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RADIO RESEARCH
AND
PROGRESS*



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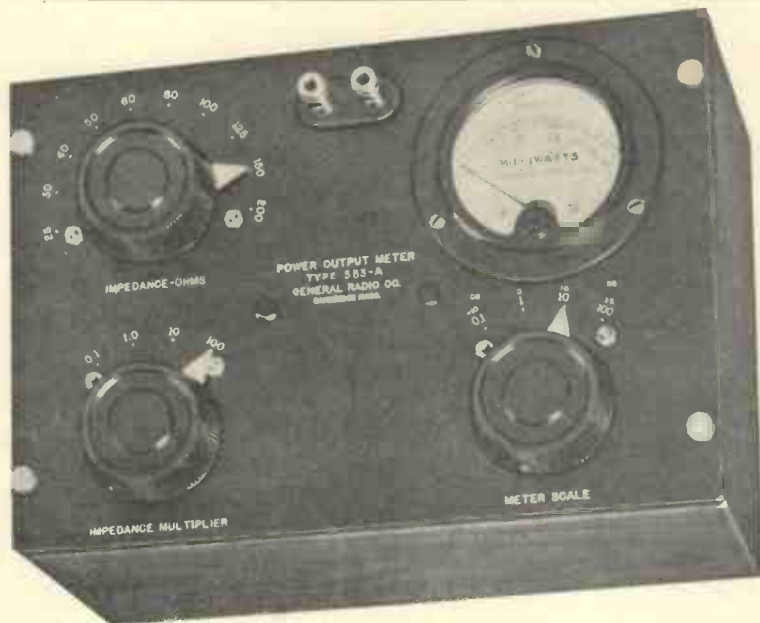
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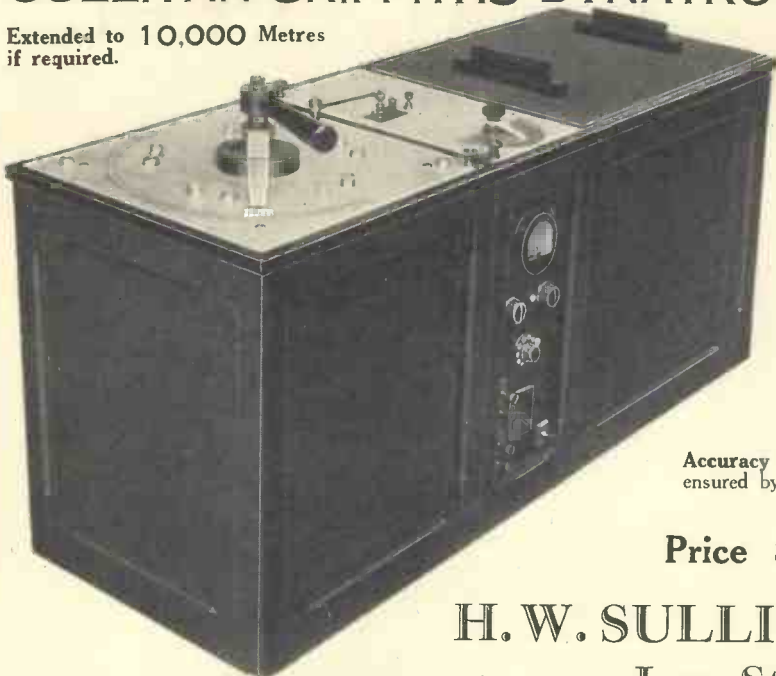
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VOL. IX No. 111

DECEMBER 1932

C O N T E N T S

EDITORIAL	665
THE EXISTENCE OF MORE THAN ONE IONISED LAYER IN THE UPPER ATMOSPHERE. By Geoffrey Builder, B.Sc.	667
FURTHER NOTE UPON THE PENTODE WITH CAPACITIVE COUPLING By L. G. A. Sims, Ph.D., A.M.I.E.E.	673
INTERFERENCE By E. T. Glas	680
CORRESPONDENCE	685
SOME RECENT PATENTS	687
GENERAL INDEX TO ARTICLES, AUTHORS AND ABSTRACTS IN VOLUME IX, JANUARY-DECEMBER, 1932.	

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CONTENTS OF THE NOVEMBER NUMBER.

SCIENTIFIC INSTRUMENTS AND AERONAUTICS.

By H. E. Wimperis, C.B.E., M.A.

The Principles and Practice of the Gravity Gradiometer.

Part I. By E. Lancaster-Jones, B.A.

A Self-Rectifying Demountable X-Ray Tube of High Power

By C. E. Eddy, D.Sc., F.Inst.P.

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WIRELESS ENGINEER

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No. III

Editorial.

Valve Data Diagrams.

IN June, 1931, we described a valve triangle, that is, a diagram, each point of which is at the intersection of three lines drawn from the three corners of an equilateral triangle to meet the opposite sides. The points where these lines meet the opposite sides enable one to read off the three principal characteristics of the valve, *viz.*, the amplification factor, the internal resistance and the mutual conductance. Such a diagram has the advantage of giving one a more comprehensive idea of the properties of a number of valves of various types than could possibly be obtained by means of tabulated data. The particular form of diagram described had, however, several disadvantages; interpolation was difficult because of the radial divergence of the three sets of co-ordinates, and the points tended to become crowded towards certain parts of the triangle. An improvement was introduced by Klingelhöffer and Walther* who described a modified valve triangle in which the crowding of the points was avoided by using logarithmic scales and interpolation was made easier by using parallel co-ordinates; the three sets of co-ordinates cut each other at an angle of 60 degrees, that is to say, they were parallel to the three sides instead of radiating from the corners of the triangle.

A further improvement has now been devised† which not only allows the three characteristics mentioned above to be read off with great ease and with accurate interpolation, but also gives a fourth characteristic, *viz.*, that which Barkhausen called the "Güte" or quality index of a valve and which is equal to the product of the mutual conductance and the amplification factor.

As will be seen from the figures, the diagram consists of two rectangular co-ordinate systems, one of which is at an angle of 45 degrees to the other. All the four scales are logarithmic. Any valve is represented by a single point; from the vertical and horizontal scales its resistance and quality index and from the sloping scales its mutual conductance and amplification factor can be read off.

In the original diagram the right-hand sloping scale gave the "Durchgriff" which is

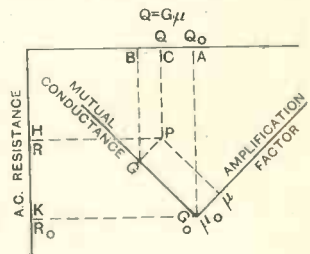


Fig. 1.

* See *Telefunken-Zeitung*, No. 59, 1931, p. 59.

† *Zilitinkewitch*.—Radio (Ukraine), Nov. 1931 and *Technika Radio i Slabogo Toka* (Russian), Jan., 1932; also *Gundlach*. *Elektrische Nachrichten-Technik* (German), Sept., 1932.

the reciprocal of the amplification factor, but we have modified it so as to read the more familiar amplification factor μ directly. At the bottom corresponding to a "Durchgriff" D of 0.1 per cent., we have $\mu = 1,000$ and at the top $D = 40$ per cent., and $\mu = 2.5$. The scale of mutual conductance G runs from 0.3 to 8.0 mA per volt. All the valves of three German makers were found to lie within these ranges, but there are now screen grid valves with amplification factors greater

meet the horizontal scale at the point A , and that through any other point P , corresponding to a valve with values G and μ , at the point C . Then

$$AC = AB - BC$$

$$= \frac{I}{\sqrt{2}} [(\log G - \log G_0) - (\log \mu_0 - \log \mu)]$$

$$= \frac{I}{\sqrt{2}} [\log G + \log \mu - (\log G_0 + \log \mu_0)]$$

$$= \frac{I}{\sqrt{2}} (\log G\mu - \log G_0\mu_0)$$

$$= \frac{I}{\sqrt{2}} (\log Q - \log Q_0)$$

The $I/\sqrt{2}$ is merely a matter of scale, and the formula shows that, if the point A is taken as Q_0 , the value of Q corresponding to any point P will be represented by the point C on an appropriate logarithmic scale.

Similarly it can be shown that a logarithmic scale can be plotted on the vertical line such that, if the point K is taken as the value R_0 of the A.C. resistance of a valve with mutual conductance G_0 and amplification factor μ_0 , the point H will give the value of R for any other valve represented by the point P .

In Fig. 2 we have plotted the data of a few typical valves to illustrate the usefulness of the diagram. Output valves are situated near the upper corner and screen grid valves near the bottom left hand of the diagram. The S4VA has an amplification factor of 1,500, and is thus somewhat outside the $G - \mu$ co-ordinates, but these could easily be extended further to the left to include such valves. G. W. O. H.

Since writing this note we have discovered that a diagram very similar in principle was described by Dr. R. T. Beatty in the *Wireless World* of July 17th, 1929, and used by him to plot the data of about 100 British valves. In Dr. Beatty's diagram R and G were plotted on the same axes as in Fig. 2 but in the reverse directions, μ was plotted on the horizontal scale, while Q , which is little used in this country, was not given. Dr. Beatty's diagram illustrates the great utility of this type of diagram for plotting the data of a large number of valves in a manner that lends itself to easy classification.

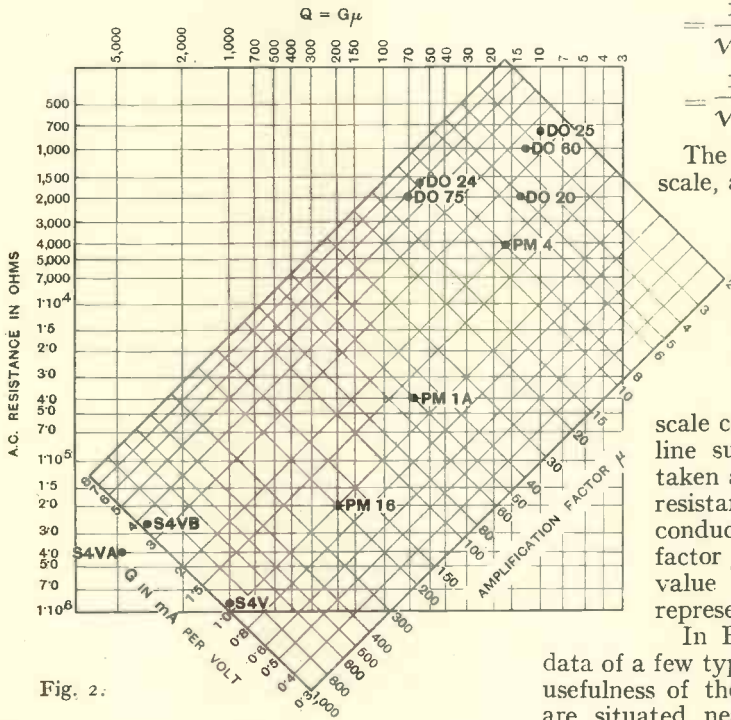


Fig. 2.

than 1,000 and to accommodate them the diagram would have to be extended to the left.

The A.C. resistances cover a very wide range, viz., from about 500 ohms to a megohm, while the quality index varies between 3 and 3,000.

So far as the sloping co-ordinates are concerned, the diagram is an ordinary logarithmic one on which G and μ for each valve are plotted. It is not so obvious that the same points will give the values of R and Q on suitable logarithmic scales on the vertical and horizontal lines, but that this is so can be readily proved.

Let the vertical through the point $G_0\mu_0$

The Existence of More Than One Ionised Layer in the Upper Atmosphere.*

By *Geoffrey Builder, B.Sc.*

(King's College, University of London.)

Introduction.

IN a recent editorial¹ in *The Wireless Engineer*, reference has been made to the problem of the number of ionised layers in the upper atmosphere. It was pointed out that the work of Goubau and Zenneck,² on 533 metres, can be interpreted in terms of reflections from a single ionised layer at a height of about 100 kms. Even though this is true it affords no criterion of the number of ionised layers which do actually exist. As will be shown, it is to be expected that these waves would always be reflected at about this height. Since there has now accumulated a large amount of evidence indicating the existence of more than one ionised layer in the upper atmosphere capable of reflecting wireless waves it seems worth while to review the data available from wireless experiments.

Experimental Methods.

There are two important wireless methods of investigating the electrical structure of the upper atmosphere. The "frequency-change" method is due to Appleton and Barnett³ and has been extensively and successfully used by Appleton and others. A small continuous change is made in the frequency of an unmodulated continuous wave transmitter and the signal amplitude at the receiving station is photographically recorded using an Einthoven galvanometer or other suitable instrument. If two sets of waves are being received simultaneously the equivalent path difference P' between them is determined by the number of interference maxima and minima through which the received signal intensity passes as the change in the transmitter frequency is made. It may be shown⁴ that

$$P' = c\delta n/\delta f$$

where

c = the velocity of electromagnetic waves in free space.

δf = the number of cycles per second by which the transmitter frequency is changed.

δn = the number of interference fringes due to the frequency change δf .
and the equivalent path of the wave is given by

$$c \int (1/U) ds$$

where ds is an element of the path and U is the group velocity of the waves at any point.

A typical record obtained by the method is shown in Fig. 1. The mean wavelength was 107 metres and the frequency change 6.30 kc. per sec. The number of interference fringes is 10.7 and therefore the equivalent path difference between the interfering waves was 509 kms. Since the distance between transmitter and receiver was 5 kms., and one of the interfering waves was the direct "ground wave," it is readily calculated that the equivalent height of reflection for the "atmospheric wave" was 257 kms.

The "group-retardation" or "pulse" or "echo" method of Breit and Tuve,^{5,6} has been very widely used, with many modifications and improvements. A short pulse of radio-frequency energy is sent out from the transmitter and the nature of the signal

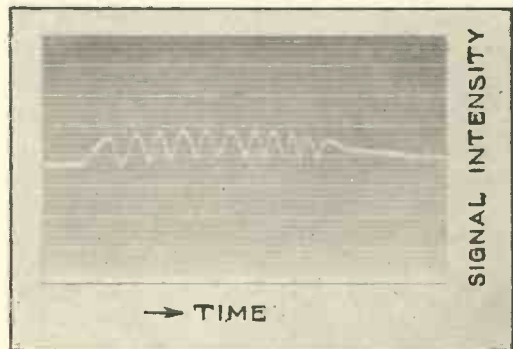


Fig. 1.—A simple fringe pattern obtained by the frequency change method. Frequency change 6.30 kc/s and equivalent path difference 509 kms.

at the receiving station is investigated by means of a high-speed recorder such as the cathode-ray or bifilar oscillograph. If there is a multiplicity of paths between the transmitter and the receiver, and if the pulse is

* MS. received by the Editor, March, 1932.

sufficiently short, a signal corresponding to each of the paths is received separately. The time differences between the arrival of the various signals is measured directly from the oscillograms and the equivalent path differences and the equivalent heights may then be calculated. In practice, a uniform sequence of pulses is transmitted with sufficient spacing between them to ensure that the received signals, corresponding to each pulse sent, do not overlap in time. Recent workers have used pulses as short as 1×10^{-4} sec. in duration, sent at a rate of about fifty per second. A typical simple record obtained in this way is reproduced in Fig. 2. The recording instrument was a Duddell oscillograph and a time-base for measurement is given by an oscillation of 1,100 cycles/sec. The

pulses marked *G* are those due to the direct ground signal and are followed by echoes F_1 and F_2 which are first and second reflections from an equivalent height of 254 kms. The distance between transmitter and receiver was 5 kms. and the wavelength 90 metres.

Equivalence of the Two Methods.

These two methods, as well as others of less importance, have been compared theoretically by Appleton⁷ and Schelleng⁸ who showed that the quantities measured by the two methods are generally equivalent. Experiments being carried out by the author indicate the validity of this conclusion. A comparison of their relative advantages for investigating the upper atmosphere has been made by Appleton and Builder⁹ who pointed out that the echo pattern is much the simpler to interpret if there is a multiplicity of paths, but that the frequency change method was much more sensitive in the detection of weak signals when a square law detector was used. The use of a linear detector, working at very high levels, for the echo observations, has since shown that the methods are essentially the same in this respect.

The Existence of One Ionised Layer.

The existence in the upper atmosphere of an ionised layer capable of reflecting wireless waves was first directly demonstrated by

Appleton and Barnett³ in 1925, using the frequency change method. Confirmation by the pulse experiments of Breit and Tuve⁶ followed shortly afterwards. Appleton and Barnett, using a wavelength of 400 m., measured heights of the reflecting layer

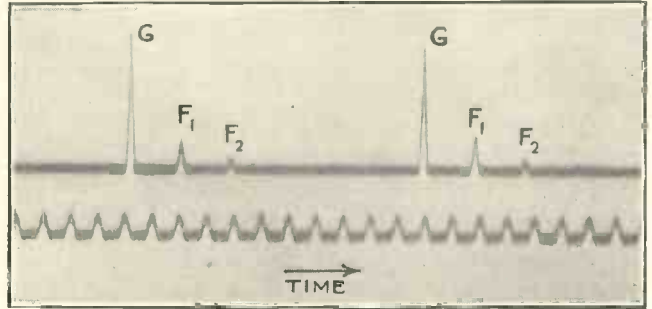


Fig 2.—First and second reflections from an equivalent height of 254 kms., as recorded by the echo method. Time base oscillator frequency 1,100 c/s.

varying from 90 kms. in the daytime to 115 kms. at night, while Breit and Tuve found heights ranging from 80 to 200 kms. for 70 m. waves. The latter measurements have, however, not been confirmed, and later Breit, Tuve, and Dahl,¹⁰ with improved pulse transmissions on 75 metres, observed that the heights of reflection measured from successive echoes were sometimes approximately in the ratio 1 : 2 : 4, and interpreted the results in terms of multiple reflections at a single layer although the relative intensities and the relative delays of the echoes are scarcely compatible with the explanation. Kenrick and Jen¹¹ obtained equivalent heights of the reflecting layer for 67 metre waves of 250 kms. in the daytime to 350 kms. at night. These values, together with those of Hollingworth¹² on 14,350 metres, Appleton and Barnett¹³ on 400 metres and Heising¹⁴ on 57 and 111 metres were employed to obtain a curve relating equivalent height and wavelength, and it was shown that the result was not incompatible, qualitatively, with the curve calculated on the assumption of a single reflecting layer.

Quantitatively, agreement was not good and the greater range of measurements now available indicate that the agreement of the shape of the experimental and calculated curves was fortuitous. Further, the single layer theory does not account for the observed relation of attenuation to wavelength, as has

been pointed out by Heising,¹⁴ Eckersley,¹⁵ and others. To explain the marked superiority of the shorter waves for long-distance communication it is necessary to assume a distinct attenuating region below the reflecting layer at which reflection of the short waves occurs.

TWO IONISED LAYERS.

Frequency Change Measurements.

In 1927 Appleton¹⁶ demonstrated the existence of two distinct regions of ionisation at heights of about 100 and 200 kms. Using the frequency-change method many of the records showed subsidiary fringes superimposed on the main ones. At a wavelength of 1,000 metres, it was always found that these subsidiaries could be accounted for in terms of multiple reflections between the ground and a single ionised layer (the Kennelly-Heaviside or *E* layer) at a height of about 100 kms. With 400 metre waves similar results were usually obtained, but in some records taken in the early morning the subsidiary fringes could not be explained in this way. A careful examination showed that the ratio of the number of primary to subsidiary fringes was not that to be expected on the assumption of multiple reflections from a single layer. Moreover, in the period just before sunrise, the primary fringes disappeared on some occasions, the subsidiary then becoming the main fringes. In these cases the primary fringes suddenly returned at about 40 minutes before sunrise at the ground, while the subsidiaries gradually weakened and disappeared.

The difficulty of interpreting such records in terms of a single reflecting layer led Appleton to postulate a second ionised layer (*F* layer) at a height of about 200 kms. and considerably richer in ionisation than the lower layer. On this basis, the subsidiary fringes are due to the radiation partly or completely penetrating the lower layer and being reflected at the upper one. The sudden return to reflection at the *E* layer, at about 40 minutes before ground sunrise, agrees well with the time of sunrise at the height of this layer. Another feature of the records which is similarly explained is that the equivalent height of *F* layer, deduced from the subsidiary fringes, began to decrease at about 80 minutes before sunrise.

Further evidence pointing to the correct-

ness of this hypothesis was obtained by Appleton and Ratcliffe¹⁷ in simultaneous observations at a number of stations receiving signals from the same transmitter. Simultaneous reflections from different layers at different receiving stations were observed at wavelengths of 400 and 212 metres, and it was found that the *E* and *F* layer heights did not differ greatly for these two wavelengths. Appleton and Green¹⁸ found that only during part of the daytime is the ionisation of *E* layer great enough to reflect 100 metre waves. Fig. 3, from their paper, shows the variation of equivalent height of the reflecting layer throughout the day measured on this wavelength. The discontinuities in the curve indicate definitely the distinct nature of the two layers, especially when it is remembered that for the greater part of the night and throughout the day 400 metre waves are reflected at a height of about 100 kms.

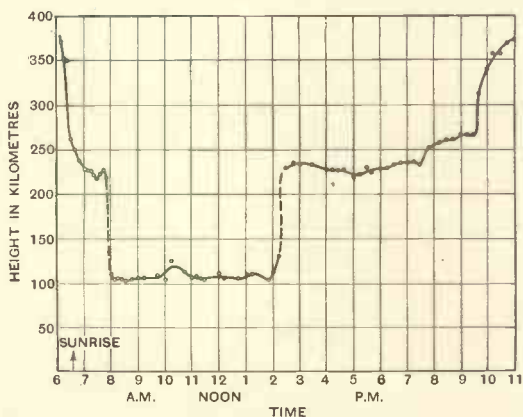


Fig. 3.—The variation of equivalent height of reflection of 100 m. waves on October 21, 1928. (After Appleton & Green.)

The frequency-change measurements therefore indicate that (a) 1,000 metre waves are always reflected at *E* layer at an equivalent height of about 90 kms., (b) 400 metre waves are reflected at *E* layer at an equivalent height of 90 kms. in the daytime to 115 kms. at night, except for short periods before sunrise when recombination in *E* layer has proceeded so far as to permit its penetration by these waves so that reflection may occur at *F* layer at about 200 kms., (c) the behaviour of 200 metre waves is very similar except for such differences as might have been expected: slightly greater equivalent heights for both layers and a greater ten-

dency to penetrate the lower layer, and (*d*) at 100 metres penetration of the lower layer occurs for the greater part of the day. Equivalent heights on this wavelength are about 105 and 230 kms. in the daytime to more than 360 kms. at night.

Group-retardation Measurements.

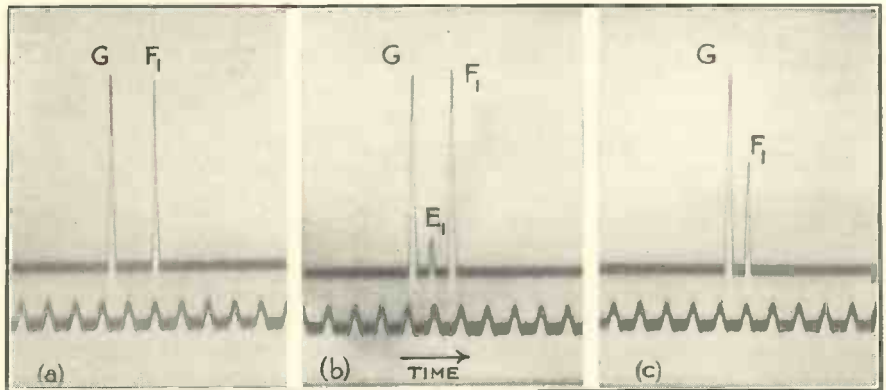
Appleton¹⁹ has interpreted the results of Breit, Tuve, and Dahl, already referred to, as confirming the hypothesis of two reflecting layers. The three echoes received indicated equivalent heights of 105, 235 and 470 kms., the departure from the ratio 1 : 2 : 4 being outside the limits of experimental error. If the three echoes are multiple reflections from a single layer it is to be noted that the third reflection is consistently absent, and that in the published records the first echo is frequently weaker than the second. These difficulties disappear at once if the echoes are interpreted as a single reflection from *E* layer and first and second reflections from *F* layer. The heights of the two layers so obtained are in good agreement with the daytime frequency-change measurements made on 100 metres.

In 1930 Gilliland,²⁰ using 74 metres, concluded that the down-coming signals during the day were due to two layers at equivalent

of *E* layer increases. The non-occurrence of multiple echoes in these records is due partly to the use of a square law detector and partly to attenuation, probably occurring in *E* layer.

Schafer and Goodall²², using 185 and 97 metres simultaneously, provided further striking evidence in favour of the two-layer theory. Curves of equivalent height against time showed, for the longer waves, a sudden change over of reflection from the upper to the lower layer, while the shorter waves continued to be reflected by the upper layer. Further, it was shown that waves just short enough to penetrate the lower layer suffered considerable group retardation so that the equivalent height of *F* layer measured on this wavelength was appreciably increased. This effect has previously been discussed by Appleton and Ratcliffe²³ and by Appleton,²⁴ and is further illustrated in Fig. 5, in which the variation of the equivalent height of the reflecting layer for 80 metre waves and the intensity of the *F* layer reflections are plotted against time. Until 1620 G.M.T. reflection from *E* layer occurred, but the waves then penetrated this layer and were reflected at *F*. The *F* echoes were at first weaker and indicated greater equivalent heights than later when the *E* layer ionisation had further decreased. The reverse process then occurs when

Fig. 4.—Successive echo records showing a change over of reflection from *F* layer to *E* layer and illustrating the distinct nature of the two layers.



heights of 119 and 235 kms. Appleton and Builder²¹ have published successive echo records showing the penetration of the lower layer by 80 metre waves in the sunset period. Similar records for 90 metres, in Fig. 4, taken at 9, 10 and 11 o'clock G.M.T., show the gradual change over of reflection at *F* layer to reflection at *E* layer as the ionisation

E layer ionisation again increases sufficiently to reflect. The inverse correlation of *F* layer height and echo intensity is very marked in this as in many other similar records.

More recently further observations by Gilliland, Kenrick and Norton,²⁵ Ranzi,²⁶ and others have added an abundance of evidence in favour of the hypothesis of a second re-

flecting layer. It is to be noted that there is no definite evidence of reflections from heights intermediate between those given for the *E* and *F* layers except those of Goubau and Zenneck² to which we now

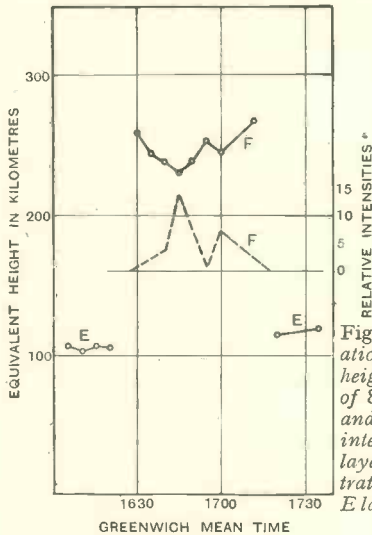


Fig. 5.—The variation of equivalent height of reflection of 80 metre waves and the variation of intensity of the *F* layer echoes, illustrates the effect of *E* layer on *F* layer echoes.

turn. From what has been said, the failure to observe echoes from *F* region is not surprising in view of the wavelength used in the experiments and the results are in this respect compatible with the simple two-layer theory. It is to be noted, however, that while the frequency change measurements gave values of 90 to 115 kms. for 400 metres, Goubau and Zenneck measured equivalent heights up to 140 kms. for 533 metres. The echoes from which these higher values were calculated were usually accompanied by others giving the more usual heights of 90 to 100 kms. The authors show that for the most part the equivalent heights may be divided into two groups at about 95 and 135 kms. Such a grouping does not suggest either a continuous layer of ionisation extending upwards from 90 kms. or that the double and complex echoes are due to undulations in the layer as suggested by the authors. It is therefore necessary to consider whether these complex echoes, which generally occurred in the early morning hours, indicate a stratification of *E* layer or whether there is any other probable explanation.

Are there more than Two Ionised Layers or are these Layers Horizontally Stratified?

Eckersley¹⁵ considers that the available

data suggests horizontal stratification of the *F* layer, the maxima of ionisation being about 10^5 electrons per cc. at 100 kms. (*E* layer) and 3×10^5 and 9×10^5 at 180 and 250–350 kms. respectively (*F* layer). The variation of equivalent height with wavelength does not appear to require such stratification, and the variation of equivalent height of the *F* layer for a given wavelength is scarcely compatible with such a hypothesis since the equivalent height increases smoothly as recombination proceeds until such time as the ionisation is no longer sufficient to cause reflection of the waves being used. There is no sudden jump to a higher stratum such as occurs in the case of penetration of *E* layer and more evidence is necessary before further complication of the layer structure need be postulated. The results of Goubau and Zenneck may at first appear to support a similar hypothesis for the *E* layer unless their own explanation of complex echoes due to scattering at an undulatory layer is accepted. Appleton and Builder⁹ have obtained double echoes from the *F* layer on 80 metres under somewhat similar conditions but consider that they may be the two magneto-ionic components due to splitting of the original signal into two polarised components having different group velocities in an ionised medium in the earth's magnetic field.* The occurrence of such splitting at times when the waves may be supposed to penetrate far into the ionised layer, the gradual increase from zero of the time interval between the components as such penetration occurs, and the different electron densities required for the reflection of the components, are all in accord with the explanation. Fig. 6 shows an echo record which is typical of such splitting of the *F* echo. Under other conditions echo patterns like that of Fig. 7 are frequently obtained owing to multiple splitting. Transitions between these two types are also observed, the two main components both showing signs of complexity but remaining distinct. If the explanation advanced is correct it accounts for such complex echoes without the need to assume further complexity in the layers themselves.

There is another type of echo pattern which at first sight might seem to suggest

* Since this paper was written this hypothesis has been confirmed. A full account will be available shortly.

the existence of more than two layers but may be very simply explained on the two-layer theory. When the wavelength being employed is such that partial penetration of the *E* layer occurs and echoes are received simultaneously from the *E* and *F* layers, it is to be expected, by analogy with multiple reflections from a single layer, that echoes will also occur due to successive reflections from the two layers. Echoes are in fact observed corresponding to an equivalent height equal to the sum of the equivalent heights of the *E* and *F* layers, as measured from the corresponding echoes on the same record. There is also some evidence that reflection from the top of the *E* layer may occur. Echoes are occasionally observed corresponding to an equivalent height approximately equal to twice the equivalent height of the *F* layer less the equivalent height of the *E* layer and may possibly be due to such reflections since they seem to occur only when the critical penetration wavelength for the lower layer is being used.*

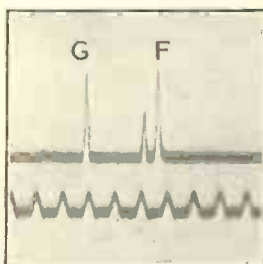


Fig. 6.—Splitting of the *F*-layer echo into two components of different retardation.

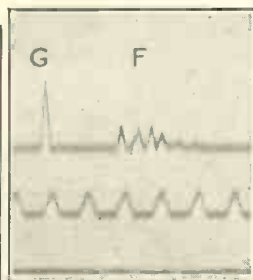


Fig. 7.—A complex *F*-layer echo which may be due to magneto-ionic dispersion.

At present it does not appear essential to postulate more than two layers or stratification of these two layers to explain the experimental data, nor does it appear to be necessary, for observations such as

* The fuller investigation of the magneto-ionic effect indicates that simultaneous reflection from the two layers is partly due to the greater electron density required to reflect the left-handed polarised component, which may penetrate the lower layer and be reflected at the upper, while the right-handed component is reflected by the lower layer. Successive reflections at the two layers are therefore not observed as frequently as might be expected from the frequent occurrence of simultaneous echoes from the two layers.

those described here, to assume an undulatory nature for the two layers, but further detailed evidence is required on these points. The occurrence of further strata is not incompatible with the generally assumed mechanism of the ionisation of the layers. Moreover, by the methods described, a layer of ionisation would not be detected if it was above another layer more intensely ionised.

Summary.

The chief wireless methods of investigating the electrical structure of the upper atmosphere are briefly described and compared. It is shown that the results obtained by both methods support the hypothesis of the existence of at least two layers of ionisation capable of reflecting wireless waves. The possibility of the occurrence of other strata of ionisation is also briefly discussed and it is concluded that the measurements available do not require the existence of more than two simple layers of ionisation for their explanation.

I am indebted to Professor Appleton and Mr. A. L. Green, and to the Royal Society for permission to reproduce the diagram of Fig. 3.

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Further Note upon the Pentode with Capacitive Coupling.*

By L. G. A. Sims, Ph.D., A.M.I.E.E.

IN a recent paper† the Author showed that the load-matching conditions which apply particularly in an output stage employing a pentode enable the output coupling capacity to improve materially the low-frequency power response of the stage. The preliminary analysis of the case

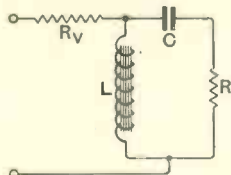


Fig. 1.

given in the paper was intended mainly to establish the existence of this effect and a further contribution containing detailed extensions was promised. Let Fig. 1 represent the equivalent circuit of a valve coupled to a resistance load by means of an inductance L and condenser C , the symbols R_v and R relating to the operating resistance of the valve and to the load respectively.

It was shown that, per volt available in the anode circuit, the volts V developed across the load R were given by

$$V = \frac{\omega LR}{\left[(RR_v + \frac{L^2}{C}) + \left\{ \omega L(R + R_v) - \frac{R_v}{\omega C} \right\}^2 \right]^{1/2}} \quad \dots \dots \dots (1)$$

where $\omega = 2\pi \times$ frequency.

Treating ω as the independent variable in order to examine the behaviour of V with change of frequency, and treating all other quantities as constants, the equation

$$\frac{dV}{d\omega} = 0 \quad \dots \dots \dots (2)$$

leads to a condition of maximum voltage and therefore of maximum power in R when ω has the special value‡

$$\omega = \left[\frac{1}{C \left(L - \frac{R^2 C}{2} \right) - \frac{L^2}{2R_v^2}} \right]^{1/2} \quad \dots \dots \dots (3)$$

In the Author's previous paper this equation was examined in order to see whether real values of ω could be expected in practice, that is, whether a peak in the power response curve could be expected. It was found that, with the load-matching conditions usually employed, such a peak could only be expected with pentode valves because the peak occurs only when, among other conditions, the load resistance is less than that of the valve—a characteristic of the pentode but not of the triode output stage.

If typical values of L , R and R_v be inserted in equation (3) and ω be evaluated for different values of C , it is found that ω approaches

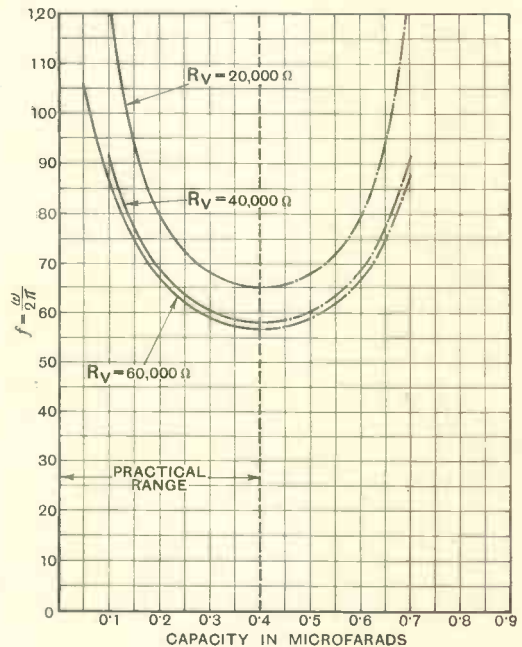


Fig. 2.—Curves plotted from equation (3).
 $L = 40$ henrys, $R = 10,000$ ohms.

infinity for two different values of C . In Fig. 2 are plotted three curves which illustrate this effect, relating to different constant values of R_v .

In order to interpret these curves it is

* MS. received by the Editor, June, 1932.
† See "Capacitive Output Coupling," Sims, *Wireless Engineer and Experimental Wireless*, June, 1932.
‡ *Ibid.*, page 315.

necessary to examine them with reference to Table I (which gives figures from which the curve of Fig. 2 relating to $R_v = 60,000$ ohms was calculated) and with reference to experimental results taken with circuit constants approximating closely to those assumed in calculation. Fig. 3 shows a series of such experimental results taken with an Osram type PT 240 pentode whose rated internal resistance is 55,000 ohms. The output inductance, measured in the circuit with the load disconnected but with the steady valve current flowing, was 40 henrys, and the load was a non-inductive resistance of 10,000 ohms. These values correspond closely to those assumed in the calculation of Table I, namely $L = 40$ henrys, $R_v = 60,000$ ohms, $R = 10,000$ ohms. The experimental curves were taken with a constant input of 1.6 volts R.M.S. to the grid of the pentode at a large number of frequencies between 45 and 6,000 cycles per second, the circuit diagram being as shown in Fig. 4. It is seen that the frequency and hence the pulsance ω at which the power peak occurs, falls continuously as the coupling

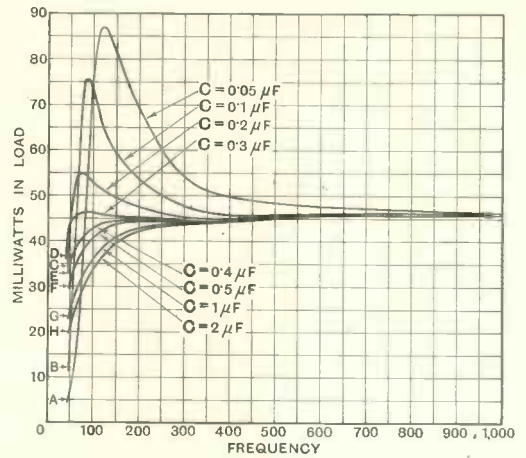


Fig. 3.—Experimental power response curves of Pentode PT240. Choke-condenser coupled to resistance load of 10,000 ohms. $R_v = 55,000$ ohms, $L = 40$ henrys, under operating conditions. Input to grid = 1.6 v. R.M.S.

condenser is increased from 0.05 microfarad to a value between 0.3 and 0.4 microfarad, the peak vanishing for values of

TABLE I.

CALCULATION OF ω FROM EQUATION (3).

$L = 40$ hys. $R_v = 60,000 \Omega$. $R = 10,000 \Omega$. C variable.

C in $\mu F.$	$\frac{R^2 C^2}{2}$	$\frac{L^2}{2R_v^2}$	$\frac{R^2 C^2}{2} + \frac{L^2}{2R_v^2}$	LC	$\frac{LC - R^2 C^2}{2} - \frac{L^2}{2R_v^2}$	$\frac{I}{LC - \frac{R^2 C^2}{2} - \frac{L^2}{2R_v^2}}$	$\omega =$	
							$\frac{I}{\sqrt{LC - \frac{R^2 C^2}{2} - \frac{L^2}{2R_v^2}}}$	$f = \frac{\omega}{2\pi}$
0.05	$\frac{0.125}{10^6}$	$\frac{0.222}{10^6}$	0.347×10^{-6}	2×10^{-6}	1.653×10^{-6}	6.04×10^5	729	116
0.1	$\frac{0.5}{10^6}$	"	0.722×10^{-6}	4×10^{-6}	3.278×10^{-6}	3.05×10^5	553	88.2
0.2	$\frac{2.0}{10^6}$	"	2.222×10^{-6}	8×10^{-6}	5.778×10^{-6}	1.73×10^5	417	66.4
0.3	$\frac{4.5}{10^6}$	"	4.722×10^{-6}	12×10^{-6}	7.278×10^{-6}	1.375×10^5	371	59
0.4	$\frac{8}{10^6}$	"	8.222×10^{-6}	16×10^{-6}	7.778×10^{-6}	1.285×10^5	358	57
0.5	$\frac{12.5}{10^6}$	"	12.722×10^{-6}	20×10^{-6}	7.278×10^{-6}	1.375×10^5	371	59
0.6	$\frac{18}{10^6}$	"	18.222×10^{-6}	24×10^{-6}	5.778×10^{-6}	1.73×10^5	417	66.4
0.7	$\frac{24.5}{10^6}$	"	24.722×10^{-6}	28×10^{-6}	3.278×10^{-6}	3.05×10^5	553	88.2
0.8	$\frac{32.0}{10^6}$	"	32.222×10^{-6}	32×10^{-6}	Negative	Negative	Imaginary	Imag.
0.9	$\frac{40.5}{10^6}$	"	40.722×10^{-6}	36×10^{-6}	Negative	Negative	Imaginary	Imag.

capacity greater than this. If reference be made to Fig. 2 it will be seen that the experimental results agree fairly closely with the theoretical prediction given by the first half of the curve relating to $R_v = 60,000$ ohms. This curve shows that no peak is to be expected for lower frequencies than about 57 cycles per second, and that a capacity of about 0.4 microfarad is then needed.

For larger values than 0.4 microfarad the theoretical and experimental curves no longer agree, as the former appear to indicate a further range of frequencies over which a power peak will occur with further increase of capacity, whilst the latter show that, in fact, the power response curve degenerates with increasing C to the form characteristic of plain transformer coupling, that is, the low-frequency response falls away.

Case of "Level Compensation."

It follows, therefore, that only the first halves of the curves shown in Fig. 2 have practical value. At the same time, it is made clear that an important practical case arises at what may be called the critical or transition point of these curves, namely, the point of minimum frequency. Here the capacity becomes such as to maintain uniform response over the widest possible range of frequencies (see Fig. 3). This, then, gives the condition for what may be termed "level compensation."

Referring to the figures in Table I, it is seen that this condition arises when the denominator of the expression for ω , defining ω for maximum power, has its greatest value. From this we may determine an expression which yields level compensation in a given pentode output circuit. Writing for the denominator expression of (3)

$$m = LC - \frac{R^2 C^2}{2} - \frac{L^2}{2R_v^2} \quad \dots (4)$$

we may differentiate m with respect to C and equate to zero to determine conditions for a maximum.

Thus
$$\frac{dm}{dC} = L - \frac{2CR^2}{2} \quad \dots (5)$$

Equating to zero gives

$$L = CR^2$$

Whence, if C' be written to denote a special value of C applying to this case

$$C' = \frac{L}{R^2} \quad \dots \quad \dots (6)$$

Inserting the values $L = 40$ henrys, $R = 10,000$ ohms into (6) and converting to microfarads gives $C' = 0.4$ microfarad, which agrees satisfactorily with Figs. 2 and 3 and Table I and confirms that (6) gives a maximum value of m and a minimum value of ω .

The value of capacity for level compensation is shown by (6) to be independent of R_v , a result which is also demonstrated by the curves of Fig. 2.

But although this is so, the lowest frequency of uniform response is a function of R_v (see Fig. 2). Clearly, by substituting from (6) in (3) this frequency can be determined. The substitution yields

$$\omega' = \left[\frac{L^2}{R^2} - \frac{L}{2} - \frac{L^2}{2R_v^2} \right]^{\frac{1}{2}}$$

where ω' represents the special value of ω associated with C' .

Then

$$\omega' = \frac{\sqrt{2} \cdot RR_v}{L(R_v^2 - R^2)^{\frac{1}{2}}} \quad \dots (7)$$

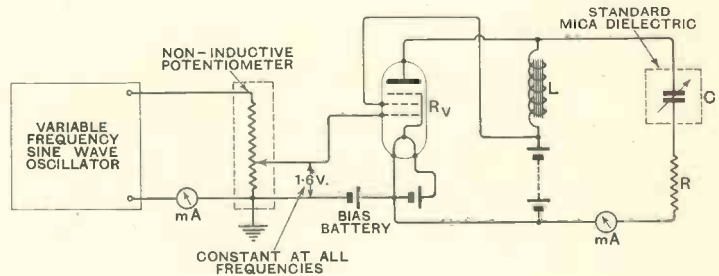


Fig. 4.

whence by writing $f' = \frac{\omega'}{2\pi}$ we have

$$f' = \frac{0.225 RR_v}{L \cdot (R_v^2 - R^2)^{\frac{1}{2}}} \quad \dots (8)$$

Substituting in (8) the values $R_v = 60,000$ ohms, $R = 10,000$ ohms, $L = 40$ henrys, as used in Table I, gives $f' = 57$ cycles per second for the lowest frequency of uniform response. This agrees exactly with the

figures calculated from equation (3) in Table I and is confirmed to a reasonable degree of approximation by the experimental curves. Thus equations (6) and (8) may be used to determine the coupling capacity and lowest frequency of uniform response.

Throughout the above reasoning a load resistance of 10,000 ohms has been employed and a transformation ratio of unity assumed at the inductance. Inevitably the varying frequency under which the output stage works in practice must complicate the theory when the true nature of the load is a complex impedance, as is the case with a loud speaker; nor could full allowance be made for this. But at the very low frequencies concerned throughout the analysis the load certainly tends to become predominantly ohmic in character,* which makes its treatment as a resistance a reasonable approximation. Since the ratio of transformation, if not unity, appears in the equations merely as a constant multiplying the actual values of resistance and capacity in the secondary circuit, it does not affect the general conclusions reached. If, for example, the ratio of primary turns to secondary turns be k , and the actual load resistance and coupling capacity be R_2 and C_2 , the substitutions

$$R = k^2 R_2, \quad C = \frac{C_2}{k^2}$$

throughout the solutions will allow for all ratios of transformation.

With pentode valves, except when used with low-resistance moving-coil speakers, the value of k is usually close to unity, and the properties of the auto-transformer of low ratio then reduce the effective series impedances of the transformer windings to values which are negligible at low frequencies, so justifying their omission from the analysis. On the other hand, the magnetising current at the lowest frequencies is by no means negligible and is taken into account in equation (1).

Capacity for Maximum Power at a Particular Frequency.

If equation (1) be differentiated with respect to C (ω being taken as constant) a

* See "The Inductor Dynamic Loud Speaker." Oliver, *The Wireless World and Radio Review*, 18th November, 1931.

solution may be derived which gives the value of C required for over-compensation of the bass response at a chosen frequency, so enabling the low-frequency response of an imperfect reproducer to be augmented. Thus, whereas the analysis has so far aimed at adjusting the characteristics of the output stage to equal, as far as possible, those of a supposed perfect reproducer, the present analysis will aim at improving the response of the complete stage, including the reproducer.

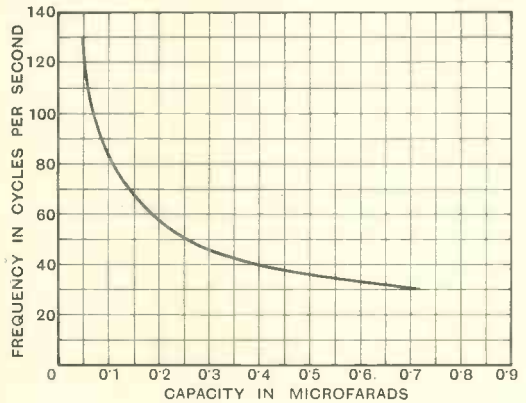


Fig. 5.

Expanding the denominator of (1) and writing

$$\beta = RR_v$$

$$\delta = \omega LR$$

$$\epsilon = \omega L(R_v + R)$$

we have

$$V = \frac{\delta}{\left[\beta^2 + 2 \frac{\beta L}{C} + \frac{L^2}{C^2} + \epsilon^2 - 2 \frac{\epsilon R_v}{\omega C} + \frac{R_v^2}{\omega^2 C^2} \right]^{1/2}} \quad \dots \quad (9)$$

Differentiating and writing (D) for the denominator expression when this rears unchanged from (9) we have, after simplification

$$\frac{dv}{dc} = \frac{\delta \left[\frac{1}{C^2} \left(\frac{\epsilon R_v}{\omega} - \beta L \right) - \frac{1}{C^3} (R_v^2 + L^2) \right]}{[D]^2} \quad \dots \quad (10)$$

The condition for maximum voltage across the load, and hence for maximum power, is obtained from (10) in the usual way by

equating to zero. This leads to the equation

$$\left[\frac{I}{C^2} \left(\frac{\epsilon R_v}{\omega} - \beta L \right) - \frac{I}{C^3} (R_v^2 + L^2) \right] = 0$$

whence, after multiplying by C^2 and collecting terms we have

$$C'' = \left[\frac{R_v^2 + L^2}{\frac{\epsilon R_v}{\omega} - \beta L} \right]$$

where C'' is written to denote a special value of C .

Substitution for ϵ and simplification yield

$$C'' = \left[\frac{R_v^2 + \omega^2 L^2}{\omega^2 L R_v^2} \right] \quad \dots \quad (II)$$

This equation, therefore, defines the capacity in farads which will develop the maximum possible power in the load at any selected single value of ω . It is of interest to note that this capacity is a function of the valve resistance R_v but not directly of the load resistance R , though the latter may operate upon C indirectly by virtue of its influence in a rational selection of the inductance L^* . But, unlike the analysis relating to variable ω (equation 3), the result expressed for variable C in equation (II) does not permit imaginary values due to the relative magnitudes of R_v and R . There is consequently an optimum capacity for both pentode and triode which, theoretically, will yield maximum power at any one frequency since the pentode and triode output circuits, for the purpose of this analysis, are to be regarded as differing only in the relations between R_v and R . But it will be shown that, in practice, the solution is virtually applicable only to the pentode.

In Fig. 5 values of capacity and frequency are plotted from (II) for a pentode circuit having the constants previously employed, namely, $R_v = 60,000$ ohms, $L = 40$ henrys, $R = 10,000$ ohms. From this curve can be read the capacity required for maximum power at any one frequency. In Fig. 6 are shown experimental curves taken with an Osram pentode, type PT 240, nominal internal resistance 55,000 ohms, the other circuit constants being $L = 40$ henrys (approximately) and $R = 10,000$ ohms. The circuit was the same as shown in Fig. 4, but the frequency was maintained constant

during each test and the capacity varied. Comparison of the theoretical curve of Fig. 5 with the measured values from Fig. 6 shows satisfactory agreement and confirms that equation (II) defines conditions for maximum power.

The "Coincidence" Effect.

If curves for the two foregoing cases, relating to the same circuit constants, be superimposed it would appear possible that an intersection may occur and fall within what is termed in Fig. 2 the "practical range." At the intersection the conditions for maximum power defined by equations (3) and (II) will be satisfied simultaneously and the power developed in the load will attain its maximum possible value.

In Fig. 7 curves plotted from equations (3) and (II) for $R_v = 60,000$ ohms, $R = 10,000$ ohms and $L = 40$ henrys are shown superimposed, intersection occurring at a frequency of approximately 108 cycles per second and with a capacity of approximately

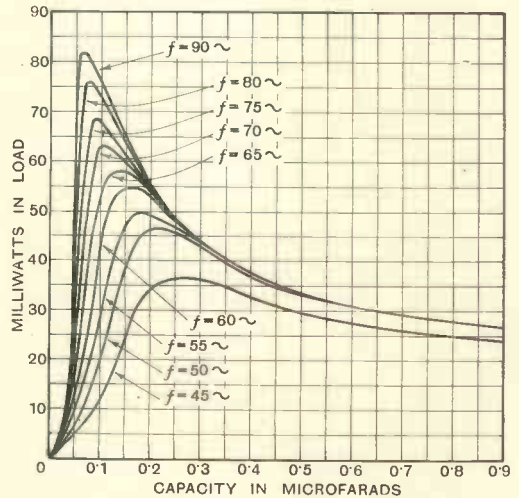


Fig. 6.—Experimental curves of coupling capacity and power plotted from response curves for different frequencies. Pentode PT240, resistance load = 10,000 ohms. Choke inductance under operating conditions = 40 henrys.

0.07 microfarad. As the above circuit constants correspond with those used in the experimental tests, it follows that, in the measured response curves of Fig. 3, the power peak shown in the curve for $C = 0.05$ microfarad is approximately the greatest

* *Ibid.*, pages 316 and 317.

obtainable with that circuit, and that, if further tests with smaller capacities had been carried out, the peak, whilst occurring at higher frequencies, would diminish in amplitude.

Throwing equation (11) into a form for the determination of ω in terms of C , L , and R_v we have

$$\omega^2 CLR_v^2 = R_v^2 + \omega^2 L^2$$

whence

$$\omega = \frac{R_v}{(CLR_v^2 - L^2)^{\frac{1}{2}}} \dots (12)$$

For coincidence between the values of ω defined by (3) and (12) we may write

$$\frac{R_v}{(CLR_v^2 - L^2)^{\frac{1}{2}}} = \frac{1}{\left(CL - \frac{R^2 C^2}{2} - \frac{L^2}{2R_v^2} \right)^{\frac{1}{2}}}$$

whence

$$R_v^2 \left(CL - \frac{R^2 C^2}{2} - \frac{L^2}{2R_v^2} \right) = CLR_v^2 - L^2$$

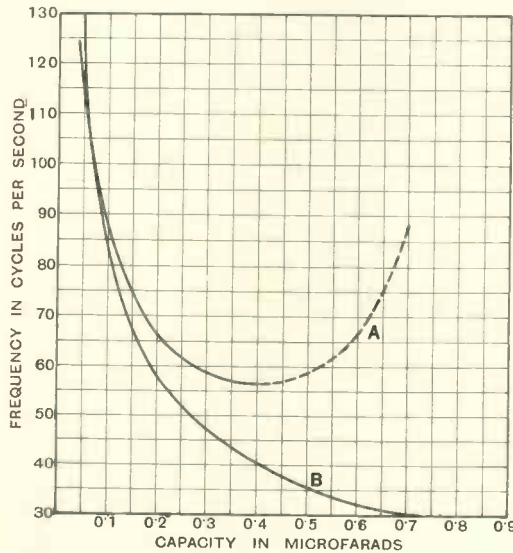


Fig. 7.—Curve A plotted from equation (3). Curve B plotted from equation (11).

Solving for C we have

$$C^2 R_v^2 R^2 = L^2$$

whence

$$C''' = \frac{L}{RR_v} \dots (13)$$

where C''' is in farads and represents the special value of C for this case.

Equation (13) therefore defines the capacity which will produce the utmost possible power peak.

The pulsance ω''' at which the coincidence peak will occur can be found by substituting for C''' in either (3) or (11). Taking the latter case we have

$$\omega''' = \left[\frac{1}{\frac{L^2}{RR_v} - \frac{R^2 L^2}{2R_v^2} - \frac{L^2}{2R_v^2}} \right]^{\frac{1}{2}}$$

whence

$$\omega''' = \frac{1}{L} \left[\frac{RR_v^2}{R_v - R} \right]^{\frac{1}{2}} \dots (14)$$

Inspection of (14) shows that ω''' is real only when R_v is greater than R . Therefore, when the usual load-matching relationships between R_v and R for pentode and triode are employed, the "coincidence effect" is confined to the pentode circuit.

Substitution of the values $R_v = 60,000$ ohms, $R = 10,000$ ohms, $L = 40$ henrys in (13) and (14) gives values of capacity and frequency of 0.067 microfarad and 108 cycles per second: these agree with the intersection shown by the curves of Fig. 7.

Summary.

The foregoing results may be summarised as below, the meanings of the various symbols being given by the circuit diagram of Fig. 1.

Case 1.—*Compensation of Power Response Curve for Uniform Response to Lowest Possible Frequency. (Level Compensation).*

$$C' = \frac{(10^6 L)}{R^2}$$

where C' is expressed in microfarads.

$$f' = \frac{0.225 RR_v}{L(R_v^2 - R^2)^{\frac{1}{2}}}$$

where f' is the lowest frequency at which uniform response can be maintained.

Case 2.—*Over-compensation of Power Response Curve at a Particular Low Frequency.*

$$C'' = 10^6 \cdot \left[\frac{R_v^2 + \omega^2 L^2}{\omega^2 L R_v^2} \right]$$

where C'' is expressed in microfarads and $\omega = 2\pi \times$ (frequency at which over-compensation is desired).

Case 3.—Maximum Possible Low Frequency Power—the Coincidence Case.

$$C''' = \frac{10^6 \cdot L}{RR_v}$$

$$f''' = \frac{1}{2\pi L} \left[\frac{RR_v^2}{R_v - R} \right]^{1/2}$$

where C''' is in microfarads and f''' is the frequency at which augmentation will occur.

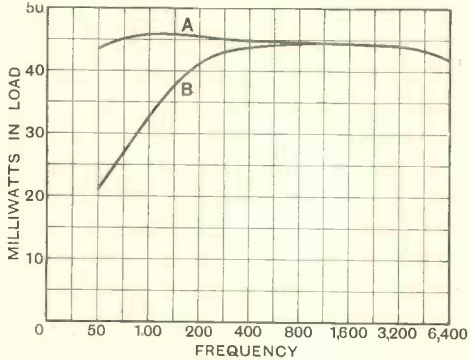


Fig. 8.—Experimental power response curves for Pentode PT240 choke-condenser coupled to resistance load. Curve A, coupling capacity, = 0.3 μF. Curve B, standard coupling condition C = 2.0 μF. Choke inductance = 40 henrys. Transformation ratio = 1.

It was pointed out in the analysis of Case 2 that the result applies to both triode and pentode. In practice, however, the over-compensation effect is sharply defined and of appreciable magnitude with the pentode, but ill-defined and of little acoustic significance with the triode. This results, as will be understood from a general explanation given in the Author's previous paper, from the much higher internal resistance of the pentode and its comparatively low resistance load. Moreover, as the effect is due to resonance between the coupling inductance and condenser, and the desired frequency of over-compensation is likely to be of the order 50 cycles per second, it follows that the triode, with its low inductance coupling, calls for a very large condenser. Thus, for a triode of 1,500 ohms internal resistance coupled to a load of 3,000 ohms, a coupling inductance of about 3 henrys is required (see reference in footnote 5, ante). For over-compensation at 50 cycles per second, the coupling capacity C''' works out to be

about 5.0 microfarads, a value which is appreciably greater than the 2.0 microfarads customarily employed. The calculation assumed a transformation ratio at the coupling inductance of unity. If this is not the case, the value of C''' must be multiplied by the square of the transformation ratio and rapidly becomes very great. Whilst, therefore, the calculation is of some value for the triode because it may indicate that, in certain cases, the usual 2.0 microfarads is much too small, at the same time it has little value as a means of augmenting power on account of the inconveniently large capacities required and the relatively small augmentation. On the other hand, a pentode of resistance 60,000 ohms calls for a coupling inductance of 40 henrys, which gives $C''' = 0.25$ microfarad for unity transformation ratio, a value of capacity which means an economy in condenser cost together with a degree of power augmentation which is of practical importance.

Experimental curves illustrating this and other aspects of the above analyses will be found in a paper published by the Author in *The Wireless World and Radio Review*, 29th June, 1932, and for this reason further illustration will be limited in the present contribution to Fig. 8, which indicates the improvement effected in a pentode experimental power response curve when the coupling condenser is reduced from 2.0 microfarads to 0.3 microfarads. The condition is approximately that of level compensation to 50 cycles per second.

Radio Research Board (of Australia) Reports Nos. 2, 3, and 4.

Report No. 2. Investigations on the state of polarisation of sky waves and height measurements of the Heaviside layer in the early morning, by A. L. Green. Pp. 80, with many diagrams.

Report No. 3. The influence of the earth's magnetic field on the polarisation of sky waves, by W. G. Baker and A. L. Green. Pp. 32, with 5 diagrams and addendum.

Report No. 4. A preliminary investigation of fading in New South Wales, by A. L. Green and W. G. Baker; Studies of fading in Victoria, on medium waves at short distances, by R. O. Cherry and D. F. Martyn; Observations on distant stations in which no ground wave is received, by R. O. Cherry. Pp. 59, with many diagrams.

Issued by the Council for Scientific and Industrial Research, Melbourne, Australia.

Interference.*

Notes on Methods for Elimination of Interference Caused by Non-radio Devices.

By E. T. Glas.

(Assistant Engineer, Swedish Board of Telegraphs.)

THE different kinds of interference caused to broadcast reception by various types of apparatus, fed from the mains, can be divided into: *low-frequency* (LF) and *high-frequency* (HF) phenomena. As in most practical matters, no sharp boundary-line can be drawn between the two species. However, no one will hesitate to characterise the well-known interference caused by a mercury rectifier with a fundamental frequency of 300 p.p.s. (6-phase rectifier) as a LF phenomenon, although it may contain HF components to some extent, nor will anyone be doubtful when confronted with a violet ray apparatus, where the fundamental frequency is usually about 200,000 p.p.s., as to the HF nature of the interference produced, although the exciting interrupter gives rise to a LF component too. As a rule, one of the two distinct components is predominant, and in most cases met with in practice this is the HF component.

As the causes of LF interference are usually well known and easily accessible to investigation, we may concentrate on the causes of HF interference. In the first place this interference seems to admit of being explained in one of the two following ways.

1.—The source of interference has the properties of a HF electromotive power, which gives rise to HF currents entering the mains.

2.—The source produces travelling pulses (which may be quite "aperiodic"), these pulses acting on periodic circuits, connected to the mains in some way, by means of shock-excitation.

In fact, experience shows that the actual interference in several cases is not affected by the insertion of an appropriately designed LF filter in the leads to the source, although oscillographic observation indicates that every irregularity of the supplied current, accessible to LF investigation, is smoothed

out. The explanation is simple if we accept alternative 1, the HF currents passing the LF filter, because the natural capacity of its coils is comparatively high. This capacity cannot be sufficiently eliminated without the inductance becoming too small for a complete smoothing action.

Thus, alternative 1 accepted, we may turn to the nature of the source. It is well known that the existence of a sparking gap of some kind or other is accompanied by radio interference. When the current through the gap tends to be large, the sparking effect usually gives place to a more or less stationary arc, and the corresponding interference will greatly diminish. However, arcs are liable to cause interference owing to the introduction of a negative resistance, the generated oscillations being modulated by such causes as mains noise, ozone-cleaners for factories, medical lamps, etc. As a rule arcs are nevertheless non-interfering. A typical example is afforded by the tramways, where experience clearly shows that the interference is strongest when the current consumed sinks to a minimum, *i.e.*, when the car is coasting and only the lighting system is fed. Moreover, the interference decreases on wet days owing to the easy formation on such days of true arcs in vapour. Any leakage, particularly in high-tension power lines, is accompanied by, it may be invisible, sparking effects and the corresponding interference will reveal the faulty insulator.

When studying any case of interference, it is essential to pay regard to three fundamental factors, namely, the wavelength of interfering currents, the time-curve of currents, and the propagation path from the source to the receiver.

1. **Wavelength**—As a rule most commutator-machines of a small and moderate size (power < 10 kw) cause the worst interference on the lowest broadcast-waves, $\lambda = 200 - 300$ m. Simple breaking-devices, as those of flashing-lamps, controlling

* MS. received by the Editor, April, 1932.

switches and relays of various types, on the contrary, are often most troublesome on the higher waves, $\lambda = 1,300 - 1,900$ m. The same may be said of violet-ray apparatus, where the actual wavelength of the tuned circuits falls within this range. Leakage, too, gives rise to considerable interference on the higher waves. With regard to arcs, fed from d.c. mains, the wavelength of the maximum interference will be found in some

in the case of apparatus designed to produce HF, such as violet-ray devices.

The three above-mentioned factors have been investigated by comprehensive practical study combined with measurements. There is, however, some doubt as regards the proper method of making such measurements. It has been established that the form of the time-curve is of great importance. As this can only be investigated by difficult and lengthy HF methods, the matter would be considerably simplified if an ordinary measurement of average values, such as a Moullin voltmeter,* could be employed. In fact, practice has shown that this can be done except in some extreme cases, where the ear alone must be relied upon. Fig. 1 shows the circuit that was used. The receiver must be operated at a normal HF input from a (local) broadcast transmitter. This cannot be done during the measuring procedure, but the results must be checked by the ear afterwards, while listening to a programme. If not, serious mistakes may be made. This quantitative method is of considerable advantage when studying the effect caused by altering the electric constants of an anti-interference device.

Before giving the results we will consider the design of such a device in the HF case. By far the simplest procedure, when the source is attacked, is to shunt a condenser

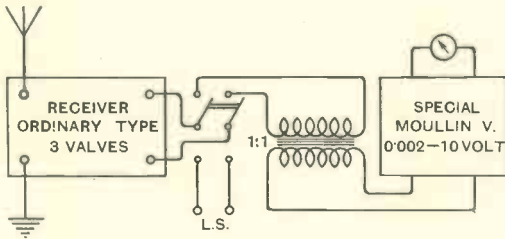


Fig. 1.

cases to change with time, owing to variable conditions of the arcing gas.

2. Time-curve of Current.—This factor is less accessible to direct observation except as regards the irregularities of the LF envelope. However, the indirect results must not be overlooked, as in the case, for instance, of a commutator machine. When one and the same machine of this kind (machine for d.c. or a.c.) is fed alternately with d.c. and a.c., the interference will be very different in the two cases and practically always at its worst in the latter case, where the commutating action is not very good, resulting, among other things, in an unfavourable time-curve.

3. Propagation Path.—Here we have to discriminate between two entirely different modes of propagation. The interfering currents may follow the mains direct to the receivers or may create induction or radiation fields, thus acting through free space, at least to some extent. Although both modes of propagation are met with in most cases, the former usually predominates, as might be expected. Even if this should not be the case, existing metallic wires and other parts have such great influence on the propagation, that the actual interfering effect is governed more by the situation with regard to the mains, etc., than by the geometric distance. Of course, the inductive influence is greatest

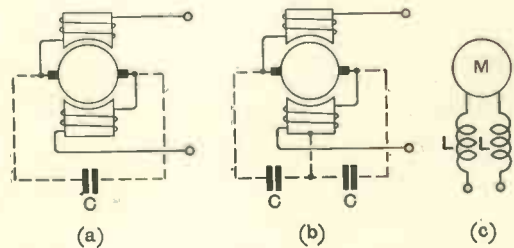


Fig. 2.

directly across the brushes or other contacts where sparks are generated (Fig. 2a). In the case of electric machines we can further take advantage of the capacity between the frame and the windings, by using two condensers

* When this instrument has a true square-law characteristic, the R.M.S. is measured independent of the curve-form. It is sometimes of considerable advantage to interconnect a filter, which cuts off very low and very high frequencies, according to the curve of sensibility of the human ear.

and connecting the midpoint to the frame of the machine* (Fig. 2b.) Where this arrangement proves to be satisfactory, ex-

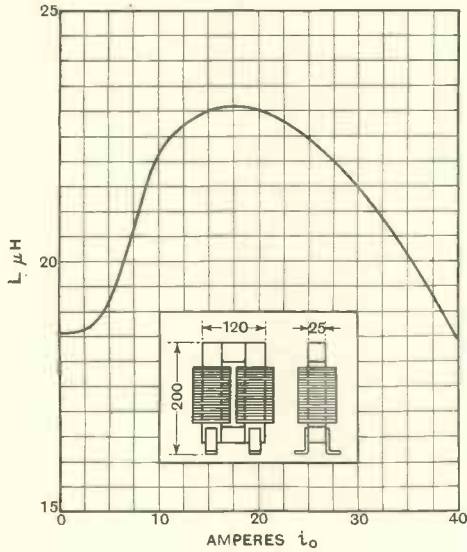


Fig. 3.

perience has shown that the following are the most appropriate values of capacity, small motors $C = 0.1 \mu F$, larger motors, generators $C = 2 - 4 \mu F$, unshielded circuit breaking devices $C = 0.5 - 2 \mu F$

In many cases, however, especially with a.c., the condenser method is ineffective, even when the condenser is combined with a series-resistance. The next step is to introduce an inductance, as shown in Fig. 2c. Here practice shows that good values are, for electric machines $L = 0.5 - 1.5$ mH circuit breaking points $L = 0.1 - 1.5$ mH according to the conditions.

The design of the coils may be discussed. Investigation has shown that a coil with iron usually has only slightly more inductance at HF than the same coil constructed without iron, although the inductance at LF may

be 50 times as high in the former case. On the other hand, the unfavourable natural capacity of the coil is increased several times by the presence of iron. Thus there does not seem to be any reason to adopt iron when the interference has a pure HF character. Where this is not the case, as for instance in a small generator or a motor of considerable size, fed from a relatively small local power supply, coils with iron will very often prove to be superior owing to the existence of a LF component, which may attain 30 per cent. of the total interference (as shown by measurement of rectified average voltages). When iron is used, care must, of course, be taken to prevent saturation. This is best done by leaving an appropriate air-gap in the magnetic path. Thus coils of at least 20 mH, measured at $\omega = 2\pi \cdot 2,000$, can be constructed at a reasonable cost. Their inductance at HF will nevertheless seldom exceed $0.5 - 1$ mH, the natural capacity is usually of the order of $300 - 700 \mu\mu F$, all values applying to coils designed for a maximum continuous current of about 50 amps. d.c. Fig. 3 shows the influence of current load on inductance for such a coil of commercial construction, at LF. When the current does not exceed say 8-10 amp.—and the HF component is predominant—coils should always be designed without iron. By well-known methods of winding, the natural capacity in this case can be lowered to about 10 $\mu\mu F$ at an inductance of $1 - 1.5$ mH, without disregarding economy.†

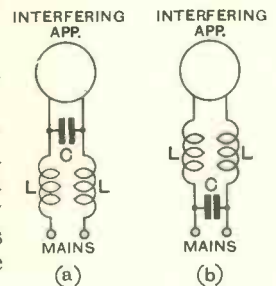


Fig. 4.

The last step is to introduce complete HF filters, which unfortunately will very often be found quite necessary for circuit breaking points such as relays, switches, keys, etc., and also for several types of electric machines, particularly big ones.

* In the a.c. case any dangerous capacity-current should be avoided by inserting a protecting condenser ($\cong 5,000 \mu\mu F$) in the lead from the midpoint of the series condensers to the frame. Where a reliable earth is present, this safety-rule can be neglected of course, but it is of importance in many cases (vacuum-cleaners, fans, etc.), where the frame may not be insulated and, moreover, easy to touch.

† It is, of course, not quite true to look upon the natural capacity as simply shortening the coil, when this capacity is not very large. However, a more intimate study reveals that the said capacity comes out to be chiefly harmful when constructing a reasonable choking coil for frequencies within the broadcasting range.

Fig. 4a, b shows the two simplest forms of symmetrical HF filters, the electrical symmetry being generally of advantage for the

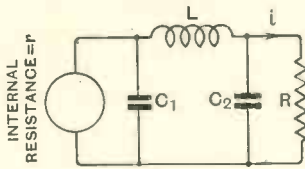


Fig. 5.

elimination. When shall type a be used, when type b? This, of course, greatly depends on the impedances of the source and of the network in relation to each other. Let us consider a simplified circuit according to Fig. 5, where the internal impedance of the sources is replaced by a lumped resistance. Instead of assuming a pure sine E.M.F., we may consider an E.M.F. of the more general form of Fig. 6.

First taking $C_2 = 0$ the method of Heaviside gives the symbolical formula,

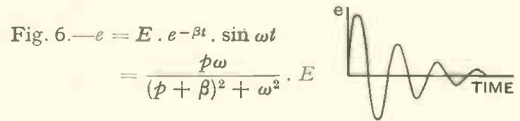
$$i = \frac{E}{rLC_1} \cdot \frac{p\omega}{\{(p + \beta)^2 + \omega^2\} \cdot \left\{ p^2 + p \left(\frac{R}{L} + \frac{I}{rC_1} \right) + \frac{I}{LC_1} \left(I + \frac{R}{r} \right) \right\}} \quad (1)$$

where $p = d/dt$.

If, however, $C_1 = 0$ we have

$$i = \frac{E}{RLC_2} \cdot \frac{p\omega}{\{(p + \beta)^2 + \omega^2\} \cdot \left\{ p^2 + p \left(\frac{r}{L} + \frac{I}{RC_2} \right) + \frac{I}{LC_2} \left(I + \frac{r}{R} \right) \right\}} \quad (2)$$

It appears immediately that the two formulas are quite identical but for the reciprocal substitution of r by R and *vice versa*. The generated current of the forced



angular frequency ω is here of interest, and for this component we have $(p = -\beta \pm j\omega)$ from . . . (1)

$$i_\omega = \frac{E}{rLC_1} \cdot e^{-\beta t} \cdot \frac{\sin(\omega t + \phi_1)}{\sqrt{\left[\frac{I}{LC_1} \left(I + \frac{r}{R} \right) - \beta \left(\frac{r}{L} + \frac{I}{RC_1} \right) - \omega^2 + \beta^2 \right]^2 + \left[\omega \left(\frac{r}{L} + \frac{I}{RC_2} \right) - 2\beta\omega \right]^2}}$$

As the curve-form is extremely variable in most practical cases, we can substitute a series of HF pulses. One of these will produce a current corresponding to $\beta \rightarrow \infty$, the square-root thus becoming independent of the circuit-constants and

$$|i_\omega| = \frac{E}{rLC_1} \cdot e^{-\beta t} \cdot f_1(\beta, \omega) \quad \dots \quad (1a)$$

Similarly from . . . (2)

$$|i_\omega| = \frac{E}{RLC_2} \cdot e^{-\beta t} \cdot f_2(\beta, \omega) \quad \dots \quad (2a)$$

Consequently a condenser C_1 should be found preferable, when the internal "resistance" of the source is much greater than the network impedance ("small" machines),

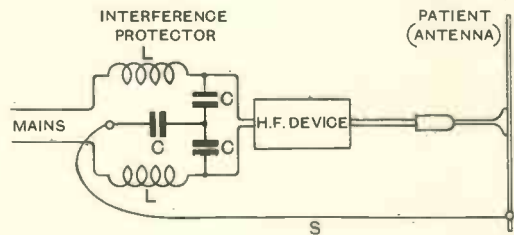


Fig. 7.

whereas a condenser C_2 should be adopted in the opposite case ("big" machines). This has been fully confirmed by practice. Thus the arrangement shown by Fig. 4a has proved to be suitable for small machines and to afford the only reliable method in the case of circuit breaking points, Fig. 4b for machines, the power of which exceeds about 2 kW. This fact does not seem to have been fully recognised in the construction of several anti-interference-devices now on the market. As a rule, the field-coils of a series-machine cannot be regarded as effective chokes at HF owing to their large distributed capacity.*

Before leaving this question we might consider a very special type of device, namely, the type designed for the elimination of interference caused by violet-ray apparatus (Fig. 7). Such a device has two functions, *viz.*, choking the mains-leads and preventing excessive induction from the patient's body. The latter function is performed by the metallic lead S, which transforms the open circuit of the body into a closed circuit with

* For unshielded breaking-points, however, a considerable choking effect of such coils is found to exist, *e.g.*, for ringing-bells.

less pronounced action at a distance. Nevertheless, the choking device must be carefully designed with coils of an inductance of the order of 50 mH, and condensers not smaller than 5,000 $\mu\mu\text{F}$. Of course, a Faraday cage could be safely used to prevent induction. The above arrangement, however, will often do. Where the interference is purely of a LF nature, the general design of the device can be maintained, but inductance and capacity must be increased. While HF interference is best attacked at the source, the LF type can usually be completely eliminated at the receiver as well. A particularly important case is the smoothing of the pulsating current from mercury rectifiers. Here a filter consisting of one coil with iron, inductance not less than 2 H, and a condenser of 4-6 μF , shunted across the leads on the receiver side, has been found commercially possible, when the current consumption of the receiver does not exceed 0.3 amp.

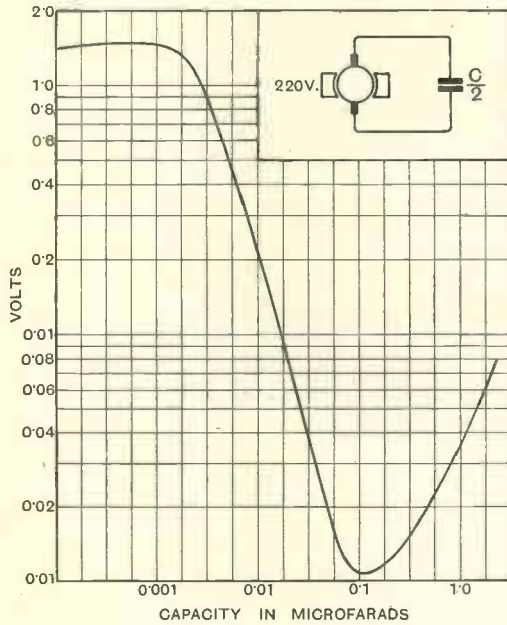


Fig. 8.

Some results of the above-mentioned measurement of average interference-voltages are shown in Figs. 8 and 9. The curves represent the interference from an adding-machine, Fig. 8 dealing with the interference from the motor (1/20 HP, 220 volt d.c., 1,725 r.p.m.) and Fig. 9 that from the start-

and-stop key. Appropriate schemes of protective devices will be seen from the drawings. The optimum values of the electrical constants (L and C) can easily be extracted. Note, in particular, the influence of the in-

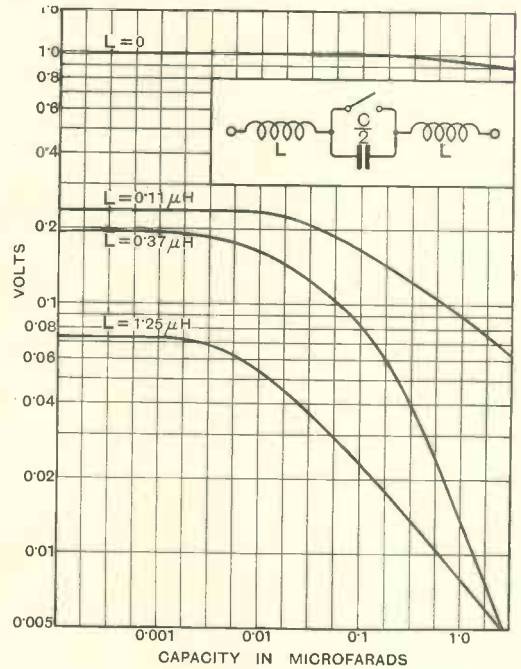


Fig. 9.

ductance in Fig. 9. If coils of a certain minimum value of inductance are not inserted, condensers are of no avail, no matter how large. Other curves of interfering devices not reproduced here show a marked resonance-effect for a certain value of the capacity, especially when the coils are very small. Such points must be carefully avoided, as otherwise a pronounced deterioration may result instead of the desired elimination of interference.

To conclude this brief survey, some words should be said about the elimination of interference from sliding contacts, such as those of tramways. The only way of solving this problem seems to be the installation of bows having the proper mechanical and electrical qualities to prevent the generation of sparks. Two different designs have been adopted in practice, namely, bows of iron (with copper-edges and lubrication grooves), called Fischer-bows, and bows furnished with carbon.

Correspondence.

Letters of technical interest are always welcome. In publishing such communications the Editors do not necessarily endorse any technical or general statements which they may contain.

High-Selectivity Tone-Corrected Circuits.

To the Editor, The Wireless Engineer.

SIR,—Since the Radio Research Board considered the subject of High Selectivity Tone-Corrected Receiving Circuits of sufficient importance to appoint a special committee to investigate and report upon the merits of receivers of this type, one would have expected a journal of the standing of *The Wireless Engineer* to have dealt with the subject in an unbiased and comprehensive manner.

Instead of this, the writer of the Editorial dealing with the subject in your November issue allowed himself to be flustered by newspaper articles to such an extent that he failed to appreciate the importance of the subject with which he was dealing, and allowed his natural bias to carry him away to such an extent that he even criticised the report itself; but on this point G. W. O. H. can safely be left to his colleagues.

If G. W. O. H. could have forgotten that he was a member of the Radio Research Board, and in his capacity as journalist endeavoured to present an unbiased and explanatory criticism of the Report for the benefit of your readers, he would have found numerous important facts concealed in the verbiage of the Report, which facts are of fundamental importance to the wireless industry, and should have been made clear to your readers.

Apart from these facts, G. W. O. H. might have remedied the omission of his Board, and in fairness to me made it clear that the Special Committee referred to was really appointed to investigate my discoveries (the "Stenode") as a direct result of the early demonstrations which I gave to certain scientists who happen to be members of the Radio Research Board, including Prof. E. V. Appleton, Mr. Watson Watt, and Col. Fuller, at which demonstrations they admitted that the "Stenode" had revealed new phenomena in wireless, which phenomena were of sufficient national importance to warrant a Government investigation.

Instead of giving me credit for these discoveries, G. W. O. H. preferred to follow the lead of his Board and endeavoured to conceal rather than reveal in a tangible form the true facts.

Probably the last paragraph of the article was put in to make up the requisite number of words for the Editorial, but surely it is not the function of your Journal to give its readers a lesson in spelling, and one would have thought that if G. W. O. H. wished to be such a purist he would have remedied such spelling defects in the early drafts of the Report, of which, presumably, he had copies.

J. ROBINSON.

London, W.I.

[It is not clear from the above letter whether Dr. Robinson regards the Radio Research Board or Mr. Colebrook or Prof. Appleton or G. W. O. H. as the chief villain of the piece.

That will depend on whether he considers the greater criminal to be he who conceals in verbiage numerous facts of fundamental importance to the wireless industry, or he who fails to find them and make them clear. The Editorial made no pretence of dealing with the subject in a comprehensive manner—that was unnecessary, as it had been done very thoroughly by Mr. Colebrook in the Report itself—but we do say, unhesitatingly, that it was entirely free from bias, even from "natural bias," which is presumably a kind of original sin.

There is one point in the Editorial to which we should like to refer. We said that the effect of the suppression of a neighbouring carrier by means of the quartz crystal rejector would be somewhat like a piano with one or two notes missing. We said "somewhat" because the notes would not be entirely missing unless the corresponding side-bands on both sides of the carrier were suppressed, but we confess that even then the analogy is hardly fair, because the reduction of loudness due to the elimination of one side-band would probably be much less than the analogy suggests, and might, indeed, be hardly noticeable in ordinary use.

What the newspaper articles are to which Dr. Robinson refers we do not know; we referred to one only, and that the one with which the "Stenode" burst upon an astonished world. Rightly or wrongly we have always regarded this as having been inspired by Dr. Robinson, but we certainly never allowed ourselves to be flustered by it. The Editorial Note drew attention to the Report, the price, and where it could be obtained, gave a brief historical preamble showing how interest in the subject had arisen, and after a brief summary of the results of the investigation, concluded by discussing one or two points of minor importance, but yet of sufficient interest, in our opinion, to merit reference. Dr. Robinson little knows how much time an Editor spends modifying spelling, symbols, and grammar: we have even taken the liberty of correcting the grammar of his letter. It becomes a habit.

We should like to emphasise that the Report was not concerned with the distribution of credit for discoveries, but only with a scientific investigation of a much discussed problem, and we respectfully decline the invitation to rush in where the Radio Research Board feared to tread. References were given throughout the Report and in the bibliography to the work of those who had published anything throwing light on the subject, and if Dr. Robinson plays a very small rôle in the list the blame does not lie at the door of *The Wireless Engineer*.

At the foot of p. 605 we gave a list of names of those who had contributed articles on the subject to this journal. This list should have included the names of Professor Appleton and Mr. Boohariwalla, whose article was published in March of

this year. Although the list made no pretence of being complete, this paper should have been mentioned, as it is discussed in the Report.—G. W. O. H.

"Capacitative."

To the Editor, *The Wireless Engineer*.

SIR,—My attention is directed to an *obiter dictum*, which, I confess, I view with certain misgiving, and which I note with amazement appears above the renowned denonimant "G. W. O. H." in the Editorial column of your journal for November, 1932.

This concerns the abrogation—I might call it wanton dereliction—of a syllable of the word which I have designated above. While I have every sympathy with your eminent contributor in his laudable campaign for brevity coupled with clear thinking, I cannot but remember that almost equally renowned savants have shared with me the euphonic if longer form of this word in the past.

I am humbly aware that precedent in the form of prior use is no concrete argument because of the notorious negligence of genius in details. Nevertheless, in my stumbling research for truth I have come upon "confirmive" evidence in several dictionaries that "capacitative" may be thought to be formed from "capacitate," not by removal and substitution, but by addition.

It is in no carping or "argumentive" vein that I approach this matter; I would like to know, however, whether your contributor's statement is "representive" of your own opinion, and is therefore to be taken as "authoritive"?

Nt. Harrow.

J. C. WILSON

To the Editor, *The Wireless Engineer*.

SIR,—I am shocked and horrified at the last paragraph of your current Editorial.

Ever since a stern comment appeared in your columns in respect of the lapses from pure English which took place at a certain I.E.E. meeting, I have regarded your Technical Editor as one before whose "authoritative" pronouncements sinners like myself might well quail, but if they are only "authoritive," how can I consider them in the same light?

I cannot waste your space in an attempt to expound my contention that the word "capacitative" is etymologically correct, but I implore Dr. Howe to investigate the Latin origins of the words at issue and then to reconsider his verdict. Any assurance that we may be spared the compulsory use of analogous abbreviations such as "qualitive," "quantitive," etc., will be anxiously awaited by

Hampstead, N.W.3.

Successive Heterodyne Receivers.

To the Editor, *Wireless Engineer*.

SIR,—In his paper in the November issue of *Wireless Engineer and Experimental Wireless*, Mr. E. L. C. White is hardly correct in attributing novelty to the practice, described in *The Wireless World's* article of May 6th, 1931, of feeding signals to the grid and heterodyne to the anode of a bottom-bend triode detector, as this method was de-

scribed seven years before the article in question, in British Patent Specification No. 226,050 (1924).

Considerations stressed in the Shorter Catechism led me in 1923 to adopt "anode-fed" front-detector circuits, with a screened heterodyne, in the pious hope that the few centimetres anode-grid capacity of the detector might not pass enough heterodyne power through two loosely coupled circuits (tuned not to heterodyne but to signal frequency) to cause appreciable heterodyne radiation. It remained for N. P. Hinton, in 1927, to devise oscillator circuits with "overhang" and to neutralise the interelectrode capacity of an anode-fed detector, and for Mr. E. L. C. White, in 1932, to show us, with a four-electrode valve, the best way of avoiding heterodyne radiation. *Palmas qui meruit fevat!*

C. R. BURCH, Research Department.

Metropolitan-Vickers Elec. Co., Ltd.

Book Review.

The True Road to Radio.

By Albert Hall, A.R.C.Sc., M.I.R.E., Wh. Ex. Ferranti, Ltd., Hollinwood, Lancashire. 3rd edition.

The object of this book is to give a comprehensive survey of the principles of wireless as applied particularly to high quality receiver design, and in this it succeeds admirably. The treatment adopted is first to describe the problem in simple terms, secondly to investigate the matter technically, and thirdly, to illustrate the practical results obtainable by measurements on Ferranti apparatus.

A large section of the book is devoted to tuning systems and high-frequency amplification; the superheterodyne, however, is only cursorily touched upon, and no mention is to be found of such a recent development as the variable- μ valve; this is, we understand, because to include this material would have meant an unjustifiable delay in publication of the new Edition which was in demand. Both anode bend and grid detection are thoroughly dealt with, and low-frequency and power output stages are treated with a wealth of illustrative data. The use of valve curves for determining the optimum operating conditions is stressed, and numerous examples are given. It seems to the reviewer, however, that a note should have been included to the effect that the curves illustrated are not necessarily applicable to valves at present available under the same type numbers, but to older specimens. It is unfortunate also that an error should have crept into the section dealing with resistance-capacity coupling, wherein it is stated that if the grid leak be increased in value so also must the coupling condenser be increased in capacity. Actually, of course, the coupling capacity is inversely proportional to the resistance of the grid leak.

Although the treatment is largely non-mathematical, a number of formulae are included as an aid to design; those intending to employ them, however, should note that they are not entirely free from printing errors. The book is profusely illustrated and the numerous curves and other data relating to Ferranti components render it as useful for reference as for its more legitimate purpose of explaining the nature of the problems of receiver design and indicating at least one method of solving them.

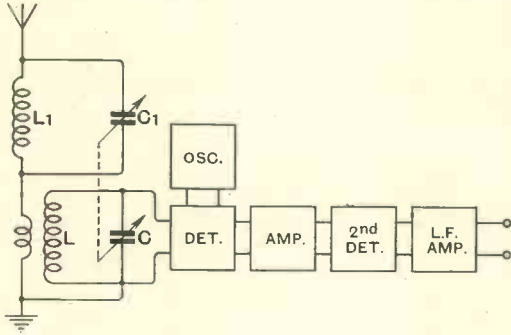
Some Recent Patents.

The following abstracts are prepared, with the permission of the Controller of H.M. Stationery Office, from Specifications obtainable at the Patent Office, 25, Southampton Buildings, London, W.C.2, price 1/- each.

SUPERHETERODYNE RECEIVERS:

Application date, 26th March, 1931. No. 375410.

In order to eliminate second-channel interference in a superhet set, more particularly one of the type in which a low intermediate frequency is used,



No. 375410.

say, 40 kilocycles, a rejector circuit L_1, C_1 is inserted in, or coupled to, the aerial, and is so ganged with the ordinary input circuit L, C as to maintain a constant "difference" frequency, equal to twice the intermediate frequency employed. Both the rotor and stator of the condenser C_1 must be insulated with respect to earth. A construction of condenser suitable for ganging the two circuits together is described in the specification.

Patent issued to J. Robinson and British Radiostat Corp., Ltd.

TELEVISION SYSTEMS.

Application date, 6th February, 1931. No. 374094.

Relates to scanning-apparatus of the type in which a rotating apertured drum co-operates with a rotating mirror-wheel set at right-angles to the drum. In an arrangement designed to scan an object in fifty lines, fifteen times per second, over a square area, the apertured drum is 9.7 inches in diameter with thirty apertures each 0.017 inch square. The mirror wheel is 9.5 inches in diameter and is fitted with twenty-five tangential mirrors each 2 by 1.2 inches. The motor speed is 1500 revs. per minute, the drum being driven through reduction gearing at thirty-six revs. per minute. This enables a picture ten feet square to be covered at a distance of approximately twenty feet from the mirror.

Patent issued to Marconi's Wireless Telegraph Co., Ltd., and H. M. Dowsett.

Convention date (U.S.A.), 2nd April, 1930.
No. 374974.

To allow the received picture to be "monitored," provision is made to project a second facsimile

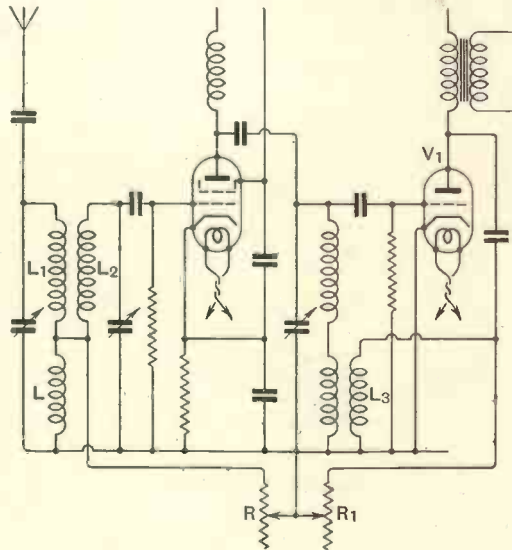
picture for the information of a station supervisor outside the cabinet containing the main observer, and without obstructing the latter's view of the primary reproduction. The spiral line of apertures on the scanning-disc overlaps the full 360° by an extra 90° , and a part of the emission from the Neon lamp is diverted through a mirror-and-lens system to pass through a part of the scanning-disc separated by 90° from the part through which the main picture is viewed. A second mirror on the far side of the scanning-disc then reflects the secondary picture through a window in the observer's cabinet to the supervising attendant outside.

Patent issued to Electrical Research Products Inc.

VOLUME AND SELECTIVITY CONTROL.

Application date, 24th March, 1931. No. 375357.

A resistance R in parallel with a coil L coupling the two tuned circuits comprising L, L_1 , and L_2 , of a band-pass input serves as an input volume control which does not disturb the tuning of the ganged circuits. In addition it can be used to regulate the band-width passed by the filter circuit, and therefore the selectivity of the set as a whole. A second resistance R_1 is inserted in parallel with a



No. 375357.

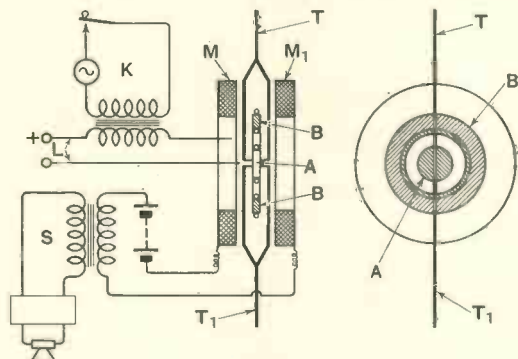
back-coupling coil L_3 in the output of the detector valve V_1 in order to control reaction. The two resistances R, R_1 are coupled together as shown.

Patent issued to F. Murphy and E. J. Power.

HIGH-FREQUENCY GENERATORS.

Convention date (U.S.A.), 14th July, 1930.
No. 374311.

High-frequency currents are generated by applying a breakdown voltage from leads *L* across two concentric electrodes *A*, *B* mounted inside a gas-filled container (not shown). As soon as the arc is formed it is made to rotate rapidly, around the annular gap between the electrodes, by the magnetic



No. 374311.

field from two solenoids *M*, *M*₁. In its rotation the arc, or discharge current, induces a rapidly alternating EMF in the bifurcated ends of a pick-up wire *T*, *T*₁ which is used as a transmitting aerial. Morse signals may be superposed by a keying-circuit *K* coupled to the supply leads *L*, or speech signals from a microphone circuit *S* coupled to the solenoid windings *M*.

Patent issued by Marconi's Wireless Telegraph Co., Ltd.

REMOTE TUNING-CONTROL.

Convention date (U.S.A.), 18th October, 1930.
No. 372687.

In order to tune a superheterodyne set from a distance, the local oscillator in the set is of the multi-vibrator type, wherein the generated frequency depends upon the value of one of the circuit elements, for instance the grid leak or the anode coupling-resistance. The space-current path of an auxiliary valve is arranged in parallel with this frequency-determining element, and the internal impedance of the auxiliary valve is then adjusted from a distance by means of a grid-bias rheostat. The frequency-adjusting rheostat is conveniently combined with a volume-control potentiometer.

Patent issued to Marconi's Wireless Telegraph Co., Ltd.

TWO-WAY TELEVISION.

Convention date (U.S.A.), 1st October, 1930.
No. 371612.

In a two-way television system the analysing system at the receiving end is also utilised to "monitor" the outgoing transmission, so as to give what might be called a "sidetone" representation to the local subscriber of the picture of himself that is being sent to his distant correspondent. The incoming picture is built up by means of a

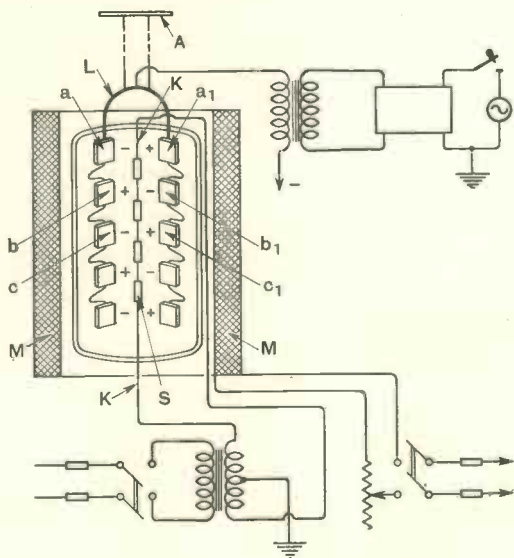
scanning arrangement of the kind in which an electric arc is traversed in zig-zag fashion along a series of interleaved electrodes by the action of a magnetic field created by an electric current encircling the electrode system. A local oscillator superposes an alternating current on the electrode system whereby the latter reproduces, during alternative half-cycles, the incoming picture of the distant correspondent, and during the intervening half-cycles serves as a mirror in which the local correspondent may observe how his image is appearing on the screen at the distant point.

Patent issued to Communication Patents Inc.

SHORT-WAVE OSCILLATORS.

Convention date (U.S.A.), 21st July, 1930.
No. 375095.

Wavelengths of the order of decimetres are generated in a valve of the split-anode "magnetron" type by making each of the anode sections electrically long relatively to the generated wave, and setting them close to each other so as to increase their mutual inductance. As shown each anode consists of a number of "targets" *a*, *b*, *c*, etc., and *a*₁, *b*₁, *c*₁, etc., connected in series by looped wires. The central cathode *K* is screened at intervals by sleeves *S*, so that the electron stream is concentrated on the "targets." The whole assembly is surrounded by a solenoid *M*, producing an axial magnetic field. The effect of this upon the transverse electron stream is to create a standing-wave on the sectionalised anodes, as indicated



No. 375095.

by the progressive + and - signs. The anode sections are connected at their upper ends by a looped wire *L*, from which the HF energy is tapped off to a radiating aerial *A*.

Patent issued to Marconi's Wireless Telegraph Co., Ltd.

SCANNING FOR TELEVISION.

*Convention date (U.S.A.), 7th August, 1930.
No. 375589.*

A single rotating cylinder is arranged to give an equivalent scanning-point to that produced by two separate rotating discs with intersecting scanning-lines. The rim of the cylinder is made sufficiently wide to accommodate a series of inclined parallel slots. Light from a Neon lamp is projected by a lens through one of the slots on to a double set of right-angled prisms, which reflect the image of the slot back through a slot on to a lower point of the same cylinder. Owing to the double reflection through the prisms, the image of the original slot is rotated through 90°, so that it intersects lower slot at right angles, so as to produce a single scanning "point."

Patent issued to A. J. Cawley.

ELIMINATING "MAN-MADE" STATIC.

*Convention date (U.S.A.), 25th February, 1931.
No. 375737.*

The specification analyses local interference into: (a) that carried by the electric mains which are the common source of supply for domestic labour-saving apparatus, lifts, violet-ray appliances, and other sparking-devices, as well as for the receiving set; (b) field "pick-up" by the aerial and the lead-in, as well as by the coupling-coils in the set, such "fields" being of comparatively limited spread. According to the invention, a receiving set is rendered substantially immune from such interference (1) by locating the aerial in some remote place, say on the top of the roof of an hotel or apartment house, outside the area of spread of the local fields of induction; (2) by providing a screened transmission line or lead-in of low impedance, coupled to the input circuit of the receiver through a filter circuit designed to reject low-frequency disturbances due to sparking-devices. (3) The mains supply unit is also carefully screened, as well as the set, and also the opening through which the sound emerges from the loud speaker. (4) The screening-sheath covering the lead-in or transmission line from the remote aerial is preferably grounded at several points along its length.

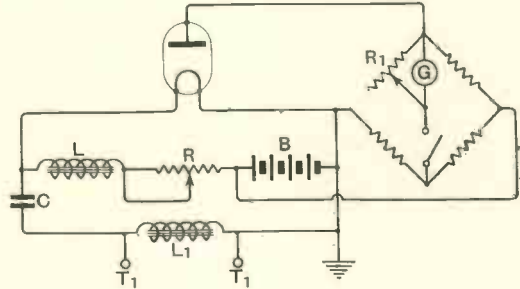
Patent issued to Marconi's Wireless Telegraph Co., Ltd.

A.C. METERS.

Application date, 20th August, 1931. No. 376066.

A direct-reading A.C. meter, suitable for low-impedance circuits, and capable of measuring currents varying in value from micro-amps to amperes, and varying in frequency from 25 cycles to 6,000 kilocycles, is based on the known principle of injecting the A.C. current to be measured into the filament of a thermionic valve and then measuring the resulting increase in plate current. The invention is characterized by the feature that the valve is at all times adjusted to pass a saturation current, the increase in the latter, after the application of the A.C. current, giving the desired indication. As shown the filament is heated by direct current from the battery B, through a resistance R and choke L which serve to reduce the applied P.D. say to 2 volts or other rated value. A unipivot

galvanometer G is inserted across the diagonal of a Wheatstone-bridge network, one arm of which contains the inter-electrode capacity of the diode or other valve. The current to be measured is applied across the terminals T, T₁, shunted by a heavy choke L₁ and passes through an electrolytic condenser C to the filament. A resistance R₁ serves



No. 376066.

to compensate the galvanometer G for casual variations in temperature.

Patent issued to H. E. M. Barlow.

GENERATING ULTRA-SHORT WAVES.

*Convention date (U.S.A.), 28th July, 1930.
No. 373847.*

Waves a fraction of a centimetre long are generated by passing spark-discharges through a colloidal solution containing metallic particles. In operation the spark "grape vines" itself, i.e., follows branched paths through the liquid and sets up a series of sub-discharges from the ends of the metallic particles. These in turn generate damped oscillations of a wavelength corresponding to the natural "period" of the particles in solution, so that with particles of uniform size the radiation is confined to a comparatively narrow band of waves. To create a more or less uniform distribution of energy, the solution may be subjected to heavy pressure, whilst further concentration is effected by means of a backing-reflector of parabolic section.

Patent issued to Marconi's Wireless Telegraph Co., Ltd.

PRODUCING CIRCULARLY-POLARIZED WAVES.

*Convention date (Germany), 13th October, 1930.
No. 375165.*

Circularly-polarised waves, which are known to be largely free from fading effects, are produced by feeding HF energy to an aerial system consisting of two conductors twisted around an imaginary cylinder, the two spiral paths being 180° out of phase. Transverse radiators are preferably arranged along the length of each wire, and may extend inwards, i.e., between the two wires, or project outwards from the double line, or both. The ends of the twisted aerials are connected together through a terminating resistance.

Patent issued to Telefunken Ges. für Drahtlose Telegraphie m.b.H.

INDEX.

VOL. IX. The Wireless Engineer & Experimental Wireless. 1932.

I. GENERAL INDEX.

	PAGE		PAGE
A BSTRACTS AND REFERENCES (<i>see separate Index</i>)		Radio Telegraphy and Telephony, Duncan and Drew	215
A.C. Motors (<i>Patents</i>)	689	Thermionic Vacuum Tubes and their Application, E. V. Appleton	328
Acoustic and Telephone Measurements (<i>I.E.E. Paper</i>), H. R. Harbottle	451	Les Unités Electriques, J. Sudria	395
Acoustic Nomenclature and Definitions (<i>Editorial</i>)	307	Alternating Current Bridge Methods (3rd Edition), B. Hague	448
(<i>Correspondence</i>)	448	Handbuch der Bildtelegraphie und des Fernsehens, F. Schröter	617
Acoustic Studies (<i>Patents</i>)	663	True Road to Radio, A. Hall	686
Aerial, Directive, New Type, T. Walmsley	622	BOOKS RECEIVED: 66, 139, 328, 395, 448, 511, 617, 679	
Aerials, Drying-out (<i>Patents</i>)	543	Broadcast Relay Systems (<i>Patents</i>)	484
Aircraft D.F. Station at Pulham	122	Broadcasting, Common Wave (<i>Patents</i>)	425
Aircraft Set in Mrs. Victor Bruce's Aeroplane (<i>Illustration</i>)	428	Broadcasting House (<i>Illustrations</i>)	309
Aircraft Sets (<i>Patents</i>)	366	Broadcasting with Ultra-short-waves (<i>Editorial</i>)	59
Amplifiers for A.C. Valves (<i>Patents</i>)	423	C apacitive Output Coupling, L. G. A. Sims	314
Amplifier Tone-control Circuits, M. G. Scroggie (<i>Correspondence</i>)	3	Carrier Interference Eliminator, W. Baggally	388
Amplifiers (<i>Patents</i>)	153	Cathode-Ray Indicators (<i>Patents</i>)	362, 365
Amplifiers, Convertible (<i>Patents</i>)	603	Cathode-ray Oscillograph in Radio Research (Royal Soc. Demonstration)	449
Amplifiers, Direct-coupled (<i>Patents</i>)	425, 246	Cathode-Ray Tubes (<i>Patents</i>)	56, 425, 664
Amplifiers, Resistance-coupled (<i>Patents</i>)	484	Cathodes, Thermionic (<i>Patents</i>)	544
Amplifiers, Short-wave (<i>Patents</i>)	306, 661	"Centimetre" Waves, The Generation of, F. W. Chapman	500
Analysis and Design of a Chain of Resonant Circuits, M. Reed	603	Changes in Patent Procedure	557
Aperiodic Impedance Measuring Set, A. T. Starr	259, 320	Circularly-Polarized Waves (<i>Patents</i>)	689
(<i>Correspondence</i>)	325	Common Error (<i>Correspondence</i>)	274
"Apparent Demodulation," Another View-point, E. Mallett	447	Condenser Circuits (<i>Patents</i>)	243
(<i>Correspondence</i>)	248	Condensers (<i>Patents</i>)	362
Articles, Preparation of (<i>Editorial</i>)	394, 247	Constant-band Tuning (<i>Patents</i>)	302
Association of Special Libraries and Information Bureaux, Scientific Abstracts	19	Constant-coupling Circuits (<i>Patents</i>)	116, 181, 481, 604
Automatic Calling Apparatus (<i>Patents</i>)	544	Constant-frequency Generators (<i>Patents</i>)	58
Automatic Gain Control (<i>Patents</i>)	365	CORRESPONDENCE, 23, 75, 150, 213, 273, 319, 394, 573, 629, 685	
Automatic Grid-bias (<i>Patents</i>)	58	Cosser Cathode Ray Oscillograph	387
Automatic "Stand-by" Circuits (<i>Patents</i>)	363	Coupled Circuits, Some Properties of, R. C. Clinker and T. H. Kinman	11
Automatic Volume Control (<i>Patents</i>)	118, 604, 662	Coupling and Coupling Coefficients (<i>Editorial</i>)	485
"Autotone," Wireless World (<i>Illustration</i>)	135	Coupling Circuits (<i>Patents</i>)	302, 364
B and-pass Circuits (<i>Patents</i>)	661	Current-limiters (<i>Patents</i>)	425
Band-pass Couplings (<i>Patents</i>)	482, 483, 484	D amping of L.F. Oscillations in a M.C. Loud Speaker, N. W. McLachlan	559
Band Pass Filter, Design of, N. R. Bligh	61	Daventry, Empire Station, Masts (<i>Illustration</i>)	607
Band Pass Filters, Resistance in, G. H. Buffery	504	Decibel and Gain Control, H. Stanesby	18
Band-pass Filters, The Theory of, C. W. Oatley	608	"Demodulation, Apparent," Another View-point, E. Mallett	248
Band-pass Filter, Two-element, R. T. Beatty	546	(<i>Correspondence</i>)	394, 629
Beacons, Navigation (<i>Patents</i>)	426	Design of the Band Pass Filter, N. R. Bligh	61
B OOK REVIEWS:		Detection by a Straight Line Rectifier of Modulated and Heterodyne Signals, E. B. Moullin	378
Wireless, L. B. Turner	25		
Siebhaltungen (Filter Circuits), W. Cauer	26		
Radio Construction and Repairing (3rd Edition), J. A. Moyer and J. F. Wostrel	66		
Dictionary of Electrical Terms, S. R. Roget	129		

	PAGE		PAGE
Detector, The, W. B. Lewis	487	Gramophone Pick-ups, etc. (<i>Patents</i>)	55, 56, 117, 304, 542
Detector Problems, The Graphical Solution, G. S. C. Lucas	202, 253	Grid Bias from Anode Current, F. J. A. Pound	445
(<i>Correspondence</i>)	273	(<i>Correspondence</i>)	630
Developments in the Testing of Radio Receivers (<i>I.E.E. Paper</i>), H. A. Thomas	269	Grid-Leak Resistances: (<i>Patents</i>)	661
(<i>Correction</i>)	319		
Dielectrics, Liquid, Losses in, at Radio Frequencies, W. Jackson	14	H armonic Analysis, A Valve Voltmeter Method, W. Greenwood	310
Direct Reading Modulation Meter (<i>Correspondence</i>)	25, 79	Heterodyne Receivers (<i>Patents</i>)	664
Direction-Finding (<i>Patents</i>)	116, 306, 663	H.F. Couplings (<i>Patents</i>)	363
Direction Signalling (<i>Patents</i>)	305, 602	H.F. Inductances (<i>Patents</i>)	303
Distortion in Screen-grid Valves, R. O. Carter	123, 429	High Frequency Generators (<i>Patents</i>)	688
Distortion in Valve Characteristics (<i>Correspondence</i>)	75	High Selectivity Tone-corrected Circuits (<i>Editorial</i>)	605
Distributing Broadcast Programmes (<i>Patents</i>)	482	(<i>Correspondence</i>)	685
Disturbances, Eliminating (<i>Patents</i>)	305, 363	Home-recording (<i>Patents</i>)	56
Dye, Dr. D. W. (<i>Obituary Notice</i>)	207		
Dynatron Oscillator (<i>Correspondence</i>)	77, 152, 213, 446, 574	I mpedance, Aperiodic, Measuring Set, A. T. Starr	325
		(<i>Correspondence</i>)	447, 573
E arthing Switches (<i>Patents</i>)	364	Impedance Measurement, A Note on, A. T. Starr	615
Electro-mechanical Rectification, N. W. McLachlan	329	Inductance Coils (<i>Patents</i>)	543
(<i>Correspondence</i>)	573	Influence of Valve Resistance in Oscillation Generators, N. W. McLachlan	130
Electron Discharge Tubes (<i>Patents</i>)	542	(<i>Correspondence</i>)	214
Empire Broadcasting, Masts at Daventry (<i>Illustration</i>)	607	INSTITUTION OF ELECTRICAL ENGINEERS (Papers Read) : 20, 84, 140, 208, 269, 331, 391, 451, 513	
Equivalent Mass of Driven Loud Speaker Cones, M. J. O. Strutt	143	Institute of Physics, Preservation of Instruments of Historical Importance	438
(<i>Correspondence</i>)	214	Insulation, High-frequency (<i>Patents</i>)	662
Existence of More than One Ionised Layer in Upper Atmosphere, G. Builder	667	Interference Eliminators (<i>Patents</i>)	424, 689
		Interference : Methods for Elimination, E. T. Glas	680
F errié, General G. (<i>Obituary Notice</i>)	207	Inter-valve Couplings (<i>Patents</i>)	544
Field in Immediate Neighbourhood of Transmitting Aerial (<i>Editorial</i>)	119		
Flash-Arc in High Power Valves (<i>I.E.E. Paper</i>), B. S. Gossling	391	L eipzig 120 kw. Broadcasting Station (<i>Illustration</i>)	625
Fog-signal Control (<i>Patents</i>)	306	Light-sensitive Bridges (<i>Patents</i>)	365
Frame Aerials (<i>Patents</i>)	56	Light-sensitive Cells (<i>Patents</i>)	363, 483
Frequencies of Double Circuit S.G. Valve Oscillators, N. W. McLachlan	439	Long and Ultra-short Wave Receiver (<i>Patents</i>)	116
Frequency Analysis of the Heterodyne Envelope, F. M. Colebrook	195	Losses in Liquid Dielectrics at Radio Frequencies, W. Jackson	14
Frequency-changer, The Screen-grid Valve As, E. L. C. White	618	Loud Speaker Coil of Optimum Mass (<i>Correspondence</i>)	214
(<i>Correspondence</i>)	686	Loud Speaker Cones, The Equivalent Mass, M. J. O. Strutt	143
Frequency-modulation, Signalling by (<i>Patents</i>)	246	(<i>Correspondence</i>)	214
Frequency Modulation (<i>Patents</i>)	426	Loud Speaker Diaphragms (<i>Patents</i>)	426, 543
Frequency Stabilisers (<i>Patents</i>)	425	Loud Speaker Diaphragms, etc., Vibrational Frequencies, N. W. McLachlan	626
		Loud Speaker Filters (<i>Patents</i>)	483
G ain Control and the Decibel, H. Stanesby	18	Loud Speaker, M.C., Damping of L.F. Oscillations, N. W. McLachlan	559
Ganged Condensers (<i>Patents</i>)	363	Loud Speaker Movements (<i>Patents</i>)	243
Ganged Tuning-controls (<i>Patents</i>)	243, 603	Loud Speakers (<i>Patents</i>) 55, 118, 245, 246, 304, 424, 426, 481, 603	
"Ganging" the Tuning Controls of a Superhet Receiver, A. L. M. Sowerby	70		
Generation of "Centimetre" Waves, F. W. Chapman	500	M agnetron Generators (<i>Patents</i>)	180
Glow-Discharge Tubes (<i>Patents</i>)	115	Magnetic Direction-finder (<i>Patents</i>)	423
Graphical Solution of Detector Problems, G. S. C. Lucas	202, 253	Mains-driven Sets (<i>Patents</i>)	243, 305
(<i>Correspondence</i>)	273	Mains Hum Eliminators (<i>Patents</i>) 364, 425, 482, 602	
Gramophone Motors (<i>Patents</i>)	305, 482	Mains Units (<i>Patents</i>)	542
		Matching Inductances (<i>Patents</i>)	115

	PAGE		PAGE
Methods of Investigating the Vibrational Frequencies of Conical Shells and Loud Speaker Diaphragms, N. W. McLachlan	626	Q uartz Resonators and Oscillators (<i>Correspondence</i>)	24
Microphones (<i>Patents</i>)	543	R adio Beacons (<i>Patents</i>)	303
Modulated and Heterodyne Signals, Detection by Straight Line Rectifier, E. B. Moullin	378	Radio Research Board, The Work of (<i>Editorial</i>)	I
Modulating Systems (<i>Patents</i>) 182, 304, 602,	604	Reaction Control (<i>Patents</i>)	481
Modulating by Light (<i>Patents</i>)	602	Receiver for Frequency-modulated Signals (<i>Patents</i>)	55
Modulation, A New Method (<i>Editorial</i>)	367	Receiver for Long and Ultra-short Waves (<i>Patents</i>)	116
Modulation Level of a Broadcast System, Recording, H. I. Kirke	369	Receiving Systems (<i>Patents</i>)	544
Month in the Air (Marconi Set on Mrs. V. Bruce's Aeroplane) (<i>Illustration</i>)	428	Recording of Modulation Level of a Broadcast System, H. L. Kirke	369
Mounting Piezo-Crystals (<i>Patents</i>)	366	Rectification, Electro-mechanical, N. W. McLachlan	329
Moving-Coil Loud Speakers of Midget Design (<i>Correspondence</i>)	75, 151	(<i>Correspondence</i>)	573
Moving-coil Magnets, C. E. Webb	67	Rectifier Units (<i>Patents</i>)	362
Multi-Channel Television (<i>I.E.E. Paper</i>), C. O. Browne	84	Rectifier Valves (<i>Patents</i>)	243
Multiples and Sub-Multiples of Ten (Symbols)	252	Rectifiers, Dry-contact (<i>Patents</i>)	181
Mutual Interference of Wireless Signals in Simultaneous Detection, E. V. Appleton and D. Boohariwalla	136	Reflection Methods of Measuring the Depth of the Sea (<i>I.E.E. Paper</i>), Commr. J. H. Slee	20
(<i>Correspondence</i>)	214, 394	Relaying Programmes (<i>Patents</i>)	424
N avigational Systems, Wireless (<i>Patents</i>)	424, 604	Remote Tuning Control (<i>Patents</i>)	688
Negative Resistances (<i>Patents</i>)	423	Reproduction, Wireless or Gramophone (<i>Patents</i>)	182
New Method of Modulation (<i>Editorial</i>)	367	Resistance-coupled Amplifiers (<i>Patents</i>)	306
New Type of Directive Aerial, T. Walmsley	622	Resistance in Band Pass Filters, G. H. Buffery	504
New Valve Characteristic, P. K. Turner	384	Resonant Circuits, Chain of, Analysis and Design, M. Reed	259, 320
New Valve Diagram (<i>Editorial</i>)	665	Royal Soc. Demonstration of Cathode Ray Oscillograph	449
O bituary Notices:		S canning for Television (<i>Patents</i>)	689
Dr. D. W. Dyer	207	Scientific and Technical Abstracts (Association of Special Libraries, etc.)	19
General G. Ferrié	207	Screen Grid Amplifiers (<i>Patents</i>)	118
Olympia, 1932, Impressions	564	Screen-grid Valves as Frequency-changer in the Superhet, E. L. C. White	618
Overcoming "Skip Distance" Effect (Zeesen Short-wave Aerial)	194	(<i>Correspondence</i>)	686
P atent Procedure, Changes in	557	Screen-grid Valve Oscillators, Double Circuit, Frequencies, N. W. McLachlan	439
PATENTS 55, 115, 180, 243, 302, 362, 423, 481, 542, 602, 661	364	Secret Telephony Systems (<i>Patents</i>)	366
Pentode Amplifiers (<i>Patents</i>)	364	Selective Reception (<i>Patents</i>) 118, 180, 366, 482	482
Pentode with Capacitative Coupling, L. G. A. Sims	673	Selectivity, Controlling (<i>Patents</i>)	182, 244
Percentage Harmonic Distortion (<i>Correspondence</i>)	23, 76	Selectivity of Broadcast Receivers (<i>Editorial</i>)	183
Phase Modulation (<i>Patents</i>)	58	(<i>I.E.E. Discussion</i>)	208
Photo Electric Amplifiers (<i>Patents</i>)	364	(<i>Correspondence</i>)	274, 631
Photo-electric Cells (<i>Patents</i>)	115, 116	Self-contained Sets (<i>Patents</i>)	664
Photo-electric Circuits (<i>Patents</i>)	57	Short-wave Oscillators (<i>Patents</i>) 115, 180, 363, 688	688
Physical Society's Exhibition (Apparatus Described)	80	Signalling Systems (<i>Patents</i>) 180, 246, 481, 542	542
Pick-up Volume Control (<i>Patents</i>)	302	Simplifying the Use of the Starr Impedance Measuring Set, J. Steffensen	512
Picture Transmission (<i>Patents</i>)	302	Smoothing Circuits (<i>Patents</i>)	245
Piezo-electric Crystals (<i>Patents</i>)	303	Sound Reporting Service (Norag)	201
Pocket Receivers (<i>Patents</i>)	544	Spreading of Electromagnetic Waves from a Hertzian Dipole (<i>I.E.E. Paper</i>), J. A. Ratcliffe, L. G. Veedy, G. F. Wilkins	140
Power Rectifiers (<i>Correspondence</i>)	24	Stabilising Frequency (<i>Patents</i>)	423, 603
Pre-Selected Tuning (<i>Patents</i>)	56	Starr Impedance Measuring Set, Simplified, J. Steffensen	512
Present Knowledge of the Upper Atmosphere (<i>I.E.E. Paper</i>), E. V. Appleton	513	Station-Indicator Dials (<i>Patents</i>)	661
Preservation of Instruments of Historical Importance (Institute of Physics)	438	Stenode (<i>Correspondence</i>)	24, 78, 150
Properties of Coupled Circuits, R. C. Clinker and T. H. Kinman	11	Straight Sets versus Superheterodynes (<i>Editorial</i>)	427
Pulham, Aircraft D.F. Station (<i>Illustration</i>)	122		
Push-pull Amplifiers (<i>Patents</i>)	57		

	PAGE		PAGE
Studies in Radio Transmission, T. L. Eckersley (<i>I.E.E. Paper</i>)	331	Ultra-short Wave Receivers, Tests on, R. L. Smith-Rose and H. A. Thomas ..	186
Sullivan Measuring Instruments	563	Ultra-Short Waves, Generating (<i>Patents</i>) ..	689
Superheterodyne Receivers (<i>Patents</i>) 244, 246,	543, 687	Upper Atmosphere: Existence of More than One Ionised Layer, G. Builder	667
Switches (<i>Patents</i>)	602	Upper Atmosphere, Present Knowledge of (<i>I.E.E. Paper</i>), E. V. Appleton	513
Synchronising Systems (<i>Patents</i>)	58		
T elevision in Colour (<i>Patents</i>)	304	V alve Amplifiers (<i>Patents</i>)	246, 362, 364
Television, Multichannel (<i>I.E.E. Paper</i>), C. O. Browne	84	Valve Cathodes (<i>Patents</i>)	244
Television Receivers (<i>Patents</i>)	55	Valve Characteristic, A new, P. K. Turner ..	384
Television Systems (<i>Patents</i>) 56, 117, 303, 484,	663, 687, 688	Valve Construction (<i>Patents</i>)	481
Testing Radio Receivers, Developments (<i>I.E.E.</i> <i>Paper</i>), H. A. Thomas	269	Valve Diagram, New (<i>Editorial</i>)	665
Tests on Five Ultra-short Wave Receivers, R. L. Smith-Rose and H. A. Thomas ..	186	Valve Generators (<i>Patents</i>)	115
Theory of Band-pass Filters for Radio Re- ceivers, C. W. Oatley	608	Valve Resistance in Oscillation Generators, N. W. McLachlan	130
Theory of Distortion in Screen-grid Valves, R. O. Carter	429	(<i>Correspondence</i>)	214, 319
Tone-control Circuits for Amplifiers, M. G. Scroggie	3	Valve Voltmeter Method of Harmonic Analy- sis, W. Greenwood	310
(<i>Correspondence</i>)	153	Valves, A.C. (<i>Patents</i>)	57
Trains, Reception in (<i>Patents</i>)	662	Valves, External Grid (<i>Patents</i>)	542, 543
Transients and Telephony (<i>Correspondence</i>) ..	23	Valves, Indirectly Heated (<i>Patents</i>) 181,	306, 663
Transformers, H.F. (<i>Patents</i>)	245	Valves, S-G., Distortion in, R. O. Carter ..	123
Transmission, Studies in Radio, T. L. Ecker- sley (<i>I.E.E. Paper</i>)	321	Valves, 3-grid (<i>Patents</i>)	306
Transmitting Aerials (<i>Patents</i>)	58, 180	Variable Condensers (<i>Patents</i>)	182
Tuning Adjustments (<i>Patents</i>)	243, 602	Variable-selectivity Control (<i>Patents</i>) ..	663
Tuning Dials (<i>Patents</i>)	363	Variation of Resist. and Cap. of Valves (<i>Correspondence</i>)	24, 79, 151
Tuning Systems (<i>Patents</i>)	483	Volume and Selectivity Control (<i>Patents</i>) ..	687
Two-circuit Tuner (<i>Editorial</i>)	545		
Two-element Band-pass Filters, R. T. Beatty	546	W ireless Engineer" Binding Cases and Complete Volumes	2
		Work of the Radio Research Board (<i>Editorial</i>)	1
		Z eesen Short-wave Aerial	194

II. INDEX TO AUTHORS.

APPLETON, E. V. (<i>I.E.E. Paper</i>)	513	MCLACHLAN, N. W. 130, 329, 439, 559,	626
APPLETON, E. V. and BOOHARIWALLA, D. ..	136	MALLETT, E.	248
BAGGALLY, W.	388	MOULLIN, E. B.	378
BEATTY, R. T.	546	OATLEY, C. W.	608
BLIGH, N. R.	61	POUND, F. J. A.	445
BOOHARIWALLA, D. and APPLETON, E. V. ..	136	RATCLIFFE, J. A., VEDY, L. G., and WILKINS, A. F. (<i>I.E.E. Paper</i>)	140
BROWNE, C. O. (<i>I.E.E. Paper</i>)	84	REED, M.	259, 320
BUFFERY, G. H.	505	SCROGGIE, M. G.	3
BUILDER, G.	667	SIMS, L. G. A.	314, 673
CARTER, R. O.	123, 429	SLEE, COMM. J. A. (<i>I.E.E. Paper</i>)	20
CHAPMAN, F. W.	500	SMITH-ROSE, R. I. and THOMAS, H. A. ..	186
CLINKER, R. C. and KINMAN, T. H.	11	SOWERBY, A. L. M.	70
COLEBROOK, F. M.	195	STANESBY, H.	18
ECKERSLEY, T. L. (<i>I.E.E. Paper</i>)	331	STARR, A. T.	325, 615
GLAS, E. T.	680	STEFFENSEN, J.	512
GOSSLING, B. C. (<i>I.E.E. Paper</i>)	391	STRUTT, M. J. O.	143
GREENWOOD, W.	310	THOMAS, H. A. (<i>I.E.E. Paper</i>)	269
HARBOTTLE, H. R. (<i>I.E.E. Paper</i>)	451	THOMAS, H. A. and SMITH-ROSE, R. I. ..	186
JACKSON, W.	14	TURNER, P. K.	384
KIRKE, H. L.	369	WALMSLEY, T.	622
KINMAN, T. H. and CLINKER, R. C.	11	WEBB, C. E.	67
LEWIS, W. B.	487	WHITE, E. L. C.	618
LUCAS, G. S. C.	202, 253		

III. ABSTRACTS AND REFERENCES.

PROPAGATION OF WAVES.

- The Absorption of Short [and Ultra-Short] Waves in Buildings.—F. Ollendorff, p. 453.
- Experimental Researches on the Propagation of Air Waves in a Long Cylindrical Tube.—Th. Vautier, p. 218.
- Estimation of Heights Reached by Air-Waves which Descend in Zones of Abnormal Audibility.—F. J. W. Whipple: Gutenberg, p. 277.
- Characteristics of Electromagnetic Radiation from Aircraft in Flight.—J. C. Coe and T. C. Rives, p. 575.
- Wavelengths for Aircraft Communication.—Carr, p. 299.
- The Action of the Appleton Layer in the Propagation of Waves of 30 kc/sec. Frequency.—Bureau, p. 517.
- The Attenuation of Medium and "Intermediate" Waves [150, 215 and 700 Metres] by Day over Sea.—J. Bion and P. David, p. 454.
- The Attenuation of Short Wireless Waves at the Surface of the Earth.—G. H. Munro, p. 514.
- Comparison of Formulae for Attenuation of Travelling Waves.—L. V. Bewley, p. 31.
- Aurora Borealis and the Heaviside Layer.—E. Brüche, p. 516.
- Australian Radio Research Board Work on the Propagation of Waves.—Australian Radio Research Board, p. 154.
- Note on Reception of Radio Broadcast Stations at Distances exceeding 12 000 Kilometres [Byrd Antarctic Expedition].—L. V. Berkner, p. 632: see also Long Paths.
- Long Distance Receiving Measurements of Broadcast Waves across the Pacific [Seasonal Variation, Dependence on Solar Conditions, etc.].—S. Namba and D. Hiraga, p. 516.
- Propagation of the Broadcasting Waves [345-441 Metres] in Japan.—Y. Takata and Y. Itow, p. 156.
- The Production of Circularly Polarised Electric Waves by a Single Total Reflection.—L. Bergmann, p. 633.
- The Propagation of Waves in Cities [Mathematical Investigation, on Optical Lines, of the Effect of Broadcast Receiving Aerials].—F. Ollendorff, p. 397.
- Contribution to the Theory of Interference Zones in Common-Wave Transmission.—W. Hübner, p. 517.
- Conductivity of the Ground for an 8.65 Metre Wave.—Palmer, p. 514.
- Short Wave Reception and [Cosmic] Ultra-Radiation.—W. M. H. Schulze, p. 88.
- The Action of Cylinders in an Electromagnetic Wave Field.—Kikuchi, p. 462.
- Radio Tests on Various Wavelengths on the Lower Danube (Bratislava-Ruse, Bulgaria).—V. Fritsch, p. 30.
- A Delay Recording Equipment using a Steel Band Telegraphone.—Decker, p. 158.
- The Diffraction of Elastic Waves at the Boundaries of a Solid Layer.—J. H. Jones, p. 576.
- The Spreading of Electromagnetic Waves from a Hertzian Dipole.—Ratcliffe, Vedy and Wilkins, p. 408.
- Dirac's Wave Equation of the Electron and Geometrical Optics.—W. Pauli, p. 517.
- The H. F. Discharge [Study of the Effect of the Distance between the Electrodes].—C. Gutton and G. Beauvais, p. 217.
- Measurement of Current in Electrodeless Discharges by Means of Frequency Variations.—J. Tykocinski-Tykociner, p. 400.
- Theory of Electromagnetic and Electrostatic Induction in Electrodeless Discharges.—J. Kunz, p. 400.
- Experimental Researches on the Dispersion in Polar Liquids, for the case of Radio Waves from 5 to 600 Centimetres.—P. Girard and P. Abadie, p. 576.
- Lorentz Double Refraction in Cubic Crystals.—F. Seitz, p. 576.
- Investigation of the Effect of Mechanical and Electrical Fields of Force on the Double Refraction of Quartz.—N. Günther, p. 517.
- The Influence of the Properties of the Earth on the Propagation of Electromagnetic Waves [Comprehensive Survey].—M. J. O. Strutt, p. 454.
- Preliminary Study of the Acceleration of Earthquake Shocks.—M. Ishimoto, p. 158.
- Echo of High-Frequency Radio Waves [Echo peculiar to Waves passing through Polar Region or Aurora Zone].—S. Namba, p. 516.
- Echo Measurements in Wireless Telegraphy.—G. Goubau, p. 87.
- Equipment for Echo Measurements on the Ionosphere [with Rapid Choice of Six Wavelengths: Cathode-Ray Observation with Circular Time Base].—G. Goubau and J. Zenneck, p. 632.
- Echo Signals in Japan.—T. Minohara, T. Inoue, and S. Ono, p. 28.
- Echo Signals in Transatlantic Picture Telegraphy [and Results in S-N Direction, Cape Town to Somerton].—H. M. Dowsett, pp. 216 and 454.
- Further Communications on Near Echoes [Delay Times of the Order of 0.01-0.02 Sec.].—H. Mögel, p. 515.
- Wireless Echoes of Short Delay.—E. V. Appleton and G. Builder, p. 155.
- Electron Shadows in "Double Eclipse" of August 31st, p. 632.
- The Wireless Eclipse: Corpuscular Ionisation "Not Proven"? p. 632.
- Eclipse Effects on Radio [in America], p. 632.
- Suggested Wireless Observations during the Solar Eclipse of August 31, 1932.—E. V. Appleton and S. Chapman, p. 396.
- Influence of Solar Eclipse upon Upper Atmospheric Ionisation.—S. Chapman, p. 632.
- Short Waves and the Solar Eclipse [Observations on Wavelengths between 16 and 25 Metres], p. 632.
- Radio during Solar Eclipses [1929 Poulou Condore Results].—A. E. Kennelly, p. 632.
- Eclipses.—See also Lunar, and under "Atmospherics and Atmospheric Electricity."
- Electromagnetic Waves and Pulses.—W. E. Sumpner, p. 400.
- Propagation of Hertzian Waves in Electronic Gas under the Influence of a Magnetic Field.—G. Todesco, p. 216.
- Experimental Confirmation of the Selective Absorption of Hertzian Waves produced by an Electronic Gas in a Magnetic Field.—G. Todesco, p. 633: see also Ionised.
- Collisional Friction on Electrons Moving in Gases.—E. C. Childs, p. 393.
- Dispersion of Explosion Waves in the Atmosphere.—P. Duckert, p. 400.
- Investigations into Polarisation Fading.—K. Krüger and H. Plendl, p. 156.
- On the Connection between Short Wave Fading and Disturbances of the Earth's Magnetic Field.—H. Mögel, p. 276.
- A New Method of Eliminating Fading?—Günther: Bureau of Standards, p. 277.
- Selective Fading and Ionosphere Height Measurements.—H. Plendl, p. 575.
- Fading and Night Distortion [Absence of Midnight Fading in Spring and Autumn: Fading Periods occurring in Cycles: etc.], p. 632.
- Measurements in the Near Field of a Broadcasting Station [and the Effects of Houses, Aerials, etc.].—Zickendraht, p. 239.
- Remarks on the Papers "On the Theory of Propagation of Electromagnetic Waves over the Earth's Surface" and "On the Field Radiated from a Finite Antenna between Two Perfectly Conducting Planes."—R. Weyrich, p. 23.
- Measurements in the Field Radiated by a Vertical Antenna, Excited in its Fundamental Oscillation, between Two Perfectly Conducting Planes.—L. Bergmann and W. Doerfel, p. 453.
- Field-Intensity Measurements at Frequencies from 285 to 5 400 Kilocycles per Second [at Distances from a Few Wavelengths to 400 Kilometres: Determination of Electrical Constants of the Ground].—S. S. Kirby and K. A. Norton, p. 515.
- Application of the Hill Differential Equation to the Wave Propagation in Electrical or Acoustic Filter Networks.—F. Noether, p. 335.
- Investigation of the Front Deformation of an Electromagnetic Wave.—I. S. Stekolnikov, p. 277.
- Automatic Recording of Heaviside Layer Heights.—E. L. C. White, p. 400.
- Automatic Recorder for Height of Kennelly-Heaviside Layer.—Note from U.S. Bureau of Standards, p. 156.
- Preliminary Note on an Automatic Recorder giving a Continuous Height Record of the Kennelly-Heaviside Layer.—T. R. Gilliland and G. W. Kenrick, pp. 87 and 334.
- Investigations of Kennelly-Heaviside Layer Heights for Frequencies between 1 600 and 8 650 Kilocycles per Second [The Existence of the E and F Regions, and the Part Played by Reflection].—T. R. Gilliland, G. W. Kenrick, and K. A. Norton, pp. 216 and 334.
- New Devices for Recording Kennelly-Heaviside Layer Reflections.—H. R. Mimmo and P. H. Wang, p. 632.
- Kennelly-Heaviside Layer Studies employing a Rapid Method [Visual Observations of Pulse Patterns on Cathode-Ray Oscillograph] of Virtual-Height Determination.—J. P. Schafer and W. M. Goodall, p. 575.
- On an Estimation of the Height of the Heaviside Layer in Bengal.—H. Rakshit, p. 29.
- Measurements of the Height of the Kennelly-Heaviside Layer in Japan [using Wavelengths of the order of 100 Metres].—T. Minohara and Y. Ito, p. 515.
- The Kennelly-Heaviside Layer [The Original Publications], p. 157.
- An Effective Apparatus for Measurements on the Heaviside Layers.—H. Rukop and P. Wolf, p. 275.
- Observations on the Stratification of the Heaviside Region. New Experimental Equipment.—I. Ranzi, p. 155.
- Propagation of Wireless Waves [Form and Origin of Multiple Layers in Heaviside Region].—H. Nagaoka, p. 155.
- Past and Future Work on Wave Propagation.—Heinrich Hertz Association, p. 277.
- Dielectric Constant, Resistance and Phase Angle of Ice.—H. Wintsch, p. 517.
- An Observation on Interference Phenomena.—J. M. Faber, p. 157.
- The Effects on D.F., Fading, etc., of "Electro-Invasions" of the Atmosphere: The Connection with Aurora.—Düll, p. 632.
- The Ionisation of the Atmosphere and the Propagation over the Earth of Short Electric Waves, 10-100 metres.—K. Försterling and H. Lassen, pp. 87 and 217.

- Tables of the Ionisation in the Upper Atmosphere.—E. O. Hulbert, p. 335.
- Some Measurements of Upper-Atmospheric Ionisation.—E. V. Appleton and R. Naismith, p. 575.
- Apparent Increase of Lower Layer Ionisation during the Night.—Schafer and Goodall, p. 575.
- The Collisional Friction Experienced by Vibrating Electrons in Ionised Air.—E. V. Appleton and F. W. Chapman, p. 398.
- The Propagation of Radio Waves in an Ionised Atmosphere.—D. Burnett, p. 27.
- The Adsorption of Ions by Conducting Spherical Particles in an Ionised Field.—M. Pauthenier and Mme. Moreau-Hanot, p. 88.
- Study of the Motion of a Heavy Sphere in an Ionised Electric Field.—M. Pauthenier and M. Moreau-Hanot, p. 217.
- Experimental Control of the Motion of Small Metallic Spheres in an Ionised Electrical Field.—M. Pauthenier and M. Moreau-Hanot, p. 217.
- Direct Electrometric Study of the Limiting Charge of a Conducting Sphere in an Ionised Electric Field.—M. Pauthenier and R. Guillien, p. 575.
- The Charge of Small Dielectric Spheres in an Ionised Electrical Field.—M. Pauthenier and M. Moreau-Hanot and R. Guillien, p. 575.
- Ionised Gases in a Magnetic Field: Proof of the Existence of the Rotating Electron.—Th. V. Jonescu and C. Mihul, p. 157.
- The Dielectric Constant and Conductivity of Ionised Gases.—Th. V. Jonescu and C. Mihul, p. 335.
- The Free Electrons of Ionised Gases in a Magnetic Field.—Th. V. Jonescu and C. Mihul, p. 399.
- On the Behaviour of Electric Waves when Passing Through Ionised Gases.—W. Hasselbeck, p. 399.
- On the Properties of Ionised Gases at High Frequencies.—A. Rostagni, p. 453.
- On the Absorption of Short Electric Waves in Ionised Gases, an Attempt at the Demonstration of Long-Wave Transitions in the Spectrum of the Hydrogen Atom.—H. Klumb, p. 517.
- Experimental Researches on the Propagation of an Electromagnetic Wave in a Magnetically Active Ionised Medium.—G. Todesco, p. 454: see also Electronic.
- The Absorption and Dissociative or Ionising Effect of Monochromatic Radiation in an Atmosphere on a Rotating Earth. Part II. Grazing Incidence.—S. Chapman, p. 27.
- The Recombination of Ions in Air at Low Pressures.—Lenz, p. 519.
- Japanese Papers in These and Recent Abstracts, p. 155.
- Kennelly-Heaviside Layer.—See Heaviside Layer.
- On the Propagation of Light in Inhomogeneous Media.—K. Försterling, p. 217.
- Velocity of Propagation of Light in Vacuo in a Transverse Magnetic Field.—C. C. Farr and C. J. Banwell, p. 576.
- Velocity of Light Constant, Not Decreasing with Time.—O. C. Wilson: Gheury de Bray, p. 576.
- Remarks on the Reflection and Transmission of Light by Dissymmetric Media.—R. de Malleman, p. 576.
- On the Scattering of Light by Supersonic Waves.—P. Debye and F. W. Sears, p. 576.
- Reference Curves for the Geographical Representation of Light and Dark Areas, at any Date and Time, at the Earth's Surface and at the Ionised Layer.—J. Williamson, p. 334.
- Comparison between a Line with Distributed Constants and a T Circuit.—A. Blondel, p. 88.
- Measurements of the Propagation Constants of an Overhead Line with Earth Return, as Functions of the Frequency.—J. Fallou: Carson: Pollaczek, p. 30.
- New Graphical Solutions of the Calculation of H.T. Transmission Lines.—A. Blondel, p. 88.
- Radio Transmission over Long Paths.—Note from the U.S. Bureau of Standards, p. 276.
- Some Studies of Radio Transmission over Long Paths Made on the Byrd Antarctic Expedition.—L. V. Berkner, p. 334: see also Broadcast.
- Long-Wave Radio Receiving (Field Strength) Measurements at the Bureau of Standards in 1930.—L. W. Austin, p. 28.
- Twenty-four-hour Receiving Measurements of Low-frequency [Long-Wave] Radio Stations Nauen and Warsaw.—E. Yokoyama and I. Tanimura, p. 156.
- Tables of North Atlantic Radio Transmission Conditions for Long-Wave [15-23 kc] Daylight Signals for the Years 1922-1930.—L. W. Austin, p. 398.
- Correlation between Long-Wave Radio Signal Strength and the Passage of Storms.—S. J. Briggs: Bureau of Standards, p. 455.
- Theory of the Propagation of Low-Frequency [Long] Electromagnetic Waves [Change from Metallic to Dielectric Reflection, etc.].—E. Yokoyama and S. Namba, p. 454.
- The Propagation of Longitudinal and Transverse Waves in Isotropic Elastic Non-homogeneous Media [Mathematical Study].—G. Lampariello, p. 158.
- Velocity of Explosion-generated Longitudinal Waves in a Nepheline System.—L. D. Lee and M. Ewing, p. 158.
- Formation of Love Waves in a Two-Layer Crust.—H. Jeffreys, p. 158.
- Investigations at the Perkins Observatory of Changes in the Kennelly-Heaviside Layers as a Function of Lunar Altitudes.—H. T. Stetson [and G. W. Pickard], p. 156.
- Notes on Correlation Investigations between Kennelly-Heaviside Layer and Lunar Altitudes.—G. W. Pickard, p. 156.
- Measurements of the Photochemical Energy of the Moon obtained during the Lunar Eclipse of 27th Sept., 1931.—G. Blum, p. 30.
- Some Observations of the Behaviour of Earth Currents and Their Correlation with Magnetic Disturbances and Radio Transmission.—Bemis, p. 88.
- Recent Developments in Radio-Transmission Measurements.—G. W. Kenrick and G. W. Pickard, p. 157.
- Effect of Meteors on the Heaviside Layer.—A. M. Skellett, p. 156.
- Effect of Meteors on Radio Transmission.—H. Nagaoka, p. 518.
- The Optics of Radio Transmission.—E. Merritt, p. 158.
- The Variations of the Ozone Content of the Atmosphere.—P. Harteck, p. 27.
- Ozone Content of the Atmosphere.—R. Mecke, p. 157.
- On the Cause of the Close Correlation between Atmospheric Ozone Content and Meteorological Conditions.—H. Petersen, p. 335.
- On the Distribution of Ozone in the Earth's Atmosphere.—D. Chalange, p. 335.
- The Shortest Wavelength in Sunlight [and the Measurement by It of the Amount of Ozone].—F. W. P. Götz, p. 157.
- The Investigation of the Vertical Distribution of Ozone in the Atmosphere.—F. W. P. Götz, p. 633.
- A Theory of the Ozone of the Lower Atmosphere and Its Relation to the General Problem of Atmospheric Ozone.—O. R. Wulf, p. 633.
- The Ultraviolet Absorption Spectrum of Ozone.—A. Jakowlewa and V. Kondratjew, p. 276.
- The Mechanism of the Formation of Ozone from Oxygen under the Influence of Electron Discharge: of Nitrogen Oxides from a Nitrogen-Oxygen Mixture.—L. A. M. Henry, p. 157.
- The Photochemical Ozone Equilibrium in the Atmosphere.—Mecke: Faraday Society, p. 335.
- On the Penetration of Daylight into the Sea [Observations to Depths of over 1400 Feet, and Their Interpretation].—E. O. Hulbert: Beebe, p. 517.
- The Possibility of a Periodic Electrical Disturbance, possessing an Axial Symmetry, passing along a Cylinder without Dissipating Itself Laterally.—R. Ferrier, p. 158.
- Radio Transmission Problems Treated by Phase Integral Methods.—T. L. Eckersley, p. 514.
- Phenomena Accompanying Radio Transmission.—G. Marconi, p. 27.
- The Piccard-Kipfer Ascent.—A. Piccard, p. 157.
- Prof. Piccard's Exploration Ascent into the Stratosphere.—A. Piccard, P. Kipfer and others, p. 157: see also Stratosphere.
- The Intermediate Free Path Case in the Theory of a Plasma.—Tonks, pp. 600-601.
- Plasma-Electron Resonance, Plasma Resonance and Plasma Shape.—L. Tonks, p. 88.
- Wireless Communication in the Polar Regions [and the Causes of its Difficulties].—K. Krüger, p. 334.
- The Polar Year Radio Research Board Expedition to Northern Norway, p. 575.
- Polarisation of Down-coming Wireless Waves in the Southern Hemisphere.—E. V. Appleton, p. 154.
- Polarisation of Down-coming Wireless Waves.—J. A. Ratcliffe and F. W. G. White, p. 276.
- Polarisation Phenomena of Low-Frequency Waves.—S. Namba, p. 87.
- Polarisation of High-Frequency Waves and Their Direction Finding.—Namba, Iso and Ueno, p. 87.
- Measurement of the Ponderomotive Force Exerted on Resonators in the Electromagnetic Field.—K. Fritz, p. 218.
- Remarks on the Papers "On the Theory of Propagation of Electromagnetic Waves over the Earth's Surface" and "On the Field Radiated . . ."—R. Weyrich, p. 28.
- Communication with Quasi Optical Waves.—Karpus, p. 34.
- Radiation from Antennae under the Influence of the Earth. D.—Radiation Measurements with Antennae.—M. J. O. Strutt, p. 27.
- A Radiometer Sensitive to Hertzian Waves [and Useful in Exploring Electromagnetic Fields].—Beauvais, pp. 474-475.
- Charts of Distance Range of Radio Waves: Day and Night Frequency Characteristics.—U.S. Bureau of Standards, p. 454.
- Distance Ranges of Radio Waves.—Notes from the U.S. Bureau of Standards, p. 276.
- Distance Ranges of Radio Waves from 10 Kilocycles to 30 Megacycles/Sec.—J. H. Dellinger, p. 398.
- Reflection Measurements on Radio Waves.—G. J. Elias and C. G. A. von Lindern, p. 396.
- Precision Measurements of Refraction Coefficients [of Water] by Drude's Second Method.—G. Mie and E. Frankenberger, p. 157.
- On the Reflection at the Surface of the Ground of a Spherical and Isotropic Seismic Wave.—L. Cagniard, p. 400.
- The Determination of Thicknesses of the Continental Layers from the Travel Times of Seismic Waves.—A. W. Lee, p. 578.
- Contour Diagrams of Field Strengths in Ship-Shore Telephony.—Anderson and Lattimer, p. 335.
- Effect of Shore Station Location upon Signals.—R. A. Heising, p. 156.
- Diurnal Variation of Predominating Directions for Short-Wave

- (40-Metre) Signals received in Schenectady.—E. H. Kanzelmyer, p. 576.
- Discussion on "Some Experiences with Short-Wave Wireless Telegraphy."—N. H. Edes : J. C. Coe, p. 398.
- Scattered Radiation from Short-Wave Beams.—G.W.O.H. : Mögel, p. 29.
- Some Effects of Topography and Ground on Short-Wave Reception.—Potter and Friis, p. 344.
- Studies in Radio Transmission [Short Waves : based on Facsimile Telegraphy and Received Signal Strength Measurements on Long-Distance Channels].—T. L. Eckersley, pp. 454 and 632.
- On the Propagation of the Short Waves.—Anazawa, Asukai, Hattori, Hayasi, Minohara, Nakagami, Tanaka, Tani and Yokoyama, p. 28.
- Solar Activity and Radiotelegraphy.—L. W. Austin, p. 276.
- Concerning the Influence of the Eleven-Year Solar Activity Period upon the Propagation of Waves in Wireless Telegraphy.—H. Plendl, p. 334.
- Short-wave Reception and Solar Activity [Increased Wavelength of Optimum Waves near Sunspot Minimum].—H. Mögel : Plendl, p. 515.
- The Influence of the Eleven-Year Solar Activity Period on the Propagation of [Short and Medium] Waves in Wireless Telegraphy.—H. Plendl, p. 29.
- Solar and Radio Periodicities.—C. G. Abbot : Austin, p. 516.
- Velocity of Sound in the Stratosphere.—B. Gutenberg : Whipple, p. 575.
- Contributions on the Subject of Sound Propagation, particularly Bending and Anomalous Propagation.—B. Sandmann, p. 335.
- Sound Rays as Extremals [Calculation of Propagation through Atmospheric Layers of Different Qualities, particularly of Different Wind Velocities].—H. Bateman, p. 455.
- Influence of Atmospheric Conditions upon the Audibility of Sound Signals.—B. R. Hubbard, p. 277.
- On the Space Waves from a Vertical Doublet on a Plane Earth.—B. van der Pol and K. F. Niessen, p. 87.
- Demonstration of Standing Electric Waves Using a Simple Receiver.—R. Ramshorn, p. 517.
- Formation of Standing Waves on Lecher Wires.—Mohammed and Kantebet, p. 175.
- The Stratosphere and the Uppermost Atmospheric Layers.—Ch. Maurain : Piccard, p. 88 : see also Piccard.
- Composition and Temperature of the Stratosphere.—B. Gutenberg, p. 276.
- The "Middle Air" and the Stratosphere.—R. Soreau, p. 575.
- On the Displacement of Water, and the Nature of the Waves recorded, in Submarine Explosions.—J. Ottenheimer, p. 576.
- Contribution to the Study of the Propagation of Electromagnetic Fields in Subterranean Caves and Tunnels [Short Wave Tests, and the Reception of Broadcasting Signals].—V. Fritsch, p. 397.
- New Optical Properties of Solids and Liquids submitted to the Action of Supersonic Waves.—P. Bigard and R. Lucas, p. 576.
- Surges in Continuously Variable Cables.—A. Gemant, p. 218.
- On the Distribution of the Energy Stream in Total Reflection.—F. Noether, p. 217.
- On the Energy Flowing in the Second Medium in Total Reflexion.—A. Rostagni, p. 400.
- The Transmission of Telegraphic Signals.—Bartelink and Bast, p. 88.
- The Non-Uniform Transmission Line.—A. T. Starr, p. 576.
- On the Transparency of the Lower Atmosphere.—Buisson, Jausseran and Rouard, p. 400.
- Transparency of the Pure Atmosphere : On the Transparency of the Air.—J. Duclaux and M. Hugon : P. Chofardet, p. 455.
- Effect of Radiation on the Equilibrium of the Higher Layers of the Troposphere, and the Nature of the Transition from Troposphere to Stratosphere.—K. R. Ramanathan, p. 575.
- A Possible Connection between the Troposphere and the Kennelly-Heaviside Layer.—I. Ranzi, p. 632.
- Gas Discharges at Ultra-High Frequencies.—L. Rohde, p. 399.
- Transmission Experiments with [Ultra-Short] 1.3 Metre Waves.—Pfetser and Beck, p. 341.
- The Attenuation of Ultra-Short Radio Waves due to the Resistance of the Earth : and An Experimental Direction Finder for Use on Ultra-Short Waves.—R. L. Smith-Rose and J. S. McPetrie, p. 29.
- The Propagation along the Earth of [Ultra-Short] Radio Waves on a Wavelength of 1.6 Metres.—R. L. Smith-Rose and J. S. McPetrie, p. 514.
- The Problem of Ultra-Short-Wave Broadcasting.—F. Schröter, p. 30.
- Effect of Iron Ore Deposits on Ultra-Short-Wave Communication.—Spangenberg, p. 576.
- Ultra-Short-Wave Ship and Shore Communication.—Uda, pp. 298-299.
- Communication Tests for Radio Telephony by means of Ultra-Short [4.6 and 5.8 Metre] Waves between Niigata and Sado.—Uda, p. 360.
- Field Strength Measurements on Ultra-Short Waves [and the Polarisation and Attenuation of Such Waves].—K. Sohnemann, p. 30.
- The Propagation of Ultra-Short Waves in a Large City.—G. Leithäuser, p. 276.
- Broadcasting with Ultra-Short Waves.—G.W.O.H., p. 218.
- Some Recent Progress in the Field of Ultra-Short Waves.—J. Marique, p. 396.
- Ultra-Short Waves, Papers dealing with.—Marconi, Karplus, pp. 27, 34.
- Radio Communication over 170 Miles with Ultra-Short Waves [Marconi's Recent Results], p. 632.
- Notes on the Waves in Visco-Elastic Solid Bodies.—K. Sezawa, p. 633.
- The Periodic Waves on the Surface of Water.—J. Baurand, p. 88.
- The Development of the Wave Conception : Part VI.—K. Uller, p. 158.
- Reception and Weather Conditions [German Amateurs' Observations], p. 223.
- Winter in the Ionosphere.—R. A. Watson Watt, p. 400.

ATMOSPHERICS AND ATMOSPHERIC ELECTRICITY.

- The Theory of the Electrification of Aerosols.—H. S. Patterson, p. 91.
- Properties of Aerosols.—S. C. Blacktin, p. 160.
- Charged Aerosols and Ball Lightning.—W. C. Reynolds, p. 91.
- On Two Different Types of Atmospheric.—F. Schindelhauer, p. 277.
- Atmospheric Electricity : Field and Ionic Distribution in a Gas Traversed by a Current and Containing Electricity Carriers of Little Mobility.—J. Scholz, p. 160.
- High-Frequency Atmospheric Noise.—R. K. Potter, p. 31.
- An Estimate of the Frequency Distribution of Atmospheric Noise.—R. K. Potter, p. 633.
- Correlation of Radio Atmospherics with Meteorological Conditions.—T. Nakai, p. 335.
- Tests on the Distribution in Space of Atmospherics [Application of Verdan Principle to Space instead of to Time].—E. Montoriol and R. Subra : Lillo, p. 517.
- Lightning Discharges as Sources of Atmospherics causing Interference with Broadcast Reception.—H. Norinder, p. 518.
- The Diurnal Variation of Atmospherics at Paris, from 1928-1931. The Respective Influences of the Sources and of Propagation.—R. Bureau, p. 401.
- Direction-Finding Researches on Atmospherics.—R. Bureau, p. 518.
- The Part Played by Propagation Phenomena in the Recording of Atmospherics [and the Action of the Appleton Layer on Waves of 30 kc/sec. Frequency].—R. Bureau, p. 518.
- Atmospherics : Analysis of Data obtained in 1928 at Monte Cassino by the Italian Atmospheric Service.—B. Paoloni and P. Ilardi, p. 218.
- On the Results of the Continuous Record of Atmospherics [at Tokyo, since 1927].—J. Asakura, p. 158.
- 27-day Period of Atmospherics in Wireless Telegraphy.—F. Schindelhauer, p. 633.
- Atmospherics and Lightning.—R. A. Watson Watt, p. 577.
- A Dynatron Trip Relay Circuit Applicable to the Recording of Atmospherics of Various Strengths.—Fucks, p. 91.
- Magnetic Disturbances observed in Potsdam on Days of S. Norwegian Aurora.—A. Röstad, p. 336.
- Radio Direction Finding Experiments [and Signal Strength Measurements] with Aurora : "Electro-Invasions" of the Atmosphere.—Düll, p. 633.
- Some New Theoretical and Experimental Results on the Aurora Polaris [Electron Ray Tests and Periodic Space Paths].—E. Brüche : Störmer, p. 336.
- Problem of the Aurora.—C. Störmer, p. 402.
- Audibility of the Aurora Polaris.—H. U. Sverdrup, p. 89.
- The Emission Bands of the Polar Aurora in the Spectrum of the Night Sky.—J. Dufay, p. 89.
- Synthesis of the Polar Aurora.—A. Dauvillier, p. 159.
- On the Theory of the Polar Aurora.—A. Dauvillier, p. 218.
- Height of the Polar Aurora in Canada.—J. C. McLennan, H. S. Wynne-Edwards, and H. J. C. Ireton, p. 89.
- Results of Cinematographic Measurements of Auroral Heights, and Proof of the Occurrence of Infra-Red Auroral Radiation [and of Auroral Penetration of 65 Kilometres above the Earth].—W. Bauer, p. 578.
- Australian R.R.B. Work of Atmospherics.—Australian Radio Research Board, p. 158.
- Meteorograph with Automatic Short Wave Transmission (for Balloon Work).—H. Kirsten : Moltchanoff, p. 220.
- New Meteorographs with Wireless Distant Recording [for Balloon Work, etc.].—L. Heck and G. Sudeck : Moltchanoff, p. 337.
- New Radiometeorological Methods [for Sounding Balloons].—P. Duckert and B. Thieme, p. 337.
- Air Breakdown at Low and High Frequencies with Various Electrodes.—F. Miséré, p. 337.
- Measurement of the Amount of Electricity Flowing during Electrical Breakdown.—P. Rosenlöcher, p. 337.
- Optical Investigation of Spark Breakdown in Air at Atmospheric Pressure using the Suppressed Breakdown.—W. Holzer, p. 635.
- Calculation of the Electrical Breakdown Field Strength of Gases by means of Nernst's Heat Theorem.—O. Mayr, p. 455.
- The Breakdown Field-Strengths of the Homogeneous Field in Air.—H. Ritz, p. 402.

- On the Growth of the Space Charges in the Electrical Breakdown of a Gaseous Path.—N. Kapzov, p. 402.
- Broadcasting and [its suggested Effect on] the Weather.—E. V. Newnham : Humphreys, p. 336.
- Electrical Conditions in Stratified Clouds.—M. Grabham, p. 160.
- Disintegration of the Atomic Nucleus by Cosmic Rays.—C. D. Anderson and R. A. Millikan, p. 160.
- Energies of Cosmic-Ray Particles.—C. D. Anderson, p. 634.
- The Nature of Cosmic Radiation.—J. Barnóthy and Magdalené Forró, p. 90.
- The Constancy of Cosmic Rays.—R. D. Bennett, J. C. Stearns and A. H. Compton, p. 90.
- Diurnal Variation of Cosmic Rays.—R. D. Bennett, J. C. Stearns and A. H. Compton, p. 578.
- The Production of Artificial Cosmic Rays [from Beryllium bombarded by Alpha Rays].—W. Bothe and H. Becker, p. 336.
- The Nature of the Cosmic Radiation.—W. Bothe, p. 634.
- Dependence of the Ionisation Produced by the Cosmic Penetrating Radiation upon Pressure and Temperature.—J. W. Broxon, p. 578.
- On the Range of Fast Electrons and Neutrons [Are Cosmic Rays Neutrons?].—J. F. Carlson and J. R. Oppenheimer : W. H. Watson and F. R. Terroux, p. 219.
- Comparison of Cosmic Rays in the Alps and the Rockies.—A. H. Compton, p. 219.
- Further Investigation of Cosmic Rays.—A. H. Compton, p. 219.
- Tests to Determine the Nature and Source of the Cosmic Rays.—A. H. Compton, p. 336.
- Cosmic Ray Intensity Varies with Change in Latitude.—A. H. Compton, p. 519.
- Variation of the Cosmic Rays with Latitude.—A. H. Compton, p. 578.
- Use of Argon in the Ionisation Method of Measuring Cosmic Rays.—A. H. Compton and J. J. Hopfield, p. 635.
- Measurements of Cosmic Radiation in Northern Sweden.—A. Corlin, p. 578.
- Contribution to the Knowledge of the Solar Component of Cosmic Radiation.—A. Corlin and V. F. Hess, p. 160.
- Contemporary Advances in Physics, XXIII. Data and Nature of Cosmic Rays.—K. K. Darrow, p. 278.
- Cosmic Ray Fluctuations Connected with Those of Magnetism, Earth Currents and Electric Field.—Dauvillier, p. 160.
- The Sun as the Origin of Cosmic Rays.—V. Cofman : Dauvillier p. 578.
- Aurorae and Cosmic Rays.—A. Dauvillier, p. 633.
- Theoretical Considerations on Cosmic Radiation.—W. Heisenberg, p. 456.
- On the Disintegration Process Caused by Cosmic Radiation.—W. Heisenberg, p. 456.
- Problems of Cosmic Radiation.—G. Hoffmann, p. 635.
- Neutrons and Cosmic Rays.—L. D. Huff, p. 219.
- On the Determination of the Nature of Cosmic Radiation from Coincidence Measurements.—J. N. Hummel, p. 579.
- Investigations on the Electron Counter [Reference to its Use in Determining the Ionising Power of Cosmic Radiation].—J. N. Hummel, p. 579.
- A Calculation Concerning the Nature of the Secondary Corpuscular Cosmic Radiation.—T. H. Johnson, p. 456.
- The Production of Multiple Secondaries in Lead by Cosmic Radiation.—T. H. Johnson and J. C. Street, p. 456.
- A Cloud Expansion Chamber for Automatically Photographing the Tracks of Corpuscular Cosmic Rays.—T. H. Johnson, W. Fleischer, Jr., and J. C. Street, p. 579.
- Experiments on the Corpuscular Cosmic Radiation.—T. H. Johnson and J. C. Street, p. 579.
- An Interpretation of Cosmic-Ray Phenomena.—T. H. Johnson, p. 634.
- Vertical Tube Counter- and Barometric-Effects of Cosmic Radiation at Sea-Level.—W. Kolhörster, p. 401.
- The Verification of the Theory of the Vertical Tube Counter Effect of the Cosmic Radiation.—W. Kolhörster, p. 635.
- The Specific Ionisation of Cosmic Radiation.—W. Kolhörster and L. Tuwim, pp. 90 and 278.
- The Specific Capacity for Coincidence Production of Cosmic Rays beyond 10 Centimetres of Lead at Sea Level.—W. Kolhörster and L. Tuwim, p. 634.
- Variation of Intensity of Cosmic Ultra-Radiation.—F. Lindholm, p. 578.
- Cosmic Ray Particles.—G. L. Locher, p. 336.
- Cosmic Ray Tracks occur in Groups of Two or Three.—G. L. Locher, p. 579.
- On the Solar Period of the Hard Cosmic Radiation.—W. Messerschmidt, p. 278.
- On the Solar Period of Cosmic Radiation.—W. Messerschmidt, p. 336.
- On the Atmospheric Pressure Coefficient of the Hard Cosmic Radiation.—W. Messerschmidt and W. S. Pforte, p. 336.
- Similarity between Cosmic Rays and Gamma Rays.—R. A. Millikan and I. S. Bowen, p. 90.
- Further Experiments on the Uniformity of Distribution of the Cosmic Radiation [Absence of Direct Solar Effect on Cosmic Ray Intensities].—R. A. Millikan, p. 278.
- Cosmic-Ray Ionisation and Electroscopie-Constants as a Function of Pressure.—R. A. Millikan, p. 278.
- Cosmic-Ray Energies and Their Bearing on the Photon and Neutron Hypotheses.—R. A. Millikan and C. D. Anderson, p. 455.
- On an Attempt to Deflect Magnetically the Cosmic Ray Corpuscles.—L. M. Mott-Smith, p. 278.
- A New Experiment Bearing on Cosmic-Ray Phenomena.—L. M. Mott-Smith and G. L. Locher, p. 90.
- On the Structure of Cosmic Radiation. II. Comparison Measurements with Two High Pressure Ionisation Chambers.—W. S. Pforte, p. 89.
- Measurement of Cosmic Radiation at a Height of 16000 m.—A. Piccard, E. Stahel, P. Kipfer, p. 579.
- The Intensity of the Cosmic Radiation at 16000 Metres Altitude.—A. Piccard, E. Stahel and P. Kipfer, p. 519.
- On the Spectrum of Cosmic Radiation. I.—The Measurements in Autumn, 1928.—E. Regener, p. 336.
- Intensity of Cosmic Radiation in the High Atmosphere.—E. Regener, p. 634.
- Absorption and Diffusion of Cosmic Rays in Lead and Iron.—B. Rossi : Steinke, p. 160.
- Tests on the Magnetic Deflection of the Cosmic Rays.—B. Rossi, p. 401.
- Terrestrial Magnetic Field and Corpuscular [Cosmic] Radiation.—B. Rossi, p. 579.
- Calculation of the Action of the Earth's Magnetic Field on a Corpuscular [Cosmic] Radiation generated in the Atmosphere.—B. Rossi, p. 634.
- The Effects on Cosmic Radiation of Passage through Different Materials.—H. Schindler, p. 219.
- Contribution to the Question of Statistical Fluctuations of the Natural Radiation of Radiation Apparatus [Application to Investigations on Cosmic Rays].—W. M. H. Schulze, p. 90.
- Angular Distribution of the Cosmic Rays.—D. Skobelzyn, p. 160.
- On the Mechanism of the Phenomena of Ultra-penetrating Radiation (Cosmic Rays).—D. Skobelzyn, p. 579.
- The Corpuscular Explanation of Cosmic Rays.—F. Soddy, p. 90.
- Factors Influencing Ionisation Produced by Cosmic and Gamma-Rays.—J. C. Stearns and W. Overback, p. 456.
- Disintegration of Lead by Cosmic Radiation.—E. G. Steinke and H. Schindler, p. 401.
- On the Disintegration of Matter by Cosmic Radiation.—E. G. Steinke and H. Schindler, p. 578.
- New Measurements of [Cosmic] Radiation at Great Heights—Preliminary Communications.—G. A. Sucktorff, p. 579.
- First Cosmic-Ray Telescope Built at [Bartol] Research Laboratory.—W. F. G. Swann, p. 219.
- Electrons as Cosmic Rays.—W. F. G. Swann, p. 634.
- The Direct Detection of Individual Cosmic Rays.—W. F. G. Swann and J. C. Street, p. 579.
- Cosmic Radiation as Neutron Radiation.—R. Swinne, p. 456.
- Neutron, Atomic Brick, May Solve Mystery of Cosmic Rays, p. 336.
- On the Calculation of the Ion Counter Tube Effect of the Cosmic Rays, and their Absorption Laws according to Counter Tube Measurements.—L. Tuwim, p. 278.
- Some Remarks on the Principles of Experiments with Cosmic Ray Coincidences.—L. Tuwim, p. 579.
- The Analysis of Cosmic-Ray Observations.—L. D. Weld, p. 578.
- Measurements of Cosmic Radiation between 57° and 67° N.—K. Wölkén, p. 160.
- Cosmic Radiation : see also Penetrating, Ultra-Penetrating, Ionisation, Geiger-Müller.
- Slow Cloud Ionisation confirms Direct-Stroke Theory.—C. L. Fortescue, p. 32.
- Electric Discharge from Water Drops [and the Difference between Positive and Negative Discharges, etc.].—J. J. Nolan and J. G. O'Keefe, p. 577.
- Studies on Electric Discharge. Part VIII [Dust Figures] : Development of Electric Discharge as affected by the Residual Charge—Study with a Unidirectional Pulsating Wave.—Toriyama and Sawa : Mochizuki, p. 577.
- The Electrodeless Discharge as Measured by the Cathode-Ray Oscillograph (Number of Initiating Electrons, etc.) : also The Step-by-Step Discharge (and Krug's Denial).—Buss, p. 421.
- Gas Discharge and Breakdown [Preliminary Note].—W. Rogowski, p. 635.
- On the Characteristics of the Currents in a Discharge in Air at Low Pressure [Cathode-Ray Oscillograph Investigation].—R. Anthouard, p. 519.
- On the Discharge Delay in Homogeneous Electric Fields and Air at Atmospheric Pressure.—R. Strigel, p. 278.
- Discharge : see also Breakdown, Spark.
- On the Electrical Properties of Dust and Fog.—H. Sachsse, p. 635.
- Dependence of the Normal Earth Current on Latitude.—D. Stenquist, p. 159.
- The Theoretical Limit of the Earth's Atmosphere.—G. Roncali, p. 456.
- Eclipse Effects on Radio [in America], p. 633.
- Eclipses.—See also under " Propagation of Waves."
- The Electric Field at the Summit of the Puy de Dôme.—E. Mathias and G. Grenet, p. 89.
- On the Value of the Electrical Field of the Atmosphere at High

- Latitudes [Explanation of Andrée's Low Average Value of 12 Volts].—E. Salles, p. 519.
- Variation of the Electrical Potential of the Atmosphere during a Storm.—R. Di Malo, p. 337.
- The Stationary Velocity Distribution of Electrons Diffusing in an Electric Field.—M. Didlauskis, p. 337.
- Variation of the Surface Tension of the "Fulminant Material" as a Function of Temperature and Molecular Weight.—E. Mathias, p. 220.
- Investigations and Applications of the Geiger-Müller Counter in a Circuit with a Cathode-Ray Tube, particularly a Coincidence Circuit [for Cosmic Rays].—G. Medicus, p. 278.
- A Simple [Thyratron in Trip Circuit] Counting Arrangement for the Impulses of a Geiger-Müller Ion Counter.—R. Jaeger and J. Kluge, p. 635.
- Short Report on the Meteorological-Aerological Observations on the Graf Zeppelin Arctic Trip.—Weickmann and Moltchanoff, p. 337.
- Impulse Testing Technique.—Foust, Kuehni and Rohats, p. 519.
- Study of the Infra-Red Radiation emitted by the Earth's Atmosphere.—J. Devaux, p. 160.
- Methods for Measuring Interfering Noises.—Epsenschied, p. 100.
- The Effect of Electron Attachment on the Ion Mobility Curves in the Zeleny Air Blast Method of Ion Mobility Measurement.—L. B. Loeb and N. E. Bradbury, p. 220.
- Character of Atmospheric Ionisation.—P. A. Sheppard, p. 219.
- Ionisation as a Function of Pressure and Temperature.—A. H. Compton, R. D. Bennett and J. C. Stearns, p. 89.
- On the Ionisation in Pressure Chambers [including those used in Cosmic Ray Experiments].—E. G. Steinke and H. Schindler, p. 219.
- Rate of Ionisation of the Atmosphere.—G. R. Wait and O. W. Torreson, p. 277.
- Ionisation at High Gas Pressures.—R. M. Sievert, p. 455.
- Determination of the Coefficient of Ionisation by Collision [in Dry Air] using Large Plate Distances and Higher Pressures.—F. H. Sanders, p. 577.
- The Residual Ionisation [due to Cosmic Radiation] in Nitrogen at High Pressures.—J. W. Broxon, p. 219.
- On Electronic Ionisation of Nitrogen, Oxygen and Air at Low and High Pressures.—K. Masch, p. 635.
- Ionisation Measurements on the Piccard-Kipfer Ascent, p. 157.
- The Ionisation of the Atmosphere Measured from Flying Aircraft.—D. C. Rose, p. 160.
- The Ionising Efficiency of Electronic Impacts in Air.—J. Thomson, p. 401.
- Theory and Method of Determination of Size of Ions in the Atmosphere.—H. Israel, p. 160.
- The Ageing of Ions in Air and Nitrogen.—J. Zeleny, p. 160.
- Distribution of Mobilities of Ions in Air.—J. Zeleny, p. 219.
- The Mobilities of Atmospheric Large Ions.—R. K. Boylan, p. 402.
- The Absolute Values of the Mobility of Gaseous Ions in Pure Gases: Mobility Experiments in Gaseous Mixtures and Ageing Experiments in Pure Gases.—N. E. Bradbury, p. 455.
- The Recombination of Ions in Air at Low Pressures.—E. Lenz, p. 519.
- The Number of Langevin Ions in the Free Atmosphere at Washington, D.C.—G. R. Wait and O. W. Torreson, p. 577.
- On the Degree of Homogeneity of the Filtered Gamma Rays of ThC^{\prime} and the Verification of the Klein-Nishina Formula.—D. Skobelzyn, p. 456.
- The Application of Lichtenberg Figures.—Y. Toriyama and U. Shinohara, p. 635.
- Polarisation of Light from the Sky and Its Connection with Other Meteorological Elements.—W. Smosarski, p. 160.
- Lightning Investigation as Applied to the Aeroplane.—A. O. Austin, p. 278.
- Unusual Lightning.—H. E. Beckett and A. F. Dufton, p. 32.
- Results of Lightning Measurements in 1931 [on a Swiss H.T. Power Line, with Two Cathode-Ray Oscillographs].—K. Berger, p. 519.
- Recent Progress in Protecting Buildings against Lightning.—A. Boutaric: Schaffers, p. 337.
- Thunderstorms and Protection against Lightning [including Figures for Duration, Current Strength, etc., of Lightning Strokes].—G. Cario, p. 277.
- Unusual Lightning.—C. J. P. Cave, p. 32.
- Correlations between the Field Changes due to Lightning and the Appearance of the Flashes.—E. L. Halliday, p. 32.
- Spherical Lightning with Multiple Explosions.—J. Imbreccq, p. 161.
- The Relation of Branching of Lightning Discharges to Changes in the Electrical Field of Thunderstorms.—J. C. Jensen, p. 519.
- The Connection between Points of an Overhead Line struck by Lightning and the Presence of Underground Streams: Divination by Hazel Twig.—Lehmann, p. 577.
- Branching of Lightning.—J. L. P. Macnair, p. 91.
- On Ascending Lightning Flashes.—E. Mathias, p. 91.
- Granulated "Bead Necklace" Lightning.—E. Mathias, p. 91.
- "Bead Necklace" Lightning composed of Short Lines.—E. Mathias, p. 160.
- Globular and Ascending Lightning in Mountains and Elevated Plateaus.—E. Mathias, p. 519.
- Measurements of Lightning Surges on Transmission Lines in Sweden.—H. Norinder, p. 401.
- The Influence of Earth Resistance on Lightning [Mathematical Investigation].—F. Ollendorff, p. 455.
- Lightning Researches at 10⁷ Volts.—F. W. Peek, Jr., p. 577.
- Branching of Lightning.—B. F. J. Schonland and T. E. Allibone, p. 91.
- Duration and Magnitude of a Lightning Discharge.—R. S. J. Spilsbury, p. 91.
- Relation between the Length of an Overhead Telephone Line in Bare Wire and the Number of Damaging Effects produced by Lightning on the Apparatus and Cables connected to the Line.—D. Stenquist, p. 577.
- On the Difference between Oak and Beech as regards Danger of Being Struck by Lightning.—B. Walter, p. 402.
- Description and Theory of the Messien Lightning Arrester [depending on Ionisation by Radioactivity].—J. Clément: Messien, p. 577.
- Lightning Arrester Grounds.—H. M. Towne, p. 337.
- Terrestrial Magnetic Activity and its Relations to Solar Phenomena.—J. Bartels, p. 633.
- Magnetic and Electric Observations in the Sahara.—C. Le Camus and F. de Saint-Just, p. 160.
- Use of Magnetic Data for Investigating Radiation from the Sun.—J. Bartels, p. 159.
- Some Observations of the Behaviour of Earth Currents and Their Correlation with Magnetic Disturbances and Radio Transmission.—Isabel S. Bemis, p. 88.
- Seasonal Variations in Magnetic Storms.—H. B. Maris, p. 277.
- Features of the Current-System of the Upper Atmosphere as Revealed by the Diurnal Magnetic Variations at Huancayo, Peru.—A. G. McNish, p. 577.
- Pulsations of Terrestrial Magnetism [Eschenhagen's Waves] as the result of the action of Clouds of Electric Corpuscles.—C. Störmer, p. 159.
- Work of the Bell System relating to Terrestrial Magnetism and Electricity.—O. B. Blackwell, p. 159.
- Meteorographs.—See Balloon.
- Radio and the Meteorological Service.—L. A. Sweny, p. 635.
- Meteorology and the Radiogoniometry of Atmospherics.—R. A. Watson Watt, p. 577.
- Do Meteors cause Static?—J. Cage, p. 337.
- Effect of Meteors on Radio Transmission [and the Production of Atmospherics].—Nagaoka, p. 516.
- Absorption Measurements of the Penetrating Corpuscular Radiation in a Metre of Lead.—B. Rossi, p. 219.
- Proof of a Secondary Radiation Caused by the Penetrating Corpuscular Radiation.—B. Rossi, p. 401.
- Photography of Penetrating Corpuscular Radiation.—P. M. S. Blackett and G. Occhialini, p. 634.
- Measurements on the Absorption of the Penetrating Corpuscular Rays coming from Inclined Directions.—B. Rossi, p. 90.
- The Variation of Penetrating Radiation with Zenith Distance.—G. Bernardini, p. 401.
- Ionisation by Penetrating Radiation as a Function of Pressure and Temperature.—A. H. Compton, R. D. Bennett and J. C. Stearns, p. 336.
- On the Penetrating Radiation.—A. Piccard (Brussels), p. 90.
- The Problem of the Penetrating Radiation.—B. Rossi, p. 160.
- Recent Researches on the Penetrating Radiation: The Absorption Curve of the Penetrating Corpuscular Radiation.—B. Rossi, p. 456.
- An Attempt to Detect the Spontaneous Transformation of Helium into Penetrating Radiation.—G. T. P. Tarrant and L. H. Gray, p. 219.
- The Physiological Effects of Atmospheric Electricity.—C. Dorno, p. 456.
- Slow Electrons Make Possible "Polar Light" in Laboratory.—V. Cofman: Dauvillier, p. 578.
- Significance of Geoelectric Data from the Polar Regions.—O. H. Gish, p. 160.
- Some Atmospheric Electrical Instruments for use on the British Polar Year Expedition, 1932-1933.—P. A. Sheppard, p. 578.
- Simultaneous Registration of Potential Drop, Space and Surface Charge.—H. Mothes, p. 277.
- Photography of the Solar Corona apart from Eclipse Times.—B. Lyot: Esclançon: Fabry, p. 89.
- Spectroheliographic Study of the Solar Corona apart from Eclipse Times.—B. Lyot, p. 219.
- Some Remarks on the Length of the Actual Solar Period.—H. Mémyer, p. 89.
- Maxima of Intensity of Solar Radiation observed at Nice and at Thorenc (Maritime Alps).—L. Górczynski, p. 89.
- Solar Radiation as a Meteorological Factor.—H. H. Kimball, p. 519.
- The Time Lag of the Electric Spark.—J. A. Tiedeman, p. 277.
- On Displacements of the Striking Point of a Fairly Long Electric Spark with Unchanged Spark Gap.—B. Walter, p. 455.
- An Optical Study of the Formation Stages of Spark Breakdown.—F. G. Dunnington, p. 91.
- Spark Constant for Spark Formation with Various Boundary Voltages.—M. Toepler and T. Sasaki, p. 337.
- Spark Discharges in the Air, Part II: Relation between High-Frequency and Impulsive Discharges.—Y. Asami, p. 577.

Sparking Potential and Electrode Material.—L. B. Loeb, p. 220.
The Kindling of Electric Sparkover.—C. E. Magnusson, p. 337.
On Electric Sparks [between Surface of Charged Insulating Plate and an Earthed Conductor: Difference in Appearance according to Polarity].—T. Kobayasi, p. 577.
The Influence of the Stratosphere on the Dynamics of the Weather (Review of the Relations between Events in the Stratosphere and in the Troposphere).—H. Ertel, p. 402.
The Second Exploration of the Stratosphere.—Piccard, p. 634.
Cyclic Variations in the Heat and Light given out by the Sun.—C. G. Abbot, p. 160.
The Electrical Properties of the Sun.—A. Dauvillier, p. 337.
The Electromagnetic Phenomena produced on the Earth by the Electron Emission from the Sun.—A. Dauvillier, p. 337.
Interruptions to Lines Concentrated at Sunrise.—E. E. George and W. R. Brownlee, p. 89.
Sunrise Interruptions [to Overhead Lines] Attributed to Ionisation of Heaviside Layer [causing Increased Tension Gradient].—A. Minge: George and Brownlee, p. 577.
Periodic Variations in Natural Phenomena [Correlation of Sunspot Periods with Climatic Elements, Submarine Upheavals, Mortality, etc.].—W. B. Schostakowitsch, p. 159.
Mean Areas and Heliographic Latitudes of Sunspots in the Year 1930, p. 89.
Correlation between Sunspots Calcium Flocculi and the Sun's Radiation.—K. Sotome, p. 89.
The Relative Numbers of Sunspots.—M. Omschansky, p. 402.
Investigation of Surface Discharge with Impulse Voltage.—P. Rosenlöcher, p. 220.
Condensers and Surges [Application of Heaviside Operational Methods to Surges—particularly of Non-Rectangular Form—on Lines].—J. L. Miller, p. 401.
Terrestrial and Solar Coronae and their Relation to Cosmic Phenomena.—L. Vegard, p. 337.
Terrestrial Magnetism: Recent Work of the Carnegie Institution: Polar Year Plans.—J. A. Fleming, p. 402.
The Eleven-Year Thermal Wave at the Earth's Surface.—F. Dilger, p. 402.
Elementary Description of the Statical Field of a Thunder Cloud.—F. Ollendorff, p. 220.
Point Discharge Measurements below Thunderstorms.—J. Schonland and C. A. Coppens, p. 31.
Correlation of Atmospherics [in Japan] with Thunderstorms.—A. Kimpapa, p. 158.
High-Frequency [Ultra-Penetrating] Rays in the Aurora Borealis, and High Altitude Tests on Mount Everest.—E. A. Smith, p. 91.
The Ultra-Penetrating Radiation.—R. Desoille: Geiger, p. 90.
The Ultra-Violet Light Theory of Comet-Activity.—H. B. Maris, p. 159.
Ultra-Violet Transmission of the Atmosphere.—R. S. Rockwood and R. A. Sawyer, p. 578.
Some Investigations on the Deformation and Breaking of Water Drops in Strong Electric Fields.—W. A. Macky, p. 31.

PROPERTIES OF CIRCUITS.

The Influence of the Interelectrode Capacity between the Grid and the Anode in Multi-Stage Resonance Amplification.—V. I. Siforov, p. 279.
The Amplification Ratio of Resistance-Coupled Valve Combinations.—P. Kapteyn, pp. 278, 338 and 456.
The Resistance-Coupled Amplifier regarded as an Oscillatory Circuit.—K. Schlesinger, p. 32.
The Resistance-Coupled Amplifier as Oscillatory Circuit: Correspondence.—H. G. Baerwald: Schlesinger, p. 221.
An Untuned Radio-Frequency Amplifier (using an Intervalve Transformer with Associated Tightly-Coupled Circuit Tuned to a High Frequency).—F. W. Schor, p. 161.
On the Indispensable and Sufficient Condition of Absence of Self-Excitation in a Multi-Stage Resonance Amplifier.—V. I. Siforov, p. 279.
A Simplified General Method for Resistance-Capacity Coupled Amplifier Design.—D. G. C. Luck, p. 635.
Switching-on Processes in Resistance-Coupled Amplifiers [Behaviour to Transients].—K. Schlesinger, p. 33.
An Outline of the Theory for the Operation of Triode Power Amplifiers [and Oscillators].—Y. Fukuta, p. 161.
Regeneration Theory [Stability of Amplifiers whose Output is Connected to the Input through a Transducer].—H. Nyquist, p. 279.
On Distortion Correction by Resonance Methods, in Resistance-Coupled Amplifiers.—H. Bartels, p. 220.
On Self-Excitation of Amplifiers by Coupling the Anode Currents.—W. O. Schumann, p. 635.
The Experimental Investigation of Parasitic Reactive Couplings in Resonance Amplifiers.—V. I. Siforov and E. V. Viland, p. 340.
On the Calculation of Resonance Amplifiers.—V. I. Siforov, p. 635.
A Theoretical Comparison of Coupled Amplifiers with Staggered Circuits.—J. R. Nelson, p. 580.
On a Generalisation of the Idea of the Anti-resonant [Stopping, Rejector] Circuit.—M. Rouseau, p. 580.

An Application of the Circle Diagram to the Design of Attenuation and Phase Equalisers.—N. M. Rust, pp. 161 and 280.
On a Method for the Determination of Roots of Auxiliary Equations of the 3rd and 4th Degree in connection with the Investigation of Electrical Oscillations in Complex Circuits.—L. Miras, p. 493.
A Common Error [in Connection with the Use of the Term "Beat Note" in the Combination of Two Sinusoids of Different Frequencies].—W. F. Floyd, p. 458.
On the Theory of Beats.—V. S. Gabel, p. 280.
Simple Telephone Broadcasting Networks.—Apanasenko, p. 360.
The Fall of Potential in a Charged Insulated Cable.—D. K. McLeery, p. 519.
Capacitive Output Coupling [between Output Valve and Acoustic Load].—L. G. A. Sims, p. 456.
The Analysis and Design of a Chain of Resonant Circuits.—M. Reed, p. 456.
The Magnetic Field Intensity Near a Circular Loop Carrying an Electric Current [Theoretical Investigation].—A. L. Fitch, p. 581.
Oscillatory Condenser Discharge.—M. Rouseau, p. 580.
Apparatus for Exhibiting Some Properties of Coupled Circuits.—R. C. Clinker and T. H. Kinman, p. 161.
Damping and Its Reduction in Coupled Circuits.—H. J. Eilers, p. 161.
Wavelength Characteristics of Coupled Circuits having Distributed Constants.—King, p. 635.
A Mechanical Analogy for Coupled Electrical Circuits [New System of Mechanically Coupled Pendulums].—H. J. Reich, p. 520.
Correction and Supplement to the Paper "Coupled Oscillatory Circuits."—H. Hecht: Petržilka, p. 458.
Potentials, Resistances and Tuning in Damped and Undamped Circuits.—M. Osnos, p. 635.
Degeneration [into Relaxation Oscillations] in Valve Oscillators.—W. Reichardt, p. 91.
The Apparent Demodulation of a Weak Station by a Stronger One.—W. B. Lewis: Colebrook, p. 33.
"Apparent Demodulation": Another Viewpoint.—Mallett, p. 460.
Mutual Demodulation and Allied Problems.—H. L. Kirke, p. 92.
Demodulation.—See also under "Reception."
Investigations into Anode Detection.—G. Ulbricht, p. 32.
Analytical Study [based on Carson's Series Development] of Valve Circuits for Anode Detection of Telephony Signals.—J. P. Woods, p. 92.
[Analytical Study of] Plate Detection of Radio Signals.—J. P. Woods, p. 281.
The Calculation of Detection Performance in a Vacuum Tube Circuit for Large Signals.—J. P. Woods, pp. 457 and 523.
The Detection by a Straight Line Rectifier of Modulated and Heterodyne Signals.—Moulin, p. 522.
The Mutual Interference of Wireless Signals in Simultaneous Detection [Apparent Demodulation].—Appleton and Boohariwalla, p. 343.
Further Notes on the Detection of Two Modulated Waves which Differ Slightly in Carrier Frequency.—Aiken, p. 343.
Detection.—See also under "Reception."
Designing Detector Circuits.—Turner, p. 224.
Quality Detectors: A Survey of Rectification.—W. Greenwood and S. J. Preston, p. 161.
Discharge Tubes: Jumping Glow Phenomenon Caused by Hydrocarbon Vapour.—W. A. Leyshon, p. 281.
On Periodic Movements of the Negative Glow in Discharge Tubes.—W. A. Leyshon, p. 341.
Is the Relation $\Phi = c/f$ in the Electrostatic Field Always Valid?—P. Andronescu, p. 458.
On the Calculation of Mechanical Vibratory Systems by the Use of the Equivalent Electrical Circuits.—A. Forstmann, p. 221.
The Representation of Electro-Mechanical Systems by Pure [Equivalent] Electrical Circuits.—W. Hähle, p. 636.
Equivalent Electrical Networks.—O. Brune, p. 222.
Equivalent Electrical Networks.—N. Howitt, p. 581.
Tube Amplifier Equivalent Parallel Circuit.—G. D. Robinson, p. 33.
The Electromagnetic Field produced by a Wire Traversed by a Sinusoidal Alternating Current above a Conducting Layer.—Dubourdieu, p. 339.
The Design of the Band Pass Filter.—Bligh, p. 224.
Extension of the Filter Network Theory.—M. J. O. Strutt, p. 402.
Calculation of the Building-Up Time of Band-Pass Filters.—Labus, p. 537.
New Theory and Design of Wave Filters.—Cauer, p. 537.
Filters.—See also Transient, Networks, and under "Subsidiary Apparatus."
On Resonance Phenomena in Frequency Division.—L. Mandelstam and N. Papalex, p. 279.
The Phenomena of Frequency Division in Radio Technique.—N. Kryloff and N. Bogoluboff, p. 403.
A Thermionic Frequency Doubler.—Stedman, p. 294.
On the Theory of the Frequency Variation of an Alternating Current Measuring Circuit with Direct Current Apparatus and Dry-Plate Rectifiers.—L. Cremer, p. 340.
Harmonic Analysis of the Plate Current in a Vacuum Tube Circuit.—S. Leroy Brown, p. 457.
Studies of the Current in a Circuit in which R, L or C are subjected to Harmonic Variations.—J. B. Pomey, p. 340.

Calculation of **Heegner's Network**.—U. B. Kobzarev, p. 340.
 A Note on the Frequency Analysis of the **Heterodyne Envelope**: Its Relation to Problems of Interference.—F. M. Colebrook: Vigoureux, p. 402.
 Simplified **H.F. Calculations**.—W. A. Barclay, p. 33.
 The Conduction of **High-frequency Oscillatory Energy**.—Roosenstein, p. 38.
 The Effect of **Hysteresis** in Heating by an Oscillating Magnetic Field.—A. Blondel, p. 458.
 Contribution to the Experimental Study of **Electrical Induction**.—Turpain and Sabatier, p. 347.
 A Point of Stable Potential of an **Insulated Electrode** in a Triode.—G. A. Beauvais, p. 221.
 Stable Potential of an **Insulated Electrode** in a Triode.—G. A. Beauvais, p. 340.
 Impedance Characteristics of Loaded **Lecher Systems**.—L. Tonks, p. 280.
 The Impedance of a Loaded **Line** with a Partially or Wholly Inoperative Coil.—E. Adam, p. 34.
 Generation of Combination and Harmonic Frequencies by **Linear and Non-Linear Vacuum Tube Circuits**.—C. P. Boner and M. O. Boner, p. 457.
 On the Admittance of **Linear Oscillating Systems**.—M. J. O. Strutt, p. 33.
 A Simple Procedure for the Investigation of the **Magnetic Field** of a System of Current-Carrying Conductors of Any Shape of Cross Section.—W. Krämer, p. 162.
 The **Magnification of the Tuned Circuit**.—Sowerby, p. 345.
 Oscillations of Systems with **Negative Characteristics**.—Runge: Rosing: Steimel, pp. 282-283.
 On an Electrical Self-maintaining System containing a **Neon Tube** [and a Method of Measuring the Leakage Resistance of a Condenser].—B. Decaux and Ph. Le Corbeiller, p. 33.
 Synthesis of a Finite **Two-Terminal Network** whose Driving-Point Impedance is a Prescribed Function of Frequency.—O. Brune, p. 280.
 On the Maintenance in Oscillation of the Most General **Passive Network**.—Ph. Le Corbeiller, p. 457.
 Electric Waves in Branched **Networks**.—F. Ollendorff, p. 580.
 On the Time Admittances of **Transmission Networks**.—J. L. Barnes and C. T. Prendergast, p. 581.
 Mathematical Analysis of **Non-Linear Circuits**.—A. Boyajian, pp. 34 and 222.
 The Question of **Non-Linear Distortion**.—Hofer, p. 223.
 Some Examples of **Non-Linear Oscillations**.—N. Kryloff and N. Bogoliuboff, p. 403.
Optical Retroaction [for Generation of Sinusoidal and Relaxation Oscillations].—Sewig, p. 342.
Optimum Tuning Conditions for High Frequency Plant [to Satisfy Various Requirements].—M. Osnos, p. 340.
 The Properties of a Freely **Oscillating Circuit** containing Inductance, Capacity and Ohmic Resistance in Series.—M. Osnos, p. 457.
 Investigation of the **Oscillation Threshold** in Triode Circuits.—Giovanni, p. 340.
 Calculation of a Valve **Oscillator** with Detuned Oscillating Circuit.—Berg, pp. 341-342.
 The Problem of **Pentode Output Fidelity**.—Tulauskas, p. 44.
 Papers dealing with **Poincaré's Law** that of All Bodies of Equal Volume the Sphere has the Smallest Capacity.—G. Szegő, p. 341.
 Real, Wattless and Apparent **Power** in Electrical Circuits with **Non-sinusoidal Current and Voltage** [New Definitions rendering valid the Formulæ holding for Sinusoidal Currents].—S. Fryze, p. 519.
 The "**Pull-In**" Effect in Radio Technique.—N. Kryloff and N. Bogoliuboff, p. 403.
 Form of the E.M.F. produced with **Pulsating Angular Velocity**.—L. V. Stecula, p. 280.
 Asymmetry of **Push-Pull Circuits**.—E. S. Aneliovich, p. 280.
 The **Quadripole** and its Special Modes of Connection.—H. König, p. 340.
 The Variation of the Apparent Resistance of a Symmetrical **Quadripole** with the Load.—H. König, p. 340.
 The Principles of **Quadripole Theory**.—E. W. Selach, p. 280.
 The Range of Validity of the **Strecker-Feldtkeller Matrix Equations** for **Quadripole Systems**.—H. G. Baerwald, pp. 221 and 519.
Quadripoles and their Applications.—H. G. Baerwald, p. 581.
 On the Stability of **Quasi-periodic Motion**.—A. Witt: Kryloff and Bogoliuboff, p. 580.
 Rectification of an A.C. Voltage by a Circuit consisting of a Diode, a Resistance and a Capacity.—N. Carrara, p. 34.
 Some Notes on Grid Circuit and Diode **Rectification**.—Nelson, p. 583.
Regeneration Theory.—Nyquist. See Amplifiers.
Resistance, Self Inductance and Capacity.—W. Holzer, p. 222.
 On the "**Retardation Networks**" (Part III).—K. Nagai, p. 403.
Wattless Retroaction.—H. Braude (Leningrad), p. 337.
 A Circuit whose **Retroaction is Independent of Frequency** [for Audio-frequencies 20 to 20 000 Cycles per Second].—L. Brillouin and M. Lévy, p. 338.
 Frequency Multiplication by the Use of a **Rochelle Salt Condenser**.—Wolodgin, p. 294.
 An Examination of **Selectivity**.—Langley, p. 343.

Property of a Circuit having **Self-Inductance, Capacity and Resistance**.—M. Osnos, p. 280.
 Some Examples of **Similarity** between Equations representing Relations of Electrical Circuits.—Y. Watanabe, p. 581.
 Investigations on the **Singing Conditions** in Two-Wire Amplifiers, and their Application to a New Amplification Measuring Method.—W. Weinitzschke, p. 92.
 Frequency-dependent **Echo Damping Measurements on Lines**, by the **Singing-Point Method**, and their Use for Determining Position, Nature and Magnitude of a Fault.—W. Weinitzschke, p. 280.
Skin-Effect in a Ring of Circular Cross Section [and the Calculation of Self-Inductance].—V. Fock, p. 636.
 Contributions to the Theory of the **Stability of Electrical Circuits**, in particular of Alternating Current Circuits.—J. J. Sommer, p. 34.
 The Natural Electromagnetic Oscillation of a Rod-shaped Conductor at the **Surface of Separation of Two Media** with Different Dielectric Constants.—Ruprecht, p. 287.
 The Phenomena of **Synchronisation** [and the Exact Processes of Beat-Note Formation].—H. Abraham, p. 579.
 On the Mutual Leakage Inductances in **Transformers** with Several Secondaries.—A. Blondel, p. 33.
Ideal Transformers and Linear Transformations [Theoretical Investigation].—W. Cauer, p. 458.
 The **Transient Current** in a Receptor Circuit [and Application of Results to Telephonic Filters].—J. B. Pomey, p. 457.
 Equilibrating **[Transient] Processes** in Some Composite Circuits.—L. Miras, p. 161.
 The **Transient Response** of the Triode Valve Equivalent Network.—W. Jackson, pp. 161 and 280.

TRANSMISSION.

Modern Radio Equipment for **Air Mail and Transport Use** [the G.E.C. Transmitter Type RT-76-A].—A. P. Berejkoff and C. G. Fick, p. 637.
 A Study of Class B and C **Amplifier Tank Circuits**.—P. H. Osborn, p. 521.
 Class "B" **Audio Power Amplifiers** [Plate Current Flowing only when Grid is Excited].—C. L. Farrar, p. 283.
 The Operation of Vacuum Tubes as Class B and Class C **Amplifiers**.—C. E. Fay, pp. 283 and 343.
 Contribution to the Study of the Electrical Oscillations of the **Carbon Arc**.—A. Kotecki, p. 459.
 On **Asymmetric Telegraphic Spectra** [and the Possibilities of Single Side Band Morse Transmission].—C. R. Burch, p. 162.
 The **Smallest Short Wave Transmitter** [for Balloon Work].—B. Thieme, p. 459; see also under "Atmospherics and Atmospheric Electricity."
 On the Question of the Generation of **Barkhausen-Kurz** Electron Oscillations.—W. J. Kalinin, p. 223.
 Outline of a Possible Interpretation of the **Barkhausen-Kurz** Electronic Oscillations.—A. Rostagni, pp. 223, 341 and 637.
 On the Influence of Gases on **Barkhausen-Kurz** Oscillations.—H. Rindfleisch, p. 581.
 Gill-Morrell and **Barkhausen-Kurz** Oscillations.—G. Potapenko, p. 581.
 The **Barkhausen-Kurz Effect** according to Wave Mechanics.—K. Umeda: Schuster, p. 582.
 Eliminating the 'Phone Monologue: Two Workable Schemes for **Break-In** Operation.—M. F. Chapin: G. Ewing, p. 583.
Broadcast Transmitter Measurement using a Common Wavemeter.—E. A. Laport, p. 343.
Constant Frequency Oscillators.—F. B. Llewellyn, p. 163.
 More About **Economical Crystal Control**: Efficient Frequency Doubling—Clearing Up Neutralization—Isolating Sources of Trouble.—G. Grammer, p. 36.
 A **Multi-Frequency Crystal-Controlled** Monitor used to Control a Transmitter.—Reinartz, p. 93.
 The **Dynatron Oscillator**: Ease of Modulation and Use as Beat-Frequency Oscillator: The Frequency Formula and the Influence of the Varying Negative Resistance.—Wm. D. Oliphant: F. P. Basto: Colebrook, p. 164.
 The **Dynatron Oscillator**: the Interdependence of its Frequency Variation and the Content of Harmonics.—J. Groszkowski: Colebrook, p. 582; other correspondence pp. 222, 342 and 404.
 A **Direct-Coupled Amplifier** for the **Dynatron Oscillator**.—E. G. Fraim, p. 342.
 The Measurement of the **Efficiency** of Valve Oscillators with the help of a [Copper Oxide] Photoelectric Cell.—J. Groszkowski, pp. 163 and 637.
 The Increase of the **Efficiency** of an Electron Tube Oscillator by the Simultaneous Working at Two Different Wavelengths.—S. I. Tetelbaum, p. 582.
Electron Oscillations in Triode Vacuum Tubes [the Relation between the Various Types—B.-K., Pierret, and Hollmann: Transmitter and Receiver for 17 Centimetre Waves].—S. Uda and T. Mikami, p. 582.
Electron-Coupled Oscillator Circuits [for Short Waves]: Combining the Features of Oscillator and Buffer Amplifier.—J. B. Dow, p. 222.

- Push-Pull Electron-Coupled Oscillators [for Steady Frequency Short-Wave Working].—Ross Jones : Dow, p. 582.
- A Recent Development in Vacuum Tube Oscillator Circuits [Constant Frequency by Electronic Coupling].—Dow, pp. 93 and 164.
- The Spread Sideband System on Short Wave Telephone Links [Effect of Selective Fading on a Displaced Frequency Privacy System of Telephony, and Its Avoidance].—L. T. Hinton, p. 35.
- A New Fading-Free Method of Broadcast Transmission.—H. Günther : Bureau of Standards, p. 283.
- A 24 000 Watt Band-Pass Filter [for Tests on Simultaneous Telephonic Transmissions on Single Aerial].—Brotherton, p. 106.
- Greatly Increased Range without Loss of Speech Quality by Suppression of Frequencies below 1 000 Cycles per Sec.—J. P. Shanklin, p. 582.
- Preventing Impedance Variations in Aerial Circuit from Affecting Frequency [Additional Screening Electrode]., p. 637.
- A Method for the Approximate Calculation of a Thermionic Frequency Changer [based on Anode Dissipation].—Joffe, p. 359.
- New Methods of Frequency Control [particularly for Ultra-Short-Wave Transmitters] employing Long Lines [Lecher Wires or Aperiodic Lines in place of Crystal Control].—J. W. Conklin, J. L. Finch and C. W. Hansell, p. 93.
- A Frequency Indicator for [Broadcasting] Transmitters, p. 343.
- A Cathode-Ray Frequency Multiplier [for Obtaining Ultra-High Frequencies].—N. C. Jamison, p. 520.
- Improvements in Frequency Multipliers [for Crystal-Controlled Aircraft Transmitters].—E. G. Watts, p. 341.
- Frequency Stabilisation of Radio Transmitters.—Y. Kusunose and S. Ishikawa, p. 342.
- The Frequency Stability of the Triode Oscillator.—C. Matteini, p. 342.
- Gill-Morrell and Barkhausen-Kurz Oscillations.—R. Cockburn, p. 223.
- Gill-Morrell and Barkhausen-Kurz Oscillations.—E. C. S. Megaw and R. Cockburn, p. 404.
- Harmonic Generation by Grid Circuit Distortion.—F. E. Terman, D. E. Chambers and E. H. Fisher, p. 222.
- Elimination of Harmonics in Vacuum Tube Transmitters.—Y. Kusunose, p. 342.
- Background Hum in Radio Transmitters [Definitions of Objective and Subjective Ripple : its Measurement and Frequency Analysis].—H. Brückmann, p. 521.
- A Point of Stable Equilibrium of an Insulated Electrode in a Triode [and the Formation of Oscillations in a Dynatron Circuit].—Beauvais, p. 221.
- Employment of Positive Ion Sheath in Signalling by Frequency Change.—Thomson-Houston Company, p. 582.
- Ionised Gases and the Behaviour of Valves with Positive Grids.—Th. V. Jonecnu, p. 92.
- Electric Oscillations in Ionised Gases—Some Remarks on Their Present Theories.—J. Kunz, p. 223.
- On the Existence of H.F. Oscillations in the Secondary Current of H.T. Magnets.—J. Jaffray and P. Vernotte, p. 458.
- On the Hull Magnetron [Calculation of Wavelength].—L. Pincherle, p. 404.
- On the [Split-Anode] Magnetron Oscillations [Types A and B].—K. Okabe, M. Isida and M. Hisida, p. 581.
- The Investigation of Amplitude- and Frequency-Modulated Transmitters.—W. Runge, p. 35.
- The Reception of Frequency-Modulated Radio Signals.—Andrew, p. 522.
- The Fourier Analysis of Modulated High Frequency Currents.—M. Grützmacher, p. 94.
- The Impedance of the Valve Generator for a Constant-Voltage Modulating Frequency.—J. Groszkowski, p. 94.
- A Stroboscopic Method of Measuring Frequency- and Phase-Modulation [in Amplitude-Modulated Transmitters].—A. Heilmann, p. 93.
- Amplitude, Phase, and Frequency Modulation.—H. Roder, pp. 162 and 520.
- A Defect in Transmissions: Frequency Modulation as a Little-Known Source of Interference.—A. M. Kngushev, p. 283.
- On Modulation of Frequency.—A. M. Kngushev, p. 283.
- Over-Voltage in the Source of the Anode Current by Grid Modulation of a Radio Telephone Transmitter.—G. A. Zeitlenok, p. 283.
- The Advantage of Moderate Depth of Modulation and Sufficient Proportion of Carrier Wave, in Ensuring True Synchronisation between Transmitter and Receiver.—Abraham, p. 582.
- Distortion in Modulation by Iron-Cored Choke, investigated on the Machine Generator [and an Improved Modulation System].—M. Pohontsch, p. 582.
- Theory of Modulation and its Practice.—Y. Fukuta, p. 405.
- Note on the "De-phasing" Method of Modulation.—S.F.R. Chireix System.—H. Chireix, p. 94.
- A New Method of Modulation (Chireix Dephasing System).—G.W.O.H. : Chireix, p. 520.
- High Audio Power from Relatively Small Tubes : Application to Transmitter Modulation.—Heising : Barton, p. 44.
- A New Method of Measuring the Degree of Modulation of a Telephone Transmitter.—J. Kammerloher, p. 35.
- A Direct Reading Modulation Meter.—A. H. Cooper and G. P. Smith, pp. 162 and 223.
- Modulation Meters and Indicators for Broadcasting Control Rooms.—Lubszynski and Weigt, p. 240.
- An Instrument for Measuring Modulation Ratio.—V. N. Lepeshinskaja-Krakau, p. 343.
- New Methods for the Measurement of Modulation Ratio [using Critical Voltage of a Neon Tube].—A. L. Minz, p. 582.
- Modulation and Sidebands : Relation . . . etc.—N. F. S. Hecht, p. 341.
- Note Relative to Hecht's Paper on "Modulation and Side Bands."—J. B. Pomey : Hecht, p. 520.
- The Modulation System of the Russian High-Power Station at Schtschelkovo.—H. Wigge, pp. 162 and 458.
- An Analogy between Abbe's Theory of the Formation of Microscope Images and the Theory of Carrier Wave and Sidebands in the Modulation of Wireless Waves.—W. F. Einthoven, p. 405.
- The Class B Push-Pull Modulator.—L. E. Barton, p. 36.
- High-Power Performance from the Small 'Phone Transmitter : a Class B Modulator for Sets using Type '10 Tubes.—J. J. Lamb, p. 94.
- Multiplex Transmission and Secret Radiotelephony.—Chireix : Villem, p. 405.
- Oscillations of Systems with Negative Characteristics.—I. Runge : Rosing : Steimel, p. 282.
- Operating Mechanisms of Negative Resistance Oscillators [Mathematical and Graphical Investigation].—R. Usui, p. 342.
- On the Maintenance in Oscillation of the Most General Passive Network.—Le Corbeiller, p. 457.
- The Question of Non-Linear Distortion.—R. Hofer, p. 223.
- Optical Retroaction [for Generation of Sinusoidal and Relaxation Oscillations].—R. Sewig, p. 342.
- Principal Electrical Relations in an Oscillating Triode [Graphical and Analytical Treatment].—S. I. Zilitinkevitch, p. 341.
- On the Influence of Valve Resistance in Oscillation Generators [and the Stabilisation of Frequency by Series Anode Inductance].—N. W. McLachlan : Mallett, p. 342.
- Valve Oscillators adjusted near to the Oscillation Threshold [Mathematical Investigation].—Y. Rocard, p. 405.
- A Reversed-Current Feed-Back Oscillator [retaining Convenience of Dynatron Oscillator but oscillating up to 10 or 15 Megacycles].—W. van B. Roberts, p. 343.
- A Recent Development in Vacuum Tube Oscillator Circuits.—Dow, pp. 93 and 164.
- Calculation of a Valve Oscillator with Detuned Oscillating Circuit.—A. I. Berg, p. 341.
- A New Treatment of Electron Tube Oscillators with Feed-Back Coupling.—C. K. Jen, p. 163.
- On the Calculation of Electron Tube Oscillators [based on Anode Dissipation].—A. I. Joffe, p. 283.
- Operating Mechanisms of Negative Resistance Oscillators (III) : Analytical Studies on the Fundamental Characteristics of Triode Oscillators.—R. Usui, p. 459.
- Parasitic Oscillations in Broadcast Transmitters [and Their Cure].—A. D. Ring, p. 583.
- Phase Displacement between Current and Voltage as a Possible Carrier of Communication.—Lubberger and Schleicher, p. 162.
- Phase Modulation and Secret Communication.—T. Kuzirai and T. Sakamoto, p. 458.
- Phase Shift in Radio Transmitters [Causes and Effects : Cathode-Ray Oscillographic Investigation and Mathematical Treatment].—W. A. Fitch, p. 520.
- Polyphase Electron Tube Oscillators [and particularly their Use for Ultra-Short-Wave Generation].—A. Arenberg, p. 282.
- Asymmetry in Push-Pull Circuits.—Anceliovich, p. 280.
- On Steady State Conditions in Quartz-Controlled Single and Two-Circuit Transmitters.—V. Petržilka and W. Fehr, p. 636.
- Application of Quartz Plates to [Broadcasting and Aircraft] Radio Transmitters.—O. M. Hovgaard, p. 521.
- Communication with Quasi Optical Waves.—E. Karplus, p. 34.
- The Resistance of the Valve Generator.—S. I. Zilitinkevitch, p. 458.
- Valve Resistance in Oscillation Generators [Reduction of Negative Resistance by Auxiliary Positive Resistance : Influence on Oscillation at Very High Frequencies, etc.].—N. W. McLachlan, p. 459.
- On the Variation of the Resistance of Thermionic Valves at High [and Ultra-High] Frequencies.—Mitra and Sil, p. 463.
- The Mode of Action of Screen-Grid Transmitting Valves [based on the Philips' Company's Valves].—de la Sablonière, pp. 527-528.
- On the Frequencies of Double Circuit [R.F. and A.F.] Screen-Grid Valve Oscillators.—N. W. McLachlan, p. 582.
- Secret Communication.—See Multiplex, Phase Modulation.
- Short and Medium Wave Transmitter on s.s. "Santa Maria."—C. J. Pannill, p. 223.
- Frequency Control Equipment of Post Office Short-Wave Transmitters.—E. J. C. Dixon, p. 35.
- The Single Side-Band System Applied to Short Wavelengths.—A. H. Reeves, p. 94.
- Stable and Unstable Oscillation of a Two-Circuit Valve Generator with Super-critical Coupling.—P. von Handel, p. 35.
- An Experimental Study of the Tetrode as a Modulated Radio-Frequency Amplifier [particularly for Radiotelephone Transmission on Frequencies of and above 500 kc].—Robinson, p. 168

- Trains of Waves** Emitted at Constant Intervals of Time.—G. Petrucci, p. 637.
- The Calculation of Leakage in Auto-Transformers [and their Use in Heising-Modulated Transmitter Circuits].—Gürtler, p. 236.
- The Non-Uniform Transmission Line.—Starr, p. 576.
- Building a Low-Cost 1750-kc 'Phone-C.W. Transmitter [using Class B Modulator and Type 46 Valves].—G. Grammer, p. 583.
- The Transmission and Reception of Ultra-Short Waves that are Modulated by Several Modulated High Frequencies.—M. von Ardenne, p. 582.
- The Production of 28 Centimetre [Ultra-Short] Waves in Water by means of a 2.5 Metre Valve Oscillator.—Bergmann, p. 636.
- A Two-Triode Circuit for the Generation of Ultra-Short Waves.—N. Carrara, p. 222.
- The Dynatron Oscillator: with a New Circuit for Very High Frequencies.—F. M. Colebrook, p. 34; see also Dynatron.
- Investigations on Valves Producing Ultra-Short Waves.—H. Collenbusch, p. 403.
- On the Ultra-High-Frequency Oscillation of the Magnetostatic Vacuum Tube.—W. Dehlinger, pp. 404 and 520.
- On the Production of Ultra-Short Electro-magnetic Waves.—A. Giacomini, p. 581.
- Electrical Oscillations of Very Short Wavelength.—E. W. B. Gill, pp. 34 and 282.
- Ultra-Short-Wave Oscillators** [Positive Grid Connection].—C. Gutter and G. Beauvais, p. 34.
- Wavelength Characteristics of Coupled Circuits having Distributed Constants [and Application to the Electron Oscillator for Ultra-Short Waves].—R. King, p. 637.
- Special Transmitting Circuit for Ultra-Short (Centimetre) Waves.—F. Noack: Kohl, p. 282.
- Increased Power for Ultra-Short Waves.—H. N. Kozanowski: Westinghouse Company, p. 404.
- A New Circuit [of Greatly Increased Power] for the Production of Ultra-Short-Wave Oscillations [Symmetrical Plate and Filament Lecher systems between Two Triodes].—H. N. Kozanowski, p. 581.
- Summary of Work on the Production of Ultra-Short Waves.—Littmann, p. 582.
- The Generation of [Ultra-] Short Waves.—W. W. Maslennikoff, p. 341.
- Vacuum Tubes as [Ultra-] High-Frequency Oscillators.—E. D. McArthur and E. E. Spitzer, p. 93.
- Electron Oscillations [Ultra-Short Waves round 35 Centimetres in Wavelength] in Four-Electrode Tubes.—K. Morita, p. 341.
- A Note on the Ultra-Short-Wave Oscillation by the Back-Coupling Connection [Diodes and Triodes].—K. Morita, p. 341.
- A New Type of Ultra-Short-Wave Oscillator ["Standing Wave Oscillator" with 12 kw Output at Minimum Wavelength around 3 Metres].—I. E. Mouroumteff and H. V. Noble, p. 636.
- Transmitter for Amsterdam Ultra-Short-Wave Broadcasting Tests.—Nordlohne: Philips' Company, p. 637.
- Practical 5-Metre [Ultra-Short-Wave] Working.—H. L. O'Heffernan and S. G. Morgan, p. 459.
- Transmission Experiments with [Ultra-Short] 1.3 Metre Waves.—O. Pfetscher and R. Beck, p. 341.
- On the Measurement of the Energy of Ultra-Short Electromagnetic Waves.—G. Potapenko, p. 281.
- On the Dependence of the Length of the Ultra-Short Electromagnetic Waves upon the Heating Current of the Tube and upon the Amplitude of the Oscillations.—G. Potapenko, p. 281.
- Investigations in the Field of the Ultra-Short Electromagnetic Waves. Parts I to IV.—G. Potapenko, pp. 281, 281, 520 and 582.
- Circuits and Valves for Ultra-Short (Decimetre) Waves.—Rindfleisch and Rohde, p. 282.
- The Generation of Ultra-Short Waves of 1 Metre and Under: Valves for.—Rohde, p. 586.
- The [Ultra-Short Wave] Oscillations occurring in Valves with Positive Grids.—A. Rostagni, p. 92.
- The Calculation, from Energy Considerations, of the Limiting Frequencies at which Inversion of the Dynamic Characteristic Occurs, for Various Reaction Coupling Methods: and the Generation of Ultra-Short Waves.—J. Sahánek: Hollmann, p. 35.
- On the Production of Ultra-Short Waves of 12 Centimetres.—S. Sonada and T. Takayama, p. 341.
- On the Production of Various Electron Oscillations [Ultra-Short—Decimetre—Waves] by an Electron Tube: T.V.V. Type D.K.: Cymotron U.F.-101.—S. Sonada and T. Takayama, p. 459.
- Direct Piezoelectric [Tourmalin] Control for Ultra-Short Waves.—Straubel, p. 235.
- Generation of Ultra-Short Waves by Grid Distortion Harmonic Generator.—Terman, Chambers and Fisher, p. 222.
- Radio Telephony by Ultra-Short [50-Centimetre] Waves.—Uda, p. 164.
- Ultra-Short-Wave Telephony Transmitter.**—S. Uda and J. Ikeuchi, p. 637.
- Investigation of Oscillators for Wavelengths of the Order of a Decimetre [Valves with Spiral Grids and Anodes, for Ultra-Short Wave Generation].—U.S.S.R. Electrotechnical Institute, p. 341.
- A New Method for Generating Ultra-Short Waves [down to a 130-cm Fundamental].—G. M. Vinnik and E. K. Zavoisky, p. 636.
- An Experimental Study of Regenerative Ultra-Short-Wave [3-Metre] Oscillators.—W. H. Wenstrom, p. 163.
- Historical Review of Ultra-Short-Wave Progress [chiefly in the Generation of Oscillations].—W. H. Wenstrom, p. 163.
- The German P.O. Ultra-Short-Wave Transmitter for Broadcasting and Television, p. 404.
- Construction of an Ultra-Short-Wave (8 m) Transmitter with Tourmalin Crystal Control, p. 459.
- Ultra-Short Waves.**—See Barkhausen-Kurz, Frequency (Control, Multiplier), Gill-Morrell, Magnetron, Polyphase, Quasi-Optical, Resistance.
- The Behaviour of the Electron Valve at Very High Frequencies.—H. E. Hollmann, p. 281.
- On the Electrical Oscillations of Very Short Wavelength.—A. Rostagni, p. 282.
- Experiments with Very Slow Oscillations [1 c.p.s. and under] produced by Thermionic Valves.—F. Moeller, p. 163.
- Study of Weak Oscillations in Valve Oscillator Circuits.—B. Giovanni, p. 342.

RECEPTION.

- A New Light-Weight Receiver for Small Aeroplanes.—Standard Telephones and Cables, Ltd., p. 166.
- An Efficient Battery-Operated Radio Receiver [using Eveready 2.5 volt "Air Cell" Batteries for Filaments and Dry Cells for Anodes, giving 1 000 Hours' Working].—L. E. Barton and L. T. Fowler, p. 284.
- Battery Design Problems of the Air Cell Receiver.—F. T. Bowditch, p. 284.
- The Amplification Ratio of Resistance-Coupled Valve Combinations.—Kapteyn, pp. 278-279 and 338-339.
- The Resistance-Coupled Amplifier as Oscillatory Circuit.—Baerwald: Schlesinger, p. 225.
- The A, B and C of Amplifier Classifications [Explanation of the Differences between Class A, Class B, and Class C Amplifiers].—G. Grammer, p. 584.
- Amplification of the Class B Audio Amplifier to A.C. Operated Receivers.—L. E. Barton, p. 583.
- An Untuned Radio-Frequency Amplifier [using an Intervalve Transformer with Associated Tightly-Coupled Circuit Tuned to a High Frequency].—Schor, p. 161.
- Amplifier Tone-Control Circuits.—Scroggie, p. 230.
- Resistance-coupled Amplifiers with an Amplification of the order of 450 per Stage.—Kapteyn, p. 285.
- Output Amplifiers for 110-Volt D.C. Receivers.—J. R. Nelson, p. 344.
- Resistance and Transformer Coupling for Amplifiers: a Comparison.—A. Forstmann, p. 522.
- Amplifiers for Bands of Frequencies [for Frequency-Changing Receivers].—P. Drouin, p. 521.
- A Theoretical Comparison of Coupled Amplifiers with Staggered Circuits.—Nelson, p. 580.
- Reducing Errors due to Atmospheres by utilising their Irregularity in Space.—Montoriel and Subra, p. 524.
- Automatic Device for Tuning-in to Different Stations at Different Times.—G. Frantz, p. 408.
- Automatic Suppression of Inter-carrier Noise in Radio Receivers [with Automatic Gain Control].—P. O. Farnham, p. 408.
- Automatic Gain Control [and the Wunderlich Double-Grid Valve].—A. Dinsdale, p. 639.
- Circuits to Obtain Detection and Delayed AVC [Automatic Volume Control: Variations of the Farnham Circuit].—J. R. Nelson: Farnham, p. 407.
- Automatic Volume Control [Resistor between Detector Cathode and Negative Terminal of Common Source of Plate Supply, with Tapping to Screen Grid of R.F. Valve].—p. 639.
- Automatic Volume Control—is it Worth While?—W. T. Cocking, p. 639.
- The Problem of Automatic Volume Control without Auxiliary Valve finally Solved.—E. Rossman, p. 639.
- Automatic Volume Control and Anti-Fading Device, p. 639.
- Automobile Radio Problems Face Solution in 1932, p. 284.
- New Use for Old Circuit [Revival of Autoplex Circuit, particularly for Midget Receivers].—H. G. Boyle, p. 584.
- The Autotone.—F. L. Devereux and H. F. Smith, p. 283.
- The Autotone Portable.—F. L. Devereux, p. 524.
- New Band Pass Circuit.—N. R. Bligh, p. 166.
- The Design of the Band Pass Filter.—N. R. Bligh, p. 224.
- Band Pass Filters [for Broadcast Receivers].—H. Brykczynski, p. 522.
- Bass Drum and Tympani—the 5 000 Cycle Limit, p. 344.
- The Battery V-M Three.—W. I. G. Page, p. 345.
- The Beelitz Overseas Receiving Station.—Mögel, p. 539.
- Number of Broadcasting Listeners at 1st January, 1932, in Various Countries, p. 524.
- Quantitative Investigations on Broadcast Receivers.—A. Harnisch, pp. 94 and 164.
- Broadcast Receivers: I.E.E. Discussion on The Trend of Design.—C. F. Phillips and others, p. 405.
- Developments in Broadcast Receivers during 1931, p. 345.
- Mass Production of Radio Cabinets.—A. W. Richards, p. 37.

- Radio in Canada—Trade Conditions in 1931, p. 525.
 [Chicago] Trade Show Sees New Sets, Circuits, Tubes, p. 459.
 Broadcast Reception in a City : Tuning to the " Calibrated " or the " Common " Tuning Point.—Ollendorff, p. 405.
 Synchronous Electric Clock for Incorporation in Radio Receivers.—Ferranti, Ltd., p. 461.
 New Development in Tuning Coils [" Ferrocort " Cores].—Hans Vogt, p. 640.
 Use of a Vacuum Tube Operated Relay to Control Blasting in Radio Receivers.—B. Ephraïm, p. 36.
 Controlling Volume with the Variable-Mu Valve.—N. R. Bligh and E. D. Whitehead, p. 95 ; see also Volume, Automatic.
 The Oscillating [Crystal] Detector.—Noack : Habann, p. 538.
 What's Wrong with our C.W. Receivers ? [Suggested Elimination of " Image " Signal on " Other Side of Zero Beat " in Beat-Note Reception, with Increased Effectiveness of Audio-frequency Selectivity].—J. J. Lamb, p. 583.
 Damping and Its Reduction in Coupled Circuits [in connection with Selective and Distortion-free Broadcasting Receivers].—Eilers, p. 161.
 " Apparent Demodulation " : Another Viewpoint.—E. Mallett, p. 460.
 Weak Signal Demodulation by a Strong Carrier.—E. V. Appleton, p. 460.
 " Demodulation. "—F. M. Colebrook, p. 523.
 Demodulation.—See also under " Properties of Circuits. "
 Radio Design and the Trend of the Radio Industries [in U.S.A.], p. 284.
 Notes on the Design of Radio Receivers [Lecture before Radio Club of America].—L. Walsh, p. 584.
 Dynamic Symmetry in Radio Design.—A. Van Dyck, p. 638.
 Investigations into Anode Detection.—Ulbricht, p. 32.
 Grid Circuit Linear Detection [using a Screen-Grid Valve].—J. R. Nelson, p. 224.
 The Mutual Interference of Wireless Signals in Simultaneous Detection.—E. V. Appleton and D. Boohariwalla, p. 343.
 The Mutual Interference of Signals in Simultaneous Detection.—E. V. Appleton : Callendar, pp. 405 and 523 ; see also Demodulation.
 Wireless Signals : their Mutual Influence in Simultaneous Detection.—E. V. Appleton and D. W. Fry, p. 583.
 Further Notes on the Detection of Two Modulated Waves which Differ Slightly in Carrier Frequency.—C. B. Aiken, p. 343.
 The Detection by a Straight Line Rectifier of Modulated and Heterodyne Signals.—E. B. Moullin, p. 522.
 The Calculation of Detection Performance in a Vacuum Tube Circuit for Large Signals.—Woods, p. 457.
 The Calculation of Detection Performance for Large Signals.—J. P. Woods, p. 523.
 Hyper-sensitive Detection Systems [using the Autopex Circuit].—H. G. Boyle, p. 36.
 Detection.—See also under " Properties of Circuits. "
 Overload Limit Extension of the Tetrode Detector [Automatic Grid Bias Regulation extended to Filament-Type Detectors].—P. O. Farnham, p. 166.
 Designing Detector Circuits.—P. K. Turner, p. 224.
 A Cure for Detector Damping.—C. H. Smith, p. 95.
 Detector Distortion at Low Input Voltages.—H. A. Brown, G. W. Pickels and C. T. Knipp, p. 284.
 The Graphical Solution of Detector Problems.—G. S. C. Lucas, pp. 406 and 460.
 Quality Detectors : a Survey of Rectification.—Greenwood and Preston, p. 161.
 The Diode.—H. L. Kirke, p. 224.
 More about the Diode.—H. L. Kirke, p. 408.
 Distant Control of a Receiver by Automatic Telephone Dial, p. 461.
 Measurement of Class B Amplifier Distortion [Plotting the Form Factor as Indicator of Distortion].—C. L. Farrar, p. 460.
 On Distortion Correction by Resonance Methods, in Resistance-Coupled Amplifiers.—Bartels, p. 220.
 Linear Distortions in Broadcast Receivers and Their Compensation by Low-Frequency Equalisation Devices.—A. Clausung and W. Kautter, p. 636.
 Analysis and Reduction of Output Disturbances resulting from the Alternating Current Operation of the Heaters of Indirectly Heated Cathode Triodes.—J. O. McNally, p. 639.
 An Undesirable Coupling Link in Radio Receivers [Common Earth Lead to Aerial System and Filaments or Chassis, or Both].—A. E. Teachman, p. 284.
 Can Radio Sets be sold to Europe ? [with Statistics].—S. E. Laszlo, p. 166.
 Tendencies in Radio Construction at the Eighth Annual Paris Exhibition.—M. Adam, p. 37.
 Receivers at the Eighth German Radio Exhibition, p. 38.
 Receivers at Olympia and other Exhibitions, p. 52 ; see also Olympia.
 A Three-Circuit Four-Valve Receiver with Exponential Valve, p. 524.
 [The Construction of] Two Receivers for the Reduction of Fading.—R. Schadow, p. 406.
 An Automatic Device for the Selection of the Temporarily Strongest Receiver Output [in Spaced-Receiver Reception for Combating Fading].—H. E. Kallmann, p. 406.
 Microphonic Feed-Back Phenomena in Radio Receivers [particularly Self-Contained Receivers].—H. A. Brooke, pp. 225 and 640.
 Counteracting Acoustic Feed-Back through the Tuning Condenser [particularly in Midget Receivers].—Z. Bouck, p. 225.
 Higher Fidelity Standards are Here !, pp. 463-464.
 Improved Fidelity of Two-Speaker Radio Receiver.—Knowles, p. 464.
 The Construction of Filter Circuits in the German Broadcast Receiver Industry.—E. Schwandt, p. 96.
 Constant Peak Band Pass Filters.—W.G.I.P., p. 37.
 Novel Wireless Receiver, Flat Elements on Flat Panel, p. 36.
 On the Action of Tuned Rectangular Frame Aerials when Receiving Short Waves.—Palmer, p. 526.
 Single Valve Frequency Changes [and the Use of the Pentode].—W. T. Cocking, p. 639.
 A New Two-Grid-Valve Frequency-Changing Circuit for 10-100 Metre Waves.—G. H. J. Horan, p. 36.
 The Reception of Frequency-Modulated Radio Signals.—V. J. Andrew, p. 522.
 A Defect in Transmissions : Frequency Modulation as a Little Known Source of Interference, p. 522.
 Should Radio Receivers be Fused ? p. 345.
 Quick-acting Fuses for Radio Receivers.—Sundt : Littelfuse Laboratories, p. 408.
 Fuses and Scale Illumination in Receivers, p. 225.
 " Ganging " the Tuning Controls of a Superheterodyne Receiver.—A. L. M. Sowerby, p. 225.
 Oscillator for Ganging, p. 639.
 G.E.C. 1932-33 Radio Programme.—G.E.C., p. 584.
 A New Circuit for the Production of High Negative Grid Bias.—L. Medina, p. 225.
 Automatic Grid Bias.—M. G. Scroggie, p. 345.
 Grid Bias from Anode Current : Some Necessary Precautions [to avoid Effects due to A.F. Component in Added Resistance].—F. J. A. Pound, p. 639.
 The Frequency Analysis of the Heterodyne Envelope : Its Relation to Problems of Interference.—Colebrook, p. 402.
 Putting Back the High Notes.—W. T. Cocking, p. 405.
 Directed Radio in Hotels, Hospitals, etc. New System eliminates Wiring for Room Reception—Steel frame of Building serves as Aerial, p. 37.
 The Measurement of Radio Interference [High Frequency Spectra of Disturbances from Motors, Rectifiers, etc.].—J. Alexander, pp. 524 and 639.
 A Carrier Interference Eliminator.—W. Baggally, p. 523.
 Radio Interference Elimination a Co-operative Task.—C. C. Campbell and H. N. Kalb, p. 37.
 Radio Interference Problems [in California].—C. C. Campbell and H. N. Kalb, p. 640.
 Electrical Interference in Motor Car Receivers.—L. F. Curtis, p. 407.
 Reducing Radio Interference from Transmission Lines.—F. B. Doolittle, p. 584.
 Reduction of Radio Interference from Telephone Power Plants.—J. M. Duguid, p. 96.
 Trolleybuses and [Interference with] Radio Reception.—S. W. Duncan, p. 95.
 Testing and Using Radio-Interference Choke Coils [for Power Lines].—B. E. Ellsworth, p. 584.
 A Portable Meter for Tracing and Measuring Interference, embodying a " Standard Noise " Generator.—Gen. Elec. Company, p. 37.
 Receiver Attachment for Cutting-Out Interference from Apparatus and Machines.—E. Gloor, p. 461.
 The Possibility of Suppressing Interference with Broadcast Reception due to Electrical Make-and-Breaks.—K. Heinrich, p. 37.
 Interference Prevention for Street Cars [Trams, etc., with Overhead Wires].—Hermie, p. 640.
 On the Nature and Causes of the Interference with Broadcast Reception proceeding from H.T. Overhead Lines.—J. Herweg and G. Ulbricht, p. 166.
 Eliminating Interference Caused by Electrical Equipment.—A. Larsen, p. 407.
 Man-Made Interference and the Best Aerial for Its Suppression.—Leithäuser : Zerlett, p. 594.
 Prevention of Interference with Broadcast Reception due to H.T. Overhead Lines : the Local Use of H.F. Chokes.—F. S. Mabry, p. 37.
 A New Contribution to the Fight against Industrial [Power Line] Interference with Broadcast Reception.—S. Manczarski, p. 37.
 Radio Interference [from Electrical Apparatus and Lines] : Its Causes and Elimination.—J. McCandless, p. 640.
 Radio Interference from Insulator Corona.—F. O. McMillan, p. 294.
 Radio Inductive Interference : Methods Employed [in Canada] to Locate and Suppress the Interference at its Source.—H. O. Merriman, p. 407.
 Radio Inductive Interference.—H. O. Merriman, p. 407.
 The Reduction of Atmospheric and Man-Made Interference in Reception.—E. Nesper, p. 224.
 Protecting Devices against Local Interference for Connection at the Receiver.—E. Nesper, p. 407.
 Transient-produced Oscillations in Branched Network, and the Interference caused by Them.—Ollendorff, p. 584.

- The Siemens Interference Tracing Apparatus.—Siemens Company, p. 95.
- The Incandescent Electric Lamp as a Cause of Radio Interference.—Wider : Koetz, p. 584.
- Eliminating Interference from Thermostatically Controlled Electric Cushions.—A. C. Wiese, p. 524.
- Polydoroff [Iron] Cores for Superheterodynes [either in Pre-Selector Stage or Oscillator].—Langley: Polydoroff, p. 345 : see also Permeability.
- The Magnetic Susceptibility of Iron Powder Compositions, and its Dependence on Particle Size and Separation.—E. Gerold, p. 640.
- Lamp Resistances for D.C. Receivers.—Henderson, pp. 477-478.
- Current Limiting Systems, p. 639.
- Generation of Combination and Harmonic Frequencies by Linear and Non-Linear Vacuum Tube Circuits.—Boner and Boner, p. 457.
- The Magnification of the Tuned Circuit.—A. L. M. Sowerby, p. 345.
- Personnel and Equipment for the Small Manufacturer.—Z. Bouck, p. 408.
- Broadcast Receivers using the "Micromesh" Valves.—Standard Telephones and Cables, pp. 492-493.
- The Modern Straight Five.—W. I. G. Page and W. T. Cocking, p. 460.
- A Six-Valve Motor-Car Receiver mounted on Steering Column and using Condenser Aerial under Running Boards.—J. W. Berge, p. 406.
- The New Zealand Radio [Receiver] Market, p. 96.
- Background Noise in [Aircraft] Receivers.—W. Brintzinger and H. Viehmann, p. 523.
- Background Noises.—W. T. Cocking, p. 165.
- Olympia—1932: Olympia in Review, p. 639.
- The Trend of Progress [Olympia Radio Show], p. 638.
- Effects on Reception of Over-Modulation.—C. E. Kilgour, p. 284.
- The Owin Radio Apparatus Works', Hanover, All-Mains Five-Valve Receiver using Exponential Valves, p. 584.
- Licences under the Amplifier Patents, p. 461.
- Extensively Used [U.S.A.] Patents relating to Amplifying Circuits, p. 584.
- A Single-Valve Portable Receiver for Pedestrians.—H. Prinzer, p. 461.
- New Pentode Output Circuit.—L. G. A. Sims, p. 524.
- The Application of Permeability Tuning to Broadcast Receivers [and the Use of Polyiron].—K. H. Langley: Polydoroff, pp. 524 and 584 : see also Iron.
- Piezoelectric Band-Pass Filter.—J. Efrusi, p. 285.
- Municipal Police and Radio.—A. Mestre, p. 525.
- Police Wireless [Pocket Receiver and Calling Device], p. 640.
- Power Grid and Leaky Grid—A Comparison.—W. I. G. Page, p. 95.
- Problems that Face the Radio Engineer.—V. M. Graham, p. 96.
- Problems of Push-push Amplification.—C. E. Kilgour, p. 344.
- The New State Radio Receiving Centre at Noiseau [Paris].—G. Espinasse, p. 96.
- The Receiver of the Future, p. 165.
- Recording Characteristics of Radio Signals and Static [at the Bureau of Standards Laboratory].—S. R. Winters: Parkinson, p. 225.
- Some Notes on Grid Circuit and Diode Rectification.—J. K. Neilson, p. 583.
- Regeneration with Differential Condenser: Introduction of 1000 Ohms Resistance in Series with Smaller Capacity, p. 461.
- The Saic "Filter-Aerial" and a Comparison with Ordinary Filters.—Saic, p. 407.
- The Schaleco-Super-DX Receiver.—Schackow, Leder and Company, p. 460.
- To Teach Schools how to Select Radio Equipment. [Paragraph on the Co-operation between R.M.A. and U.S. Office of Education], p. 285.
- Receiving Equipment for Schools Broadcasting.—H. Fasal, p. 406.
- What Should the Ideal Schools Broadcasting Receiver Look Like? Construction of a Battery-driven Receiver for Schools. The Detection of Faults in School Receivers. The Most Suitable Installation of a School Receiving Equipment, p. 407.
- The Modern Screened Coil.—A. L. M. Sowerby, p. 36.
- A Highly Selective Audio-frequency Transformer (Vibrating Reed Type) for Radiotelegraphic Channels spaced only 75 Cycles.—Gunn, p. 345.
- Problems in Selective Reception.—M. V. Callender, p. 638.
- Selectivity in Radiotelegraph Reception: Audio and Radio Frequency Selectivity: the Application of Band-Pass and Low-Pass Filters: the Simplification of their Design and Construction.—R. A. Hull, p. 224.
- More About Audio Selectivity [and Its use in Radiotelegraphy].—L. W. Hatry: Hull, p. 345.
- An Examination of Selectivity.—R. H. Langley, p. 343.
- Super-Selectivity versus Sidebands [Advantages of Great Selectivity with Audio Compensation], p. 343.
- The Selectivity of Broadcast Receivers: I. E. E. Discussion, p. 405.
- The Selectivity of Broadcast Receivers. I.E.E. Discussion: A Correction.—H. L. Kirke, p. 460.
- The Selectivity of Broadcast Receivers [Introduction to Discussion].—C. L. Fortescue, p. 522.
- Increasing Selectivity by Crystal in Intermediate Circuit of Superheterodyne, p. 522.
- Selectivity and Tone Correction.—F. M. Colebrook, p. 165.
- Eckert Selectivity-Increasing Attachment.—C. H. W. Nason, p. 224.
- Modern Fabrication of Radio Receivers and Other Like Assemblies [particularly the use of Self-Tapping Screws].—A. C. Lescarboura, p. 225.
- Sensitivity Controls—Manual and Automatic.—D. D. Israel, p. 344 : see also Volume, Automatic.
- Formation of the Institute of Radio Service Men in Chicago, p. 37.
- German Shielded Down-Leads, p. 640.
- Marconi Short-Wave Receiver Type Rg. 31a [15 to 200 Metres: Suitable for Duplex Working], p. 584.
- Onward March of Short-Wave Radio [and the R.M.A. Statement on Short-Wave Reception], p. 584.
- Short-Wave Adaptors for Broadcast Receivers.—Burne Jones & Company, p. 584.
- Some Effects of Topography and Ground on Short-Wave Reception.—R. K. Potter and H. T. Friis, p. 344.
- Short Wave Reception and Ultra-Radiation.—Schulze, p. 88.
- The Modulated Current in the Resonance Circuit, the Side Band Coefficient, and the Radio Receiver Characteristics related to Them.—S. Takamura, p. 344.
- Physical Reality of Side-Bands [and the Relative Height of the Three Peaks].—F. M. Colebrook, p. 165.
- Practical Points in Connection with Single-Knob Tuning.—H. Fasal, p. 408.
- Engineering Acoustics: No. 88. The Stenode Principle, p. 584.
- The Stenode Radiostat.—F. G. Philpott: G.W.O.H., p. 165.
- The Stenode Radiostat.—J. Robinson, p. 225.
- The Stenode Radiostat.—P. G. Davidson: Robinson, p. 343.
- The Stenode Receiver and the Side-Band Theory.—J. Robinson: Fortescue, p. 36.
- Straight Sets versus Superheterodynes, p. 584.
- Receiver for Submarines: Reception under Water [3000-20000 Metre Waves].—Soc. Franç. Rad.élec., p. 406.
- Radio Reception and Sun Spots.—H. T. Stetson, pp. 95 and 408.
- The Single-Signal Superhet.—Lamb, p. 583.
- Single Dial Superheterodyne.—F. H. Haynes and W. T. Cocking, p. 95.
- An Advanced Television and Short-Wave Superheterodyne Receiver [avoiding Motor-Boating and Other Reaction Troubles by Use of Carborundum Detectors in Both Stages].—Tanner, p. 591.
- The Modern Band Filter Superheterodyne with Fading Compensator, for Amateur Construction: Introductory.—E. Rossmann, p. 524.
- The Superheterodyne as the Receiver of the Future.—R. Wigand: Brüller, p. 95.
- The Superheterodyne as the Long-Distance Receiver of the Future.—S. Brüller, p. 406.
- Changing a Tuned R.F. Type of Receiver to a Superheterodyne ["Superheterodyne Converter with Remote Control."].—General Motors Radio Corporation, p. 408.
- Stabilising Superheterodyne Performance: Electron-Coupled Oscillators Using Heater-Type Tubes.—J. J. Lamb: Dow, p. 406.
- Superheterodyne Improvements.—W. T. Cocking, p. 345.
- The Padding Condenser: Graphic Solution of a Single-Dial Superheterodyne Problem.—B. F. McNamee, p. 461.
- [Prevention of] Acoustic Feedback in Superheterodyne Receivers.—E. Messing, p. 406.
- A Solution of the Superheterodyne Tracking Problem [Mathematical: Determination of the Oscillator Inductance and Fixed Series Condenser].—V. D. Landon and E. A. Sween, p. 639.
- Single Control Superheterodynes.—H. Andrews, p. 95.
- One Knob Control for Superheterodynes.—A. L. M. Sowerby, p. 345.
- Super-regeneration and Short [and Ultra-Short] Waves.—H. B. Dent, p. 406.
- The Action of the Super-regenerative Receiver.—G. Gorelik and G. Hintz, p. 164.
- A Balanced Modulator Super-regenerative Circuit.—W. van B. Roberts: Armstrong, p. 584.
- A Cigar-Box Super-regenerative Receiver [550-1000 kc, using a 4.5 v Anode Battery and One Triode].—W. van B. Roberts, p. 406.
- The Reimann "Synchronous" Receiver.—Reimann, p. 461 : see also Zero-Beat.
- "Synchronous" Reception.—H. de Bellescize, p. 521.
- A Modern Receiver for Telegraphic Traffic on "Medium" Waves [3000 to 21000 Metres: the Noiseau Station Equipment].—G. Espinasse, p. 523.
- Developments in the Testing of Radio Receivers.—H. A. Thomas, pp. 460 and 524.
- The Testing of Broadcast Receivers [at the Radio Institute, Warsaw].—S. Dierewianko, p. 524.
- Modern Production Sensitivity Measurement [Receiver Testing Equipment for Large or Medium Size Plants].—R. F. Shea, p. 584.
- Testing Radio Receivers on the Assembly Line.—A. E. Thiessen: General Radio Company, p. 584.
- Testing Set for Broadcast Receivers, p. 584.
- German Testing Sets for Radio Servicing, p. 639.
- Continuity Tests of Radio Receivers.—J. F. Rider, p. 408.
- A Receiver for the Automatic Recording of Time Signals [for Longitude Determinations] and the Response Time of the Apparatus.—A. Schagger, p. 284.

Tone Correction and Distortion.—N. W. McLachlan, p. 460.
Tone Correction Explained, p. 638.
Ford Car Planetary Gear Principle for Tuning Dial of Receiver.—American Radiostat Company, p. 37.
Luminous Neon Column Operated by Amplified Carrier Wave as Tuning Indicator for Receivers (Fada Automatic Flashograph), p. 37.
Receivers for Ultra-Short-Wave Broadcasting.—Nordlohne: Phillips' Company, p. 638.
Historical Review of Ultra-Short-Wave Progress.—Wenstrom, p. 163.
Ultra-Short-Wave Receivers [German].—R. Raven-Hart, p. 285.
Tests on Five Ultra-Short-Wave Receivers [7 to 13 Metres: Two-Stage with Retroactive Detector; Super-regenerative; and Supersonic Heterodyne].—R. L. Smith-Rose and H. A. Thomas, p. 406.
An Ultra-Short-Wave Super-Regenerative Five Metre Receiver.—E. P. Hufnagel and G. J. Herrscher, p. 585.
Do Ultra-Short-Wave Transmissions Interfere with Broadcast Reception? p. 95.
Radio Telephony by Ultra-Short [50-Centimetre] Waves.—S. Uda, p. 164.
Receivers for Ultra-Short (Decimetre) Waves.—Rindfleisch and Rohde, p. 285.
Special Receiving Circuit for Ultra-Short (Centimetre) Waves.—F. Noack: Kohl, p. 285.
The Detection of Micro-Waves [Ultra-Short—Decimetre—Waves].—N. Carrara, p. 461.
Highly Sensitive Indicators for Ultra-Short Waves below 10 Centimetres [Radiometer and Bolometer Reception].—W. Zobel, p. 585.
The Aperiodic Amplification of Ultra-Short Waves [by the Use of Loeve Multiple Valves with Tuned Choke Coupling].—M. von Ardenne, p. 637.
The Transmission and Reception of Ultra-Short Waves that are Modulated by Several Modulated High Frequencies.—von Ardenne, p. 582.
Ultra-Short Waves.—See also Super-regeneration.
The Variable-Mu Three.—W. I. G. Page and W. T. Cocking, p. 95.
Visual Tuning of Band-Pass Amplifiers [using Dynatron Oscillator].—R. De Cola, p. 408.
The Desirability of Incorporating Automatic Mains Voltage Control in a Receiver.—A. C. Lescarboura, p. 36.
The Remote Volume Control.—W. T. Cocking, p. 95.
Volume Control in Screen-Grid Valve Receivers.—W. Nikolaus, p. 639.
Volume Controls: a Review of the Development of Volume Control Systems, including Design to meet Present-Day Requirements.—W. S. Parsons, p. 408: see also Automatic Control(ling) Limiting, and Sensitivity.
Causes of Volume Fluctuations in A.C. Mains-Driven Receivers, p. 284.
The Importance of Volume Level.—R. Raven-Hart, p. 407.
Communication in the New Waldorf Astoria, p. 37.
Distributing Programs in the Waldorf Astoria.—J. J. Kuhn, p. 284.
A Balanced Wave Trap.—W. S. Percival, p. 638.
Reception and Weather Conditions.—German Amateurs, p. 223.
The Wireless World "Autotone": High Circuit Selectivity with Tone Correction, p. 344.
The Wireless World Baby Superhet.—W. T. Cocking, p. 639.
Wireless World Monodial A.C. Super.—W. T. Cocking, p. 345.
Wireless World Power Radio-Gram.—A. L. M. Sowerby and H. F. Smith, p. 171.
The Wireless World Three.—F. H. Haynes: W. T. Cocking, pp. 37, 37 and 284.
Zero-Beat Tuning used in Highly Selective (Oscillating) Broadcast Receiver.—F. Reimann, p. 344: see also Synchronous.

AERIALS AND AERIAL SYSTEMS.

The Absorption of Energy by a Wireless Aerial.—J. A. Ratcliffe, p. 38.
Investigation of Airplane Antennas on Models.—P. A. Petrov, p. 285.
Characteristics of Airplane Antennas for Radio Range Beacon Reception.—H. Diamond and G. L. Davies, p. 348.
The Vertical Polar Diagram of a Marconi Beam Aerial.—T. L. Eckersley, p. 346.
The Space Radiation Diagram of the Telefunken Beam Aerial System.—R. Bechmann, p. 38.
Radiation Measurements on a Modern Telefunken Beam Aerial System at the Nauen High-power Station.—K. Krüger and H. Plendl, p. 167.
Aeroplane Measurement of the Radiation Characteristics of Short Wave Beam Aerials.—K. Krüger and H. Plendl, p. 226.
Portable Apparatus for the Adjustment of Beam Aerials.—Soc. Franç. Rad'élec., p. 408.
Radiation Characteristics of Beam Antennas [and the Dispersion of the Beam by the Heaviside Layer].—T. Minohara, K. Tani, and Y. Ito, p. 527.
Calculation of the Radiation Energy of Dipole Aerials—Telefunken Beam Systems—according to the Poynting Method.—J. Labus, p. 285.
Broadcasting Aerial System for the Suppression of Fading.—C. Lorenz Company and German P.O., p. 346.
Short [and Ultra-Short] Wave Broadcasting Aerials [to Eliminate Skip Distance Effect: as at Zeesen Station].—O. Böhm, p. 525: see also Skip Distance.
"Long Wave" [Medium Wave] Broadcasting Aerials with Suppression of High Angle Radiation [the "Disc" or "Wheel," "Cylinder" or "Polygon," and "One-Wire" Aerial Systems].—O. Böhm., p. 526.
The Breslau Broadcasting Station One-Wire Aerial for the Suppression of Near Fading.—Böhm, p. 526.
Preliminary Communication on Experiments on the Prevention of [Short Range] Fading in Broadcast Transmissions with Aerial Systems of Ordinary Height—Quarter Wavelength—and Great Horizontal Spread [Suppression of Space Wave].—H. Harbich and W. Hahnemann, p. 166.
A Continuously Loaded Cable for use at High Frequencies [at Receiving Stations of Long-Wave Transatlantic Telephony Circuit].—F. E. Nancarrow and H. Stanesby, p. 226.
Circuit Relations in Radiating Systems and Applications to Antenna Problems.—P. S. Carter, p. 585.
The Action of Cylinders in an Electromagnetic Wave Field.—H. Kikuchi, p. 461.
The Spreading of Electromagnetic Waves from a Hertzian Dipole.—J. A. Ratcliffe, L. G. Vedy and A. F. Wilkins, pp. 347 and 408.
Study of the Harmonics of Symmetrical and Asymmetrical Dipole Oscillators.—K. F. Lindman, p. 347.
The Radiation Energy of the Dipole Aerial with Reflector.—J. Labus, p. 640.
Experiments on the Tuning of Directional [Lecher Wire Type] Short Wave Aerials.—F. Kiebitz, p. 226.
Development of Directive Transmitting Antennas by R.C.A. Communications, Inc.—P. S. Carter, C. W. Hansell and N. E. Lindblad, p. 38.
Directive Aerial System with Groups of Varying Effective Height, p. 640.
Short Wave Directive Aerials at Bandoeng.—W. F. Einthoven, p. 408.
Field Distribution and Energy Emission of Directive Aerials.—E. Siegel and J. Labus, p. 347.
Application of Plane Wave Optical Theory to Calculation of Vertical Plane Directivity of Aerials.—Potter and Friis, p. 347.
Radiation from Antennae under the Influence of the Earth. D.—Radiation Measurements with Antennae.—Strutt, p. 27.
The Effect of the Earth on the Natural Wavelength, Impedance and Admittance of a Single Horizontal Wire.—G. Hara, p. 285.
A Method for Determining the Effect of the Earth on the Radiation from Aerial Systems.—J. S. McPetrie, pp. 347 and 527.
A Simple Non-polarising Earth for Curing "Noisy Grounds" [Daniell Cell Porous Pot, Copper Sulphate Solution and Copper Rod].—W. Butz, p. 348.
An Experimental and Analytical Investigation of Earthed Receiving Aerials.—F. M. Colebrook, p. 526.
Reducing Fading by Alternately Connecting Power Amplifier to Vertical Aerial and Horizontal Dipole, p. 640.
Aerials for Suppression of Fading.—See also Broadcasting, Skip Distance.
Feeder Adjustments for Short Wave Vertical Aerials.—N. Wells, p. 167.
Note on a One-Wire Feeder for Travelling Waves.—G. A. Uger, p. 346.
Elimination of Reflection in H.F. Feeders.—K. Posthumus, p. 346.
The Conduction of High-frequency Oscillatory Energy [Feeder Theory and Measurements].—H. O. Roosenstein, p. 38.
New Damping Measurements on High-Frequency Feeders.—K. Baumann and H. O. Roosenstein: Gothe, p. 226.
Transmission Lines [Transmitting and Receiving Feeders] for Short-Wave Radio Systems.—E. J. Sterba and C. B. Feldman, p. 585.
Remarks on the Papers . . . "On the Field Radiated from a Finite Antenna . . ."—Weyrich, p. 28.
Measurements in the Field Radiated by a Vertical Antenna, Excited in Its Fundamental Oscillation, between Two Perfectly Conducting Planes.—Bergmann and Dertel, p. 453.
The Field in the Immediate Neighbourhood of a Transmitting Aerial.—G.W.O.H.: Ratcliffe, Vedy and Wilkins: Zickendraht, p. 347.
The Electromagnetic Field produced by a Wire [of Infinite Length] Traversed by a Sinusoidal Current above a Conducting Layer.—Dubourdieu, p. 339.
The Fields produced by a Line traversed by an Alternating Current with Earth Return, and by a Horizontal Aerial.—F. Pollaczek, p. 462.
Mast Foundations in Sea and in Wet Ground, p. 527.
When a Frame Aerial is Worth While.—A. L. M. Sowerby, p. 586.
Receiving Frame Aerials for Low-frequency Alternating Magnetic Fields [for Loth System].—Bourgonnier and Durepaire, p. 350.
On the Action of Tuned Rectangular Frame Aerials when Receiving Short Waves.—L. S. Palmer, p. 526.
The Action of Short-Wave Frame Aerials.—L. S. Palmer and L. L. K. Honeyball, p. 640.

- Graphical Determination of Polar Patterns of Directional Antenna Systems.**—G. L. Davies and W. H. Orton, p. 527.
- Graphical Method of Calculating the Mechanical Design of an Aerial.**—I. S. Gonorovsky, p. 348.
- A Graphical Synthesis of Aerial Arrays.**—A. W. Ladner, p. 167.
- Mutual Impedance of Grounded Wires above the Surface of the Earth.**—R. M. Foster, p. 641.
- Effect of Height of Transmitting Aerial (Aircraft in Flight).**—Coe and Rives, p. 586.
- Contribution to the Experimental Study of Electrical Induction.**—A. Turpain and H. Sabatier, p. 347.
- A Half-Wave Mast Antenna, p. 167 :** see also Tower.
- Multi-Hertzian Oscillators.**—H. Kikuchi, p. 462.
- Aerial Lead-in in an Area of High Noise Level.**—H. J. Loftis and H. C. Forbes, p. 226.
- Eliminating Background Noise [from Lift Relays, etc., using Dipole Aerial with Closely Coupled Transformer and Two-Wire Shielded Cable leading to Short-Wave Receiver].**—W. Bell, p. 586 : see also Screened, Shielded.
- The Propagation of Radio Frequency Currents along a Wire of Finite Length.**—F. W. G. White, p. 585.
- The Radiation Characteristics of Earthed Umbrella, L and T Aerials.**—L. Hochgraf, p. 226.
- Radiation Resistance of Complex Antennas.**—K. Tani, pp. 167 and 285.
- More about the Radiation Resistance.**—B. L. Rosing, p. 285.
- A Method of Calculating Radiation Resistance, and Its Application to the Investigation of the Efficiency of Multiple Aerials of Simple Type.**—E. T. Glas, p. 586.
- Tests with Receiving Aerials.**—E. Neckenbürger, pp. 226 and 408.
- A Reciprocal Theorem in the Theory of Diffraction [Application to Theory of Loud Speakers and Aerial Arrays].**—Smith, p. 640.
- On the Free Electrical Vibrations of Rod-Shaped Conductors.**—K. F. Lindman, pp. 461 and 640.
- What Can the "Screened Aerial" Do? [Possibility of Cutting-Out Local Disturbances by Screening the Down-Lead].**—E. Nesper, p. 409.
- Special "Soludra" Cable for Screened Down-Leads, p. 527.**
- German Shielded Down-Leads, p. 640.**
- Reducing "Radio Inductive Susceptiveness" of Broadcast Receivers by Use of Shielded Lead-in or Underground or Grounded Aerials.**—Merriman, p. 409.
- On the Straight Wire [Short-Wave] Receiving Antenna with Distributed E.M.F.**—H. Iwakata, p. 462.
- Developments in Short-Wave Directive Antennae.**—E. Bruce, p. 96.
- Overcoming "Skip Distance" Effect [New Single-Mast Short Wave Aerial System at Zeesen], p. 408 :** see also Broadcasting.
- On the Space Waves from a Vertical Doublet on a Plane Earth.**—van der Pol and Niessen, p. 87.
- Man-Made Static and the Best Aerial for Its Suppression.**—Leit-häuser : Zerlett, p. 524.
- [Insulated] Radio Tower Tuning and Lighting.**—V. V. Gunsolley, p. 586.
- Single Insulated Tower as Broadcasting Aerial.**—I. T. and T., p. 285 : see also Mast.
- Principles of Radio Tower Design.**—T. W., p. 38.
- Towers with Reduced Staying, Bouvier-Bourseire System.**—Soc. S.F.R. : Bourseire, p. 96.
- Radio Towers and Antennas.**—N. Gerten, p. 38.
- Short-Wave Broadcast Towers [Base and Guy Insulators for].**—R. L. Jenner, p. 586.
- Antenna Resonance Transformers.**—V. V. Tatarinov, p. 285.
- Tuning Dipole Aerials by Shunted Flash-Lamp Combined with Weston Photronic Cell leading to Microammeter in Operating Room, p. 586.**
- Aerials and Reflectors used in Italian 50-Centimetre [Ultra-Short-Wave] Demonstration.**—G. Marconi, p. 96.
- Effect of Aerial Height in Ultra-Short-Wave Broadcasting in Cities.**—Schröter, p. 38.
- Reflectors and Feeders for Ultra-Short—18 Centimetre—Waves [Dover-Calais Service].**—R. Darbord, p. 346.
- Application of the Principle of Huyghens to the Calculation of Reflectors for Ultra-Short-Waves.**—R. Darbord, p. 525.
- The Action of Sheet Metal and Grid Reflectors for Ultra-Short Waves [Experimental Investigation].**—W. Köhler, p. 525.
- VALVES AND THERMIONICS.**
- Can Radio Tubes Be Sold Abroad?**—S. E. Laszlo, p. 350.
- The Use of Thermionics in the Study of Adsorption of Vapours and Gases.**—J. A. Becker, p. 410.
- The Development of an Electron-Emitting Alloy.**—O. S. Duffen-dack, R. A. Wolfe and D. W. Randolph, p. 227.
- The New 57 as a High Gain Audio Amplifier.**—L. C. Waller, p. 587.
- An Automobile Tube of Increased Output [Eveready Raytheon Type LA].**—M. Baireiss, p. 350.
- The Electrical Conduction of Barium Oxide and its connection with Electronic Emission [the Actions in the Activating Process and in Actual Working].**—W. Meyer and A. Schmidt, p. 348.
- A Measurement of Boltzmann's Constant by means of the Fluctua-tions of Electron Pressure in a Conductor [containing Description of Attenuator System].**—H. D. Ellis and E. B. Moullin, p. 588.
- On the Burning-Out Process of Wires Heated in Vacuo.**—L. Pránsnik, pp. 168, 410 and 588.
- Thermionic Emission in Caesium-Oxide Photocells at Room Temperatures.**—E. F. Kingsbury, p. 228.
- Cathode-Ray Tube as a Recorder of Receiving Valve Character-istics.**—M. von Ardenne, p. 97.
- Experimental Investigations of Distillation Cathodes [Acid Process, Barium on Platinum].**—W. Hinsch, p. 96.
- Cathodes.**—See also Alloy, Barium, Cobalt, Cold, Filaments, Oxide.
- Determination of the Cube Term in a Valve Characteristic.**—Sted-man, p. 286.
- A New Valve Characteristic [for Comparing or Designing De-tectors].**—P. K. Turner, p. 528.
- The Various Types of Characteristic Curve [particularly of German Screen-Grid and Pentode Valves].**—K. Nentwig, p. 528.
- Thermionic Valve Characteristics.**—A. Gehrts, p. 348.
- Desirable Tube Characteristics : A New Point of View, with Special Reference to Screen-Grid Amplifier Tubes [by Consideration of the Equivalent Parallel Circuit].**—G. D. Robinson, p. 586.
- "Cheater Circuits" for Synthetic Testing of Mercury-Vapour Tubes [for Economy in Power and Apparatus].**—J. L. Zehner : G.E.C., p. 588.
- Papers on the Use of Valves as Class A, B and C Amplifiers.**—Farrar : Fay, p. 283.
- New Tubes for Class B Audio : the Type RCA-46 Amplifier [Zero Bias] and Type RCA-82 Rectifier.**—G. Grammer, p. 587.
- A Tube for Class B Amplifier Service [Radiotron RCA-46 and Cun-ningham C-46].** p. 587.
- The Operation of Vacuum Tubes as Class B and Class C Amplifiers.**—Fay, p. 349.
- Photoelectric and Thermionic Emission from Cobalt.**—Cardwell, p. 234.
- Cobalt Alloy Filaments [with Tensile Strength Four Times that of Nickel].**—De Forest Company, p. 168.
- A "Gold" Filamentless Radio Tube.**—C. W. Hough : A. Hund, p. 38.
- [Cold] Valve without Filament or Vacuum.**—A. Hund, p. 349.
- Status of Cold-Cathode Tubes Abroad.**—I. J. Saxl : Seibt : von Ardenne, p. 286.
- Filamentless [Cold Cathode] Radio Tubes [on Glow-Discharge Principle].**—M. Guntherschulze and F. Keller, p. 168.
- Effect of the Target on Breakdown in Cold Emission.**—W. H. Bennett, p. 228.
- Effect of a Glass Target on Cold Emission.**—W. H. Bennett, p. 588.
- Dynamic Arrangement for Comparing the Constants of Two Triodes.**—C. Dei, p. 409.
- Spurious Contact Potentials and "Trapped" Electrons.**—W. B. Nottingham, p. 228.
- Which Tube for the Crystal Oscillator?**—G. Grammer, p. 349.
- The Influence of the Grid/Plate Capacity of the Detector Valve in Radio Receivers without Retroaction.**—A. van Sluifers, p. 228.
- A New High Quality Detector Tube.**—Wunderlich, p. 409.
- The RCA 55 : A Duplex-Diode Triode Unipotential Cathode Detector Valve, p. 463.**
- Remarks on the Triangular Valve Diagram.**—H. Klingelhöffer and A. Walther, p. 227.
- Diffusion of Electrons Back to an Emitting Electrode in a Gas.**—I. Langmuir, p. 228.
- The Diode.**—Kirke, p. 224.
- More About the Diode.**—Kirke, p. 498.
- The Deviation of Anode Currents in Diodes from the Three-Halves Power Law.**—A. Gehrts, p. 463.
- Distortion in Valve Characteristics.**—G. S. C. Lucas, pp. 168 and 229.
- Coefficients of Non-Linear Distortion of Amplifying Triodes.**—A. Clausing, p. 587.
- Measurement of Class B Amplifier Distortion [Plotting the Form Factor as Indicator of Distortion].**—C. L. Farrar, p. 463.
- The Theory of Distortion in Screen-Grid Valves [Mathematical Investigation, and Application to Design of Screen-Grid Valves, particularly of Variable-Mu Type].**—R. O. Carter, p. 587.
- An Electronmagnetically Controlled Three-Electrode Vacuum Tube.**—F. B. Haynes, p. 168.
- Simple Method for the Measurement of Very Low Grid Currents in "Electrometer" Valves.**—L. Sutherland, p. 97.
- An Electrometer Triode.**—Curtiss : Leprince-Ringuet, p. 642.
- A Valve with Sudden Fall of Emission at End of Life, p. 641.**
- A Method of Measuring Emission Current of an Electron Tube [Short-Period Application of Anode-Voltage to avoid Damage in Overloading].**—E. Iso and H. Ikushima, p. 350.
- The Energy Distribution of Electrons [Extracted from a Cold Tungsten Filament by means of a High Electrical Field] in Field Current Emission.**—J. E. Henderson, p. 588.
- The Equilibrium Distribution of Potential and of Electrons Outside the Surface of a Conductor.**—A. T. Waterman, p. 97.
- Recording the Equipotential Lines of the Field in a Valve.**—McArthur, p. 463.
- Accommodation Coefficient of Hydrogen : a Sensitive Detector of Surface Films [on Tungsten Filaments].**—K. B. Blodgett and I. Langmuir, p. 410.
- Filaments.**—See also Cathodes.

- The Flash-Are ["Rocky Point Effect"] in High-power Valves.—B. S. Gossling, pp. 409 and 528.
- The Upper Frequency Limit of Oscillator Valves [Theoretical Treatment].—C. Matteini, p. 642.
- Development of Valves in Germany.—Urtel, p. 641.
- Control of the Glow Discharge on a Grid Cathode by means of a Third Electrode behind the Cathode.—A. Güntherschulze and F. Keller, p. 227.
- Thermionic Valve with Fall of Potential across the Grid.—A. Lo Surdo, p. 38.
- Control Conditions of Grid-Controlled Gas Discharges—Ion Control Valves [e.g., Thyratrons].—Klemperer and Lübcke, p. 359.
- The Heptode—a Novel Thermionic Valve [Push-Pull H.F. Amplifying Valve for Short Wave Control].—E. J. C. Dixon, p. 227.
- A Heavy-Duty Industrial Amplifier Tube [Type RJ-563, Amplification Factor 4, Anode Current 0.20 A as D.C. Amplifier, 0.10 A as A.C. Amplifier].—C. B. Upp: Westinghouse Company, p. 463.
- Amplifier Tubes for Industrial Applications.—L. R. Harness, p. 588; see also Phototube Circuits.
- Insulator Developments point to Noiseless A.C. Tubes.—H. L. Crowley, p. 587.
- Ionisation in Vacuum Tubes [and the Advantage of the Buckley Method of Checking Gas Content].—R. de Cola: Buckley, p. 410.
- Investigation of the Thermionic Emission of Iron.—G. Siljeholm, p. 97.
- Konel—a Substitute for Platinum [and the Use of Nickel for Filaments].—E. F. Lowry, p. 227.
- A New Low Noise Vacuum Tube.—G. F. Metcalf and T. M. Dickinson, pp. 409 and 587.
- Purification of Magnesium.—W. Kaufmann and P. Siedler, p. 98.
- Eccentric Split-Anode Magnetron for Generation of Type A Oscillations.—Okabe, Isida and Hisida, p. 586.
- The Mains Valve.—W. T. Cocking, p. 38.
- Modern Manufacture of Radio Tubes.—J. B. Nealey: Grigsby Grunow Company, p. 39.
- Costs in Radio Tube Manufacture.—T. E. Conway, p. 588.
- Manufacturing Spray Shield Tubes.—Lewis: Grigsby-Grunow Company, p. 98.
- Vacuum Tube Performance versus Manufacturing Tolerances.—W. Charton, p. 350.
- On the Electron Theory of Metals.—L. Nordheim, p. 97.
- The "Micromesh" Valve.—I. T. and T., p. 286.
- Broadcast Receivers using the "Micromesh" Valves.—Standard Telephones and Cables, p. 462.
- On Micropyrometry, especially on an Objective Micropyrometer [for Temperature Measurements on Filaments, etc.].—G. Lewin, W. W. Loeb and C. Samson, p. 642.
- The Mobility of Caesium Atoms Absorbed on Tungsten.—I. Langmuir and J. B. Taylor, p. 463.
- Negative Grid Polarisation in a Triode [particularly in a Triode with a Weakly Emitting Cathode].—S. A. Obolensky, p. 286.
- Development of a Circuit for Measuring the Negative Resistance of Plodinatrons.—E. N. Dingley, Jr., p. 97.
- A New Group of Receiving Tubes [Types 56, 57 and 58].—p. 587.
- More New Tubes [Pentode with Low Hum Level, Oscillating Detector, Detector or Volume Control Valve, Two-Volt Pentode, Detector-Amplifier, Diode, Automobile Output Pentode, and Low Noise-Level Valve P.J. 11].—L. Martin, p. 587.
- New Electron Tubes—Facts and Rumours, p. 98.
- New Tubes—Detectors, Rectifiers, Amplifiers [Triple-Twin, Class B Amplifier Valve, Wunderlich Detector, etc.], p. 349; see also Progress, Recent.
- Technical Data on New Tubes [Heater-Type Power Pentode 4 Double-Diode Triodes 55 and 85, Triple-Grid Power Amplifier 89, and Heavy-Duty Full-Wave Rectifier 83], p. 641.
- On the Calculation of an Electron Tube Oscillator [Nomograms for the Barkhausen Formula $V_s = (10.4i)^{2/3}$].—G. A. Kiandsky, p. 286.
- On the Calculation of Electron Tube Oscillators [based on Anode Dissipation].—Joffe, p. 283.
- The Output Power of the Final Stage.—Benz, p. 349.
- Photocell Control of Temperature for Filament-Coating Ovens.—W. P. Koechel, p. 463.
- Thermionic Emission and Electrical Conductivity of Oxide Cathodes.—A. L. Reimann and L. R. G. Treloar, p. 96.
- Strengthening of Interference Colours of Thin Oxide Layers [on Valve Metals].—A. Güntherschulze and F. Keller, p. 410.
- Phenomena in Oxide Coated Filaments. II. Origin of Enhanced Emission.—J. A. Becker and R. W. Sears, p. 227.
- Space-Charge Currents in Oxide-Coated Cathodes.—A. Gehrts, p. 348.
- The Apparent Conductivity of Oxide Coatings used on Emitting Filaments.—R. H. Fowler and A. H. Wilson, p. 642.
- Photoelectric and Thermionic Properties of Palladium.—L. A. Du Bridge and W. W. Roehr, p. 228.
- The Photoelectric and Thermionic Properties of Palladium.—W. W. Roehr and L. A. Du Bridge, p. 463.
- Researches on the Penetration Coefficient or Mutual Controlance of Receiving Valves.—F. Greve, p. 167.
- The Radio-Frequency Pentode; a New Use of the Suppressor Grid.—E. W. Ritter, p. 285.
- Pentode Tubes Used as Triodes.—J. R. Nelson, p. 97.
- Power Detection Characteristics of Pentode Tubes.—H. A. Brown and C. T. Knipp, p. 349.
- Variable-Mu Radio-frequency Pentode Type 39 [6-Volt D.C. Heater-Type].—L. Martin, p. 409.
- Pentode with Extra Electrode for Detection, p. 409.
- A New 6-Volt Output Pentode [Eveready Raytheon LA], p. 587.
- Pentode with Second Screen Grid replacing Usual Outer Grid, p. 641.
- The Pentode in the Output Stage [and the Use of a Frequency Filter to prevent Non-Linear Distortion of the Higher Frequencies and to improve the Sound Pressure Characteristic].—P. Cornelius, p. 641.
- A New Industrial Amplifier Tube for Phototube Circuits [Westinghouse RJ-550].—L. Sutherland, p. 409; see also Industrial.
- The Positive-Grid Tube [working as a Class B Amplifier and giving 20 Watts Undistorted Output].—L. Martin, p. 349.
- The Action of Positive Ions of Caesium on a Hot Nickel Surface.—P. B. Moon, p. 97.
- The Emission of Positive Ions from Cu and Ag.—H. B. Wahlin, p. 169.
- The Emission of Positive Ions from Metals.—H. B. Wahlin, p. 228.
- A Theory of the Emission of Positive Ions from Glowing Metals.—N. Morgulis, p. 410.
- The Surface Ionisation of Potassium by [Hot] Tungsten.—P. B. Moon and M. L. E. Oliphant, p. 588.
- Progress in Tubes, p. 587.
- Recent Trends in Receiving Tube Design.—J. C. Warner, E. W. Ritter and D. F. Schmit, p. 641; see also New, Progress.
- Resistance of an Oscillating Triode.—S. I. Ziltinkevitch, p. 286.
- On the Variation of the Resistance of Thermionic Valves at High [and Ultra-High] Frequencies.—S. K. Mitra and B. C. Sil, p. 463.
- Valve Resistance in Oscillation Generators.—McLachlan, p. 459.
- The Characteristic Surfaces of the Russian Valve Type J-1.—W. Patruschew, p. 168.
- Choosing a Screen-Grid Tube [and the Failure of Transconductance as an Index to the Operating Characteristic].—R. de Cola, p. 349.
- Distortion in Screen-Grid Valves: with Special Reference to the Variable Conductance Type.—R. O. Carter, p. 409.
- The Mode of Action of Screen-Grid Transmitting Valves [based on the Philips' Company's Valves].—C. J. de la Sablonière: Philips' Company, p. 527.
- The Characteristics of Two Screen-Grid Valves Coupled Directly to Each Other.—T. Amishima, p. 409.
- Indirectly Heated Screen-Grid Variable-Mu Valves, Types V.DS and V.MS4, for D.C. and A.C. respectively.—General Electric Company, p. 587.
- Measurement of [Control] Grid-Anode Capacity of Screened Tubes.—E. G. Momot, p. 286.
- On the Effect of Secondary Electrons on the Static Working Condition of the Single Grid Valve.—S. A. Obolensky, p. 228.
- Total Secondary Emission of Electrons from Metals as a Function of Primary Energy.—P. L. Copeland, p. 410.
- The Shot Effect on the Quantum Mechanics [Theoretical Investigation].—H. Fröhlich, p. 97.
- Shot Effect in Space Charge Limited Currents.—E. W. Thatcher and N. H. Williams, p. 286.
- On the Reduction of Shot Effect Fluctuations by Electron Space Charge.—E. W. Thatcher, p. 410.
- Shot Effect and Thermal Noise in the Photo-cell Amplifier.—von Orbán, p. 642.
- British Standard Specification for the Dimensions of Radio Valves and Valve-Sockets, p. 463.
- Surface Heating by Neutralised Positive Rays before and after Return to Normal State.—M. C. Johnson, p. 410.
- Special Symmetrical R.F. Amplifier Valve.—Angwin, p. 97.
- Universal Tube Test Equipment.—O. H. Brewster and K. F. Mayers, p. 97.
- Valve Test Standards.—American Standardisation Committee, p. 286.
- An Automatic Testing and Sorting Machine for Amplifier Valves.—W. Traub and F. Menzler, p. 97.
- An Experimental Study of the Tetrode as a Modulated Radio-Frequency Amplifier [particularly for Radiotelephone Transmission on Frequencies of and above 500 kc.].—H. A. Robinson, p. 168.
- On Thermal Electronic Agitation in Conductors.—N. H. Williams and E. W. Thatcher, p. 410.
- The Investigation of the Thermal Inertia of a Filament by means of a Three-Electrode Kerr Cell.—Rohde and Schnetzler, p. 588.
- On Thermionic Currents Limited by Pure Electron Space Charge.—E. W. Thatcher, p. 588.
- Thermionic Emission from a Plane Electrode.—R. S. Bartlett, p. 97.
- On the Theory of Thermionic Emission.—N. H. Frank, p. 227.
- Thermionic Emission and Space Charge.—N. H. Frank, p. 410.
- Transmission of Electrons through Potential Barrier of Thoriated Filament.—W. B. Nottingham, p. 228.
- Evaporation and Migration of Thorium on Tungsten.—W. H. Brattain, p. 588.
- Special Three-Grid Valve for Alternative Purposes [Pentode, Class A and Class B Triode], p. 463.

A Self-Stopping D.C. Thyatron Circuit [using a Glow-Discharge Tube].—H. J. Reich, p. 168.

B.T.H. Mazda Thyatron, Type BT.1, p. 98.

Thyatron.—See also Grid-controlled, and under "Subsidiary Apparatus."

Dynamic Transconductance Meters.—R. de Cola, p. 588.

A 500 kW [Transmitting] Wireless Valve, p. 39.

The 500 kW Demountable [Transmitting] Valve.—Angwin, p. 98.

500 Kilowatt Demountable [Transmitting] Valves.—Metropolitan-Vickers Company, p. 349.

A Giant [Transmitting] Tube for Radio Transmission.—A. Dinsdale, p. 409.

Transmitting Valves of 300 Kilowatts Output.—Telefunken Company, p. 528.

A German 150 kW Niobium-Cathode [Transmitting] Valve, p. 168.

A New Water-Cooled Power Vacuum [Transmitting] Tube [with Water-Cooled Grid consisting of a Column of Molybdenum Discs].—I. E. Mourumtseff: Westinghouse Company, p. 528.

Two Sets of Elements in One Tube [the Triple-Twin Valve and Circuit].—C. F. Stromeyer, p. 285.

An Improved 120-Volt D.C. Audio Amplifier [Triple Twin Type 291 Valve].—C. F. Stromeyer, p. 463.

Triple-Twin Tubes.—C. F. Stromeyer, p. 587.

Vacuum Tubes as [Ultra] High-Frequency Oscillators [including G.E.C. Water-cooled Triode for 1.5 to 5 Metres].—McArthur and Spitzer, p. 93.

Characteristics of the UV-858 Power Tube [Radiotron Triode, Water-Cooled] for High [and Ultra-High] Frequency Operation.—M. A. Acheson and H. F. Dart, p. 348.

Investigations on Valves Producing Ultra-Short Waves.—Collenbusch, pp. 403-404.

Special Valve for Ultra-Short Waves (5 Watts at 3-Metre Wavelength).—Telefunken Company, p. 463.

Transmitting Valve for Ultra-Short Waves.—Telefunken Company, p. 642.

Multiple Valves for Semi-Aperiodic R.F. Amplification of Ultra-Short Waves.—von Ardenne: Loewe Company, p. 642.

Transmitting Valves for the Generation of Ultra-Short Waves of 1 Metre and Under.—L. Rohde, p. 586.

The Advantages of the Variable-Mu Valve.—W. T. Cocking and W. I. G. Page, p. 87.

On the Connection between "Durchgriff" [Penetration Coefficient] and Emission Law in "Variable Mu" Valves.—G. Jobst, p. 226.

Variable-Mu Valves.—W. I. G. Page, p. 463.

The Variable Slope Valve.—L. Chretien, p. 528.

Variation of the Resistances and Inter-Electrode Capacities of Thermionic Valves with Frequency.—L. Hartsborn: W. E. Benham, pp. 168 and 228.

On One Kind of Variation of Thermionic Emission from Wehnelt Cathode.—Y. Takamura, p. 463.

Welded Transmitting Valves.—Philips Lamp Works, p. 98.

A New Method of Determining Thermionic Work Function by Photoelectric Cell.—Harris, p. 233.

Notes on the Wunderlich Tube [for Grid Leak Power Detection].—F. E. Terman: Wunderlich, p. 349.

Further Description and Characteristics of the Wunderlich Radio Tube.—F. E. Terman, p. 587.

The RCA-46, a Zero-Bias Output Valve for Class B Operation in an A.C. Mains Receiver.—Barton, p. 587.

A New Zero-Bias Output Tube [Type ER-49, for Class B Operation in 2-Volt Receivers].—J. R. Nelson: Raytheon Corporation, p. 587.

DIRECTIONAL WIRELESS.

S.F.R. Compensated Night Effect Radiogoniometer [Adcock Aerials with Air-Core Transformers].—Soc. Franç. Rad.élec., p. 410.

The Performance of the Marconi-Adcock Direction Finder.—N. E. Davis, p. 588.

Electricity in Aerial Navigation, p. 39.

Progress in Aeronautic Radio Research [Equi-Signal Beacon Receivers, etc.], p. 410.

Two-Way Five-Metre Telephony Aeroplane Tests.—Lyman and Kelly, p. 411.

Five-Metre Aeroplane [to Ground Stations] Tests Overwhelmingly Successful.—Lyman, p. 588.

Radio Direction Finding Applied to Air Lines [and in particular the Suppression of Night Effects and "Aeroplane Effect," leading to a description of the "Aéropostale" Opposed Frame Radiogoniometer].—Serre, pp. 39 and 98.

Radio Communication on the International [Pan American] Air Lines.—H. C. Leuteritz, p. 287.

Radio Aids to Air Navigation.—L. A. Sweny, p. 287.

New Aircraft Beacon: Visual Type [Equi-Signal] Course Indicator for Croydon Aerodrome.—Marconi Company, p. 98.

Acoustic Sounding by Echoes on board Noisy Aircraft.—C. Florisson, p. 350.

The "Askania" Telecompass for Aircraft [with Air Transmission], p. 411.

Long-Wave Communication for Aircraft.—Eisner, p. 644.

Prevention of Aircraft Collisions by Infra-Red Rays and the Fournier-Céma Cell, p. 350.

Airplane Receiving Equipment for Visual Radio Range-Beacons.—Note from the U.S. Bureau of Standards, p. 410.

A Simultaneous Radiotelephone and Visual Range Beacon for the Airways.—F. G. Kear and G. H. Wintermute, p. 350.

The Radio of the [Pan-American] Airways.—H. C. Leuteritz, p. 588.

Direction Finding for Aviation, especially for the Luft-Hansa Line.—E. Schwandt, p. 169.

Wireless Engineering in connection with Aviation.—H. Fassbender and others, p. 644.

Radio Direction Finding Experiments with Aurora.—B. Düll, p. 643.

Systems of Radio Beacon [particularly Besson's "Associated Loop-and-Aerial" or "Symmetrical Cardioids" System used at La Pallice].—P. Besson, p. 39.

Equi-Signal Beacon on Lorry.—C. J. Madsen, p. 643.

New Developments in Radio Beacons [Visual Reception, and the Use of Ultra-Short Waves].—E. Kramar: Lorenz Company, p. 642.

On the Bearing Breadth in Direction-Finder Receivers [and Its Dependence on Signal Strength and Background Noise Level].—P. Hermanspann, p. 528.

Landing Blind [use of a Series of Concentric Cables to give Position and Approximate Height].—F. Celler, p. 350.

Electrical Aids to Blind Flying.—A. Klemin, p. 40.

An Electrical Method of Indicating the Limits of a Landing Ground, to assist Blind Landings.—H. Gromoll, p. 644.

Australian R.R.B. Results with the Cathode Ray Direction Finder, p. 158.

Coastal and Harbour Wireless Services.—Marconi Company, p. 39.

Electronic Direction Finder [Compass].—P. Schwerin, Perriman Electric Company, p. 350.

New Method for Distance Finding [Combination of Radio Signal and Fog Horn Blasts], p. 644.

The Natural Electromagnetic Oscillation of a Rod-Shaped Conductor at the Surface of Separation of Two Media with Different Dielectric Constants [Application to Direction Finding Errors caused by Resonance with the Ship's Hull].—H. Ruprecht, p. 287.

Airplanes See Through Fog with New Photo-cell Device.—Langmuir and Westendorp, p. 169.

Echoes from Danger Points Guide Boat Through Fog [Sonic Locator, using 3000-Cycle Whistle].—C. W. Rice, p. 350.

Fog-penetrating Properties of Infra-red and Ultra-violet Rays.—S. H. Anderson, p. 98.

Receiving Frame Aerials for Low-frequency Alternating Magnetic Fields [for Loth Systems].—C. Bourgonnier and M. Durepaire, p. 350.

Directional Observation of Low-frequency Waves.—E. Yokoyama, T. Nakai and I. Tanimura, p. 350.

The Development and Application of Marine Radio Direction Finding by the U.S. Coast Guard.—C. T. Solt, p. 287.

Radiogoniometers for Marine Work [Comparison of Fixed Loop and Rotating Frame Receivers], p. 98.

The Use of Radioelectric Waves in Maritime Signalling.—Besson, p. 528.

Marconi Direction Finder Type D.F.G.9b [for Naval Purposes, using Small Shielded Frame Aerial], p. 588.

Direction Finder Type D.F.G.9a [particularly for Naval Work].—Marconi Company, p. 410.

Navigation by Wireless.—C. G. Phillips, p. 287.

Directional Records [on several spaced Direction Finders] of Night Effect.—M. Dieckmann, p. 287.

Night Errors and the Polarisation of Down-Coming Waves.—Appleton, p. 169.

The Causes of Night Errors in Direction Finding.—B. Düll, p. 643.

Portable [Equi-Signal] Beacon Transmitter for the [U.S.] Army, p. 287.

Diagram for Position Finding by Long Distance Bearings and for Finding the Bearing of One Point from Another.—T. J. Richmond, p. 98.

Position Location at Sea.—R. Naismith, p. 98.

Theory of Design and Calibration of Vibrating Reed Indicators for Radio Range Beacons.—G. L. Davies, p. 169.

Direct-Reading Stroboscopic Radio Direction Finder.—R. Hardy and Bertrand-Lepaute, p. 642.

An Experimental Direction-Finder for Use on Ultra-Short Waves.—Smith-Rose and McPetrie, p. 39.

Ultra-Short Waves.—See also Beacons.

Variation of Bearings observed in Short-Wave Direction-Finding [on a Small Rotating Frame].—M. Asukai and T. Hayasi, p. 169.

A Watch Compass for Navigational Direction Finding [for use on Rotating Loop Beacon Signals].—S. J. Matthews, p. 98.

New Wireless Compass, p. 39.

ACOUSTICS AND AUDIO-FREQUENCIES.

A New Industry—Manufacture of Sound Absorbing Materials.—Bureau of Standards, p. 647.

The Absorption of Sound in Acoustic Tubes and Horns.—Y. Rocard, p. 647.

- The Acoustic Absorption Band of Carbon Dioxide.—E. Grossmann, p. 290.
- Measurements of High Frequency Sound Absorption in Gases.—E. Grossmann, p. 466.
- Application of Norris-Andree Method of Reverberation Measurement to Measurements of Sound Absorption.—R. F. Norris, p. 352.
- An Automatic Reverberation Meter for the Measurement of Sound Absorption.—W. F. Snyder, p. 588.
- Some of the Factors which Affect the Measurement of Sound Absorption [Effect of Absorption by Moist Air, and Choice of Initial, Average or Final Slope of Decay Curve].—V. L. Chrisler and C. E. Miller, p. 647; see also Humidity.
- Equipment for Simple and Rapid Measurement of Sound-Absorption Properties of Materials.—A. L. Albert and W. R. Bullis, p. 40.
- A Simplified Instrumental Method of Measuring Sound Absorption Coefficients.—J. F. Mackell, p. 40.
- The Precision of Measurement of Absorption Coefficients by Reverberation Methods.—P. E. Sabine, p. 171.
- The Determination of Absorption Coefficients for Frequencies up to 8000 Cycles.—F. L. Hopper, p. 352.
- Objective Measurement and Subjective Observation of Acoustic Phenomena.—F. Trendelenburg, p. 99.
- Recent Developments in Acoustics, particularly Applied Acoustics (Continued).—F. Trendelenburg, p. 99.
- The Effects of Interior Acoustics in the Recording and Reproduction of Sound.—F. Trendelenburg, p. 288.
- Studies on the Room-Acoustics, Part I [Comparison between Results with Sustained and Impulsive Sounds: the Equivalent Sphere representing a Room].—A. Hirayama, p. 647.
- Modern Treatment of Broadcasting Acoustics.—S. K. Wolf, p. 288.
- Acoustics of a Building Improved 25% by the Audience Standing Up.—S. K. Wolf, p. 171.
- Bibliography of the Acoustics of Buildings.—F. R. Watson, p. 171.
- Papers on the Acoustics of Buildings.—E. Michel: F. R. Watson, p. 288.
- Correction of the Acoustics of Buildings [Some New Sound-Insulating Materials], p. 229.
- The Acoustics of Halls.—P. M. Prache, p. 529.
- Acoustics of Very Large Auditoriums do not conform with Customary Methods of Analysis and Correction.—S. K. Wolf, p. 99.
- On the Admittance of Linear Oscillating Systems [Application to Loud Speaker Cones].—Strutt, p. 33.
- On the Circulations Caused by the Vibration of Air in a Tube.—E. N. da C. Andrade, p. 100.
- On the Groupings and General Behaviour of Solid Particles under the Influence of Air Vibrations in Tubes.—E. N. da C. Andrade, p. 647.
- On the Determination of Pressure in Impulsive Air Waves.—W. Schneider, p. 290.
- Acoustic Altimeter for Aircraft.—Florisson, p. 350.
- The DVL Audimeter used in Measuring Background Noise of Aircraft Receivers.—Brintzinger and Viehmann, p. 529.
- A Note on the Sound Generated by a Rotating Airscrew.—E. T. Paris, p. 229.
- Some Properties of the Sound Emitted by Airscrews.—C. F. B. Kemp, p. 466.
- Audio Frequency Amplification [and the Use of a Special Transformer-coupled Amplifying Circuit].—L. A. Meyerovitch and P. A. Lossizky, p. 466.
- D.C. Gramophone Amplifier [with Undistorted 5 Watt Output].—R. A. Fereday, p. 589.
- The Measurement of Power in Amplifiers [the Burstyn "Audimeter" for Sound Film Apparatus].—P. Hatschek: Burstyn, p. 646.
- Contributions to the Design Calculations of Amplifiers for Multiple Address Systems.—H. Reppisch, p. 590.
- A Simple Harmonic Analyser.—Nicholson and Perkins, pp. 416-417.
- A New Method of Sound Frequency Analysis [Hot-Wire Resistance Method using a Valve Filament].—T. Theodorsen, p. 229.
- A Valve Voltmeter Method of Harmonic Analysis.—W. Greenwood: Suits, p. 465.
- A Simple Method of Harmonic Analysis.—F. Nachtkal, p. 589.
- Sound Analysis by the Control of the Saturation Current of a Two-Electrode Valve.—J. Diebitsch and H. Zuhrt, p. 644.
- Sound Analysis by Use of Brightness Fluctuations of an Incandescent Bulb Filament, registered by a Photoelectric Cell.—Diebitsch and Zuhrt, p. 645.
- Transmission of Sound through Apertures [Confirmation of Lamb's Predictions].—E. Ritchie, p. 352; see also Openings.
- Articulation in Telephonic Communications.—P. Chavasse, p. 44.
- An Automatic Device for Recording, Correcting and Analysing Articulation Results.—J. Collard, p. 287.
- Articulation Tests in English, German and French using Esperanto Pronunciation, p. 99.
- The Connection between Auditory Sensation and the Effective Value of the Exciting Sound Pressure, and Its Influence on the Audibility of Distortions.—W. Janovsky, p. 172.
- The Bechstein-Siemens-Nernst "Grand": a New Universal Instrument [Small Grand Piano with Amplifiers and Timbre-Selecting Damping, etc.].—Schultz: Noack, p. 101.
- Further Study of [Biological] Effects of Intense Audio-Frequency Sound.—N. Gaines and L. A. Chambers, p. 466; see also Sterilisation.
- Measurement of Capacities at Audio-Frequencies by Double-Beat Method.—Colebrook, p. 171.
- Bell-less Electric Carillon [at Camden, N.J.; Reed Vibrations amplified by 1 Kilowatt Audio-Amplifier].—RCA Victor Company, p. 646.
- Acoustical and Electrical Power Requirements for Electric Carillons [and the Use of the Sound Measuring Meter].—A. N. Curtiss and I. Wolff, p. 413.
- The Use of the Cathode-Ray Oscillograph in the Study of Distortion, Phase-Relations, etc.—Zworykin, p. 99.
- A Method of [Audio-] Frequency Measurement with the Cathode Ray Oscillograph [used as Source of Comparison Frequency and as Indicator].—L. A. Wood, p. 589.
- Three Simple Investigation Methods [based on Chladni Figures] for Experimental Acoustics.—N. Andrejew, p. 100.
- Audio-frequency Compensation Methods.—J. G. Aceves, p. 99.
- Theory of the Acoustic Conductivity of Simple and Composite Partitions.—E. Wintergerst, p. 466.
- Curves of Equal Sound Strength.—R. Berger, p. 647.
- On the Sound Radiation from a Circular Diaphragm vibrating with Nodal Lines.—M. J. O. Strutt, p. 169.
- Air Column Resonances and Symmetrical Modes of Truncated Conical Shells (Loud Speaker Diaphragms).—N. W. McLachlan, p. 230.
- Nodal Lines on Vibrating Diaphragms.—N. W. McLachlan, p. 41.
- The Behaviour of Conical Diaphragms used in Acoustic Apparatus for the Reproduction of Speech and Music.—N. W. McLachlan and G. A. V. Sowter, p. 41.
- The Effective Mass of Flexible Discs and Conical Diaphragms Used for Sound-Reproduction.—N. W. McLachlan, p. 169.
- Measurement [by Ultra-Micrometric Method] of the Static and Dynamic Displacements of Telephone Diaphragms.—G. Sacerdote and E. Gotta, p. 42.
- The Law of Similarity for the Natural Frequencies of Elastic Bodies and Particularly Loud Speaker Diaphragms.—E. Spenke, p. 169.
- Sound Diffraction by Rigid Circular Plate, Square Plate and Semi-Infinite Screen.—L. J. Sivian and H. T. O'Neil, p. 645.
- A Direct-Indicating Acoustic Measuring Equipment [using the Hollmann-Schultes "Room Acoustic" Relaxation Oscillations].—H. E. Hollmann and Th. Schultes, p. 171.
- Directive Audition in Space.—J. L. Van Soest and P. D. Groot, p. 40.
- On the Sound Field in the Neighbourhood of an Oscillating Plane Disk.—R. Ruedy, p. 41.
- The Dispersion of High Frequency Sound Waves in Carbon Dioxide Gas.—H. O. Kneser, pp. 229 and 467.
- On Acoustic Dispersion Theory.—H. O. Kneser, p. 229.
- Percentage Harmonic Distortion.—Greenwood: Bedford: Calendar: Scroggie, pp. 100 and 230.
- Distortion in Microphones and Loud Speakers.—C. A. Hartmann, p. 289.
- Audio-frequency Distortion Measurements [Grützacher Analyser: Failure of "Klirrfactor" to give Distortion as heard by Ear; Another Method giving Combination Tones throughout Entire Audible Range].—Hoffmann, p. 645.
- Distortions, Audibility of.—See Auditory Sensation.
- Doppler Effect with Piezo-Quartz Crystals.—H. Müller and T. Kraefft, p. 466.
- Differential Pitch Sensitivity of the Ear.—E. G. Shower and R. Biddulph, p. 230.
- Remarks on the Theory of the Most Favourable Echo Duration in Large Rooms.—G. v. Békésy, p. 40; see also Reverberation.
- On the Calculation of Mechanical Vibrating Systems by the Use of the Equivalent Electrical Circuits.—Forstmann, p. 221.
- Papers on L.F. Feed-Back in Radio Receivers.—Bouck: Brooke, p. 230.
- The Delusiveness of Filtering Compound Sounds.—M. F. Meyer, p. 590.
- Precision Methods Used in Constructing Electric Wave Filters for Carrier Systems.—Harris, p. 417.
- On Acoustic Filters.—E. Waetzmann and F. Noether, p. 466.
- The Theory of Acoustic Filtration in Solid Rods.—R. B. Lindsay and F. E. White, p. 466.
- A New Method of Measuring Frequencies [using Johnsen-Rahbeck Effect].—Makower and Makower, p. 104.
- Bass Drum and Tympani—the 5000 Cycle [Frequency] Limit, p. 344.
- A Tachometer-Type Frequency Meter for Loud Speaker Testing and Other Purposes.—E. Thielmann: Formig: Lenzola Company, p. 412.
- A Sound Transmitting and Reproducing Equipment with a Wide Frequency Range [30 to over 10 000 Cycles per Second].—W. Willms, p. 288.
- What the Ear Hears [Frequency Range for Faithful Reproduction], p. 464.
- Higher Fidelity Standards are Here! [Increased Frequency Ranges], p. 463.
- Audible Frequency Ranges of Music, Speech and Noise.—W. B. Snow, p. 98.

- An Improved Audio-frequency Generator.—E. G. Lapham, pp. 44 and 287.
- A Beat Frequency Generator for Frequencies from 30 to 10 000 c/s, p. 465.
- An Adjustable Frequency Generator for the Voice Range [Valve-controlled Three-phase Motor Generator Set].—J. R. Power, p. 287.
- Generator of Electrical Oscillations at Musical Frequencies [Musical Heterodyne].—Soc. Franç. Rad.élec., p. 413.
- Correction to "Measuring Frequency Characteristics with the Photo-Audio Generator."—J. H. O. Harries: Schäffer and Lubszynski, p. 352.
- The "Nunan" Circuit as a Valve Note Generator (Valve Hummer).—W. Muchlinsky, p. 100.
- Investigations on the "Howl" Generator.—W. L. Barrow, p. 229.
- "Howl" Generators.—H. von Hartel, p. 413.
- Generators.—See also Oscillators.
- Acoustic Properties of Glass Sheet.—E. Meyer, p. 647.
- The Steel Band [Insulated and Wound into a Spiral] as Gramophone Disc.—F. Noack: Stille, p. 413.
- Frequency Characteristics and Record-Wear of Gramophone Pick-Ups.—M. Kluge, p. 646.
- Photomicrographs of Gramophone Records [and the Use of a Thin Coating of Immersion Oil].—A. Morris Thomas, p. 171.
- Reproduction de Luxe: Inauguration of New Branch of the Gramophone Company, Limited, p. 43.
- Electrical Gramophone Recording and Reproduction.—A. Forstmann, p. 43.
- The Home-Recording of Gramophone Discs.—E. Nesper, p. 529.
- Improved "Mid-Odi" Long-Playing Gramophone Needle, p. 101.
- Gramophones.—See also Phonographs, Recording, Reproduction, Talking Machines, Vertical Cut.
- Eliminating Harmonics in Bridge Measurements.—R. F. Field, p. 287.
- A Device for Separating the Harmonics of Complex Waves, with Special Application to the A.C. Potentiometer [Extension of Joubert Contact Maker].—D. C. Gall: Messrs. Tinsley, p. 589.
- Binaural Hearing.—G. W. Stewart, p. 464.
- Sound and Hearing.—N. F. Cave-Brown-Cave, p. 413.
- Theories of Hearing.—H. Hartridge, p. 647.
- On the Theory of Hearing with Sound Received by Conduction through Bone.—G. v. Békésy, p. 413.
- The Heating of Liquids by the Absorption of Sound, and Its Relation to the Energy of Intense High-frequency Sound Waves.—W. T. Richards, p. 100.
- High Audio Power from Relatively Small Tubes: Discussion.—R. A. Heising: Barton, p. 44.
- The Relation of Relative Humidity to the Absorption of Supersonic Waves in Various Mixtures of CO₂.—H. H. Rogers, p. 647.
- Humidity: see also Absorption.
- A Method of Measuring Acoustic Impedance.—P. B. Flanders, p. 589.
- The Study of Sound-Insulating Building Materials by Means of Electrical Measuring Apparatus.—Cellerier, p. 171.
- The Insulation of Sound [Tests on Cork, Kapok, Bamboo Tissue, Newspaper, etc.].—R. Moens, p. 352.
- Sound Intensity Measurements by the Method of "Acoustic Twinkling."—F. Canac, p. 288.
- The Acoustic Resonator Interferometer.—J. C. Hubbard, pp. 171 and 647.
- Multiple Peaks in Supersonic Interferometry.—W. D. Hershberger, p. 529.
- The Müller Metallic Membrane Light-Control Device.—Müller: Mey, p. 529.
- The Principles of the Light Valve.—T. E. Shea, W. Herriott and W. R. Goehner, p. 646.
- Effects of Optical Slits in Light-Valve Sound Recording.—J. P. Livadary, p. 43.
- Dynamic [Loud] Speaker Design.—A. R. Barfield, pp. 464 and 645.
- A Loud Speaker without Baffle.—Bethenod, p. 42.
- Measurement of the Phase and Amplitude Curves of Electrodynamic Loud Speakers.—W. Binder, p. 229.
- A Device for Rapidly Plotting Loud-Speaker Response Curves.—F. H. Brittain, p. 412.
- Loud Speaker ensuring Low Note Fidelity.—Charlin and Toulon, p. 42.
- A Novel Loud-Speaker Movement [Eddy-Current Drag from Rotating Disc].—Gladenbeck, p. 589.
- Dynamic Loudspeaker Design [of Magnetic Circuit].—J. E. Goeth, p. 42.
- The Calculation of Loud Speakers with Rigid Disc Membranes.—W. Hähnle, p. 170.
- New Dual Loud Speaker.—H. A. Hartley, p. 645.
- The Determination of the Efficiency of Loud Speakers [by a purely Acoustic Method].—W. Heimann, p. 645.
- Improved Fidelity of Two-[Loud] Speaker Radio Receivers.—H. S. Knowles, p. 464.
- The Loud Speaker Coil of Optimum Mass.—N. W. McLachlan: Strafford, pp. 351 and 464.
- Electro-Mechanical Rectification [and Its Effect on Loud Speaker Reproduction].—N. W. McLachlan: P. K. Turner, pp. 464 and 589.
- On the Symmetrical Modes of Vibration of Truncated Conical Shells; with Applications to Loud-Speaker Diaphragms.—N. W. McLachlan, p. 411.
- Radio Loud Speakers.—N. W. McLachlan, p. 230.
- Building-Up and Decay Processes in Electrodynamic Loud Speakers with Strong Magnetic Fields.—H. Neumann, p. 170.
- The Inductor Dynamic Loud Speaker.—D. A. Oliver, p. 100.
- Loud Speakers with Independent Control added to Radio Receivers.—W. L. Parsons, p. 589.
- Loud Speakers in Opera Production.—R. Raven-Hart, p. 412.
- The Loud Speaker Equipment of the Stadium of the Darmstadt Technical College.—F. Schilgen and C. Starkloff, p. 170.
- The Influence of the Resistance of the Current Source [Output Valve Stage] and Parallel Capacity on the Frequency Characteristic of a Loud Speaker.—F. Söchting and W. Nowotny, p. 351.
- The Theory and Application of the Horn Loud Speaker [and the Superiority of the Exponential Horn].—H. Stenzel, p. 170.
- The Horn Loud Speaker.—H. Stenzel, p. 289.
- Moving Coil Loud Speakers of Midget Design.—F. R. W. Strafford, p. 290.
- The Loud Speaker Coil of Optimum Mass.—F. R. W. Strafford: McLachlan, p. 412.
- On the Amplitude of Driven Loud Speaker Cones: Discussion.—M. J. O. Strutt: N. W. McLachlan, p. 101.
- On the Equivalent Mass of Driven Loud Speaker Cones.—M. J. O. Strutt, p. 350.
- Effective Mass of Loud Speaker Cones.—G. A. V. Sowter: Strutt, p. 411.
- Extension of the Frequency Range faithfully reproduced by Loud Speakers [Combination of Several Loud Speakers with Different Characteristics, Several Amplifiers and Corresponding Filters, for Sound Film Reproduction].—P. Toulon: Établissements Charlin, p. 350.
- The Moving Iron Loud Speakers.—S. J. Tverll, p. 100.
- The Singing Condenser [Electrostatic Loud Speakers, especially the Double-Sided Oscilloplane with Aluminium-Magnesium Alloy Diaphragm].—H. Vogt, p. 42.
- The Generation of Sound by the Electrostatic Field and the "Statophone" and "Oscilloplane" Loud Speakers.—H. Vogt, p. 170.
- Calculation of Loudspeaker Efficiency.—I. Wolff, p. 351.
- The Use of Two Loud Speakers in a Single Set, in U.S.A., p. 464.
- Loud Speakers Under Test.—p. 101.
- Loud Speakers.—See also Admittance, Diaphragms, Disks, Distortion, Frequency, Networks, Plate, Radiation (Resistance), Radiators, Rochelle Salt, Tone Control.
- The Apparent Reduction of Loudness.—D. A. Laird, E. Taylor, and H. H. Wille, Jr., pp. 352 and 589.
- The Loudness of Sound.—N. W. McLachlan, p. 590.
- The Importance of the Magnetic Bias in Electromagnetic Telephones [and Loud Speakers].—L. Draub, p. 645.
- Moving Coil Magnets: Precision Measurements of the Gap Flux Density.—C. E. Webb, p. 290.
- The Measurement of [Low Audio-frequency] A.C. Potentials by means of Dry-Plate Rectifiers [a Method independent of Wave-Form and Frequency].—Focaccia, p. 473.
- Absolute Measurement of Sound-Amplitudes and Intensities.—E. N. da C. Andrade, p. 590.
- The "Phonic Tester" for the Measurement of the Mechanical Intensity of Sounds.—J. F. Cellerier, p. 413.
- Some Acoustic and Telephone Measurements [British Post Office: including Loud Speaker Tests].—H. R. Harbottle, pp. 413 and 589.
- Acoustic Measuring Instruments.—C. V. Drysdale, p. 590.
- The Dynatron Audio-Frequency Meter.—J. Kahan, p. 529.
- Technique of Microphone Calibration.—S. Ballantine, p. 412.
- Boutonnière Microphone for Broadcasting Speeches, in place of Array of Fixed Microphones.—Bell Telephone Laboratories, p. 43.
- New Moving Coil Microphone.—A. Dinsdale, p. 101.
- Carbon Microphones [A Defence of Their Transmission Quality].—S. T. Fisher, p. 170.
- The Development of the Microphone.—H. A. Frederick, p. 43.
- Microphone Technique in Radio Broadcasting.—O. B. Hanson, p. 170.
- An Efficient Miniature Condenser Microphone System.—H. C. Harrison and P. B. Flanders, p. 589.
- The Lapel Microphone [for Public Address Speakers].—W. C. Jones, p. 289.
- A Moving Coil Microphone for High Quality Sound Reproduction.—W. C. Jones and L. W. Giles, p. 289.
- A Method of Calibrating the Condenser Microphone by the Use of a Periodically Varying Substitution Condenser.—W. Lange, p. 412.
- A New Carbon Microphone [with a Good Frequency Characteristic].—M. Marinisco, p. 43.
- The Ribbon Microphone.—G. S. Mitchell, p. 42.
- A New Ribbon Microphone with Plane of Zero Reception, for Sound Film Recording.—H. F. Olson, p. 43.
- The Calibration of Microphones.—H. F. Olson and S. Goldman, p. 43.
- Researches on a Microphone for Broadcasting [Development of a Radio-frequency Circuit for Use with the Wentz Condenser

- Microphone in place of the usual Amplifying Circuit].—A. H. Reeves, p. 42.
- A Sensitive Moving-Coil Microphone of High Quality: Adapting the Moving-Coil Microphone to Commercial Use: Mountings, Connectors and Amplifier for Moving-Coil Microphone.—Thuras: Giles: Leuvelink, p. 589.
- All German Broadcasting Stations to Use Condenser Microphone (Neumann Type) in place of Reiss Marble-Block Microphone.—p. 465.
- Microphones.—See also Distortion, Moving Coil, Rochelle Salt. An Analysis of the Series Type Mixing Control [for several Microphones].—L. B. Hallman, Jr., p. 43.
- Moving Coil Microphone and Loud Speaker of Special Type.—G. Giulietti, p. 412.
- Moving-Coil Telephone Receivers and Microphones.—E. C. Wentz and A. L. Thuras, pp. 43 and 101.
- Additional Experiments on Moving Coil Reproducers and on Flexible Discs.—N. W. McLachlan, p. 189.
- Electrical Music.—O. Vierling, p. 352.
- The New Music of Electronic Oscillations: the Latest Instruments of Theremin, Ranger and Miessner, p. 352.
- Electrical Music and the Building-Up of Tones.—F. Trautwein: Backhaus, p. 465.
- Musical Requirements for Note-Modulated Scanning [Television of Music].—F. W. Winckel, p. 529.
- The Electrical Musical Instrument: the Generation of Vibrations by Thermionic Valves [Comprehensive Survey, with List of Papers and Patents].—O. Vierling, p. 529.
- Electrical [Musical] Instrument gives Piano and Organ Effects.—B. F. Miessner, p. 44: see also Bechstein.
- The Electrical Musical Instrument: the Generation of Vibrations by Mechanical-Electrical Methods.—Vierling, p. 646.
- The Sound Spectra of Musical Instruments.—E. Meyer, p. 172.
- The Sound Spectra of Musical Instruments.—E. Meyer and G. Buchmann, p. 646.
- High Frequencies Necessary for Correct Reproduction of Certain Musical Instruments.—Stokowski, p. 646.
- Circuit Matching in Networks for Radio Distribution [to Loud Speakers].—Six and Vermeulen, p. 299.
- Noise.—N. W. McLachlan, p. 413.
- The Measurement of Noise: a New Service of Electrical Research Products.—S. K. Wolf: Acoustic Consulting Service, p. 288.
- Measuring *versus* "Judging" Loudness of Noise [The Cube Root Law of Perceived Intensities].—E. E. Free: Parkinson and Ham, p. 288.
- Measurements on Noise and Din.—G. Bakos and S. Kagan, p. 288.
- The Noise Survey of the Rapid Transit Lines of New York City.—G. T. Stanton and J. E. Tweeddale, p. 352.
- On the Loudness of Noise.—H. B. Marvin, p. 352.
- Noise Recorder for Comparing Street-Car Sounds, p. 413.
- Measures for Preventing the Transmission of Noise in Ventilating Systems.—J. Lindner, p. 466.
- Measurement of Noise.—G. W. C. Kaye, p. 466.
- The Measurement of Noise [Barkhausen Noise-meter: Eisenberg's Modification: the Dold-Thiele Integrating Meter using Evolution of Gas], p. 529.
- The Measurement of Noise.—A. H. Davis, p. 590.
- Testing Motor Tyres for Noise, p. 647.
- On the Use of Acoustic Filters as Noise Absorbers.—K. Schuster and M. Kipnis, p. 646.
- Noise and its Measurement.—G. W. C. Kaye, p. 41.
- Noises.—K. W. Wagner, p. 529.
- Methods for Measuring Interfering Noises.—Lloyd Espenschied, p. 100.
- Report on Noises and Their Measurement.—P. Chavasse, p. 466.
- Analysis of Noises and Musical Sounds.—E. Meyer, p. 590.
- Acoustic Nomenclature and Definitions [Phon and Decibel].—C. F. Kemp: G.W.O.H., pp. 466 and 589.
- The Passage of Sound through Small Openings [Badly Closing Doors, Keyholes, etc.].—E. Wintergerst and W. Knecht, p. 647: see also Apertures.
- Electronic Organ, Coupleux-Givelet System, at the Church of Villemonble, near Paris, p. 413.
- A Neon Tube Audio-Frequency Oscillator.—D. Pollack, p. 229.
- String Oscillator.—J. Zahradníček and Z. Zák, p. 413.
- An Audio Oscillator of the Dynatron Type.—Don Hale, p. 465.
- Oscillators.—See also Generators.
- Oscillograms as a Logical Form of Written Speech [and Musical Composition].—L. Stokowski, p. 287.
- The Rapid Record Oscillograph in Sound Picture Studies.—Curtis, Shea and Rumpel, p. 413.
- Graphical Determination of the Maximum Output of Single- and Multiple-Grid Valves for a Given Anode Potential and Full Modulation of the Working Characteristic in the Negative Region.—J. Kammerloher, p. 43.
- Calculation of the Necessary Power Output of the Final Stage of a Sound Reproducing Apparatus [for Any Given Room].—F. Aigner, p. 411.
- Capacitive Output Coupling [between Output Valve and Acoustic Load: Improvement of Frequency Curve by Suitable Choice of Capacity].—Sims, p. 456.
- The Determination of the Output Power of Amplifiers.—F. Benz, p. 352.
- The Problem of Pentode Output Fidelity.—L. Tulauskas, p. 44.
- The Pentode in the Output Stage [and the Use of a Frequency Filter to prevent Non-Linear Distortion or the Higher Frequencies and to improve the Sound Pressure Characteristic].—Cornelius, p. 646.
- Some Overlooked Opportunities for Electrical Phonographs.—V. Karapetoff, pp. 412 and 413.
- Practical Units in Acoustics, and Phonometric Measurements. A New Phonometer for All Frequencies [using a Neon Tube Generator].—A. Bernini, p. 352.
- Determination of the Resolving Power of Photographic Layers.—H. Frieser, pp. 171 and 288.
- The Production of [Photographic] Negatives with Finer Grain than that of the Original Emulsion, by Development with Paraphenylene-Diamine.—A. Lumière and A. Seyewetz, p. 101.
- Optical Methods for Reducing the Effects of Photographic Plate Graininess. With Special Reference to Special Line and Star Image Measurements.—F. E. Wright, p. 43.
- The Natural Vibrations of Open Pipes.—H. P. Leopold, p. 467.
- Transverse Vibrations of an Annular Plate of Variable Thickness.—J. Ghosh, p. 645.
- The Forced Vibrations of a Circular Plate.—W. Flüge: Elsas, p. 414.
- The Vibrations of a Circular Plate.—R. C. Colwell, p. 414.
- The Mathematical Theory of Chladni Plates.—R. C. Colwell, p. 414.
- Diagonal Symmetry in Chladni Plates.—R. C. Colwell, p. 645.
- The Vibrations of Rods and Plates.—R. C. Colwell, p. 645.
- A New Sound Pressure Rectifier [for the Direct Measurement of Sound Pressures of 50-8000 Bars].—F. Ribbentrop, p. 645.
- The Dollar Cost of Tone Quality.—W. R. McCanne, p. 44.
- The Calculation of the Radiation at the Edges of Stretched Membranes, and the Derivation and Use of General Formulae for the Radiation Resistance.—H. Stenzel, p. 289.
- On the Radiation Resistance in connection with the Vibrations of a Cone-Shaped Membrane.—A. Th. Van Urk, p. 42.
- The Acoustic Radiated Power of Radiator Groups, particularly the Circle and Sphere Groups [Application of a Rayleigh Formula].—F. A. Fischer, p. 464.
- High Power Radiators for Frequencies below 100 Cycles per Second.—E. W. Kellogg, p. 170.
- The Definition of the Titles "Pressure" and "Motion" Receivers.—K. Schuster, p. 589.
- A Reciprocal Theorem in the Theory of Diffraction [Application to Theory of Loud Speakers and Aerial Arrays].—F. D. Smith, p. 645.
- A Simple Stylus and Rotating Drum Speech Recorder, from a Loud Speaker Movement.—Ketterer, p. 101.
- Glow-Lamp Noiseless Recording.—E. H. Hansen, p. 101.
- Sound Recording on Unsensitized Back of Picture Film by Variations in the Thickness.—Bracher: Huguenard, p. 101.
- The Recording of Sound and its Use in Broadcasting [particularly the Huguenard System of Inscription on Celluloid].—Huguenard, p. 646.
- The A.E.G. Home Recording Outfit.—A.E.G., p. 101.
- Recording of Long Programmes or Books: an Austrian Device.—J. Saxl: Thirring and Richtera, p. 351.
- A New Method of Recording Sound and Vibrations [Photographic Version of the Hydraulic Microphone].—H. Greinacher, p. 351.
- The Sound Recording Camera [Sound-on-Film Recording Systems].—W. H. O. Sweeny, p. 465.
- Physics in Sound Recording.—A. Whitaker, p. 170.
- The Recording and Reproducing of Sound (Cantor Lecture).—A. G. D. West, p. 41.
- Frequency Characteristics in Film Recording and Reproducing.—G. Lewin, p. 352.
- Electro-Mechanical Rectification: A Moving Coil L.S. Phenomenon.—N. W. McLachlan: Turner, pp. 464 and 589.
- The Use of the Dry-Plate Rectifier in Audio-frequency Measuring Technique.—W. Wolman and H. Kaden, p. 41.
- Phase-Sensitive "Rectifier Bridge" for Measuring a Desired Component in an A.C. Potential.—Walter, p. 589.
- The Use of the Rectifier Bridge in Test Room Technique [as Phase-Sensitive Indicator, Frequency Analyser, etc.].—Walter, p. 645.
- The Reflection of Sound Waves in Thin Anisotropic Plates.—A. Seiffert, p. 530.
- Measurements of Sound Reflection Coefficients of Materials for Defined Sound-Field Ratios.—L. Casper and G. Sommer, p. 172.
- On the Construction of Sound Reflectors [for Pulpits, etc.].—A. D. Fokker, p. 288.
- "Room-Acoustic" Relaxation Oscillations.—H. E. Hollmann and Th. Schultes, p. 99: see also Direct-Indicating.
- Broadcast Reproduction.—H. A. Hartley, p. 464.
- Modern Apparatus for the Reproduction of Speech and Music.—N. W. McLachlan, p. 101.
- The Bottle-Pipe Resonator.—A. E. Bate, p. 44.
- The Volf Resonator and Modulator, p. 351.
- Wattless Retroaction [and its Application to Electro-mechanical Systems such as Tuning Forks and Various Resonators].—Braude, pp. 337-338.

- A Circuit whose **Retroaction** is Independent of Frequency.—Brillouin and Lévy, p. 338.
- Reverberation Measurements** with a Completely Automatic Apparatus.—M. J. O. Strutt, p. 529.
- The Acoustics of Famous European Concert Halls, and the Optimum **Reverberation Time** for Rooms of Various Size and for Various Types of Music.—V. O. Knudsen, p. 40.
- A Simple Time-Integrating Device [especially for **Reverberation Time** Measurement].—A. G. Granston Richards, p. 40.
- Reverberation Time** Measurements in Coupled Rooms.—C. F. Eyring, p. 229.
- A Bridge Arrangement for Measuring **Reverberation Times** with Pure Notes.—H. E. Hollmann and Th. Schultes, p. 40.
- Reverberation Times**.—See also Echo.
- A "Whisper" Microphone of Rochelle Salt.—Möller: Heinrich Hertz Association, p. 289.
- Piezoelectric Loud-speakers and Microphones [Rochelle Salt: the Development of the Bimorph Principle].—A. L. Williams, p. 464.
- Piezoelectric Properties of Rochelle Salt Crystals.—Schulwas-Sorokin, p. 467.
- On a Characteristic Temperature Point in Rochelle Salt Crystals.—Schulwas-Sorokin, p. 595.
- The Use of Rochelle Salt Crystals for Electrical Reproducers and Microphones.—C. B. Sawyer, p. 101.
- The Electrical Properties of Rochelle Salt Mixed Crystals.—B. Kurtzschaw and M. Ermejew, p. 589.
- Sound Films and Television in Russia.—G. E. Roth, p. 646.
- The Transmission of Sound Through Sea Water.—H. G. Dorsey, p. 466.
- The Use of Copper Oxide Rectifying Elements for Protecting Operators from Acoustic Shocks.—Collet, p. 530.
- The Action of Oscillating Piezoelectric Quartz on Solutions and Suspensions of Colloids.—N. Marinesco, p. 467.
- Sound Film** Engineering in 1931: a Retrospect.—P. Hatschek, p. 465.
- Physical Properties and Construction of [Alkali] Photoelectric Cells for **Sound-Film** Purposes.—W. Kluge, p. 171.
- Papers on AEG **Sound-Film** Work.—Hehlgans and Lichte: AEG, p. 288.
- A New Method of Blocking Out Splices in **Sound Film**: The Surface Treatment of **Sound Film**: Photographic Characteristics of **Sound Recording Film**: The Measurement of Density in Variable Density **Sound Film**: Apparatus for the Analysis of Photographic **Sound Records**.—Crabtree, Ives, Sandvik, Jones, Tuttle, McFarlane, p. 412.
- Rhythmography—a New **Sound-Film** Production Process [rendering into Speech].—H. Dilje: Blum, p. 646.
- Controllable Light Sources for **Sound-on-Film** Recording.—F. Skaupy, p. 589.
- The Present Position of Photographic Technique in **Sound-on-Film** Recording.—J. Eggert, p. 171.
- Light Sources for **Sound-on-Film** Recording [and in particular the "Lichtspritze" Lamp].—H. Ewest, p. 171.
- Researches on the Figure of Merit of Recording in **Sound-on-Film** Records [including an Objective Method of Testing It]: The Measurement of Sensitivity in **Sound-on-Film** Recording.—A. Küster and R. Schmidt, p. 170.
- Investigations on Non-linear Distortion in **Sound-on-Film** Systems on the Intensity Principle.—A. Narath, p. 288.
- The Distribution of Light in the Recording Slit in the Black-and-White [Amplitude: **Sound-on-Film**] Process [including a Description of the Röntsch—Siemens and Halske—Optical System].—H. J. Eilers, p. 171.
- The Reproduction of **Sound-on-Film** Records [particularly the "Stellor" Reproducing Equipment].—P. Toulon, p. 352.
- The Types of Distortion in **Sound-on-Film** Records.—F. Fischer, p. 288.
- Optical System for **Sound-on-Film** Reproduction, comprising a Straight-Filament Lamp, a Cylindrical Objective, and an Ordinary Objective, p. 230.
- Studio Practice in "Noiseless" [**Sound-on-Film**] Recording.—G. Lewin, p. 43.
- The Connection between Gradation and Frequency Characteristic in **Sound-on-Film** Recording by the Intensity Process.—R. Schmidt, p. 43.
- The Recording of **Sound Films** in the Tobis and Kerr-Karolus (Klangfilm) Systems, p. 170.
- The Development of the Loud Speaker for **Sound Films**.—H. Warncke, p. 646.
- The Technique of **Sound Films**.—H. Kotte, p. 529.
- [The Intimate Connection between] **Sound Films** and Television.—R. Thun, p. 465.
- Sound Films**, Motion Pictures.—See also Recording, Reproduction, Talking, Vertical Cut, Vowels, and below.
- Physical Factors Affecting the Illusion in **Sound Motion Pictures**.—J. P. Maxfield, p. 170.
- Some Acoustical Problems of **Sound Picture** Engineering.—W. A. MacNair, p. 40.
- Supply and Cost of 16-mm. Film for the Home [for **Sound-Picture** Equipment].—F. S. Irby, p. 43.
- Acoustic Power Levels in **Sound Picture** Reproduction.—S. K. Wolf and W. J. Sette, p. 43.
- New Talkie Film [Sound] Printer.—Bell and Howell Company, p. 529.
- Sound Printer** compensating automatically for Shrinkage of Negative.—J. S. Watson and R. V. Wood, p. 101.
- Noisy Audience Limits **Sound-Proofing** of Theatre.—S. K. Wolf and J. E. Tweeddale, p. 465.
- Soundproof Partitions**.—Notes from the U.S. Bureau of Standards, p. 171.
- Soundproof Partitions** [of Cinder Block and Clay Tile], p. 413.
- Sound Rays** as Extremals.—Bateman, p. 455.
- Sound Waves**, Effects on Liquids, etc.—See Biological, Heating, Echo Sounding; The Advisability of Using Continuous Recording.—P. Marti, p. 101.
- Echo Sounding**: British Admiralty Gear, Type 752: Submarine Signal Corp. Universal Fathometer, Type 432, p. 101.
- Sonic Sounding** by the Fessenden System "Fathometer," p. 44.
- Echo Sounding** for Aircraft and Ships: A Direct-Reading Chronograph for the Exact Measurement of Short Time Intervals.—Dubois and Laboureur, p. 414.
- Sounding** the Ocean Depths, p. 290.
- Reflection [**Sounding**] Methods of Measuring the Depth of the Sea.—J. A. Slee, p. 290.
- Portable **Speech-Input Equipment**.—E. G. Fracker, p. 101.
- Sterilisation of Milk** by High-Pitched Sound Waves.—N. Gaines and L. A. Chambers, p. 172: see also Biological.
- The Acoustical Problems of Broadcasting Studios.—N. Ashbridge, p. 40.
- The Design and Acoustics of Broadcast Studios.—S. J. Ebert, p. 288.
- Planning the NBC Studios for Radio City.—O. B. Hanson, p. 647.
- New Optical Properties of Liquids submitted to Supersonic Waves. R. Lucas and P. Biquard, p. 530.
- Action of **Supersonic Waves** on Isolated Cells in Suspension.—E. and H. Biancani and A. Dognon, p. 530.
- Supersonic**.—See also Ultrasonic, Biological and Sterilisation.
- Supersonic Satellites** and Velocity.—W. H. Pielemeier, p. 100.
- Contributions to a Methodical Valuation of **Talking Machines** and **Sound Records**.—L. Hajek, p. 43.
- Development and Use of **Talking Motion Pictures** [General Description].—H. M. Wilcox, p. 646.
- An Analytical Theory of the Telephone [and Allied Electromagnetic Instruments] and Its Significance for Experiment.—H. Hecht, p. 42.
- The Subscriber Output Amplifier: Part I.—Considerations on the Fundamental Design Calculations of Telephone Sets with Loud Speaker Equipment.—R. Winzheimer and H. Reppisch, pp. 465 and 590.
- A Working Calibration Standard for Telephones [the Setem].—C. A. Hartmann and E. Döring, p. 44.
- A Terminology for Acoustics: A Suggestion for a Proper System analogous to that of Optics.—J. B. Pomey, p. 413.
- On the Influence on the Audition Threshold of Distortion of the Sound Field caused by the Head and Auditory Passages.—G. von Békésy, p. 647.
- Investigations on Acoustic Threshold Values. I. On the Measurement of the Threshold of Sensation of Hearing with Resonance Telephones.—E. Waeitzmann and H. Heisig, pp. 42 and 99.
- The Time Factor in Telephone Transmission.—O. B. Blackwell, p. 290.
- Amplifier **Tone Control** Circuits [Suggestion of Simplified Mathematical Treatment].—R. H. Nisbet: Scroggie, p. 351.
- The **Tone Control** Adjustment, a New Component for Better Broadcast Reproduction.—E. Schwandt: Rhein, p. 590.
- Amplifier **Tone-Control** Circuits.—M. G. Scroggie, p. 230.
- Tone Correction** and Distortion.—McLachlan, p. 460.
- "**Tone Equalisers**" in Broadcast Receivers, p. 351.
- Interspaced [Audio-frequency] Transformer Windings [and the Production of Flat Response Curves without the use of Special Core Material or Change of Mass of Core or Copper].—W. J. Leidy, p. 172.
- On the Dependence of the Equivalent Iron Loss Resistance of a [Telephone] Transformer on the Current.—G. A. Tschaijanov, p. 466.
- The Significance of **Transient** Processes in Acoustics.—H. Backhaus, p. 289.
- The **Transient** Current in a Rejector Circuit [and Application of Results to Telephonic Filters].—Pomey, p. 457.
- The Recording of **Transients** by the C.-R. Oscillograph.—Hollmann, p. 170.
- Transients** and Telephony.—T. S. E. Thomas, pp. 42 and 230.
- A Balance Method of Measuring **Sound Transmission**.—A. E. Knowler, p. 40.
- Transmission** of Sound through Partitions [Measurements at the National Physical Laboratory].—A. H. Davis, p. 229.
- Two Speakers from One Set**, p. 645.
- On the Application of Hot Wires to Measurements in the Ultrasonic Region—Preliminary Communication.—H. Müller and T. Kraeft, p. 467.
- Ultrasonic Absorption in Gases**.—J. C. Hubbard, p. 647.
- Ultrasonics**: Some Properties of Inaudible Sound.—F. L. Hopwood, p. 100.

- Pick-Up Amplifier Valve with Photo-sensitive Cathode and External Electrostatic Control Electrode, p. 647.
- Sound Velocity in Reactive Mixtures of Real Gases.—D. G. C. Luck, p. 466.
- Velocity of Propagation of Ultra-Acoustic Oscillations in Cylindrical Rods.—K. Röhrich, p. 466.
- A Direct Method of measuring the Velocity of Sound in Paper.—D. A. Oliver, p. 645.
- A New Method for Measuring the Velocity of Sound in Various Materials [depending on Stereo-acoustic Observations].—G. Veenekamp and H. Schmidt, p. 229.
- Asymmetry of Sound Velocity in Stratified Geologic Formations.—B. McCollum and F. A. Snell, p. 466.
- Velocity of Sound in Tubes at Audible and Ultrasonic Frequencies.—C. B. Vance, p. 290.
- Velocity of Sound in Cylindrical Rods.—G. S. Field, p. 229.
- Velocity of Longitudinal Vibration in Solid Rods (Ultrasonic Method) with Special Reference to the Elasticity of Ice.—R. W. Boyle and D. O. Sproule, p. 229.
- Advantages of Vertical Cut Sound Records.—H. A. Frederick, p. 101.
- Some Observations on Vibrating Tubes [and Their Use in Detecting and Measuring High Audio-Frequencies].—H. Kröncke, p. 414.
- The Natural History of the Vibrato.—C. E. Seashore, p. 172.
- The Vibrometer.—H. Subra, p. 351.
- A Voice and Ear for Telephone Measurements.—A. H. Inglis, C. H. G. Gray and R. T. Jenkins, p. 413.
- Voice Training on a Scientific Basis.—D. Stanley, p. 44.
- Voices Beautified for Radio by Ingenious Mechanisms.—O. H. Caldwell, p. 590.
- Vowel Characteristics.—A. Stefanini, p. 172.
- The Nature of the Vowels [Investigation by Sound-on-Film Technique].—E. W. Scripture, p. 590.
- The Physical Nature of Japanese Vowels.—M. Takahashi and G. Yamamoto, p. 647.
- ### PHOTO TELEGRAPHY AND TELEVISION.
- An Attempt to Detect High Photoelectric Absorption in Caesium Vapour at Double the Series Limit.—E. T. S. Appleyard, p. 291.
- Photoelectric Absorption in Hydrogen-Like Atoms.—P. A. M. Dirac and J. W. Harding, p. 470.
- Secondary Phenomena Following the Primary Photoelectric Effect in Caesium Atoms Adsorbed by Salt Layers.—J. H. de Boer and M. C. Teves, p. 355.
- The Displacement towards the Red of the Photoelectric Ionisation of Alkali Atoms by Adsorption at Negatively Charged Salt Surfaces.—J. H. de Boer and M. C. Teves, p. 291.
- On the Retrogression Effect in Alkali Cells.—A. E. H. Meyer, p. 46.
- Spectral Photoelectric Sensitivity of Thin Alkali Metal Films at Room Temperature and at the Temperature of Liquid Air.—R. Suhrmann and H. Theissing, p. 354.
- Electron Diffraction and Photoelectric Effect at Alkali Metal Surfaces. Part I. Method of Investigation.—W. Kluge and E. Rupp, p. 649.
- Photoelectric Properties of Thin Films of Alkali Metals [in conjunction with Silver].—S. Asao, p. 292.
- New Method for the Study of the Photoelectric Effect of Alkali Vapours.—J. Kunz, p. 470.
- An Amplifier (Loftin-White Circuit) for use with Photoelectric Cells.—Bressi, p. 470.
- Papers on the Resistance-Coupled Amplifier and its Behaviour to Transients.—Schlesinger, p. 47.
- Resistance-Capacitance Coupled Amplifier in Television.—H. M. Lane, p. 415.
- A Resistance-Coupled Amplifier for Television [and the Tracing and Compensation of Losses at the Higher Frequencies].—C. Bradner Brown, p. 647.
- A New Industrial Amplifier Tube for Phototube Circuits [Westinghouse RJ-550].—Sutherland, p. 409.
- Automatic Mean Amplitude Control in L.F. Amplifiers.—G. Krawinkel and E. Perchermeier, pp. 47 and 470.
- The Input Circuit of Photoelectric Current Amplifiers.—H. Lux, p. 47.
- Attenuating Layer.—See Barrier Layer.
- On the Effect of Polarised Light on Barrier Layer Photoelectric Cells.—L. Bergmann, p. 291.
- Barrier-Layer Photoelectric Cells [Siemens and Halske Copper Oxide Cell and Its Use in Photometry].—A. Dresler, p. 414.
- On the Barrier-Layer Photoelectric Effect.—E. Duhme, p. 290.
- The Barrier Layer in Lead Sulphide.—F. Heineck, p. 469.
- A Physical Model of Barrier Layer Photoelectric Cells.—F. v. Kőrösy and P. Selenyi, p. 231.
- Photoelectric Cell and Light Element [Barrier Layer Photoelectric Cell].—F. v. Kőrösy and P. Selenyi, p. 469.
- Report on the Conference on "Barrier-Layer Photoelectric Cells and Rectifiers."—I. Kurtschatow, p. 649.
- Investigation of the Barrier-Layer Photocell.—I. Kurtschatow and C. D. Sinelnikow, p. 649.
- The Variation with Temperature of the Barrier-Layer Photoelectric Effect.—B. Lange, p. 232.
- The Becquerel Effect as a Special Case of the Barrier-Layer Photoelectric Cell.—R. H. Müller and A. Spector, p. 649.
- New Results with Barrier-Layer Photoelectric Cells.—E. Perucca, p. 232.
- Is the Barrier-Layer Photoelectric Effect a Hallwachs Effect?—E. Perucca and R. Deaglio, p. 232.
- Magnetic Control of the Photoelectric Current in Barrier-Layer Cells.—E. Rupp, p. 354.
- On Variation of Resistance of Barrier-Layer Photoelectric Cells and Crystal Cells, due to Magnetic Fields.—E. Rupp, p. 531.
- Conductivity and Photoelectric Effects at Barrier Layers.—W. Schottky, p. 232.
- The Constancy of Action of the Commercial Barrier-Layer Photoelectric Cell.—Schwarz, p. 469.
- The Becquerel Effect in Copper Oxide as a Barrier-Layer Photoelectric Effect.—F. Waibel, p. 532.
- Some New Observations on the Barrier-Layer Photoelectric Effect.—F. Waibel and W. Schottky, p. 649.
- The Electrostriction of Benzene.—M. Pauthenier and P. Delahaye, p. 414.
- A Mechanically Controlled Bolometer and Its Use as a Highly Sensitive Quantitative Relay and as a Quantitative D.C. Amplifier [applicable to Photocell Currents].—H. Sell, pp. 415 and 535.
- The Electrical Behaviour of Boundary Layers.—H. Teichmann, p. 468.
- On the Photoelectric Properties of Cadmium, and in Particular the Influence of Gases thereon.—H. Bonke, p. 102.
- Power Input and Dissipation in the Positive Column of a Caesium Discharge.—F. L. Mohler, p. 591.
- Ionisation of Caesium Vapor by Light.—F. W. Cooke, p. 103.
- Spot Brightness Control in Cathode-Ray Tubes, with Special Reference to a New Method [Combination of Electrostatic Deflection on and off Anode Aperture, Deflection Compensation by a Second Deflecting Plate, and Post-Concentration by Cylinder].—M. von Ardenne, p. 468.
- Investigations on Gas-Filled Cathode-Ray Tubes.—von Ardenne, p. 648.
- Increasing the Brightness of Cathode-Ray Television by Using the Ray as a Mobile Conductor making Contact with Different Conducting Points, p. 531.
- Long Distance Television Tests with the Cathode-Ray Receiver [London and Berlin to Dresden: Comparison of Cathode-Ray and Nipkow Disc Receivers].—E. Busse, p. 353.
- A New Cathode-Ray Tube with Small Ray Velocity.—Dobke: AEG, p. 648.
- A New Sweep-Circuit Device for the Cathode-Ray Oscillograph.—Field, p. 648.
- Particulars of American Cathode-Ray Television Systems [Zworykin "Kinescope" and Farnsworth "Oscillite" Systems.]—H. Hewel: Zworykin, Farnsworth, p. 45.
- Spot Brightness Control in Cathode-Ray Tubes [and the German P.O. Methods].—E. Hudec, p. 531.
- The Cathode-Ray Television Apparatus of the German Post Office.—E. Hudec and E. Perchermeier, p. 45.
- The German Post Office Cathode-Ray Television System.—E. H. Traub: Hudec and Perchermeier, p. 231.
- The Cathode-Ray Tube for Television.—E. Hudec and E. Perchermeier, p. 468.
- The Distortions in the Cathode-Ray Oscillograph at High Measuring Velocities.—Klemperer and Wolf, p. 596.
- The Limits of Performance in Cathode-Ray Television.—H. Peters, p. 45.
- On the Suitability of Various Cathode-Ray Oscillograph Tubes for Television Transmissions [particularly a Comparison between Magnetic and Gas Concentration].—H. Peters, p. 531.
- Improvements in Cathode-Ray Tube Design ["Kinescope."].—Zworykin, p. 106.
- The Structure Analysis of Photoelectric Cathodes by Means of Electron Interference.—W. Kluge and E. Rupp, p. 232.
- Photoelectric Coagulation of Sodium in Rock Salt.—E. Rexer, p. 291.
- Photoelectric and Thermionic Emission from Cobalt.—A. B. Cardwell, p. 234.
- The Applicability of Photoelectric Cells to Colorimetry.—H. E. Ives and E. F. Kingsbury, p. 46.
- Transmission of Colour Pictures, p. 648.
- Experimental Investigations of the Current Conduction in Dielectric Fluids at High Fields.—Nikuradse, p. 479.
- Conductivity of Dielectric Fluids [Summarising Report].—A. Nikuradse, p. 650.
- The Electrical Conductivity of Acetone [and Nitrobenzene] for Direct Current.—Garrigue, p. 103.
- The Role played by the Nature of the Electrodes in the Conductivity of Semi-Conducting Liquids [Nitrobenzene].—J. Sambussy, p. 471.
- Contact Potential Differences between Iron and Nickel and their Photoelectric Work Functions.—G. N. Glasoe, p. 102.
- On the Electric and Photoelectric Properties of Contacts between a Metal and a Semiconductor.—J. Frenkel and A. Joffé, p. 290.
- The Sensitivity of Copper Oxide Photoelectric Cells with Copper Grids: Comparison with the Optical Absorption and Photoconductivity of Copper Oxide.—L. Dubar: Auger and Lapique, p. 46.
- Structural Investigation of the Copper Oxide Rectifier: Contribu-

- tion to the Crystal and Attenuating Layer Photoelectric Effect.—K. Scharf and O. Weinbaum, p. 469.
- On the Composition of the Oxide in Copper Oxide Rectifiers and Photoelectric Cells.—Dubar, p. 419.
- On the Photoelectric Effect in the Cuprous Oxide-Copper Rectifier.—E. Perucca and R. Deaglio: von Auwers and Kerschbaum, p. 103.
- Copper Oxide Photocells.—See also Rectifiers.
- A Crystal Photoelectric Cell [using Cuprite, Proustite and other Crystals].—H. Dember, p. 232.
- On the Theory of the Crystal Photoelectric Effect.—H. T. Wolff, p. 650.
- The Current/Voltage Relation in the Photoelectric Conductivity in Crystals.—W. Flechsig, p. 232.
- On the Dependence of the Maximum Velocities and Work Function of Photo-Electrons at Fractured Surfaces of Single Zinc Crystals on the Direction of the Surface.—A. Nitzsche, p. 650.
- On the Mechanism of the Primary Photoelectric Current in Insulating Crystals.—K. Hecht, p. 649.
- [Certain Rare Types of] Diamonds Yield Electricity when Bathed with Light, p. 649.
- The Effect of the Diffused Light on Photoelectric Measurements.—T. D. Gheorghiu, p. 470.
- A Stroboscopic Method of Measuring Electrical Double Refraction.—R. Lucas and M. Schwob, p. 471.
- The C.C.I.T. Standard and Alternative Drums.—Ritter, p. 467.
- The [Electrolytic] Distribution of Silver and Sodium between Glass and Nitrate- or Bromide-Enamels in the State of Equilibrium.—A. Güntherschulze and O. Mohr, p. 592.
- Electrons and Light Quanta.—Fleming, p. 478.
- Telecinema Transmitters and Receivers for a Large Number of Picture Elements.—G. Schubert, p. 45.
- Number of Elements and Element Frequency [and the Use of Screens with Persistence of Glow].—G. G. Reissaus, p. 45.
- The Inertia of the Eye.—G. G. Reissaus, p. 533.
- Note on Facsimile Transmission from the Air to Earth and vice versa.—U. Guerra, p. 230.
- Photographic-Type Facsimile System for Tactical Work in connection with National Defence.—L. R. Philpott, p. 648.
- Measurement of Fidelity in Television Systems.—A. F. Murray, p. 46.
- A Method of Measuring the Integrated Light from Short Flashes of High Intensity [Photoelectric Tube Charging a Condenser in Grid Circuit of Thyatron].—L. R. Koller, p. 103.
- The Measurement of Fluorescence by means of the Photoelectric Cell.—R. Toussaint, p. 103.
- The Frequencies in Television Signals [The Failure of the "Dot" Theory, etc.].—E. G. Bowen, p. 416.
- A Further Study of Galvanoluminescence [Development of Light at Aluminium and other Anodes at Passage of Current through the Electrolyte].—R. R. Sullivan and R. T. Dufford, p. 174.
- Field and Ion Concentration near the Cathode of a Glow Discharge Tube.—W. de Groot, p. 103.
- Glow Discharge Tubes and Their Technical Applications.—F. Michelssen, p. 293.
- Glow Discharge Lamps for the Generation of "Kipp" Oscillations.—von Hartel, p. 536.
- Measurements [of Infra-Red Radiation] with the Photoelectric Relay.—Barnes and Matossi, p. 474.
- On Conducting and Photo Electrons in Insulators and Semi-Conductors.—B. Gudden, p. 173.
- High Voltage Kerr Cell.—H. M. Dowsett, p. 353.
- Contributions to the Physics of the Nitrobenzol Kerr Cell.—F. Hehlgers, pp. 47, 103 and 471.
- Investigation of the Distribution of Strong Alternating Electric Fields in the Nitrobenzene Kerr Cell.—F. Hehlgers, p. 234.
- Resonance Effects in Kerr Cells using Bipolar Substances in Nitrobenzene.—C. E. G. Bailey, p. 353.
- Some Principles governing the Design of Kerr Cells.—W. D. Wright, p. 414.
- The Kerr Constant of Nitrobenzol.—R. Möller, p. 47.
- The Electro-Optical Kerr Constant of Liquid and Dissolved Substances, and the Nature and Cause of the Mutual Influence and Orientation of the Molecules in the Liquid State.—G. Briegleb, p. 292.
- Phenomena accompanying the Electro-Optical Kerr Effect in a High-Frequency Field.—H. Hoyer and L. Pungs, p. 591.
- The Validity of Kerr's Law for Nitrobenzene under Strong A.C. Electric Fields.—F. Hehlgers, p. 234: see also Conduction, Conductivity, Liquid, Nitrobenzene.
- New Development of the Gaseous Discharge Lamp for Television.—H. Ewest, p. 292.
- The Development of the Sodium Vapour Lamp for Television.—G. Schubert, p. 292.
- A New Crater-Tube [Lamp] Development, p. 414.
- The U-shaped Osram Sodium Vapour Lamp, p. 591.
- Sources of Light for Television [Modern Flat Plate and Crater Lamps].—A. E. Lyle, p. 591.
- On the Forward Motion of Electrons under the Action of Light.—H. Dember, p. 291.
- Television on a Light Beam.—E. F. W. Alexanderson: G. E. C., p. 352.
- Sensitive Light Control by Mirror Membrane.—C. Müller: Mey, p. 354.
- A New Light Control Device by C. Müller [Thin Reflecting Metal Membrane].—S. Wagerer: Müller and Mey, p. 533.
- Simplicity Extends Light Control Possibilities [Burgess Radiovisor Bridge], p. 47.
- On Momentary Frequency Analysis of Light Fluctuations using Rotating Discs.—T. von Nemes, p. 533.
- New Sodium Light Source of High Luminous Intensity.—M. Reger, p. 354.
- The "Positive Column" Light Source.—Fernseh A.G., p. 231.
- The "Lichtspritze" (Light-Spray) Lamp with Oxide-Coated Filament, and other Light Sources.—Ewest, p. 174.
- Controllable Light Sources for Sound-on-Film Recording.—Skaupy, p. 589.
- [Highway] Lighting in Holland.—Philips' Company, p. 650.
- Cyclical Line-Shift Process.—Hudec. See Physiology.
- The Breakdown of the Liquid Dielectric [Influence of Pressure, Temperature, Purity, Frequency, Electrode Form, etc.: the Various Hypotheses].—A. Nikuradse, p. 650.
- The Behaviour of Absorbed Air in the Breakdown of Liquid Dielectrics.—F. Koppelmann, p. 47.
- Variation of the Magnetic Susceptibility of Paramagnetic Ions under the Influence of Light.—O. Specchia, p. 174.
- Papers on the Magneto-Optical Effect of Thin Iron Films.—Cau: Pogány, pp. 471 (two) and 533.
- The Construction and Operation of Capillary Mercury Arcs [free from Decrease of Intensity and Deterioration of Quartz].—R. H. Crist, p. 47.
- Number of Elements, Image Dimensions and Brightness with the Mirror Helix.—F. von Okolicsanyi, p. 45.
- New Types of Mirror Wheel for Television Reception.—R. Schadow, p. 231.
- Model for Demonstrating Television and for Testing Characteristics of Amplifiers, etc.: Model for Illustrating the Fundamental Principles of Television.—R. Wilson and A. A. Waters: R. W. Corkling, p. 468.
- Series Modulation for Television Transmitters.—C. Bradner Brown, p. 648.
- A New Method of Measuring the After-Glow of Discharges in Gas [and the Limitations of the Neon Lamp in Television].—L. Rohde and K. Schnetzler, p. 591.
- Neon Tube with Metallic Coating on Wall as Positive Electrode, p. 47.
- "News" by Television: A Marconi Development.—H. M. Dowsett, p. 530.
- The Optical Properties of Nitrobenzene in Thin Layers submitted to an Electrostatic Potential.—A. Cotton and H. Mouton, p. 354: see also Kerr.
- The Mirror Oscillograph in Television.—K. O. Kiepenheuer, p. 47.
- Photoelectric and Thermionic Properties of Palladium.—L. A. Du Bridge and W. W. Roehr, p. 234.
- The Photoelectric and Thermionic Properties of Palladium.—W. W. Roehr and L. A. Du Bridge, p. 470.
- On the Thermo-Electric Forces of Palladium Iron and Palladium-Silver Alloys with Adsorbed Hydrogen.—R. Nübel, p. 47.
- Photo- and Thermo-Electric Effect in Palladium-Silver and Palladium-Gold Alloys with Adsorbed Hydrogen.—F. Schniederermann, p. 532.
- New High-Efficiency PhotoCell.—Lorenz Company, p. 292.
- A Vacuum Photo-Cell Type of [Television] Transmitter.—C. E. C. Roberts, p. 231.
- Photo Cells: the Valves Which Operate by Light.—C. C. Paterson, p. 354.
- Thermionic Emission in Caesium-Oxide Photocells at Room Temperatures.—Kingsbury, p. 228.
- Some Experiments with Gas-filled Cs-O-Ag Photo Cells.—K. H. Kingdon and H. E. Thomson, p. 291.
- Photocells and Their Applications in Optical Technique [Survey and Bibliography of Recent Work].—H. Singer, p. 532.
- Lag in Gas-Filled Photocells.—F. Ollendorf, p. 592.
- Manufacture of Caesium Silver-Oxide Photocells.—W. H. Nickless, p. 648.
- Time-Lag in Photo-Cells and the Townsend Discharge.—N. R. Campbell, p. 648.
- The Fournier-Céma Photoelectric Cell, p. 354.
- Silver-Selenium (on Iron-Nickel Alloy) Photoelectric Cell.—Western Elec. Instrument Company, p. 554.
- A Photoelectric Cell Circuit [Special Modification of Hull Circuit for Wide Linear Response: Mathematical Analysis].—G. A. Wootton and R. G. Elson, p. 592.
- The Caesium-Oxygen-Silver Photoelectric Cell. An Investigation of the Relations in a Composite Photoelectric Surface.—C. H. Prescott, Jr., and M. J. Kelly, pp. 592 and 648.
- The "Patina" Photoelectric Cell.—F. Noack: Lorenz Company, p. 470.
- Constancy of Emission of Gas-Filled Photoelectric Cells after a Momentary Glow Discharge.—W. R. G. Atkins, p. 173.
- The Construction of Photoelectric Cells with Large Cathode Surfaces.—R. Fleischer, p. 292.
- Experiments on the Behaviour of [Gas-filled] Photoelectric Cells with Varying Frequency of Illumination.—P. Fourmarier, p. 46.

- A Study of Sluggish Response in Gas-Filled Photoelectric Cells.—P. Fourmarier, p. 233.
- The Response of a Gas-Filled Photoelectric Cell to a Sudden Illumination.—P. Fourmarier, p. 648.
- The Application of Photoelectric Cells Sensitive in the Infra-Red to Stellar Photometry [and the Reduction of the "Dark Current" in Caesium-Oxide-on-Silver Photocells].—J. S. Hall, p. 592.
- Characteristic Constants of Photoelectric Cells.—S. N. Kakurin, p. 354.
- Photoelectric Cells for Sound-Film Work.—Kluge, p. 173.
- Modern Alkali Photoelectric Cells.—W. Kluge: AEG, p. 470.
- Some New Facts observable with Ordinary Photoelectric Cells.—Q. Majorana, p. 355.
- The Glow in Photoelectric Cells.—Rayleigh, p. 648.
- Further Progress in Photoelectric Cells.—H. Kröncke: Sewig, p. 292.
- Photoelectric Cells with Cathodes of Thin Layers of Alkali Metals.—R. Sewig, p. 469.
- Sensitized Potassium Photoelectric Cells [and Their Selective Emission].—R. Suhrmann, p. 173.
- Photoelectric Cells and Their Use.—H. Simon and R. Suhrmann, p. 470.
- Vacuum Photoelectric Cells of High Sensitivity.—M. C. Teves, p. 172.
- Investigations on the Lower Limit of Sensitivity of Commercial Potassium Photoelectric Cells and their Suitability for the Photoelectric Measurement of a [Ray]-Preparations.—G. A. Teves, p. 649.
- Current Increase in Photoelectric Cells due to Gas Discharge.—P. W. Timofeev and N. S. Chlebnikow, p. 233.
- Gas-filled Photoelectric Cells.—P. W. Timofeev and N. S. Chlebnikow, p. 592.
- Photoelectric Cells with Silver/Silver Bromide Electrodes in Potassium Bromide Solution.—B. Vanselow and S. E. Sheppard, p. 292.
- Photoelectric Cells.—See also Alkali, Barrier, Boundary, Cathodes, Copper Oxide, Crystal, Lag, Photocells, Photo-sensitive, Selenium, Silver, Ultra-Violet, Weston.
- Photoelectric Currents in Gases between Parallel Plates as a Function of the Potential Difference.—N. E. Bradbury, p. 532.
- On a New Photoelectric Effect.—L. Bergmann, p. 232.
- Contribution to the Knowledge of the Crystal and Attenuating Layer Photoelectric Effect.—W. Bulian and H. Schreiber, p. 592.
- Internal and External Photoelectric Effect [from γ -rays].—H. Casimir, p. 103.
- The Selective Photoelectric Effect and Absorption of Light.—R. Fleischmann, p. 47.
- Absorption of Light and the Selective Photoelectric Effect.—H. Fröhlich, p. 470.
- The External Photoelectric Effect in Liquids. Determination of the Long-Wave Limit in Water.—P. Görlich, p. 533.
- On the External Photoelectric Effect with Phosphorescent Materials [Alkaline Earth Sulphides] and its Mode of Dependence on the Excitation Condition.—H. Göthel, p. 47.
- The Photoelectric Effect for γ -Rays [Theoretical Investigation].—H. R. Hulme, p. 103.
- The Vectorial Photoelectric Effect in Thin Films of Alkali Metals.—H. E. Ives, p. 102.
- The Photoelectric Effect from Thin Films of Alkali Metal on Silver.—H. E. Ives and H. B. Briggs, p. 102.
- The Distribution of Electrons in the Photo-Effect by Röntgen Rays, Classically Treated [Theoretical Investigation].—J. Kunz, p. 649.
- Correlating the Selective Photoelectric Effect with the Selective Transmission of Electrons through Crystalline Surface Structures.—A. R. Olpin, p. 233.
- An Interpretation of the Selective Photoelectric Effect from Two-Component Cathodes.—A. R. Olpin: W. H. Zachariasen, p. 233.
- The Photoelectric Effect in Thin Metallic Films [Theoretical Investigation].—W. G. Penney, p. 46.
- On the Influence of Plastic Deformation on the Internal Photoelectric Effect in Rock Salt Crystals.—M. N. Podaschewsky, p. 649.
- On the Atomic Photoelectric Effect for Very Hard Exciting Radiation [Theoretical Investigation].—F. Sauter, p. 103.
- On the Atomic Photoelectric Effect in the K-Ring on Dirac's Relativistic Wave Mechanics.—F. Sauter, p. 234.
- Causes of the Selective Photoelectric Effect.—R. Suhrmann, p. 173.
- New Observations on Field- and Photoelectric-Effects at Outer Border Surfaces ["Mono-Layers"].—R. Suhrmann, p. 233.
- Some Remarks on the Theory of Photoelectric Effect in Metals.—I. Tamm, p. 291.
- Temperature Dependence of Photoelectric Effect in Metals.—L. A. Young and N. H. Frank: Fowler, p. 103.
- Photoelectric Efficiencies in the Extreme Ultraviolet.—F. H. Spedding, p. 233.
- The Physico-chemical Composition of the Metallic Surface in the Selective Photoelectric Electron Emission from the Alkali Metals.—R. Suhrmann, p. 291.
- A Further Experimental Test of Fowler's Theory of Photoelectric Emission.—L. A. Du Bridge, pp. 291 and 470.
- Photoelectric Emission from Cadmium and Mercury.—D. Roller and M. Zenov, p. 470.
- Dependence of the Photoelectric Emission from Potassium on the Arrangement of Atomic Hydrogen and Potassium Films on its Surface.—P. I. Lukirsky and S. Rijnoff, p. 532.
- Photoelectric Emission from Different Metals.—H. C. Rentschler, D. E. Henry and K. O. Smith, p. 649.
- Additional Experimental Verification of Fowler's Photoelectric [Emission] Theory.—G. B. Welch, p. 470.
- Photoelectric Effect and Emission.—See also Photo-thermionic, Selenium, Semi-Conductors, Surface Changes, Surface Electrons.
- A More Rigid Proof of the Photoelectric Law.—N. R. Campbell, p. 416.
- A New Photoelectric Phenomenon [Increase of Resistance of Thin Films of Silver, Gold, Platinum, etc., on Glass, produced by the Action of Light].—Q. Majorana, p. 592.
- The Photoelectric Properties of Films of Beryllium, Aluminium, Magnesium and Thallium.—H. de Laszlo, p. 470.
- Photoelectric Properties of Thin Films of Rubidium and Caesium on Silver.—J. J. Brady, p. 291.
- Some New Photoelectric Researches.—Q. Majorana, pp. 173 (two) and 291.
- Papers on Photoelectric Technique in Various Applications, p. 47.
- Angular Distribution of Photoelectrons.—A. Sommerfeld, p. 173.
- The Resemblance between the Longitudinal Asymmetry of the Classical Field of an Accelerated Electron and the Distribution of Scattered Photoelectrons.—L. Simons, p. 648.
- The Depth of Origin of Photoelectrons.—H. E. Ives and H. B. Briggs, pp. 416 and 532.
- Photoelectrons and Negative Ions.—E. M. Wellish, pp. 102 and 173.
- Photoelectrons and Negative Ions.—J. L. Hamshere, p. 173.
- Photoelectrons and Negative Ions.—V. A. Bailey, p. 234.
- Optimum Outputs of Photo-Sensitive Devices.—E. D. Wilson, p. 173.
- Modern Phototelegraphy [Bartlane System].—R. C. Walker, p. 467.
- Phototelegraphy with Cliché Reception [Guth "Radiotype" System on the "Bremen"].—Guth, p. 531: see also Radiotype.
- On the Photo-Telephony [Successful Use of Incandescent Electric Lamp at Transmitter].—Kujai, p. 540.
- On the Nature of a Photo-thermionic Effect due to Red and Infra-Red Radiation.—I. Ranzì, p. 355.
- Influence of the Electrolytes on Photovoltaic Phenomena.—R. Audubert, p. 174.
- Photovoltaic Properties of Cadmium Sulphide.—R. Audubert and C. Stora, p. 470.
- Some Photovoltaic Properties of Cu: Cu₂O/Pb(NO₃)₂ Solution/Cu: Cu₂O Photocells.—W. E. Meserve, p. 650.
- Discontinuous Variation of the E.M.F. of Photovoltaic Cells with Coloured Liquids.—A. Grumbach and F. Taboury, p. 103.
- On the Law of Equidistance in Photovoltaic Cells.—A. Grumbach and F. Taboury, p. 174.
- The Part Played by Water in Photovoltaic Cells.—R. Audubert, p. 46.
- The Role of Photoconductance Phenomena in the Photovoltaic Effect.—R. Audubert and J. Rouleau, p. 46.
- On the Physiology of Television [and the Cyclical Line-Shift Process].—E. Hudec, p. 172.
- Echo Signals in Transatlantic Picture Telegraphy [and Results in S-N Direction, Cape Town to Somerton].—Dowsett, p. 216.
- Half-Tone Picture Telegraphy on Short Waves [Telefunken "Channel-Change" System].—F. Schröter: Schriever: Ilberg, p. 230.
- The Transmission of Half Tone Pictures by Short Waves.—F. Schröter, p. 290.
- Difficulties encountered in Transmitting Pictures over Telephone Circuits.—E. S. Ritter, p. 467.
- The Transmission of Pictures and Facsimiles.—I. T. and T. Laboratories, p. 44.
- Piezoelectric-Photoelectric Amplifier for Electric Current Variations.—A. Thomas, p. 470.
- Plane Waves of Light: Absorption by Metals.—T. C. Fry, p. 533.
- The Photo-ionisation of Atomic Potassium.—M. Phillips, p. 291.
- Directional Distribution of the Electrons Emitted from the Potassium Atom under the Action of Polarised Ultra-Violet Light.—A. Kraus, p. 649.
- Photo-ionisation Probabilities of Atomic Potassium.—M. Phillips, p. 355.
- The Importance of the Programme for the Success of a Television Transmission.—R. Thun, p. 530.
- On the Way to Projected Television.—F. Kirschstein: Sanabria, p. 467.
- Television Turns to Projection.—A. Dinsdale, p. 44.
- Tables for Planck's Radiation Formula.—W. de Groot, p. 103.
- Printed Page by Radio ["Radiotype" System on the "Bremen"].—Radiotype and Debeg Radio Companies, p. 591: see also Phototelegraphy.
- Photoelectricity and Rectification in Cuprox Rectifiers.—V. Brazzoduro, p. 592.
- Photoelectricity and Rectifiers: Comparison between Cuprox and Selenium Rectifiers.—R. Deaglio, p. 592.
- Reflection of Electrons by a Special Potential Field.—E. L. Hill, p. 173.
- Symmetrical Relaxation Oscillations and Their Synchronisation.—H. E. Holmann: Frühauf, p. 45.

- The Rome Television Transmitter.—R. Möller, p. 531.
 Sound Films and Television in Russia.—G. E. Roth, p. 530.
 The Part Played by Russian Workers in the Development of Electrical Television.—B. L. Rosing, p. 415.
 Peck Scanning System for Television.—W. H. Peck, p. 353.
 Suggested Slow-Speed Survey of Object superimposed on usual Detail Scanning [making use of Continuity of Partial Observation].—G. E. Land, p. 353.
 New Scanning Method [Irregular Strip Sequence].—Toulour, p. 352.
 A Scanning Suggestion [Superimposing an Oppositely Curved Scanned Area, by Two Partial Spirals on same Disc, put into action Alternatively].—G. E. Land, p. 45.
 Design of Lens Scanning Systems for Television.—I. Bloch, p. 591.
 Problems of Brightness in Television Transmitters [Quantitative Treatment, including Comparison of Various Scanning Methods].—R. Möller, p. 468.
 The Lens [Scanning] Disc.—E. Busse, p. 468.
 New Scanning Method [Subdivision into Squares, Corresponding Elements being Scanned in Successive Squares].—Toulour, p. 468.
 Television depending on Brightness Modulation, and on Scanning Speed Modulation.—R. Thun, p. 44.
 The Use of Screens with Persistence of Glow.—See Elements.
 Secondary Emission from Nickel by Impact of Metastable Atoms and Positive Ions of Helium.—M. C. Harrington, p. 102.
 Progress in the Construction of Selenium Photoelectric Cells.—S. German Apparatus Works, p. 354.
 A New Selenium Tube: an Application of Modern Vacuum Technique.—G. F. Metcalf and A. J. King, p. 173.
 Manufacture of Stable Selenium Sulphide, p. 650.
 Catalysis and Photo-Conductors [Effect of Added Substances on the Resistance Variation of Selenium produced by Light].—F. H. Constable and A. F. H. Ward, p. 649.
 Photo-E.M.F. of Selenium.—V. Brazduro, p. 592.
 Measurements on Selenium Barrier Layer Photoelectric Cells.—L. Bergmann, p. 591.
 Selenium.—See also Rectifiers, and under "Subsidiary Apparatus and Materials."
 Papers on Semi-Conductors.—Wilson: Leo, p. 108.
 On a Photoelectric Effect in Semi-Conductors.—L. Bergmann, p. 291.
 Television on Short [70-Metre] Waves.—W. Federmann, p. 45.
 The Shot Effect in Photoelectric Currents.—B. A. Kingsbury, p. 102.
 The Small-Shot Effect in Photoelectric Currents.—B. A. Kingsbury, p. 233.
 Shot Effect and Thermal Noise in the Photocell Amplifier.—F. von Orban, p. 649.
 Thin Films of Alkali Metals [in conjunction with Silver].—S. Asao, p. 292.
 [The Intimate Connection between] Sound Films and Television.—R. Thun, p. 468.
 The Storage of Light in Television Apparatus.—W. Friedel: Jenkins, p. 468.
 Submarine Television.—Hartmann, p. 353.
 Submarine Television [for Exploring the Depths of the Sea], p. 353.
 Television Reception with the Superheterodyne.—R. W. Tanner, p. 44.
 An Advanced Television and Short-Wave Superheterodyne Receiver [avoiding Motor-Boating and other Reaction Troubles by Use of Carborundum Detectors in Both Stages].—R. W. Tanner, p. 591.
 The Effect of Surface Changes on the Photoelectric Emission of Silver and Gold.—T. E. Clarke, p. 292.
 The Surface-Electrons [Application to Photoelectric Effect].—J. E. Nyrop, p. 355.
 Synchronised Mechanically Oscillating System for Television Synchronisation.—R. Barthélemy, p. 531.
 A New Synchronising System for Television.—T. Sone, p. 353.
 The Photoelectric Properties of Tantalum.—Cardwell, p. 234.
 Television Receiver with Brighter Image.—W. H. Peck, p. 353.
 A New Method of Studying and Regulating a Television Transmission.—M. Robert, p. 415.
 Progress in Television: Television Progress from an Engineering Viewpoint.—J. Dunsheath: P. G. Weiller, p. 353.
 The Problem of Television Transmission—Baird, Lyon and Stoyanowsky System.—E. Labin: Baird Company, p. 591.
 Technical Problems in Connection with Television.—C. O. Browne, p. 45.
 New Television System [Variable Scanning Speed].—Von Ardenne: Thun, p. 416.
 The Fundamental Optical Equation for Television Apparatus.—R. Thun, p. 468.
 A Contribution to the Calculation [and Specification] of Television Apparatus.—R. Thun, p. 590.
 The Television System of the Fernseh Company using an Intermediate Film Stage.—G. Schubert, p. 530.
 The Influence of the Nature of the Subject, as regards Contrast, and of the Analysing System, on Television Transmission.—E. Busse, p. 530.
 Television in America.—A. Dinsdale, p. 415.
 Television in U.S.A., p. 103.
 Some Notes on Television in the U.S.A. [with Comparative Data of Jenkins, Westinghouse (KDKA), Bell Telephone Laboratories, and Baird (English) Systems].—J. H. O. Harries, p. 231.
 Television at the 1931 Berlin Radio Exhibition [with Comparative Data of German P.O., Fernseh A.G., Tekade (Telehor) and Loewe (von Ardenne) Systems].—E. H. Traub, p. 231.
 Television at the 1931 Berlin Radio Exhibition.—G. Kette, p. 45.
 Unsuccessful Test of Television between New York and Berlin, p. 45.
 Multi-Channel Television.—C. O. Browne: Gramophone Company, pp. 231 and 353.
 Two-Way Television [in Paris].—Baird Television Corporation, p. 467.
 Inauguration of a "Visiotelophony" [Television] Service [between Galeries Lafayette and the Offices of "Le Matin," Paris].—Lyon and Stoyanowsky: Baird Company, p. 467.
 Television in the U.S.S.R.—P. Shmakov, p. 468.
 90 Years of Television: On the History of Television, p. 531.
 The Present State of Television in England.—E. H. Traub: Haskell, p. 468.
 Recent Advances in Television.—H. J. Barton Chapple, p. 468.
 Television—Seven Years of Research and Investigation.—R. W. Corkling, p. 468.
 The Peck Television System.—W. H. Peck, p. 590.
 New Television Home Receiver with Mirror Wheel, Larger Screen and Special Kerr Cell.—Baird Company, p. 590.
 A New Television System [including an Improved Mirror Drum Scanner throwing Picture directly on to Screen].—R. W. Tanner, p. 321.
 Bibliography on Television [Partial, up to 1931].—p. 648.
 Television Apparatus [at the British Association Meeting].—Marconi Company, p. 648.
 "Reading" by Television [Equipment for Transmitting and Recording Script or Type].—H. J. Barton Chapple, p. 648.
 Recent Developments in Television.—H. J. Barton Chapple, p. 45.
 The Derby by Television.—Baird Television Co., p. 467.
 Television Now on Schedule.—D. E. Replogle: Jenkins Corporation, p. 45.
 An Early [1922] Television and Picture Transmission Proposal.—J. L. McQuarrie and W. W. Cook, p. 45.
 Television Projector with Transparent Scanning Disc using Spark Decomposition of Acid Film.—C. F. Jenkins, p. 353.
 A New Method of Determining Thermionic Work Function by Photoelectric Cell.—R. E. Harris, p. 233.
 The Use of the Turner Kallitron Circuit as a Trip Relay.—Hollmann and Schultes, p. 103.
 A New Dynatron Trip Relay Circuit and Pulse Generator.—Fucks, p. 103.
 The Determination of the Photoelectric Threshold for Tungsten by Fowler's Method.—A. H. Warner, p. 234.
 Ultra-Short Waves and Television.—G. von Arco, p. 103.
 Television Tests [German P.O.] on Ultra-Short Waves.—G. Krauwinkel and K. Ziebig, p. 467.
 Results obtained in the Calibration of Cadmium [Photoelectric] Cells [for Ultra-Violet Light].—F. Levi, p. 648.
 Intensity Measurements in the Ultra-Violet by Photoelectric Cells Sensitised by Sodium Salicylate.—A. Chevallier and P. Dubouloz, p. 233.
 Vision and Sound on One Wave.—Columbia Broadcasting System, p. 591.
 Intensity, Area, and Distance of Visual Stimulus.—E. Freeman, p. 535.
 Discussion, on the Lines of Wave Mechanics, of the Conductivity and Photoelectric Effects.—F. Bloch, p. 234.
 Light Sensitive Cell for Direct Relay Operation [Weston Photronic Cell giving 5 mA in Direct Sunlight].—p. 46.
 Characteristics of the Weston Photronic Cell, p. 470.
 On the Directional Distribution of the Photoelectrons from High Frequency X-Radiation.—E. Lutze, p. 103.
 Lateral Space Distribution of X-Ray Photoelectrons.—P. Kirkpatrick, p. 234.
 The X-Ray Televisor.—F. Levy-Michel, p. 471.
 A New Method of Measuring X-Ray Intensities Employing an Electronic Photocell.—P. R. Gleason, p. 470.
 Spectral Distribution of the Depolarising Current in the Photoelectric Conducting Effect of Rock-Salt under the Action of X-Ray.—N. Kalabuchow and B. Fischelw, p. 649.
 The Compound Photoelectric Effect of X-Rays in Light Elements.—G. L. Locher, p. 471.

MEASUREMENTS AND STANDARDS.

- On Absorption Measurements in Pure Liquids and Electrolyte Solutions in the Region of Short Electric Waves, by a New Method.—J. Malsch, p. 474.
 Valve Ammeter for Small Alternating Currents from 25 to 6×10^8 Cycles/Second.—Messrs. Tinsley: Barlow, p. 416.
 Singing Conditions in Two-Wire Amplifiers, and their Application to a New Amplification Measuring Method.—Weimtschke, p. 105.
 A Valve Voltmeter Method of Harmonic Analysis.—Greenwood, pp. 465-466.
 Attention Measurements on Telephone and Telegraph Lines.—J. W. Horton, p. 236.
 A High Sensitivity Power Factor Bridge [modified Schering Bridge:

- with Analytical Theory].—W. B. Kouwenhoven and A. Banos, Jr., p. 236.
- A **Nernst Bridge Arrangement for the Highest Precision** [Reduction of Input Energy and Amplification of Output].—J. Hadamard, p. 534.
- A **Bridge for Capacitance and Low Power-Factor Measurements**.—H. W. Bousman, p. 535.
- The Sensitivity of Null Instruments in **Bridge Circuits for the Measurement of Alternating Voltages**.—W. Spielhagen, p. 594.
- Some Aspects of the **Valve Bridge** with a Description of a New Compensated Valve-Voltmeter.—A. S. McFarlane, p. 650.
- An A.C. **Wheatstone Bridge for Audio- and Radio-Frequency Measurements**.—A. Hemingway and J. F. McClendon, p. 535.
- Conditions of Equilibrium in the **Wheatstone Bridge for Measurements of Audio- and Radio-Frequency**.—A. Marino: Wagner, p. 175.
- What are the Uses of the "Glow Discharge **Bridge**" and How is It Arranged?—Geffcken and Richter: Huth, p. 651: see also Capacity.
- A **Precision Bridge for Resistance Measurement at Speech Frequencies** [New Method of Avoiding Capacity Effects].—P. Klaudy, p. 651.
- Refinement of the **Bridge Method for Measuring Electrolytic Resistances at High Frequencies**.—W. Geyer, p. 651.
- Two **Precision Condenser Bridges**.—A. Campbell, p. 47.
- Visible Null Indicator for A.C. **Bridges** [Combination of A.C. Microammeter or Galvanometer and Triode].—E. H. W. Banner, p. 594.
- Brownian Motion as the Limit of the Technique of Measurement**.—M. Czerny, p. 651.
- A **Method of Measuring Small Capacitance** [e.g., $5\mu\mu\text{F}$].—R. Barton, p. 357.
- The **Measurement of Capacities by Means of Valves and a Seconds Clock**.—L. Sesta, p. 48.
- Measurement of Small Capacities** [Substitution Equipment for D.C. Mains Operation].—V. V. Sathe and T. S. Rangachari, p. 48.
- A **Method of Comparing Small Capacities** [Oscillating Neon Tube Method].—M. Durepaire, p. 534.
- A **Method for Measuring Small Capacities** [Vibrating Contacts Device, Second Method].—J. A. Van den Akker, p. 472.
- Capacitance and Power Factor of a Mica Capacitor** as measured at the Bureau of Standards and the National Physical Laboratory.—H. L. Curtis, C. M. Sparks, L. Hartshorn and N. F. Astbury, p. 534.
- A **Standard of Small Capacity Differences**.—A. C. Bartlett, p. 48.
- The **Electroscope Capacity Balance** [for Measuring Capacities of a Few Micro-microfarads].—E. S. Brown, p. 357.
- The **Double Beat Method of Frequency Adjustment**: Applications to the Measurement of **Capacity and Inductance**.—F. M. Colebrook, p. 175.
- Oscillating Glow-Discharge Tube Capacity Meter for Small Capacities** [50–11,000 cm, with an Accuracy of 1%].—Geffcken and Richter, p. 175: see also Bridge.
- The **Measurement of the Self-Inductance of Iron-Cored Chokes** [with or without D.C. Polarisation: a Simple Method].—H. Teuchert, p. 357.
- Slow Motion Motor Will Run Indefinitely** [for Clock Frequency Integrator, etc.]. p. 595.
- Gearless Clock** [Synchronous Motor with Four Moving Parts, Slowest revolving Twice per Day, Fastest Once per Second: Vernier Cascade Principle].—L. W. Watts: Chubb, p. 595.
- Synchronisation of the Balance Wheels of Clocks**.—Salmon-Legagneur and Bertrand-Lepaute, p. 595.
- High Frequency Coil Measurements**.—W. D. Oliphant, p. 356.
- Calculation of Reactance Coils with Open Iron Cores**.—Buchholz, p. 477.
- The **Design of Single Layer Coils**.—R. T. Beatty, p. 651.
- A **Method of Measuring the Leakage Resistance of a Condenser—Neon Tube Circuit**.—Decaux and Le Corbeiller, p. 48.
- Absolute Measurement of the High-Frequency Conductivity of Liquids at 3 m Wavelength**.—H. Schaefer, p. 651.
- A **New Method** [Vibrating Condenser] of **Measuring Contact Potential Differences in Metals**.—W. A. Zisman, p. 594.
- Rectifier Circuits for Measurement of Small Alternating Currents** [Ripple in an H.T. Circuit].—J. A. Darbyshire, p. 356.
- Measurements of Small Currents using Photon Tubes**.—L. R. Hafstad, p. 594.
- A **Through** [Ring] **Type Current Transformer and Amplifier for Measuring Alternating Currents of a Few Milliampères**.—W. B. Kouwenhoven, p. 105.
- The **Experimental Determination of the Damping Couple of an Oscillator**.—J. Haag, p. 355.
- A **Delay Recording Equipment using a Steel-Band Telegraphone**, for the Measurement of **Transit Time Effects in Communication Systems**.—H. Decker, p. 175.
- A **New Method of Dielectric Constant Measurement** [Gases] at **Radio Frequencies**.—H. L. Andrews, p. 294.
- The **Dielectric Constant of Water and Its Temperature Coefficient** as determined by a **Resonance Method**.—E. P. Linton and O. Maass, p. 651.
- Measurement of the Dielectric Constants of Salts**.—P. Schupp, p. 474.
- The **Dielectric Constants of a Number of Oxides** [in particular Al_2O_3].—A. Güntherschulze and F. Keller, p. 474.
- Measurement of Dielectric Constants of Liquids by Means of a Crystal-Regulated Resonance Apparatus**.—H. Ulich and W. Nespital, p. 651.
- A **Proposal to Abolish the Absolute Electrical Dimension Systems**.—E. Weber, p. 452.
- The **Direct Measurement by Diodes of the Mean and Maximum Values of an Alternating Quantity**.—Vecchiacchi, p. 235.
- Dipole Moments and Molecular Structure. Part I. A Simple Resonance Method for the Measurement of Dielectric Constants** [of Solutions].—J. W. Smith, p. 652.
- The [Siemens and Halske] **Distortion Meter for Telegraphic Signals**.—A. Jipp and O. Römer, p. 535.
- A **New Apparatus for Measuring the Resistance of Earth Connections**.—J. Gerstbach: Masa, p. 652.
- Earth Resistance Measurement** [Megger and MEG Earth Testers].—Evershed & Vignoles, Ltd, p. 652.
- An **Instrument for Measuring the Resistances of Earths**.—L. Triau: Siemens & Halske, p. 473.
- Principles of a New Portable Electrometer**.—R. Gunn, p. 473.
- A **New Tilted Electrometer** [Quartz Fibre "Leaf" in Hydrogen].—H. Carmichael, p. 474.
- A **New Electrometer** [Small, with "Multi-needle" Moving Element, giving 1 600 Divisions to the Volt with 1 Second Period].—Kerr Grant, p. 293.
- The **Principles of a New Portable Electrometer**.—R. Gunn, p. 651.
- The **Formulae of Three Torsion Electrometers** [Quadrant, Binant and Duant].—G. Nadjakoff, p. 293.
- How Electron-Coupled Oscillators Make Still Better Frequency Meters**: Constructional Details of Two New Models.—R. B. Parmenter: G. D. Meserve, p. 651.
- Field-Strength Measuring Equipments for Broadcasting Wavelengths, and their Calibration**.—R. Thomson, p. 105.
- Marconi Portable Field Strength Measuring Equipment** [14 to 2 000 Metres], p. 593.
- On the Measurement of Electrical Field Strength at the Surface of Conductors**.—H. Jess, p. 594.
- Plotting the Form of an Alternating Voltage by means of Diodes** [a Simple Method for Certain Cases].—F. Vecchiacchi, p. 356.
- New Method of Determining the Ratio of the R.M.S. to the Mean Value of an Alternating Voltage** [Form Factor].—F. Vecchiacchi, p. 356.
- Report of the Work and Researches of the French National Laboratory of Radio-electricity during 1931**.—C. Gutton, p. 474.
- An **Objective Method of Calibrating** [High] **Alternating Frequencies**.—A. Wainberg and L. Segebart, p. 234.
- A **New Method of Measuring Frequencies** [using Johnsen-Rahbeck Effect].—A. J. Makower and W. Makower, p. 104.
- Notes on Generation of Absolute Frequencies**.—T. Kujirai and S. Fujitaka, p. 174.
- The **Service Available from the Standard-Frequency Transmissions of the Bureau of Standards**.—J. H. Dellinger, p. 174.
- Radio Dissemination of the National Standard of Frequency**.—J. H. Dellinger and E. L. Hall, p. 594.
- The **Accuracy of the Primary Frequency Standard of the Bureau of Standards**.—C. G. McIlwraith, p. 174.
- A **Method of** [Audio-] **Frequency Measurement with the Cathode-Ray Oscillograph** [used as Source of Comparison Frequency and as Indicator].—L. A. Wood, p. 593.
- The **Precision Frequency Measuring System of R.C.A. Communications, Inc.**—H. O. Peterson and A. M. Braaten, 593.
- A **Source of Error in the Capillary-Wave Method of Measuring Frequency**.—M. Katalinic: Schultze, p. 473.
- International Frequency Measurements. The Production of Standard Frequencies by means of Piezoelectric Oscillators**.—A. Scheibe and U. Adelsberger, p. 473.
- Frequency Comparison at Great Distances** [including Italian Measurements of U.S. Bureau of Standards' Standard Frequency Transmissions].—F. Vecchiacchi, p. 534.
- Radio Frequency Standard Established at the Electrotechnical Laboratory**.—S. Kanzaki, p. 356.
- A **Device for Accurate Measurement and Checking of the Frequency of a** [Distant] **Radio Station**.—N. K. Titov and A. J. Weinberg, p. 293.
- Constant Frequency by Electronic Coupling**.—Dow, p. 235.
- Visit to Foreign Laboratories for the International Comparisons of Frequency**.—B. Decaux, p. 174.
- Frequency Measurement in the British Post Office**.—F. E. Nancarrow, p. 48.
- P.O. Frequency Measurements**.—Angwin, p. 104.
- Radio Problems** [P.O. Work on Frequency Measurement].—A. S. Angwin, p. 103.
- Frequency Measurement and Control**: I.E.E. Wireless Section, Chairman's Address.—A. S. Angwin, p. 174.
- Frequency Measuring Circuit**, p. 651.
- Frequency Measuring Outfit for Checking Wavelengths of French Transmitters** [at the Noisau Receiving Station], p. 651.
- The **Frequency Stability of the Triode Oscillator**.—Matteini, p. 342.
- Frequency**.—See also Wavelength, Wavemeter.

- The Coupled Steel [Frequency Standard] Oscillator.—C. H. Becker, p. 104.
- On the Theory of the Frequency Variation of an A.C. Measuring Circuit with D.C. Apparatus and Dry-Plate Rectifiers.—Cremers, p. 340.
- Frequency (Stabilisation, Standards, etc.).—See also Magnetostriction, Multivibrators, Oscillators, Plates, Quartz, Rochelle Salt, Rods, Tourmalin, Ultra-, and under "Transmission."
- The Gain Control and the Decibel.—H. Stanesby, p. 294.
- A Portable String Galvanometer for Use at Moderate Frequencies.—E. W. Marchant, J. K. Burkitt, and A. H. Langley, p. 50.
- An Aperiodic Impedance Measuring Set.—A. T. Starr, p. 534.
- A Method of Measuring Acoustic Impedance.—Flanders, p. 589.
- Measurement of Impedances.—H. F. Trewman: Starr, p. 594.
- A Cathode-Ray Oscillographic Method of Measuring Inductance.—G. I. Finch and R. W. Sutton, p. 357.
- The Inductance of Linear Conductors of Rectangular Section.—A. H. M. Arnold, p. 474.
- Measurement of Inductance: the Cathode-Ray Oscillograph Method.—G. I. Finch and R. W. Sutton, p. 293.
- Inductance.—See Choke, Coil.
- Electrodynamic Arrangement for the Measurement of Small Mutual Inductances.—Gillet, p. 361.
- High Insulation Testing and Surface Leakage.—D. C. Gall, p. 175.
- Sensitive Insulation Tester [using Grid Volts/Anode Current Characteristic of a Triode].—T. A. Ledward, p. 535.
- The Measurement of Radio Interference [High Frequency Spectra of Disturbances from Motors, Rectifiers, etc.].—Alexander, p. 652.
- Impedance Characteristics of Loaded Lecher Systems.—Tonks, p. 280.
- Formation of Standing Waves on Lecher Wires.—A. Mohammed and S. R. Kantebet, p. 175.
- Measurement at High Frequencies [10 to 6 400 kc/s] of the Loss Angles of Dielectrics.—M. Boella, p. 356.
- A New Method of Measuring the Loss Angles of Dielectrics, particularly Insulators in Series.—A. M. Angelini, p. 356.
- Losses in Liquid Dielectrics at Radio Frequencies [and the Meissner "Immersion" Method of Measuring the Self-Capacity of Coils].—Jackson, p. 298.
- A [Mercury Thermometer] Method of Measuring an Alternating Magnetic Field of High Frequency.—F. Esclangon, p. 105.
- The Damping of Magnetostriction Resonators.—E. A. Kopilowitsch, p. 355.
- On the Magnetostriction of Iron-Nickel Alloys.—Y. Masiyama, p. 293.
- Theory of Magnetostriction.—A. Perrier, p. 49.
- Improved Magnetostriction Oscillator.—Comp. Thomson-Houston, p. 50.
- On the Transverse Effect of Magnetostriction.—A. Esau, p. 49.
- The Magnetostriction of Ferromagnetic Materials.—G. Dietsch, p. 49.
- Magnetostriction and Hysteresis.—W. N. Bond, p. 49.
- Composite-Coil Electrodynamic [Measuring] Instruments.—F. B. Silsbee, p. 356.
- Indicating Electrical [Measuring] Instruments.—C. V. Drysdale, p. 651.
- Radio Measuring Instruments: Types and Applications.—E. H. W. Banner, p. 594.
- A Universal Meter for Laboratory and Workshop: the "Mavometer" with Its Auxiliary Attachments, p. 50.
- Hot-Wire Meter with Automatic Zero Error Compensation.—Etab. Brion, Leroux, Jeanno et Cie., p. 50.
- I.E.E. Meter and Instrument Section: Chairman's Address.—F. C. Knowles, p. 105.
- The Variation with Temperature of Meters with Dry-Plate Rectifiers, and Its Compensation.—H. Kaden, p. 416.
- Frequency Correction in Meters with Dry-Plate Rectifiers.—H. Kaden, p. 473.
- Meters and Instruments: Remote Indication and Earth Measurement Devices.—F. C. Knowles, p. 105.
- The Thermionic Valve Microvoltmeter.—E. Wöhlisch, p. 235.
- A Stroboscopic Method of Measuring Frequency and Phase Modulation: The Fourier Analysis of Modulated High Frequency Currents.—Heilmann: Grützmacher, pp. 93 and 94.
- A Direct Reading Modulation Meter.—Cooper and Smith, pp. 162-163.
- Moving-Coil Meter and Copper Oxide Rectifier for Measuring Modulation Ratio.—Lepeshinskaja-Krakau, p. 356.
- Multiples and Sub-Multiples of Ten [German Proposals], p. 474.
- The Adjustment of the Multivibrator for Frequency Division.—V. J. Andrew, p. 175.
- Dissymmetrical Multivibrators.—F. Vecchiacchi, p. 355.
- On the Theory of Beats [Application to the Calibration of Multivibrators].—Gabel, p. 280.
- Development of a Circuit for Measuring the Negative Resistance of Plidynatrons.—Dingley, p. 97.
- The Use of a Neon Lamp in Determining the Amplitude of a Periodically Varying Voltage.—S. Franck, p. 175.
- The Nomenclature of the Fundamental Concepts of Electrical Engineering.—G. W. O. Howe, p. 106.
- A Recent Development in Vacuum Tube Oscillator Circuits [Constant Frequency by Electronic Coupling].—Dow, p. 93.
- The Crystal Monitor: a Multi-frequency Crystal-Controlled Oscillator [with 6.25 kc Steps].—J. L. Reinartz, p. 104.
- Improved Radio-Frequency Measurements [including Oscillator with Output Transformer having Special Material for Core, giving Constant Output from 100 to 1 500 kc/sec.].—Wigand: Siemens Company, p. 473.
- A New Treatment of Electron Tube Oscillators with Feed-Back Coupling.—Jen, p. 163.
- Constant Frequency Oscillators.—Llewellyn, p. 163.
- The Isochronism of a Pendulum actuated by Impulses after passing through the Vertical.—Ch. Féry and N. Stoyko, p. 293.
- An Unrecognised Property of the Reversible Pendulum.—P. R. Heyl, p. 595.
- Measurements [of Infra-Red Radiation] with the Photoelectric Relay.—R. B. Barnes and F. Matossi, p. 474.
- The Design of Temperature Control Apparatus for Piezo Oscillators.—V. J. Andrew, p. 595.
- The Temperature of a Piezoelectric Crystal as a Function of Its Oscillatory Régime.—A. de Gramont and D. Beretzki, p. 473.
- A Piezoelectric Oscillator of Improved Stability [using a Screen-Grid Valve and giving a Constancy within 4.9×10^{-4}].—J. K. Clapp, p. 595.
- An Interpretation of the Effect of Piezoelectric Oscillations on the Intensity of X-Ray Reflections from Quartz.—B. E. Warren, p. 49.
- The Electric Network Equivalent of a Piezoelectric Resonator.—K. S. Van Dyke, p. 595.
- Piezoelectric Wattmeter for Rapidly Varying Powers.—Aerlikon, p. 236.
- Piezoelectricity [and the Testing of Various Crystals].—G. Greenwood and D. Tombouljan, p. 595.
- The Forced Vibrations of a Circular Plate.—W. Flügel, p. 416.
- The Elastic Equilibrium of a Thick Rectangular Plate.—B. Galerkin, p. 105.
- The Elastic Displacement, Normal to the Surface, of Thin Rectangular Plates Subjected to Variable Forces.—Sonier, p. 235.
- A Capacitive Potential Divider for High Frequency Measurements.—K. Schlesinger, p. 48.
- The Measurement of A.C. Potentials by means of Dry-Plate Rectifiers.—B. Focaccia, p. 473.
- The Wenner Potentiometer [reducing EMFs and Resistance Variations at the Contacts].—L. Behr: Wenner, p. 356.
- Theory and Technique of Valve Potentiometers for the Measurement of E.M.F.—F. Müller, p. 175.
- A Simple Method for Measurements of Residual Inductance on Potentiometers and Four-Terminal Resistance Coils.—N. F. Astbury, p. 48.
- On the Method of Measuring A.C. Power [and Power Factor] with a Triode.—A. Okitsu, p. 594.
- [Photometric] Dosimeter for Determining the Power in H.F. Circuits of Frequency 1 Megacycle and Over.—K. Heinrich, p. 236.
- Power Measurement with Electronic Valves.—H. Lange, p. 650.
- Power Factor Measurement by the Capacitance Bridge.—R. P. Siskind, p. 236.
- The Absolute Measurement of High Electrical Pressures.—W. M. Thornton and W. G. Thompson, p. 652.
- Determination of Quality as a Basis for Commodity Standards.—F. W. Reynolds, p. 595.
- Examination, by Immersion, of Large Quartz Crystals [Detection of Faults, Determination of Rotatory Power, etc.].—A. Arnulf, p. 473.
- Vibrations of Quartz Plates.—U.S. Bureau of Standards Notes, p. 104.
- The Vibrations of Quartz Plates [Chladni Plates Investigation].—R. C. Colwell, p. 533.
- Experimental Study of Parallel-Cut Piezoelectric Quartz Plates.—G. W. Fox and W. G. Hutton, p. 533.
- The Variation with Temperature of the Piezoelectric Constant of Quartz.—V. Fréedericksz and G. Michailow, p. 534.
- On the Series Law of the Free Elastic Vibration Frequencies of Quartz Rods. Part I: Elongation Oscillations.—E. Giebe and A. Scheibe, p. 48.
- Notes on the Frequency Stability of Quartz Plates.—L. B. Hallman, Jr., p. 293.
- Quartz Plate Mountings and Temperature Control for Piezo Oscillators.—V. E. Heaton and E. G. Lapham, pp. 49 and 293.
- Discussion on "Quartz Plate Mountings and Temperature Control for Piezo-Oscillators" [Spattered Film replaced by Soft Metal Rubbed On: Suggested Possibility of Obtaining Zero Frequency/Temperature Coefficient by Compensating Holder Pressure].—V. J. Andrew: Heaton and Lapham, p. 595.
- The Use of Supersonic Interferometry in Studying the Modes of Vibration of Quartz Crystals.—Hershberger, p. 534.
- Piezoelectric Quartz: Its Applications to Wireless Telegraphy and a New [Quartz] Oscillator for Broadcast Frequencies [Type 700-A].—O. M. Hovgaard, p. 104.
- Micrography of Piezoelectric Quartz.—P. T. Kao, p. 49.
- Longitudinal Vibrations of Thin Circular Quartz Plates.—I. Koga, p. 49.

- On the Temperature Coefficient of Frequency of Y-Wave in X-Cut Quartz Plates.—S. Matsumura and S. Kanzaki, p. 533.
- Physical Properties of Piezo Quartz Plates in connection with their Accurate Manufacturing for a Given Frequency.—E. S. Muchkin, p. 293.
- An Interferometer Method of Studying the Vibrations of an Oscillating Quartz Plate.—H. Osterberg, p. 235.
- The Quartz Oscillator.—T. D. Parkin, p. 594.
- Silvering Electrodes on Quartz Crystals [Brashear Process].—G. S. Parsons, p. 355.
- Silvering Electrodes on Quartz Crystals: a Warning.—Parsons, p. 595.
- On the Connection between the Optical and Piezoelectrical Properties of Oscillating Quartz Plates.—V. Petřílka, p. 105.
- Anomalous Variation of the Electrical Conductivity of Quartz with Temperature at the Transformation Point.—H. Saegusa and S. Shimizu, p. 105.
- A Preliminary Report on the Anomalous Variation of the Electrical Conductivity of Quartz with Temperature.—S. Shimizu, p. 473.
- Electrical Conductivity of Loaded Piezo-Quartz Crystals.—F. Seidl, p. 473.
- A New Method of Investigating the Modes of Vibration of Quartz Crystals.—J. A. Strong, p. 174.
- A Method of High-Frequency Stroboscopy [for Observation of Density Changes within a Vibrating Quartz Crystal].—J. A. Strong, p. 235.
- The Origin of the Third Fundamental Frequency of Piezoelectric Quartz Oscillators.—E. P. Tawil, p. 48.
- Piezoelectric Quartz in Vibration [Interferometer Study of Surface Vibrations].—G. Wataghin and G. Sacerdote, p. 595.
- Quartz Oscillator Wave Constants.—E. G. Watts, p. 48.
- Some Experimental Studies of the Vibrations of Quartz Plates [0° and 30° Cut].—R. B. Wright and D. M. Stuart, p. 104.
- Frequency Stabilisation to 5×10^{-6} by Quartz Crystal and Bolometer Combination.—German P.O. (Harnisch), p. 174.
- Natural Observation Limit of Radiometric Measurements.—C. H. Cartwright, p. 651.
- The Campbell-Shackleton Shielded Ratio Box.—L. Behr and A. J. Williams, Jr., p. 594.
- Quantitative Investigations of Broadcast Receivers.—Harnisch, p. 94.
- Developments in the Testing of Radio Receivers.—Thomas, p. 524.
- The Use of the Rectifier Bridge in Test Room Technique [as Phase-Sensitive Indicator, Frequency Analyser, etc.].—C. H. Walter, p. 651.
- A [Balanced] Rectifier Measuring Circuit [Phase-Sensitive "Rectifier Bridge" for Indicating or Measuring a Desired Component in an Alternating Potential, particularly suitable for Audio-frequency Use].—C. H. Walter, p. 593.
- The Measurement of Reflection Coefficients for Oblique Incidence [by Spreading the Material on the Metal Receiver of a Thermopile].—H. E. Beckett, p. 652.
- A Method of Measuring the Effective Resistance of a Condenser at Radio Frequencies, and of Measuring the Resistance of Long Straight Wires.—E. B. Moullin, p. 593.
- The Measurement of Electrical Resistance in Terms of a Mutual Inductance and a Period.—H. R. Nettleton and F. H. Llewellyn, p. 357.
- High Resistance Measurement [with the G.E.C. Low Grid Current Valve Type FP-45].—F. A. Lidbury, p. 356.
- Application of the Electrometer Triode to the Measurement of High Resistance.—J. A. C. Teegan and N. Hayes, p. 416.
- A Method for Measuring Very High Values of Resistance [up to 10^{17} Ohms].—G. M. Rose, p. 175.
- Design of Resistors [Resistance Boxes and Fixed Standards] for Precise High-Frequency Measurements.—L. Behr and R. E. Tarpley, p. 593.
- Piezoelectric Properties of Rochelle Salt Crystals.—R. D. Schulwas-Sorokin, p. 355.
- On a Characteristic Temperature Point in Rochelle Salt Crystals.—R. D. Schulwas-Sorokin, p. 595.
- Low Frequency Vibrations in Rochelle Salt and Quartz Plates.—W. G. Cady, p. 474.
- On the Forced Vibration of an Elastic Rod [taking into account the Internal Friction].—S. Higuchi, p. 175.
- Measurement of the Selectivity of Beat-Note Receivers.—Lamb, p. 594.
- Self-Capacity.—See Losses.
- Conductivity Measurements on Powders [of Semi-Conductors].—P. Guillery, p. 236.
- On the Current Compression in Cylindrical Tube Conductors [Skin Effect Formula].—E. Grünwald, p. 594.
- Skin-Effect in a Ring of Circular Cross Section [and the Calculation of Self-Inductance].—V. Fock, p. 636.
- The Natural Frequencies of Single-Layer Solenoids: Determination by taking Elementary Sections and applying a System of Elliptical Co-ordinates.—G. Zuhrt, p. 474.
- British Standard Letter Symbols for Use in Electrotechnics, p. 106.
- The Effect of Pressure upon the E.M.F. of the Weston Standard Cell.—T. C. Poulter and C. Ritchey, p. 474.
- International Comparison of Electrical Standards.—G. W. Vinal, p. 594.
- Stroboscopy.—See Quartz.
- On the Crystalline Structure of Thin Layers of Metals [sputtered on Quartz and Mica].—Z. Debinska, p. 293.
- A Chronograph for the Very Accurate Recording of Time.—P. Lejay, p. 49.
- Talking Clocks for the Distribution of Time over Telephone Networks [Sound-on-Film System].—E. Esclangon, p. 356.
- The Time Services of the U.S. Naval Observatory: Time Services of the Telegraph Companies: Synchronous Electric Time Service.—Hellweg: Janson: Warren, p. 235.
- The Necessity for a Standard Time Measurement, and My Results up to the present in Creating a Standard of Time.—M. Schüler, p. 235.
- On the Possibility of Constructing an Arrangement for the Measurement of Time which shall be Independent of the Accelerations of Its Support.—P. Le Rolland, p. 174.
- Papers on the Precise Measurement of Time: Short Clocks, Loomis Chronograph, Bell Telephone Crystal Oscillator.—Loomis: Brown and Brouwer, p. 49.
- Modern Developments in Precision Time-keepers.—A. L. Loomis and W. A. Morrison, p. 695.
- Photoelectrically-Controlled Time Signals at Bandoeng.—W. F. Einthoven: Vening Meinesz, p. 474.
- Communication of Standard Time Signals [U.S.A. Naval Observatory].—M. M. Dupré, p. 474.
- Symposium on Time-Signals: U.S.A. Naval Observatory Time-Service: Time-Signals for Electrical and Physical Measurements: Time-Signal Needs for Geodetic Work: Establishment of World-Time.—Hellweg: Wenner: Brown: Lee, p. 174.
- Tourmalin Crystals for Waves under 60 Centimetres.—Leithäuser: Heinrich Hertz Association, p. 293.
- A Tourmalin Oscillator for Wavelengths down to 1.2 Metre.—Straubel, p. 174.
- Fundamental Crystal Control for Ultra-High Frequencies: Tourmalin Oscillators for Wavelengths Down to 1.2 Metres.—H. Straubel, p. 355; see also Ultra-short.
- The Triode and the Tracing of the Hysteresis Cycle of Iron.—F. Vecchiacchi, p. 235.
- The Triode and the Determination of the Instantaneous Integrals of a Periodic Alternating Quantity.—F. Vecchiacchi, p. 235.
- The Triode and the Measurement of the Phase Angles of Condensers by the Method of Substitution in the Resonant Circuits.—F. Vecchiacchi, p. 356.
- Some Observations on Vibrating Tubes [and Their Use in Detecting and Measuring High Audio-Frequencies].—Kröncke, p. 414.
- The Measurement of Ultra-High-Frequency Currents.—H. Schwarz, p. 471.
- Measuring Technique and Apparatus for the Ultra-Short-Wave Zone.—K. Schiesinger, p. 650.
- Field-Strength Measurements on Ultra-Short Waves.—Sohnemann, p. 30.
- Direct Piezoelectric [Tourmalin] Control for Ultra-Short Waves.—H. Straubel, p. 235; see also Tourmalin.
- Electric and Magnetic Units.—V. Karapetoff, p. 652.
- Choice of a System of Electromagnetic Units [and the Selection of the Fourth Fundamental Unit].—D. Germani, p. 652.
- Dimensions of Fundamental Units.—W. Cramp, p. 652.
- Three Superfluous Systems of Electromagnetic Units.—G. A. Campbell, p. 652.
- Electromagnetic Equations and Systems of Units.—Leigh Page, p. 652.
- Magnetic Units.—A. E. Kennelly, p. 652.
- On the Structure of Systems of Units and the Definition of Magnitudes in Electrical Technique.—C. Budeanu, p. 652.
- On the Question of Electrical and Magnetic Units.—A. Blondel, p. 652.
- A System of Practical Units with Four Fundamental Dimensions.—E. Bodea, p. 652.
- A Standard Microvolter using Second Harmonic Principle [for Generating and Measuring Very Weak R.F. Voltages for Calibrating Signal Generators, Obtaining Performance Data on Receivers, etc.].—W. F. Diehl, p. 594.
- Using the Vacuum-Tube Voltmeter [for Radio Servicing, etc.].—B. B. Bryant, p. 594.
- A Linear Electronic Voltmeter.—J. L. McLaughlin, p. 594.
- Electron Tube Voltmeter.—F. N. Trotschitch, p. 356.
- A New Type of Valve Voltmeter [using Space-Charge Grid Valve].—L. Medina, p. 356.
- A New Thermionic Voltmeter [for Peak Potentials 200-2000 Volts up to Very High Frequencies].—J. Thomson, p. 472.
- Comparing Oscillatory Peak Factors by a Special Thermionic Voltmeter.—Thomson, p. 473.
- An Electrostatic Voltmeter [possessing Several Unique Features].—W. W. Nicholas, p. 293.
- A Generating Voltmeter for the Measurement of High Potentials.—P. Kirkpatrick and I. Miyake, p. 293.
- [Portable] Vacuum Tube Voltmeter of High Sensitivity.—H. J. Reich, G. S. Marvin, and K. A. Stoll, p. 50.
- An Electrostatic Voltmeter for Measuring High Voltages at High Frequency.—E. Wilkinson, p. 175.
- On Temperature Compensation in A.C. Low-Tension Voltmeters with Copper-Oxide Rectifiers.—V. Rozhdestvensky, p. 651.

Voltmeters.—See also Diodes, Measuring, Meters, Micro-, Neon, Potentials, Standard Cell.
 A New **Wattmeter** [for A.C. and D.C.] based on the Principle of the Hall Effect.—S. Fukuda, p. 474.
 A Precision Method of Measuring Short and Ultra-Short Wave-lengths.—W. Fehr, p. 293.
 Wide Wave Band Precision **Wavemeter** (10–300 Metres, with Neon Tube Oscillator for Reception Measurements).—Soc. Franç. Rad. élec., p. 473.
 The Station Finder [Buzzer Wavemeter].—A. L. M. Sowerby, p. 298.
 A Simplified Method of Interpolation by High-Frequency Measurements [Interpolation Formula for **Wavemeter**].—I. B. Selutin, p. 298.
 An Experimental Machine for Measuring Fine Wire.—F. H. Rolt and C. O. Taylerson, p. 595.
 Young's Modulus for Two Directions in a Steel Bar.—G. A. Wedgwood, p. 175.

SUBSIDIARY APPARATUS AND MATERIALS.

On the Absorption of Dipole Liquids and Electrolyte Solutions in the Region of Short Electrical Waves [of lengths 76 m, 48 m, and 28 m].—J. Malsch, p. 298.
Absorption in Liquids.—See also Dispersion.
 A New Iodine Accumulator.—F. Boissier, p. 420.
 New Storage Battery [Accumulator] using Iodine.—Boissier, p. 538.
 Articles on the Drumm Accumulator., p. 597.
 The Rapid Charging of Accumulator Batteries.—A. E. Langs, p. 597.
 The Theory of the Lead Accumulator.—C. Liagre, p. 51.
 On Local Action and the Theory of the Lead Accumulator.—L. Jumau : Féry, p. 51.
 Some Factors affecting the Performance and Life of Lead Accumulators : Part III.—J. T. Crennell and A. G. Milligan, p. 477.
 Characteristics of Lead Accumulators under Reduced Atmospheric Pressure [Improved Capacities under 13 mm Pressure].—S. Makio, p. 477.
 Accumulators for Broadcast Receivers.—R. Albrecht, p. 177.
 Papers on Air Cell Batteries and their Use for Radio Receivers, p. 284.
 An Electrostatic Alternator [giving Pure Sine Wave and Various Special Wave Forms].—C. A. Culver, p. 598.
 The Effects of Iron on the Electrical Conductivity and Tensile Strength of Aluminium.—M. Kuroda, p. 298.
 Characteristic Curves of the Aluminium Rectifying Cell.—L. L. Barnes, p. 296.
 Study of an Amplifier for Continuous Potentials.—A. Bressi, p. 475.
 The Very Sensitive Valve Amplifier throws light on the Problems of Nuclear Physics : Transmutation, and the Penetrating and Cosmic Radiations.—L. Leprince Ringuet, p. 475.
 A Vacuum Tube Amplifier for Feeble Pulses [and an Electrometer Valve after Leprince-Ringuet].—L. F. Curtiss, p. 654.
 A New Amplifier for Direct and Alternating Currents.—H. Peek, p. 535.
 A Stable Laboratory Amplifier [for Bridge, Photoelectric Cell, and other Work].—C. T. Burke, p. 239.
 Increasing the Charge Sensitivity of Vacuum Tube Amplifiers.—G. F. Metcalf, p. 297.
 Amplifiers for Precise Oscillographic Measurements.—S. K. Waldorf, p. 536.
 One-Tube Balanced Circuit for D.C. Vacuum Tube Amplifiers of Very Small Currents.—W. Soller, p. 654.
 Automatic Curve Analyser.—C. G. Abbot, p. 177.
 A Simple Harmonic Analyser.—M. G. Nicholson and W. M. Perkins, p. 416.
 Discussion on "A Simple Method of Harmonic Analysis for Use in Radio Engineering Practice."—J. R. Ford : Roder, p. 358.
 A Simple Method of Harmonic Analysis.—Nachtkal, p. 589.
 An Air-Bubble Method of Measuring Very Small Angles of Rotation—down to 0.27 Sec.—G. Siadbei, p. 598.
 Anode Supply for Automobile Receivers from Car Storage Battery.—A. B. Bedrossyan, p. 239.
 Papers on Attenuating Layer Photoelectric Cells.—Körösy and Scélyni : B. Lange : Perucca, p. 239.
 The Attenuating Layer in Lead Sulphide.—Heineck, p. 469.
 Conductivity and Photoelectric Effects at Attenuating Layers.—Schottky, p. 232.
 The Electrical Behaviour of Attenuating Layers.—Teichmann, pp. 468-469.
 Simplified Attenuation Network Design.—L. B. Hallman, p. 50.
 A Measurement of Boltzmann's Constant by Means of the Fluctuations of Electron Pressure in a Conductor [containing Description of Attenuator System].—Ellis and Moulin, p. 588.
 The Thermal After-Treatment of Bakelite for Precision Uses.—Vogt, p. 177.
 Report on the Conference on "Barrier-Layer Photoelectric Cells and Rectifiers."—Kurtschatow, p. 654.
 Investigation of the Barrier-Layer Photocell.—Kurtschatow and Sinelnikov, p. 654.

Primary Batteries, Dry and Wet, according to Recent Patents.—L. Jumau, p. 538.
 A New Battery [Dry Cell with Device for Sealing in the Active Ingredients but Giving Free Exit to Evolved Gases].—Siemens Company, p. 597.
 Primary Battery Improvements : Ammonium Persulphate as a Depolariser.—A. M. Codd, p. 597.
 Development of B-Battery Devices for Auto-Radio, p. 420.
 An Improved B Eliminator for Automobile Receivers [with Automatic Load Release Circuit for Preventing Burning of Vibrator Contacts before Rectifier Heater reaches Working Temperature].—W. W. Garstang, p. 655.
 B Power Supply Devices for Automobile Radio.—H. E. Thomas and L. P. Kongsted, p. 597.
 The Elgin-Cartier Baudot Reproducer without Rotating Parts.—P. Mercy, p. 110.
 Bolometer.—See Relay.
 On the Mechanism of Electrical Breakdown [in Rock Salt, Mica, etc.].—A. Joffé, p. 655.
 Screens for Raising the Breakdown Voltage in Air.—H. Roser, p. 418.
 Proximity Effect in Cable Sheaths.—H. B. Dwight, p. 109.
 A New Type of Non-Uniform Cable [Impedance per Unit Length Increasing Linearly with Distance].—M. Federici, p. 177.
 Attenuation of a Surge along a Cable.—W. Fucks, p. 418.
 Surges in Continuously Variable Cables.—Geman, p. 218.
 A Simple Harmonic Continuous Calculating Machine.—J. M. Robertson, p. 295.
 Capacitance and Power Factor of a Mica Capacitor as measured at the Bureau of Standards and the National Physical Laboratory, p. 534.
 The Electrical Conductivity of the Different Varieties of Carbon.—R. Cordebas, p. 476.
 On the Electrical Resistance of Carbon.—Z. Nishiyama, p. 110.
 Type II Phosphorescence of the Carborundum Detector, Electrical Conductivity of Carborundum and Unipolar Conductivity of Crystal Detectors.—O. W. Lossev, p. 108.
 On the Rectifying Action and Luminous Effects of Carborundum Crystals.—B. Claus, p. 108.
 Delay Circuits for Recording with the Cathode-Ray Oscillograph [Comparison between Surge Line Circuits and Condenser Circuits, with Description of a Condenser Circuit with Adjustable Delay Time].—H. Baatz, M. Freundlich and W. Holzer, p. 596.
 On the High Voltage Plant of the Cathode-Ray Oscillograph.—K. Beyerle, p. 238.
 A New Type of Cathode-Ray Oscillograph with Cold Cathode and Pre-concentration.—H. Boekels, p. 536.
 On Potential Dividers for Cathode-Ray Oscillographs.—F. P. Burch, p. 358.
 Screen Size and Width of Trace in the Cathode-Ray Oscillograph.—K. Buss, p. 475.
 Cossor Cathode-Ray Oscillograph.—A. C. Cossor, Ltd., p. 536.
 Cathode-Ray Oscillograph [Internal] Recording Direct on Photographic Paper.—W. Förster, p. 596.
 On Control by Surges, Beam Locking in Cathode-Ray Oscillographs, and the Production of Very Short Light Impulses.—W. Fucks, p. 238.
 A New Cathode-Ray Oscillograph Tube [Type FP-53, giving Visual Observation by a Large Group in Full Daylight].—G. F. Metcalf : G. E. C., p. 475.
 The Focusing Coil [in the Cathode-Ray Oscillograph] as a Magnifying Lens.—F. Hamacher, p. 358.
 A Lecture-Demonstration [Cathode-Ray] Oscillograph [with Linear Time Scale, using Western Electric Gas-filled Hot-Filament Tube].—W. W. Hansen, p. 536.
 A New Glass Discharge Tube [with High Vacuum Jacket] for the Cathode-Ray Oscillograph.—F. Hauffe, p. 106.
 Recording Non-Periodic Phenomena with the Cathode-Ray Oscillograph.—H. E. Hollmann, p. 176.
 The Cathode-Ray Oscillograph.—J. B. Johnson, p. 294.
 The Cathode-Ray Oscillograph [and the Western Electric Tube No. 224].—J. B. Johnson, p. 176.
 New Method for the Simultaneous Recording of Phenomena by Cathode-Ray Oscillograph and the Determination of the Scale of the Magnitudes Recorded.—K. Kasai, H. Takagishi and B. Tadano, p. 475.
 The Distortions in the Cathode-Ray Oscillograph at High Measuring Velocities.—H. Klemperer and O. Wolff, p. 596.
 The Cathode-Ray Oscillograph. Literature to the Middle of 1931 : Development up to the Middle of 1931.—M. Knoll, p. 358.
 Remark on the Paper "Glass or Metal Discharge Tube" [for Cathode-Ray Oscillograph].—M. Knoll and H. Knoblauch : Dicks, p. 358.
 The Blackening of Photographic Films in the Cathode-Ray Oscillograph.—Remark on the Paper by W. Rogowski, E. Flegler and P. Rosenlöcher.—M. Knoll : W. Rogowski, p. 418.
 Pre-concentrating Coils and Electron Density in the Cathode-Ray Oscillograph.—F. Malsch, p. 358.
 Theory of Voltage Dividers and Their Use with Cathode-Ray Oscillographs.—M. F. Peters, G. F. Blackburn and P. T. Hannen, p. 596.

- The Cathode-Ray Oscillograph in Radio Research: Royal Society Demonstration and Lecture.—Radio Research Station, Slough: R. A. Watson Watt, p. 653.
- The Limit of Performance of the Cathode-Ray Oscillograph.—W. Rogowski, p. 50.
- Cathode-Ray Oscillographs.—W. Rogowski, p. 418.
- The Blackening of Photographic Films at Low Excitation Voltages of the Cathode-Ray Oscillograph.—H. Schäfer, p. 475.
- The Cathode-Ray Oscillograph and Fluorescent Materials.—A. Schloemer, p. 417.
- Cathode-Ray Oscillograph operating on 350 v.—Standard Telephones and Cables, p. 106.
- A Sealed-Off Cathode-Ray Oscillograph of High Efficiency.—K. Szegehő, p. 418.
- The Use of the [von Ardenne] Cathode-Ray Oscillograph for Recording the Wave Form of High Voltages.—R. Vieweg and G. Pfestorf, p. 653.
- Phase Measurements with the Cathode-Ray Oscillograph.—L. A. Wood, p. 50.
- Recent Developments in Cathode-Ray Oscillographs [Survey with Literature References up to 1931].—A. B. Wood, p. 536.
- Cathode-Ray Oscillographs.—See also Amplifiers, Electron, Glow, Oscillographs, Relay, Stroboscopic, Sweep, Time Axis and Base, Timing Axis, Trip, and below.
- A Cheap Cathode-Ray Tube for 800 Volts Potential, or 2000 Volts for Photographic Recording.—R. Wigand: G. Budich Company, p. 475.
- Improvements in Cathode-Ray Tube Design.—V. K. Zworykin, p. 106.
- A New Cathode-Ray Tube with Small Ray Velocity [Sensitivity around 1 mm/volt with a Working Voltage of 300 v].—G. Dobke: AEG, p. 653.
- The Physics of the Braun [Cathode-Ray] Tube.—M. von Ardenne, p. 653.
- The Cathode-Ray Tube at Very High Frequencies [up to about 10^{10} c/s].—H. E. Hollmann, p. 652.
- Accuracy of Measurements made with Hot-Filament Cathode-Ray Tubes of the Gas-Focused Type [with Particular Attention to the Threshold Effect].—J. T. MacGregor-Morris and H. Wright, p. 536.
- Investigations on Cathode-Ray Tubes containing Gas.—M. von Ardenne, pp. 237 and 653.
- Cathode-Ray Tubes and Their Use.—E. Alberti, p. 653.
- The Short Space-Charge Field of an Auxiliary Discharge as a Collecting Lens for Cathode Rays.—B. von Borries and E. Ruska, p. 536.
- The Photographic Effect of Moderately Rapid Cathode Rays.—A. Becker and E. Kipphan, p. 50.
- Demonstration of the Focus and Resolving Properties of a Cylindrical Condenser Field on Cathode Rays.—H. Voges, p. 536.
- The Dependence of the Brightness of the Light Emitted by Calcium Tungstate under the Impact of Electrons [Cathode Rays] on the Energy of the Electrons.—A. Güntherschulze and F. Keller, p. 596.
- Relativity Correction of the Laws of Image Formation of a Magnetic Collecting Lens for Cathode Rays.—F. Ollendorff and G. Wendt, p. 536.
- Registration of Cathode Rays by Thin Films of Metals and Metal Compounds.—W. W. Nicholas and C. G. Malmberg, p. 295.
- The Photographic Effect of Slow Cathode Rays.—V. Weidner, p. 294.
- On the Concentration of Cathode Rays by means of Gas Particles.—W. Ende, p. 238.
- The Important First Choke in High-Voltage Rectifier Circuits.—F. S. Dellenbaugh, Jr., and R. S. Quimby, p. 358.
- High Inductance Smoothing Choke.—H. B. Dent, p. 654.
- The Design of Iron Core Chokes.—M. G. Scroggie, p. 477.
- Utilisation to the Fullest Extent of Iron-Cored Chokes carrying Direct Current.—R. Gürtler, p. 477.
- Remarks on the Design of Iron-Cored Choking Coils.—J. Hak, p. 598.
- Chokes.—See also Reactance.
- A Direct-Reading Electric Chronograph for the Exact Measurement of Very Short Intervals of Time [Condenser-Charging Principle using an "Electrometer" Valve and a Neon Lamp as Relay: Application to Echo Sounding for Aircraft and Ships].—R. Dubois and L. Labourer, p. 416.
- An Application of the Circle Diagram to the Design of Attenuation and Phase Equalisers.—Rust, pp. 161 and 280.
- A Simple Clamp for Fine Wires [Low-Current Fuses, etc.; using Press Fasteners].—L. Bainbridge-Bell, p. 239.
- The Dielectric Properties of Varnished Cloth at Low Voltage Gradients (E.R.A. Report).—L. Hartshorn, p. 476.
- The Electrical Properties of Russian Colophony.—Bogorodizky and Maigeldinov, p. 109.
- A New A.C. Potential Comparator.—D. C. Gall, p. 359.
- Compound Compass for Drawing Arcs of Great Radius.—L. W. McKeehan, p. 295.
- Measuring Condenser Whose Capacity Increases Linearly from an Exact Zero.—K. Kuhlmann, p. 108.
- A New Type of High Voltage Condenser [replacing Leyden Jars].—H. Wommelsdorf, p. 537.
- The Use of the Positive Ion Sheath on an Electrode to give a Variable Condenser Effect: Employment of such a Condenser in Signalling by Frequency Change.—Thomson-Houston Company, p. 599.
- A Standard of Small Capacity Differences [Variable Condenser for Inter-Electrode Capacity Measurements].—Bartlett, p. 48.
- On the Theory of the Paper Condenser.—M. I. Mantrov, p. 599.
- Life Test for [Paper] Condensers.—H. W. Houck, p. 109.
- Absorption in Electric Condensers [Paraffin Wax—Paper Type].—R. E. W. Maddison, p. 655.
- Condensers made by Deposition of Metallic Powder by Jet of Acetylene Gas.—Soc. Duret, p. 478.
- Telephone Condensers [Foil and "Mansbridge" Types].—R. E. W. Maddison and S. Chapman, p. 51.
- Equivalent Circuits of Imperfect Condensers.—C. L. Dawes and W. M. Goodhue, p. 420.
- Principle, Construction, and Use [and Testing] of Electrolytic Condensers.—W. Hoersch, p. 51.
- Measuring the Power Factor of Electrolytic Condensers, p. 51.
- Methods of Testing Characteristics of Electrolytic Condensers.—W. W. Garstang, p. 420.
- Electrolytic Variable Condensers.—W. W. Garstang, p. 420.
- Electrolytic Condensers for the Transmitter.—W. M. Bailey, p. 599.
- Power Losses in Electrolytic Condensers: Film Characteristics of Electrolytic Condensers.—F. W. Godey, Jr., p. 239.
- Mica Condensers in High-Frequency Circuits.—I. G. Maloff, p. 420.
- Tests on Japanese Standard Mica Condensers.—K. Yamaguchi and S. Inoue, p. 420.
- Contact-Making [Metering] Instruments.—F. S. Marcellus and S. W. Spengler, p. 656.
- Preliminary Communication on Metallic Contacts with an Interposed Very Thin Film of Foreign Material.—R. Holm: Meissner, p. 237.
- Investigations on Gold Alloys for Contacts. Part I.—C. Benedicks and J. Hårdén, pp. 295 and 417.
- Behaviour of the Copper-Cuprous Oxide Rectifier at High Frequencies.—W. P. Piacce, p. 597.
- Rectifier Effect and Heterogeneous Catalysis in Copper-Cuprous Oxide Systems.—Wo. Ostwald and H. Erbring, p. 419.
- Structural Investigation of the Copper Oxide Rectifier. Contribution to the Crystal and Attenuating Layer Photoelectric Effect.—Scharf and Weinbaum, p. 469.
- Current-Voltage and Thermal Characteristics of the Copper Oxide Rectifier.—W. B. Pietenpol and G. W. Presnell, p. 478.
- On the Composition of the Oxide in Copper Oxide Rectifiers and Photoelectric Cells.—L. Dubar, p. 419.
- On the Nature of the Attenuating Layer in Copper Oxide Rectifiers.—F. Waibel and W. Schottky, p. 419.
- Copper Oxide Rectifiers.—K. Singh, p. 107.
- The Electronic Conductivity of the Copper Oxide.—M. Le Blanc and H. Sachse, p. 238.
- Cotton for Insulation.—R. I. Martin, p. 177.
- Counter, Automatic.—See Thyatron.
- The Oscillating Crystal [Crystal Detector] and the Reasons for its Behaviour.—E. Habann, p. 108.
- The Oscillating [Crystal] Detector.—F. Noack; Habann, p. 538.
- The Oscillating Crystal and its Technical Form.—E. Habann, p. 659.
- On the Nature of Electron Motion in Crystals and Its Significance in the Electrical Behaviour of Solids [including Rectifying Action].—L. Nordheim, p. 597.
- A Manual Recorder [Manual Curve Drawing Equipment developed from the Radio Fading Recorder].—H. S. Wilkins, p. 295.
- A Method of Interpreting Static Frequency- or Distribution-Curves.—H. C. Plaut, p. 418.
- An Auxiliary Appliance for Work with Lucas Curves—The Inversion Ruler and Slide Rule [for Graphs of Electrical Networks].—H. Reppisch, p. 478.
- On the Theory of Detector Action.—L. Nordheim, p. 420.
- The Trend in Dielectric Research [including a Bibliography].—B. Whitehead, p. 239.
- The Constancy of the Dielectric Constant at Extremely High Field Strengths.—A. Güntherschulze and H. Betz, p. 51.
- The Influence of Electrolytes on the Dielectric Constant of Water.—R. T. Lattey and W. G. Davies, pp. 109 and 298.
- The Dielectric Constant and Power Factor of Some Solid Dielectrics at Radio Frequencies.—W. Anderson, p. 476.
- A Beat Method for Determining the Dielectric Constants of Liquid Conductors.—W. Graffunder and R. Weber, p. 109.
- Discussion on "Dielectric Phenomena at High Voltages."—Goodlet, Edwards and Perry, p. 655.
- The Dielectric Strength of Certain Substances [CCl₄ and CS₂].—H. Eisler, p. 476.
- Thermal and Electrical Conductivity of Dielectrics [and a Possible Relation between the Two].—M. I. Mantrov, p. 298.
- The Amplifier-Oscillograph Applied to the Study of Dielectrics with Continuous Potentials.—S. K. Waldorf, p. 596.
- The Theory of Thermal Breakdown of Solid Dielectrics.—P. H. Moon, p. 109.
- The Predetermination of the A.C. Behaviour of Dielectrics [by Measurement of Charge and Discharge Currents under Continuous Potential].—J. B. Whitehead and A. Banos, Jr., p. 298.
- Ionisation of Solid Dielectrics by X-Ray Irradiation [Resulting Conductivity obeys Ohm's Law: at 570 Volts the Ionisation in Sulphur exceeds that in Air].—M. Bender, p. 655.

- Measurement of Power Factor and Loss in Dielectrics [Liquid, Solid and Composite].—T. J. Mirchandani, G. Yoganandam, S. K. Roy and N. V. Narayanaswami, p. 655.
- A Method of Determining the Impedance of Hot Cathode [Neon and Mercury Vapour Arc] Discharge Tubes.—W. F. Westendorp, p. 51.
- Improvements in Electric Discharge Tubes [Reduction of Secondary Emission from Grid by Increasing Heat Radiation].—Philips' Company, p. 598.
- Improvements in Discharge Tubes with Hot Cathodes: Reduction of Power Consumed in Heating, by Thermal Insulation of Cathode.—Claude, p. 238.
- Gas-Filled Discharge Tubes with Control Grid—Schottky "Wall Current" Relay Tube and Hull "Thyratron".—E. Lübecke, p. 235.
- Control Conditions of Grid-Controlled Gas Discharges—Ion Control Valves [e.g., Thyratrons].—H. Klemperer and E. Lübecke, p. 359.
- Dispersion Measurements of Liquids, in particular Biological Solutions with Undamped Waves of Length 1 to 4 m.—E. May and H. Schaefer, p. 298.
- Constructional Methods for the Driving of Bands or Tapes in Apparatus of High Precision.—K. H. Sieker, p. 538.
- British Standard Specification for Ebonite for Electrical Purposes.—British Engineering Standards Association, p. 51.
- The Effect of Sunlight on Ebonite.—M. C. Timms, p. 109.
- A Three-Dimensional Adjustment of an Electrode in Vacuo.—J. L. Miller and J. E. L. Robinson, p. 598.
- Voltage Effect in Electrolytic Solutions and Cathode Ray Oscillograph.—W. Fucks, p. 295.
- New Researches on Electrolytic Valve Action.—A. Güntherschulze and H. Betz, pp. 296 and 419.
- Electrolytic Valve Action and Electrolytic Rectifiers.—E. Newbery, p. 597.
- On the Theory of the Electrolytic Valve Action.—W. J. Müller, p. 296.
- Contribution to the Geometrical Optics of Electron Beams: I and II.—M. Knoll and E. Ruska, p. 418.
- Remark on the Form of Stop to be Used with Electron Beams in Gases.—H. Seyfarth, p. 536.
- Electron Microscopes.—Brüche and Johansson: Knoll and Ruska, p. 653.
- Electron Optics and Electron Microscope.—E. Brüche and H. Johansson, p. 476.
- Sensitive Electroscopes [Three Types].—C. Lukens, p. 598.
- On an Effect shown by Ferromagnetic Materials in an Alternating Electromagnetic Field.—A. Esau and H. Kortum, p. 477.
- The Thermoelectric Properties of Ferromagnetic Substances.—L. F. Bates, p. 297.
- Symposium on Ferromagnetism.—F. Bitter, S. L. Quimby, R. M. Bozorth, K. J. Sixtus, L. Tonks, T. D. Yensen, P. P. Cioffi, S. R. Williams and L. W. McKeehan, p. 477.
- Determining Field Distribution by Electronic Methods [Recording Field Diagrams by Exploring in Distilled Water and Transferring Position by Pantograph].—E. D. McArthur, p. 475.
- The Properties and Calculation of the Multiple Bridge Filter.—A. Jaumann, p. 595.
- A 24000 Watt Filter.—M. Brotherton, p. 106.
- Rectifier Filter Circuits.—R. Lee, p. 598.
- Filter Circuits.—W. Cauer, p. 50.
- New Theory and Design of Wave Filters.—W. Cauer, p. 537.
- Calculation of the Building-Up Time of Band-Pass Filters.—J. Labus, p. 537.
- An Electrodynamic Band Pass Magnifier as a Substitute for Filters and Valve Amplifiers in Note-Frequency Telegraphy.—M. Wald, p. 357.
- The Economical Design of Smoothing Filters.—F. S. Dellenbaugh, Jr., and R. S. Quimby, p. 419.
- Precision Methods Used in Constructing Electric Wave Filters for Carrier Systems.—G. R. Harris, p. 417.
- The Measurement of Fluorescence by means of the Photoelectric Cell.—R. Toussaint, p. 177.
- Electrodeposited Metal Foils.—H. Kersten, p. 110.
- A Method for the Approximate Calculation of a Thermionic Frequency Changer [based on Anode Dissipation].—A. I. Joffe, p. 359.
- On Resonance Phenomena in Frequency Division.—Mandelstam and Papalexi, pp. 279-280.
- A Thermionic Frequency Doubler.—C. K. Stedman, p. 294.
- A Cathode-Ray Frequency Multiplier [for Obtaining Ultra-High Frequencies].—Jamison, p. 520.
- Automatic Frequency Regulation.—H. Martin, p. 359.
- Contributions to the Theory of the [Magnetic] Frequency Transformer.—F. Gutzmann, p. 294.
- The Protection of Potential Transformers by the "RL" Micro-Fuse.—R. Loubet, p. 110.
- Boric Acid Fuses [extinguishing Arc by Water Vapour generated in the Fuse], p. 359.
- Saving Instrument Losses by Proper Fuse Protection [Oscillographic Investigation; Quick-acting "Littelfuses"].—E. V. Sundt: Kollath, p. 421.
- A New Protection for Galvanometers [Use of Triode as Overload Bye-Pass].—C. Moerder, p. 478.
- An Improved McLeod Gauge.—S. D. Dryden, p. 107.
- A Clock-Controlled Constant-Frequency [Motor-] Generator.—A. B. Lewis, p. 294.
- Variation with Frequency and Temperature of the Dielectric Properties of Different Varieties of Glass.—M. J. O. Strutt, p. 177.
- The Dielectric Constants of Glasses and Their Dependence on the Composition.—F. Keller, p. 476.
- Glow Discharge Lamps for the Generation of "Kipp" Oscillations.—H. von Hartel, p. 536.
- Oscillographic Investigation of Intermittent Glow Discharges.—R. Rinke, p. 239.
- A Device for Separating the Harmonics of Complex Waves.—Gall, p. 589.
- Elimination of Harmonics superposed on a Continuous Current, p. 593.
- The Limits of Validity of the Steinmetz [Hysteresis Loss] Formula.—I. Lucchi, p. 477.
- Ilium [a New Alloy], p. 598.
- Impulse Prolonging Circuits in which the Secondary Time is dependent on the Primary Time.—W. Grube, p. 295.
- The Prolongation of Impulses.—W. Grube, p. 50.
- Iron-Cored Inductances, with Air-Gap, carrying a Direct Current Component.—R. Gürtler, pp. 236 and 296.
- Trolital: a Synthetic Material, Transparent, Not Brittle, and Highly Insulating, p. 359.
- The Behaviour of Rubber-less Insulating Moulding Materials under Prolonged Immersion Tests.—W. Zebrowski, p. 109.
- A New Insulating Material, particularly for Cathode Construction in A.C. Valves.—Crowley, p. 599.
- New Steatite as an Insulating Material for High Frequencies.—E. Albers-Schönberg and J. Gingold, p. 359.
- Properties of Moulded Plaskon [Insulating Material], p. 476.
- Phenol Plastic [Insulating Material] for Moulded Cases for the Tropics.—I. T. and T., p. 293.
- The Loss Curve of Air-Containing Insulating Materials.—A. Gemant, p. 476.
- Dielectric Losses in Insulating Materials.—H. H. Race, p. 476.
- On the Dielectric Loss of Insulating Materials at High [and Ultra-High] Frequencies.—H. Irino, p. 359.
- Insulating Materials.—A. R. Dunton, p. 109.
- The Survey of Progress in Insulating Materials.—A. R. Dunton, p. 476.
- Low-Thermal-Expansion Ceramics [Insulating Materials].—W. W. Winship, p. 476.
- Insulating Materials.—"Formapex" Miacarta: "Linapex," p. 51.
- On the Variation with Potential of the Dielectric Loss Angle of Certain Insulating Materials.—M. Hirsch, p. 655.
- Chemical Research in Insulating Materials [a Résumé of Papers].—F. M. Clark, p. 655.
- Some Insulating Materials.—A. R. Matthis, p. 655.
- Tests on Raising the Dielectric Strength of Insulating Oils by Filtration through Glass Powder Compositions.—P. H. Prausnitz and F. Obenaus, p. 298.
- Dielectric Properties of Some Glycols: Development of Polar Characteristics in Insulating Oils.—A. H. White and S. O. Morgan: W. N. Stoops, p. 655.
- A Glowing-Wire Instrument for Burning Away Insulation during the Wiring of Broadcast Receivers, etc.—AEG, p. 538.
- Insulation.—See also Dielectric.
- Insulations.—H. Warren, pp. 109, 298 and 599.
- The Disc Leading-In Insulator.—H. Brülle, p. 476.
- The Best Shapes for Condenser Leading-In Insulators.—H. Einhorn, p. 477.
- On the Surge Testing of Insulators.—J. Kopeliovitch, p. 50.
- The Shot Effect and Electrical Breakdown in Insulators.—R. M. Bozorth and F. E. Haworth, p. 476.
- Electro-Mechanical Integrations and the Solution of Differential Equations with Variable Coefficients.—P. Fourmarier: Bush, p. 656.
- The Magnetic Susceptibility of Iron Powder Compositions, and Its Dependence on Particle Size and Separation.—E. Gerold, p. 654.
- Iron.—See also Magnetic, Magnetisation, Permeability.
- Isolantite Characteristics [at Frequencies from 246 to 1 375 kc/sec.], p. 476.
- Laue Spots from Perfect, Imperfect and Oscillating [Quartz] Crystals.—C. S. Barrett, p. 108.
- Losses in Liquid Dielectrics at Radio Frequencies [and the Meissner "Immersion" Method of Measuring Self-Capacity of Coils].—W. Jackson, p. 298.
- An Improved Permagmeter for Testing Magnet Steel.—B. J. Babbitt, p. 239.
- Relationships Amongst the Magnetic Properties of Magnet Steels and Permanent Magnets.—K. L. Scott, p. 297.
- Magnet Steels and Permanent Magnets.—K. L. Scott, p. 598.
- Russian Papers on the Magnetic Behaviour of Iron, Powdered Iron Compounds, etc., in High- and Low-Frequency Fields: including Magnetostriction and Magnetron Resonance.—Malow, Volkova, Arkadiev and others, p. 176.
- A Theory of Magnetic Permeability for Frequencies ranging from the X-Ray Region to Commercial A.C.—W. Arkadiev, p. 177.
- Contribution to our Knowledge of Magnetisation of Iron by Alter-

- nating Currents [chiefly Theoretical Investigation].—H. S. Hallo and R. H. Borkent, p. 236.
- Barkhausen Effect. III. Nature of Change of Magnetisation in Elementary Domains.—R. M. Bozorth and J. F. Dillinger, p. 654.
- The Magnetisation of Ferromagnetic Powders in Weak Fields.—R. Chevallier, p. 477.
- Magnetisation of Macroscopic Powders in Weak Fields.—R. Chevallier, p. 477.
- The Influence of the Condition of Elastic Strain on the Value of the Permeability at Low Magnetising Forces.—M. Kersten, p. 176.
- A Vacuum Make-and-Break Device for Potentials up to 65 kv.—G. Vaudet, p. 418.
- Dielectric Losses in Micanite Insulation of H.T. Generator Coils: Survey.—W. Boller and M. Wellauer, p. 239.
- The Permittivity and Power Factor of Micas: Discussion.—Dannatt and Goodall, p. 51.
- Some Electrical Properties of Foreign and Domestic Micas and the Effect of Elevated Temperatures on Micas.—A. B. Lewis, E. L. Hall, and F. K. Caldwell, p. 51.
- The Dielectric Strength of Russian Micas.—Florensky, Mantrov and Budnicky, p. 298.
- Theory of Thermal Micromanometers.—M. Matricon, p. 238.
- The Problem of Motion Picture Projection from Continuously Moving Film.—F. Tuttle and C. D. Reid, p. 418.
- Shock-Proof Mounting using Air Cushioning.—E. Gehrcke and B. Voigt, pp. 239 and 655.
- The Effect of Mechanical Disturbance on a Neon Lamp [Demonstration].—T. J. Dillon and C. M. Lovett, p. 176.
- The Series Circuit with Neon Lamp and Condenser, giving Train of Flashes.—Decaux and Le Corbeiller, p. 33.
- Apparatus for Measuring the Number of Turns, up to 3000, in a Winding.—C. Dannatt, p. 110: see also Turn.
- Elastic Stop Nut [with Unthreaded Fibre Collar] Applications in the Radio Industry.—H. B. Thomas, p. 599.
- Constant Frequency Oscillators.—F. B. Llewellyn, p. 294.
- The Piezoelectric Oscillograph [Sensitivity of 200 v/mm and Frequency Range up to 7500 Cycles/Sec.].—W. von Philippoff, p. 418.
- The Rapid Record Oscillograph in Sound Picture Studies.—A. M. Curtis, T. E. Shea and C. H. Rumpel, p. 418.
- New Blondel Portable Oscillograph.—J. Vassilière-Arlhac, p. 107.
- The "Osio" Oscillograph Equipment for the Automatic Recording of Random Phenomena [with Device for Rapid Lighting-Up of Recording Lamp].—J. T. Johnson, p. 654.
- A Vibrating Reed Oscillograph [Moving-Coil Loud Speaker Design, Coil held by Reed].—F. J. Shollenberger, p. 653.
- Characteristics of the Oscillograph-Galvanometer. Some Practical Considerations in the Design and Application of the Oscillograph-Galvanometer Vibrator.—V. S. Thomander, p. 176.
- The Calibration of Oil-Damped Oscillographs.—E. L. E. Wheatcroft, p. 107.
- Contribution to Kerr-Cell Oscillography.—E. Trümper, p. 653.
- A Neon-Tube Oscilloscope.—Guerbilsky, p. 238.
- On the Chemical Nature of the Oxide Layers which Form on the Metals Al, Zr, Ti and Ta with Anodic Polarisation.—W. G. Burgers, A. Claassen and J. Zernike, p. 419.
- The Dielectric Constants of a Number of Oxides (in particular Al_2O_3).—Güntherschulze and Keller, p. 419.
- Potential Distribution Radiation and Electrical Conduction in Paper.—E. B. Baker and R. F. James, p. 298.
- The Electrical Conductivity of Black Paper. Applications [to the Making of High Resistances and the Tracing of Equipotential Lines].—L. Grillet, p. 476.
- Effect of Ionisation on Impregnated Paper Insulation.—K. S. Wyatt, p. 599.
- Modern Loading Equipment [including Coils with Permalloy Dust Core—"Stanelec"]—Part I.—J. B. Kaye, p. 297.
- How the High Frequency Permeability of Iron Wires Depends on the Field.—M. Wien, p. 297.
- The Relative Permeability of Iron, Nickel and Permalloy in High Frequency Electromagnetic Fields.—E. M. Guyer, p. 297.
- Hydrogenised Iron of High Permeability.—P. P. Cioffi, p. 297.
- Permeability of Iron at Ultra-High Frequencies.—Schwarz, p. 477.
- The Photoelectric Recorder [for Electrical Indicating Instruments requiring Small Energy Input].—C. W. La Pierre, p. 295.
- The Variation with Temperature of Photographic Processes [for Light, X- and Alpha-Rays].—J. Eggert and F. Luft, p. 238.
- Photographic Plates for Use in Spectroscopy and Astronomy.—C. E. K. Mees: Eastman Kodak Company, pp. 238 and 418.
- A Special Planimeter for Measuring R.M.S. Values.—H. Adler, p. 110.
- [Transmitter] D.C. Plate Supply from Ford Spark Coils.—V. Davis, p. 597.
- A Preliminary Communication on Ferromagnetic Platinum-Chromium and Platinum-Iridium Alloys.—E. Friederick, p. 297.
- VDE Requirements for Wall Plugs and Sockets, and Methods of Testing, p. 656.
- A Combination of Bridge and Potentiometer, and Its Advantages as a Potential Divider.—E. Denina, p. 110.
- The Calculation of a Mains Unit stabilised by the Glow-Discharge Potential Divider, for a Given Current Output.—L. Körös and R. Seidelbach, p. 596.
- The Basis of Current Sources "Stabilised" by the Glow-Discharge Potential Divider.—L. Körös and R. Seidelbach, p. 655.
- A Precision Potentiometer of Improved Design [Low-Resistance Type without Slide-Wire, Effect of Contact Resistance Negligible].—F. C. Bobier and L. O'Bryan, p. 420.
- The New Brown Potentiometer Recorder.—T. R. Harrison, p. 110.
- Multi-Ply Presspapers: Processes of Manufacture.—A. R. Duntton, p. 599.
- The Prism Derivator.—E. von Harbou, p. 656.
- A Prismatic Derivator.—E. von Harbou, p. 111.
- The Tangent Plate, an Auxiliary to the Prismatic Derivator. Graphical Differentiation with Prismatic Derivator and Tangent Plate.—J. Picht: von Harbou, p. 656.
- The Diffusion Air Pump using Oil [with Low Vapour Pressure: a New Design giving Fractional Distillation during the Working of the Pump Itself, by Adjustment of the Three Water Jackets].—W. Gaede, p. 418.
- Speed, Speed Factor and Power Input of Different Designs of Diffusion Pumps, and Remark on Measurements of Speed.—T. L. Ho, p. 537.
- Time-Pressure Characteristics of Various Diffusion and Molecular [Vacuum] Pumps.—P. J. Mills, p. 537.
- The Use of Organic Substances in High Vacuum Technique, particularly in the Working of High Vacuum Pumps.—M. von Brandenstein and H. Klumb, p. 537.
- Radio-frequency Filament Supply.—Möckel, p. 177.
- Radio-frequency Plate and Filament Supply for Receivers.—Edelstein, p. 107.
- A New Type of Radiometer [using the Condenser Ultra-Micrometer Principle].—A. L. M. Dunge, p. 297.
- A Radiometer Sensitive to Hertzian Waves [and Useful in Exploring Electromagnetic Fields].—G. A. Beauvais, p. 474.
- The Calculation of Reactance Coils with Open Iron Cores.—H. Buchholz, p. 477.
- Apparatus for Automatically Recording the Rate of Variation of a Slowly Varying Physical Quantity.—G. Aprile, p. 420.
- Contribution to the Theory of Rectification.—Y. Rocard, p. 296.
- A Note on the Theory of Rectification.—A. H. Wilson, p. 597.
- Photoelectricity and Rectification, Papers on.—Brazzoduro: Deaglio, p. 592.
- Current Rectification at Metal Contacts.—S. P. Chakravarti and S. R. Kantebet, p. 654.
- Rectifier Valve with Indirectly Heated Cathode at Full Mains Voltage ["Ostar"].—H. Olvenstedt, p. 296.
- The Use of the New High-Voltage Rectifier Valves on 220-Volt Mains, p. 419.
- Rectifier Valves working off Full Mains Voltage (200 v A.C. Mains).—G. Ganz Company, p. 296.
- The Design of Power Rectifier Circuits: Applications of Mercury Vapour or Thermionic Valves.—D. McDonald, p. 108.
- The Design of Power Rectifier Circuits.—M. V. Callendar: McDonald, p. 296.
- Micrographic Investigation of the "Kuprox" Rectifier.—M. Torres, p. 296.
- Various Dry-Plate Rectifier Patents, p. 597.
- The Jet Wave Rectifier.—J. Hartmann, p. 478.
- A New Arc-in-Air Rectifier for Very High Voltages and Powers.—E. Marx, p. 597.
- Comparison between Crystal, Copper-Oxide, and Electrolytic Aluminium Rectifiers.—A. Stefanni, p. 108.
- Engineering Features of Gas Filled [Rectifier] Tubes.—Steiner, Gable and Maser, p. 597.
- Investigations on the Influence of the Electron Emission at the Anode on the Occurrence of Back Discharges in the Mercury Vapour Rectifier.—E. Kobel, p. 597.
- Researches on the Influence of the Mercury Vapour Density in the Anode Space on the Voltage Drop in Mercury Vapour Arc [Rectifiers].—E. Kobel, p. 654.
- The Use of Hot-Cathode Rectifiers in Various Connections.—K. Meyer, p. 654.
- A Method of Eliminating Pulsations in the Terminal Voltage of Mercury Arc Rectifiers [Use of a Special Single-Phase Three-Winding Compensating Transformer].—K. Ohsumi, p. 419.
- The Advantages and Disadvantages of the Various Methods of Connecting-Up a Number of Rectifiers: and a Suggested Nomenclature.—J. G. W. Mulder, p. 419.
- The Advantages of the Nickel-Band Cathode in Rectifiers.—Telefunken Company, p. 359.
- Papers on Mercury Arc Rectifiers.—Hull and Brown: Slepian and Ludwig: De Bleuex, p. 108.
- New Designs in High Power Mercury Vapour Rectifiers and their Physical Bases.—M. Wellauer, p. 296.
- Glass Bulb Rectifiers: Their Life, Efficiency and Special Advantages.—A. M. Browne, p. 238.
- Gas-filled Hot-Cathode Rectifiers—Part I.—A. Gehrts, p. 597.
- New Applications of the High-Power Mercury Vapour Rectifier with Grid Control.—E. Kern, p. 108.
- Characteristics of a [Grid Controlled] Mercury Vapour [Rectifier] Tube.—A. C. Seletzky and S. T. Shevki, p. 598.

- New Applications of High-Power Mercury Vapour Rectifiers with Grids to Voltage and Power Regulation.—M. Schenkel and J. von Issendorff, p. 108.
- The Fundamental Technical Principles and the Applications of Rectifiers and Inverters with Grids.—M. Schenkel, p. 597.
- Capabilities of Mercury Arc Rectifiers and Mercury Arc Valves with Controlled Grids.—Brown Boveri Company, p. 238.
- Grid-Controlled Mercury-Arc Rectifiers.—H. D. Brown, p. 654.
- Current Directors: the Use of Controlled Gas Discharges: Rectifiers, Inverters, etc.—H. Laub, p. 597; see also Relays (Lewer).
- Pulsation in Valve Rectifiers [Investigation of Simple Theoretical Formula].—H. Bockels, p. 238.
- Rectifiers.—See also Aluminium, Attenuating, Barrier, Copper Oxide, Crystals, Detector, Discharge, Electrolytic, Selenium, Thyatron.
- Improving the Regulation of a Motor-Generator.—R. A. Fereday, p. 107.
- Improvements in the Gradual Regulation of Alternating Currents, p. 655.
- Symmetrical Relaxation Oscillations [with a Two-Triode Circuit] and their Synchronisation.—Hollmann: Frühauf, p. 45.
- A [Copper-Oxide] Photoelectric Relay for [Mirror] Galvanometer Measurements.—A. V. Hill, p. 110.
- The Use of the Turner Kallitron Circuit as a Trip Relay.—Hollmann and Schultes, p. 107.
- A Simple Pulse Generator for [Control by] Single and Periodic Phenomena [Dynatron Trip Relay Circuit for Use with C.-R. Oscillograph, etc.]—W. Fucks, p. 106.
- Relay working off A.C. and supplying D.C.—Ducrot, p. 110.
- Tuned Selective Relay on Ferrari Rotating Disc Principle.—Landis and Gyr, p. 598.
- A Mechanically Controlled Bolometer and Its Use as a Highly Sensitive Quantitative Relay and as a Quantitative D.C. Amplifier.—H. Sell, p. 535.
- A New Galvanometer-Relay [using an Ultra-Micrometer Device].—S. Reich, p. 109.
- Some Developments in Telegraph Technique as applied to Radio Circuits [including a Self-Restoring Valve Trigger-Effect Relay].—H. Faulkner and G. T. Evans, p. 656.
- The Gulstad Vibrating Relay Circuit as an Application of the "Mitnahme" [Pull-In] Effect.—H. Salinger and A. F. Schönau, p. 237.
- Non-linear Circuits for Relay Applications [particularly Saturable Core Reactor Circuits].—C. G. Suits, p. 236.
- A Vacuum Tube Relay and Race Timer.—W. M. Roberds: Speakman, p. 109.
- Gasfilled Relays. Part I.—Theory and Design.—S. K. Lewer and C. R. Dunham, p. 417.
- The Combined Working of Valve- and Magnetic Relays.—H. Strohmeyer, p. 417.
- Investigations into the Response Times of Relays.—J. Rybner, p. 237.
- An Apparatus [Opposed Condenser Discharge Method] for Measuring the Operating Time of Electromagnetic Relays.—V. I. Kovalenkov, M. V. Raskin and M. F. Nečtajlo-Andrejko, p. 295.
- Two Billion Ohms Resistance [Glass Rod Helix surrounding Straight Carbon Rod and sputtered with Thin Film of Carbon], p. 359.
- A Grid Resistance of 10^{11} Ohms, of Manganese Dioxide and Aluminum made into a Cement with Water Glass.—D. R. Morey, p. 297.
- A Spark Method of Measuring High Resistance [of the order of 10^8 ohm].—J. A. C. Tegan, p. 110.
- On the Measurement of High Resistance by the Bridge Method.—J. A. C. Tegan, p. 110.
- An Improved High Resistance Unit [from a few to several hundred thousand Megohms].—K. C. Rentschler and D. E. Henry, p. 297.
- Cathode Ray Oscillograph Methods for Measuring Resistance Changes during Short Voltage Impulses. Investigation of Solid Semi-Conductors.—W. Fucks, p. 418.
- [Non-Inductive, Non-Capacitive] "Silko" Wire Resistances in Ribbon Form, p. 110.
- Lamp Resistances for D.C. Receivers.—F. E. Henderson, p. 477.
- Investigations of the Electrical Conductivity of Thin Metallic Layers [Application to the Production of High Resistances].—G. Braunsfurth, p. 110.
- High Resistances Made from Metallic Oxides.—E. R. Mann and D. R. Morey, p. 51.
- The High Ohmic Resistances of the Hochohm Company, Berlin, p. 655.
- The Design of Liquid Resistances, taking into account the Wehnelt Effect.—G. Becker, p. 420.
- Composition Type Resistors for Radio Receivers [Faults, Requirements and Tests].—L. Podolsky, p. 298.
- The Evolution of Resistors used in Radio [Compression-type and Wire-wound].—H. G. Cisin: Clarostat Company, p. 298.
- Electrolytic Resistors of High Resistance.—H. L. White and E. A. Van Atta, p. 476.
- A Note on a Mercury Rheostat.—W. B. Mann, p. 177.
- Frequency Multiplication by the Use of a Rochelle Salt Condenser.—V. Wologdin, p. 294.
- Dielectric Losses in Rocksalt.—P. L. Bayley, p. 476.
- Dielectric Loss and Relaxation Time in Rosin.—J. B. Whitehead, p. 298.
- Electrical Properties of Stretched Rubber.—A. Gemant, p. 298.
- A Method for the Purification of Rubber and Properties of the Purified Rubber.—A. T. McPherson, p. 599.
- Rubber Substitute unaffected by Solvents [Thiokol], p. 655.
- The Shielding Action of Metallic Screens against Alternating Magnetic Fields.—H. Kaden, p. 654; see also Shielding.
- The Selenium Rectifier [A Survey].—E. Presser, p. 419.
- Progress in the Construction of Selenium Rectifiers.—S. German Apparatus Works, p. 359.
- Contact Rectifiers [Experimental Comparison of Copper-Oxide and Selenium Rectifiers: and the Advantages of the Latter].—G. S. Altmann, p. 654.
- Selenium.—See also under "Phototelegraphy and Television."
- Conductivity Measurements on [Semi-Conducting] Powders.—Guillery, p. 236.
- Electrical and Optical Behaviour of Semi-Conductors. IV. On Surface Charges on Semi-Conductors in Vacuo.—W. Leo, p. 108.
- The Theory of Electronic Semi-Conductors.—A. H. Wilson, p. 108.
- Papers on the Electrical and Optical Behaviour of Semi-Conductors.—A. Vökl: P. Guillery, p. 597.
- Shielding of an Electrode from a High Potential Gradient by means of a Charged Dielectric.—C. M. Slack, p. 476.
- Shielding for Electric Circuits.—J. G. Ferguson, p. 110; see also Screens.
- The Electro-Optical Shutter—Its Theory and Technique.—F. G. Dunnington, p. 111.
- Operating Characteristics of the Electro-Optical Shutter.—H. W. Washburn, p. 295.
- Aspects of Standard-Signal Generator Design.—J. D. Crawford, p. 359.
- A Machine for the Graphical Study of the Composition of Simple Harmonic Motions.—T. Solter, p. 598.
- Skin Effect Curves.—G. B. Robinson, p. 298; see also Stroboscopic.
- An "Exponential" Slide Rule.—L. B. Sklar, p. 656.
- The Suppression of Ripple in Direct Currents [Design Calculations of Smoothing Circuits for D.C. from Dynamos].—F. Weichart, p. 107.
- A Solder for Aluminium (Alumaweld), p. 359.
- Cathode Sputtering—a Commercial Application [to Covering Microphone Diagrams with Gold Electrode Surfaces].—H. F. Fruth, p. 478.
- Factors of Reflection and Transmission of Certain Metals deposited by Cathode Sputtering.—A. de Gramont, p. 297.
- A New Charging Rod for Static Electricity [Mercury in Evacuated Glass Tube].—J. I. Hopfield, p. 177.
- Steel-Copper Alloys for Dynamos and Transformers.—Kussmann, Scharnow and Messkin, p. 359.
- The Stroboglow [Grid-Glow Tube Stroboscope].—L. R. Quarles, p. 295.
- The "Stroboglow," a Portable Stroboscope.—W. E. Bahls and D. D. Knowles, p. 598.
- Stroboscopic Device for Use with the Oscillograph and its Application to the Investigation of the Skin Effect.—A. Moskwittin, p. 107.
- A Method of High-Frequency Stroboscopy for Observance of Density Changes within a Vibrating Quartz Crystal.—J. A. Strong, p. 239.
- Phosphorescent Sulphides: the Intervention of Collisions of the Second Type.—M. Curie, p. 476.
- The Dielectric Constant of Liquid Sulphur.—H. J. Curtis, p. 655.
- Surges and the Cathode-Ray Oscillograph.—S. Teszner, p. 238.
- A New Sweep-Circuit Device for the Cathode-Ray Oscillograph [giving Saw-Tooth Waves up to 50 kc/s and probably over].—G. S. Field, p. 653.
- Over-Voltages at "Break" in Small Vacuum Switches.—E. O. Seitz, p. 110.
- Vacuum Switches [Breaking in Vacua of 10^{-4} to 10^{-6} mm Hg].—K. A. Wiedemann, p. 237.
- The Eddy Current Delay of Magnetic Switching Processes [e.g., in Relays].—W. Wolman and H. Kaden, p. 656.
- The Synchronisation of D.C. Motors by means of Contact Discs.—W. Bussmann: Steage, p. 538.
- Small Synchronous Motors: Improvement due to Grooves in Auxiliary Pole-Pieces.—Siemens and Halske Company, p. 655.
- An Apparatus for the Automatic Recording of Very Small Temperature Changes over a Wide Range [suitable for H.F. Calorimetry: Temperature Changes down to $1/10$ 000°C].—H. Rieche, p. 599.
- Automatic Temperature Control [to within 0.001°C] by Resistance Thermometer, Mirror Galvanometer and Optical Relay.—H. Moser, p. 656.
- An Improved Constant Temperature Device.—L. M. Pidgeon and A. C. Egerton, p. 108.
- Temperature Regulator maintaining a Furnace at 1000° C. with a Constancy of 0.2%.—H. Rechenberg, p. 108.
- Automatic Temperature Regulator [using Thermo-Junction and Galvanometer with Periodic Contacting], p. 656.
- Temperature Regulator for Electrical Resistance Furnaces.—R. F. Proctor and R. W. Douglas, p. 656.
- Tellurium-Bismuth Vacuum Thermocouple.—C. H. Cartwright, p. 297.
- Thermocouples of Longitudinally and Transversely Magnetised Wires.—C. W. Heaps, p. 110.

- Thermocouples** Whose Elements are Longitudinally and Transversely Magnetised Ferromagnetic Substances.—S. Seass, p. 110. Some Properties of Vacuum Thermocouples [Contact and Non-Contact Types].—J. Jaffray, pp. 110 and 297.
- A Quantitative Thermoelectric Magnifier for Optical Pointers.—J. H. Jeffree, p. 656.
- Construction of Thermo-elements by Electro-deposition.—H. Kersten and R. Schaffert, p. 598.
- Tellurium Thermo-elements.—B. Lange and W. Heller: M. A. Lewitsky and M. A. Lukomsky, p. 239.
- The Production of Sensitive Vacuum Thermo-elements and Vacuum Thermo-relays by Cathode Sputtering.—Z. Klemensiewicz and Z. Wasowicz, p. 109.
- A Precision Thermo-junction Needle.—R. W. Brown, p. 598.
- Notes on Radiation Thermopiles.—J. Strong, p. 297.
- Construction of Thermo-relay Amplifiers [for Increasing the Scale Distance of a Mirror Instrument without Loss of Resolving Power].—C. H. Cartwright, p. 598.
- Thermotat Heating Current Stabilised against Mains Fluctuations.—H. Abraham, p. 239.
- A Sensitive Flexible Thermostat [using Photoelectric Cell as Link between Galvanometer and Heating Current].—J. R. Roebuck, p. 295.
- S.F.R. Precision Thermostat for Piezoelectric Oscillators.—Soc. S.F.R., p. 108.
- A Precision Thermostat for Temperatures from 25°C. to 500°C.—J. A. Beattie, p. 51.
- A Resistance Thermostat with Light-sensitive Cell [Radiovisor Selenium Bridge] Operation.—E. J. C. Dixon, p. 359.
- A Sensitive Bimetallic Strip Temperature Regulator for Thermostats.—L. Dubar, p. 51.
- Diffraction of Electrons by Thin Films of Nickel and Copper Oxides.—Darbyshire, p. 421.
- On the Crystalline Structure of Thin Layers of Metals.—Debinska, p. 293.
- Notes on the Evaporation of Ag, Be, Cr, and Si [Deposition of Thin Metallic Films].—C. H. Cartwright, p. 598.
- Magnetic Properties of Thin Metallic Films [Iron and Nickel].—W. Elenbaas, p. 654.
- Investigations on the Specific Resistance of Thin Metallic Layers, especially of Silver and Tungsten.—L. Hamburger and W. Reinders, p. 297.
- D.C. [Thyratron] Inverter for Radio Receivers.—W. R. G. Baker and J. I. Cornell, p. 108.
- A Thyratron "Scale of Two" Automatic Counter.—C. E. Wynn-Williams, p. 535.
- A Self-Stopping D.C. Thyratron Circuit [using a Glow-Discharge Tube].—H. J. Reich, p. 176.
- Hot Cathode Thyratrons [including the Use of Indirectly Heated, Heat-Shielded Cathodes].—L. J. Davies, p. 359.
- Thyratrons.—See also Rectifiers, Relays, Voltage, and under "Valves and Thermionics."
- A Method of Obtaining a Linear Time Axis for a Cathode Ray Oscillograph.—A. L. Samuel, p. 107.
- Thyratron Linear Time Axis for Cathode-Ray Oscillograph.—H. Neustadt: Nottingham, p. 475.
- Cathode-Ray Oscillograph Time Axis [Neon Tube, Indirectly-Heated Tetrode and Transformer Circuit].—F. T. Brewer, p. 176.
- A New Type of Time Base for the Cathode-Ray Oscillograph [for Frequencies up to 10⁷ Cycles/Sec. and Over].—G. Ulbricht, p. 417.
- Dissymmetrical Two-Valve Multibrator Circuits [for Linear Time Base, etc.].—Vecchiacchi, p. 358.
- A Time Base for the Cathode-Ray Oscillography of Irregularly Recurring Phenomena.—G. I. Finch, R. W. Sutton and A. E. Tooke, p. 50.
- A Circular Time Base giving Radial Deflections, for use with the Cathode Ray Oscillograph.—Staff of Radio Research Station, Slough, p. 535.
- A Method of Radial Deflection in the Cathode-Ray Oscillograph [Circular Time Base with Radial Deflection].—G. Goubau, p. 596.
- Investigation of Time Base Release in the Cathode Ray Oscillograph by Involuntary Transient Phenomena.—K. Girod, p. 176.
- A Linear Time-Base Oscillator for Cathode-Ray Oscillography.—Appleton and Builder, p. 176.
- The [Thun] Time Extender with Mechanical Light Regulation as an Auxiliary in Technical-Physical Research [High-Speed Cinematography].—W. von Ohnesorge: Thun, p. 598.
- An Electric Time Marker for Self-Recording Instruments.—L. H. G. Dines, p. 51.
- The Self-Regulating Static Transformer giving a Constant Value of Current.—F. Correggiari, p. 477.
- A Mechanically Resonant [Audio-frequency] Transformer.—Ross Gunn, p. 357.
- The Transformer with Evolute Core.—R. Edler: Vidmar: Zopp, p. 598.
- The Theory of the Transformer.—H. Barkhausen, p. 110.
- A Direct Method of Measuring the Leakage Field of a Transformer [Neutralisation of Main Field].—Brückmann and Engelenburg, p. 177.
- The Tesla Transformer as a High Frequency Test Generator and Its Investigation with the Cathode-Ray Oscillograph.—P. Hochhäusler, p. 654.
- Transformer Equipment for Large Experimental Radiotelephone Transmitter [Long-Wave Transoceanic].**—W. R. Lyon, p. 654.
- The Calculation of Leakage in Auto-Transformers.—R. Gürtler, p. 236.
- Determination of the Constants of Low-Damping Transformers [Graphical Method].—P. Oehlen, p. 296.
- Production Testing of Small Power Transformers.—R. M. Hukle, p. 597.
- Intermediate Frequency Transformers.—Cost versus Quality.—C. C. Henry and R. E. Stemm, p. 420.
- Charts for [Telephone or Radio] Transmission Line Problems.—H. E. Hertig, p. 296.
- A Trip Circuit for Nerve Excitation [for C.-R. Oscillographic Recording].—H. König, p. 536.
- A Trip Relay with Very Short Response Time, for C.-R. Oscillographs.—M. Knoll and M. Freundlich, p. 596.
- Electric Coil Turn-Counter.—B. M. Smith, p. 420; see also Number.
- A Greaseless and Chemically Inert Valve for High Vacuum [Silver Bellows and Seating of Fused Silver Chloride].—H. C. Ramsperger, p. 107.
- A Pressure Reducing Valve for Vacuum Apparatus.—W. Klose, p. 107.
- A Device for Controlling the Flow of Gas into a Vacuum System [Introducing a Piece of Wire into Rubber Tubing before applying Pinch Clamp].—H. P. Knauss, p. 107.
- High Vacuum Pressure Control Apparatus [Galvanometer Contact controlling Mercury Valve through Valve Amplifier].—T. L. Ho, p. 50.
- A New High Vacuum System.—J. A. Becker and E. K. Jaycox, p. 238.
- Sources of Error in Vacuum Measurements with a Mercury Vapour Condensing Trap.—M. Rusch and O. Bunge, p. 295.
- An Improved Cut-Off for High Vacuum Work.—R. W. Ditchburn, p. 107.
- Vapour-Pressure Tests on Greases for High Vacuum Work, by a Thermionic Method.—W. Espe and I. Kroczek, p. 653.
- The Use of Glycol-Phthalic Anhydride Resin as a High-Vacuum Cement.—T. P. Sager and R. G. Kennedy, Jr., p. 295.
- A Valve for the Introduction of Small Quantities of Gas [Capillary Tube closed by Rubber Pad on Bimetallic Strip, Electrically Heated].—K. Becker and M. Pirani, p. 418.
- A New Vibration-free Mounting for Measuring Instruments.—R. Müller, p. 51.
- Note on Julius [Anti-Vibration] Suspensions.—M. J. Brevoort, p. 51.
- Automatic Voltage Control by means of a Photoelectric Cell.—H. T. Clark and W. Kohlhaagen, p. 295.
- The Use of a Thermionic Tetrode for Voltage Control.—J. C. Street and T. H. Johnson, p. 653.
- A New Voltage Quadrupler.—W. W. Garstang, p. 358.
- Voltage-Regulating Auto-Transformer.—F. Bedell and J. Kuhn, p. 295.
- Improving the Voltage Regulation of Rectifier-Filter Systems: Two Novel Schemes [Voltage-Regulating Input Choke and Voltage Regulating Transformer] for Reducing Plate Voltage Variation with Change in Load.—E. Glaser, p. 107.
- Automatic Voltage Regulation [Voltage Regulator Transformer].—K. Howe: Ward Leonard Company, p. 478.
- The "Isovolt" Voltage Regulator.—H. André, p. 420.
- A Thyratron Voltage Regulator.—C. E. Weinland, pp. 295 and 420.
- A Corona Tube Voltage Regulator [regulating the Output of a Full-Wave Rectifier and thus controlling the Excitation of a Generator].—H. W. Dodge and C. H. Willis, p. 359.
- The Philips Triode Voltage Regulator [for D.C. and A.C. Generators].—N. A. J. Voorhoeve and F. H. de Jong, p. 538.
- A Voltage Regulator for Furnace Control [Mercury Thermometer Relays giving constant R.M.S. Voltage in Heating Circuit].—V. H. Stott, p. 108.
- Battery Voltage Regulator [Periodic Connection through Condenser to a Second, Constant Voltage Battery].—p. 655.

STATIONS, DESIGN AND OPERATION.

- The Cape Air Route: Experiments with Short Wave Wireless, p. 478.
- Radio Communication on the International [Pan American] Air Lines.—H. C. Leuteritz, p. 299.
- Wavelengths for Aircraft Communication.—C. B. Carr, p. 299.
- Long-Wave Communication for Aircraft.—F. Eisner, p. 656.
- The Position of Broadcasting Technique in America and Germany [A Comparison].—W. Reichardt, p. 538.
- The Austrian Broadcasting Network.—G. Schwaiger and others, p. 111.
- The Beelitz Overseas Receiving Station.—H. Mögel, p. 539.
- The Broadcast Installations in the New "House of Radio," Berlin.—G. Lubszynski and K. Hoffmann, p. 111.
- The New High Power Broadcast Station at Beromünster, Canton Lucerne.—H. A. Ewen, p. 421.
- Radio Broadcast from Fast Bobsled [3rd Olympic Winter Games], p. 299.
- Lining Up Broadcasting Circuits [and a Criticism of the C.C.I. Decisions].—E. K. Sandeman, p. 299.

- Broadcasting House, London, p. 478.**
Broadcasting over Lines.—See Land Line, Light, Lighting and Power, Telephone, Wired.
Broadcast Channels for Canada, p. 599.
Probable Future Increase in Available Radio Channels [from 2 240 to 3 022 in 5 Years' Time].—S. R. Winters: Bureau of Standards, p. 299.
The Menace to Broadcasting: "Clear Channels" [for Rural Listeners: worked by only One High-Power Station] being Destroyed under Pressure of Political Expediency, p. 599.
Coastal Wireless: Radio Telephone Apparatus to be Installed at Eight More Stations.—Marconi Company, p. 600.
The Coltano Radio Station, p. 478.
Commercial Wireless.—Chetwode Crawley, p. 178.
Some Developments in Common-Frequency Broadcasting.—G. D. Gillett, p. 111.
Contribution to the Theory of Interference Zones in Common-Wave Transmission.—Hübner, p. 517.
Common-Wave or -Frequency Broadcasting.—See also Parallel, Shared, Synchronisation.
Modulation Meters and Indicators for Broadcasting Control Rooms.—G. Lubszynski and H. Weight, p. 240.
Piping System for Power Tube Cooling Water at Radio Station KDKA.—E. M. Sollie, p. 299.
Broadcast Station Coverage [and its Estimation].—Westinghouse Company, p. 52.
Broadcast Station Coverage Surveys.—V. V. Gunsolley, p. 239.
On the Use of Field Intensity Measurements for the Determination of Broadcast Station Coverage.—C. M. Jansky, Jr., and S. L. Bailey, p. 240.
From Croydon to the Cape.—R. F. Durrant, p. 657.
A Visit to the New Installations of the Eiffel Tower Radio Station.—J. P. Delatour, p. 599.
Prevention of Fading in Broadcasting by Use of Aerial System of Ordinary Height and Great Horizontal Spread.—Horbich and Hahnemann, p. 177.
Measurements in the Near Field of a Broadcasting Station [at Base: and the Effects of Houses, Aerials, etc.].—H. Zickendracht, p. 239.
Field Strength Chart of the Buda Pesth High-Power Broadcasting Station.—S. Baczynski, p. 111.
Field Strength Chart of the Norrköping Relay Station.—S. Lemoine, p. 111.
Field Strengths.—See also Coverage.
The Marconi System for Distant Control by Wireless of Fog Signals [working between Light Vessels in Thames Estuary], p. 600.
Radio Sets in the Forest Service [for Fire Fighters], pp. 360 and 659.
The French Colonial Broadcasting Services.—M. Adam, p. 111.
French Broadcasting's Gigantic Construction Programme, p. 178.
The New French Broadcasting Network, p. 538.
Radio Installations in the French Colonies.—H. Staut, p. 111.
Present Position of Organisation of the International Control of Frequencies: the U.S.A. Control Organisation, p. 599.
Frequencies of European Broadcasting Stations measured at the Brussels Laboratory of the U.I.R., p. 657.
Type Testing of Frequency-Checking Apparatus for Broadcasting Stations.—Bureau of Standards, p. 360.
Frequency Control Monitor for Broadcast Stations.—Western Electric Company, p. 599.
Frequency Deviation Tolerance at Broadcast Stations [the New 50 Cycle Tolerance], p. 599.
A Frequency Indicator for [Broadcasting] Transmitters, p. 343.
Government-Owned Radio Broadcasting is Out [Federal Radio Commission's Report to U.S.A. Senate], p. 599.
The Heilsberg High Power Broadcasting Station, East Prussia.—H. Schumacher, p. 299.
Communications in India—Future Control of Telegraphs, Telephones and Radio, p. 539.
Radio Interference, p. 52.
Propagation of the Broadcasting Waves [345-441 Metres] in Japan.—Takata and Itow, p. 156.
Standard Broadcasting Land-Line Equipment.—A. R. A. Rendall and J. S. Lyall, p. 657.
Swiss Land-Line Radio, p. 299.
League of Nations Radio: Some Particulars of the Transmitting and Receiving Stations at Geneva, p. 360.
Broadcasting Distribution and the Electric Light Network.—Philips Company, p. 421.
Feasibility of Broadcasting with Carrier Current applied to Lighting and Power Lines.—I. Tanimura, p. 360.
New Methods for the Measurement of Modulation Ratio [using Critical Voltage of a Neon Tube].—A. L. Minz, p. 600.
Recording of Modulation Level of a Broadcast System.—H. L. Kirke, p. 538.
The Modulation System of the Russian 100 kw. Station at Schtschelkowo.—Wigge, p. 162.
The Radio [Frequency] Monitoring Station at Grand Island, Nebraska, p. 299.
Multiplex Transmission and Secret Radio-telephony.—Chireix: Villem, p. 405.
Circuit Matching in Networks for Radio Distribution [to Loud Speakers].—Jhr. W. Six and R. Vermeulen, p. 299.
Simple Telephone Broadcasting Networks.—A. D. Apanasenko, p. 360.
New Overseas Radio-Telephone Extensions.—A. A. Oswald, p. 178.
The Parallel Working of Radio Broadcast Stations.—S. I. Panflov, p. 599.
The New "Radio-Vitus" Broadcasting Station [near Paris], p. 111.
The New Broadcasting Station Radio Paris [at Saint Rémy l'Honoré].—H. Staut, p. 299.
New Broadcasting Station ("Parisian Station") of the Compagnie Générale d'Énergie Radioélectrique, p. 421.
The New Broadcasting Centre, the "Poste Parisien," of the Compagnie Générale d'Énergie Radioélectrique.—Le Duc and Sallard, p. 599.
The New [High Power] Broadcasting Station "Poste Parisien," p. 538.
Paris.—See also Saint Rémy.
Wireless Communication in the Polar Regions [and the Causes of its Difficulties].—Krüger, p. 334.
Paperson Police Radio Signalling Systems.—Dunsheath: Kavanagh: Lampkin, p. 299.
Radio to the Rescue [Police Radio, especially De Forest Radio Police System in Los Angeles].—W. J. Barkley, p. 111.
Polish National Broadcasting, p. 599.
The Pontoise Radiotelegraph Station.—V. Vigneron, p. 111.
The Pontoise Radiotelegraph Station.—Veaux, p. 177.
The New Radioelectric Stations of Pontoise and Noiseau.—E. Picault, p. 360.
Power Equipment at KDKA's New Station.—R. L. Davis, p. 111.
Prague Broadcasting Station, p. 111.
The Prague High-Power Broadcasting Equipment.—D. B. Mirk, p. 299.
The Prague [Cesky-Brod] High-Power Broadcasting Station.—Strong, Mirk and Gallant, p. 478.
Application of Printing Telegraph to Long-Wave Radio Circuits.—A. Bailey and T. A. McCann, pp. 111 and 178.
European Broadcast Programme Exchange [with Some Statistics].—H. Antoine, p. 478.
The Communication System of the Radiomarine Corporation of America.—I. F. Byrnes, p. 360.
Radiotelephone Service is Expanding [Survey including Some Details of the New Service California-Hawaii].—J. J. Pilliod, p. 52.
Radiotelephone Experiments over Short Distances [Linking Isolated Settlements, etc., in B.C. and Alaska: Wavelengths 50 to 200 Metres].—C. H. McLean, p. 600.
Distance Ranges of Radio Waves.—Dellinger, p. 398.
Relay Broadcast Transmitter, Type BR.1A [for Sweden], p. 111.
Medium Wave Receiver for Broadcasting Relay, p. 657.
Remote Control of Broadcast Programmes.—G. W. Haug, p. 599.
Broadcast Repeaters: A Discussion of the Requirements of Line-Amplifiers used for Programme Transmission over Broadcasting Land Lines.—Vogel, p. 177.
Broadcasting in Russia: Organisation and the Five-Year Plan.—G. E. Roth, p. 240.
The New Russian Radio "Five-Year Plan," p. 178.
New Russian "Five-Year Plan."—Wigge, p. 178.
New Broadcasting Station of the Compagnie Française de Radiophonie at Saint Rémy [and the Use of the "De-phasing" System of Modulation], p. 111.
The New Radio Station at Saint-Rémy l'Honoré (the New Radio Paris).—M. Adam, p. 299.
Scottish Regional Station [at Westerglen], p. 478.
Wireless at Sea, p. 178.
Interference Effects with Shared-Frequency Broadcasting.—C. B. Aiken, p. 111.
Operation of a Ship-Shore Radiotelephony System [North Atlantic Service].—C. N. Anderson and I. E. Lattimer, p. 359.
Ship to Shore Telephone Installation on the s.s. Empress of Britain.—Marconi Company, p. 111.
Radiotelephony Communication with Ships [including R.M.S. Olympic Installation].—F. de Fremery, p. 539.
Short-Wave Broadcasting Stations of the World [List and Map], p. 111.
Short-Wave Beam Broadcasting from Spain to America, p. 599.
Simultaneous Telegraphy and Telephony on Short-Wave Circuits.—D. Thierbach, p. 538.
Single Wavelength System [of Duplex Radiotelephony, on the "Olympic."].—I. T. and T. Company, p. 178.
The "Spread Side-Band" System for Short-Wave Telephony Communications [Madrid-Buenos Aires Services].—L. T. Hinton, p. 657.
Empirical Standards [of Reception, Interference and Service Area] for Broadcast Allocation.—A. D. Ring, p. 421.
The New Swiss Broadcasting Station [Sottens, near Lausanne]: The Swiss Broadcast Network.—F. C. McLean: A. Muri, p. 657.
Broadcasting in Switzerland, p. 111.
A New Broadcasting Station in Switzerland, p. 421.
Synchronisation of Westinghouse Radio Stations WBZ and WBZA.—S. D. Gregory: Westinghouse Company, p. 111.
New Possibilities in Broadcast Reception [Distribution over Telephone Network or Special Lines, in Switzerland], p. 240.

- Broadcasting in a Train.—A. Dinsdale, p. 538.
 Ten Years of Transradio—A Retrospect.—E. Quäck, p. 240 (two).
 Optimum Tuning Conditions for High Frequency Plants [to satisfy Various Requirements].—Osnos, p. 340.
 Two-Way Radiotelephone Circuits [Connection to Land Lines: the Use of "Vodases"].—S. B. Wright and D. Mitchell, p. 600.
 Papers on Ultra-Short-Wave Broadcasting.—Schröter: Sohne-mann, p. 30.
 Broadcasting with Ultra-Short Waves.—G.W.O.H., p. 218.
 Seven-Metre [Ultra-Short-Wave] Broadcasting.—W. F. Floyd, p. 240.
 Ultra-Short-Wave Broadcasting: Unsatisfactory Results and the Need for Better Receivers.—von Ardenne, p. 657.
 Broadcasting Tests in Amsterdam on a 7.85-Metre [Ultra-Short] Wave.—P. J. H. A. Nordlohne: Philips' Company, p. 657.
 Proposed Ultra-Short-Wave Telephone Services between Hawaiian Islands, p. 51.
 Ultra-Short Wave in Hawaii Telephone Service, p. 299.
 Duplex Radio Telephony on Few Metre [Ultra-Short, 4-Metre] Waves between Ship and Shore.—S. Uda, p. 298.
 Communication Tests for Radio Telephony by means of Ultra-Short [4.6 and 5.8 Metre] Waves between Niigata and Sado.—S. Uda p. 360.
 Ultra-Short-Wave [42 Centimetre] Signalling.—Westinghouse Company, p. 360.
 Reflectors and Feeders for Ultra-Short Waves [Dover-Calais Service].—Darbord, p. 346.
 A Portable 56-Mc [Ultra-Short-Wave] Transmitter-Receiver.—F. A. Gunther, p. 600.
 Radiation of Multiple Modulated Carrier Waves due to Common Plate Battery for Transmitter and Receiver, in Ultra-Short-Wave Working (Five Metre Waves).—L. Spangenberg, p. 600.
 Ultra-Short-Waves.—See also Radiotelephone.
 Intercontinental Radiotelephone Service from the United States.—J. J. Pilliod, p. 177.
 The Vatican Short-Wave Telegraph Station.—G. Gianfranceschi, p. 111.
 The Wavelength Problem.—Noel Ashbridge, p. 599.
 The Wavelength Problem and the U.J.R.—P. Münch, p. 111.
 Wavelengths.—See also Channels.
 Weather Service for All.—T. Herbert, p. 539.
 Westinghouse Radio Station at Saxenburg, Pa. [for Broadcasting and Experimental Work].—R. L. Davis and V. E. Trouant, p. 599.
 Wired Broadcasting in Switzerland, p. 360.
 Cannot Refuse Wired Music [Decision against Refusal of New York Telephone Company to furnish Leased Lines], p. 240.
 The Present Status of Wired Wireless Broadcasting on Power Lines.—G. Squier, p. 177.
- ### GENERAL PHYSICAL ARTICLES.
- The Slowing-Down of Alpha Rays in the Air, and Bethe's Theory.—G. Mano, p. 539.
 The Motion of a Charged Particle. Part I.—C. Störmer, p. 299.
 Relativistic Theory of the Interaction of Two Charged Particles.—A. D. Fokker, p. 601.
 Classical Electrodynamics and the Conservation of Energy.—W. F. G. Swann, p. 52.
 The Nature of Electrical Contact between Metals.—T. H. Osgood and E. Hutchisson, p. 658.
 Contact Potential.—See Dielectric Constant.
 On the Nature of Electron Motion in Crystals and Its Significance in the Electrical Behaviour of Solids [including Rectifying Action].—L. Nordheim, p. 601.
 Experimental Investigations of the Current Conduction in Dielectric Fluids at High Fields.—A. Nikuradse, p. 479.
 The Breakdown of the Liquid Dielectric.—Nikuradse, p. 650.
 Conductivity of Dielectric Fluids [Summarising Report].—A. Nikuradse, p. 658.
 On the Conduction of Current in Liquid Dielectrics.—W. O. Schumann, p. 659.
 Dielectric Constant and Contact Potential.—T. Takéuchi, p. 178.
 Dielectric Constants of Aqueous Solutions.—R. Weber, p. 112.
 The Diffusion of Particles [emitted by a Reflecting Plane] taking into Account the Energy Loss.—W. de Groot, p. 112.
 On the Townsend Discharge in Heavy Mist, when Loaded with Space Charge.—W. Deutsch, p. 112.
 Is the Initial Electron in an Impulsive Discharge Set Free by Photoelectric Action?—K. Buss and K. Mosch, p. 112.
 The Breakdown Process in the Discharge across a Spark Gap.—W. Rogowski, p. 241.
 The Step-by-Step Discharge in Gases.—W. Rogowski: Krug, p. 361.
 The Step-by-Step Discharge [and Krug's Denial].—K. Buss: Rogowski, p. 421.
 Step-less and Step-by-Step Discharge in Air according to New Oscillograms.—W. Krug: Rogowski, p. 658.
 Experiments on the Glow Discharge.—G. Valle, p. 178.
 Investigation of Surface Discharge with Impulse Voltage.—Rosenlöcher, p. 220.
 The Electrodeless Discharge as Measured by the Cathode-Ray Oscillograph [Number of Initiating Electrons, etc.].—K. Buss, p. 421.
 Papers on the Electrodeless Discharge.—Tykociner: Kunz, p. 421.
 Control of the Glow Discharge on a Grid Cathode by means of a Third Electrode behind the Cathode.—Güntherschulze and Keller, p. 241.
 The High Frequency Discharge [Study of the Effect of the Distance between the Electrodes].—Gutton and Beauvais, pp. 217-218.
 The Extension of Paschen's Law to include the Electrodeless Glow Discharge.—O. Stuhlmann, Jr., 421.
 Further Experimental Data on the Electrostatic and Magnetic Components in the Electrodeless Discharge.—C. T. Knipp and V. M. Smith, p. 658.
 The Colour of the Light from High-Frequency Discharges in Helium.—J. S. Townsend, p. 112.
 Electrodeless Discharges.—J. S. Townsend, p. 658.
 Electrical Discharges in Gases at Low Pressures.—I. Langmuir, p. 658.
 Discharges Maintained by Electrical Oscillations in Solenoids.—G. D. Yarnold, p. 658.
 Electric and Magnetic Double Refraction.—J. W. Beams, p. 479.
 Sir A. S. Eddington's Recent Theories.—W. N. Bond, p. 478.
 The Kinetics of Electrode Processes. Part I.—Depolarisation Effects by Hydrogen and Oxygen at Platinum Electrodes.—J. A. V. Butler and G. Armstrong, p. 659.
 The Dispersion of Conductivity of Some Aqueous and Non-Aqueous Solutions of Electrolytes.—H. Gaertner, p. 241.
 The Theory of Electrolytic Polarisation.—H. Fricke, p. 659.
 On the Dielectric Constants of Electrolytic Solutions.—W. Orthmann, p. 112.
 On the Conductivity and Dielectric Constant of Electrolytic Solutions at High Frequency.—M. Wien, p. 241.
 On the Analogy between the Electromagnetic Field and a Fluid containing a Large Number of Vortex Elements.—J. J. Thomson, p. 112.
 A New Electron Inertia Effect and the Determination of m/e for the Free Electrons in Copper.—S. J. Barnett, p. 52.
 A New Characteristic of the Dirac Electron.—Al. Proca, p. 299.
 The Characteristic Values of the Dirac Electron.—Al. Proca, p. 479.
 The Diamagnetism of the Free Electron.—T. Takéuchi, p. 539.
 On the Canal Breadth of Electron Avalanches.—F. Ollendorff, p. 600.
 Multiple Excitation of Complex Atoms by Electron Impact.—L. Goldstein, p. 539.
 The Structure of Electron Waves.—L. Infeld, p. 600.
 The Theoretical Bases of Electrotechnics: Electronic Interpretation of Energy Exchange in Alternating Currents.—M. Boll, p. 112.
 Diffraction of Electrons by Thin Films of Nickel and Copper Oxides.—J. A. Darbyshire, p. 421.
 Diffraction of Electrons by Single Crystals: the Case of Paraffin and the Saturated Fatty Acids.—J. J. Trillat and Th. v. Hirsch, p. 658.
 The Angular Distribution in the Scattering of Slow Electrons by Gas Molecules.—C. Ramsauer and R. Kollath, p. 241.
 The Effect Produced by a Cloud of Electrons on the Structure of the de Broglie Wave.—Szczeniowski and Infeld, p. 178.
 Electrons and Light Quanta [Negative Experimental Test on Acceleration or Retardation of the Former by the Momentum of the Latter].—Ambrose Fleming, p. 478.
 Electrons in a Gravitational Field.—T. Takéuchi, p. 539.
 Electrons, Protons and the So-called Electron Magnetism.—A. Güntherschulze, p. 601.
 The Molecular Theory of Electro-Optical Phenomena.—R. de Malleman, p. 52.
 A Search for an Electrostatic Analog to the Gravitational Red Shift [Negative Results in Test for Change in Frequency of Light due to Difference in Electrostatic Potential between Source and Measuring Apparatus].—R. I. Kennedy and E. M. Thorndike, p. 112.
 Energy Fluctuations in a Radiation Field.—W. Heisenberg, p. 178.
 The Derivation of Maxwell's Equations from the Equations of the Quantum Theory.—M. Fahmy, p. 478.
 On the Equations of Laplace and Maxwell.—K. F. Herzfeld, p. 658.
 An Experiment in Support of the Hypothesis of a Time Lag in the Faraday Effect.—F. Allison and J. L. Condon, p. 600.
 The Changes in Electrical Conductivity of Ferromagnetic Substances in Magnetic Fields: Comprehensive Survey.—O. Stierstadt, p. 658.
 Ferromagnetism and Electrical Properties. 3rd Communication. The Connection between Resistance Increase and Magnetisation.—K. Schneiderhan, p. 241.
 Investigation of the Electric Field Distribution in Dielectric Liquids by means of Electrical Double Refraction—Electro-optical Kerr Effect.—J. Dantscher, p. 112.
 Electromagnetic Fields Derived from Non-Commuting Potentials.—B. Cassen, p. 112.
 Relationships between the Energy of Gamma Rays, emitted by an Atom following a Beta or Alpha Particle Emission, and the Fundamental Physical Constants.—A. Bramley, p. 52.
 Unified Theory of Gravitation and Electricity.—A. Einstein and W. Mayer, pp. 478 and 657.
 The Relationship of Gravitation and Electromagnetism.—W. A. Tripp, p. 657.

- Gravity and Electricity are merged in New Mathematics.—C. Lanczos, p. 299.
- The Hall Effect [in Tellurium] with Audio-frequency Currents.—L. A. Wood, p. 658.
- The Hall Effect in Single Bismuth Crystals.—H. Verleger, p. 658.
- Theoretical Study of Induced Currents [with an Application to Instrument Design].—M. Biot, p. 178.
- Interconversion Factors for Numbers in Energetic and Related Units.—C. H. D. Clark, p. 600.
- Papers on the Motion of a Heavy Sphere in an Ionised Electric Field.—Pauthenier and Moreau-Hanot, p. 241.
- The Probability Law governing Ionization by Electron Impact in Mercury Vapor.—C. E. Haupt, p. 112.
- Absolute Values for the Mobilities of Gaseous Ions in Pure Gases.—N. F. Bradbury, p. 360.
- The Changes which Gaseous Ions undergo with Time.—J. Zeleny, p. 361.
- A Method for Determining the Mobility of Ions of the Rare Gases by means of the Negative Layers.—M. J. Druyvesteyn, p. 361.
- The Kerr Effect in Rochelle Salt.—H. Müller, p. 241.
- The Magnetic Permeability of Space and the Theorems of M. Chipart.—J. Cayrel; Chipart, p. 657.
- Deduction of the Maxwell Equations with the aid of Eddington's Undulatory Tensor.—J. J. Placinteanu, p. 478.
- Remarks on our Paper: "Electric and Magnetic Effects on Metallic Wires Structurally Influenced by Heat, Magnetisation or Sound."—A. V. Hippel and O. Stierstadt; Supplementary Remarks by O. v. Auwers, p. 112.
- The E.M.F. of an Electrode in Motion, and the Electrokinetic Potential of Metals.—S. Procopiu, p. 52.
- On an Electromotive Force Between Two Metals in Relative Motion.—J. B. Seth, B. Gulati and S. Singh, p. 52.
- The Force Acting Between Moving Charges.—A. D. Fokker and C. J. Gorter, p. 601.
- A New Method of Producing Negative Ions.—J. S. Thompson, p. 112.
- Neutron, the Zero Element.—Swinne, p. 479.
- Theory of the Diffusion of Neutrons, Coefficient of Absorption and Ionisation.—J. L. Destouches, p. 479.
- Orientated Atoms in a Variable Magnetic Field.—E. Majorana, p. 658.
- On High Frequency Permeability. Some Remarks on the Papers of R. Michels and M. Wien.—W. Arkadiew, p. 240.
- Papers on Photochemical Processes.—Faraday Society, p. 361.
- Photoelectrons and Negative Ions.—Wellish, p. 102.
- The Photon considered as a Material Point and treated by Quantum Mechanics: The Existence of Photon Spin.—Al. Proca, p. 52.
- Plasma Oscillations and Selective Optical Reflection from Metals.—M. Steenbeck, p. 539.
- The Intermediate Free Path Case in the Theory of a Plasma.—L. Tonks, p. 600.
- Effect of Nuclear Spin on Polarisation of Radiation excited by Electron Impact.—W. G. Penney, p. 658.
- The Form of Potential Barrier at the Surfaces of Conductors.—A. T. Waterman, p. 658.
- Two Problems in Potential Theory.—T. C. Fry, p. 600.
- The Probable Values of ϵ , η , ϵ/η , and α .—R. T. Birge, p. 478.
- A Possible Explanation of the Difference in Mass between the Proton and the Electron.—Al. Proca, p. 360.
- Electrodynamics and the Theory of Quanta.—J. Solomon, p. 178.
- Quantised Singularities in the Electromagnetic Field.—P. A. M. Dirac, p. 113.
- Electrodynamic Masses in Quantistic Electrodynamics.—E. Fermi, p. 178.
- Some Difficulties of the Quantum Theory.—J. Solomon, p. 178.
- Quantum Theory of Radiation.—E. Fermi, p. 479.
- Quantum.—See also Photon.
- Radioactive Disintegration.—W. Heisenberg, p. 658.
- Electricity as a Natural Property of Riemannian Geometry.—C. Lanczos, p. 300.
- Electromagnetism as a Natural Property of Riemannian Geometry [Theoretical Investigation].—C. Lanczos, p. 300.
- On the Appearance of Vector Potential in Riemannian Geometry.—C. Lanczos, p. 479.
- A New Relation between Electrical Resistance and Energy of Magnetisation.—W. Gerlach and E. Englert, p. 52.
- Total Secondary Electron Emission from Metal Faces.—S. R. Rao, p. 658.
- Secondary Electron Emission from a Nickel Surface Produced by Positive Ions of Mercury.—R. M. Chaudhri, p. 658.
- Theory of Secondary Electron Emission from Metals.—H. Fröhlich, p. 658.
- The Emission of Secondary Electrons from Tungsten.—A. J. Ahearn, p. 241.
- Influence of the Electrical Discharge on the Secondary Emission from the Cathode.—W. J. Jackson, p. 658.
- On the Complete Differential Secondary Radiation in Air for Medium Velocity Electrons.—E. Kipphan, p. 361.
- Application of the Principles of Similarity to the Flow of Electricity in Gases.—H. Mache, p. 360.
- Sparking Potential and Electrode Material.—Loeb, p. 241.
- The Solution of Steady-State Problems in Dielectric, Magnetically Permeable, and Conducting Media, with Special Reference to Mathematical Analogies between Magnetic Problems and Current-Flow Problems.—W. F. G. Swann, p. 658.
- On a Possible Explanation of the Difference in Wavelengths of the Spectral Lines of a Given Element produced on the Sun and on the Earth.—F. Sanford, p. 52.
- A Theory of Surface Conductance at an Electrolyte-Solid Interface.—K. S. Cole, p. 659.
- Thermoelectromotive Forces Produced by a Magnetic Field.—S. R. Williams, p. 112.
- Remarks on the Variations in Electrical Behaviour of Various Substances [including Application to Thermionic Emission].—L. Hamburger, p. 299.
- Treatment by Wave Mechanics of the Problem of the Free Electron under the Simultaneous Influence of a Homogeneous Magnetic Field and a Plane Electromagnetic Wave (Compton Effect in a Magnetic Field).—F. Lüdi, p. 600.
- Liquid Currents and Space Charge round Wire Electrodes in Water.—M. Katalinic, p. 659.
- Note on "The Effect of Piezoelectric Oscillation on the Intensity of X-Ray Reflections from Quartz."—S. Nishikawa, Y. Sakisaka and I. Surnoto, p. 178.
- The Dispersion of X-Rays by Water.—E. Amaldi, p. 241.

MISCELLANEOUS.

- Abbreviation of the Titles of Technical Journals, p. 300.
- Shock Measurements [with the Langer-Thomé Acceleration Meter].—P. Langer, p. 301.
- New Algebraic Representation of Alternating Currents and of all other Oscillatory Phenomena.—A. Blondel, p. 479.
- Amateur Radio in Great Britain.—J. Claricoats, p. 601.
- Amateurs to Co-operate with H.M. Forces, p. 659.
- The Extension of Electrical Engineering Analysis through the Reduction of Computational Limitations by Mechanical Methods.—H. L. Hazen, p. 422.
- The Use of the Projection Microscope and Photoelectric Cell (Determination of Areas of Irregularly Shaped Microscopic Objects).—A. Savage and J. M. Isa, p. 242.
- Australian Radio Research Board, Report for Year ending 30th June, 1931, p. 178.
- The Concept of Beauty as related to Engineering.—A. E. Kennelly, p. 540.
- A Comparison between the Biological Effects of Short and Ultra-Short Waves.—J. Saidman, p. 113.
- Biological Effects of Gamma Rays.—W. G. Whitman and M. A. Tuve, p. 113.
- The "Photoelectrograph" Device [for the Blind], p. 242.
- The "Photoelectrograph" for the Blind.—Brachet; Thomas, p. 422.
- Reading Machines for the Blind: the Visagraph and the Photoelectrograph.—P. Henri; Naumburg; Thomas, p. 540.
- Print Reading by the Blind.—Thomas, p. 659.
- Annual Report of the Director of the Bureau of Standards, 1930-31, p. 179.
- The Pende Cardiac and Pulmonary "Teletransmitter."—G. Santucci, p. 301.
- Electro-Cardiographs Using Voltage, not Current, Indication.—H. Gabler, p. 301.
- Australian Carrier System, p. 361.
- Carrier Current.—See also High Frequency, Power T. Lines, and under "Stations, Design and Operation."
- The Use of Cable Coatings and Conductors as Capacitative Coupling for Carrier Current Working, p. 540.
- The Use of Blocking (Rejector) Circuits in Carrier Current Telegraphy or Telephony over Power Lines, p. 540.
- Carrier Current Telephony on H.T. Lines.—G. Bourelly, p. 300.
- Speed of Signal Transmission over Carrier Telegraph Channels, p. 300.
- Experimental Study of Cathode Rays Outside of the Generating Tube.—W. D. Coolidge and C. N. Moore, p. 601.
- Cathodic Evaporation in a Magnetic Field.—E. Henriot and O. Goche, p. 422.
- Second Meeting of the International Technical Consulting Committee on Radio Communication (C.C.I.R.), Copenhagen, 1931, p. 179.
- A Magneto-Optic Method of Chemical Analysis [resulting in the Discovery of the Elements "Va" (87) and "Am" (85)].—F. Allison, p. 422.
- Magneto-Optical Method of Chemical Analysis [Depending on Lag of Faraday Effect].—J. W. Buchtá; Allison, p. 601.
- Further Research on Element 87 [Magneto-Optical Chemical Analysis Method].—Allison, Bishop, Sommer and Christensen, p. 660.
- A Chronological History of Electrical Communication.—Telegraph, Telephone and Radio, p. 300.
- A New Method of Preparing Colloidal Silver and Gold by means of a Continuous High Frequency Electrical Discharge.—A. N. Fraser and J. Gibbard, p. 660.
- Communication Carriers in the Technique of Distant Communication.—F. Lubberger and M. Schleicher, p. 179.

- Communication Engineering in the Second Half of 1931.—Kölsch : Watson, p. 540.
- The Present Status of **Complex Angles** in Their Applications to Electrical Engineering.—A. E. Kennelly, p. 479.
- Investigations on the Recoil of **Compressed Air Tools** [using Radio Technique].—O. Voigt, p. 54.
- Fifth Pacific Science Congress, June, 1933 ; Preliminary Programme of Papers and Authors, p. 179.
- On **Contact Conduction and Rectification** [on the Electronic Theory].—G. Hara, p. 242.
- Oscillations due to **Corona Discharges** on Wires.—R. E. Tarpley, J. T. Tykociner and E. B. Paine, p. 179.
- Counting Objects** without Photocells [by Effect of Approach on a Circuit including a Low-Grid-Current—"Electrometer"—Valve].—W. C. White, p. 114.
- A **Photoelectric Rapid Counting Equipment** for the Exact Counting of up to 1 200 Objects per minute.—E. Bornitz, p. 480.
- Rapid Counting Relays** for Impulses up to 20 per Second.—O. Dworeck, p. 480.
- Measurements by means of Models of the **Coupling** between Two Lines or Cables through Earth Currents.—A. Mühlhngaus, p. 114.
- On **Curve-Fitting** by means of Least Squares.—W. R. Cook, p. 113.
- The **Dielectric Constants** of Colloidal, Biological Sub-strata [Serum, etc.] ; Wavelengths 10-30 Metres.—C. Albrecht, p. 660.
- The **Differential Analyzer**. A New Machine for Solving Differential Equations.—V. Bush, p. 113.
- A Mechanical Method for the Solution of Second Order Linear **Differential Equations**.—E. C. Bullard and P. B. Moon, p. 113.
- Simultaneous Integration** of Two Differential Equations of the First Order.—B. Gambier, p. 113.
- The Application of **Quadratic Forms** in an Infinity of Variables to Boundary Problems in Partial Differential Equations.—S. W. P. Steen, p. 300.
- A Simple Method for the Numerical Solution of **Differential Equations**.—W. G. Bickley, p. 479.
- Precision Measurements** of Mechanical Dimensions by Electrical Measuring Devices.—A. V. Mershon, p. 422.
- On **Dissipative Systems** and Related Variational Principles.—H. Bateman, p. 113.
- Dosimeter** for High- and Ultra-High Frequency Therapeutic Treatments.—K. Heinrich, p. 113.
- On the Forces acting on **Drops** in an Electric Field.—G. D. West, p. 540.
- On Some Properties of the **Electret**.—T. Tiku : Eguchi, p. 540 and 660.
- Types of Changes in Brain, Spinal Cord and Nerve Cells following an **Electric Shock**.—W. B. Kouwenhoven and O. R. Langworthy, p. 301.
- Electrical Communication in 1931**.—I. T. and T., p. 300.
- A Survey of the Most Important Work in **Electrical Engineering during 1931**.—German Elektrotechnischer Verein, p. 540.
- A₁ Improved Form of **Electrocardiograph** [with Special High Input-Impedance Valve Amplifier].—S. H. Caldwell, C. B. Oler and J. C. Peters, p. 541.
- A New Method of **Electrolysis**.—A. Klemenc, p. 53.
- Rubber Conveyors are Synchronised by [Electron] Tubes [using Variable Reactors and Thyratrons].—B. S. Havens, p. 301.
- The Reliability of **Electron Tubes** in Elevator Service.—C. C. Clymer, p. 480.
- Electron Tubes** in Traffic-Actuated Control Systems, p. 54.
- An [Electronic] Vacuum Tube Relay and Race Timer.—Roberds, p. 109.
- An **Electronic High-Speed Timing Device**.—W. M. Roberds, p. 480.
- Electronic Devices** as Aids to Research.—A. W. Hull, p. 539.
- Electronic Speed and Acceleration Recorder**.—H. M. Partridge, p. 660.
- Electronic Devices in Industry**.—See also Counting, Internal Combustion, Light Sensitive, Lifts, Moisture, Photocells, Photoelectric, Piezoelectric, Thyratrons, Ultra-Micrometer.
- Industrial Uses of **Electronic Diffraction** [Study of Surfaces, e.g. of Photoelectric or X-Ray Cathodes].—C. J. Phillips, p. 361.
- The Design and Construction of **Electrostatic Generators**.—H. Chaumat and E. Lefrand, p. 112.
- Electrostatic Machines** : the Chaumat Principle applied to the Ramsden Frictional Machine.—H. Chaumat and E. Lefrand, p. 242.
- New **Electrotherapeutic Apparatus** for the Production of Alternating Long-period Wave Currents and of Pulsating Currents.—Delherm and Laquerrière, p. 113.
- Selective Heating by Short Radio Waves and Its Application to **Electrotherapy**.—J. C. McLennan and A. C. Burton, p. 301.
- Emergency Employment Committee Report** [with Numbers of Applicants with Various Qualifications], p. 601.
- Making New Emulsions at 300 000 Cycles, p. 361.
- From the Great German Radio and Phono Exhibition, Berlin, 1931.—W. Burstyn, p. 52.
- The Berlin Radio and Phono Exhibition, p. 113.
- The Great German Radio and Phono Exhibition.—A. Harnisch, p. 179.
- The German P.O. Section at the 8th Berlin Radio Exhibition.—G. Kette, p. 300.
- Forecast of the 1932 Berlin Radio Exhibition, p. 601.
- The Physical and Optical Societies' Exhibition, p. 179.
- Physical and Optical Societies' Exhibition :—Radio and Allied Instruments and Apparatus : Laboratory Electrical Instruments.—R. L. Smith-Rose : C. V. Drysdale, p. 422.
- The Physical Society's Exhibition : Matters of Wireless and Laboratory Interest, p. 300.
- The Radio Exhibition, p. 659 : see also under "Reception."
- Faraday Centenary Celebrations, 1931, p. 52.
- Some Electrical Instruments at the Faraday Centenary Exhibition, 1931.—R. W. Paul, p. 179.
- New Remarks on **Fermat's Last Theorem**.—L. Pomey, p. 178.
- Trawling by Electricity : Fundamental Considerations on the Catching of Fish by Galvanotaxis.—W. Holzer, p. 113.
- The Tracing of **Dissymmetry and Flaws** in Ferromagnetic Machine Parts.—J. Peltier, p. 54.
- The Addition of a "Memory" [Gas-filled Trigger Relay Tube] to a Photoelectric Cell detecting Flaws, p. 480.
- Experiments on **Fluids Oscillating** under the Influence of Alternating Electromagnetic Fields.—B. Claus, p. 660.
- Fourier Analysis** of Functions with Discontinuities, Angular Points and Similar Properties.—G. Koehler and A. Walther, p. 113.
- Report on the Work and Studies of the French National Laboratory of Radioelectricity : with List of Publications.—C. Gutton, pp. 422 and 474.
- Fundamental Considerations on the Use of **Gamma Rays** for Testing Materials.—R. Berthold and N. Riehl, p. 541.
- On the Magnitude and Depth Effect of the Capacitive Influence on a Line by a Dishomogeneity of the Subsoil [Method of Geophysical Exploration].—W. Stern, p. 114.
- An Apparatus for the Generation and Measurement of Low-frequency Electromagnetic Alternating Fields [for Geophysical Exploration] : 5-1 000 Cycles/Sec. : Frequency independent of Load.—M. Müller, p. 480.
- Some Experiments relating to **Geophysical Prospecting** [Equiquadrature Method].—D. C. Gall, p. 114.
- Geophysical Prospecting** by 10-30 Metre Waves.—W. Stern, p. 179.
- Geophysical Exploration, Prospecting.—See also Prospecting.
- The Seventh Meeting of the German Physicists and Mathematicians in Bad Elster, November, 1931.—E. Lübcke, p. 422.
- Graphical Symbols** for Communication Engineering (Commission Électrotechnique Internationale), p. 479.
- Effect of **Ground Permeability** on Ground Return Circuits.—W. H. Wise, p. 114.
- Ultra-Violet Light and High-Frequency Current Harden Steel.—J. J. Egan, p. 53.
- Properties of **Harmonic Functions** of Two Variables in an Open Area Limited by Particular Lines.—C. de la Vallée Poussin, p. 601.
- The Kelvin Lecture : Dr. Sumner on the Work of Oliver Heaviside.—W. E. Sumner, p. 479.
- Note on the **Heaviside Expansion Formula**.—J. M. Dalla Valle, p. 178.
- Fun with **Heaviside's Calculus**.—W. C. Johnson, Jr., p. 300.
- The 1931 Meeting of the **Heinrich Hertz Association**, p. 300.
- The Present Position of **High-Frequency Telephony** on High-Tension Lines.—W. Pinski, p. 179.
- The Sensitivity of the **Human Body** to Weak Alternating Currents (50 c.p.s.).—E. Albers-Schönberg, p. 113.
- The Periodic Fluctuation of the Electric Field of the **Human Body**.—W. E. Boyd, p. 422.
- On the Normal Resistance of the **Human Body** for High-Frequency Currents.—N. N. Malov and S. N. Rschevkin, p. 541.
- The Variation with Frequency of the Resistance of the **Human Body** in the Range 365 to 8×10^6 Cycles per second.—N. N. Malov and S. N. Rschevkin, p. 540.
- Electrical Analogies in **Hydrodynamics**.—J. Pérès and L. Malavard, p. 540.
- I.E.E. Wireless Section** : Chairman's Address.—A. S. Angwin, p. 112.
- A Cold-Cathode 110-Volt Gaseous Illuminant.—Spanner, Germer, Doring, p. 113.
- Balancing Methods for the Elimination of **Induced Noise** in Telephone Cables.—H. Jordan : Collard, p. 114.
- Theory of the Co-existence of Power and Communication Lines from the Point of View of Their Mutual Induction, p. 114.
- Phenomena of Low Frequency **Induction** [Power Lines and Communication Lines].—National Electric Light Association, p. 659.
- Measurements of the Mutual Induction between Lines with Ground Return, in Skillingaryd.—H. Klewe, p. 179.
- The **Inductive Effects** of a Single Line traversed by an Alternating Current.—F. Pollaczek, p. 114.
- Inductive Induction**—See also Interference, Wires.
- Use of the Photoelectric Relay in the **Infra-red**.—F. Matossi : Bergmann, p. 54.
- The "Invisible Barrage" and the Prevention of Accidents by means of **Infra-Red Rays**.—Fichet-Céma Company, p. 361.
- Discussion on "Interference between Power and Communication Circuits : Summary of Recent Information (1926-1929)."—D. W. Roper : Radley, p. 541.
- Measures to Protect Telephone Lines against **Interference** from High Current or High Voltage Power Lines.—C.C.I.T., p. 114.

- Interference between Power and Communication Circuits: Summary of Recent Information (1926 to 1929).**—W. G. Radley, p. 114.
- Interference.**—See also Induced, Induction, Coupling, and below.
- The Disturbing Influence of High Current or High Voltage Lines on Communication Lines: The Interfering Potential and Its Measurement.**—Ch. Degoumois, p. 114.
- Measurement of the Hygrometric State of a Gaseous Mass by a Relaxation Oscillation Method: Application to Tests of Internal Combustion and Steam Engines.**—P. Le Rolland and T. Te Lou, p. 300.
- The Method of Least Squares.**—H. J. Brennen, p. 300.
- The Calculation of Errors by the Method of Least Squares.**—R. T. Birge, p. 479.
- Radio Legislation in the U.S.A.: The Legal Basis for Broadcasting in Germany: The Regulation of Television.**—Loucks: Hoffmann: Smith, p. 179.
- The Leipzig Spring Fair, p. 422.**
- Tube Control of High-Speed Lifts [Plotron Oscillations Stopped by Entrance of Metal Plate between Grid and Plate Coils].**—p. 242.
- 100% Efficient Light Produced in Laboratory.**—M. Pirani, p. 53.
- Light-Sensitive Cells in the Service of Man.**—F. H. Constable, p. 659.
- Light-Sensitive Relays now on the Market, p. 114.**
- Linotype operated direct from Typewritten "Copy": the Sema-graph.**—B. L. Green, p. 479.
- German Technical Literature on Broadcasting during 1931, p. 421.**
- Automatic Locomotive Cab Signalling Using Valve Amplifiers, p. 54.**
- The Relations between the Characteristic Curves for Losses and Efficiency [of Machines in General].**—L. Binder, p. 480.
- New Methods of Measurement for Workshop Machines [Dresden Developments in Mechanical, Mechanical-Optical, Electrical and Optical-Electrical Methods].**—E. Sachsberg and W. Osenberg, p. 422.
- The Measurement of Rapidly Changing Mechanical Forces by Alteration of Cross Section of Liquid Resistances: Discussion.**—Wallichs and Optiz: Schmaltz, p. 480.
- Electricity in Modern Medicine: Artificial Fever: Electrosurgery: Electrocardiograph.**—Tenney: Ward: Williams, p. 301.
- Medicine, Electricity in.**—See also Physiological, Surgical.
- The Action at a Distance of Metals on Bacteria and Yeasts: on Microbes.**—G. A. Nadson and C. A. Stern, p. 541.
- A Grid-Glow Micrometer [for Measuring Displacements of Less than One Ten-Thousandth of an Inch].**—R. W. Carson, pp. 361 and 480.
- Increased Resolution in Microscopy by Television Technique: the Use of Quartz Crystals for Scanning.**—E. H. Syngé, p. 601.
- Action at a Distance on the Development of the Eggs of the Echinus [Mitogenetic Radiation].**—J. and M. Magrou and P. Reiss, p. 301.
- Valve Method for the Measurement of the Modulus of Rigidity of Materials.**—L. N. Tomilina, p. 361.
- The Rapid Determination of Moisture in Seeds and Other Granular Substances [including a Valve-Oscillator Method].**—R. M. Davies, p. 480.
- Lumber Moisture Content Determined Electrically [Portable Apparatus using Two Tuned Neon Flashing Circuits].**—C. G. Suits and M. E. Dunlap, p. 54.
- Determination of the Moisture Content of Wood by Electrical Means.**—C. G. Suits and M. E. Dunlap, p. 241.
- On the Moment Distribution of Moments in the Case of Samples Drawn from a Limited Universe.**—L. Isserlis, p. 113.
- Monochromatic Sources of Red and Yellow Light using the Electrodeless Discharge.**—F. Esclangon, p. 422.
- An Electric Motor working on the Kinetic Energy of Gaseous Ions.**—H. Chaumat and E. Lefrand, p. 601.
- A Voice Frequency Multi-channel Telegraph System.**—J. M. Owen and J. A. S. Martin, p. 361.
- A Trip Circuit for Nerve Excitation [for C.-R. Oscillographic Recording].**—König, p. 536.
- A Comparison of the Efficiencies [in their action on Nerves] of Wedge-Shaped Waves of the Second Type and Condenser Discharges, of Equal Initial Intensity.**—P. Fabre and P. F. Quesnoy, p. 541.
- A Short Monograph on Nomography.**—F. M. Wood, p. 479.
- Obituary: Dr. D. W. Dye, F.R.S.: General Gustave Ferrié.**—G. W. O. Howe, p. 421.
- Obituary: General Ferrié.**—R. Jouaust, pp. 361 and 421.
- Olympia, 1931: Impressions of the Radio Show.**—A.L.M.S., p. 52.
- The Trend of Progress [Olympia Show], p. 52.**
- Radio Apparatus for 1932 [Olympia Show].**—P. K. Turner, p. 52.
- Operational Calculus.**—H. V. Lowry, p. 479.
- Generalised Division and Heavyside Operators: Classicism and the Electromagnetic Equations of Lorentz.**—A. Press, p. 659.
- The Electrical Measurement of Mechanical Oscillations.**—H. Thoma, p. 301.
- Making High-Frequency Electrical Oscillations Visible with the Electrodeless Glow Discharge.**—F. Herold, p. 480.
- Notice to Authors—Some Notes on the Writing of Scientific Papers [including the Treatment of Mathematical Expressions], p. 178.**
- On the Preparation of Papers for "The Wireless Engineer," p. 479.**
- The Necessity of Compression in Papers and Letters to Technical and Scientific Journals during the Present Conditions, p. 242.**
- Can Inventive Genius be Organised? [Radio Patent Pool].**—G. P. Simons, p. 301.
- A New Patents Act, p. 659.**
- The Penetration of Radiation from Different Sources into Water and Body Tissues.**—W. E. Forsythe and F. Christison, p. 113.
- Simplified Method for Calculating Periodicities.**—S. R. Savur, p. 601.
- Heat Tempering of [Motor Car] Valves controlled by Photo-cells.**—F. J. Prentiss, p. 601.
- Photo-cells and Their Applications in Optical Technique [Survey and Bibliography of Recent Work].**—H. Singer, p. 539.
- Photo-cell Circuits: Photo-cells and Their Applications.**—R. C. Walker, pp. 54 and 242.
- Photo-cells and Advertising.**—R. C. Walker, p. 301.
- Photo-cells for Replacing Hand Picking in the final Cleaning of Coal.** p. 659.
- The Automatic Recording of Light-Distribution Curves by the Use of Photo-cells.**—W. Little and H. I. Eckweiler, p. 660.
- Photo-cells protect Public from Power-Operated Doors [of Lifts, etc.].**—C. E. Ellis, p. 660.
- The Use of Barrier-Layer Photo-cells for Reflection and Other Measurements in a Glass-Working Laboratory: and a Simple Photoelectric Microphotometer.**—B. Lange, p. 660.
- Photo-cell Control of Temperature for Filament-Coating [and Other Electric] Ovens.**—W. P. Koechel, p. 480.
- Photo-cell Controlled Elevator Doors.**—C. E. Ellis, p. 361.
- Automatic Egg-Candling [Freshness Test] Machine uses Photo-cell.**—W. C. Ferris, p. 660.
- Photoelectric Cells: Some of their Applications to Industry [Counting Gift Coupons: Alarm for Breakage of Delivery in Paper Mills, etc.], p. 601.**
- Photoelectric Cells for Adjusting the Illumination of Vehicle Tunnel in Paris to correspond with the Outside Lighting, p. 480.**
- A Precision Photoelectric Controller.**—C. W. La Pierre, p. 539.
- The Nature of the Photoelectric Cell, and Its Application to (Chemical) Measuring Processes—Automatic Electrophotometer for Light-Absorption Measurements.**—G. Gollnow: Geffcken and Richter, p. 480.
- Photoelectric Control of the Weighing of Batches, p. 361.**
- Photoelectric Cells in Precision Inspection Work [by Automatic Reading of Deflection-type Measuring Instruments].**—W. J. Tietz and C. Paulson, p. 301.
- Commercial Applications of Photoelectric Cells.**—E. H. Vedder, p. 242.
- Photoelectric Equipment for Sorting Cards into 100 Compartments, p. 54.**
- Objective Photometry by the use of Photoelectric Cells, and the Automatic Testing and Sorting of Incandescent Lamps.**—W. W. Loebe and C. Samson, p. 53.
- A Photoelectric Method of Measuring the Smoothness of Metal Plate.**—E. Gerold, p. 54.
- Photoelectric Method of Measuring Evenness of Yarn.**—G. R. Stanbury, p. 242.
- New Uses of Photoelectric Cells in Industry, p. 114.**
- Papers on a Photoelectric Apparatus for the Quantitative Investigation of Particle Size.**—N. N. Andrejev, p. 422.
- A Photoelectric Recorder [for Measuring Smoke, Heat, Light, Pressure, Noise, and Thicknesses of Thin Materials].**—C. W. La Pierre, p. 422.
- Continuous Weighing with Light-Sensitive [Photoelectric] "Telescope."**—E. J. White, p. 361.
- Archaeologists put Photoelectric Tube to New Use [Classification of Specimens according to Geological Area, by Ultra-Violet Ray Analysis], p. 660.**
- Photoelectric and Thyatron Devices in Industry.**—B. S. Havens, p. 241.
- Photoelectric Applications.**—See also Electron, Electronic, Light Sensitive, Selenium, Solutions, and below, down to Photronic.
- The Amplification of Small Photoelectric Currents by the Philips Electrometer Valve.**—R. P. Lejay, p. 53.
- Successful Design of a Photoelectric Polarimeter.**—G. Bruhat and P. Chatelain, p. 660.
- On a New Photoelectric Relay for Amplifying Small Movements.**—L. Bergmann, p. 53.
- Photoelectric Relay for A.C. or D.C. Mains [with Light Source bridging up to 20 Metres].**—AEG, p. 660.
- Photoelectric Relays.**—W. R. King, p. 660.
- Papers on Photoelectric Telemeters.**—A. J. Johnston and T. A. Busby, p. 660.
- Photoelectrically Controlled Humidifier governed by Moisture on Window Pane.**—B. S. Havens, p. 361.
- Applications of the Schlieren Method of Photography [for Making Gases Visible by Presence of Discontinuities in Density].**—D. B. Gawthorpe, p. 179.
- The Mekapion Photometric Recorder.**—S. Strauss, p. 480.
- The "Electric Eye" Now Enters Industry [including List of Commercial Applications of Photo-sensitive Cells], p. 54.**
- On the Photo-Telephony [Successful Use of Incandescent Electric Lamp as Transmitter].**—T. Kujirai, p. 540.
- Phototubes Control Furnace Temperatures.**—L. R. Koller, p. 242.
- Photronic Cell a Direct Aid to Better Lighting.**—A. H. Lamb, p. 601.
- The Use of Valves in Physico-Chemical Measurements, Part I.**—W. Hiltner, p. 54.

- The Work of the **Physikalisch-Technischen Reichsanstalt** in 1930, p. 179.
- Physiological and Biological Effects of High Frequency** [Short Bibliography of Recent Papers], p. 541.
- Piezoelectric Properties of Rochelle Salt Crystals.**—R. D. Schulwas-Sorokin, p. 480.
- Determination of the Tensile Strength of Thin Wires by Piezoelectric Methods.**—F. Seidl, p. 601.
- The Measurement of Acceleration of Motors, etc., by a Piezoelectric Equipment.**—H. Lund: AEG, p. 539.
- Piezoelectric Device for Measurement of Engine Acceleration.**—Physik. Tech. Reichsanstalt, p. 54.
- Piezoelectric Measurement of Acceleration, etc., in Motors.**—H. Lund, p. 480.
- A Piezoelectric Method of Measuring the Pressure Variations in Internal Combustion Engines.**—H. G. I. Watson and D. A. Keys, p. 660.
- Recording the Instantaneous Pressures in Fire-Arms by a Piezoelectric Instrument.**—C. T. Ervin, p. 680.
- Ballistic Gas Pressure Measurements with Piezoelectric Indicator and Cathode-Ray Oscillograph.**—H. Joachim and H. Ilgen, p. 660.
- The Piezoelectric Measurement of Mechanical Quantities [Vibration, Acceleration, etc.]**—J. Kluge and H. E. Linckh, p. 54.
- Measurement of Rotational Vibration with Piezoelectric Crystals.**—H. Lund, p. 480.
- Investigations, by Piezoelectrical Technique, into the Fatigue of Steel Bars.**—D. Schenk, p. 54.
- Some Arrangements for the Electrical Transmission of Signals, etc., along Power Transmission Lines [using Beats between Two Musical Frequencies].**—J. Bethenod, p. 540.
- Production Peaks and Valleys.**—A. C. Lescarboura, p. 301.
- Radio—Broadcasting—Television [Progress] in 1932: Advances in Sound-Recording; Industrial Uses of Tubes, p. 300.**
- Ten Years' Progress in Communication Services.**—P. Craemer, p. 540.
- Electrical Progress in 1931—Television: Radio Telegraphy: Vacuum Tubes.**—W. G. W. Mitchell: H. Faulkner: L. J. Davies, p. 300.
- Methods used in Electrical Prospecting.**—J. I. Heller, p. 114.
- Some Aspects of Electrical Prospecting Applied in Locating Oil Structures: Effects of Heat Treatment on Fine Metallic Suspensions [Eliminating Wandering Zero]: Asymmetry of Sound Velocity in Stratified Formations: and Other Geophysical Papers, p. 541.**
- Application of Electrical Methods of Prospecting to the Study of the Foundations of Dams, etc.**—M. Lugeon and C. Schlumberger, p. 660.
- Communication with Quasi Optical Waves.**—Karplus, p. 34.
- Radiation Effect (Decreasing the Delay Time of a Spark Discharge) from a Disconnected Mercury Vapour Quartz Glass Lamp.**—Heyne, Meyer and Otto, p. 659.
- A Sensitive Radiation Meter using a Bimetallic Strip [Thin Quartz with Bismuth Coating].**—M. Weingeroff, p. 659.
- The Problem of Radiations [Solar Spectrum: Radiation from Gases: Mitogenic Rays: Roentgen and Gamma Rays: Irradiation of Ergosterol, etc., etc.]**—H. Koenen, p. 113.
- The Spokesman for the Radio Engineer.**—S. C. Cooper, p. 113.
- The Radio Research Board Report, p. 112.**
- The Work of the Radio Research Board, p. 179.**
- Annual Convention of the Radio Society of Great Britain and British Empire Radio Union, p. 659.**
- Review of Progress: Radio Telegraphy and Radio Telephony.**—A. S. Angwin, p. 179.
- Radiothermy [Survey with 25 Literature References].**—W. R. Whitney, p. 660.
- An Alternative to the Rejection of Observations.**—H. Jeffreys, p. 601.
- "Resistance Cells": Absorbable Radiation, Activation of Matter, Production of X-Rays.**—G. Rebol: G. Déchéne, pp. 53, 301 (two) and 541.
- Royal Society Conversazione: Cathode-Ray Oscillograph in Radio Research: in Measuring Telegraph Time Distortion: Thermionic Electrometers: Photo-Conductivity of Diamonds, etc., p. 601.**
- The E.M.F. of Filtration produced by the Rise of Sap in Plants [Characteristic Curve resembling that of a Detector, and explaining certain H.F. Results].**—N. Marinisco, p. 113.
- The Influence of an Artificial Electrical Atmosphere on the Rising of Sap.**—N. Marinisco, p. 660.
- The "Chirotherm": Improved Apparatus for Bloodless Surgery [H.F. Electric Scalpel].**—Messrs. Watson and Sons, p. 660.
- Thermionic Seismograph, p. 660.**
- The Selenium Cell as Colorimeter.**—A. Mickwitz, p. 53.
- Infra-Red Sextant used on Mauretania during Days of Cloudy Weather.**—MacNeil, p. 480.
- The Action of Short-Wave Apparatus compared with that of Diathermy Apparatus.**—Rhenisch, p. 301.
- A Reliable Method of Obtaining the Derivative Function from Smoothed Data of Observations.**—G. Rutledge, p. 479.
- The Constitution of Solutions deduced from Absorption Measurements: Infra-Red Absorption Spectra of Liquids determined by Thalofide Photoelectric Cell.**—P. Vaillant: R. Freymann, p. 54.
- Ether Spectrum Chart showing Recent Radio Reallocation [and Audible and Photoelectric Spectra], p. 479.**
- [Spectrum] Chart of Some Electromagnetic Relations [Wavelength Scale from 10^7 to 10^{-13} cm].**—W. E. Deming and F. G. Cottrell, p. 541.
- The Standardisation of Books and Periodicals in Germany.**—A. F. C. Pollard, p. 421.
- Statistics of Radio and Sound-Pictures, p. 361.**
- Sterilisation of Milk by High-Pitched Sound Waves.**—Gaines and Chambers, p. 172.
- Electricity in Healing. Recent Advances in Surgical and Medical Applications.**—E. P. Cumberbatch, p. 541.
- Symbolic Calculus.**—B. van der Pol and K. F. Niessen, p. 300.
- The Transmission of Telegraphic Signals.**—Bartelink and Bast, p. 88.
- Telemetering over the Telephone Network, p. 242.**
- Summation Measurement Methods in Telemetering, and their Chief Deficiencies.**—W. Stablein, p. 300.
- A Vacuum-Tube Device for Current-Balance Telemeters.**—B. E. Lenchan and P. MacGahan, p. 242.
- The Exhibit of Testing Apparatus and Machines held in connection with the Annual Meeting of the American Society for Testing Materials.**—H. V. Cadwell, p. 179.
- The Variation in the Conductivity of a Thin Metallic [Tungsten] Film as an Effect of an Electric Charge [Increase of Conductivity for Negative Charge, Decrease for Positive: approximately Proportional to the Field].**—M. Pierucci, p. 541.
- Application of Thyratrons to the Winding of Copper Wire under a Constant Tension.**—Rhea, p. 54.
- Thyratrons Control 3 500-lb Steam Boilers, p. 660.**
- Thyratrons.**—See Electronic, Photoelectric, and under "Subsidiary Apparatus" and "Valves and Thermionics."
- A New Use of the Vacuum Tube in Electrometric Titrations. I. Polarisation of Platinum Electrodes in Oxidation and Reduction Reactions.**—Kassner, Hunze and Chatfield, p. 539.
- A New Electrical Pick-Up for Measuring Forces on Tools, Cutting Pressures, etc. [based on Variation of Liquid Resistance].**—A. Wallich and H. Opitz, p. 540.
- Electronic Equipment in Train Control, p. 242.**
- Stationary and Non-Stationary Conditions in Inductive [Resonance Principle] Train Control.**—A. Kammerer, p. 242.
- The Transformation of $\sqrt{-1}$: A New Equation for the Cycloid.**—G. S. Berkeley: C. Turnbull, p. 113.
- Investigations of Service Transformers with the Cathode Ray Oscillograph.**—J. Röhrig, p. 54.
- Transients in Grounded Wires Lying on the Earth's Surface.**—J. Riordan, p. 114.
- The U.I.R. Assembly at Ouchy-Lausanne.**—M. Adam, p. 113.
- The U.I.R. Congress at Rome, p. 479.**
- High Precision Method of Measuring Lengths and Thicknesses [Ultra-Micrometer on Pneumatic Principle].**—M. Mennesson, p. 422.
- Ultra-Micrometer Circuits for Studying the Vibrations at the Surface or in the Interior of a Solid, particularly the Framework of a Bridge [Absorbmicrometer].**—P. Santo Rini, p. 361.
- Ultra-Micrometer on the Absorbing Wave-Meter Principle [for Strain Tests in Ferro-Concrete, etc.]**—P. Santo Rini, p. 53.
- A New Electrical Ultra-Micrometer.**—S. Reisch, p. 53.
- The Reich Ultra-Micrometer Used as a Galvanometer Relay.**—Reisch, p. 114.
- The Instantaneous [Ultra-Micrometer] Pressure Recorder and Its Applications.**—M. Horioka, T. Uchiyama and E. Mizuguchi, p. 242.
- A New Form of Dilatometer [Recording Ultra-Micrometer Circuit for Determining the Temperature at which any Abnormal Change in Length occurs].**—W. E. Prytherch, p. 480.
- New Applications of the Condenser Principle for Measuring Purposes [Ultra-Micrometer: Idometer: Siccometer].**—W. Jaekel: Siemens Company, p. 242.
- The Rectifier Bridge and Its Use in Ultra-Micrometer Circuits.**—Walter, p. 660.
- Electrical Methods of Measuring Pressures and Displacements [Comprehensive Survey of Ultra-Micrometer, Piezoelectric and Magnetostrictive Methods].**—G. Sacerdote, p. 480.
- Contribution to the Design and Use of an Apparatus for the Measurement of Small Deformations [Outline of Electromagnetic Ultra-Micrometer Devices].**—A. Guillet, p. 242.
- Ultra-Micrometer based on Change of Coupling between Windings of a Transformer: Galvanometer Deflection Method and a Null Method.**—A. Guillet, p. 114.
- Electrodynamic Arrangement for the Measurement of Small Mutual Inductances: Application to the Examination of [Ultra-] Micrometers.**—A. Guillet, p. 361.
- Electronic Oscillators [Ultra-Micrometers] for Industrial Process Control.**—H. Olken, p. 53.
- Ultra-Micrometers.**—See also Acceleration, Compressed Air, Dimensions, Machines, Mechanical, Micrometer, Oscillations, Piezoelectric, Tools, Very Small, Vibration(s), Vibro-, and below.

- Ultra-Micrometric and Other Electrical Methods of Measuring Pressures and Displacements.**—G. Sacerdote, p. 601.
- A Mechanically Controlled Bolometer applicable to **Ultra-Micrometric Use.**—Sell, p. 540.
- A Remote Electrically-Recording Accelerometer [Electromagnetic **Ultra-Micrometric Device**] with Particular Reference to Wheel-Impact Measurements.—F. Aughtie: Dufton, p. 241.
- Measuring Instruments and Processes for Interchangeable Parts [**Ultra-Optimeter**, etc.].—G. Berndt, p. 660.
- Experiments on the Biological Effects of d'Arsonvalisation on **Ultra-Short (10-Metre) Waves.**—H. Bordier, p. 361.
- Special **Ultra-Short Wave** Issue of "Funk-Magazin," p. 541.
- Researches on the Effects of **Ultra-Short-Wave Irradiation** on Plant Life and on Silkworms, etc.—Mezzadrolì, p. 541.
- On the Physics of **Ultra-Short-Wave Therapy: the Wave Band of Selective Heating.**—J. Pätzold, p. 541.
- The Latest in High-Intensity X-Rays and "Fever Machines" [**Ultra-Short Wave Treatment**], p. 361.
- The Application of Fluorescence to **Ultra-Violet Photometry.**—A. Chevallier and P. Dubouloz, p. 422.
- A New Method of Irradiating the Body Cavities with **Ultra-Violet Rays** [using a Tungsten Spark-Gap].—G. Loock, p. 301.
- The Practical Applications of **Ultra-Violet Rays.**—R. Gourjon, p. 541.
- Breakdown Message Speech Transmission System of the London **Underground Railways.**—F. Clark and A. A. Chubb, p. 540.
- Scheme of Ursigram Transmissions by French Radiotelegraph Stations, from 1st January, 1932, p. 173.
- Utilisation of the E.M.F.s of Induction for the Registration of Variations in the Velocity of Conducting Liquids: a New Haemodromograph without a Blade in the Blood.—P. Fabre, p. 480.
- Local Effects on Rats due to **Very High Frequency Fields** [20 Megacycles].—J. Saidman, J. Meyer and R. Cahen, p. 113.
- An Apparatus for the Measurement of **Very Small Displacements** [Measuring Microscope aided by Quartz Pointer as Lever, Measuring Displacements of Order of 0.001 mm.].—H. Whitaker, p. 53.
- Replacement of a Mechanical Vibrating System by an Equivalent Electrical Circuit [in Study of Diesel Engine **Vibration**].—F. J. Domerque, p. 660.
- A New Portable Recording Acceleration and **Vibration Meter** on the Piezoelectric Principle, using Valve Voltmeter and String Galvanometer.—R. Ambronn, p. 480.
- The Registration of Rapid **Vibrations** [Ambronn's Piezoelectric Instrument].—R. Ambronn, p. 242.
- Recording the Deformations and **Vibrations** of the Wing of an Aeroplane in Flight [using the Variations of Resistance of a Thin Graphite Layer].—A. Guerbilsky, p. 241.
- Calculation and Experimental Investigation of the **Vibrations** of Aeroplanes [Recording a "Vibration Spectrum" by the Küssner "Optograph"].—H. G. Küssner, p. 301.
- The Experimental Investigation of **Vibrations** in Turbine Wheels and Blades [including **Ultra-Micrometric Methods**].—B. Pochobradsky, L. B. W. Jolley, and J. S. Thompson, p. 241.
- The Mecascope for Recording **Vibrations** of Machines, etc.—J. Vassillièrre-Arlhac, p. 54.
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- Vibrations.**—See also Piezoelectric, **Ultra-Micrometer**, and below.
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- Electromagnetic **Vibrograph** [**Ultra-Micrometer Device** with Balanced Transformer Circuit and Varying Air-Gap] and Its Use in connection with Turbo-Generator Rotors.—F. Sieber, p. 301.
- The **Vibrometer.**—Subra, p. 351.
- A New Voice Frequency Telegraph System.—J. A. H. Lloyd, W. N. Roseway, V. J. Terry and A. W. Montgomery, p. 540.
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