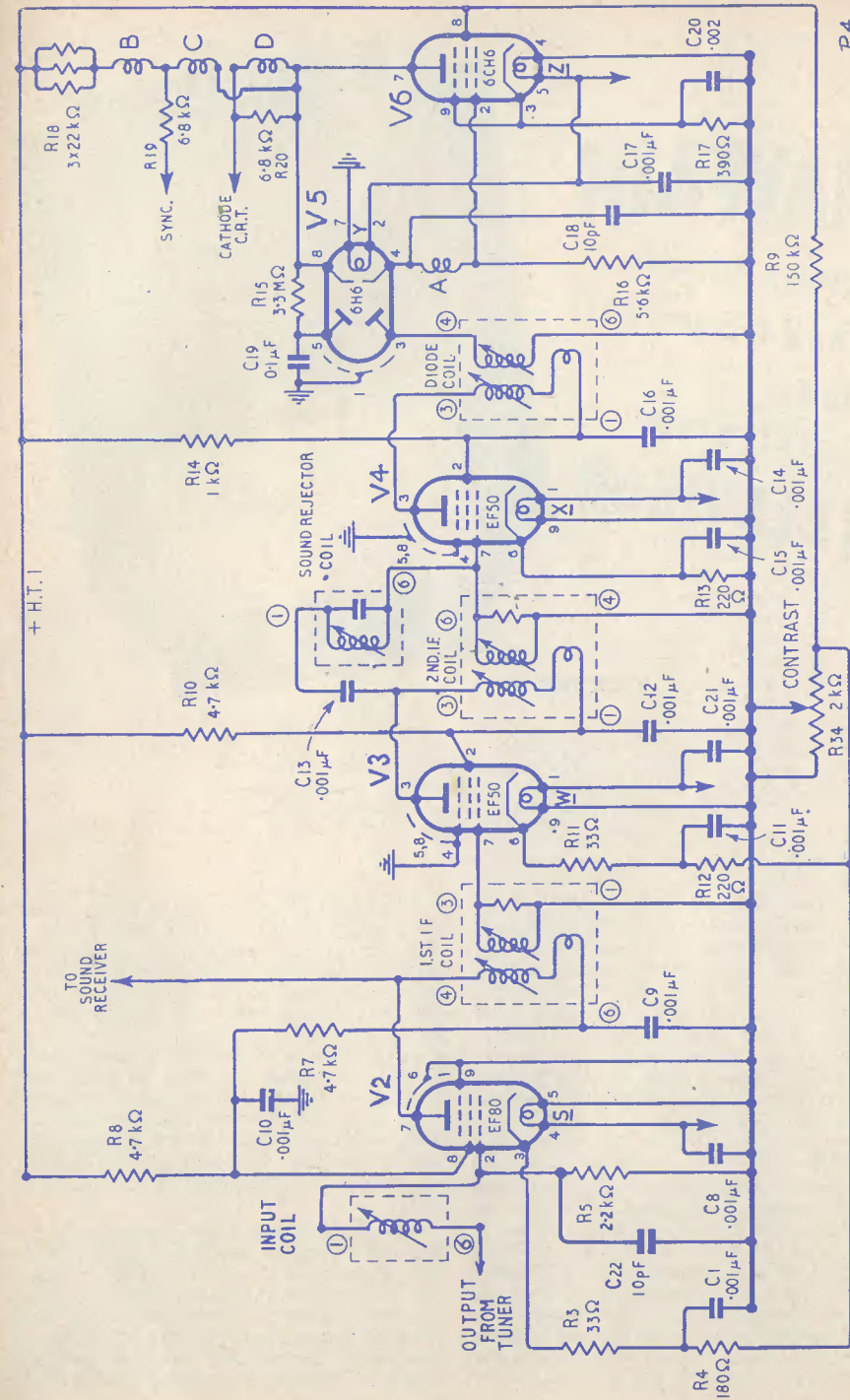


Fig. 4. The circuit of the vision i.f. strip

P.4.

COMPONENTS LIST SET OUT FOR EASY REFERENCE TO FIG. 4.

Vision I.F. Strip

Resistors (all  $\frac{1}{2}$  watt unless otherwise stated)

- R<sub>3</sub> 33Ω
- R<sub>4</sub> 180Ω
- R<sub>5</sub> 22kΩ
- R<sub>7</sub> 4.7kΩ
- R<sub>8</sub> 4.7kΩ
- R<sub>9</sub> 150kΩ
- R<sub>10</sub> 4.7kΩ
- R<sub>11</sub> 33Ω
- R<sub>12</sub> 220Ω
- R<sub>13</sub> 1kΩ
- R<sub>14</sub> 3.3MΩ
- R<sub>15</sub> 5.6kΩ
- R<sub>16</sub> 390Ω
- R<sub>17</sub> 390Ω
- R<sub>18</sub> 3 × 22kΩ 1 watt in parallel
- R<sub>19</sub> 6.8kΩ
- R<sub>20</sub> 2kΩ variable

Condensers

- C<sub>1</sub>, C<sub>8</sub> to 1,000pF
- C<sub>17</sub>, C<sub>21</sub> 10pF
- C<sub>18</sub> 0.1μF
- C<sub>19</sub> 0.1μF
- C<sub>20</sub> 2,000pF

Valves

- EF50 - 2
- EF80 - 1
- 6H6 - 1
- 6CH6 - 1

Chassis and Chassis Components

- 1 Vision i.f. chassis, fully punched—Premier Radio
- 2 Valveholders, B9A
- 2 Valveholders, B9G
- 1 Valveholder, International Octal
- 4 3-way tag strips (end tag earthed)
- 2 5-way tag strips (end tag earthed)
- 1 5-way tag strip (centre tag earthed)
- 1 Co-axial plug and socket

Miscellaneous

- 1 Grommet
- 2yd 2mm sleeving
- 2yd tinned copper connecting wire (22 s.w.g.)
- 1½yd p.v.c. covered wire
- Nuts, screws, solder tags, etc.

Coils

- 1 Input Coil—Premier Radiadio
- 1 First I.F. Coil—Premier RO
- 1 Second I.F. Coil—Premier Radio
- 1 Sound Rejector Coil—Premier Radio
- 1 Vision Diode Coil—Premier Radio
- 3 Video Chokes type 604 ("B," "C," and "D")—Premier Radio
- 1 Video Choke type 872 ("A")—Premier Radio

\* R<sub>34</sub> is fitted at a later stage.

by the more usual transformer assembly wherein primary and secondary are separate coils spaced away from each other. Also connected to the anode of the EF80 is a take-off lead feeding into the sound i.f. strip. As will be gathered, the EF80 carries out the dual functions of sound and vision i.f. amplification, whilst the remaining valves in the strip are concerned with handling the vision i.f. signal only.

The second i.f. amplifier valve, V<sub>3</sub>, follows the first I.F. Coil, and consists of an EF50. As was mentioned in last month's issue, the use of readily obtainable valves which are still "current," whilst also being available through ex-Government channels, is part of the policy behind the design of the Mayfair. Where such valves have no detrimental effect on performance their inclusion in the circuit confers the obvious advantage of saving in cost. An EF50 is a very good choice for the

second i.f. amplifier, and, in practice, performs very well in this position.

In order to maintain a stable input capacity for V<sub>3</sub> during changes in bias voltage (given by adjustments to the contrast control), part of this valve's cathode bias network consists of the unbypassed 33 ohm resistor R<sub>11</sub>. As the use of an unbypassed resistor at this point stabilises input capacity, it also prevents detuning of the first I.F. Coil secondary when contrast is varied. An unbypassed resistor, R<sub>3</sub>, is included in the cathode circuit of the EF80 for the same reason.

The anode of the second i.f. amplifier couples into the second I.F. Coil, this feeding the third i.f. valve, V<sub>4</sub>, in normal fashion. A second EF50 is employed here and, since this valve has a fixed bias potential, its cathode bias resistor is by-passed by the 0.001 μF condenser C<sub>15</sub>. Also connected between the second and third i.f. amplifiers is the Sound

Rejector Coil. This coil resonates with its parallel condenser to provide rejection at the sound i.f., giving, therefore, a "dip" in the overall response at this particular frequency. C<sub>13</sub>, connected in series with the Sound Rejector Coil, has negligible impedance at the frequencies involved, and functions merely as a d.c. blocking condenser.

The third i.f. amplifier valve feeds into the Diode Coil and, thence, to the video diode itself. This diode consists of one-half of the 6H6, V<sub>5</sub>, and it functions in a simple series-connected circuit. The rectified video signal provided by the diode appears across R<sub>16</sub>, the choke between this component and the cathode of the diode functioning as an i.f. filter. The video appearing across R<sub>16</sub> is then applied directly to the control grid of the 6CH6 video amplifier. Since the video at its grid is positive-going, the 6CH6 may be biased well back, thereby preventing excessive cathode current in the absence of signal voltage. The video at the anode of the 6CH6 is negative-going and is applied to the cathode of the c.r.t. As will be seen, no a.c. couplings at all are employed in the video amplifier section of the Mayfair, this representing a very desirable design feature. Three peaking chokes appear in the 6CH6 anode circuit, these ensuring that the higher video frequencies are applied to the c.r.t. cathode without undue attenuation. Also connected to the anode of the video amplifier is a simple noise limiter circuit which includes the remaining diode of the 6H6. The noise limiter circuit operates in the following manner. In the absence of interference the condenser C<sub>19</sub> remains charged at a value corresponding to the peak negative voltage level in the picture. Interference pulses causing greater negative excursions in video amplifier anode voltage are not normally of sufficient duration to alter the voltage across C<sub>19</sub>, with the result that the diode then prevents them from rising to levels noticeably higher than the peak picture level.

#### Layout and Construction

The layout of the vision i.f. strip is shown in Figs. 5 and 6. As occurred in the layout illustrations given in last month's article, all components in these two diagrams are designated either with their circuit reference or with a separate letter or number reference. These references are then used in the step-by-step instructions which describe the assembly. Valves, incidentally, are identified here by their reference letters, viz. "S" to "Z." It may be noted that one tag on each of the tag-strips is shown black. This tag is that which is used for mounting and which is, consequently, at chassis potential. All the i.f. coils have four tags, tag No. 1 being indicated on the coil itself by a red spot. The remaining

tags are then numbered 3, 4 and 6 in a clockwise direction looking down at the bottom of the coil. Coil tag numbers are clearly illustrated in Fig. 6.

Construction commences by fitting the major components to the chassis. The first of these are valveholders S and Z, both being mounted above the chassis. Care should be taken to ensure that correct orientation is observed. One of the mounting screws of valveholder Z secures 5-way tag-strip H, whilst the other mounting screw secures earthing tag T2. One of the fixing screws of valveholder S secures 3-way tag-strip K. Valveholders W, X and Y are next fitted, these being on the underside of the chassis. As with the two previous valveholders, care should be taken to ensure that correct orientation occurs. Next come the three 3-way tag-strips B, D and F; the two 5-way tag-strips E and L; earthing tag T1; and grommet G1. The positions of all these components are clearly shown in Figs. 5 and 6. They are followed by the input socket, under one fixing bolt of which is secured earthing tag T3. Finally, the coils are fitted, taking care once again to ensure that the pins take up their appropriate positions as shown in the diagram.

It should be stated at this point that it is possible that constructors making the vision i.f. strip may be supplied with a chassis which is punched for one valveholder and two coils in excess of those required by the Mayfair circuit. The additional holes in such chassis appear at the input socket end, and should be ignored.

Wiring up now commences. It is important to see that the components fitted take up the positions illustrated in the layout diagrams and that connections are kept short. The first components to wire up are the i.f. coils. Commence by connecting tag 1 of the Input Coil to pin 2 of valveholder S. Connect tag 1 of the first I.F. Coil to tag 3 of tag-strip E; tag 3 of this coil to pin 7 of valveholder W; tag 4 of this coil to pin 7 of valveholder S; and tag 6 of this coil to tag 2 of strip K. Next connect tag 1 of the second I.F. Coil to pin 2 of valveholder W; tag 3 to pin 3 of valveholder W; tag 4 to earthing tag T1; and tag 6 to pin 7 of valveholder X. The Sound Rejector Coil follows, tag 6 of this coil being connected to pin 7 of valveholder X. Tag 1 of the Sound Rejector Coil is connected later. Finally make the following connections to the Diode Coil: tag 1 to pin 2 of valveholder X; tag 3 to pin 3 of valveholder X; tag 4 to pin 3 of valveholder Y; and tag 6 to tag 3 of strip F.

We now carry on to the general wiring of the strip. The heater wiring is first of all completed by connecting together pin 4 of valveholder S, pin 1 of valveholder W, pin 1 of valveholder X, pin 2 of valveholder Y and

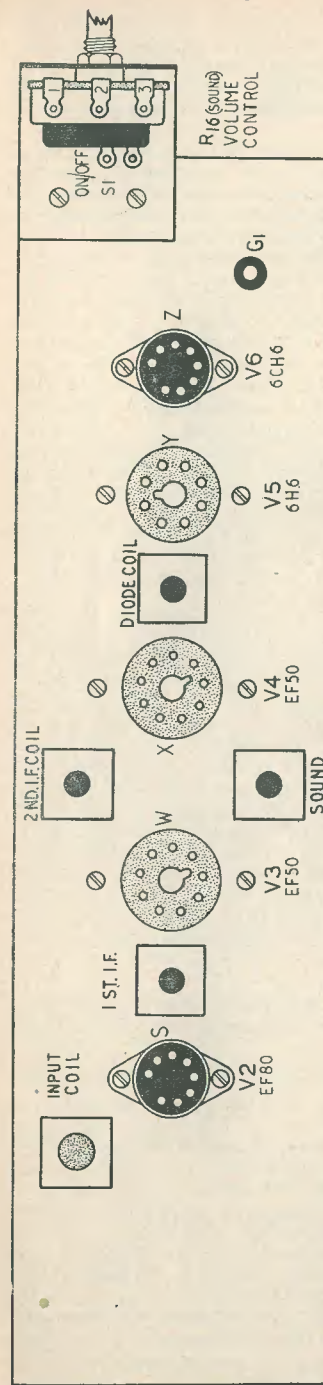


FIG. 5

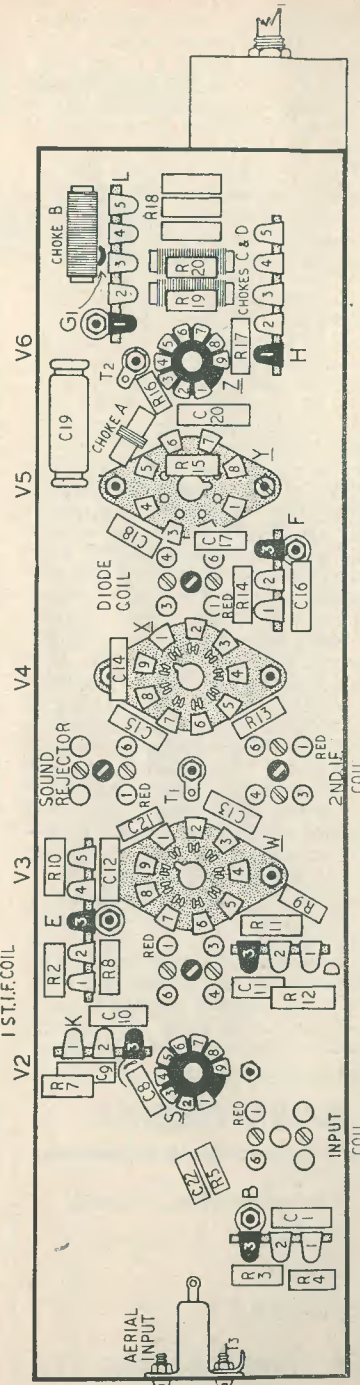


FIG. 6

Fig. 5. Layout of the vision i.f. strip above the chassis. Although illustrated in this diagram, the volume control with its bracket, need not be mounted at this stage. Fig. 6. Under-chassis layout of the vision i.f. strip.

pin 5 of valveholder Z. The condensers are tackled next, in the following manner. C<sub>1</sub> connects between tags 2 and 3 of strip B; C<sub>2</sub> between pin 4 of valveholder S and tag 3 of strip K; C<sub>3</sub> between tags 2 and 3 of strip K; and C<sub>10</sub> between tags 1 and 3 of strip K. These are followed by C<sub>11</sub> between tags 2 and 3 of strip D; C<sub>12</sub> between tags 3 and 5 of strip E; C<sub>13</sub> between pin 3 of valveholder W and tag 1 of the Sound Rejector Coil; C<sub>14</sub> between pins 1 and 8 of valveholder X; and C<sub>15</sub> between pins 6 and 8 of valveholder X. Wiring up of the condensers is completed by connecting C<sub>16</sub> between tags 1 and 3 of strip F; C<sub>17</sub> between tag 3 of strip F and pin 2 of valveholder Y; C<sub>18</sub> between tag 3 of strip F and pin 4 of valveholder Y; C<sub>19</sub> between pin 5 of valveholder Y and earthing tag T2; C<sub>20</sub> between pin 3 of valveholder Z and tag 1 of strip H; and C<sub>21</sub> between pins 1 and 8 of valveholder W.

The condensers are succeeded by the resistors. First of all connect R<sub>3</sub> between pin 3 of valveholder S and tag 2 of strip B; R<sub>4</sub> between tags 1 and 2 of strip B; R<sub>5</sub> between pin 2 of valveholder S and tag 3 of strip B; R<sub>7</sub> between tags 1 and 2 of strip K; R<sub>8</sub> between tags 2 and 4 of strip E; R<sub>9</sub> between tag 4 of strip E and tag 1 of strip D; and R<sub>10</sub> between tags 4 and 5 of strip E. R<sub>11</sub> next connects between pin 6 of valveholder W and tag 2 of strip D; R<sub>12</sub> between tags 1 and 2 of strip D; R<sub>13</sub> between pins 4 and 6 of valveholder X; R<sub>14</sub> between tags 1 and 2 of strip F; and R<sub>15</sub> between pins 5 and 8 of valveholder Y. The resistors are completed by connecting R<sub>16</sub> between pin 2 of valveholder Z and earthing tag T2; R<sub>17</sub> between pin 9 of valveholder Z and tag 1 of strip H; R<sub>18</sub> between tag 5 of strip H and tag 4 of strip L; R<sub>19</sub> between tag 2 of strip L and tag 2 of strip H; and R<sub>20</sub> between tag 3 of strip L and tag 3 of strip H. This completes the resistors.

The four chokes have next to be connected. These components should be handled with some care in order to avoid damage to their windings. Choke A (the diode filter choke, type 872) connects between pin 4 of valve-

holder Y and pin 2 of valveholder Z. Choke B connects between tags 2 and 5 of strip L; and choke C connects between tag 2 of strip L and tag 3 of strip H. Choke D connects between tag 3 of strip L and tag 3 of strip H.

All that now remains is the completion of the interstage and valveholder wiring. Chassis connections to valveholder S are first made, this being done by connecting together pins 5, 6, 9 and the centre spigot of this valveholder and earthing these to tag 3 of strip K. Similarly connect together pins 4, 5, 8, 9 and the centre spigot of valveholder W, earthing to tag 3 of strip E. Also connect together pins 4, 5, 8, 9 and the centre spigot of valveholder X, connecting to chassis via earthing tag T1. Pins 1 and 7 of valveholder Y are next wired together, these connecting to chassis via earthing tag T2. Also connected to tag T2 are pin 4 and the centre spigot of valveholder Z. Follow these operations by connecting together tag 4 of strip E, tag 2 of strip F, tags 4 and 5 of strip H, and pin 8 of valveholder Z. Connect together tag 1 of strip K and pin 8 of valveholder S. Also connect together pins 1 and 3 of valveholder S.

The vision strip is completed by carrying out the following final wiring. Connect together pin 8 of valveholder Y, pin 7 of valveholder Z and tag 3 of strip H. Next connect together the following pairs of circuit points: tag 1 of strip K to tag 2 of strip E; tag 5 of strip E to pin 2 of valveholder W; tags 4 and 5 of strip L; tag 1 of strip F to pin 2 of valveholder X; pins 3 and 9 of valveholder Z; and tag 1 of strip B to tag 1 of strip D. Connect an 11-in lead to tag 1 of strip D. This lead will be later connected to the contrast control. Finally connect a 24-in lead to tag 3 of strip L. This lead later connects to the cathode of the c.r.t.

The vision i.f. strip is now complete.

#### Next Month

In next month's issue the assembly and wiring of the timebase section will be dealt with.

## ELIMINATING



by J. G. WARD

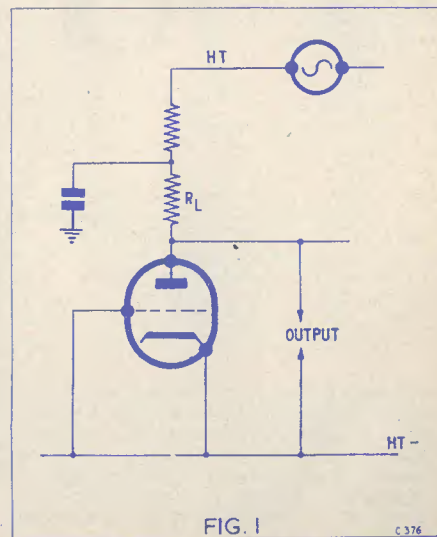
THE ELIMINATION OF HUM IS A PROBLEM that sooner or later confronts every designer or builder of high quality amplifiers. It becomes increasingly difficult as the input signal level decreases and when high gain is necessary. Some recognition of the characteristic types of hum from different sources and how it enters into the system is necessary to enable practical methods to be devised to get rid of it. Shielding, layout, planning of earth leads and filtering all form part of the problem, and although instruments—an oscilloscope and a valve voltmeter—are helpful, these are not generally available to the average home constructor, and moreover, a very satisfactory job can be done without them.

It should be clearly understood that high fidelity reproduction demands a much lower relative hum level than does ordinary radio quality. In a good amplifier, the hum level should be 50 to 60 db below average listening level. The low level inputs available from tape playback heads, microphones and some pick-ups, together with the bass boost required, tend to aggravate the situation and good quality reproduction requires more care when dealing with this problem.

Anode supply ripple, due to insufficient filtering, is always a 100 cycle note, and can readily be located by connecting extra condensers across the h.t. supply. The power supply filter should contain components, chokes and condensers adequate for the equipment it is intended to operate; a single section filter, using a good choke and, if possible, paper condensers, is generally adequate for any power stage, and with additional decoupling for each preceding voltage amplifier stage will generally ensure freedom from ripple. Where negative smoothing is employed, it is as well to have some series impedance in the positive line to get rid of ripple, which may be

coupled through the mains transformer capacitance.

The filtering action of any given section is better the lower the d.c. current drain, so that an R-C filter section, supplying only one or two milliamps to a resistance-coupled stage, will provide much more filtering than a similar stage drawing a heavy current. Push-Pull stages require less filtering and decoupling than do single-ended stages; power pentodes and tetrodes are more tolerant of anode supply ripple than are triodes, because of their higher anode resistance, i.e., a volt of ripple produces less anode current swing. Negative feedback over the output stage will reduce hum originating in that stage, but will not reduce hum originating in the earlier stages which may be included in the feedback loop.



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The a.c. ripple voltage actually appearing at the anode of a valve is less than that at the h.t. connection by the ratio

$$\frac{R_a}{R_L + R_a}$$

where  $R_L$  is the anode load resistance and  $R_a$  the anode resistance of the valve. In Fig. 1, if the valve is an L63, operating with an anode load of 100,000 $\Omega$  and an anode impedance of 10,000 $\Omega$ , only 1/11 of the h.t. supply ripple will appear at the anode.

where one side of the heater supply is earthed, it is from 20 to 30 db. The optimum point is best determined by trial and error, and is less critical the lower the impedance of the grid circuit. In the event of it being necessary to replace a valve at some future date, the adjustment may need varying.

It is not obvious why the heater supply should be tied to earth. If this were not done, the heater winding would assume a high a.c. potential, obtained through its capacitance to the high voltage winding of

to the nominal rating of the heater supply voltage, i.e., with most modern valves, 6V instead of about 300V. When the centre tap of the heater supply is earthed, two a.c. potentials of about 3V each can couple hum into the grid circuit; these two 3V potentials are 180 degrees out of phase and their effects more or less cancel each other. It may be thought that an exact centre tap would be all that is necessary for the hum to be neutralised; but the stray impedances from each side of the heater to the grid are rarely equal; it is for this reason that the hum balancing potentiometer adjustment generally effects an improvement.

#### Wiring Techniques

Capacitance from any a.c. wiring to a low level signal circuit introduces a 50 cycle voltage therein in direct proportion to the a.c. voltage present, the stray capacitance and the impedance of the affected circuit. In Fig. 2 is depicted a grid circuit with a resistance  $R$  of 1M $\Omega$  coupled to a stray capacitance of 1pF shown as  $C_1$ . If the hum voltage  $E_1$  is 1 volt there will appear at the grid 1/3,200 of a volt, about 1/3 millivolt, since the reactance of 1pF at 50 c/s is about 3,200M $\Omega$ ; if  $C_1$  should be coupled to a 300 volt mains transformer lead the grid circuit would receive 300/3,200 volt, about 0.10 volt. 1pF is about the capacitance between two pieces of push-back wire, an inch long, loosely twisted together. Fig. 3 shows the same situation where the signal source  $C_2$  is capacitance, as from crystal microphones and pick-ups. The stray hum capacitance and the signal source act as a capacitive voltage divider.

This does not mean that all low-level input wiring should be located feet away from everything else or that everything should be elaborately screened; rather it is necessary to be aware of the problem and the extent of the effects. Extravagant use of screened wire is rarely necessary; if it is, it indicates a poorly planned chassis layout. The capacitance between two wires can be kept very low, (a) if they are about 2in apart, (b) if they are kept close to the chassis and not up in the air, (c) if the layout is planned so that bypass condensers and other components not associated with the "hot" grid circuits assist in the shielding. Twisting heater leads together helps, although not absolutely necessary, providing they are close together and grid leads are kept away. It is as well to use screened braid on the grid lead to a top cap grid and to use a grid cap shield as well. The hole where such leads pass through the chassis should have a rubber grommet in it to avoid an

earth loop. It is not wise to use a blank tag on a black phenolic valveholder as an anchor point for top cap grid leads, as there can be an unbalanced leak across the valveholder tags.

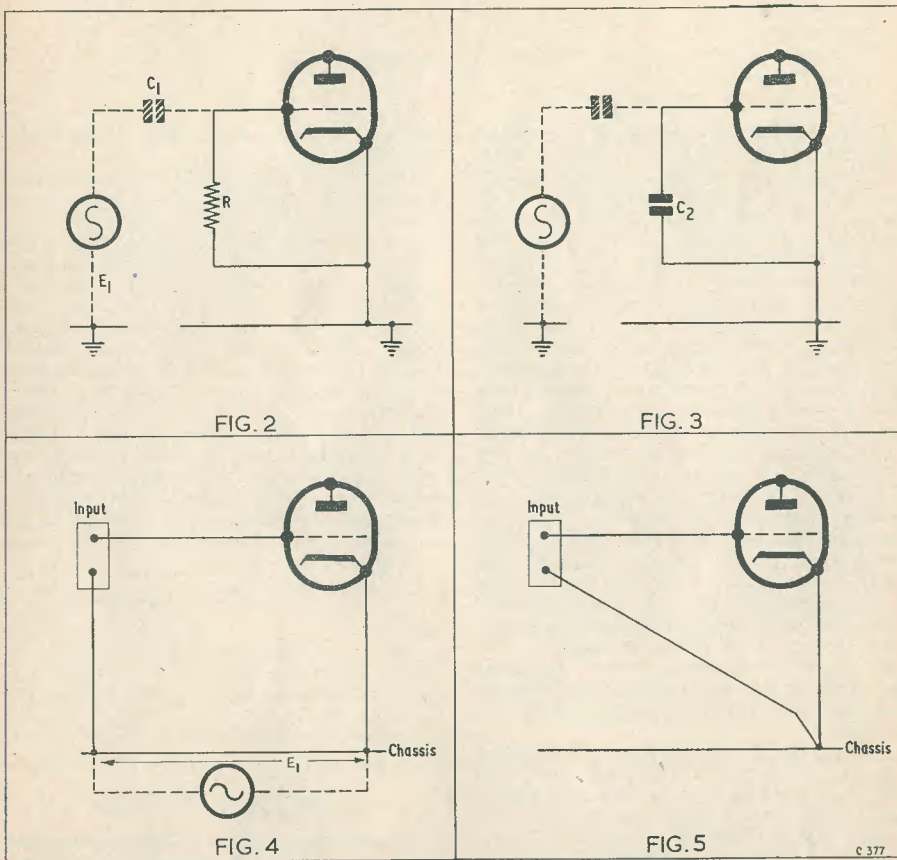
#### Earth Loops

Currents of half a millivolt per foot often exist across a chassis on which a mains transformer is mounted; the transformer winding induces a 50 cycle voltage, causing a current to circulate in the chassis. It is asking for trouble to include a section of chassis in series with a low-level input circuit. Fig. 4 shows what happens when the cathode and grid are returned to different points.  $E_1$  is a hum voltage distributed along the chassis; this voltage is included with the signal; the remedy is to return the grid and cathode to the same point, as in Fig. 5.

When wiring from a diagram it pays to study the purpose of each lead, to avoid a situation shown at Fig. 6 from developing. In this example too many earth leads have been used, forming a shorted turn or earth loop. Stray magnetic fields will induce an a.c. voltage in such a loop and the voltage across the loop is included in the grid circuit. If the grid lead and grid return lead are too widely separated, as in Fig. 7, another one-turn coil is created, ready for the induction of a 50 c/s voltage. As the voltage induced in a loop is proportional to its area, the remedy is to keep the grid return lead and the grid lead close together.

Fig. 8 shows how the pick-up lead can innocently cause hum to be introduced into the input circuit. This shows the screened pick-up lead earthed to the gramophone motor frame at one end, and to the amplifier chassis at the other. The motor frame has a capacitance to the mains line, as has the amplifier chassis; these capacitances are shown as  $C_1$  and  $C_2$  in the sketch with the mains voltage in between. A hum voltage is thus applied across the ends of the pick-up lead screening. The remedy, shown at Fig. 9, is to use the screening only for the signal voltage and to use a separate wire to connect the motor frame to the amplifier chassis; better still is to use twin screened lead. In this way loop pick-up effects can be avoided.

Sometimes an otherwise perfect amplifier when used with a radio tuner unit will produce modulation hum, when the tuner is tuned to a powerful carrier wave. This is due to rectification of r.f. picked up by the house wiring, the rectified signal being modulated by a.c. The remedy is to eliminate the r.f. signals by preventing them from



In high fidelity low level amplifiers with a.c. heater supply, it is advisable to use a hum-balancing potentiometer of about 200 ohms across the heater supply, with the movable arm earthed. This arrangement will generally reduce the hum in the input stage 10 db over the level apparent when the transformer centre tap is used; in cases

the mains transformer. Through capacitance and leakage from heater to grid and other paths, this high a.c. potential couples large hum voltages into the signal circuits; it may even break down the heater-cathode insulation inside the valve. When one side of the heater supply is earthed, the a.c. potential for such stray coupling is reduced

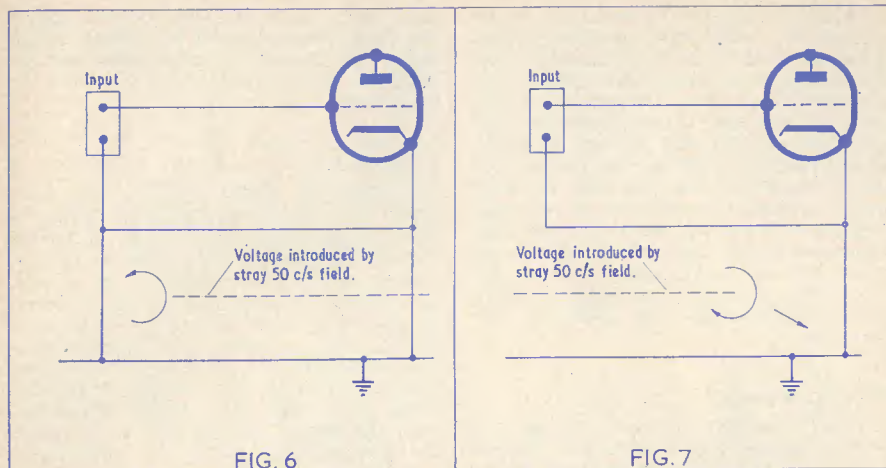


FIG. 6

FIG. 7

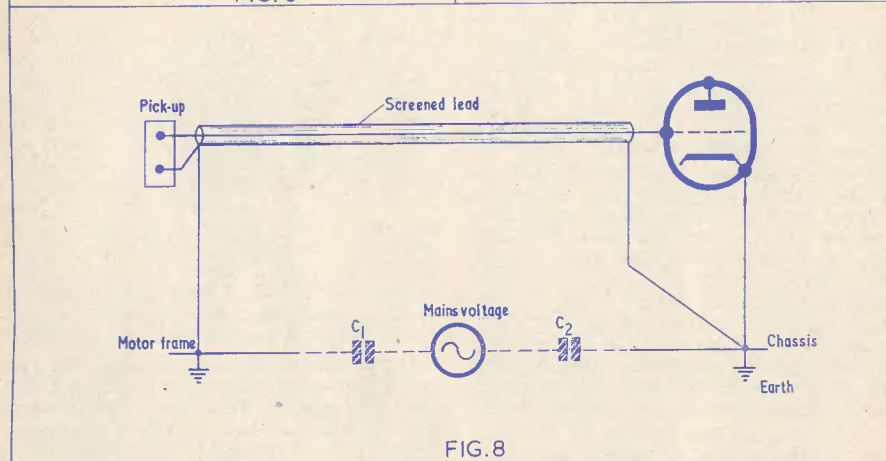


FIG. 8

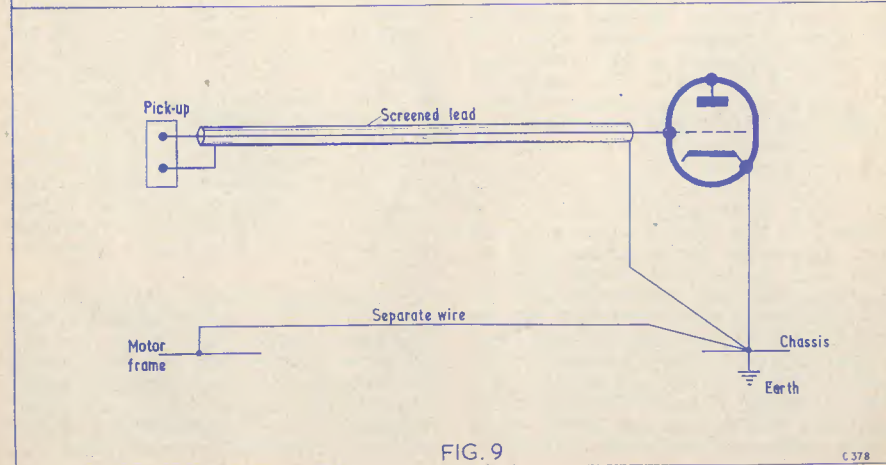


FIG. 9

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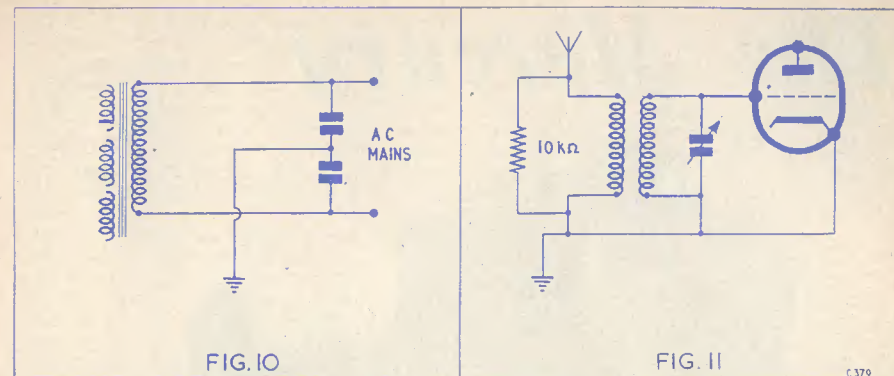


FIG. 10

FIG. 11

C.379

getting into the amplifier from the a.c. line; this can be done by earthing both sides of the mains through condensers of about 0.005 to 0.01 $\mu$ F; see Fig. 10. If the

hum persists, a 10,000 $\Omega$  resistor connected between the earth and aerial terminals of the tuner will generally clear the trouble; see Fig. 11.

## Can Anyone Help?

Requests for information are inserted in this section free of charge; subject to space being available

B. N. HOPKINS, ZL1DJ, c/o 145 Euston Road, Morecambe, Lancs., would like to purchase the manual, or circuit, of the Hallicrafters SX28A communications receiver.

J. R. NORRIS, 98 Wickham Hill, Hassocks, Sussex, wishes to obtain an aerial coil for a pre-war Pye Model PS/B, and wishes to know if anyone has such a component to dispose of.

S/Sgt. SOUTHWY, 23 Para FD AMB, Parsons Barracks, Aldershot, wishes to purchase or borrow for payment the circuit and/or instruction manual for the ex-AM Test Set No. 31. All correspondence answered.

D. GIBSON, G3JDG, 5 Edward Close, St. Albans, Herts, is praying some kind angel will lend a circuit diagram of the Premier 6in televisor. Would return same unmarked by return of post.

W. KAY, 66 Kirk Street, Bolton, Lancs., wishes to borrow or purchase information, service data, etc., for the American u.h.f. receiver type R-3A/ARR-ZX (also type numbered: Receiver R1584—possibly British Services number).

G. HEDLEY, 4 Furze Road, Tadley, Basingstoke, Hants., wishes to obtain circuit details, valve types and conversion data for the Unit No. LU244.

C. E. WARD, 280 Deansgate, Manchester 3, Lancs, wishes to obtain circuit diagram or any relevant information on the R.1355 for conversion to inexpensive television (or a copy of Data Book 4, "Inexpensive Television").

A. F. SMITH, 61 Westfield Road, Dagenham, Essex, wishes to borrow or purchase any information on, or the circuit of, the 12in Defiant T.V. Model TR1246, drawings No. 2817 and 2818.

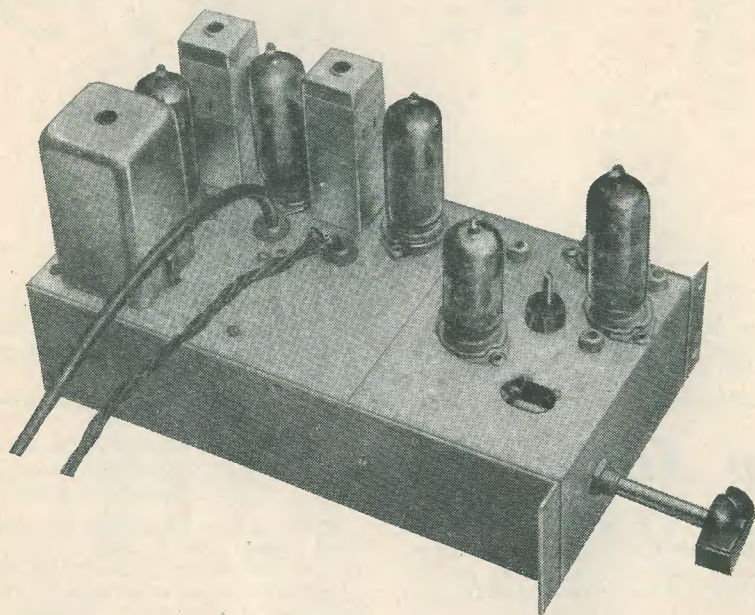
J. H. BACHELOR, 36 Hadley Way, Winchmore Hill, London, N.21, wishes to obtain information on, or uses for, the Raytheon valves JRP5676, JRP5672, JRP5678 and JRP2621 (2G21?).

C. G. PRATT, 1 Ridley Street, Kettering, Northants, wonders if any reader can supply information and circuits of transistorised hearing aids.

R. LENG, 12 Poplar Street, Failsworth, Lancs, wishes to borrow or purchase servicing data and the circuit of the Baird model T165 televisor. He has a number of old copies of *The Radio Constructor* and various radio books for disposal; please state wants.

F. G. MORGAN, 68 Arnfield Road, Withington, Manchester 20, would like to buy or borrow a copy of *The Radio Constructor* for May 1952.

# The Mercury



## SWITCHED F.M. TUNER

### Part 1

A new Jason kit described by G. BLUNDELL.

THE V.H.F.-F.M. METHOD OF TRANSMISSION has now been in use for a number of years and covers a considerable part of the country. The quality and freedom from interference is something which the man in the street has now come to accept and expect. The woman in the street, though, finds the tuning a little more complex and is not prepared to tune for maximum reduction of interference. She will not really accept f.m. until all tuners are as simple to use as the switched tuner described in this article.

### Why V.H.F.?

The medium waves are, of course, already overcrowded, and even with a limited audio range a whistle filter must be used to intercept the carrier of the adjacent stations. Also, the sidebands of the adjacent stations will be heard and the background can never be really quiet except under very favourable conditions. V.H.F. was, therefore, the only choice, and this has the advantage that the range of trans-

missions is not much greater than line of sight, and so stations spaced 200 miles apart can use the same frequency with no danger of interference. This does not mean that the service area of the v.h.f. station is less than that of a M.W. one, since the latter will not give a first class service area much greater than that covered by line of sight, although, of course, poorer signals can be obtained at much greater distances.

### Why F.M.?

The decision to use f.m. was nearly unanimous by the committee set up to study the problem. One point made against f.m. was that it was more complex and difficult to align, and to ensure the life stability necessary to achieve the best results. This, surely, is a challenge which will be met by manufacturers, and is met in the tuner described in this article.

Pre-war life-stability of 465 kc/s i.f.'s was something of a problem when almost univer-

sal use was made of compression condensers for tuning, but with the advent of dust iron cores this problem has nearly vanished. The simplest possible f.m. set is more complex than the equivalent a.m. set, but when the latter is fitted with the necessary impulse limiting circuits, there is not much difference.

A simple listening test, though, at almost any position except, perhaps, within a couple of miles of the station, shows the superiority of the f.m. signal as regards freedom from impulsive interference and far lower background noise. Complex limiters on the a.m. receiver could, of course, improve the rejection of the impulsive interference, but there is nothing that can be done about the background noise. This test could only be made when the B.B.C. were radiating the same programme on both f.m. and a.m.

It might be expected that the a.m. transmission would require a narrower bandwidth receiver, and that there could be more transmitters in the same band. Unfortunately, though, the complex limiters used rely, for optimum working, on having a wide bandwidth in the receiver in order to produce interference pulses with a sharply rising wave shape. When this is taken into account, and it is also remembered that the stability of v.h.f. oscillators is not so good as lower frequency types, one realises that the spacing could not be less than 0.2 Mc/s between stations. This is, in fact, the spacing chosen for f.m. transmissions.

transmissions, it is of interest to note that most of the new t.v. aerials are fitted with slot aerials, which are capable of radiating three f.m. programmes simultaneously.

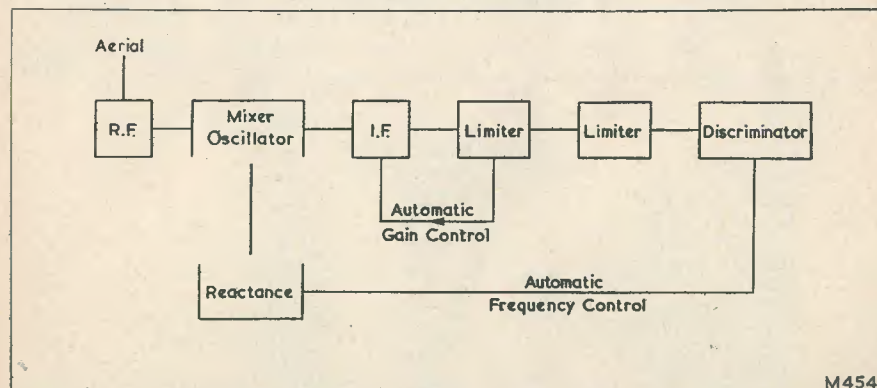
As reception is limited to line of sight, a switched f.m. tuner need only receive the three programmes once the novelty of listening to the police (an offence!—Ed.) and commercial transmissions has worn off. This does so rapidly, as the "programmes" radiated, while interesting, do not have much variety.

### Choice of Frequency of F.M. Stations

In any one area the three programme frequencies will be found to be spaced 2.2 Mc/s apart. The only limitation on choice is that adjacent channels should be about 2-300 miles away. This leads to the simplified method of switching used in this tuner. On the medium waves, frequencies have to be chosen to avoid after-dark interference. Interference may be expected from stations in Russia, Germany, Italy, etc., and, therefore, there is no simple relationship of frequencies of programmes in any one area.

### Wiring

In order to produce a successful design of tuner it is necessary to take into account all the variations of wiring which are possible. For example, all the exhortations about short wiring still does not make the average constructor forget his audio experience. Neat wiring is not necessarily the best from the v.h.f.



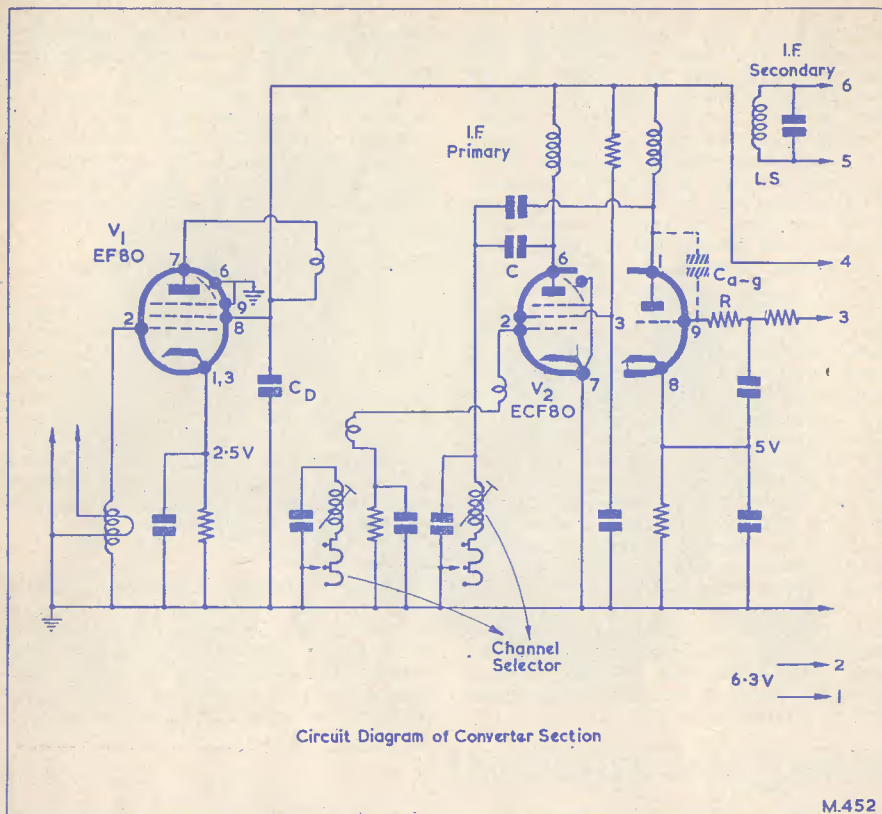
Block diagram showing arrangement of stages in the "Mercury" tuner

F.M. transmission can use any nominal bandwidth; the choice of the B.B.C. has been that  $\pm 75$  kc/s deviation of the v.h.f. carrier represents full modulation, and this happens at maximum audio amplitude at the frequencies normally encountered.

As Band I transmissions have approximately the same service area as Band II t.v.

point of view. Tag strips carrying components in the v.h.f. side are an impossibility.

The f.m. tuner described in Radio Reprint No. 2 has proved very tolerant of variations in wiring, and has thus been very successful. Long wiring in the r.f. stages produces instability, but elsewhere appears to have very little effect. The Argonaut A.M./F.M. Tuner,



### COMPONENT LIST

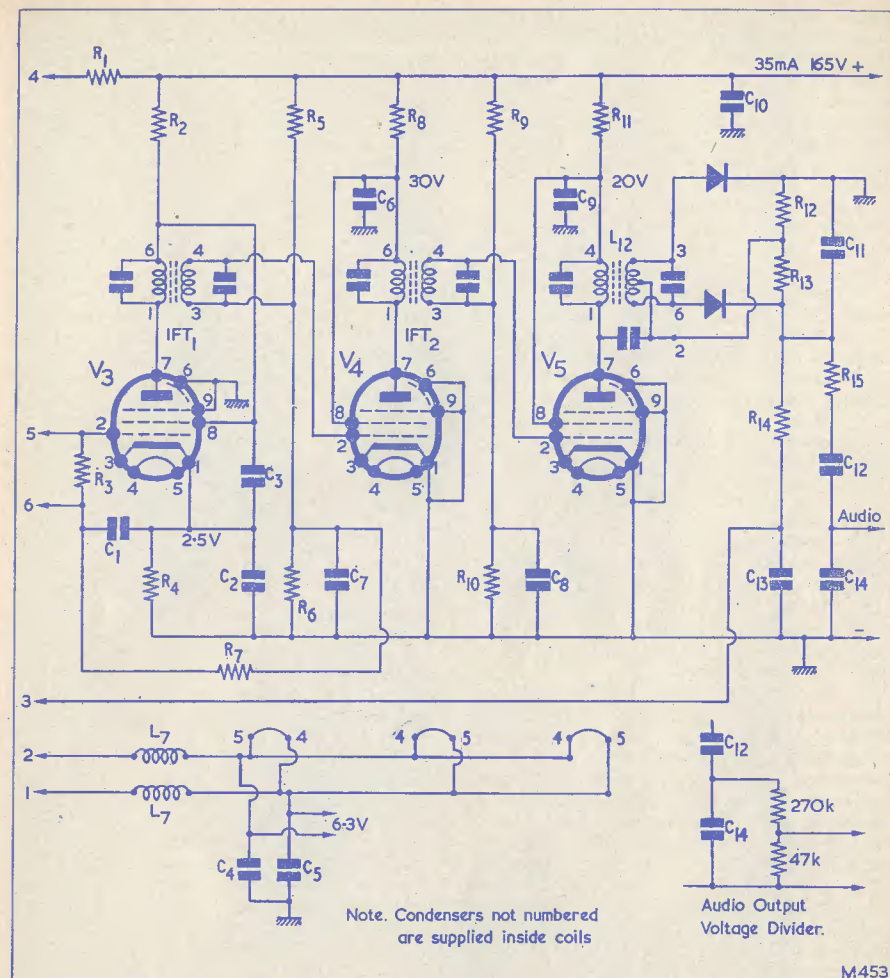
- |                 |                    |
|-----------------|--------------------|
| C <sub>1</sub>  | 0.005μF ceramic    |
| C <sub>2</sub>  | 0.01μF ceramic     |
| C <sub>3</sub>  | 0.005μF ceramic    |
| C <sub>4</sub>  | 0.001μF ceramic    |
| C <sub>5</sub>  | 0.001μF ceramic    |
| C <sub>6</sub>  | 0.005μF ceramic    |
| C <sub>7</sub>  | 47pF silvered mica |
| C <sub>8</sub>  | 47pF silvered mica |
| C <sub>9</sub>  | 0.005μF ceramic    |
| C <sub>10</sub> | 0.005μF ceramic    |
| C <sub>11</sub> | 200pF ceramic      |
| C <sub>12</sub> | 0.05μF paper       |
| C <sub>13</sub> | 0.05μF paper       |
| C <sub>14</sub> | 500pF ±10% ceramic |

- |                 |                      |
|-----------------|----------------------|
| R <sub>1</sub>  | 270Ω                 |
| R <sub>2</sub>  | 1kΩ                  |
| R <sub>3</sub>  | 47kΩ                 |
| R <sub>4</sub>  | 270Ω                 |
| R <sub>5</sub>  | 10MΩ                 |
| R <sub>6</sub>  | 100kΩ                |
| R <sub>7</sub>  | 100kΩ                |
| R <sub>8</sub>  | 47kΩ $\frac{3}{4}$ W |
| R <sub>9</sub>  | 2.2MΩ                |
| R <sub>10</sub> | 47kΩ                 |
| R <sub>11</sub> | 47kΩ $\frac{3}{4}$ W |
| R <sub>12</sub> | 100kΩ                |
| R <sub>13</sub> | 100kΩ                |
| R <sub>14</sub> | 2.2MΩ                |
| R <sub>15</sub> | 100kΩ                |

Chassis, ready punched, Jason Motor & Electronic Co.

Side panels (2), Jason Motor & Electronic Co.

- |                |       |                           |
|----------------|-------|---------------------------|
| V <sub>1</sub> | EF80  | } supplied with converter |
| V <sub>2</sub> | ECF80 |                           |
| V <sub>3</sub> | EF80  |                           |
| V <sub>4</sub> | EF80  |                           |
| V <sub>5</sub> | EF80  |                           |
- Crystal Diodes, GEX34



The converter section (Drawing M452) is supplied ready-built and tested, hence the absence of values  
The I.F., limiter and discriminator stages (Drawing M453) are assembled and wired by the constructor—the values of components are given in the list herewith

- IFT<sub>1</sub>, IFT<sub>2</sub> Type L4, Jason Motor & Electronic Co.  
IFT<sub>3</sub> Type L12, Jason Motor & Electronic Co.  
Heater chokes Jason Motor & Electronic Co.  
Valveholders (3), Nylon loaded B9A, McMurdo  
Tag strips, one 2-way, one 6-way, one 3-way less earth.

- Grommets (2)  
4-way power supplies lead  
Single screened audio lead  
Pointer knob  
Front end unit with name plate, completely wired and tested, Jason Motor & Electronic Co.

though, is more complex and, therefore, proved more troublesome. In fact, if the unit is built as described in the instructions (R.R. 3), no trouble results. There is, however, a great temptation to "tidy it up"; alternatively, if all condenser leads are carefully covered with systoflex, it is almost impossible to keep the wiring short enough.

Because of these points it has been decided to produce this design in two parts—converter and i.f. strip, and to supply the converter only as a ready-built unit in the same way as some Continental tuning units are available here. This decision was made because the frequency changer and reactance circuits have proved to be intolerant of alterations of layout and lead lengths.

The circuit, therefore, consists of the following stages as shown in the block diagrams: R.F.—F.C. and Oscillator—Reactance Section—I.F. Stage—Limiter—Limiter—Discriminator. The function of each stage will now be described.

#### The Converter

This unit, which is supplied ready-tuned, consists of the first three stages: R.F.—Frequency Changer—and Reactance Section.

The r.f. stage is an EF80 with the aerial/grid circuit pretuned to the middle of the band. In the anode circuit is a coil which is switch-tuned to each frequency.

The second valve is an ECF80 with the pentode section operating as a tri-oscillating frequency changer, while the triode section acts as the variable reactance.

Various types of frequency changer circuit were tried to find one which would give a reasonable gain in the presence of the damping imposed by the reactance valve. This is a type which, in addition to acting as a pentode mixer, also oscillates between anode and grid No. 1. The i.f. tuning condenser is marked C in the circuit diagram of the converter. It will be seen that the oscillator coil is in series with this condenser, but at i.f. the impedance of the oscillator coil can be ignored. The impedance of the decoupling condenser  $C_D$  is also low and, therefore, the condenser C is effectively across the coil at i.f. At oscillator frequency the circuit behaves quite differently. The condenser C now acts as a coupling condenser from anode to the oscillator coil, and the i.f. coil acts merely as a choke supplying h.t. to the anode, and otherwise may be ignored. A coupling coil is taken to the grid of the pentode and the circuit, therefore, oscillates. In series with this coupling coil is a second coil which injects programme signal from the r.f. stage to complete the frequency changing process.

#### Reactance Section

In order to keep the oscillator in tune there must be a variable reactance to correct

any mistuning, and appropriate circuitry makes the triode section of the ECF80 look like a capacity from the point of view of the oscillator circuit.

A reactance may be recognised in a circuit solely by the phase angle between the voltage across the circuit and the current in the circuit. If the voltage and current cycles are in step, maximum voltage and current occurring simultaneously, then the circuit is, in effect, a pure resistance. If the current cycle is  $90^\circ$  ahead of the voltage cycle, then the circuit is effectively a pure capacitance. Therefore, if a valve can be made to take current  $90^\circ$  ahead of the a.c. voltage (in this case the oscillator frequency), then the valve will look like a capacitance. This is done by feeding voltage to the grid of the valve through the internal capacity of the valve marked  $C_{ag}$  on the circuit. The phase of this voltage is altered by the resistance R in the grid circuit.

This results in a reactance whose actual capacity may be varied by altering the gain of the valve. Because the current and voltage are not exactly  $90^\circ$  apart, there is also a resistive component which does damp the oscillator section of the frequency changer circuit, hence the previous remarks about choice of suitable mixing circuit to work well in the presence of this damping.

A varying voltage is fed from the discriminator which is positive on one side of correct tune and negative on the other, and corrects any mistuning of the oscillator.

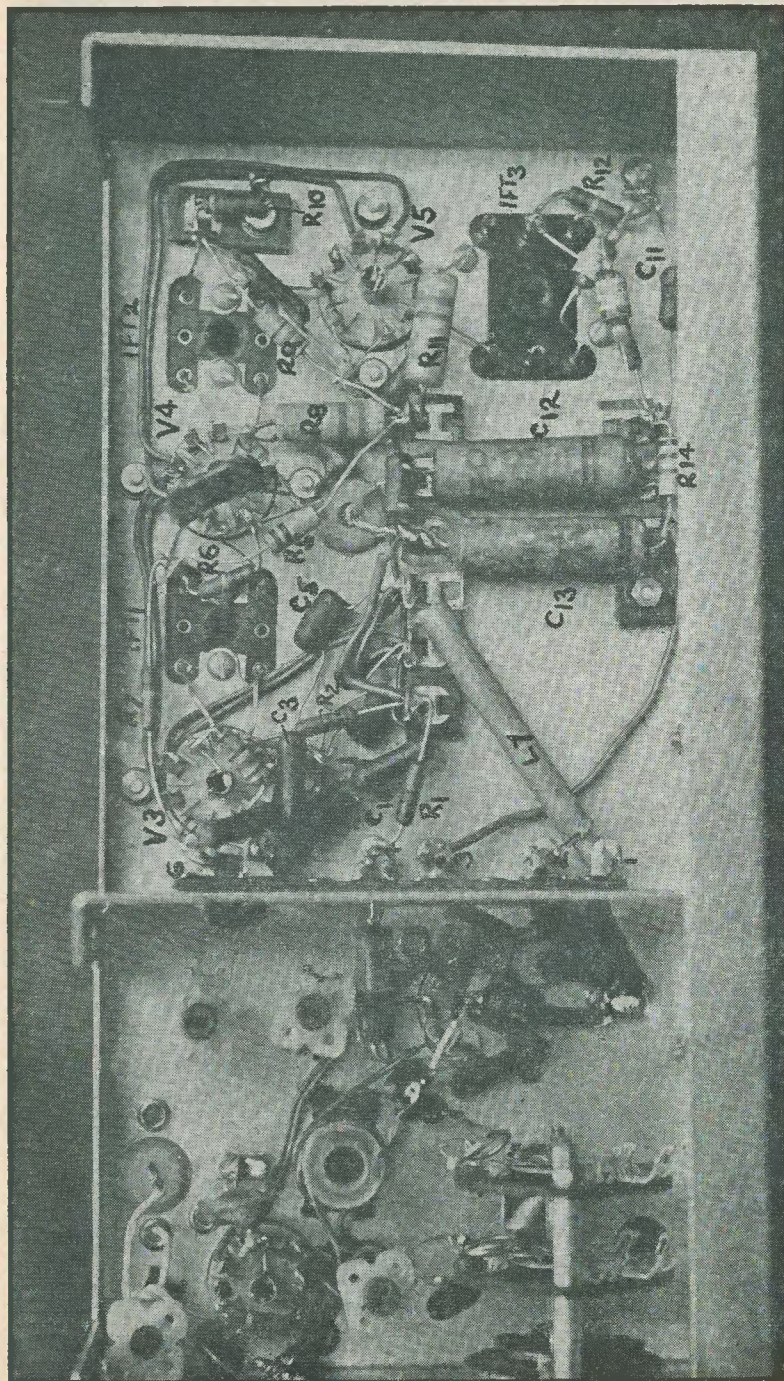
#### I.F. Stage

This is quite conventional, automatic gain control being fed back from the limiter to the grid of this valve.

Twin limiters are used. Without the second limiter the gain of the set is such that 100 microvolts of aerial signal produces 1 volt at the grid of the limiter. This is adequate to cover the average signal area of any of the stations. Unfortunately, considerable variations from the average signal may be found due to, for example, the receiving site being in a valley, or behind a gasholder. Alternatively, near an airport considerable variations of signal are found due to the strong signal reflected from the plane, which may momentarily cancel the normal signal. Twin limiters help to combat this, and result in an aerial sensitivity of better than  $10\mu V$ . A positive bias is applied to the grids through resistors  $R_5$  and  $R_9$  to improve the limiting action.

The Foster-Sceley Discriminator is the part of the set which differs most from the normal a.m. set. This circuit was chosen because of the greater output which results in a bigger correction voltage being applied to the reactance valve, and is the simplest circuit for normal use.

(to be continued)



Layout showing, on right, the location of main components of the I.F., limiter and discriminator section. This should be compared with the point-to-point wiring diagram to be given next month. Note that only one heater choke (L7) can be seen in this view, though there are actually two

## Radio Miscellany

JUDGING BY THE REQUESTS I HAVE RECEIVED in recent weeks from those who wish to be recommended an "ideal test-piece" record, there has been quite a revival in gramophone interest. Maybe this recent outburst is due to the fact that a wide range of 3 and 4-speed electric motors has recently been available at attractive prices. Or, of course, it may be that even in the matter of hi-fi, in order to keep up with the Jones's one's hi-fi has to be just that bit hi-fi-er than one's neighbours!

The latest enquiry comes from an Aberdeen reader who asks for a recommendation for a 45 r.p.m. (extended play) record of *permanent* interest. Seeing that these records are far from cheap he, with native thrift, wants one which can also be played for enjoyment. For the same reason he is not particularly interested in 33 r.p.m. (long play) records. He wants a recording of a good standard work which will be as satisfying to listen to in ten years time as it is today. Something which has solo passages, as well as the full crash of the whole orchestra in order to check for overloading. His ideal would have strings, brass and wind instruments all thrown in, with plenty of top and bags of bottom.

I am a little diffident about making a recommendation. So many saxpences will go bang if it fails to please. However, I have made a couple of modest suggestions by post, but I dare not put them forward publicly. There must be lots of records that meet such a demand more adequately than my limited knowledge of the record world covers. Every time I look at a catalogue of standard recordings I become deeply conscious of the shortcomings of my musical education!

Among the 33 r.p.m. long play types there are a couple of recognised favourites. The Petrouchka Ballet Suite (Stravinsky) has been used for years by Decca to demonstrate and popularise modern long-play record reproduction—a role it serves very effectively. That, however, is an expensive record—39/7½, or seventy-nine and a quarter saxpences. Another (at the same price) which might prove of interest is Britten's "Young Person's Guide to the Orchestra." The value of the latter as a test record lies in the fact that solo parts are provided for practically every instrument.

However, our reader wants a 7in extended play, so these two scarcely fill the bill.

Can any reader who has alighted (by accident or recommendation) on an extended play record which goes most of the way to satisfying the demands of a careful Aberdonian, both for test and entertainment purposes, please quote the make and number—and I will prepare a list (with any comments of interest) of those that get several votes.

### Like Topsy, it just Grewed

My reference to the use of the CQ call last month has raised a query as to its origin. A reader enquires whether it started simply because the letters seemed to be the most appropriate to use as a general call or an invitation to anyone to reply, or as part of a planned code. Its origin, of course, goes right back to the days before telephony, when with other abbreviations it quickly became general usage. It was readily recognised that sending common phrases in full was a shocking waste of time and effort. Hence the Q-code came into use—groups of three symbols all of which could be readily understood either as a request or confirmation. QSY, for instance, means either "Please change frequency" or "I will change frequency; and QRA, "What is your position?" or "My position is—"

As the most frequent use of radio communications was by the English-speaking peoples, "Seek-you" would undoubtedly be readily accepted as a most logical general call. Up to about 1912 the letters CQD (CQ-Distress) were used to mean exactly the same thing as the more modern SOS call. At the time of the *Titanic* disaster it was the CQD call which was used in the early transmissions asking for help. Later it was changed to SOS—a signal which had been agreed upon only a little earlier by an International Convention. It was felt that an unskilled operator could more easily send it, being a simple group of three dots and three dashes, and the humblest amateur picking it up would more readily recognise it. Some people, oddly enough, still harbour the belief that the letters stand for *Save Our Souls*, although obviously it would be meaningless to anyone who did not speak English.

Apart from all other considerations, the letters C and Q when linked in Morse possess a lovely natural rhythm. If you are not a code user, just sing to yourself the words "Charlie, Charlie. Here comes the Queen." There you have the perfect CQ call, the long syllables being the dashes and the short ones the dots. It also has the virtue that it is easily remembered as the dominant initial letters are C and Q.

### Chassis Bashing

I am beginning to wonder if this heading is not the most appropriate I have ever chosen. Recently I have seen so many chassis that were literally bashed out, rather than fashioned to shape by gentle persuasion, that it almost suggested itself.

I hate to feel that this column, which is supposed to be chatty, is in danger of developing into a lecture, but having ruined more good aluminium than anyone else in the United Kingdom, perhaps I can speak with some authority on the subject.

If you want the finished job to look like an exhibition piece—and who starting off with a sheet of virgin polished aluminium doesn't?—cover the bench with a pile of opened news-

papers. As the work proceeds, keep peeling the top sheet off. This way you will remove all the swarf which causes the horrible scratches which no amount of subsequent polishing will erase. In bending, scribe deeply and form the bends on angle iron by light, evenly spaced blows with a leather covered mallet. It is also important to keep hand pressure on the free end and so prevent it springing and whipping.

### Short Ends

Several more letters have come to hand from readers who would like to see a "Described—but not forgotten" column as a regular feature. To remind those with short memories, such a column was for constructors to air their views on the success (or otherwise) they met with in building sets described in these pages, or to share with others ideas for successful modifications they had tried. Judging by the correspondence on this subject, the Jason FM Unit was the most widely constructed item described in recent times. Incidentally, for Jason fans there is a new

CENTRE  
TAP

talks about

Items of  
General Interest

papers. As the work proceeds, keep peeling the top sheet off. This way you will remove all the swarf which causes the horrible scratches which no amount of subsequent polishing will erase. In bending, scribe deeply and form the bends on angle iron by light, evenly spaced blows with a leather covered mallet. It is also important to keep hand pressure on the free end and so prevent it springing and whipping.

So far these points are usually observed by the intelligent constructor, but only too often the aluminium doesn't readily bend. Hence the blows get heavier until it does, and the finished chassis is covered with small scars and bruises which permanently mar its appearance. Worse still, cracks often appear along the bent edge. The reason for this is that the aluminium is "old." Too much force used on old aluminium is almost certain to result in cracking.

What is not generally realised among beginners is that old aluminium can be rejuvenated, making it easier to work and avoiding cracking. Incidentally, pure aluminium is softer and does not age or become brittle like duralumin, etc. Aluminium alloys all appear to suffer from age hardening. The

model full details of which are to be found in this issue. The second most popular item was the Mullard "3-3" Quality Amplifier described in our April, 1956, issue. This, no doubt, would have proved even more popular if it had not required buying the more recently introduced valves!

Mr. A. J. Felstead of St. Luke's Road, Maidenhead, suggests a modification to the Rambler Portable, which he has used with excellent results in hotel bedrooms from Kent to Cornwall. When he tried to use it in his caravan which has an aluminium roof and body, the screening was so effective that the otherwise strong signals obtained were completely lost. He then arranged for a short throw-out wire aerial to be quickly attachable as an optional addition. A length of 15 feet was found to give full volume. It is connected via a 100pF capacitor to the grid of the first valve, the aerial being plugged into a neat socket brought out to the upper edge of the panel.

An interesting point is raised by a "3-3" amplifier builder, J. R. of Bristol. His model greatly impressed a neighbour, who persuaded him to build him one like it. When he built  
*(continued on page 202)*

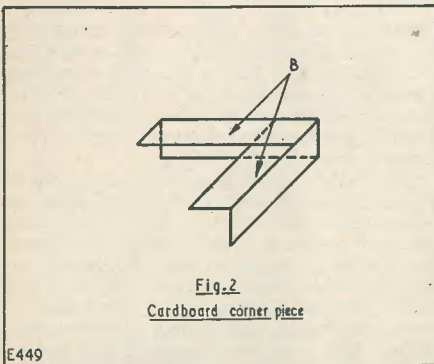
# Sand Filling the W.B. Senior Bass Reflex Corner Console

by E. G. WILSON

THIS ARTICLE DETAILS A SIMPLE METHOD of sand filling a commercial cabinet normally supplied in kit form. The materials required are easily obtainable, and the total cost of conversion does not exceed thirty shillings.

A sand-filled cabinet similar to the one described has been used for over two months in the writer's home, and in his opinion it represents a considerable improvement over the non-sandfilled version. This is due to the increased clarity of the bass response and a general reduction in resonances even on heavy orchestral passages and sustained organ notes.

The technique of construction is quite simple. By the use of  $1\text{in} \times \frac{3}{8}\text{in}$  strip and hardboard, cavities are added to each of the walls of the cabinet. These cavities are filled with dry sand.



Materials required are listed below. It is advisable to check dimensions and quantities before ordering to avoid waste.

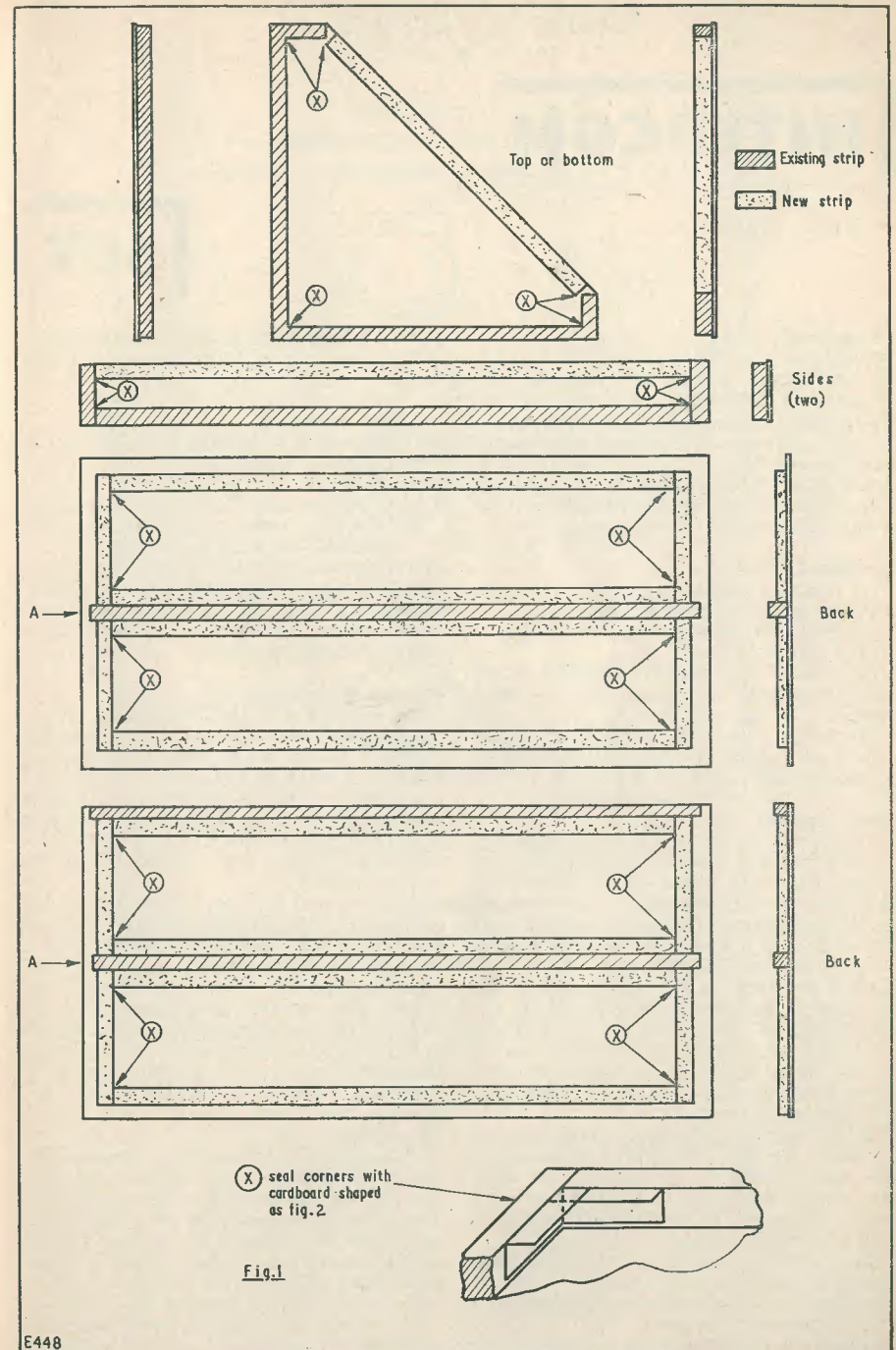
$\frac{3}{8}\text{in}$ hardboard ..	..	18 square ft.
$1\text{in} \times \frac{3}{8}\text{in}$ softwood ..	..	40ft
Builder's sand ..	..	2 bucketsfull
$1\text{in}$ and $\frac{3}{8}\text{in}$ panel pins ..	..	as required
"Casco" glue ..	..	or similar
"Croid" glue ..	..	or similar
$\frac{3}{4}\text{in}$ carpet underfelt ..	..	1 square yd.
Drawing pins ..	..	as required

Cut and fix lengths of  $1\text{in} \times \frac{3}{8}\text{in}$  strip to the top, bottom, sides and backs to form recesses as shown in Fig. 1. In dimensioning the strips remember that the whole cabinet has to be fitted together, and due allowance must be made for any extra thickness of hardboard introduced. For example, the struts already fitted to the backs (A in Fig. 1) will need to be shortened to allow for the hardboard fitted on the top and bottom cabinet walls. The writer found no difficulty in working with the cabinet assembled and the backs removed. If, however, an unassembled cabinet is being converted, it will probably be easier to do all the constructional work before assembly. Butt joints are adequate for the corners, and Casco glue and panel pins make solid and sandtight joints. The cardboard corner pieces make additionally sure that no sand leaks occur at the corners. These are made from cigarette packets and are secured with Croid (Casco is unsuitable as it requires considerable pressure to obtain good adhesion). The flaps marked "B" in Fig. 2 should be at the top of the cavity to engage with the hardboard top when it is fitted.

When the glue on the strips and corner pieces has hardened, fill the cavities with dry sand packed fairly tightly. Cover the tops of the cavities with hardboard cut to size and secured with Casco glue and panel pins. Remember to put Croid on the flaps B of Fig. 2 before fitting the hardboard. This ensures a good sandtight joint on the finished job.

Fit the  $\frac{3}{4}\text{in}$  carpet felt to the two backs, covering to within  $1\text{in}$  of the edges. This is most easily done using Croid and drawing pins.

When all the joints are dry, assemble the cabinet—bearing in mind that all panels are now considerably heavier than the designer originally intended, and therefore additional care is necessary to make sure that no damage is done to the cabinet as a whole. The same care should be exercised when the cabinet is moved to its working position, which should, if possible, be such that it does not have to be changed very often for cleaning or other domestic reasons.



E448

# INTERCOM

by R. H. SMART

# SET

### Introduction

THIS UNIT WAS PRIMARILY DESIGNED AS AN amplifying intercom between the author's workshop and the house. It was thought that an amplifier used exclusively for this purpose would be unnecessarily wasteful, and so a number of features were included to enable the unit to be used for general experimental work without detracting in any way from its original purpose.

### Facilities Offered

- (1) Intercom between two stations with complete secrecy at both if required.
- (2) High and low gain amplifier inputs.
- (3) Mixing of inputs.
- (4) "Slave" may be disconnected when amplifier is used for experimental work if desired.
- (5) Should "slave" be disconnected under item 4 an audible or visual alarm is incorporated should "slave" wish to speak.

### Main Amplifier

The circuit is shown in Fig. 1, and it will be seen that it is a conventional three-stage design with the following modifications. Provision is made to switch the intercom input transformer  $T_3$  out of circuit and replace it with a socket and volume control  $VR_1$  to provide a high gain input. A low gain input is provided via  $VR_3$  to the grid of  $V_2$ . This may be mixed with the output from  $V_1$ .  $VR_2$  should be adjusted for normal intercom working, but as it is likely to be altered during testing, etc., it would be just as well to mark the amplifier panel and  $VR_2$  knob to facilitate quick return to intercom.

It will be noted that the coupling between  $V_1$  and  $V_2$ , condenser  $C_2$ , is of an unusually low value. This is to decrease the bass response on intercom, and it may be lowered further if desired. It does, however, affect the bass response of "Input 1."

The power supplies incorporate full-wave rectification and are well smoothed to avoid hum troubles. Modifications may be made to suit components available, but it is *not* recommended that the mains be connected to

chassis, as this could result in the full mains voltage appearing on the remote wiring to the "slave."

### Amplifier Switching

This function is performed by  $S_2$ . It has three positions, viz.:

- (1) Intercom
- (2) Amplifier only, "slave" disconnected
- (3) Amplifier only, "slave" connected in parallel with main loudspeaker

When switched to (2) or (3) and the "slave" wishes to speak, operation of relay CO (Fig. 2) completes a circuit via  $S_{2c}$  for the audible or visual alarm. Switching to (1) immediately restores intercom facilities.

### Intercom Switching

Fig. 2 shows a comprehensive system requiring a three-wire connection between the stations.  $K_1$  and  $K_2$  are Post Office type key switches, it being an advantage if  $K_1$  is of the non-locking type, i.e. to return to normal when finger pressure is removed. CO is a relay of the well-known 3000 type. The relay and key switches are obtainable on the surplus market.

With  $K_1$  and  $K_2$  "up," both stations are connected to the amplifier output. If  $K_2$  is depressed, the negative (chassis) line is extended via  $K_1$  to operate relay CO. CO<sub>1</sub> then connects the "slave" to "input" and "slave" may speak. Operation of  $K_1$  disconnects CO, returning the "slave" to output and connects the master to input. Note that the master may speak whether or not  $K_2$  is depressed. Should  $K_2$  be left in the "on" position, the "slave calling" alarm can be disconnected at  $S_3$ .

The positive potential to operate the relay and buzzer (if used) may be obtained from the HT line via suitable dropping resistors. The value of these resistors will vary with the resistances of relay and buzzer used. Alternatively, a battery may be used and an extra pole added to  $S_1$  (Fig. 1) to switch it out of circuit when the unit is turned off.

$3\frac{1}{2}$ in or 5in loudspeakers perform well as microphones and can be used to good

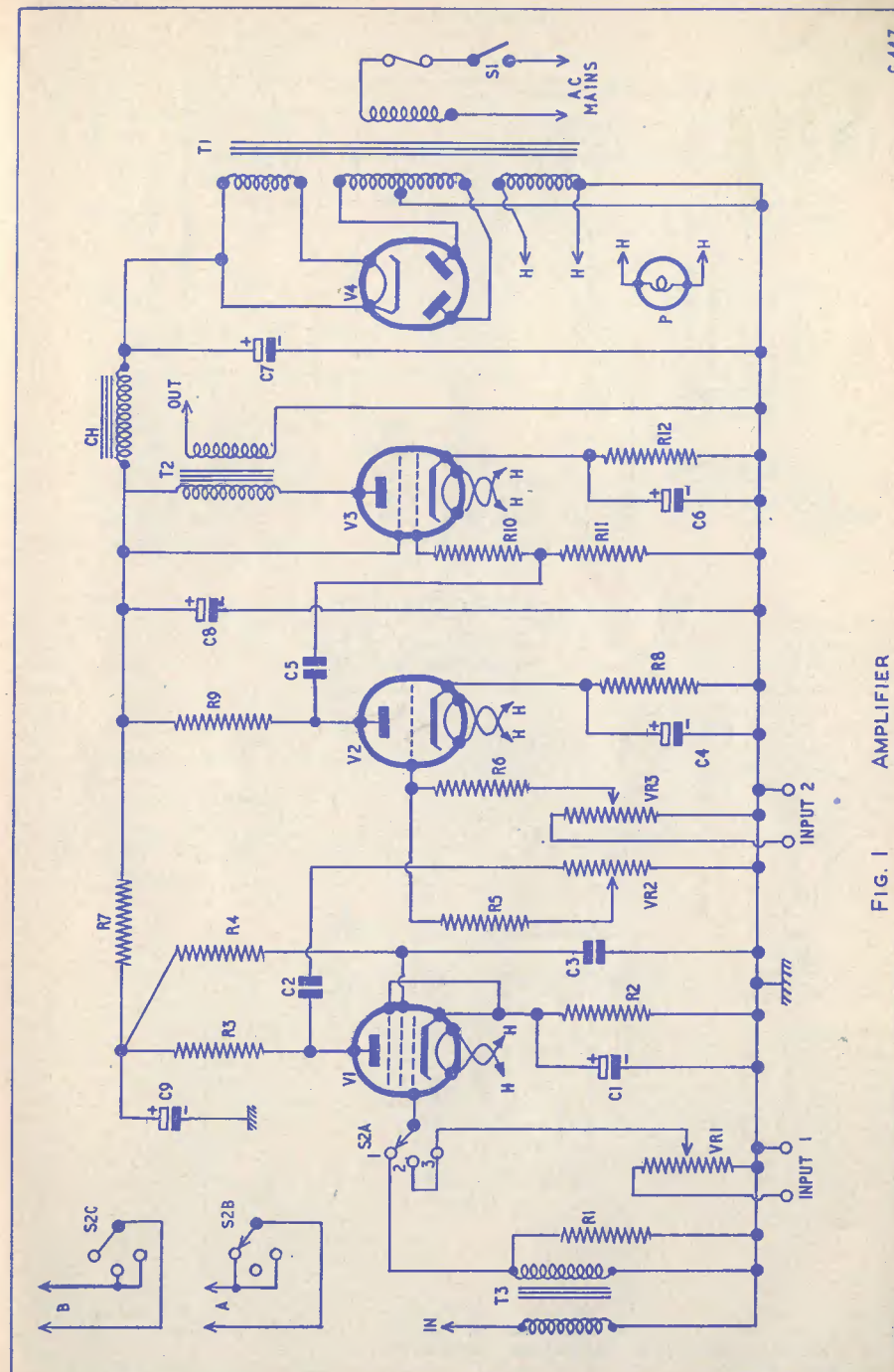


FIG. 1 AMPLIFIER

G 447



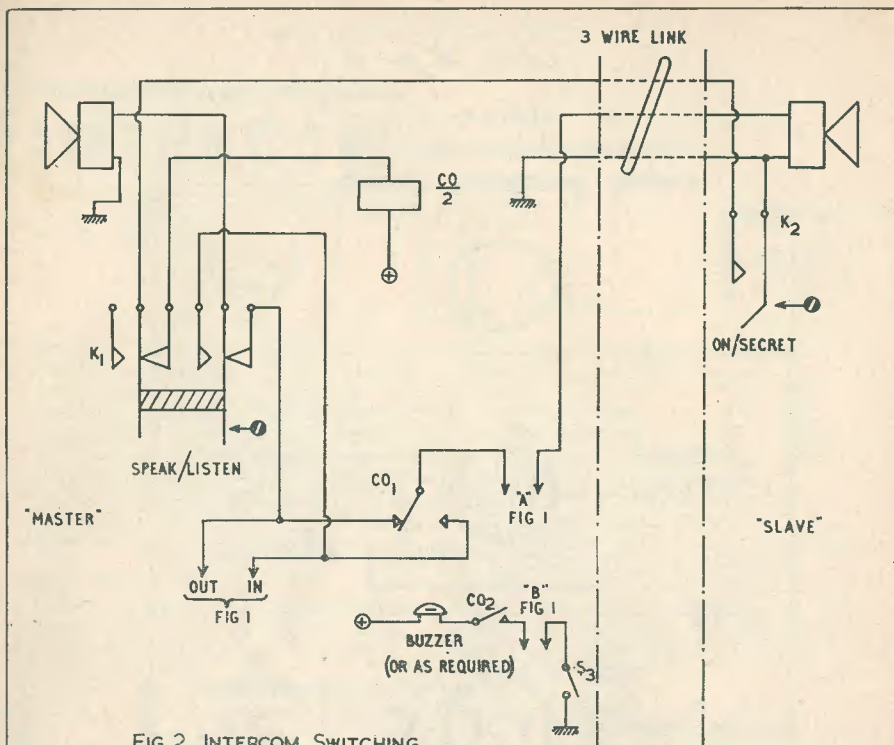


FIG. 2 INTERCOM SWITCHING

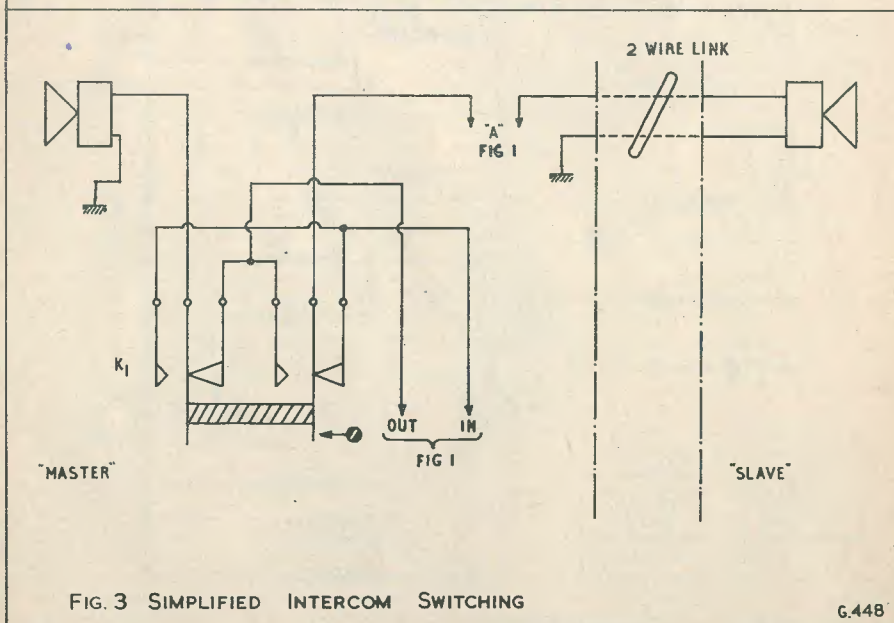


FIG. 3 SIMPLIFIED INTERCOM SWITCHING

G.448

### List of Components

C <sub>1</sub>	25 $\mu$ F 25V electrolytic	R <sub>1</sub>	100k $\Omega$
C <sub>2</sub>	0.001 $\mu$ F 350V paper	R <sub>2</sub>	2.2k $\Omega$
C <sub>3</sub>	0.1 $\mu$ F 350V paper	R <sub>3</sub>	470k $\Omega$
C <sub>4</sub>	25 $\mu$ F 25V electrolytic	R <sub>4</sub>	1M $\Omega$
C <sub>5</sub>	0.05 $\mu$ F 350V paper	R <sub>5</sub>	470k $\Omega$
C <sub>6</sub>	25 $\mu$ F 25V electrolytic	R <sub>6</sub>	470k $\Omega$
C <sub>7</sub>	16 $\mu$ F 450V electrolytic	R <sub>7</sub>	10k $\Omega$
C <sub>8</sub>	32 $\mu$ F 450V electrolytic	R <sub>8</sub>	1k $\Omega$
C <sub>9</sub>	8 $\mu$ F 450V electrolytic	R <sub>9</sub>	47k $\Omega$
V <sub>1</sub>	6J7, etc., plus base	R <sub>10</sub>	4.7k $\Omega$
V <sub>2</sub>	6J5, etc., plus base	R <sub>11</sub>	470k $\Omega$
V <sub>3</sub>	6V6, etc., plus base	R <sub>12</sub>	240 $\Omega$ w/w $\pm 10\%$ (for 6V6 only)
V <sub>4</sub>	5Z4, etc., plus base	VR <sub>1</sub>	1M $\Omega$ pot
T <sub>1</sub>	Output: 250-0-250V, 60mA; 6.3V, 1.5A; 5V, 2A.	VR <sub>2</sub>	1M $\Omega$ pot
T <sub>2</sub>	Output transformer to suit o/p valve and loudspeakers	VR <sub>3</sub>	500k $\Omega$ pot
T <sub>3</sub>	Microphone type input transformer	CO	Relay P.O. "3000" type, 1 make, 1 changeover contacts
S <sub>1</sub>	250V 1A toggle	K <sub>1</sub>	Key type, 2 changeover contacts "non-locking"
S <sub>2</sub>	3-pole 3-way Yaxley type	K <sub>5</sub>	Key type, 1 make contact
S <sub>3</sub>	(if required) on/off toggle		Two loudspeakers, 3 $\frac{1}{2}$ in or 5in P.M. (see text)
P	6.3V Pilot lamp		Smoothing choke (CH) 10-20H, 60mA
	Buzzer or Indicator as preferred		Chassis, Sockets, Case and sundries as required.

advantage in the unit. For general work, however, a larger unit is generally required, and the author has used a 6 $\frac{1}{2}$ in energised speaker successfully in the past with the amplifier. At the present time a 9in speaker is in use in the workshop in conjunction with a 3 $\frac{1}{2}$ in at the house. Naturally, one has to speak closer into a larger speaker, but at the controlling end this is no disadvantage.

Figure 3 shows a much simplified system of switching when secrecy at the "slave" is not required, and no calling alarm is incorporated.

### General

As stated previously, the amplifier is of the conventional type, so existing amplifiers that may be in use or available should be easily modified. No constructional details are given, as the unit may quite easily be built from the junk box, and layouts could vary considerably with different components and valves to those specified. It is recommended, however, that the input transformer T<sub>3</sub> be placed as far as possible from the mains transformer T<sub>1</sub>, and that all wiring associated with the grids of V<sub>1</sub> and V<sub>2</sub> be screened.

### LITERATURE RECEIVED

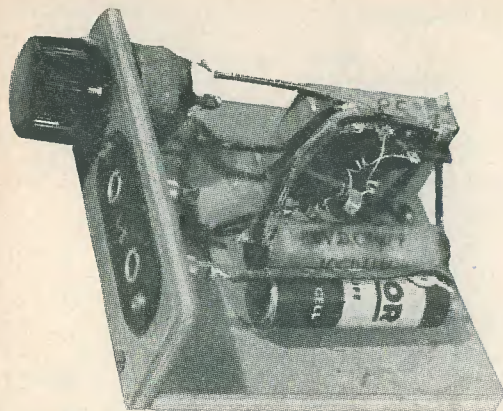
From Clyne Radio Ltd., 18 Tottenham Court Road, London, W.1, we have received the new *Comprehensive Catalogue 1957* of over 100 pages packed with radio and television components, kits, cabinets and all manner of other items of interest to the home constructor. One of the most comprehensive that we have seen, it is available from the above address, price 2s. post free. A monthly Newsletter—well worth receiving, is also available.

Standard Telephones and Cables Ltd., Footscray, Sidcup, Kent, have now produced and released the latest in their manual series, the *Brimar Radio Valve and Teletube Manual No. 7*. Complete details of all the Brimar range of valves, t.v. tubes, transistors, Brimistors, metal rectifiers, etc., together with base connections, data, and characteristic curves are included. In addition to the foregoing, other items include contact-cooled rectifiers, germanium diodes, abacs, formulae and a complete section of circuits of amplifiers, receivers, f.m. tuner unit,

radio tuner unit and various transistor circuits. The Manual is available from radio dealers, etc., price 6s.

The Wireless Institute of Australia have forwarded the latest edition of the *Australian Radio Amateur Call Book* (June 1957). The VK call signs listed are complete as at 15th May, 1957, and stations in Antarctica are listed for the first time under the new VKO prefix, VK1 now being allotted to Australian Capital Territory. Of 136 pages, with an attractive art board cover, it costs 5s., postage extra. The address is The Wireless Institute of Australia, C.O.R. House, 191 Queen Street, Melbourne, C.1, Victoria.

**Correction.** In the circuit of the Sensitive Signal Tracer, page 119 of the September issue, the electrolytic condensers C<sub>10</sub>, C<sub>13</sub>, C<sub>14</sub>, C<sub>15</sub> and C<sub>16</sub> were inadvertently shown as being connected in reverse, i.e. positive connections to chassis. These connections should, of course, be reversed.



# TRANSISTOR MORSE OSCILLATOR

by F. G. RAYER

WHEN PRACTISING MORSE, IT IS SOON found that the note from a buzzer is not very satisfactory, as it does not resemble the tone heard from Morse transmitters. A valve oscillator is frequently employed to overcome this, the signal being heard in phones, or listened to with a speaker. The usual type of simple valve oscillator is shown in Fig. 1, and it is vastly superior to the buzzer.

Though such an oscillator had been used on and off for many years, it was felt that a transistor circuit would be preferable, primarily because of the considerable economy in current consumption. No h.t. would be necessary, and even a single small dry cell should have a very long life.

With this in view, it was found that the circuit in Fig. 2 was satisfactory. Multi-vibrator circuits using two transistors were well known, but it was felt that a worthwhile saving would arise from having one transistor only, a transformer being used exactly as in Fig. 1. The circuit in Fig. 2 was, therefore, used. It is a ready oscillator, and gives ample volume for two sets of phones with a 1½V battery. The current drain is only around 1mA.

The 100kΩ potentiometer was provided to vary the audio tone, as this was felt desirable. As resistance is reduced, the tone rises until the transistor goes out of oscillation. The lowest audio frequency will depend upon transformer, transistor, and room temperature. The characteristics of the phones also vary it somewhat.

### Transformer

This item requires special mention, because a component suitable for the valve circuit may not function well with a transistor. The latter is a current-operated device, whereas a valve is voltage-operated. The transformer thus needs to have windings of fairly low

resistance. It is also helpful if its inductance is a little low, so that it would not be a very good component by a.f. coupling standards.

When the circuit has been connected up, the results to expect will soon become apparent. If no oscillation arises, it may be necessary to reverse connections to one winding. The effect of exchanging the circuit positions of primary and secondary can also be tried.

If the transformer will not give satisfactory results, another component of different type must be tried. If several old or ex-service transformers are to hand, one is likely to suffice. The ratio is not important, but may best be around 1 : 5 to 1 : 15.

A component with low inductance, which gives a very high-pitched note, may have a condenser of about 0.05μF upwards wired in parallel with the primary.

### Constructional Points

The wiring plan is shown in Fig. 3; dimensions are of no importance. Of the various possible methods, that of wiring phones and key in series with the battery has been selected, as this avoids the need for any on/off switch, and means that the oscillator is always out of action when the key is open, or phones removed. The components are so few that in some cases it may be possible to assemble the oscillator on an old Morse key, complete, to form a single unit.

When wiring up, the polarity of the battery must on no account be incorrect, the inner carbon rod being positive. The cell is soldered directly into position, as its normal life is several months.

The transistor must on no account be heated, or permanent damage is likely. It is best, for this reason, to leave its wire ends full length. The soldered joints should be made with reasonable speed, the transistor lead being held by flat-nosed pliers to conduct heat away.

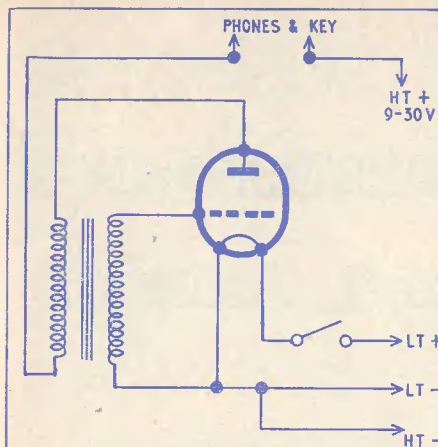


FIG. 1 THE ORIGINAL VALVE CIRCUIT

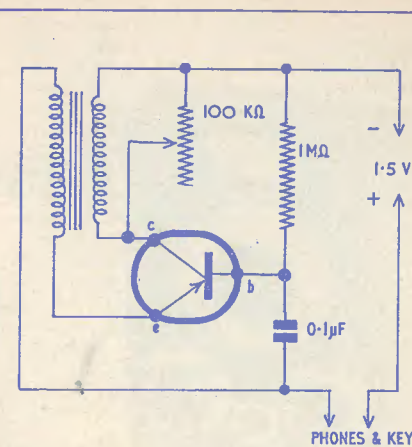


FIG. 2 TRANSISTOR OSCILLATOR

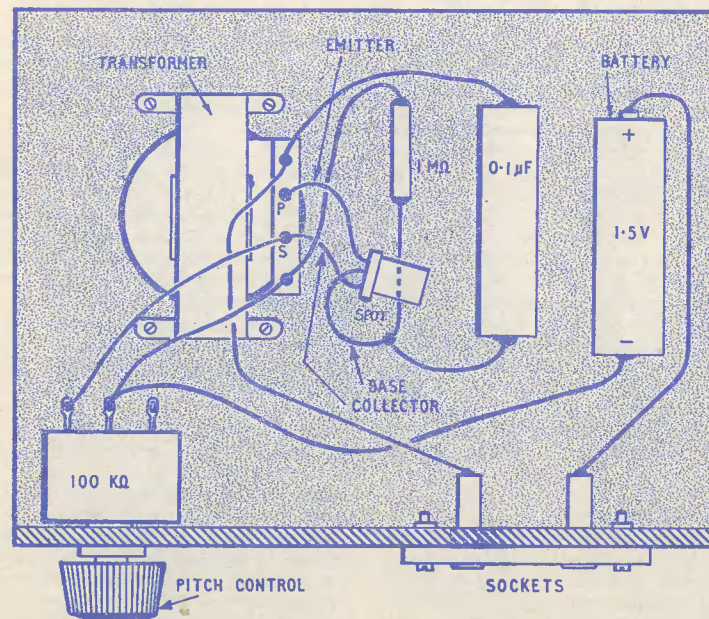
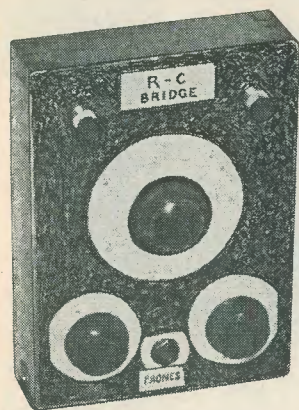


FIG. 3 WIRING PLAN

G 449



# TRANSISTORISED

## R.-C. BRIDGE

by S. A. MONEY

SOME FORM OF RESISTANCE-CAPACITANCE bridge is a valuable asset to the experimenter's workshop, since with its aid the value of any capacitor or resistor can be measured quite accurately. In the instrument to be described an accuracy of  $\pm 5\%$  or better may be obtained, depending upon the accuracy of the components used.

A disadvantage of many R-C bridges is that they require the use of a mains supply to operate them. By using a transistor in the circuit it is possible to make the bridge work from a  $1\frac{1}{2}$  volt torch battery, thus making the instrument both portable and economical.

The instrument comprises a bridge network, in which the unknown component is measured, and an audio frequency oscillator which provides an a.c. supply for the bridge network. Since only a small amount of power is required from the audio oscillator, a transistor may be used.

### The Audio Oscillator

One of the small p-n-p type junction transistors which are now obtainable is used for the oscillator. It is connected in the common emitter arrangement, with transformer feedback from the collector to the base. As with a valve oscillator, there is a phase reversal in the transistor and the transformer is connected to give a further phase reversal, so that a positive feedback is obtained.

The transformer should have a ratio of about three to one, with the larger winding in

the collector circuit. Some valve type transformers are unsuitable because they have windings with high d.c. resistances which cause large voltage drops and may prevent oscillation.

A suitable transformer may easily be wound on the core of an old audio transformer using, say, 200 turns of 30 s.w.g. wire for the primary and 60 turns for the secondary. Alternatively, a suitable transformer specially made for transistor work may be obtained. A small heater isolating transformer was also found to be suitable for this circuit.

The windings must be connected up the right way round for oscillation. If the transformer is not marked and the circuit does not oscillate, then one of the windings should be reversed.

Any of the small junction transistors now available will work in this circuit, although it may be necessary to alter the circuit constants to suit the differing characteristics of various makes of transistor. With some transistors it is found that a rough note is produced. This appears to be due to excessive feedback and may be cured by damping the primary of the transformer with a shunt resistor. The value required will vary from about  $2.2k\Omega$  to  $10k\Omega$ , depending on the transistor used. For convenience a variable resistance is used here, the value being adjusted to give a clean note with the transistor in use.

The primary of the transformer is tuned by a shunt capacitor to give an audio note of

about 1,000 c/s. The actual value of this capacitor will depend upon the inductance of the transformer used. A value of from 1,000pF to 5,000pF will usually be required.

In the base circuit, the transformer secondary is connected in series with a bias resistor to the negative side of the supply. This resistor provides a current bias of about 75 microamps for the base circuit and is decoupled by a capacitor. The use of this bias helps to produce a clean note.

### The Bridge Network

In this instrument the bridge network has been arranged to give six ranges with a linear scale on both resistance and capacitance measurement. This makes the scale easy to draw and allows good accuracy to be obtained.

For measurement of resistances a Wheatstone bridge is used with a pair of headphones as the detector. In the measurement of capacitance a DeSauty type bridge is used. This is a Wheatstone bridge in which two of the resistors are replaced by capacitors.

For the Wheatstone bridge shown in Fig. 1, the value of  $R_1$  when the bridge is balanced is

$$R_1 = R_4 \frac{R_2}{R_3}$$

In the case of the DeSauty bridge shown in Fig. 2, we get

$$C_4 = C_1 \frac{R_2}{R_3}$$

It will be noted that the ratio  $\frac{R_2}{R_3}$  is common to

both circuits and, in fact, the resistors  $R_2$  and  $R_3$  are known as the ratio arms of the bridge. It will be convenient to make  $R_1$  and  $C_4$  the unknown components, so that  $R_4$  and  $C_1$  become the standards against which the unknowns are compared. By making  $R_2$  variable, and calibrating it, the ratio of  $R_2$  to  $R_3$  may be varied to balance the bridge, and the value of the unknown component read off from the scale fitted to  $R_2$ . For both resistance and capacitance this scale will be linear since the unknown is directly proportional to  $R_2$ .

The usual practice for changing the range of the bridge is to change the value of the standard component  $R_4$  or  $C_1$ . For six ranges this means that twelve high tolerance components are needed, six of them being capacitors. An alternative method is to switch the value of  $R_3$  so that the ratio of  $R_2$  to  $R_3$  is changed. With this arrangement only two standard components are needed, one for resistance and one for capacitance.

If  $R_2$  is a  $10k\Omega$  potentiometer, then the scale fitted to it would read from 0 to  $10k\Omega$  and multiples of this. This arrangement

places the  $1k\Omega$ ,  $10k\Omega$ ,  $100k\Omega$  values at the ends of the scale, so that it may be difficult to obtain accurate readings for these values. To overcome this, the scale is made to read from  $1k\Omega$  to  $11k\Omega$ , thus bringing the 10 values in at the upper, and more accurate, end of the scale. This result is easily obtained by adding a  $1k\Omega$  fixed resistor in series with the  $10k\Omega$  potentiometer, thus making the range of values of  $R_2$   $1k\Omega$  to  $11k\Omega$ .

When switching from resistance to capacitance measurement, it is necessary to transpose the standard and unknown components in order to make the capacitance scale linear. Thus  $C_4$  becomes the unknown capacitor. The switch used for this is a three-way type, the third position being used to switch off the battery supply to the oscillator when the instrument is not in use.

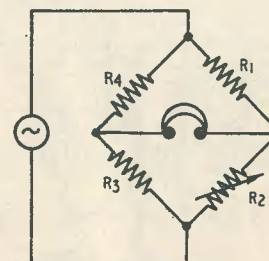


Fig. 1  
The Wheatstone Bridge

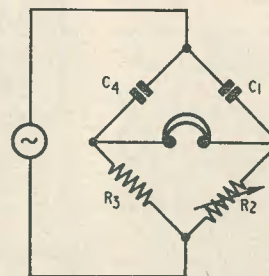


Fig. 2  
The DeSauty Bridge

### Construction

The complete circuit diagram of the instrument is shown in Fig. 3. No specific details will be given of the construction of the unit, since these will vary according to the components used and the requirements of the constructor himself. It is an advantage to mount all of the components upon the front

panel since the completed unit can then be simply dropped into its case and fixed with screws. When a battery has to be replaced, it will then be a simple matter to make the change.

The size of the instrument is limited by the size of scale required in order to achieve reasonable accuracy and ease of reading. A panel size of about  $7\frac{1}{2}$ in  $\times$   $5\frac{1}{2}$ in was found to be about the minimum usable.

The battery is a  $1\frac{1}{2}$  volt torch cell, type U11, or similar, and this is clamped to the panel by means of a capacitor clip, thus making the panel the negative side of the supply. The positive connection to the battery is then soldered to the top cap of the cell. Since the current drain of the transistor oscillator is only some 3 to 5mA, the cell should last for at least its shelf life, so that replacements will be very infrequent.

The transistor must be soldered into the circuit with some care by gripping the leads, with a pair of pliers, as they are soldered. This prevents damage to the transistor due to heat from the soldering iron. If a small iron is used and the joint made quickly, this precaution may be unnecessary. The collector connection is usually indicated by a coloured dot on the body, and the other connections should be obtained from the data sheet for the transistor used.

Components used for the bridge network must be of at least 5% tolerance, and if desired closer tolerance components may be used. The potentiometer must be of the linear type and about  $1\frac{1}{2}$ in or  $1\frac{1}{4}$ in diameter. Smaller diameter components have a shorter track and will not be as accurate as the larger unit. No great advantage is obtained by using a miniature component here, since the

size of the unit is governed by the scale dimensions. For the oscillator circuit ordinary 20% components may be used.

For convenience the phones should be connected to the circuit through a jack plug and socket. The test leads for the unknown component may be brought out to terminals, or to flying leads fitted with crocodile clips.

#### Calibration

When the instrument has been wired up, a scale must be drawn so that the values of the components being measured can be read off directly from the scale. The most accurate method of making the scale would be to calibrate each range separately, using an accurately calibrated variable resistance and an accurate capacitor box. Since such apparatus is unlikely to be available to the amateur constructor, a simpler method must be used. For this method the track of the potentiometer is assumed to be perfectly linear and the other components of the bridge accurate.

Most potentiometers have an angle of rotation of  $300^\circ$ , although there are some types which have an angle of rotation of only  $270^\circ$ . This angle can easily be found by fitting a knob to the potentiometer and measuring the angle of rotation with a protractor.

Having found the required scale angle, a circular scale is drawn having a diameter of about  $2\frac{1}{2}$ in. The sector corresponding to the rotation angle of the potentiometer is then marked off and this sector is divided up into 100 divisions by using a protractor. Every tenth division is marked with a longer stroke and numbered from 1 to 11. The scale should then be marked in with indian ink, cut out and glued into position on the panel. Readings obtained on this scale will then be multiplied by a constant factor, according to the range in use, to give the value of the unknown resistor or capacitor. This method of calibration will give an accuracy of about  $\pm 5\%$ .

#### Operation of the Bridge

To measure the value of an unknown resistance or capacitance, connect the component across the test terminals. Select resistance or capacitance range and set the range selector to a suitable range. The potentiometer is then rotated until the volume of the note in the phones drops to a minimum. The value of the unknown component may then be read directly from the scale. It is not usually possible to obtain zero signal in the phones because of stray capacitance and leakage resistance. The operation of the bridge should be checked by measuring a few known resistors and capacitors.

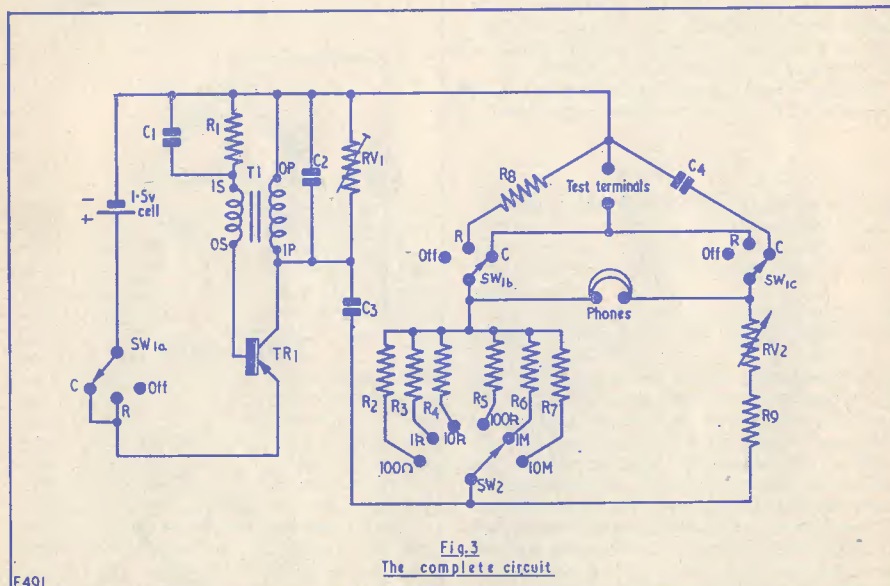


Fig. 3  
The complete circuit

#### COMPONENT LIST

##### Resistors

- R<sub>1</sub> 22kΩ
- R<sub>2</sub> 1MΩ 5%
- R<sub>3</sub> 100kΩ 5%
- R<sub>4</sub> 10kΩ 5%
- R<sub>5</sub> 1kΩ 5%
- R<sub>6</sub> 100Ω 5%
- R<sub>7</sub> 10Ω 5%
- R<sub>8</sub> 10kΩ 5%
- R<sub>9</sub> 1kΩ 5%
- RV<sub>1</sub> 10kΩ preset
- RV<sub>2</sub> 10kΩ variable linear

##### Condensers

- C<sub>1</sub> 0.05μF
- C<sub>2</sub> see text
- C<sub>3</sub> 0.002μF
- C<sub>4</sub> two 5,000pF 5% silver mica
- TR<sub>1</sub> Red Spot, OC71, GT2, GET3 or similar
- T<sub>1</sub> 3 : 1 ratio transformer
- SW<sub>1</sub> 3-pole 3-way rotary
- SW<sub>2</sub> 1-pole 6-way rotary
- Phones high impedance
- Battery 1.5V cell

## BOOK REVIEW

**UNDERSTANDING HI-FI CIRCUITS.** By Norman H. Crowhurst. 224 pages, 180 diagrams. Published by Gernsback Library Inc., New York. Obtainable in England from The Modern Book Co. (Dept. RC), 19-23 Praed Street, London, W.2. Price 23s. 0d.

The author of this interesting book has resided in America for the past few years and has already become well established there as a writer on audio subjects in technical journals. He produced many articles in this country some time ago which were notable for their ingenious design charts, so he is well able to discourse on the aspects of hi-fi sound reproduction contained in this volume.

The text is almost wholly descriptive and conversational. Very few mathematics are used; one could almost say that a little arithmetic appears here and there just to emphasize an explanation or to give simple proof of a circuit function. On the other hand, much that could have been expressed mathematically has been made comprehensible by means of several graphs and charts. This, and the author's lucid style, makes the book absorbing to read and refreshingly easy to understand.

The ten chapters forming the major part of the book are liberally illustrated with basic circuit diagrams, each of which is discussed in detail. Component values are given only where it is necessary to discuss specific values, and their effects on a particular circuit principle. As a result, it is hardly possible to formulate a complete amplifier circuit design simply by stringing together individual circuits that catch the eye in various chapters.

It may well be that they have been denuded of component values deliberately, for the author remarks quite early in the book that many "original" designs seem to have been born by such grafting methods; not without some truth, one imagines.

It is not possible in this short review to do justice to the wealth of information contained in the volume. Even a mention of all the principles, circuits and functions could take up much space. The following few aspects selected at random may serve to show how widely the subject of hi-fi has been covered: triodes, pentodes and tetrodes in ordinary, ultra-linear and cathode-follower output stages, the use of feedback; phase correction, frequency response, output impedance; transformers and chokes in driver and inverter stages, paraphase and cross-coupled inverters; thermal noise, hum, and microphony; matching of input and output stages; equalization for disc and tape recordings, passive and feedback type equalizers, triode, pentode and two-triode equalization stages; single and multiple speaker units, cross-over networks, channel separators; stepped and continuously variable loudness and volume controls; feedback, peaking, variable slope, and step-by-step tone controls.

Considering the amount of useful material contained in it, the book appears to be smaller than one would expect, but the reader should not be deceived on this account. The book is really good value for its price, particularly for those who would learn from an instructive writer many things about hi-fi and audio that would be difficult to find written elsewhere.

W. E. THOMPSON

## A CONSTRUCTOR VISITS THE . . .

# 1957 NATIONAL RADIO AND TELEVISION SHOW

THE WRITER HAS ALWAYS HELD A FOND BELIEF THAT it is possible to gain entry into almost any London exhibition by the simple process of flashing a business card at the entrance and stating briskly: "Press!" If one looks scruffy enough the attendant will then let one through. This scheme has worked excellently in the past, especially at the London Audio Fair. (Would "Free Grid" of *Wireless World* please note?) Just for fun the writer tried it out this year at the Earl's Court Exhibition but the attempt was unsuccessful, and your somewhat embarrassed reporter had to rummage for his correct Press Ticket before a disdainful thumb indicated that he could pass through the turnstiles.

However, despite this rather discouraging start, the writer enjoyed his visit to the Radio Show as much as he has always done in the past. There was less "gadgets" this year than has appeared at previous exhibitions—incidentally, the major radio and television manufacturers tending to present their wares in almost an overly dignified and staid manner. On hot days the atmosphere in Earl's Court tends sometimes towards a certain stuffiness, and it is a pity if this is added to by a stuffiness in the stand layouts.

Part of the restrained tone of this year's show may have been due to the fact that no major technical developments have recently occurred or are impending in the domestic radio and television scene. Because of this, manufacturers have had the time to consolidate their present position, and have been able to concentrate more on cabinet design and presentation.

Television  
The preoccupation with cabinet styling was very apparent on the stands devoted to television. One technical development in conventional t.v. receivers consisted of the introduction in some models of 90 degree tubes but, even here, the results given are more apparent in the form of shallower cabinets than in any improved picture response. There is a strong tendency towards making the tube face occupy a large area of the front of the cabinet. The "push-through" type of tube mounting, wherein the whole of the front of the tube is visible instead of being partly masked, is becoming more and more popular.

Possibly the biggest change in television production was the introduction by almost every manufacturer of transportable receivers. Most of the models shown employed 14in tubes and were housed in cabinets of the same style as are used by portable radios, viz., cloth-covered plywood, or moulded plastic.

The chassis inside such housings employ conventional circuitry, of course, and it is possible that, since the cabinets conform to the design idiom to which portable radio has accustomed the public taste, they not only become acceptable in the home but also incur a noticeable saving in cost. A particularly interesting transportable model was the Ferguson 14in receiver

(type 45), insofar that it had a very comprehensive inbuilt telescopic aerial system, this being capable of a considerable range of adjustment. The two telescopic aerial rods employed with this receiver could be drawn out of the cabinet and set to any length and at any angle to each other. Thus, it was possible to extend both rods to form a pair of "rabbit's ears" or extend one vertically to act as a quarter-wave aerial, the other being left in the cabinet or laid horizontally outside to act as a partial reflector. Since the aerial rods may be moved in any direction it is not necessary to orientate the receiver itself to receive any particular signal.

A large number of firms exhibited televisions which were also capable of reception of v.h.f. signals in Band II. Reception of v.h.f. with these sets is obtained by rotation of the tuner to the desired f.m. channel, this automatically changing the detector circuit in the sound i.f. strip from a.m. to f.m. and putting the purely television circuits out of action. F.M. reception is then achieved via the tuner, the sound i.f. strip, and the a.f. stages of the set. Technically, the introduction of f.m. represents an interesting departure, because it creates quite a number of engineering problems. Probably the most difficult of these are involved in the switching circuits themselves, as it is not only necessary to alter the method of working at the sound strip detector but also to change the power supply circuits. In many f.m./t.v. receivers the power supply problems are solved by switching off the heaters of the tube and the valves not required when the tuner is set to f.m.

An interesting device exhibited by G.E.C. is worthy of mention at this stage. This consisted of a small 6in cathode ray tube (type 1668 VMH) which could be fitted into any television receiver in place of its regular tube in order to facilitate servicing and manufacturing processes. In most modern televisions the deflector coils are mounted to the chassis metal-work, with the result that the 6in tube may remain in position merely by inserting it into the deflection yoke and fitting the base socket and e.h.t. clip. The tube gives a normal and, of course, smaller picture under these conditions, and obviates the awkward problems involved when chassis with large tubes have to be handled. The writer understands that the 6in tube works with the same e.h.t. voltage as is employed by the much larger one it temporarily replaces.

### Sound

So far as sound reproduction was concerned, the major change evident at the Show was the greatly increased number of record players on display. There is a very thriving market for this type of instrument just now, and the range available extends from portable models priced below £15 to hi-fi units (at £40 up), having two or more loudspeakers and carefully designed

cabinets/enclosures. Pyc exhibited a transistorised record player.

Transistors are slowly entering the portable radio market, but the high prices of transistorised receivers preclude large sales as yet. There is, nevertheless, considerable interest in transistor equipment when advantage is taken of their small size, and a popular exhibit was the Perdio PR-1 transistor receiver, whose outside dimensions are 3½in by 5½in by 1in. The PR-1 covers 185 to 565 metres and is powered by six small torch-batteries. A do-it-yourself transistor receiver built into a 20 cigarette packet was to be seen on the Siemens Edison Swan stand.

Readers may remember the new Periphonic speaker system introduced by G.E.C. at this year's Audio Fair. These speakers were employed in a most impressive demonstration of stereophonic reproduction at Earl's Court. Other high fidelity equipment was much in evidence, and it would appear that prices are becoming more and more competitive. The trend towards producing "unit" hi-fi systems is very strong and, here again, much work has been put into providing attractively styled cabinets or housings for equipments which have undergone no dramatic technical changes. Careers

If the more technical details were soft-pedalled in the "domestic" part of the Show, the same statement could not be made for the exhibits on the stands in the Careers and Services area on the first floor. A particularly well designed and well presented exhibit was devoted to television fault finding. Inside a glass case a working television chassis was seen alongside a c.r.o. displaying the waveform at its video output stage. By means of press-buttons on the outside of the case it was possible to "select" typical faults, such as loss of sync, etc., whereupon these were at once exhibited by the receiver and the oscilloscope. A similar exhibit utilised a Murphy receiver switched to one of the programmes piped through Earl's Court. This receiver exhibited faults which were selected sequentially by an automatic control box.

The Radio Society of Great Britain laid emphasis on home-construction at their stand, items shown ranging from a complete transmitter to a simple one-valve receiver. An interesting exhibit here was a three-stage do-it-yourself short wave receiver for the beginner. The first unit to be built consisted of a single valve detector stage which, on its own, formed a complete receiver. R.F. and a.f. add-on units could then be added later as and when required. Also to be seen on the R.S.G.B. stand were two 10 metre walkie-talkies which gave evidence of considerable attention to mechanical as well as electrical detail.

An interesting device, also in the Careers area, consisted of a crystal-controlled clock which required only a small frequency control unit (some eight or nine inches cube), and whose cost should be low relative to its timekeeping accuracy. The crystal was a 100 kc/s unit, four successive binary stages dividing this frequency down to 50 c/s. The 50 c/s frequency was then amplified and applied, push-pull, to the motor windings of a synchronous clock. The clock itself was a standard Smith's model intended for operation from synchronous a.c. mains, the only modification carried out being that the motor had been rewound to accept the low voltage output of the crystal control unit. The binary stages and amplifier in the control unit were transistorised, the transistors employed being twelve Mullard OC71's and two Mullard OC72's.

Another item of transistorised equipment was a three-stage a.f. amplifier employed on one of the G.P.O. stands for the purpose of locating a particular "pair" in a multi-conductor telephone cable. The stand was made up as a replica of the familiar "hole in the road" scene wherein G.P.O. engineers may be seen sorting their way through large numbers of wires; and visitors were invited to try their skill at finding a particular pair themselves. The procedure involved consisted of first hooking a portable telephone on to any pair in the bunch being checked and of dialling a code number. This number connected the engineer to an oscillator at the exchange which put a continually repeated squeaking oscillation on the line. The engineer then dialled the number corresponding to the pair he wished to trace, whereupon the squeaking signal was

fed to that pair as well. The next job consisted of switching on the transistorised a.f. amplifier and, with the aid of a probe connected to it via screened cable, locating the desired pair. It was necessary only to hold the probe near the cable in order to pick up the squeaking tone, this becoming loudest when the probe was held on the pair being traced. The same transistor amplifier could be used to locate pairs even when they were completely screened inside lead sheathed cables. In this case a more sensitive probe was plugged into the amplifier and held against the lead sheathings of the cables being checked. The first probe, incidentally, was merely a test prod whose inner "hot" conductor was completely screened except for the tip.

### Gadgets

Both Standard Telephones and Cables, and Mullard, exhibited ingenious devices which fall into the category of "gadgets" and which helped to make the Show more interesting for the technically-minded visitor or, indeed, for the non-technical person who is merely prepared to stand and stare.

The S.T.C. exhibit consisted of a machine on which a game of electronic snakes and ladders could be played. "Shaking the dice" for each move was carried out by pressing a button, whereupon a system of relays and uniselectors selected a figure which was shown as a number of illuminated spots corresponding to the spots on a dice. The appropriate move on the "board" was then carried out, also by illuminated spots. Ascend up ladders and descent down snakes was handled automatically by the uniselector circuits.

The Mullard exhibit included quite a few gadgets, one of these consisting of what was called "The Gambler's Dice." With this device a dice was made to jump in the air at the sound of a hand-clap near a microphone. The impulse causing the dice to be thrown was provided by an electromagnet under its platform, this being energised momentarily by the hand-clap. It was possible for "sixes" to be thrown to order, these being controlled by a stand attendant carrying a transistorised pocket transmitter. By means of this transmitter the attendant could cause the electromagnet to be continually energised. The dice, incidentally, was a cube of Magnadur magnetised so that the poles occurred at the "one" and "six" faces.

A more ambitious Mullard display was provided by a number of electronic "beetles" whose movement on a glass platform could be controlled by means of lights placed above them. Each beetle consisted of a small framework on wheels driven by a motor which received its power from a 6 volt battery. Also supplied by this battery was a phototransistor circuit. The phototransistor was mounted at the top of a rotating neck coupled to the steering mechanism of the beetle. When the phototransistor became energised by a light source a clutch mechanism stopped further rotation, with the result that the beetle moved towards the light. By moving the angular relationship between the neck holding the phototransistor and the steering mechanism through 180 degrees the reverse effect could be obtained, the beetle this time moving away from the light source. A setting between these two extremes would cause the beetle to approach a light source with a sideways movement and then circle around it. In the Mullard exhibit a number of lamps were suspended above the platform on which the beetles moved, these being switched on or off individually at intervals.

### Test Gear Kits

Mention should be made in this report of the fact that the Cossor Instruments range of home-constructor test gear kits now includes a double-beam oscilloscope. Labgear have also entered this field and have kits available for an oscilloscope using printed circuits, a 1,000 ohms-per-volt multi-range testmeter and an a.f. power output meter.

A final point which is worthy of emphasis is that home-constructors wishing to meet fellow-devotees of the hobby could do so at the Mullard Home Constructor Centre, where examples of equipment built to Mullard design were to be seen and where questions were answered quickly and comprehensively. This latter fact was demonstrated very forcibly to the writer who spent quite a lot of time at this stand, and who heard some of the really difficult posers that were raised by visitors!

# SOUND ONLY

*A suggestion for those who depend on batteries*

by A. S. CARPENTER

A FAIRLY LARGE PERCENTAGE OF BRITAIN'S population still rely on dry (and sometimes wet) batteries to provide them with radio entertainment and, generally speaking, for them television is out of the question. There seems no reason, however, why they should not enjoy t.v. sound at any rate, and to assist them the circuit shown in Fig. 1 is offered merely as a suggestion.

The valves required are in cheap and plentiful supply, and the fact that they have 2V filaments presents no difficulty if they are connected series-fashion and fed from a 4.5-volt two-terminal battery via a limiting resistor.

A super-regenerative detector can be successfully employed as its poor selectivity characteristic is of no consequence, rather an advantage, as a fairly wide bandwidth is desirable. Nor does the quality of the output matter particularly, as few existing battery receivers give undistorted output.

An undesirable feature of this kind of detector is its ability to radiate, and on no account must an aerial be connected to its input direct. Radiation can, indeed, take place even when no aerial is connected, and adequate screening is a *must*.

A layout is suggested in Fig. 2—an under-chassis diagram. It will be noted that all components capable of radiating are effectively screened by the chassis box. V<sub>2</sub> is mounted horizontally, and as a further precaution a plate of 16 swg aluminium should be firmly bonded across the bottom of the chassis on completion, so that a closed-in construction results. Holes drilled in the chassis sides will ensure ventilation. A top-of-chassis diagram is not shown, as only V<sub>1</sub> and L<sub>1</sub> (shown dotted) will be visible. While V<sub>1</sub> does contribute to the gain, its main purpose is to act as a buffer between the aerial and V<sub>2</sub>, and it should not be omitted.

Coils may be wound on 3/8in Aladdin formers, iron dust cored, using 22 swg enamelled copper wire, the turns spaced from each other slightly. Six turns were found

suitable for Channel 5, but variations in wiring, etc., may possibly necessitate some deviation from this figure. Initially 7-8 turns should be wound on, and turns removed one at a time until the desired transmission is heard. The primary of L<sub>1</sub> consists of 2 turns of P.V.C. covered wire wound over the earthy end of the secondary winding. Alternatively, ready-made coils may be used and suitable types are obtainable from Osmor, Denco, Teletron, etc.

The chokes are easily made by winding a length of fine wire on a 1/4in mandrel. The length is readily calculated in the case of a quarter-wave choke by multiplying the quarter wavelength by ten and winding on this number of inches. For example, if 1 metre = 40 inches (actually 39.37in) and the working wavelength is 5 metres, then

$$\text{Length} = \frac{40}{4} \times 5 = 50 \text{ turns.}$$

## Component List

### Capacitors

C <sub>1</sub> , C <sub>2</sub> , C <sub>7</sub>	1,000pF
C <sub>3</sub>	10pF
C <sub>4</sub>	100pF
C <sub>5</sub>	500pF
C <sub>6</sub>	0.5-2μF

### Resistors

R <sub>1</sub> , R <sub>2</sub>	10kΩ
R <sub>3</sub>	270kΩ
R <sub>4</sub>	27kΩ
R <sub>5</sub>	100kΩ potentiometer
R <sub>6</sub>	10Ω

### Valves

V <sub>1</sub>	VP23	AM12
V <sub>2</sub>	VP23	

### Coils (see text)

### Miscellaneous

Valve bases: Mazda Octal (2). Chassis 6in × 5in × 2 1/2in plus base panel. Chokes (see text). Co-axial plugs and sockets (2) Belling-Lee. S<sub>1</sub>: on/off toggle switch. H.T. Battery 90V. L.T. Battery 4.5V. One control knob. Nuts, bolts, etc.

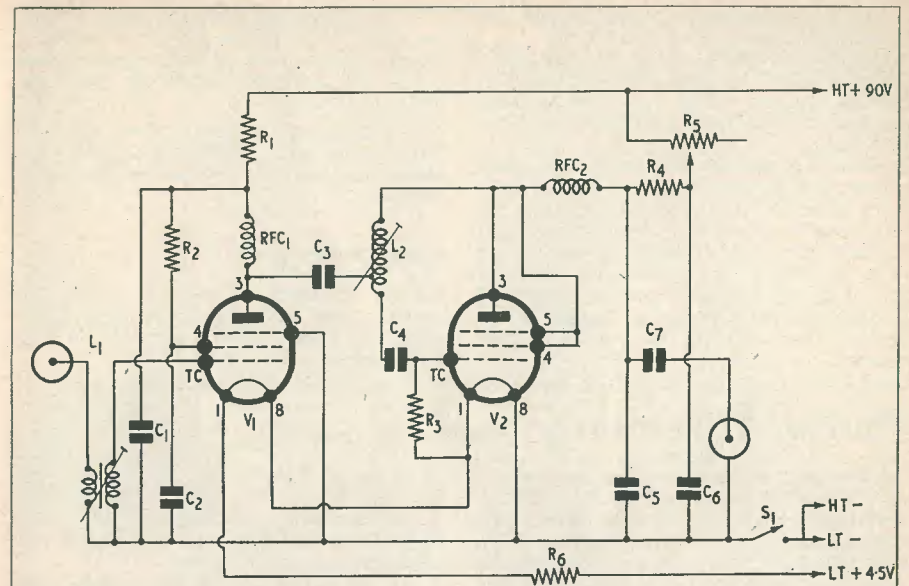


FIG. 1.

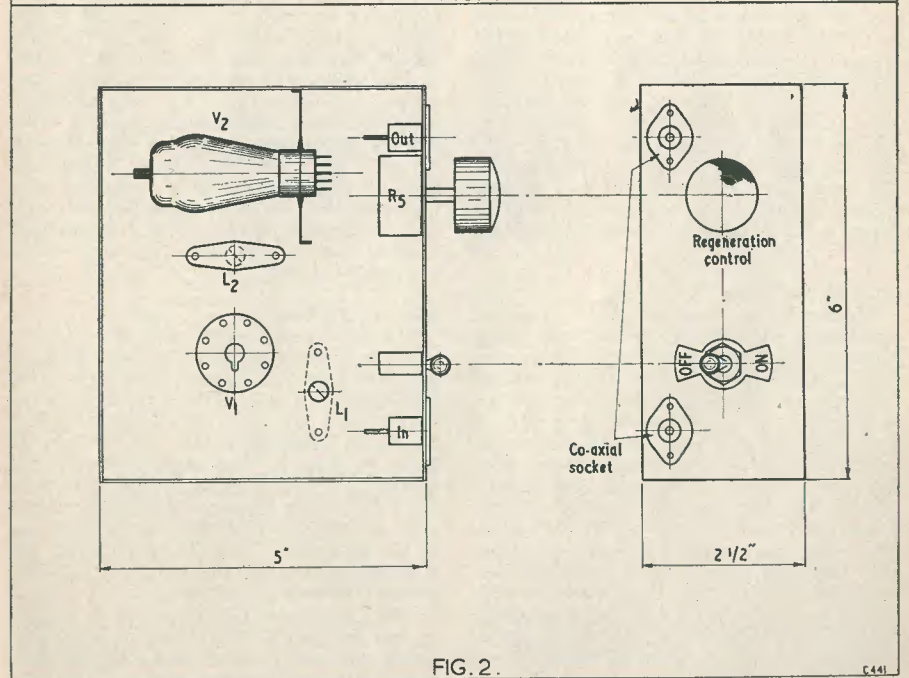


FIG. 2.

The approximation is near enough for practical purposes.

Output is available via a co-axial socket and may be fed into the gram sockets of an existing receiver. If no such sockets exist, connection can be made to the grid pin of the l.f. valve.

Initial adjustments are best made using phones, and in areas of good signal strength 7-8ft of aerial wire connected directly to the top cap of V<sub>1</sub> will suffice. A loud hiss should be heard when the receiver is switched on, the strength of which is adjustable by means of R<sub>5</sub>. This hiss disappears entirely when the transmission is received, the strength of the signal being sufficient to render it non-existent.

L<sub>2</sub> should receive attention first. Should no signal be heard at any core setting, a reduction in the number of turns is necessary—this will only apply when the coils have been self-wound.

Once the signal has been resolved, attention can be turned to L<sub>1</sub>, and with a proper dipole aerial connected, this coil may be adjusted to resonance.

#### Constructional Note

Keep all leads as short and direct as possible, and use also only high grade capacitors—paper types are useless at high frequencies.

## Radio Miscellany (continued from page 185)

the second he used a 10-way tagboard to hold all the resistors and capacitors in a neat row, thinking it would make the under-chassis look really ship-shape and Bristol fashion. His original model had these small components wired-in point to point. He says it took him over twice as long to wire up, and many of the leads were lengthened by several inches! Actually this often happens in amateur assembly. The great virtue of tagboards is that, in mass production, sub-assemblies can be completed *before* they are fitted to the chassis. Wiring them after they are mounted in a small chassis can often be a tricky business. From the point of view of the constructor who is habitually rebuilding, they possess a very solid virtue—resistors, etc., which have been stripped from something else and have only a quarter of an inch of their original wiring left can be used again without having a lot of knobby joints all over the place!

#### On with the Show

Another Radio Show has come—and gone—but as in recent years it was once again, from a constructors' point of view, little more than a furniture exhibition. Older readers will well remember the time when Radio-lympia was an exciting event with lots of interesting things to see and a number of samples to collect—perhaps even a couple of cardboard valves! When home construction was at its peak and the Mullard Master Three, the Cossor Melody Maker, the Osram Four, etc. were all the vogue, interested enquirers were given packets containing the wire needed to complete them, each piece cut to length with neatly hooked ends to fasten to the terminals as per pictorial plan. Whether you used them for that particular purpose was a matter for your conscience. Even the complicated receivers of that period could be

wired in an hour or so, and keen types stripped down and re-wired with slight variations a couple of times a week. Nicely tinned wire was thus very acceptable, and consciences are easily salved.

For the constructor the R.E.C.M.F., a far more recently introduced affair, has greater attraction. This, however, comes in the spring when interest is less keen than in the autumn, and is primarily for the trade, so it has never achieved great importance in the radio amateurs' calendar. The major event for us has been the R.S.G.B. Exhibition, although there has always been a widespread feeling that this was for the very advanced constructor or the transmitting amateur. It is a pity that this impression has been allowed to grow so firmly entrenched. True, the R.S.G.B. has pointed out several times that their exhibition was not concerned solely with the transmitting fraternity, but it seems that nothing but a vigorous campaign could obliterate the idea.

#### Showing the Flag

The constructor again comes into his own with the Radio Hobbies Exhibition, which is being held at the Royal Horticultural Old Hall from 23rd to 26th October, when home construction is the *main* theme. This exhibition takes the place of the Annual R.S.G.B. event. The significance is not merely the change of name. Rather, the name more accurately describes its widened scope and, although it is under the management of a well-known transmitting amateur, the Amateur Transmitter side of it is, rightly, just one of the important aspects.

Phil Thorogood, G4KD, who is managing it, has had great experience in exhibition work, and apart from his keen v.h.f. activities he has been prominently connected with local club affairs and the radio world generally.

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**F.M. TUNER-UNIT** (87 mc/s—105 mc/s) by Jason. Designer Approved Kit of parts for only 5 gns., post free. Set of 4 spec. valves 30/-, post free. Illustrated handbook with full details, 2/-, post free. 48-hr. Alignment Service, 7/6. P. & P. 2/-

**CONDENSERS.** Mica or S. Mica. All pref. values. 3pF to 680pF, 6d. each. Ceramic types, 2.2pF to 5,000pF, 9d. each. Tubulars, 450V, Hunts and T.C.C. 0.0005, 0.001, 0.005, 0.01 and 0.1, 350V, 9d.; 0.02, 0.05, 0.1, 500V Hunts, T.C.C., 1/-; 0.25 Hunts, 1/6; 0.5 Hunts, 1/9; 0.001 6kV T.C.C., 5/6; 0.001 20kV T.C.C., 9/6.

**TRANSISTORS.** Mrs. surplus PNP Junction type. Audio Type, 800 kc/s 250mW, 9/6; R.F. and L.O. Mixer Type, 2.5 Mc/s, 19/6. All tested and guaranteed.

**TRANSISTOR COMPONENTS.** Midget i.f. transist. 315 kc/s, 5/-; Ferrite Slab Aerial (dual range), 13/6; M. and L.V. Osc. and 1st I.F., 11/6; Push-pull interstage transist., 8/6; Push-pull output transist., 8/-; M/coil phone inserts dia. 2", 4/6; M/I dynamic inserts dia. 1 1/8", 3/9

**RESISTORS.** Pref. values 10 ohms to 10 megohms, 20% tol., 1/2W, 3d.; 1/2W, 5d. 1W, 6d.; 2W, 9d.; 10% tol., 1/2W, 9d.; 5% tol., 1/2W, 1/-; 1% hi-stab., 1/2W, 2/-

**PRE-SET W/W POTS.** TV knurled slotted knob type. 25 ohms to 30,000 ohms, 3/-; 50,000 ohms, 4/-; 50,000 ohms to 2 Megohms (carbon), 3/-

**S.T.C. RECTIFIERS.** E.H.T. types, K3/25 2kV, 5/-; K3/40 3.2kV, 6/9; K3/45 3.6kV, 7/3; K3/50 4kV, 7/9; K3/100 8kV, 13/6, etc. Mains types: RM1 125V 60mA, 4/9; RM2 125V 100mA, 5/6; RM3 125V 120mA, 7/6; RM4 250V 250mA, 16/-; RM4B type 250V 275mA, 17/6, etc.

**LOUDSPEAKERS.** P.M. 3 ohm. 2 1/2" Elac, 16/6; 3 1/2" Goodmans, 18/6; 5" R & A, 17/6; 6" Celes., 18/6; 7" x 4" Goodmans, 18/6; 8" Rola, 20/-; 10" R. and A., 25/-

**SPEAKER FRET.** Expanded bronze anodised metal: 8" x 8", 2/3; 12" x 8", 3/-; 12" x 12", 4/3; 12" x 16", 6/-; 24" x 12", 8/6, etc. **TYGAN FRET** (Murphy pattern): 12" x 12", 2/-; 12" x 18", 3/-; 12" x 24", 4/-, etc.

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**2 VALVE AMPLIFIER** (to fit above cabinet), modern circuit with EL84 output, ready built, with 6" speaker and output transformer, **£3.12.6**, carr. and ins. 2/6.

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**AUTO CHANGERS** 3 sp. COLLARO (RC54), £7. 19. 6. 4 sp. BSR (UAB), £8. 15. 0. 4 sp. COLLARO (RC456), £9. 15. 0. 4 sp. GARRARD (RC120/4H), 9 1/2 gns. Carr. and ins., 4/6. All above models Brand New and Guaranteed. Fitted latest style l'weight Xtal. P.U. with turnoverhead and twin sapphire stylii.

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Linear Ratio, 10,000 ohms—2 Megohms. Less switch, 3/- each. Coax Plugs, 1/2. Coax Sockets, 1/-, Couplers, 1/3. Outlet Boxes, 4/6.

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STANDARD 1/2" diam. Polythene insulated. Grade "A" only. 8d. yd.

Special. Semi-air spaced polythene. 80 ohm. Coax 1/2" diam. Stranded core. Losses cut 50%. Ideal Band 3, 9d. yd.

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**L.F. CHOKES**—10H 65mA, 5/-; 15H 100mA, 10/6; 10H 120mA, 10/6; 20H 150mA, 15/6.

**OUTPUT TRANSF.**—Standard pentode, 4/6; push-pull 12 watt, 13/6 Small pentode, 3/9. Midget battery pentode (15A, etc.), 4/6.

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8+8/500V Dub.	4/6 32+32/450V T.C.C. 6/6
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to 1/2 lb 7d., 1 lb 1/1, 3 lb 1/6, 5 lb 2/-, 10 lb 2/9. Bargain lists 3d.

**TRS**

**GLYNE RADIO LTD.**



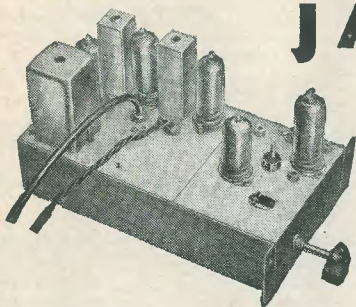
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MUSEUM 5929/0095

All correspondence to  
162 HOLLOWAY ROAD  
LONDON N7  
NORth 6295/6/7

Monday-Friday  
9-6 p.m.

Saturday  
9-1 p.m.



## JASON SWITCH TUNED FM FEEDER KIT

(AS DESCRIBED IN THIS ISSUE)

Designer approved kit

This excellent unit enables the selection of Home, Light or Third programme at the touch of a switch. Complete freedom from drift is ensured by the incorporation of Automatic Frequency Control. When used in conjunction with a suitable amplifier superb

quality is obtainable. The highest standards of efficiency and reliability that are the well-known features of the Jason Standard and Fringe Model FM Tuners have been maintained.

Up to the time of going to press a special price for the complete kit has not been finalised. However, as usual, we shall be offering this kit at a most competitive price. Send 2/- for our itemised price list and the instruction book.

**STOP PRESS**—Price just announced — Complete kit £9. 19. 6 P. and p. 2/6

## IMPORTANT ANNOUNCEMENT

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**ALL MAIL ORDERS** and **CORRESPONDENCE** in future to **HOLLOWAY ROAD** please.

**JUST ARRIVED!** Further limited quantity of Acos HGP37 crystal pick-up inserts complete with sapphire stylii, suitable for B.S.R. Monarch, etc. Brand new, only 18/6 and 9d. post and packing.

We carry the most up-to-date and comprehensive valve stocks in London at most competitive prices. Send stamp for list.

Our new 109 page comprehensive catalogue is now available at 2/- post free. Containing invaluable information on our kits of parts, chassis, components, transistors, loudspeakers, cabinets, etc., etc. This book is a "must" for all constructors !!!



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## PRECISION-BUILT COMPONENTS

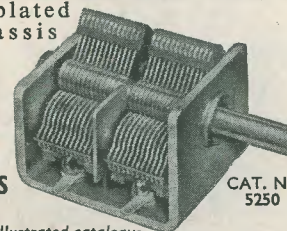
**JACKSON**

### 'O' GANG CONDENSER

Miniature model in 1 or 2 gang, capacities up to 365pF swing, front area  $1\frac{3}{8}'' \times 1\frac{1}{2}''$  including sweep of vanes,

length 1 gang  $1''$ , 2 gang  $1\frac{3}{4}''$ , spindle  $\frac{1}{4}''$  dia. x  $\frac{3}{4}''$  long. Aluminium vanes, cadmium plated steel chassis  
1 gang 7/6  
2 gang 11/6

It's Reliable  
If It's Made  
By JACKSONS



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5250

Please write for illustrated catalogue

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## No Resistance with ERSIN MULTICORE

### SOLDER

One imperfectly soldered joint can ruin reception and frustrate hours spent in assembly work. Be sure you use Ersin Multicore Solder on all connections in your equipment. Five cores of extra-active, non-corrosive Ersin flux, prevent oxidation, clean surface oxides and eliminate "dry" and H.R. joints. The Size One Carton gives you waste-free, trouble-free soldering without the need for extra flux. Get a carton today—and ensure good reception.



SIZE 1 CARTONS 5/- RETAIL

Catalogue Ref. No.	Alloy Tin/Lead	S.W.G.	App. 1'gth per carton
C 16014	60/40	14	19 feet
C 16018	60/40	18	51 feet
C 14013	40/60	13	17 feet
C 14016	40/60	16	36 feet

**MULTICORE SOLDERS LTD., MULTICORE WORKS, HEMEL HEMPSTEAD, HERTS (BOXMOOR 3636).**



## TELETRON Type FX.25

Self-tuned, dual wave  
Ferrite rod aerial. 15/- each



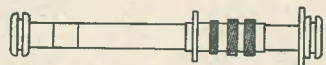
Specified for the "Companion" 3 Transistor regenerative pocket receiver.  
Type 24 Inductor ... .. 3/6 each



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High Q "potted" construction, with Ferrite screw cores. Mounted in screening cans 1" x 3/4" dia., 6/6 each. Oscillator coil, 6/6. Transistor type Ferrite rod aerial for MW band, 10/- . Selective crystal diode coil type HAX, 3/- each. Type HAX.L (for LW band), 3/6. Dual wave TRF coils, type A/HF, matched pair, 7/-, with adjustable iron dust cores.

## FERRITE ROD AERIALS



Wound on high permeability Ferro-cube rod. No external aerial required. Full sensitivity. Ideal for battery portable receivers. Medium wave, type FRM 4" x 1/8", 8/9. Dual wave type FRD, 8" x 1/8", 12/9. Miniature R.F. Chokes, wound on iron dust cores, with wire end terminations. 2.5 and 5mH, 3/- each; 10mH, 3/6. 200mH top lift Inductors, 6/6 each. Bias rejector coils, 4/6 each. Tape oscillator coils for push-pull operation, 8/6 each.

Send 5d. in stamps for complete data and circuits. All types available from advertisers in this Magazine and local component stockists.

## THE TELETRON COMPANY LIMITED

266 Nightingale Road . London N9

Telephone HOW 2527

Trade enquiries to sole distributor

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## DB5 TV FAULT FINDING

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Get your new Test Set by return of post on the easiest of terms. Write for descriptive literature.

## PULLIN MULTI-RANGE TEST SETS

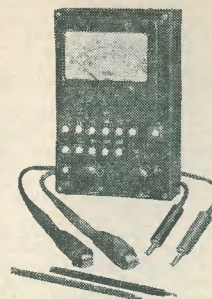
HOME RADIO (Mitcham) LTD.  
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Telephone MITcham 3282

### MINIATURE

19 ranges a.c./d.c., from 200 microamps to 1,000 volts. Sensitivity 5,000 ohms per volt.

£2.00 deposit and nine monthly payments of 19/6

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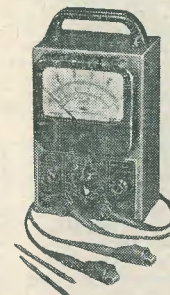


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21 ranges a.c./d.c., from 100 microamps to 1,000 volts. Sensitivity 10,000 ohms per volt.

£2.10.0 deposit and nine monthly payments of £1.4.6.

Cash price £12.7.6 complete



## TRANSISTORWISE

### "RECO" TRANSISTOR ONE

Make this simple little set up in about 30 minutes. Complete kit including transistor, diode, super sensitive phone and neat plastic case, 27/6, post and packing 2/-; nothing else to buy. Parts price list, etc., 9d. plus S.A.E.

### "RECO" EXPERIMENTER'S KIT

All parts, transistors, diode, transformer, high-Q frame aerial mounted on metal base plate 5 3/4" x 3 3/4", set of coils for short wave listening, balanced armature output unit, etc., 47/6, post and packing 2/-. Parts price list and circuit, 9d. plus S.A.E.

### "RECO" TWO

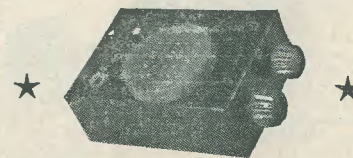
Receives home and continental stations. Neat plastic case 4 1/2" x 4 1/2" x 1 1/2". Complete with balanced armature output unit. Parts price list, etc., 9d., plus S.A.E.

## The RADIO EXCHANGE CO (Dept. RC)

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## The Teletron "COMPANION"

Three transistor pocket receiver



### COMPLETE KIT (as spec.) £4.15.0

(See our advert September issue)

List of components, circuit diagram, etc. 9d.

Bridisco crystal sets in attractive bakelite cases (various colours) ... .. 19/6  
Headphones for above, 125 ohms resistance 12/6  
2 pairs for 24/-  
Suitable all purposes (worth treble)

Teletron ferrite aerials:  
Medium wave, type FRM ... .. 8/9  
Dual wave, type FRD ... .. 12/9  
Teletron I.F. Transistor Transformers each 6/6  
(Complete range of Teletron coils in stock)  
Postage and packing on above items, 1/-

## ELEC-RADIO

172a BLACKSTOCK ROAD HIGHBURY  
LONDON N5 Telephone CANonbury 1672  
Callers Welcome

**A.C. Superhet 5-valve Chassis.** Medium and two short, unused, but less valves and mains transformer. Uses standard Octal range. 27/6. (Again, coil pack worth much more.) Non-callers add 6/6

**A.C. Superhet 7V 5-Waveband Chassis.** H.F. stage. Unused. Less valves and power pack. Slightly soiled. Coil pack worth twice as much, circuit diagram supplied. £2.15.0, carriage and insurance 7/6

**A.C. 4-valve Superhet,** complete with valves, but less scale and pointer, unused. Circuit diagram supplied. 39/6 plus. Note that the above three chassis, although unused, will need checking. On account of low price, no guarantee is given. Nor, we regret, can technical assistance be given.

**0.1µF 350V Small Tubular Metal cased Condensers.** Made by Dubilier. 2/6 per dozen. **Germanium Diodes.** B.T.H. with wire ends. 10d. each or 9/- dozen

**Midget I.F. Coils.** Dust cored, size 1½" x 1", 465 kc/s. 4/6 pair **Standard Size. I.F. Coil.** Dust cored, 465 Mc/s. 4/6 pair

**Coil Pack for Superhet.** 465 kc/s. I.F. Medium and 2 Short waves. 9/6

**Cathode-Ray Tube.** VCR97. Instrument type. New 7/6 each, carriage 3/6

**Bakelite 5 amp Electric Wall Switch.** "Hicraft," 9d. each, or 8/- per dozen

**Series, parallel and off-electric wall switch** made by Crabtree. Price 1/3 each, or 13/6 per doz. NOTE: Additional technical data is not available on these bargain items.

**Amplifier, ex-Government unit 1134** contains one double triode and one triode. 6/6, post and ins. 2/6

**Connecting Wire, P.V.C.** covered 24 s.w.g. copper. 2/6 per 100ft, or 5 coils, different colours for 10/-

**Scanning Coils** by very good maker. New and unused. 4/6 complete

**10 v. Superhet, 1½ metre.** Ex-Govt. but unused. Complete with valves. Easily converted for Band III. 39/6, carriage and packing 7/6

**Cathode-Ray Tube, VCR517.** 8/6 each, carriage 2/6

**Mains Lead.** Metal screened to stop interference, 9d. yard

**Midget Push-pull Input Transformer** and push-pull output transformer to match. 8/- pair. NOTE: Orders for small components over £2 are post free, otherwise please add sufficient.

## AUTO-CHANGER 30/- DEPOSIT

### 3-SPEED & 4-SPEED GRAMOPHONE AUTO-CHANGER

Latest types by all famous makers are invariably in stock at competitive prices. B.S.R. Monarch, Garrard, etc. Latest models from £8.10.0, or deposit £1.10.0 and 8 payments of £1 plus 5/- carriage and insurance.

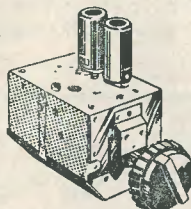


### THIS MONTH'S SNIP

**Tape Deck**—Made by the famous Truvox Company. This contains exactly the same essentials as the current model. Only the styling is different. It also takes the stereophonic head.

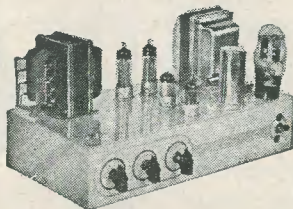
Specification: 3 B.T.H. shaded pole motors with silent friction drive eliminating wow and flutter. Push-button controls, electrically and mechanically interlocked. Patented electric type push-button controlled brake. Tape loading on the drop-in principle, accommodation for reels of 7" diameter. Tracking sense to British and American standards. Playing time: up to 3 hours with L.P. Tape or 2 hours with L.P. Tape or 2 hours with Standard Tapes. Two tracks side by side with safety gap. Positive Azimuth adjustment of Record/Player head. High impedance heads. Overall size 14½" x 12½" x 5" approx. 120 only of these fine decks offered at non-repeatable price of £17.10.0 or £3.10.0 down and eight monthly payments of £3. Non-callers add 10/- carriage and insurance.

## TURRET TUNER

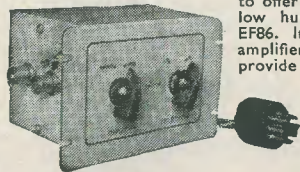


Brand new stock, not surplus, with coils for Band I and III, complete with valves PCC84 and PCF80—I.F. Output 33/38 Mc/s with instructions and circuit diagram 79/6. With knobs 3/6 extra, post and insurance 2/6

## MULLARD AMPLIFIER



A Quality Amplifier designed by Mullard. Power output exceeds 10 watts. Frequency response almost flat from 10 to 20,000 c.p.s. For use with the Acos "Hi G" and other good pick-ups. Made up and ready to work is £12.10.0 or £1.10.0 down and 8 payments of £1.10.0, plus 10/- carriage and insurance.



**MULLARD PRE-AMP.** We are pleased to offer as a ready-made unit. It uses the low hum/noise high gain pentode type EF86. It takes its power supply from the amplifier and incorporates 2 switches to provide immediate compensation, for radio, microphone, L.P. and 78 records. The price of this unit is £4 post and insurance 3/6 extra. Or 10/- down and 9 payments of 10/-. If purchased with above, combined price is £16 or 30/- down and 8 payments of £2.

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## High "Q" Coils



4/- EACH  
Iron dust cores. Clip in fixing. EXTREMELY SMALL. AMAZING EFFICIENCY. For Superhet T.R.F. or Transistor operation.

## OSMOR (Frequency Controlled) F.M.

Switch-tuned Feeder  
With special quick-build chassis

A completely stable drift-free unit for adding to existing radio or Hi-Fi amplifier  
**EASY TO BUILD** Size 4½in x 5½in  
Wiring diagram and circuit on request.

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Crystal Tuner  
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The Radio Constructor  
TRF Tuner  
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WE HAVE A FULL RANGE OF COILS FOR TRANSISTOR CIRCUITS

OSMOR COILS FOR HIGH "Q"  
SELECTIVITY & PERFORMANCE



**FREE!** Send 10d. (stamps) for fully descriptive literature including OSMOR DESIGNS—5-Valve Superhet, Miniature ditto, Battery and Battery/Mains Receiver, Mains T.R.F. Superhet and T.R.F. Feeders. Band 3 Converters, Wiring Diagrams, Chassis Templates, Coil and Coilpack information and price lists and information on circuits in Wireless World, Practical Wireless, The Radio Constructor  
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Available for the first time in this country, these are the product of a famous manufacturer. The following values are now in stock:

25µF 6V 8µF 6V  
16µF 12.5V 5µF 12.5V  
8µF 25V 1.6µF 6V

All at 4/- each  
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T.C.C. Sub-miniatures. 32µF 1.5V, 6µF 3V, 10µF 3V, 2µF 12V, 4µF 12V, 8µF 15V all 4/9 each

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Red Spot (equiv. OC71) 10/-, R.F. Blue Spot (1.6 Mc/s) 15/-, Superior type (packeted with data): Audio 11/- each, R.F. (2.8 Mc/s) 21/- each

THREE DEE KIT ... .. £5.2.6  
(Instructions 1/-)  
COMPANION KIT ... .. £5.6.6  
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**TRANSISTOR HOLDERS.** Enable transistors to be plugged in and out like valves, without danger from heat of soldering iron. For any type of transistor. Recommended by R.C. (June). 1/- each, 6 for 5/6, 12 for 10/9

ALL JASON PARTS STOCKED. SEND FOR LISTS

Send for Catalogue price 5d.

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(British Manufacture)

RED-SPOT 800 kc/s Audio Frequency	10/-
BLUE SPOT 1.6 Mc/s Mixer and Frequency Changer	15/-
WHITE-SPOT 2.5 Mc/s R.F. and I.F. Amp.	20/-

All Transistors are Tested and Guaranteed

N.B.—The Red-Spot is similar to Mullard OC71 Transistor Bases 9d. each

### TRANSISTOR PUSH-PULL AUDIO AMPLIFIER

(200 Milliwatts Output)

Build this Push-Pull Amplifier which is ideal for Crystal or Magnetic Pick-up Amplification, Baby Alarm, Microphone Amplifier, etc. Powered by 6-volt Dry Battery lasting for months. Complete Kit of Parts including 4 Transistors and all Components with Circuit (less Speaker), £4. 10. 0

### COLLARO RC456

4 speed auto-changer. Latest type with crystal turnover pick-up £9. 15. 0

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Complete Kit with 2 Transistors, components, phones, with circuit and plastic case 42/6

### TRANSISTOR SQUARE WAVE GENERATOR

Complete Kit with 2 Transistors, Components, Circuit and plastic case 25/-

### DIODES

B.T.H. Germanium	1/6
Mullard OA74	2/6
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1N22, 1N23, 1N21A	5/-

### MODEL-MAKERS' MOTORS

Two types available, 12 or 24V with 1/4" spindle, 10/- each

### 6V VIBRATOR PACKS

Output 120V 30mA. Brand new 12/6

## Valves — Valves — Valves

We have over 300 different types of British and American valves in stock. We give below new types that are available. Send for 28-page Catalogue for further details of valves, components, etc.

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ECC83 9/-	EZ80 10/-	UF85 12/-	12AX7 9/-
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EF41 10/-	PCL83 15/-	6L18 12/6	117Z3 8/6

All Valves Tested and Guaranteed



### MINI-TWO

2-TRANSISTOR MINIATURE POCKET RADIO  
(No Aerial or Earth)

The smallest transistor set offered on the market. Variable tuning. Drilled chassis, plastic case size 3" x 2" x 3/8", miniature hearing aid, 2 transistors and all components including 1 1/2 volt battery, circuits and full practical layout diagrams.

Total cost 49/6 complete

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2-TRANSISTOR PERSONAL PORTABLE  
No Aerial or Earth required

Variable Tuning

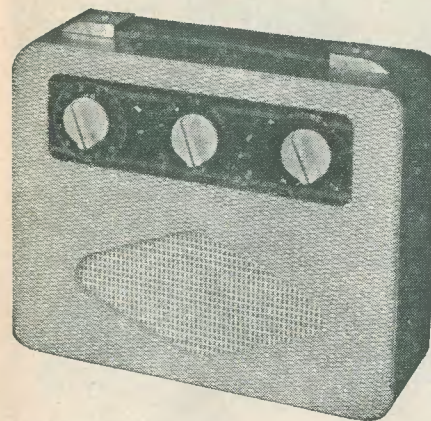
We can supply all components including 2 transistors, diode, resistors, condensers and miniature hearing aid and plastic case, size 4 1/2" x 2 3/8" x 1 3/8", and 1 1/2 V battery, for 52/6. All items sold separately

### COLLARO RC/3/554

3-speed single player with crystal turnover pick-up type "T," £6.19.6, carr. 3/6. Brand new in original carton

# The NEW "TRANSISTOR - 8"

Push-Pull Portable Superhet



Can be built for £11/10/-

### TEN STAR FEATURES

- ★ 8 specially selected Transistors
- ★ 250 Milliwatts output push-pull
- ★ Medium and Long Waves
- ★ Internal Ferrite Rod Aerial
- ★ 7" x 4" elliptical High Resistance Speaker
- ★ Drilled plastic Chassis 8 1/2" x 2 1/2"
- ★ Point to point wiring and practical layout
- ★ Economical. Powered by 7 1/2 V battery
- ★ Highly sensitive
- ★ Attractive lightweight contemporary case

We can supply all these items including cabinet for £11.10.0  
All parts sold separately

Send for circuit diagrams, assembly data illustrations and instructions, and full shopping list 1/6

This Portable 8-Transistor Superhet is tunable for both Medium and Long Waves and is comparable in performance to any equivalent Commercial Transistor Set. Simplified construction enables this set to be built easily and quickly into an attractive lightweight cabinet supplied.

N.B.—Pair of OC72's supplied at additional cost of 40/-  
Call and hear demonstration model

As featured in August issue and described on page 28

## "EAVESDROPPER"

THREE-TRANSISTOR POCKET RADIO

(No Aerial or Earth required)

Variable tuning—medium wave. Total cost, as specified including Transistors, Transformers, Coils, Condensers and Battery, etc., with circuit, plastic case and battery.

All items sold separately 77/6 POST FREE

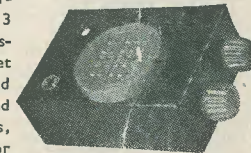
With miniature hearing aid ... .. 90/-

With balanced armature ... .. 82/6

## THE TELETRON 'COMPANION'

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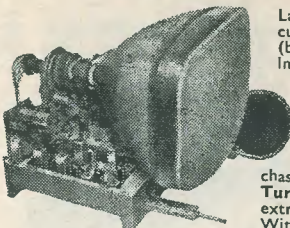
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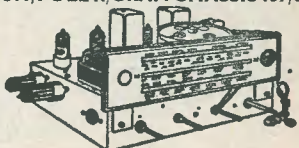
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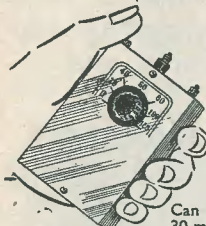
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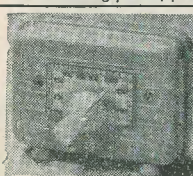
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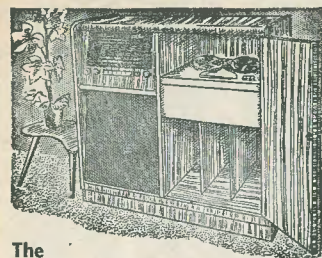
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continued on page 215



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continued from page 213

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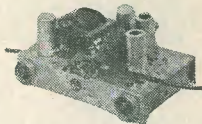
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