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6L6WGB/5881	£25.00	£50.00	£100.00
KT66	£25.95	£52.00	£104.00
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We have a vast range of tubes available from manufacturers all over the world including rare and vintage types. A 70 page booklet of valves available is updated monthly and can be provided at a cost of £2.50 per copy including U.K postage or you may telephone our Sales Desk for a prompt quotation. Prices exclude VAT. Please add VAT at 17.5%.

A selection from our stock of over 2,500 different audio quality valves. Please enquire for items not listed

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arising from the construction or use of any of the designs published.

The performance and specification of these projects can only be guaranteed

Supplement

Contents

KIT NEWS

All the news from the DIY hi-fi industry.

REVIVING THE QUAD FM1 TUNER

We bring Quad's vintage classic tuner back to life, with a dedicated power supply and a complete tune up.

THE OPEN BAFFLE LOUDSPEAKER

Prompted by one of your letters, we take a theoretical look at building a simple, passive open baffle loudspeaker.

K5881 GOES TRIODE

Well, on its input at least. The latest version of our popular 20W K5881 stereo power amplifier now uses a 7025 double triode input valve for a sweeter, warmer sound. We bring you the latest circuit.

BOOK REVIEW:

LOUDSPEAKER AND HEADPHONE HANDBOOK

Edited by John Borwick and containing chapters from some of the industry's leading experts, this is one of the most complete reference works we've come across.

DIY LETTERS

Here's where you can write in to tell us about your own unique designs and ideas as well as ask for help along your way to DIY hi-fi bliss.

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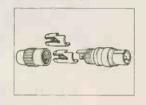
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EL84	£6.00	12AX7 PREMIU	M £4.50
6L6WGB/5881	£10.00	EL34	£4.90
6SL7WGT	£6.00	EL84M	£5.00
6SN7WGTA	£6.00	6L6/5881	£4.90
6V6GT	£6.50	6922	£4.00
6550A	£30.00	7199	£8.00

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REPAIR/CALIBRATION. Even the finest equipment's will suffer an occasional breakdown and need meticulous repair, calibration and alignment. The only standards we recognise and work to are Manufacturers Original. Our Test & Measurement facilities are probably the best in this sector of the Industry... and we know how to use them!

KIT-BUILDING. There are numerous kits around nowadays. They all require skill/experience to build satisfactorily and, in the case of valve equipment, safely. Some designs are good, otherswell, let's just say their 'designers' would benefit from a sojourn on that celebrated desert island with only Terman and Langford-Smith for company! Whichever kit you choose, though, it will benefit from a professional build. We will build it, de-bug it and give you a set of Final Test figures

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KIT NEWS

THE NEW POWERS THAT BE

Svetlana Electron Devices of
Huntsville, Alabama, have
just introduced
four new

power triodes intended specifically for use in high quality amplifiers. Like the 845 and 211A, these new Svetlanas have directheated, thoriated tungsten filaments, but come with massive graphite anodes. Rated at 125w, there's power on tap even in single-ended operation.

Four amplification factors are offered for circuit design flexibility, with the SV572-3, for example, claimed to give a clean sound without feedback, while a pair of SV572-160s can produce 300w output in Class B.

Svetlana Electron Devices 8200 South Memorial Parkway, Huntsville, AL 35802 Tel: (205) 882 1344 Fax: (205) 880 8077

MORE SVETLANA GOLD

Watford Valves have started importing the latest Svetlana EL34 and 6550C Gold power valves. The latter benefits from a new tri-plate anode, precise grid/screen alignment and gold-plating on the grid itself. There is also a free matching service on both valves throughout October.

Watford Valves 3 Ryall Close, Bricket Wood, St. Albans, Herts. AL2 3TS. Tel: 01923 893270

BACK TO THE FUTURE

PM Components are taking a trip down memory lane with their new Retro range of valves, recreations of original designs from companies like GEC and Marconi. Thus far two valves have been produced, the KT88-R and KT66-R, both using the same materials in their construction as the originals and built to the same standard. For prices and more information contact:

PM Components
Unit B3
Springhead Enterprise Park,
Gravesend,
Kent DA11 8HD
Tel: 01474 560521

AUDIOCOM GO ALUMINIUM

Audiocom are now able to supply 450v aluminium capacitors from Panasonic. These have a large ripple current capacity and can be used in valve amp power supplies and the like. Audiocom are also offering 10% off prices of OSCON capacitors and high purity silver wire during November, and any order over £25 will include a free metre of silver solder.

Audiocom
2 Swallowtree Gardens,
Saundersfoot,
Pembrokeshire SA69 9DE
Tel: 01834 814036

CHELMER'S LION

Chelmer Valve Company can now supply a version of the KT88 which is a close copy of GEC's Gold Lion valve. The valves are manufactured in Europe and come in matched pairs with individual test reports at £60 a set.

Chelmer Valve Company 130 New London Road, Chelmsford, Essex. CM2 0RG. Tel: 01245 355296

SJS TRANSFORMATION

Extending their existing range of valve amplifier output transformers, SJS Electroacoustics are now producing four new single-ended transformers designed for maximum bandwidth with interleaving and split bobbins. For those who like transformers in their pre- as well as power amps, there are also new arrivals on the interstage and pre-amp output transformer scene, SJS claiming a bandwidth of I 20kHz for both types. For the final aesthetic touch, black, chrome and brass finished caps are available.

SJS Electroacoustics Ben-Dor, Lumb Carr Road, Holcombe, Bury, Lancs. BL8 4NN Tel/Fax: 01706 823025

SIMPLE SWITCHERS

If you'd like to follow Linn down the road to high efficiency switch-mode power supplies, then Farnell might have what



you're looking for. They now stock the new £7.50 LM2825 from National Semiconductor, which contains a complete IA switching regulator on a single chip - all you need to add for a 5v or 3.3v output is a 7-40v input. Also available is a variety of regulators from Melcher's IMR6 range, concentrating mainly on 5v and 12v supplies with prices starting at £28.69.

Farnell Electronic Services Edinburgh Way, Harlow, Essex CM20 2DF Tel: 01279 626777

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K1100 AUDIO DESIGN 80 WATT POWER AMPLIFIER



and the Ideal powerhouse for your ultimate his fit system. This kit is your way to get EX performance at bargain basement prices. Unique design features such as fully FET stabilised policy supplies gives this ampiller World Class performaline with starting clairly and transparency of sound, allied to the famous HART quality of components and ease of construction

Jseful options are a stereo LED power mater and a versatile passive front end own of switched inputs with ALPS precision Blue Velve, low-paise volume and

Construction is very simple and enjuyabili with all the difficult worl done for you even the wiring is pre-terminal id in to $\sigma_{\tau} = 1$ and $\sigma_{\tau} = A$ vertices are available. ith Standard components or specially we edied Super Audiophile components at £29 60 extra per channel plus £2 40 if you want to include Gold Pialed speaker

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K1100 Standard Stereo Amplifier	£415.21
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K1100M Monobloc Power Amp	£271.20
RLH10 Reprint of Latest Amplifier Articles	£4.50
K1100CM Construction Manual with Full Parts List	£5.50
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First module to appear in our new 2000 Range" of kits. This unit provides a high quality phone output for those many amplifiers that do not have one. Easily istalled with special link through facility the unit draws its power from our Invalid. Hart minibox it features the wide frequency response, low distortion and musicality, that one associates with designs from the renowned John Linsley. Hood: Pre-terminated interconnecting leads and PCB mounted societs prevent supply potar ly and on bioard diagnostics pro-dury sual indication of supply line integrity. Volume and balance controls are Alps "Blue Velvet" components. Very easily built, even by beginners, since all components fit directly on the single. printed circuit bourd and there is no conventional wiring whatsoever. The kit has

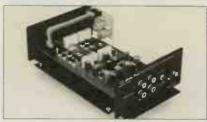
rery de ailed instructions and even comes with a roll of Hart audiograde silver solder. It can also be supplied factory assembled and tested. Selling for less than the total cost of all the components of they were bought separately this unit represents incredible value for money and makes an attractive and harmonious addition to any hi fi system K2100 Chiara Headphone Amplifier

K2100SA 'Super Audiophile' Version £115.46

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K1450 Pickup Preamp Kilform £116.58 K1450SA Super Audiophile Version £138.94

Why not buy the reprints and construction manual for the kit you are interested in to see how easy it is to build your own equipment the HART way. The FULL cost can be credited against your subsequent fut purchase

ALPS "Blue Velvet" PRECISION AUDIO CONTROLS.



Now you can throw out those noisy ill-matched carbon pots and replace with the real fu-fi components only used selectively in the very top flight of World class amplifiers. The improvement in track accuracy and matching really is incredible giving better tonal balance between channels and rock solid image stability

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noiliza	P26 Q8

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Reviving the Quad FM1 valve tuner

Noel Keywood investigates the restoration of the Quad FMI valve tuner.

I ve seen boxes of unloved Quad FMIs tuners sitting under trestle tables, to clear for around £10 apiece. Why does a lovely valve tuner like this so commonly inhabit the lowlier regions of a vintage swap-meet? A Leak Troughline these days goes for £50 minimum - and often a lot more.

There is a reason Quads remain ignored of course, but it

power amp. The mains connection to the preamplifier exists only so that the whole shooting match can be switched on by the volume control. In those days - the late 1950s - power amps were hidden away, leaving a set up as compact as any today, and certainly more elegant,

Both Mission and Linn acknowledge the example of Quad in this respect, and both use complex castings that cost a fortune to tool up. Trouble is, neither really exploit the styling benefits casting provides, certainly not in the way Quad did with the FMI, sculpting wonderful curves, bevels and ledges, difficult to achieve by any other method. Linn and

Mission castings are too planar to clearly advertise their uniqueness and - woe! - they are painted black.

isn't related to performance.

The big drawback with the Quad FMI is that it is powered from the Quad II valve power amplifiers (yes, both of them), via the preamplifier. It is also switched by the Quad II preamplifier. So an FMI is the most inert tuner going if you don't happen to own an entire Quad 22/II set up. Peter Walker, founder of Quad, showed some ingenuity with his first integrated system arrangement (he did beat B&O), but he didn't do much for second hand prices.

Unbelievably, to split the load, the Quad 22 preamp and the FMI draw L.T. for their heaters (6.3V) from one power amp, and H.T. (330V) from the other

but difficult to switch on without a complex arrangement like this

For me, the volume control mounted power switch and illuminated Quad legend were distinguishing features of Quad pre'powers, not to mention the delightfully solid cast fascias. I was soing to say they don't build 'em like it today, but they do

So that's the glory of the FMT it's beautiful to look at and to use, one of a kind, but a trifle difficult to get going.

What do you expect for a tenner?

There's definitely leeway here for many evenings entertainment, restoring an

FMI, so as usual let me first pour a little cold water on the idea.

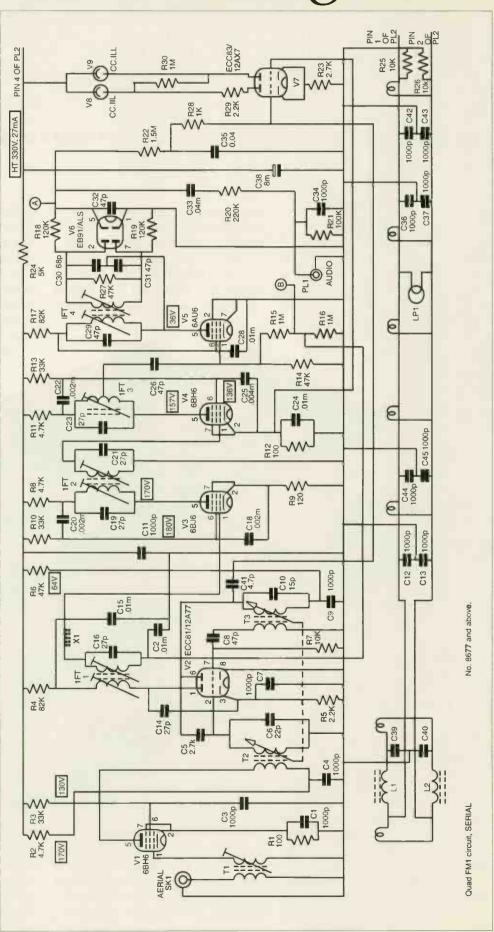
Building a power supply for the FMI gets it up and running as an independent unit. This is a simple enough task for anyone conversant with electronics, but dangerous if you don't know how. The FMI needs 330V H.T. (High Tension). The good news is that a complete supply will cost just £20 or so.

The other big problem with old tuners is alignment. This is quite likely to be awry and tuner realignment is not an easy task. If a simple RF generator is used it requires skill and experience. A poorly aligned tuner will distort, be insensitive and suffer interference. But I have more good news: Quad offer an alignment service that costs £40.

Ageing valve units like this - and the FMI is now 40 years old - usually have a lot of resistors and capacitors that need replacing, since old components drift in value over the years and fail. The few decent condition FMIs I've encountered to date worked in a fashion, but not properly. However, armed with a circuit diagram and a good electronic multimeter it isn't difficult to repair a tuner like this, if you have a little electrical knowledge. Fail, and you have either lost £20 or so, or you can ask Quad to bail you out, since they still service and repair the FMI.

I need to point out that this article is a guide to getting the FMI going, identifying the main problems. You must have some electronic knowledge to be able to tackle such a project. This is not a subject for beginners and this article is not meant for those with scant knowledge.

Circuit Diagram



CIRCUIT DESCRIPTION

Here is Quad's circuit description:
"A broad band fixed tuned transformer couples the low impedance aerial to a RF pentode (6BH6) the output of which is transformer coupled to a low noise triode (one half of 12AT7) mixer stage.

The local oscillator (other half of 12AT7) is fully temperature compensated and provides an output 10.7MHz above the signal frequency. It is capacitively coupled to the mixer grid.

Both the mixer grid and local oscillator circuits are ganged and permeability tuned by special low loss cores driven from the spindle via a precision worm drive mechanism.

The resultant 10.7MHz IF signal at the mixer anode is transformer coupled to the automatic gain controlled first IF stage (6BJ6). A combination of critical and over coupled circuits and a single tuned circuit in the second IF stage (6BH6) together with a close control of the Q of these circuits ensures a wide passband with a steep cut-off outside the band.

The second IF anode tuned circuit is coupled via a short time constant CR circuit to the limiter valve (6BH6), the anode of which contains a transformer with a capacitively centre tapped secondary winding feeding two diodes (6AL5) in a phase discriminator circuit. Again, the coupling and Q are chosen to give low distortion in the audio output.

The audio signal is fed via a two position switch either, in the unmarked mono position, to the appropriate deemphasis network and DC blocking condenser, or in the red spot position, to the output cable when an uncorrected signal is needed for feeding into a stereo decoder.

The DC component at the discriminator output whose magnitude is proportional to the amount of mistune and of polarity dependent upon the direction of mistune, is fed to a cathode coupled phase invertor stage (12AX7) which contains a miniature neon in each anode. Slight mistuning extinguishes one neon, showing the direction of mistune, while even illumination of both indicates correct tuning. In addition, this stage provides Automatic Frequency Control, one section of the double triode acting as a reactance valve across the local oscillator tuning coil."

CHECKING WITH A MULTIMETER

Quad quote the H.T. as "between 250V and 350V". However, the nominal is 330V, the exact value being determined by mains supply volts and component tolerances, etc. The tuner consumes 27mA. The heaters consume 1.5A, and there's a 0.3A lamp, making for 1.8A total L.T. consumption, at 6.3V. These values must be checked with a multimeter.

The valves V1 (6BH6), V3 (6BJ6) have around 170V on the anodes, and V4 (6BH6) has 157V. Around 0.75V-IV should exist on the cathodes. The mixer/oscillator, V2 runs at lower voltages and the limiter, V5, works in saturation mode. It has no

grid bias, so the cathode is connected to ground, and it has just 35V on the anode. All the main voltages are marked on our circuit.

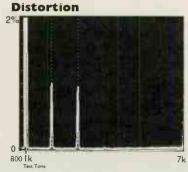
Ken Bunting, who has been with Quad servicing their products since 1970, told me that all the resistors in the high voltage lines tend to go high; one of ours had drifted from $82k\Omega$ up to $103k\Omega$ over the years, for example. They inspect and replace these first. The old capacitors, he

told me, might look a little rough by modern standards, but they were more likely to be acceptable. In 'our' FMI, a tidy unit supplied by Graham Tricker I should point out, all the capacitors had been replaced, but not the resistors. In spite of the resistors being generally high, and the voltages a little low, it worked well. However, it was obvious to me from distortion figures, frequency response and the way it tuned into and out of stations that alignment of our FMI was out, and the de-emphasis needed tweaking. So, be aware that just checking all DC voltages with a meter is not enough.



Ken Bunting, who has been with Quad servicing their products since 1970, checked and re-aligned our FMI for optimum performance.

QUAD FM1 TEST RESULTS



Frequency response Stereo separation Distortion (50% mod.) Hiss (CCIR) 7k So 14Hz-16kHz Signal mono Selecti

1.3%

-81dB

+30
-350
20k

Signal for minimum hiss
Selectivity (at 0.4MHz)
Sensitivity
mono

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Our circuit shows an early mono FM1 with an internal de-emphasis network. Later stereo compatible units have a two-position switch that, moved to the Red position, switches out deemphasis to give a raw feed for a stereo decoder. This must be used to feed either Quad's own original decoder or the modern design such as the 1310 based design Graham Tricker can supply. De-emphasis is then applied later, within the decoder. Quad told me that C32 between the discriminator cathodes should be reduced to 15pF or so (from 47pF) when feeding a decoder direct, in order to strengthen the 19kHz pilot tone.

I should explain here that in order to lessen the audibility of hiss an FM signal is pre-emphasised above 2kHz (i.e. has treble lift) by the broadcaster to increase treble energy. The signal is then de-emphasised (i.e. has reciprocal treble fall) after demodulation in the receiver to give a net flat response. This technique is used in mono and stereo FM transmissions alike.

The Zenith GE stereo system, introduced in the late 1950s and used today, possesses a 19kHz pilot tone and a 38kHz suppressed sub-carrier, modulated with the stereo information. De-emphasis would ruin this composite signal, so it is applied after stereo decoding. So a stereo decoder always takes a raw audio feed, lacking deemphasis.

For mono listening the stereo decoder can be ignored, but then the capacitors C33 (DC blocking) and C34, and resistors R20 and R21 must all be correct value. De-emphasis is carried out by R20,21 and, believe it or not, the output load (100k) all in parallel, in conjunction with C34, to give nominally 48μS de-emphasis time constant (the UK uses 50μS). Incorrect values here upset audio frequency response, as will any stereo pre-amp input impedance other than 100kΩ! So you must pay special attention to these component values and

to the item an FM1 feeds if it is to sound right when delivering mono audio direct out.

Because I wanted to assess the basic tuner and not get too involved in the stereo decoder at this time - a whole subject in itself - I chose to set up, use and measure the FM1 in mono (dual-channel). Feeding an Audiolab 8000S preamplifier I found putting $47k\Omega$ in series with the output and increasing C34 to I250pF gave a flat response to I6kHz (there's no mpx filter to limit treble extension), shown in our spectrum analysis.

A Leak Troughline suffers none of this interfacing trouble, having a buffered output. And it is self powered of course, so now you know why the FMI comes cheap nowadays. Audio output from our FMI, without decoder, measured 600mV at 100% modulation (i.e. full output).

Most FMIs are fitted with a piggy-back Quad stereo decoder, which is solid-state, using old germanium type transistors like OC44s (which some people insist sound better than modern silicons). By and large, early decoders give somewhat mediocre results, and Quad's has a complex power supply arrangement, which is why I've not concentrated on it here. My apologies if this is a slur on Quad's first decoder. I suggest the use of a modern stand-alone decoder such as Graham Tricker's.

I visited Quad to get our FMI aligned. Ken Bunting confirmed that it was in fair working order, but it could be improved by resistor replacement. He had some other interesting observations to make.

The neon tune indicators have 'popeye' lenses on them and, also, they produce RF interference that causes spurious whistling when tuning into and out of stations. Since the original popeye types are not now available Quad choose to fit a small circuit board carrying LEDs that do the same job, but better.

Many chip-based stereo decoders have been brewed up over the years for the FMI. National Semiconductor publish a circuit in their Audio Handbook that uses a LMI800 chip.

Quad have most parts for the FMI,

but not the front panel. The gold bands normally corrode, making the FMI look tatty after a time. Graham told us that "ours" (his in fact!) was the best sample he'd ever seen, and Quad agreed. Realignment showed that the IFs were too peaked. Ken flattened the passband and ensured the demodulator was fine.

This work optimises selectivity, minimises distortion and, very importantly, gives and optimum tune point. Where the tune indicators had appeared not to work properly, after alignment they did. Having built quite a few valve receivers myself in the past I knew not to bother assessing the FMI until it had been aligned properly.



The Quad FMI is simple enough inside to make servicing and renovation fairly straight forward.

Quad themselves and specialists like GT Audio can help here if you're unsure what to do.

Tracking across Band II (88-108MHz) cannot be made perfect. Quad ensure the tuner is station accurate at the bottom end of the band (Radio 2/3/4) but admit it may be up to IMHz out at the top end, around Radio I, for example. Also, component position in the RF head (the metal box into which the tuning shaft goes) affects tracking so if any component is disturbed or replaced here - and it is likely that some resistors will need to be - then tracking needs to be reset.

You might have gathered there's a bit too all this. Sadly, there seem to be few books available now on this subject, especially referring to valve tuners. Just bear in mind, if you are looking for a book on the subject, that a tuner like the FMI is configured much like any superheterodyne receiver, AM or FM, right up to its demodulator.

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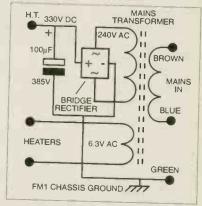
Very conveniently, 330V happens to be the peak value of 240V rms. This means that a mains 1:1 transformer can be used, since with a bridge rectifier, electrolytic smoothing capacitor and low current drain of 27mA we can expect 330V to be achieved almost exactly and it was. Even more conveniently Maplin have just the right transformer. It delivers 240V AC at 100mA, plus 6.3V at 1.5A.

Whilst we need a little more than the rated LT current, it's an extra 2VA from a 34VA transformer, and since we are 8VA short from full drain on the HT I'd not expect core heating. In practice this was the case; the transformer ran cool and the LT didn't droop, giving 6.3V at 1.8A, with 240V AC in. Maplin identify this part as Valve Transformer XP27E, priced at £12.99, on p991 of their Sept-Aug 96 catalogue. I bought one from Maplin's Hammersmith branch in West London one Saturday morning.

You need a bridge rectifier of IA-I.5A capacity rated at a minimum of 260 forward volts, and 400 Peak Inverse Volts (PIV) minimum. The electrolytic needs to be around 100 μ F, rated at 385V or more. You'll have difficulty detecting hum (a buzz in fact) with this. However, to get rid of it completely a Ik Ω /IW resistor should be used with up to 100 μ F either side, in π filter arrangement. Better still the resistor should be replaced by a choke.

These parts must be mounted in an earthed metal box, or a plastic box, for safety. It should be fitted with a mains switch.

Connecting up the power supply to the FMI is easy enough. I'd suggest the existing power leads and, especially, the horrid 4-pin plug, now unavailable, are cut off and replaced by modern cable. Trace the power lead back into the tuner and you will find it terminates at three feed-through insulators. A new cable can be soldered in here. Note that the heater feeds are not grounded, but the HT is, so there are two heater lines and one (red) HT line. HT negative runs via the chassis and there is a suitable solder tag close to the feed-throughs.



Building a separate power supply can be easily done with standard components from Maplin Electronics

PERFORMANCE

Under measurement, frequency response was flat, our de-emphasis values giving a little +0.5dB lift at 8kHz. Mono noise figures are always much better than stereo, but the FMI was still very good, giving -81dB hiss no less -better than most solid-state tuners. Mono -50dB sensitivity was a healthy 4µV and quieting so good that the FMI will, in mono, should work well even with a poor aerial. Selectivity was a bit lop sided on ours, giving a mediocre 48dB rejection to stations +0.4MHz away, but a healthy 60dB to stations -0.4MHz away.

In listening tests I was not surprised to find the FMI lacked the hardness of tone, flatness of imaging and treble glare that can afflict solid-state designs. It wasn't as sweet and deeply atmospheric as our Troughline, that's for sure, and I have to say that I did have to wrestle it into action with a lot fiddling to ensure the de-emphasis components matched the preamplifier load. Since this was done with the aid of a stereo generator and spectrum analyser, to ensure a flat frequency response, the investment here

was not inconsiderable. There's a good case for letting Quad's excellent service department sort out this sort of thing. You will have to pay of course, but their charges are reasonable.

Both Classic FM and Radio 3 transmissions lacked hiss, hardly surprising considering the unit's fabulous -81dB noise figure. To eliminate hum completely power supply smoothing must be very good. The FM1 also has its own internal smoothing capacitor, C38, which needs to be checked.

Lacking inter-station muting, and working from a large outdoor aerial, the FMI picked up many "ghost" stations. These were distant transmitters in fact, solid-state tuners experiencing the same effect with muting out (mono mode). The difficulty here was tuning into the proper station in the absence of a signal strength meter. I listened for hiss and crackles; local transmissions are always quieter (stronger signal). The FMI also produces images above and below a wanted signal, something modern tuners avoid, but the tune indicator indicates an off-tune condition to them.

With good solid bass and clean, well differentiated treble free from solid-state grain and rasp (excellent tuners like NAD's 412 excepted) I felt the Quad FMI more than justified its £30 or so basic outlay. It pulled in myriads of stations, proving very sensitive, and it separated most satisfactorily. However, to be realistic, getting it running properly wasn't without its problems, making this a project for engineers with a bit of time on their hands. The FMI is an elegant looking tuner though, and it's lovely to use as well. I hope to be able to tackle the stereo decoder problem in future.

Our thanks to:

GT Audio, tel: 01895 833099

Quad, Tel: 01480 52561

Classique Sounds, Tel: 0116 283 5821

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AN-CABLE 750	UAN-V allear pres	Eponomical 99 99% shop to com 15 shops 0.09 mm	52.35
AHEAH F300	MHVs abor proc	named 99 99% show the COAX 20 shows 0.69 mm	382 19
AN-CABLE-400	AN Ye show prov	Buil symmetrial 99 99% where the cooks 60 strands	1 174 47

AMDIO INDTE Speaker & Waveg Cables

Order Code Type/Cultur Code LAN-WIES-500 AN-8 place or red AN-NIES-550 AN-8 place orders ormog	Construction Page speaker well double sheed, screened 6H speaker well double sheed, screened 6H speaker even	6 85 12 34 25 11
U.S.+WEE-600 AM-Ediso block writing	double strend. screened 6N fitz capper speaker were smalls care 15 strend 99 95% litz silver	106 38
Janville-700 MHSPs shor	single case 20 should 99 975, let silver	387 98
JAHWINE-800 MI-SPz Brows	Seeile care 4 extendinaductor 60 strend	2 085 11

AUDIO HOTE HIGH QUALITY STEPPED ATTENUATOOS & SWITCHES

These handmarks ortunators; and switches are manufactured by a found of Mr. Londo of MJDD MDTs and manusard the text available systems consider and switches you can see any exe processing for the manufacture of 45 stages and with their Administration systems and the same and the same of launchine fill are supported. The procedure seeders are found constructed and off charming actions. The procedure seeders are found as a second processing and approximate seed with Charming actions, time in the received processing all the procedure seeders and the second processing and the second processing action act

Order Code	Type	Value	Price Ex. UK Vet
SWPT01-260	Stores Putantiamates/Afforeactor	10columns	221 75
SWITTH 245	Storeo Potentiomens / Attenuator	SEXEhms	221.75
CMTT/ 1.273	Steen Polesternete / Albetretter	1CDEChes	237 75
SWID 5 2704	Storeo Potentiametre / Altenestre	250000 MEW	262.55
CHITTIA 2708	Storag Patentiometer/Adlamation	SOUTTO MEN	267.45
Sw. C. 2100	? Channel switch	6 wer adustable	98 75
	4 Channel switch	6 - way adjustable	124.75

AUDIO NOTE HIGH QUALITY CERANIC VALVE BASES

Order Code	El gardales	Mounting	Pin Contexts	Pace Ex
VBASE-185	14-per IDIA for 3008/2A3/801A	Chassis	Floring Gold	01 25 ⁵
VBASE 180 VBASE 170 VBASE 175 VBASE 175 VBASE 190 VBASE 190 VBASE 110 VBASE 110 VBASE 110 VBASE 115	14-pm of lam 2010 / 283 / 2018 14-pm (LEA WE-type for 3008 / 283 / 2018 14-pm Lambe of lam 211 / VEA / 2045 15-pm 175 for 207 7-pm 18 for 284 OA2 7-pm 18 for 244 OA2 7-pm	Chests with beyond Chests with beyond PCB PCB Chessis been above Chessis been above	uckal Silver Silver Silver/classe Gold Silver Gold Silver Gold Silver Gold	17 25 14 75 48 95 59 95 9 75 6 15 7 85 6 75 7 95 5 45
VBASE 160 VBASE 165			Geld	8.65
VILISE-005 VILISE-010 VILISE-015	61.66, etc 9 pm 89 for ECC83, ECC88, 5487, 6350 9 pm 89 for ECC83, ECC88, 5487, 6350 9-pm 898 for ECC83, ECC88, 5487	PCS PCS Chapter from above	Silver Gold Silver	3 5 5 75 4 45
VBASE-020	6350, etc. etc. 9-pas 894 for ECC83, ECC88, 5687, 6350 etc. etc.	Chesas from above	Gotd	6.75
VBASE-025		Chasses from below	Silver	4.95
VBASE-030	9-pm 89A for ECC83, ECC88, 5687, 6390 on on. TOPCAPS	Chassis from below	Gold	7.15
following "		Fee 807 pantada et and for this purpose	e itolei we con offer t	9.75 he
Order Code VBASE-215 VBASE-205 VBASE-300	7pm for CA2 6X4, 8-pm for FL34 6550, KT66 6L66	Mounting PCB Charses with Institute Charses with shore	at .	2 55 1 45 1 85

ALTION WATE SELECTED ALTION MAYES.

Our subsects consistent from the best constability, some so and one to have for the passess strangent streament, and we supply that passess strangent streament alters and may supply that passess the passes of the passe

Outer Code	Miles Fees		Descriptor/Resolutions	Page Ex
Company Company	- Lave - pp-			10 W
- March Complete	18907 (15)	MPNL/7u/5	Santakaladia trada	2.95
		n/1-2017WS	Sacral, high gave super line neess	3 95
mit-mid	PROCESS A	HAT THE PARTY	Sweet, year law reso, less recoglisses ando vorzen	2.05
mire mad	BUTTONDI	/ ENE/ WILL	410	
				11.45
WALVE-0080	728		General Elector, MSA, double trade, low gam ECC.83	11.92
			type, exceptional secoding used in CHEAGS INTRibe	
			Shor 135000 probably boat seconding ECCRO	
1800-3188	12A17		GE. USA two exceptions version of 6072A	
W 15-00	DOD 149	72 10,099,7300	South dealer study, for recognitive	4.75
WE 739	5018		Philips/FCS USA, low encouplings & make good sound	
WYE 70	H-54, 474	3 /1729	Barrier majo versos el fin smell porteda	6.45
WEY5-0140			Philips/ECG WSA, dealth reads and spec	5.95
IIA 16-01 62			Tugodines, bost ECER7 available from now production	4.95
ANE AE-0140			dealth their USI have	3.79
AW AE-0180			dealth tends proposed US-mode, less managherry, super	10.95
ANT 45-0 180	9287 W914	- Sharen	andre .	
	Transmitter.		Basses double trade, UEX latter	3.25
FTAL			Western death tends for door	103
McGull			Shalle make and an over	9.85
MAKE 40	5587W8 S	Sphoton BSA	double tends, posselal door mad in 045420	7.0.
			ELECTR etc	10.00
MELVE-UC60	£1102£C/7	1119/7044 General	dealer made very parented driver per-reported of	4.7
	Stactor US	A	568799	
HAME-0200	BD.87 / 68	LHAS.	South tenderprotein	2.6
ALVEO D	0 B.M.	/680.5	Custon seed power pontoin	1.5
WE017	FI FI B 42	N 6805WA	small power pasteds mil spec verson	4.5
VF-1334			Soviet strail power telepide	2.4
4 F U6			Soviet 5750 power tetrodo Reposes mandares power pomissão	2.7
VALVE-040	0 6883	WITH VALUE OF	Soviet medium power televide	4.5
MVE-042		wort and	Sortal, reading power totrode, stendard from	5.5
		/FL34 For Buff!	Soviet power telrode	8.8
VALVE-044			Sovide power periods	6.4
WILLIAM OTE			power books, Audio Mich branded and hished to our	56.4
VALVE-048	0 3000		specification, Chinese manufacture	30.7
			Specification, University Institutional Property and Prop	29.4
VALVE-050	0 1/721	1	power tends, Audio Nata barried and tested to our	27.4
			specification, Chinese manufacture	33.4
VALVE-052	0 MH84	15	power made, Jurilo Nate Intended, tested and med	22.4
			Chinese misse	
VALVE-054	0 6033		powerful flatton medicapitato indicarly heared	24.6
			Inode	
VALVE-056	0 MSZ	16080	story Resear regulator collectly heated stude	6.4
WLVE-0580	263.4	ion or Box litt hade	deadly heated shall power words. Owners mode	17.5
114.4.4.201		nations, Second Aut		
	Sept.		22.03	
VALVE-060		- Benner	(fleetfar	3.2
AVEAL-093			Marchine .	27
		Selvania	H-oofin	3.5
ANTAE-OP-	N C234	/5/d4 Page	If colfe	8.7
VALVE-OAL	N 6634	/ SNR4 REMANDE	I UPeff	49 9
VALVE-071	JU 6/34	VETISTY Melica	INTERNAL CONTRACTOR OF THE PARTY	9.5
VALVE-07	50 653)	Arazig Memor	off-section equivalent to 6232/34 but before	y :
			transless	24.5
VALVE-07		HGB Colvon USA	Very powerful Iff-receffor, 2 500volt at 100mb1	
VALVE-07	60 634		III vecifier very good for pro-coapitions, 7-yes base,	. 3
			Byssian reverse pan version	
VALVE-07	80 6X5		HT-actifies for pro-amplifiers & power amplifier front-mids, URS bose, forcom made	40
2.6.4.	-		frantistifs, USX base, Russian media	

Flores usin, on 300% yer remarkational of both Digmy-Nephrone, but can be the in-house eather out outloop conditions to presention seemed to condition of the condition of outloop conditions. The condition is the condition of th

permanent consider that when you plus your project or receive your existing carefiller.

Name of the control to stack the enter \$17 cmps of all the alliment enters of surrows that no stack, many the next house of time cubins which we extraored county; so as also we have street where their \$10 cmm; and was \$31 \text{ Miles of subary to be lower upon \$10 \text{ Fig. them is stack the counter has particularly different properties in the finance and houseant has relative can be usy have stack contains under \$4\$ works.

We have the stack of the stack of the stack and the stack of th

The 1/2 work Shakah tentulum receives on non-magnetic and cost £ 2.26 and

Some values are evaluate as 1 want from Shatlach at £ 4.60 each list of stack available

AUDIO NOTE 1/2 WATT TANTALUM RESISTORS

With our philoson storage of transform necessary accessing of the tone and Standard Incorrang laws and been able to a guidy, we how found in accessary to remain-fracture to 1/2 user when a collabor to the collaboration to t

The 1/2 watt hade Note tunnium reasters cast £ 1 99 each

AUDIO ADTE 1 WATE TANTALIAM RESISTORS

By to see the taxabless like resistors have been contently difficult to get, borrows, of the mode personance and quested assumes questive generation have been both that S is the resulting resulting property in some law group of S is the personal property in the resulting p

Firstly to complement the range of Audio Note 1 ways tentralism necisiars we have started stacking a levised number of 2 worts, normally, 1 Mag. 1 MS and 2 Mag.

The AUDIO NOTE 2 work 1% tentulum resisters cost £ 5.65 each

We shall now be weating an getting a fuller 2 west range and start stocking the 3 West tentalism reasons as well, and who takes pushage we will be able to build complifiers in a year's free dust bow all business reasons as all parts of the cross?

in authors in the pre-comment families season, we are going in thick is mapp or pressure, profession (and in requires, in many cases the coll will require the profession for the coll with the comments in most or an experience of most of most or wanter. When the collection of the collection is the first or most of the collection of most or wanter fine the collection of t

They cost for the 1/2 west \$3.30 each 1 west \$4.85 each 2 west \$6.89 each

hostable in the E12 maps of values, the 1 vect cost £1.43 each spills with C42 was believed to the E155 COS. In a new times with out officing in ange of 2-15 will vect-voxed seasiles, we shall be starting with a small range and expectably the vector of spills of the removant the following is credible), all these receives my 5% believes and officier.

1650-67 01 2 1 1 1 1 1 1 1			
Order Code Wattage	Value	Security	Proce Ex LIK 1
855-0328 .6 well	472	5%	Ü
855-0330 & well	1002	5%	0
BES-0346 6 wolf	470R	59	0
855-0360 6 well	1 10	5%	0.
BES-0369 6 worth	2112	50	0
RES 9:80 6 well	150	50	1
BESOIST & well	20E	51	
855-0307 9 wall	1008	51	1
RES-0284 9 wall	185	50	
Manuel P. Harris 200	IDI	50	1

PRESERVOIR THE PROTECTION FOR MUCKEGATE CAPACITIONS IS A GUIDELINE GROUP, DUE TO THE COMMITTEE OF THE ADMINESS FEW, IT IS INFOSSIBLE TO PRINT UP-TO-DATE PRINCES MIGHT TREES AND ATTEMPT OF THE ADMINESS FEW IN IS INFOSSIBLE TO PRINT UP-TO-DATE PRINCES MIGHT TREES AND ATTEMPT OF THE OFFICE AND ATTEMPT OF T IS OF THE MANNESS YEN, IT IS IMPOSSIBLE TO PRINT UP TO BATE PRICES MIDNITHLY

ndor Cordo	Value	Voltage	BG-Type	Recoveremented Use CRC Visit	Price És
AP 9000	47mF	25valt	PE	legillers	1.6
NP-9005	33mF	35volt	15	Acyuhass	17
M-9010	Q 47mf	50velt	PK.	Jayahara	10
AP-9015	Inf	50velt	PE	Arryshare	1.1
MP-9070	2.2mf	50 clt	PE	Jaywhere	1.7
AP-9025	3.3HF	50valt	PK .	Apywhere	13
AF 9030	4.7mf	52velt	- 15	Argehere	1.6
MP-9035	I Omf	50valt	FK.	Arryston	1.8
AP-9040	22mf	50velr	PE.	Anywhere	2.6
AP9045	272=nF	1 świt	5-50	Anywhere	2.8
AP 9050	33 mF	1 limb	Standard	Jayahara	3.4
AP + \$55	47mF	1 firelt	Standard	keyehara	91
AP-9060	330wf	1 (vol	Standard	Accyclare Accyclare	100
AP 9045	1 Oraf	50 vult	Standard	Appropries	2.5
AP 9070	47mF	50valt	Constitut	Approved the state of the state	- 11
AP-9075	100mf	16velt 50velt	Canadag	Anywhare	5.4
AP-9080 AP-9085	1 00mF 220mF	50ven 50ven	- Journal of	Appelue	
AP 9090	1 Ower	1 DOwn	Standard .	Approhes	10-4
AP-9095	77mF	100vah	Charles	Appriors	6.3
AP-9100	47mF	100valt	Created	Anyohere	1
AP-9105	IDOm/	100vah	Change	Anywhere	7
AP 9110	210m	100valt	Stanfiel	Arcelon	121
AP-9115	1000eF	16mit	Challed	Assystem	81
M-9120	1000mf	50valt	(Arrefuse	24 5
MP-9125	220mf	1 évolt	Stendard	Jayohara	4.3
AP-9 130	470mF	T Swalt	Creation	Jeyologo	- 6
M-9135	2200=≠	1 Svelt	-	Acurban	134
AP 9140	10.000mF	80volt	Smith	PSU smoothing	234.
38-9145	4700=F	16-40	Committee	Arrovhuse	140
AP-9150	47mf + 47ml	500volt -	S&z-Type	PSU filter concellor	85
		550v 900			
CAP-9155	100:1F +100:11		SEPTYPE	PS beautigracitor	101
			557v suga		
CAPI9160	IO0mF	500valt	S\$2-7 po	PSU filter capacitiz	72
			550x surge		
CNP-9165	220mF+ 220	ne 350volt	SERTIFO	PSU filter capacitor	92
				400v surge	
CNP-9170	100mf + 100m	of 350volt	SIZ-Type	PSII filter capacitor	75
			400v surge	1 444	100

CAP-9180	47+47mF	500sult WKz-Type PSU Mor capation	159.85
CMP-9185	State .	Silverit Witz-Type PSU false capacitin	144.55
CMP-9190	100+100mF	350- WILE-Type PSLifferengenter	151.74
CAP-9195	220+22unf	400's sec. 350: Wile year PSU Mor capacity	181 95
CAP 9200	72mf	400's suit 8 35 b VE-Functions can as filter capacitor	18.15
CAP-9205	150mF	350mb VX-Type PSU-lifter counsitor	41 23
CAP 921U	0.47mF	Shart F-Typelow FSR, Lew cranditure use easy	11
CMP-9215	22mf	6 Teach F-Type As above	1.72
GP 9220	IO3mF		1 56
CNP 9/25	720mf	6 Fligge As in	676
CMM2/0	2230	6.3 milt F-Type As above	
CAP 9235	47mF	16 all: FE/republic four ESE ventors, comparable to Mi	1 113
C100010	100mF	16 cch FE Typeliko kue ESE versus campanish to file	13.71
CMP 9240	TOUR	CORP. LE L'ÉTATION DES L'AN ANOMINE PROPERTY AVEN	
CAP 9245	220mF	1 detail: FE-Typoiding line ESR vectors, comparable to file	19.95
ORINZAS	Stome	CODE	
GNF-9250	100mF	25 rolt FE-Tipo As above	14.28
GAP-9255	220mF	25-suit FE-Type As above School: FE-Type As above	21 43
CAP-9260	100mF	Sthell FE-Type As above	15.71
CM 1215	1000mF	SOught FK-Type As above use seryohare	58.71 55.71
CMP-9270	2200mf	35 colt FE-type As above one onlychical	101.43
CMP-9275	7200mF	130 volt FE-Type As above use emperature 100 volt FE-Type As above use crossfore	32 85
(AP-9280	100mf	100 valt FEType As allows use considere SOugh CTypeFor cazalis with DL patential differ	
CAF 9285	2 2mf 4 2mf	50-uit C-TypeFor crosss with DC potential differ	mare 3.35
CAP-9290 CAP-9295	A mark	SOuth Burnerfor Inchroecker crossover national	17.65
CAP 9300	1 limit	SCheele Baselos de salacres	16.85
CMP 9305	72m5	Straft Banker et abern	23 %
CAP 9310	47-9	Chair Reeler at above	3 95
GAP 9315	0.47mf	50volt BC-Itx Type For PSU decompling	12 35
CMP-9320	220mF	6 Sada BG-Hz yearfer super less noise PSUs	11 85 24 65
CAP 9375	100x#	Youth BGN TypeFor super low name PSU's	28 95
CAP 9330	47(a)(f	16 mb BGH Type on obers 35 ms BGH Type on obers	710 45
CMP-9335	4700=	School: 8G-N Type: Us shows	5.45
CAP-9340 CAP-9345	4.7mf	SOvel BG-N Type as obove	6.65
CAP-9350	10mF	SOugh BGH Type es above	7.55
CAP-9355	47 ruf	5Ovall BGH Type as obeve	13.75
CAP-9360	100mF	50volt 8G-H Type as above	20 35
(AP-9365	1000mF	50valt BGH Type as above	99 95
CAP-9370	2200mf	100mit 8GH Type es obove	423 35

In our companies that your will find a latting of all revisions stack (our cytion, begains there exists) beyond companies, our sample is every of more manufactly presed companients, sell genetic quality, our control of any late of the Childrick Powland England England England in the Childrick Powland England England in the Childrick C

Order Code	Yolke	TO	100 USB	Linfa CY
HE Vot			1000	
(AP-9740	10G+100mF	350 + 0	Power sum (Trailing	19.95
CAP-9750		31 will	Power States	21 5
CAP 4 (0)	Allen	Si val	Power summer state of	12.95
Cue ell 10	4 -470 45071	SUT will	Power seasor training	19 95
(18/9038)	+100mf	500 vsb	Pour suit fluits	29 95
(18.02) 6	I WEN I	500 valt	Primer passer finances	29 95 29 95
	111×7/04	MEN 1500 volt	Power sounty Bharma	39 75
CYD 1120	WITH WALL	500 valt	Power State of State of	34.95
		100 valt	Paula saudy filteras	34 95
CMPSED			Bullet States	4 95
CNP #530	4,/0000	6.3 volt	Bent market	4 95 2 95
CAP 1670	100mF	100:sh	Marie miles	195
CMP #550	Tuffref	50 valt	Different annual	0.05
CMP 4640	EL 100	100 voli	Digues convolues	8 95
CAP 9560	220mf	50 volt	Bytame paywhere	5
CAP-9570		50 volt	Mysbare	5.55
CAR-95WD	22 mF	50 valt	Arreton	1 15

Order Code	(market)	Construction Price Ex	if the
Shuttlen.	10 = 0 Stores, logi	Franchips, PCB macraed	495
SWITCH210	10740 Stores logureret	Episterial type, PCB mounted	18 65

A lease of numerous is the UD-DA column controls which can used an procurable for the 4th N-T-labs.

1870-to. and is a more version on the injust on the NEED, LASSO EEGON and GALUES, those very good transfer, park by one of the Column park by one of th

SWITCH-271 SWITCH-272 SWITCH-273		no logarilist no, la ses esc no la sestant	Encormists Large Enco Large Error	dend and has not		32 25 70 65 07 45
Order Code	-		Construction		Price Ex.	UK Yer
SWITCH-205 SWITCH-2111 SWITCH-274	100KOhm 100KOhm 100KOhm KO	1-O ⁶	Enterpolited	PCB mounted hype PCB meaning L PCB meaning		5 45 19 25 32 25
STANCAS TYPE Order Coup SHITCHCO SI SHITCH TO SI	1990	Feality 6-way, 2 channel 6-way, 2 channel	ndjerobio esperobio	Construction PCB meeting PCB meeting	Pice Ex	UK Val 5 95 30 65

E = C = Sender Gold play = 12	PADD EX. UK Vol AN-C Gold plus AN-GP AULIO NOTE gold plug AN-P AULIO NOTE Sold Shor	155 play, follow married, assemp	3 45 8 51
25.51			

Type IKA secker rector plated IKA secker rector plated IKA secker rector plated AACS AUTO NOTE non-magnetic rector, gold plated	Mounting Price Es Cheers meanful Cheess meanful tulion coalated Cheess meanful	04' 04' 06' 34'

BNC Flags & Sockets Order Code Type COMMISS Standard BNC plug

LONGS I	ing 3810 brief 2000 patter seasons		2.00
Banana Plays, I	autopaker Catio Spales. Chasse Levelpooker Terrarels.		
Dudos Codo	e Es UK est you Occurren	Pice Is	Evet 245
CONTRACT	A) in G(() house plus, gold plant, tyring looded teason A (()) Leadmantin (plin spain, along plant), non-magnatu		4.65
P 201 7	AULUS) NOTE ANST Speaker Territoral chasses mesons, racked photo- aurus war E and C I'll Speaker Territora, chasses mesons, gold photol and o	bfork	2/5
	ALUNO HOTE AN-STR Special Terrains' charas mounts hely gold non-magnetic and or black	plated 1	475
C0N-015	Gournal Territoric chasses resourced and sockel plantil I		1.45

FERRUTE BINGS

ORDER COSE . CON-018 AUDITOR CONTROL C

Order code Price Ec. UK		Celour o	ode Physory/Secondary mediunous - Am	m U
TRANS-465	117687	(Insur-	3 & 12 thm - 103 Ohm, capper wood (60 medium)	51.5
TRANS-470		Red	15 & 600m - 10 moves, cooper wred, ME matching	51 5
TRAUES-460	117490		PC married 1111	
TRANS-455	177691	Green	15 g 6/hm	78:
			that many til numbers	
TBU/5-450	117692	Blog	150 & 600 abov 245 & 1040 bm, copper word high	78
TRAS-475	177693	Violet		78.
			mathem	
TEAMS-410	177494	Village	150 - 1500 km copper wood High Quality hor	01
			residing	
10x15-415	17749411	Clear	150 - 6000hm capper sweed High Quality line 1	01
			politing	
TBAKS-420	117495	Sher		378
TRANS-476	177696	Block	3 & 12thm 10010hm shee street MC metrics 3	178

The law matching transformers can be used in a marshar of application, other-component cylinics and matching (as we recommend between CD-Player and pro-complient, to seponds earth planes and IS

We find around this ways in calcula must hypes as we go and out? Omes So. We have decided to fill be not find two contained domes. That we use for production of the ONE/SOR/ONE, coping of life careful hardy of DIT products. Omes is not interest, official a more? Some in the second of the cold only will find course that we show various for products to record times on the family. For yell the delight into rest of more of a finding to the the record of the cold of th

Order Codo	(gi	NAME AND	Page Ex 16 Her
1 5e	0-1	10,000	⊈ 84 50
	Chassis 1 Copper	4 73 = 1 25 4x 1 2 4 73 = 12	£ 69 50 £ 198 50
Cut will live	Communication of the Communica	4x x y Obs	£ 165 50 £ 78 90 £ 116 70

AUDIO NOTE COMPLETE DTS

As manifested order on on developing a range of complete US; in just fitter of you while how the shallow, but it is easily to the fitter of the confine a wayed that the primary is to speak, begand the con-traction of the confirmation of the confirmation that have been also be good from creative with one to all your supplies and comproposes, all the laters upon entires contract to drive use of a might survival fact. prove supplies and comproposes, all the laters upon entires contract to drive use of a might survival fact. (Polypow door 1).

The AUDIO NOTE ICT O-IE

Based crowd the party famous 2000 dractly hasted reads we see this lat or the attraffiction by faulty amountments or covers of the experient expects of dumps recovery, for an facility by Feedback, Claim A, Beachy Housed Fredn to become a member of this exchange clab of any party of the contract of this exchange clab of any party of the contract of the sections of the contract of the sections of the contract o

Go One has no 2008 per decimal entering at 470 other 477 feet course group 9, 10 other 41 decimals group you are found to the feet to the

IOT ONE ORDER CODE AN-KIT-001

Price £ 599 00 mcl. Vct. endudes volves, but not postage/packing, cover a extra at £ 99 00. With pullabed chosen classes and channel believels on the tensionness £ 799 00.

IST TWO ORDER COITE AN-EXE-OGS

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DIT THREE OF HE COME ANNOTAGOS

TOT FO OR THE COLD A 40T-004

The AUDIO HOTE Pre-American Kir.

Viscon programme of the composition of the sendered where to have some party of unch to program have not rest developed provide to a solidary the industrial projects and foliation by proposed unch make the control of the control of the control of the other hand the foliation to the proposed unch the control of the co

L. O. LIE UTO Let. of C. Pascock in rul Sp. Lyan Class 125-127 Douglas Miles BIS 156, East Control Confund February 01273 220511/6 Inst. Sm. 01273 731476 Direct line to sales 01273 770778 UT) Ent. or C. Peacock have not fine. Lyon Class 125-127 Dovigiles How

HOLLAND phase contact, do long Components, Longfurhambout 11 NL - 5605 LV Engliseen Internal, Tel. 040 257 4744, Fee. 040 257 4944

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PEN BAFFILIES

Prompted by a reader's letter, Dominic Baker produces a theoretical design for a passive open baffle loudspeaker.

> Dolphin Square, London.

DEAR Hi-Fi World.

I am a regular purchaser and reader of Hi-Fi World (every

issue so far) with a particular interest in DIY articles and ideas.

Your recent article describing an open baffle sub-woofer is of interest to me, as I wish to build something a bit similar. Some time ago now I bought a pair of Audax HM170Zo aerogel bass midrange units from you, with which I have been experimenting. I now plan to use four of these units per channel mounted in vertical array on an open baffle, to cover the frequency range up to about 400Hz in an active loudspeaker design which I am working on.

This will use a Linkwitz type active filter (fourth order Butterworth). The actual crossover frequency is 420Hz. The baffle width would be similar to your sub-woofer design, so I am assuming that the cancellation roll-off effect would set in from below

200Hz, at -6dB per octave, again as in your design.

I wonder if you could help me with three questions. With the units wired in series/parallel (to maintain the same, 8 ohm nominal input impedance as for a single driver), what gain in efficiency could I expect from the quadrupling of total-radiating area? Would it be approximately +6dB, or more? (The more the better, as far as I am

Related to that, and given sensible usage with predominantly classical and jazz programme, what is the maximum electronic boost (again in dB) that it would be prudent to apply at low frequencies to the four driver array? I had in mind somewhere between +9dB and +12dB, which would extend the 'flat' response down to about 70Hz or 50Hz, respectively, assuming roll-off at -6dB/octave from 200Hz. I would be happy to incorporate a 'bottom end' filter to roll off the input signal more sharply below the driver resonance frequency, in order to reduce displacement and distortion at very low frequencies.

Lastly, can you suggest a circuit which would be compatible with the Linkwitz filter circuit, and would achieve the required bass boost? I ask because I have to hand a circuit and equations - Linkwitz again - for step boost of +12dB per octave with

variable turnover frequencies, but not for +6dB per octave boost.

Perhaps I should just add that I plan to use the four Audax units in conjunction with a Lowther Voigt PM5a(f) wideband mid/treble driver, loaded by a short, tractrix profile midrange horn, above 420Hz. Hence the interest in high efficiency, and the attraction of this specific multi-driver configuration below 420Hz, as the effective moving mass would be comparable to that of the Lowther unit, with a better chance of achieving seamless integration. I am more concerned with optimising the midrange and lower treble performance than with extracting very deep bass.

Brian Wadsworth

You're about to open up a large can of worms here, one that'll require a lot of experimentation to get the best performance. Using four drivers, two in parallel then the pair in series gives the same impedance as a single unit, which as you say keeps things at a nominal 8Ω . Because you have four times the cone area though, you will see an increase of 6dB output.

That's the easy bit. You're going to run into phase problems though, where the distance between the drivers is close to the half wavelength of sound you are using them at. This will more than likely cause a lumpy, phasey lower midrange response, something to be avoided if you want a coherent sound. Also, applying +6dB/octave bass lift to a 6" driver, even though there are four of them, is going to push them close to their limits. Basically, I think you're going to struggle with this arrangement, and that's before we even consider the electronics.

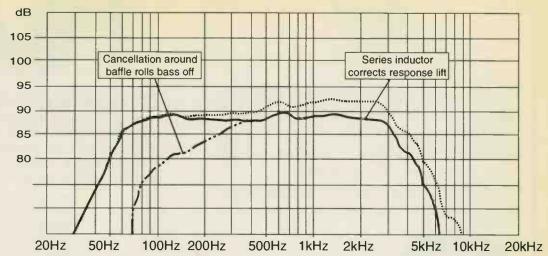
For this reason, I'd like to suggest a slightly different approach, one that'll be a lot simpler to build. The bass of an open baffle relies on serious cone area and high power units capable of really shifting air; I'd use a pair of the 13in. professional Audax

PR330M0 bass drivers for each channel as part of a three-way system on a 450mm wide open baffle. These, in parallel, will draw more current from your amplifier (use a good solid state amplifier and it'll still be able to drive them easily enough though) increasing apparent sensitivity by 3dB. It does this by halving impedance and doubling the amount of current drawn, but a dipole is inefficient anyway, so even if you went the active route you'd need a powerful amplifier. Doubling the cone area by using two per channel adds another

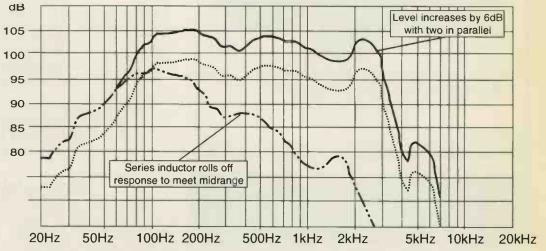
This 6dB on top of its 98dB sensitivity gives you a massive 104dB to play with. Why? With this much sensitivity you can afford to implement the 6dB/octave rise towards low frequencies with a passive circuit, making this system much simpler. Use a series inductor to apply 6dB/octave cut above 60Hz. The effect will be a response that rises at 6dB/octave from 350Hz down to 60Hz, countered by the 6dB/octave roll off of an open baffle.

This combined response should be flat from 350Hz down to 60Hz, with a -6dB (bass cut-off) point of 30Hz. Above 350Hz the response will continue to fall at 6dB/octave under the effect of the inductor.

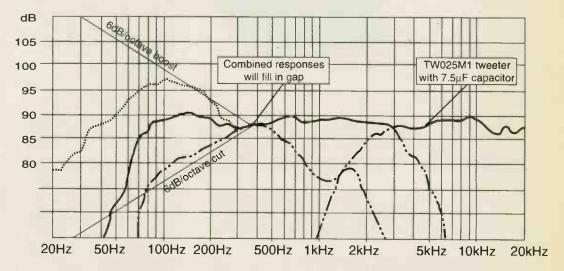
You could then use your HM170Z0 drivers for midrange, one per channel, with a simple series inductor to flatten the response and give a 1st order roll-off characteristic. Around 1mH should be about right, but if you want a slightly softer



The original frequency response of the HM170Z0 driver rises with frequency. This can be simply corrected with a series inductor. Mounted on the open baffle, the lower response will roll-off due to cancellation.



Hovering at around 97-98dB between 100-300Hz, the PR330M0 is a very sensitive bass driver. Using two connected in parallel increases sensitivity by 6dB; +3dB from the doubled cone area and +3dB because connected in parallel they will draw more current. As with the midrange driver, a series inductor will tilt the upper response downwards. This time we are looking to produce a 6dB/octave roll-off rather than a flat response though.

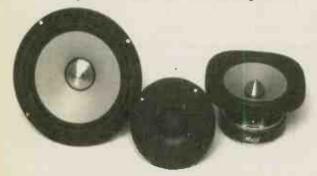


With bass and midrange on an open baffle you can see that the 1st order roll-offs will combine well to give a smooth (predicted) response. The 6dB/octave rise through the bass is cancelled out by the 6dB/octave roll-off caused by cancellation around the baffle, resulting in a flat response. The TW025M1 soft dome tweeter needs just a single capacitor forming a 1st order crossover to get a smooth response, so this could be a good choice for the top end.

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even fully assembled amplifiers for those who cannot wait to listen to them.

The Riverside 4040 is our integrated amplifier. It features dual mono construction and has five line level inputs and both 40, and 80, outputs. The output stage is configured in the classic Mcintosh connection, which gives stable, wide-band operation even with difficult loudspeaker loads. The stainless steel chassis and transformer cover are hand polished to a mirror finish, and come with a semi-matt black valve cover. 4xEL34, 4xEC38, 2xECC32, At 10 description, including circuit diagram, is given in the 4040 reference manual, £5.50. Kit £780, hilly assembled £995.

Technical specification: dual mono construction, 40W/channel, 12Hz to 25kHz power bandwidth, distortion <0.1%, five line level inputs, tape output, 2300/240V mains input. Stereo amplifier circuit board: board only £9.50; component pack (including valve bases), add £63; populated board £125; full valve set, add £45. Power supply board: board only £9.50; component pack, add £44; populated board £66. Input board: board only £15.50, component pack, add £16; populated board £33.

The output transformers are configured for the McIntosh connection and have excellent for

he output transformers are configured for The output transformers are configured for the McIntosh connection and have excellent low frequency response and a primary reflected impedance of 3800Ω. Full connection instructions provided. Price £70. The mains transformer is wound for dual mono construction, as this gives superior isolation between channels which sharpens imaging and eliminates inter-changed cruyed loops in the between channets which sharpens imaging and eliminates inter-channel ground loops in the amplifier. Primary 0-230-240V. Secondaries 2x295V@0.25A (0.4A int.), 2x70V@30mA, 26.3V@5A. Price £50. Other primary voltages can be supplied to special order. Data sheets giving connection diagrams, specifications, as well as circuits for using each transformer, £2.50 each

each.

The chassis, comprising main chassis and transformer cover, is hand polished, welded 1/16" stainless steel - NC machine tooled for a perfect fit and clean finish. Each kit also includes a mesh valve cover and baseplate, finished in

semi matt black. Price £310. Also available in mid steel finished in black. £195. For those who wish to use one of these high quality chassis for their own projects, details of the chassis are given in the 4040 reletence manual, £6.50.

Connector kit: twelve gold plated phono connectors, two sets of loudspeaker terminals, an IEC mains socket with integral fuse and switch, and an IEC mains lead with fitted 13A plug. £51.50. Cable kit: all cables required for the 4040, £6.

The Riverside P2 phono preamplifier is

plug. £51.50. Cabe kir. all cabes required for the 4040, 26.

The Riverside P2 phono preamplifier is designed to partner the Riverside 4040 for those who enjoy the vinyl sound. Equalization is provided for moving magnet output to line level. The P2 features a high accuracy feedback RIAA equalization circuit, ensuring a natural tonality, a regulated high voltage supply per channel and cathode follower outputs. 3xECC83, 1xECC81, 2xECP80. Full details and circuit diagram in the P2 reference manual, £6.50. Kit £225, fully assembled £275.

Technical specification: 47kΩ input impedance, 1kΩ impedance output for driving long interconnects. Stereo circuit board: board only £25; component pack, add £37.50; populated board £70; full valve set £20.

The mains transformer is wound for dual

The mains transformer is wound for dual The mains transformer is wound for dual mone construction and is toroidal for low leakage flux. Primary 0-230-240V. Secondaries 2x295V@20mA, 2x6.3V@0.45A, 16V@1A. Price £30. Other primary voltages can be supplied to special order. These transformers are also suitable for power supplies in preamplifiers and other line level valve circuits see data sheet for details, £2.50.

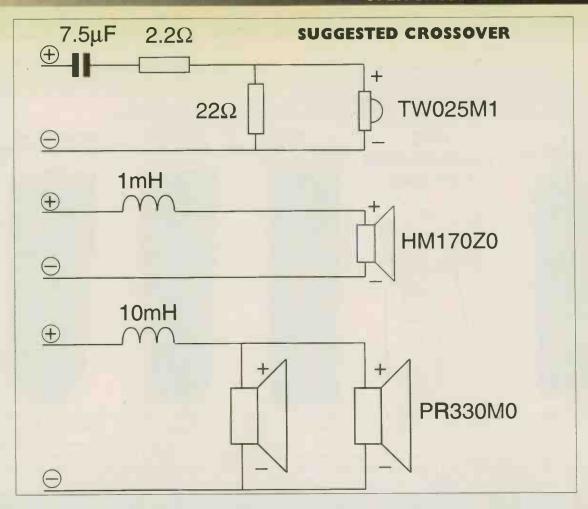
The chaesic final nesses and transformers are transformers.

see data sheet for details, £2.50.

The chassis (main chassis and transformer cover) is made from mild steel. Each kit comes complete with a mesh valve cover and baseplate, finished in black. Price £110. For those who wish to use a high quality chassis for their own projects, details of the chassis are given in the P2 manual, £6.50.

Connector kit four gold plated phono connectors, IEC mains socket with integral fuse and switch, and IEC mains lead with fitted 13 A plug, £15.

and switch, and the mains about plug. £15.
We normally ship within three working days. If we do not have the flem in stock we will advise you of expected delivery and confirm before despatch. P&P (in UK): £2 for each part of £40, maximum of £10; manuals free of charge. Assembled units despatched by courier free; courier service on other flems £10.
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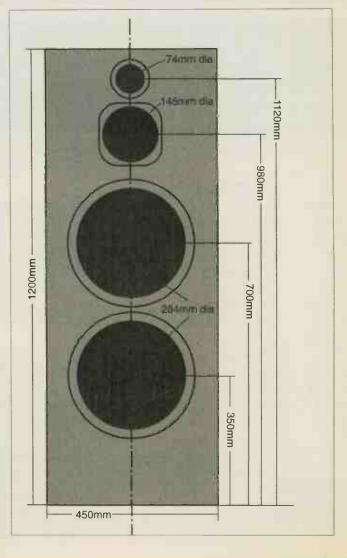
presentation, try upping this to 1.2mH or so. This should match nicely with the TW025M1 1in. fabric dome tweeter, which flattens out very nicely with a single capacitor 1st order filter, allowing it to match the midrange well in terms of phase. Such a simple crossover should give an excellent sound too. The tweeter will probably need about 3dB of attenuation, but this can be easily implemented with a 2.2Ω resistor in series and 22Ω across the driver's

terminals.

Because the response of the HDA midrange driver will also be rolling off at 6dB/octave due to cancellation around the baffle, it should match well with the bass end.

This is only a suggestion, and as I have not built one I can't guarantee it will work. But there's definitely potential, and it should produce an excellent sound being so simple; no cabinet and only simple 1st order crossovers. DB

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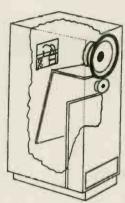
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K5881 MKIII VALVE AMPLIFIER

Our K5881 20watt valve amplifier now uses a new S.R.P.P. triode input stage, explains Noel Keywood.

Ideveloped our K5881 kit valve amplifier from the Mullard 5.20 circuit many years ago and it has been a delight to us and hundreds of users ever since. Although pure Class A, which can run hot, K5881 has proven wonderfully reliable. It's always been popular because of its reasonable price, coupled with fine performance and low maintenance costs. So why change it?

Predominant comments about K5881 are that it's 'difficult' to build because it does not use a circuit board, that it is of surprisingly high build and finish quality for a kit, and that it has a fast sound with plenty of treble and bass. I've always thought of it as a "bouncy sounding" amplifier, that is, fast, detailed and with lively bass.

What were we going to change? I've opposed moving to circuit boards for simplicity of build. I am not at all certain that the sort of person who needs to build by numbers should be tampering with a valve amplifier like this. K5881 isn't a toy; it has 450V on the H.T. line and we actively discourage people from buying if they have no experience. Furthermore, hard wiring is better in terms of sound quality and easy for a constructor to modify. When we do a real budget amp. then we will use a circuit board, but the chassis work will also be far less expensive than K5881's welded 16gauge steel affair.

We decided instead to hone K5881's sound quality by making it smoother, more neutral and more valve like. In my original re-working of the Mullard 5.20 I discarded ultra-linear operation in the output stage, finding that it wasn't especially linear at all. We have the benefit here of using a fast computing distortion analyser that shows harmonic structure and how it changes with level. My whole basic approach to amplifier design is to optimise open-loop (i.e. no



feedback) linearity, then close the loop, using feedback only to tiddle up final results. Feedback skews an amplifier's transfer characteristic and ultra-linear working commits this sin.

A well designed amplifier should offer at least reasonable results without feedback. You might not be surprised to learn that transistor amplifiers are unable to meet this criterion, whilst a highly optimised design like our 300B needs no feedback at all. Like 300B, I ensured good linearity with K5881 by running it at a high 450V H.T. and using relatively high impedance output transformers. Under these conditions ultra-linear gave worse results than simply running the screen grids a few volts below the H.T. line. Some advocate running the screens from half H.T. but this only reduces output power and increases distortion.

Most valve amps run from low 350V H.T. lines so cheap electrolytic capacitors can be used, these items being a major cost in any valve amplifier. K5881 was never meant to be a cheap amplifier though. We use a massive 5H choke in the power supply in conjunction with a special twin 50µF+50µF / 500V electrolytic in classic π filter arrangement. In my view this arrangement incorporates the best of choke-input and capacitorinput power supply arrangements, being effectively a compromise between the two. It pulses the mains transformer less than a pure capacitor input type (which all transistor amps use and which the EC are threatening to ban), whilst offering excellent smoothing and regulation. It

avoids the hum fields, mechancial buzz and voltage drop of a choke input filter too.

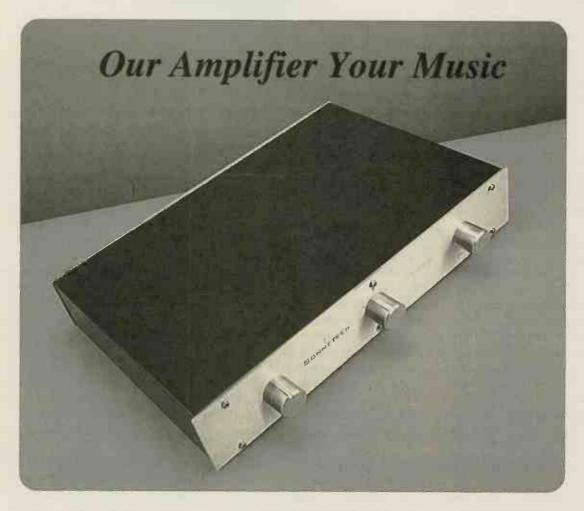
In my original circuit the EF86 input stage was strapped to run in triode mode. We decided that, in light of experience, the Shunt Regulated Push-Pull stage based around the 7025 double-triode (high performance ECC83) valve would be a good upgrade for the front-end. The Japanese swear by SRPP and, with this valve, I must say it gives superb results. This front-end change has eliminated the bright and treble we were getting with the EF86, bringing a smooth neutrality to K5881.

After finding, from our 300B, that lowering feedback increases the sense of air and space around images on the sound stage, as well as lessening that dry, clinical presentation that is the bane of transistor amps., I decided also to reduce feedback, in so far as this might be possible within the limitations of using output tetrodes. That's why I again spent a lot of time ensuring K5881 was as linear as possible without feedback applied. Feedback was introduced only to maintain bandwidth, set to -1dB at 22kHz. For this I found just 18dB was needed, a reduction of around 8dB from the previous design. Sensitivity has increased to 75mV for full output (20W) whilst distortion remains around 0.1% at full output. The sensitivity is so high, a preamp is not needed, just a volume control.

As expected, lowering feedback opened out the sound and made it more

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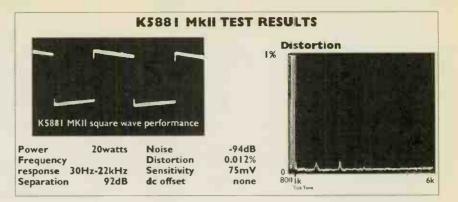
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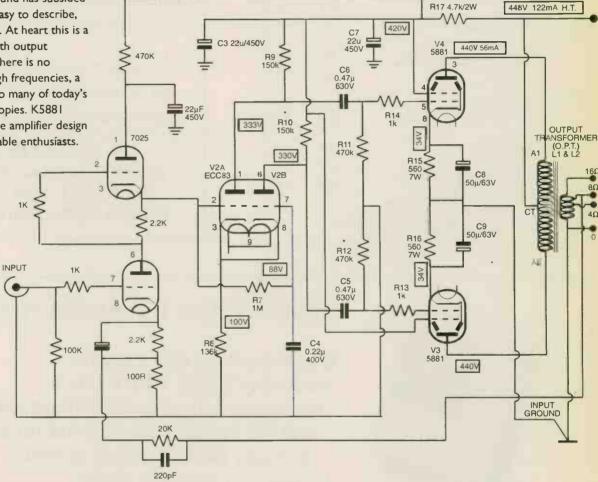
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valve like in terms of spaciousness and ease of presentation. This last property is difficult to describe. Some people call it liquidity, a not inappropriate term. Music flows more easily and naturally; it sounds less 'clinical' or 'forced'.

Overall, the amplifier has changed considerably in its sound. It has swung from being distinctive to neutral, which is what I wanted to achieve. There's a better sense of insight than before, plus greater openness and clarity. Curiously, the amplifier's actual sound has subsided so much it isn't really easy to describe, but I'm happy with that. At heart this is a very linear amplifier, with output transformers so good there is no slewing or ringing at high frequencies, a problem that affects too many of today's thermionic "me-too" copies. K5881 remains a first rate valve amplifier design suitable for knowledgeable enthusiasts.





K5881 Mkll Sound Quality

I souled out to start K5881 off with Marvin Gaye's What's Going On? My tapping feet told me this inherently warm, rhythmic recording was having little trouble making it to our KLS 3 loudspeaker intact. 'Right On' had nimble bass guitar joining with sweet percussion to move the music along. Imaging was stable and detailed, the zither that appears at stage right on this song placed clearly in the soundstage, the feeling of space around it adding to the realism of the performance. Vocals were smooth, flowing naturally with the melody and possessing realistic body and substance. Triangles, drums, bass

guitar and vocals knitted together in 'Inner City Blues (Make Me Wanna Holler)', emphasising K5881's smooth, organic delivery.

Musicality and emotional communicativeness featured high on the sonic menu with Rimsky-Korsakov's Scherezade. Strings were smooth, as was the flow of the music, clearly painting a picture of Sinbad sailing across the sea. A nicely proportioned soundstage gave the various sections of the orchestra plenty of elbow room, increasing the sense of involvement with its openess. Raising the tempo in the fourth movement proved K5881 no dynamic slouch, crescendi building

impressively on crashing cymbals, powerful snare drums and thunderous tympani.

More heavily processed music punched cleanly out of KLS 3. Upper bass caught leading edges of drum machine notes well and gave synthesisers their full measure of pungency. A valve warmth to the bottom end played a part in giving bass lines weight and an easy foot-tapping quality. K5881's transparency also helped make whatever was coming through it comprehensible, an ability appreciated on thick Rock mixes, where insight stopped the music becoming confused. Jon Marks

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Loudspeaker and Headphone Handbook

reviewed by Dominic Baker

inding a reference book that covers all areas of loudspeaker performance, from design and manufacture to the acoustic interaction within a room, ain't easy. It's even harder to find one that's up to date and thorough. That's the problem editor John Borwick has tried to address with the Loudspeaker and Headphone Handbook, enlisting the help of top industry experts along the way.

Before I go any further, a word of warning. The Loudspeaker and Headphone Handbook is not a gentle read on loudspeakers. It is more of a technical manual, many of the sections launching into quite complex maths of at least 'A' level standard (integration and differentiation). Enthusiasts without the maths to understand the equations shouldn't be put off though, the chapters all provide plenty of easily digestible reading material.

The Loudspeaker and Headphone Handbook starts with the ubiquitous 'Principles of Sound Radiation', this chapter written by R. D. Ford, a lecturer from Salford University's Applied Acoustics department. It's a fairly standard introduction, describing the way sound waves are generated, their dispersion patterns and how they are specified in terms of level.

Next up, Stanley Kelly provides one of the most comprehensive introductions to drive unit mechanisms I've seen. It's a little dated in places "for domestic loudspeaker systems. . . a frequency response of I 00Hz to around 7kHz with, possibly, a small tweeter unit added to accommodate the high frequencies". But he does go on to explore various cone materials, profiles, surrounds and diaphragms in useful detail. Most of the chapter, as expected, covers the moving coil driver, but there is also a section on ribbons.

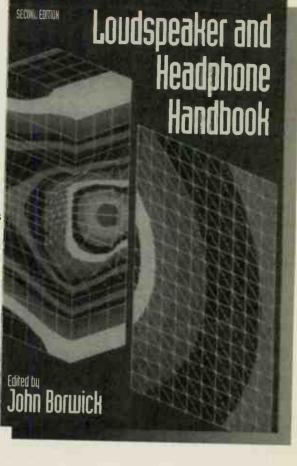
At the beginning of Kelly's chapter is a section on the lonophane driver, which works by causing an ionic discharge to occur in sympathy with the audio signal. This is done at the bottom of a horn, the gas discharge causing a wave to travel down the horn, producing sound from no moving parts. Unfortunately the lonophane's discharge was Ozone (O3) which is poisonous (try getting one of these past current safety standards). It is a small section, but the

Peter Baxandall takes over next to cover the electrostatic loudspeaker. It is mainly a theoretical look at the principles behind electrostatic operation, suitable materials and their constraints, rather than a practical guide to building one like Wagner's Electrostatic Loudspeaker Design and Construction. It doesn't so much tell you what materials to look for and how to construct an electrostatic, as give you the maths and theory to research the thing for yourself. It was also good to see that the two practical descriptions of commercial electrostatics are of Quad's 57 and 63 models - what else?

only one I've seen on the lonophane.

The world of the crossover is explored, mathematically, by Laurie Fincham, ex Chief Engineer at KEF, now hidden somewhere deep in the Harman empire over in L.A. This is one of the least accessible chapters for the amateur, launching into the maths almost straight away. The Loudspeaker Design Cookbook would be a better bet if this is your area of interest.

Loudspeaker enclosures, as described by Celestion's Graham Bank and Julian Wright, seems almost lightweight by



comparison. Brief descriptions of all the various enclosure types are followed by some useful practical considerations, such as cabinet material, damping and bracing.

The following chapters expand into public address, studio monitoring, measurement and subjective evaluation, to complete a very broad look at the loudspeaker. The chapter on headphones contains useful descriptions of the human ear and the book concludes with standards and definitions, which really are more a commercial consideration than being any particular use to the enthusiast.

In the Loudspeaker and Headphone Handbook, a valiant attempt has been made to cover all aspects of sound radiation. As such, there is little else available today that betters it. Individual areas of loudspeakers are covered in more depth in specialised texts, Robert Bullock's Bullock on Boxes springs to mind in the case of loudspeaker enclosures. But as a single reference work, no engineer or keen enthusiast should be without a copy.

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D.I.Y. Letters

TWEAKING THE UPGRADE BUG

I have the following system:
Micromega Drive I and DAC
on sorbothane CD feet,
Mission Cyrus II and PSX,
Mission 75 I speakers and
Partington Dreadnought
stands. Cables are 0.5m
Siltech HF6 between CD and
DAC, 0.5m Insert Audio
Status 3.4 interconnect and
Audioquest Indigo speaker
cable.

I am thinking of upgrading the speaker crossovers (I am experiencing some sibilance) and would be grateful for your opinion. Would it be worth making up external crossovers? What are the benefits? I would like to upgrade the internal wiring as well.

I want to upgrade the PSX and amplifier either by Russ Andrews' mods, or what about going for a valve kit bearing in mind the speakers? What kit would you suggest, i.e. World Audio, Audio Innovations,

Audio Note, and how do you feel about upgrading the parts to Black Gates, etc, or would I be better off going for a transistor pre and power like Audiolab or Naim. I do intend to upgrade the Drive I to Drive 3 status at some point.

Lee Duckett Wimbledon, London.

Upgrading the components in your Missions should bring about a worthwhile improvement, if a little care and consideration are taken in doing so. First of all, I'd start by removing the original crossover in its entirety. Build your new upgraded crossover completely separately - that way, if anything doesn't quite work, you have a chance to revert back to the original.

You will need to measure the DC resistance as well the inductance of the coils used in your 751s. I've heard very good things about the CFAC Copper Foil Air Core inductors advertised in the American magazine Speaker Builder, so these may well be worth investigating. They're available through The Parts Connection, Tel: 001 800 769 0747.

For the capacitors I'd use Solen polypropylenes (available from Falcon Acoustics, Tel: 01508 578272), which strike a fine balance between performance and price. If you really want the ultimate, try Hovland's Musicaps, available from SJS Electroacoustics, Tel: 01706 823025. These are smoother, more detailed and open, but you pay for it.

Internal wiring should be at least Ortofon SPK100, perhaps Chord Co. Rumour, if you're using the CFACs and Hovlands so that you capitalise on the improvements. Use a good quality silver loaded solder which not only makes a better electrical join, but is stronger mechanically too. Keeping the whole caboodle out of the boxes and close to the amplifier does have its advantages sonically, as long as you don't mind putting up with two sets of cables lying on the floor.

Upgrading the components in your amplifier is a different matter. You will need to have considerable electronic experience before taking on this task. The Cyrus II with PSX is a fine sounding amplifier, very clean and detailed along with plenty of power. I'd leave it as is, trading it in against a new Cyrus III. To this you could add a Cyrus power amplifier, biamping your system which I feel will bring a far greater improvement than tweaking your existing Cyrus II. DB

BRIDGING IT

Here is an idea that might be of interest to anybody experimenting with Motional Feedback.

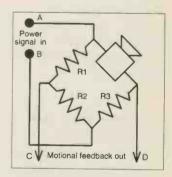
To avoid the complication of a second voice coil and make it possible to use any loudspeaker, why not make the loudspeaker part of a balanced Wheatstone Bridge. The voltage across C-D will be proportional to the signal generated by the motor effect of the speaker. If R I = R2 the system will be only 50% efficient. A 95% efficiency will be achieved by making a 20:1 bridge as shown.

To balance the bridge: replace the power signal with a few volts D.C. across A-B and adjust R1 until there is zero volts across C-D.

Theoretically, a small inductance should be put in series with R3 to compensate the loudspeaker inductance. However, the inductance would be so small that it could probably be ignored.

I must point out that I have not tried out this idea, not having any test equipment.

R. Turner Chalfont St Giles, Bucks.



Mr Turners suggestion for a motional feedback system uses a Wheatstone bridge to providing a sensing signal without the need for a second voice coil.

Looks OK to us. But bear in mind that a transformer introduces serious phase shift at the edges of its passband, which reduces the available feedback



stability margin. In theory a least, the 90 degree swing from the transformer plus the 90 degree swing from the voice coil adds to give a 180 degree total shift, at which point negative feedback is going positive, or positive would be going negative. This will set the stability limits and determine the amount of feedback that can be applied.

In practice the amount of shift will depend upon

such an item, one could have purchased a dozen valves and still had some change left over! The fact remains that the output transformer is still, and always will be, the weakest link in any amplifier in which it is used.

While I do not profess to be an electronics expert or a 'Golden-Eared' hi-fi buff, I derive great pleasure from building various valve amplifiers (this being one of them) and exploring ways in which they can be improved. Most of the tests which I was able to conduct on this amplifier do confirm the findings of the designer - flat from near DC to over 158kHz, and still some more.

those who cannot afford radio-metal iron cores oxygen-free silver wire or toroidal winding machines. I have successfully hand-wound three output transformers on high quality Siemens power transformer cores using the bifilar winding technique of the primary. The secondary was interleaved at three intervals, precise and exact turn ratios were adhered to before all three secondary windings were paralleled.

The diameter of the primary wire was 0.3mm, which was relatively easy to handle. The one output transformer is in service in a home-brew Williamson amp and the remaining two in a

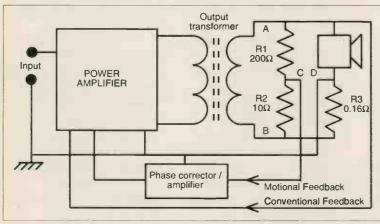
> Mullard 5-20 type amplifier. Impedance and frequency tests which I conducted on these transformers indicated good results, if not better than a conventionally wound component of good standing. However, one sees little mention of this winding technique in constructional

articles or reviews.

The only valve amplifier that I have read of using this winding technique in its transformers was the MacIntosh, where feedback was also fed to the cathodes of the output tubes. Apart from the possibility of a flashover between the two halves of the primary at high power, and the impossibility of getting a machine to do bifilar winding. What does this method have against it.

I look forward to many more informative issues of Hi-Fi World's DIY Sections, as well as any circuits (valve of course) that you come up with for home constructors here in darkest Africa.

Garth Moore East London, South Africa.



Mr Turner's full circuit for a motional feedback system.

frequency, motional impedance and other factors, especially if acceleration feedback is used, which introduces a -90 degree shift. NK

CUTTING OUT THE TRANSFORMER

I would be very grateful if you could spare a few moments to comment on the enclosed circuit diagram of the 25watt output transformerless amplifier. Today one does not see many of these kinds of circuits around and I wonder if they will ever find a place in the current upsurge in interest in valve amplifiers. With all the work that goes into constructing a quality valve output transformer, not to mention the final costs of

The photo of the square wave test is as it shows. I had to use 6080 tubes as there were no 6082s to hand.

I understand that this push-pull output stage is not the most symmetrical around, but then neither is a non-one transistor output stage. Worse still is the power MOSFET. An obvious safety improvement would be the use of a suitable isolation transformer and reconfiguration of the power supply section. Admittedly, the output impedance is not the norm by today's standards (i.e. 16 ohms) but this should present little problem to anyone interested enough to build the amplifier.

Now onto item no. 2 dedicated DIY slave, and

works into a simple 8 ohm load, even if paralleled valves are used. Because of the thermionic nature of valves, relatively high voltages and impedances are needed for successful operation and good linearity, and this is where the output transformer comes in. It's like a gearbox between the output valves and the speaker. In the same way, a car engine works at low torque and high rpm, so the gearbox steps the torque up and lowers the rpm to effectively transfer power and propel the vehicle. Running the valves into a low impedance without a transformer is like trying to pull away in 5th gear. If the impedance problem can be overcome by using either a large number of valves in parallel and/or using very high current valves (which is like increasing the capacity of the engine), there is still a problem in that the two halves of the output stage operate in totally different

The output transformer

amplifier's signal path. It

is the interface between the

necessary because there are

very few valves which can

loudspeaker voice coil. The

can be seen to be the

output stage and the

operate into a low

impedance load like a

6080 with its 100 ohm

anode impedance barely

loudspeaker load, made

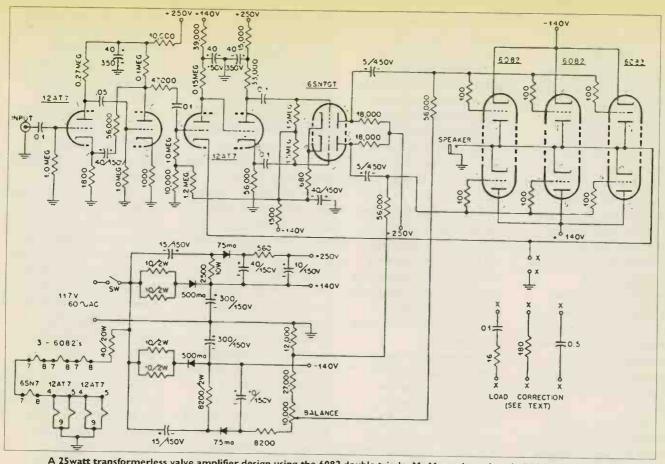
meakest link in an

This results in a totally different gain for the two halves, and the generation of large quantities of distortion. This imbalance is far worse than the differences between NPN and PNP devices or FETs. They are nearly always operated as unity gain followers, and as their transconductance is so

modes, one as an anode follower, the other as a

cathode follower.

which is really for the



A 25watt transformerless valve amplifier design using the 6082 double triode. Mr Moore intends to build his with the more easily available 6080 double triode.

much greater than that of any valve, the differences are mostly swamped by local feedback. In the OTL amplifier, however, these differences are laid bare. The article mentions that 40dB of feedback has been applied; that is, the gain has been reduced by 100 times. But the distortion of the amplifier at 25W, its rated output, is still 0.4%. Multiply this figure by the 100 times feedback factor to see what the distortion was before feedback and of course you get 40%!

The most ingenious solutions to this problem are generally attributed to Julius Futterman. He used local negative feedback around the phase splitter stage to decrease the gain to the anode follower half of the output stage, and later changed to local positive feedback to increase the gain to the cathode follower half. Check out the Futterman

circuits, you could modify your amplifier to work as such and the performance would be much better.

Another improvement would be either to parallel up a lot more 6080s (say 10 pairs per channel) or go to 6C33CBs, or triode or pentode connected PL519s. which would be the cheapest option. The later versions of the Futterman amplifiers used 6LF6s which are big TV valves like the PL519, only a lot rarer. You could end up with an excellent amplifier if you went over to the Futterman topology and threw money at the output stage, but you may also wind up spending more and getting worse performance than, say, a pair of push-pull 845s and wideband output transformer. Additionally, the 845s would be Class A and wouldn't vapourize your speakers if something went wrong with one of

them. There have been a few commercial OTL amplifiers such as the Futterman, and there are the Croft OTLs, but the cons seem to outweigh the pros and they are still quite rare beasts.

In bi-filar windings the two wires are wound together and so have excellent inductive coupling due to their proximity, the only downside being a large capacitance between the windings. This can be used to positive effect if the phase of the signal on the two is the same, but if the two halves of a push-pull primary (with 180 deg phase difference between the two valves' anodes) were wound in a bi-filar manner, the capacitance between them would be detrimental, causing the load impedance to decrease at high frequencies.

The MacIntosh amplifiers use a very

elegant output stage with a bi-filar wound transformer. The cathode of one valve is coupled to the anode of its partner by bi-filar winding. This works because on each of the valves there is a 180 degree phase shift between its anode and its cathode, so when one's cathode is coupled to the other's anode, they are back in phase again. There is, however, a large DC potential between them. The output transformers for the solid state SE amplifier are bi-filar wound, and in a lot of my driver and output transformers I use bi-filar and even tri-filar up to penta-filar windings depending on the application.

The transformers in switch mode PSUs often use bi- and tri-filar windings, or even Litz wire, which has many strands all insulated from

each other to reduce the skin effect. When I first started building valve amps, I used to wind my own output transformers with a hand drill and stripped down mains transformers! Grain oriented silicon steel (the most common type is called M6) laminations are quite easy to get hold of if you ask around, and you can make bobbins from thick card. The wire is available from catalogues like Maplin and Electromail, and these companies even offer mains transformer kits which could be adapted to make an output transformer, although the iron is of quite poor quality.

Nickel iron such as Radiometal or Permalloy, which is used in the best transformers, is very expensive and comes in various grades of permeability and hysteresis loss. The core for a small 15W push-pull output transformer, for example, would cost in the region of £70, but offer superior sound and performance if the winding technique is up to the mark. Even higher performance can be obtained with customdimensioned C cores, then you could use exotic materials inside like teflon. . . The sky's the limit. AG

NO MOTION AT THE

Your item on motional feedback in speakers (Supplement No. 23) was very interesting. An article worth reading was written by H. D. Harwood, then at the BBC, in "Wireless World", March, 1974 (p51). His thesis was that a well designed nonfeedback system could perform as well as a feedback one, and that feedback "possesses no magical

properties". The article certainly ruffled some feathers in the Philips camp.

Motional feedback to control an electro-mechanical transducer was patented in 1938 by Western Electric in respect of a moving coil disc cutting head. The principle has been applied to modern stereo heads and offers some points of interest.

The Ortofon head shown uses two feedback coils, wound in phase opposition and placed within opposite polarity magnetic gaps, hence the motionally derived output is summed whilst any coupling from the drive coil's field is cancelled.

The resonance frequency (which would normally be placed at the top of the working range to ensure stiffness control) is placed at the logarithmic centre, e.g. 2 kHz. No mechanical damping is used. The effect of varying degrees of feedback is shown, yielding an optimally flat response after which phase shifts in the upper region begin to cause a peak, which if increased would lead to instability. The difference in the l.f. response between the two graphs is due to an integrating circuit in the feedback amplifier which allows greater control at low frequencies.

Whilst not directly transferable to a loudspeaker system the above may suggest avenues of research.

S. Davies Aylesbury.

Motional Feedback offers an avenue of escape from the straight-jacket that embraces current loudspeaker design. Most of today's domestically acceptable models are modelled, to a useful degree of accuracy, as networks of masses and compliances (i.e. reactive mechanical elements), with of course the odd resistor thrown in. Thiele-Small equations, which computers gobble up,

manipulate these
parameters with such
speed and accuracy that
industry has become
completely wired into the
idea of designing a
loudspeaker's bass section
by this method. We use it and boy does it work.

Trouble is, you become locked into certain immovable trade-offs and ways of thought. That's why 'speakers are so alike these days. Innovation has gone out of the window, to be replaced by convenience and design efficiency. Plus a catalogue of standard trade-offs: for example, increase cone mass to decrease LF resonance to get deeper bass, and you lose sensitivity. It's impossible to use small boxes for deep bass unless the system is made very insensitive. And small drivers in small boxes distort badly.

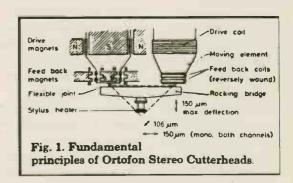
Motional feedback overcomes these limitations. Most importantly, it can be made to suppress or eliminate the basic box resonance problem that currently sets the low frequency limit and behaviour around that point (i.e. bass quality). So we could hardly agree with Dudley Harwood's observations. Not only can motional feedback reduce the considerable distortions generated by small bass drivers in particular (20% second harmonic, 5% third), it can

also provide optimal and adjustable damping. It is quite fundamentally different from what faces us today and also quite radical in what it can achieve. It just cannot be compared with a passive box system, since it overcomes its constraining parameters.

All this is not academic either. Those who have heard Motional Feedback working are struck by the tightness and impact of the bass it can produce. And if the industry is ever to get more or better bass from a small, domestically acceptable box this is one of the only routes available.

Why is motional feedback so rare? We are not entirely sure. We do suspect however that it raises all sorts of marketing and R&D problems for companies that, although thoroughly prosaic, still conspire to keep M.F. off the market. Philips, for example, built their power amps. into their speakers. It seems perfectly sensible, but the sort of buyer knowledgeable enough to choose such a system is likely to want a choice.

We are interested in seeing Motional Feedback brought to market in sensible form. This is likely to be provoked by open discussion, so a wider understanding of its problems and benefits takes place. NK



Ortofon's motional feedback moving coil disc cutting head



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