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#### Abstract

Tyis $1 / 1112 / 2430 / 99$  GN7401N $0.20 \quad 0.18 \quad 0.16$ GN74OIAN 0.380 .3880 .33 $\begin{array}{llll}\text { AN7402N } & 0.20 & 0.18 & 0.18 \\ \text { SN7403N } & 0.20 & 0.18 & 0.18\end{array}$ $\begin{array}{llll}\text { SN7403N } & 0.20 & 0.18 & 0.16 \\ \text { N } 7403 \mathrm{AN} & 0.38 & 0.38 & 0.33\end{array}$ $\begin{array}{llll}\text { BN7403AN } & 0.38 & 0.38 & 0.33 \\ \text { ON7404N } & 0.24 & 0.21 & 0.18\end{array}$ $\begin{array}{lllll}8 N 7405 N & 0.20 & 0.18 & 0.16\end{array}$ SNTHOSAN 0.440 .440 .38 SN7406N $\quad 0.400 .88 \quad 0.35$ $\begin{array}{llll}\text { SN7407N } & 0.40 & 0.38 & 0.85 \\ \text { SN7408N } & 0.25 & 0.22 & 0.19\end{array}$ $\begin{array}{llll}\text { 8N7408N } & 0.25 & 0.22 & 0.18 \\ \text { GN7409N } & 0.33 & 0.33 & 0.28\end{array}$ $\begin{array}{llll}\text { SN7409N } & 0.33 & 0.33 & 0.28 \\ \text { SN7409AN } & 0.44 & 0.44 & 0.38\end{array}$ $\begin{array}{lllll} \\ S N 7410 N & 0.20 & 0.18 & 0-10\end{array}$ $\begin{array}{llll}\text { BN7411N } & 0.25 & 0.23 & 0.21 \\ \text { SN7412N } & 0.28 & 0.28 & 0.25\end{array}$ $\begin{array}{llll}\text { SN7412N } & 0.28 & 0.28 & 0.25 \\ \text { BNT412AN } & 0.38 & 0.38 & 0.38\end{array}$ $\begin{array}{llll}\text { SN7412AN } & 0.38 & 0.38 & 0.38 \\ \text { SN7413N } & 0.30 & 0.27 & 0.25\end{array}$ $\begin{array}{llll}\text { SN7413N } & 0.80 & 0.27 & 0.25 \\ \text { SN7414N } & 0.72 & 0.72 & 0.83\end{array}$ $\begin{array}{llll}\text { SN7414N } & 0.72 & 0.72 & 0.83 \\ \text { SN7416N } & 0.30 & 0.27 & 0.25\end{array}$ $\begin{array}{lllll}\text { SN7416N } & 0.30 & 0.27 & 0.25 \\ \text { SN7417N } & 0.30 & 0.27 & 0.25 \\ \text { SN74 }\end{array}$ | gN7420N | 0.20 | 0.18 | 0.18 |
| :--- | :--- | :--- | :--- | :--- | $\begin{array}{llll}8 N 7422 N & 0.28 & 0.28 & 0.25\end{array}$ $\begin{array}{lllll}\text { SN7422N } & 0.288 & 0.28 & 0.25 \\ \text { SN7422AN } & 0.38 & 0.38 & 0.33 \\ \end{array}$ $\begin{array}{llll}\text { GN7423N } & 0.37 & 0.34 & 0.38 \\ \text { GN7425N } & 0.37 & 0.37 & 0.32\end{array}$ $\begin{array}{llll}\text { 8N7425N } & 0.37 & 0.37 & 0.32 \\ \text { SN7427N } & 0.87 & 0.87 & 0.38\end{array}$ $\begin{array}{llll}\text { SN7427N } & 0.87 & 0.87 & 0.38 \\ \text { SN7428N } & 0.43 & 0.43 & 0.37\end{array}$ $\begin{array}{llll}\text { SN7428N } & 0.43 & 0.43 & 0.37 \\ \text { SN7430N } & 0.20 & 0.18 & 0.18\end{array}$ $\begin{array}{llll}\text { 8N7430N } & 0.20 & 0.18 & 0.18 \\ \text { SN7432N } & 0.37 & 0.37 & 0.32\end{array}$ $\begin{array}{lllll}\text { SN7432N } & 0.37 & 0.37 & 0.32 \\ \text { SN7433N } & 0.48 & 0.43 & 0.38\end{array}$ $\begin{array}{llll}\text { SN7433N } & 0.48 & 0.43 & 0 \\ \text { SN7433AN } & 0.57 & 0.67 & 0.50\end{array}$ $\begin{array}{llll}\text { SN7433AN } & 0.57 & 0.67 & 0.80 \\ \text { SN7437N } & 0.43 & 0.43 & 0.87\end{array}$ $\begin{array}{lllll}\text { BN7437N } & 0.43 & 0.43 & 0.37 \\ \text { SN7438N } & 0.43 & 0 & 43 & 0.37\end{array}$ SN7438AN $0.57 \quad 0.67 \quad 0.50$ SN7440N 0.200 .18 0.16 GN7441AN $0.85 \quad 0.79 \quad 0.78$ SN7442N $0.85 \quad 0.79 \quad 0.73$ $\begin{array}{llll}8 N 7443 N & 1.60 & 1.27 & 1.13 \\ \text { 8N7444N } & 1.50 & 1.27 & 1.18\end{array}$ $\begin{array}{llll}\text { gN7444N } & 1.50 & 1 \cdot 27 & \frac{1}{1} \cdot 18 \\ \text { RN7445N } & 2.16 & 2.16 & 1.80\end{array}$ $\begin{array}{cccc}\text { BN7445N } & 2 \cdot 16 & 2 \cdot 16 & 1 \cdot 89 \\ \text { SN7446N } & 2 \cdot 16 & 2 \cdot 16 & 1 \cdot 89\end{array}$  MTEO GERIES IS CAD O.E.M. PRICES PHONE (OI) T23 38MS. PRICING OF REGARDLESS OF MIX SNTA HIGH POWER SNTM SERIES IN STOCK. . SEND FOR LIST 36, FREE ON REQUEST゙. LOW PROFILE SOCKETS IIPIN . . . isp is PIN. . . I7p. 8 PIN . . . I4p


TRANSISTORS A SELECTION FOR
AAZ13 10p $\mid$ BC182 12D


 \begin{tabular}{ll|l}
AC128 \& 20p \& BCY39 <br>
AC187 \& 200 \& BCY65 2.50 <br>
ACY

 ACY17 85p 

ACY17 \& 3D \& BCY70 \& 16 D <br>
ACY \& 65D \& BCY71 \& 20 D

 

ADY \& B6D \& BCY71 \& 20 D <br>
AD \& 50p \& BCY72 \& 13 D

 

AD161 \& 89 D \& BD124 \& 80 D <br>
AD162 \& 39 D \& RD131 \& 80

 

AD162 \& 39p \& RD131 \& 45D

 $\begin{array}{ll}\text { AF117 } & 20 \mathrm{p} \\ \text { AF118 } & 80 p\end{array}$ $\begin{array}{ll}\text { AF118 } & \text { 80p } \\ \text { AF139 } & \text { 33p }\end{array}$ 

AF186 \& 30p \& BF194 \& 13p <br>
\& BFX13 \& 250

 

AF186 \& 40 p \& BFX13 \& 25 D \& <br>
AF239 \& 44p \& BPX34 \& 550 \& M <br>
A8Y27 \& 30 p \& BPI88 \& 82 D \&
\end{tabular}

$\qquad$ | BAll | 10 D | B |
| :--- | :--- | :--- |
| BAX13 | 5 p | BP | |  |  |  |
| :--- | :--- | :--- |
| BCl 107 | 12p | B | | BCl 08 | $12 p$ | BPYY 90 | 75 |
| :--- | :--- | :--- | :--- | :--- |

 \begin{tabular}{ll|ll}
BCl09C 14p \& BSX20 \& 16 <br>
BC113 16p \& BU10S 2.90

 

BC113 \& 16D \& BU105 \& 2.20 <br>
BC147 \& 12 p \& BY100 \& 16 D
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Two
two operated 45 volts $\& 4.57$
TG9014P Stere0.

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\begin{aligned}
& \text { TG9014P Stereo on } \\
& \text { two channel preamplin } \\
& \text { (circult book No, } 42
\end{aligned}
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\begin{aligned}
& \text { Twadip Stereo on } \\
& \text { two channel preampliner. \&1-50 } \\
& \text { (clicult book No. } 42 \text { prlce 180) }
\end{aligned}
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Operate at 40 Khz up 10100 yda Ideal remote switching and slonalling Complete with data franmitter and recelver new I.C. clrcults. TA960 IC with socket £I-80
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| 100 | ..... $42 p$ | 100 | ......13p |
| 500 | . . . . . 39 p | 500 | .....12p |
| 1000 | ......34p | 1000 | ......10p |
| BY12] |  |  |  |
| 25 | ......120 ea | OC3s |  |
| 100 | .......10p |  |  |
| 500 | ...... | 25 |  |
| 1000 | ..... ${ }^{\text {dp }}$ | 100 | . . . . . 420 |
|  |  | 500 | . . . . . 340 |
| ZENE | R DIODES | 1000 | . . . . . 340 |

## $400 \mathrm{~m} / \mathrm{w}$ BZY88/ $\mathrm{BZX} \times 3$. From 3.3

 volt - 33 volte ito each$$
\begin{aligned}
& 1.3 \text { watts } 5 \% \text { MI } \\
& \text { atura Tubulars } \\
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\end{aligned}
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& \text { From } 3.3 \text { volt }-33 \\
& \text { volt } 18 p \text { each. }
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10 \text { watt Sin }
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\begin{aligned}
& \text { Mounting. } Z S \\
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\begin{aligned}
& \text { serles } 8-8 \text { volte } \\
& 100 \text { volts } 5 \% \text { 40p } \\
& \text { each. }
\end{aligned}
$$

each.

## SILICON RECTIFIER

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IN4001 to IN4007
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702C (T05) 750 $\begin{array}{ll}702 \mathrm{C}(\mathrm{T} 05) & 75 \mathrm{p} \\ 709 \mathrm{C}(\mathrm{T05}) & 31 \mathrm{p}\end{array}$ 709 C (D.1.L.) 33 p $\begin{array}{ll}\text { 723C (TO99) } & \text { 90p } \\ \text { 723C (D.1.L.) } & 90 p\end{array}$ 728C (D.I.L.) 45p 728C (T099) 45p $\begin{array}{ll}741 \mathrm{C} \text { (T05) } & 50 \rho \\ 741 \mathrm{C} \text { (D.1.L.) } & 500\end{array}$ 747C (TO99) E1-8p 148C (D.I.L.) A1p


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& \text { FEATURES SMALL SIZE AND } \\
& \text { LOW COST Slzee, are approx. }
\end{aligned}
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\begin{aligned}
& \text { LOW COST SIzes.are approx. } \\
& \text { 250MIA QUARTER AMP }
\end{aligned}
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\begin{aligned}
& \text { 250M/A QUARTER AMP } \\
& \text { B025/05 50 PIV } 16 p
\end{aligned}
$$

$$
\begin{array}{ll}
\mathrm{B025} / 05 & 50 \mathrm{PIV} \text { I6p } \\
\mathrm{B025/10} 100 \mathrm{PIV} \text { 18p }
\end{array}
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## TEST

## EQUIPMENT

MULTIMETERS
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200 H (M210) $20 \mathrm{~K} / \mathrm{V}$ olt Silmiline with case TLH33D $2 \mathrm{~K} / \mathrm{V}$ olt Robusit with case U437 $\quad 10 \mathrm{~K} / \mathrm{V}$ oit Steel case. AC up to 40 KH $\begin{array}{ll}\text { U4324 } & 20 \mathrm{~K} / \mathrm{V} \text { olt with AC current ranges } \\ \text { AF105 } & 50 \mathrm{~K} / \mathrm{Volt} \text { wlth }\end{array}$ AF105 $50 \mathrm{~K} / \mathrm{V}$ olt with Leather case U43i3 20K/Volt AC current. Steel case U4341 Plus Built
Model 500 30kivoll


OTHER EQUIPMENT
$\begin{array}{ll}\text { SE250B } & \text { Pocket Signal Inlector } \\ \text { SE500 } & \text { Pocket Sidnal Tracer }\end{array}$
1.90 carr. 15p

SE500 Gocket Sidnal Tracer
TE15 280 mHz 1.50 carr. 15p

TEst AC Millivolimeter 1.2 mHz 18.75 carr, 35 p TE65 28 Range valve voltmeter is. 25 carr, 40D TE20D $120 \mathrm{kHz}-500 \mathrm{mHz}$ RF Generator TE22D $20 \mathrm{~Hz}-200 \mathrm{hHz}$ Audlo Generator carr. 40 D SE350A Deluxe SIgnal Tracer $\quad \mathbf{9 . 9 5} \mathbf{~ c a r r . ~} 20 \mathrm{D}$ SE400 Volts IMm /R-C sub. / 20

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| Phase Sequence | 5.95 |
| EHT Probe | 5.95 |
| Shunts 25/50/100A | 4.50 |
|  | each |


| A SELECTION OF INTERESTING ITEMS |  |  |
| :---: | :---: | :---: |
| 3025 | Co | 5.50 p \& p15p |
| 1300 | Mono mag. cart. preamp. | 1.95p\& p 15p |
| 1310 | Stereo mag. cart. preamp. | 4.95 p\& p 25 p |
| asiph | ne telephone amplifler | 6.15 p \& p 25p |
| 01203 | Teleamp. with PU coil | 3.60 D \& D 20p |
|  | Door Intercomm. and chimer | 11.95 p \& p 25p |
| Chatta | (lights as you talh) | 13.90 p \& p 20p |
| Kw | mmer/controller | $3 \cdot 00$ p \& p 10p |
| Twin | spring unlt For | 2.75 p\& ${ }^{\text {c }}$ 15p |
| 16" Tw | n spring unlt Reverbs | 6.50 p \& p 25p |
| Car Ta | chometer Electronic | 7.50 p \& p 15p |
| HF 10 | 5 Alrcratt Band Corrector | 3.95 p\& p 15 p |
| 82005 | Ch. mic, mixer | 2.95 p ¢ p 15 p |
| 0042 | ch. Stereo mixer | 4.75 p\&p15p |
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Catalogue


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GARRARD 2 speed $\theta$ volt tape decks. Fitted record/ play and oscillator/Erase heads. Wind and rewind controls. Takes up to 4" spools. Brand new complete with head circults.
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Z50, 30 watt 50 volt 4.37 1210, $2 \frac{1}{2}+2 t$ watts RE500, 5 watt IC mains operated Amplifier with controls E.S-30 SAC14; $7+7$ watt Stereo with controls
SAC13, $15+15$ watt Stereo with controls
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BUILD THIS TUNER
MW/LW Radlo Turnor to use with any ampllfer. in battery. Excellent resulte. Slze $7^{\prime \prime} \times 24^{\prime \prime} \times 3^{\prime \prime}$ All parts $£ 4 \cdot 85$, carr. 15 p .

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670C $6 / 71 / 9$ volt 300 MA (Includes Multi-Adaptor for Tape Recorders, etc.)
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P11 24 volt 500 mA (chassis)
P15 $26 / 28$ volt 1 amp (chassis)
P1080 12v 1 amp (chassis)
P1081 45v 0.9 amp (chassle)
P12 4t-12 volt 0. 4-1 amp
SE101A $3 / 6 / 9 / 12$ volt 1 amp (Stab.)
RP164 6/71/0/12 1 amp (Stb.)

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0.01 Diam. Mono Fllament E1-50 per 25
0.13 Sheathed. Ef:00 per metre SPRAYS 15 mm Der melam Mares Talla $\mathbf{\text { Es. }} 50$.
3.25 carr. 30 D
4.25 carr. 30 p 4.25 carr. 30 p
2.30 post 20 p 2.30 post 200
2.80 post 200 2.80 post 20 p
$\mathbf{2} \cdot 70$ post 20 p 1.25 post 20p +.40 post 20p - 75 post 30p 1.15 post 25p
$\mathbf{2} .05$ post 30 p
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|  | $\begin{aligned} & \text { A A } 5200 \\ & \text { AAS500 } \end{aligned}$ |
|  | AA5800 |
| AMSTRAD | $\begin{aligned} & \text { 1C2000 Mk. II } \\ & 4000 \mathrm{Mk} \mathrm{II} \end{aligned}$ |
| EAGLE | TSA149 |
|  |  |
|  | AAA |
|  | AA6 |
| HOWLAND WEST | DA1000 |
| HENELEC TEXAN |  |
| henelec texan NIKKO | Bull |
|  | TRM 300 |
| PIONEER <br> ROTEL | TRM400 |
|  | SA500A |
|  | RA 211 |
|  | RA311 |
|  | RA611 |
|  | RA810 |
|  | RA1210, |
| SINCLAIR | 2000 |
|  | ${ }^{3000}{ }^{\text {T }} 300$ |
| TANDBERG TELETON | TA 300 |
|  | SAO207 |
|  | GA202 |

## STEREO RADIO TUNERS

(carr./packing 50p)

## AMSTRA

HENELEC Stereo
HENELEC Slereo KH HOWLAND WEST DA1000T PIONEE
ROTEL

| ROT |  |
| :---: | :---: |
|  | $\begin{aligned} & \text { RT } 322 \\ & \text { RT } 622 \end{aligned}$ |
| SINCLAIR | 2000 |
| TELETON | ${ }^{3} \mathrm{G}$ T202 |

DECODERS I
SYNTHESIZERS (carr. etc. 30p)
DYNACO OUADRATOR
EAGLE
EAGLE
AA26
TATE 1
TATE 3
Chassis
MATCHED SPEAKER SYSTEMS
Recommended palrs 8 ohms
(Carr. / Packing £1-50 pair)
RANK DOMUS
RANK DOMUS
150
175
250
MARSDEN HALL
$180 \quad 10$
150
$\begin{array}{ll}110 & 1 \\ 150 & 1 \\ 200 & 2 \\ \text { DYNACO } \\ \text { A10 } \\ \text { A }\end{array}$
10 watt
5 watt
$\left.\begin{array}{l}\text { A10 } \\ \text { A } 25 \\ \text { A5 } \\ \text { WHARFEDALE }\end{array}\right\} \quad 20-60$ watts
WHARF
$\begin{array}{lll}\text { Denton } 2 & 18 \text { watt } & 27-20 \mathrm{pr} \\ \text { Unton } 2 & 20 \text { watt } & 32.65 \mathrm{pr}\end{array}$
25 watts
LEAK
50 18 wa
CELESTION
$\begin{array}{ll}20 \\ \text { COUNTY } & 20 \text { watt } \\ 25 & \text { watt }\end{array}$
$\begin{array}{lll}15 & 30 \text { watt } & 50.40 \mathrm{pr} \\ 44 & 44 \text { watt } & 81.20 \mathrm{pr}\end{array}$
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|  | N2211 | 19.95 |
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P8 32
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| :---: | :---: |
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| PS | D.I.N. 4 Pio |
| PH 4 | D.I.N. 8 Pln $180^{\circ}$ |
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| P8 | 8.1.N. 7 Pln |
| P8 | Jack 2.5 mm Bereenel |
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| P8 11 | Jack $\mathbf{i}^{\text {² P Plastlc }}$ |
| P8 12 | Jack !" Bereened |
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# PROJECTS ... THEORY. 

## PREVENTIVE MEASURES

The electronics enthusiast has frequent opportunities to provide good service for others, apart from satisfying his own personal interests and needs. This is because of the varied nature of the end-products of his hobby. In this context, a rather special case arises this month, which we feel merits the attention of all constructors.
We are all very familiar with the phrase "prevention is better than cure". The old adage is one of the first things to be implanted in our minds when quite young. This logic becomes part of our subconsciousness, though often we fail to heed this sound advice in our day-to-day affairs until damage or loss has been suffered.
True the increase in house break-ins and car thefts has brought attention to the need for security devices and systems that, if they do not actually prevent unauthorised entry, will at any rate give prompt indication immediately such a felony is attempted.
The basis of all modern intruder alarms is electronics, though systems may differ widely in the kind of sensing techniques employed. Many designs have been published for simple alarm systems suitable for protecting premises and motor vehicles. This month we publish another security system, but one that has been designed to counter the threat and danger of a baby or young child being unlawfully taken from a pram or other baby carriage.
lncidents of baby snatching from unattended prams and pushchairs have been headline news during the last few months. Although this inexplicable crime has not reached epidemic proportions, like other well-publicised offences, it could become "catching". The best way to discourage further incidents is to provide protection that frustrates an attempt to baby snatch by giving out a strident warning to alert passers-by.

The Baby Snatch Alarm described in this issue will take little in time, effort, or money to assemble. In use, it will give peace of mind to the busy mother when she has to leave a baby unattended, if for but a few moments. while she goes about her shopping.

Remember, electronics is our servant, and we constructors should be prepared at all times to use it whenever feasible to help solve everyday problems. Here is an excellent example of circuitry put to worthwhile use as a preventative measure. Why not make this project your good turn?


Our Jonuary issue will be published on Wednesday, December 19

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[^0]
# EASY TO CONSTRUCT SIMPLY EXPLAINED 

VOL. 2 NO. 12
DECEMBER 1973

## CONSTRUCTIONAL PROJECTS

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## NEXT MONTH

V.C.O. Effects Unit<br>Sewing Machine Speed Control<br>Fetset Receiver

## PLUS

Semiconductor Primer No. I
More details on page 685


This alarm has been designed to fit easily on any pram or push chair, to sense the baby without actual contact, and to be virtually foolproof in operation. When the unit is connected and switched on, the baby cannot be removed, the pram cannot be pushed away, and the unit cannot be disconnected or opened without the alarm sounding.

There are ways of preventing the alarm sounding but without studying the actual operation of the unit a would-be snatcher would not be able to take the baby:

## BABY SYSTEM

The sensing element used is a pressure mat that is virtually waterproof and is placed under the sheet or mattress to sense when the baby is actually in the pram. This mat is connected to the main unit, which is hung on the side or end of the pram, by a twin lead and a jack plug.
If the jack plug is removed, the lead cut, or the pressure taken off the mat, the alarm sounds. To prevent the pram being taken away the lead is passed through one of the wheels before being plugged into the main unit, thus the wheel cannot turn unless the wire is un-plugged-sounding the alarm.

The whole system is controlled by a switch operated by a key-in the same way as a car's ignition switch-and is supplied by a 6 volt lantern battery so it is safe even if it gets wet.

## the circuit

The circuit diagram of the alarm is shown in Fig. 1, SK1 is the socket into which the pressure mat is plugged, Sl is a microswitch fitted under the front panel of the case so that should the unit be opened while turned on, the alarm bell WD1 will sound. Switch S2 is the master, key operated on/off switch and LP1 and LP2 provide visual indication of the alarm condition and light a small sign reading "Baby Snatch."



With the pressure mat connected and the unit closed and turned on, capacitor Cl will charge through the mat, S1, R1 and D1, thus holding TR1 on. Diodes D1 and D2 prevent TR1 from being turned off when the unit is first switched on and Cl is discharged.

With TR1 on, TR2 is off and the thyristor CSR1 will not be fired and thus no current will flow to LP1, LP2 and WD1. If the circuit from TR1 base to the the negative line is broken-by removing the pressure from the mat, unplugging the mat or opening S1, capacitor Cl will discharge through D2 and VR1 at a rate determined by VR1 and, after a short delay TR1 will turn off, TR2 will turn on and hence fire CSR1 which will pass current to the warning devices LP1, LP2 and WD1.

Once CSR1 is passing current it cannot turn off until the current falls to nearly zero or the voltage is removed. Although the bell only requires intermittent current, LP1 and LP2 pass enough continuous, current to keep CSR1 conducting and thus the lights will show and the bell will continue to ring until the unit is turned off by the key switch.

Capacitor C1 and VR1 provide a short delay -up to about 10 seconds depending on the setting of VR1-so that should the baby jump up and down or in some way temporarily remove its weight from the mat. the alarm will not

sound. Only if the weight remains off the mat for longer than the set time will the alarm sound.

Power for the unit is from a 6 V SP996 battery which, on standby will last a very long time (probably at least six months to a year with normal use) and would certainly be capable of sounding the bell for about half an hour continuously. Hopefully the alarm will only be operated for test purposes.

## Components....

## Resistors



## Capacitor

C1 $500 \mu \mathrm{~F}$ elect. 12 V
Semiconductors
TR1 AC128 germanium pnp
TR2 AC128 germanium pno
CSR1 1A 50 p.i.v. thyristor
D1, 2 OA81 or similar diodes (2 off)
Miscellaneous
SK1 jack socket with plug
Si s.p.s.t. micro switch
VR1 50ks skeleton preset
LP1, 2 6V 0.06A bulbs in double holder with motif plate
WD1 4.5 V or 6 V bell (Friedland type)
S2, key operated s.p.s.t. switch
B1 SP996 6V battery
Veroboard 23 holes $\times 13$ strips $\times 0.15$ matrix, small brackets to fix Veroboard, case (see text) metal for pram mounting brackets, wire, 4BA fixings, Pressure mat.

## BABM SNATED ALABC



Fig. 2 (right) Veroboard layout and wiring for the alarm circuit.

Fig. 3 (below) Layout and wiring of the
 complete alarm unit.


## CONSTRUCTION

The main circuit is built on a piece of Veroboard. The strips must be cut and separated as shown in Fig. 2. Larger holes in the board are drilled for VRI, also two more holes are drilled to take the two fixing brackets. Make sure that you remember to strap together strips $D, E$ and $F$. All the external connections are made by using terminal pins, these are fitted to each end of the board as shown. Mount all the components on the board, soldering the transistors in last using a heat shunt on each wire as it is soldered.

The cabinet call be to your own personal choice but the one used on the prototype is a standard chassis size $205 \times 150 \times 75 \mathrm{~mm}$. The sloping front was produced by measuring down 25 mm on each side of the chassis and then cutting two pieces out, one each side. The lid of the chassis was also cut down to match.

The chassis is then drilled and finally covered in Contact or a similar covering. Advertise what the unit is on the front using Letraset, this will deter would-be baby snatchers and also warn other mothers not to pick the baby up, however innocent the motive is. Some holes are cut in the bottom of the box to allow the sound from the bell to be heard and to take SK1. The lamp indicator hole should be cut in the top. The micro-switch is fitted inside and to the front of the box so that it operates (opens) when the lid is removed.

The key switch is fitted to the front of the box on the lid. The unit can be then wired up as shown in Fig. 3. Two brackets are made up to fit onto the pram and are fastened to the rear by fixing screws. Two of these screws also serve to fix into position the Veroboard assembly.

The battery is soldered in as it should be quite a while before this needs replacing; also the battery is difficult to connect using other methods and as reliability is required, soldering seems to be best. The lid is fastened on making sure that the microswitch operates correctly.

## FITTING AND TESTING

The pressure pad is fitted underneath the baby. If extra pressure is required (because the baby is very light) either place some extra weight on the mat to "bias" it, double the mat or place under the mat a piece of hardboard with indentations in it. The mat seems to operate better sometimes by point pressure rather than overall pressure. The pressure mat wires should be long enough to pass through a pram wheel and join the main unit via a jack plug.

## TESTING

When testing the unit allow it to be turned on for some time before triggering it, this enables Cl to charge fully and thus provides a check on


Photograph of the circuit board for the Baby Snatch Alarm.
the delay time. Adjust VRI to provide the required time delay before the alarm soundspossibly one or two seconds.

In use the mat can be left in the pram and connected to the unit by passing the lead through the wheel and plugging in the jack plug when needed. The unit is then turned on by operation of the key switch and the key removed. When the mother returns, she turns off the unit with the key, unplugs the mat and pushes the pram away.

## PRACTICAL ELECTRONICS

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## THE GOOD COMPANIONS



## TEMTH-11" 74 FOR BEGMWERS IV ELECTRONCS ... THEDRY AND EXPERMEWTS

## TUTOR: PHIL ALLCOCK* <br> LESSON 3 Zener diode and the Gapacitor

IN addition to the IN4001, the shopping list includes a second diode known as a Zener diode. This component is very similar to the IN4001 diode except that the maximum current is less and the breakdown voltage is carefully controlled during manufacture to be close to a specified level, in this case 4.7 volts $\pm 5$ per cent. Diodes such as this are sometimes called breakdown diodes and they are specifically designed to be used in the reverse direction at the breakdown voltage.

In Fig. 2.8 the diode voltage in the breakdown region is almost constant and independent of the reverse breakdown current. Providing the current and power dissipation are restricted the diode can be operated in this manner to give an almost constant voltage difference of approximately 4.7 volts without harmful effects. The dissipation limit for the diode specified is 400 mW ( 0.4 watt) and since the voltage is 4.7 volts the reverse breakdown current must be limited to a maximum value of

$$
\begin{aligned}
& I_{\mathrm{mas}}(\mathrm{~mA})=\frac{400}{4 \cdot 7} \quad\left(\mathrm{~mA}=\frac{\mathrm{mW}}{\text { volts }}\right) \\
& \approx 85 \mathrm{~mA}
\end{aligned}
$$

Figure 3.1 shows a circuit using the Zener diode. Notice the different symbol for the Zener diode and also the direction in which it is connected relative to the battery polarity.

Fig. 3.1. Circuit using a Zener diode.


With the switch closed the full 9 volts is applied to the 100 ohm potentiometer but only a fraction of this voltage is fed to the Zener diode via the 1 kilohm current-limiting resistor. As the potentiometer slider moves from $A$ towards B the fraction of this 9 volts passed to the diode increases until a point is reached, about mid-way along the $100 \Omega$ potentiometer, at which the voltage equals the Zener breakdown voltage of $4 \cdot 7 \mathrm{~V}$. Up to this point no current can flow via the 1 kilohm resistor but once the breakdown voltage is reached, or exceeded, current can flow via the 1 kilohm and the Zener diode.

Since the voltage across the Zener has to remain almost constant the excess voltage supplied by the potentiometer must appear across the 1 kilohm resistor. It is this resistor which limits the diode current to a safe value when the potentiometer slider is at point $B$. Under these conditions the Zener current will be approximately

$$
\frac{(9 \quad 4 \cdot 7)}{1 \cdot 0}=4 \cdot 3 \mathrm{~mA} \quad\left(\frac{\text { volts }}{\mathrm{k} \Omega}=\mathrm{mA}\right)
$$

If the 1 kilohm resistor was changed to 100 ohm the maximum current would be approximately ten times greater i.e. 43 mA .

## CAPACITOR ACTION

This month we are introducing another very useful component, the capacitor. Like resistors, capacitors are made in a wide range of values and there are several distinct types, but before considering these in detail we will examine the behaviour of the basic capacitor illustrated in Fig. 3.2. This is simply a pair of metal plates arranged close together but not in actual contact. The space between the plates can be filled with air or some other insulating material


Fig. 3.3. Variation of current and voltage in circuit shown.
such as dry paper or plastic.
Now we already know that the metal plate is a good electrical conductor because it has "free" electrons in its structure and these can be made to move under the influence of an e.m.f. provided, by say, a battery. However, in the circuit of Fig. 3.2 the path for current flow is different to that previously considered since the capacitor plates are not in contact.

When the switch is closed electrons leave plate $A$ and accumulate on plate $B$ and a current $l$ flows in the metallic parts of the circuit due to the applied e.m.f. Each electron "carries" a fixed negative electric charge and initially the metal plates are electrically neutral (i.e. they have their correct quota of electrons). Consequently this movement of electrons causes plate $A$ to become positively charged with respect to plate $B$, since $B$ now has an excess whilst $A$ has a deficiency of electrons.

This charge transfer, around the circuit, causes a voltage difference $V_{A B}$ between the capacitor plates which is in opposition to the battery e.m.f. Because of this opposition, the rate of charge movement (which is simply the circuit current l) decreases as the voltage $V_{\text {AI }}$ increases.

An equilibrium condition is eventually reached and the capacitor is then said to be fully charged. In this state the voltage $V_{\text {AB }}$ would be equal to the battery voltage of 4.5 volts and the current $I$ would be zero. The resistor R1 is included to limit the initial level of the current when the switch is closed. The process is similar to the flow of water from a full to an empty container. The flow stops when the water levels are equal.

Fig. 3.2. The basic capacitor and charging circuit.

SMALL GAP
AIR OR DIELECTRIC FILLEO
SEPARATION $=d$

## CURRENT AND VOLTAGE VARIATION

We are now in a position to sketch the variation of current $l$ and voltage $V_{\text {A }}$ against time in the form of a graph, as shown in Fig. 3.3. Since the capacitor is initially uncharged, $V_{A 1}$ is zero and the current is limited to

$$
I_{\operatorname{lax}}=\frac{E}{\mathrm{R} 1} \text { (from Ohm's law) }
$$

At all times the circuit voltages must obey our previous rules and so we can also write $E=l \mathrm{R}]+V_{\mathrm{AB}}$ (Kirchhoff's law).
This equation states that the sum of the voltage across the resistor (IR1) and the capacitor ( $V_{\mathrm{AB}}$ ) is always equal to $E$ and since $E$ is constant (in this case) any increase in $V_{A B}$ must occur simultaneously with a decrease in current $l$ (Rl is also constant). Clearly, when $I$ is zero $V_{A R}$ and $E$ are equal as already discussed. The rate at which the charging process occurs depends on the values of both the resistor Rl and the capacitor Cl .

The basic unit of capacitance is the farad but as this is a fairly large unit it is usual to deal with sub-divisions such as microfarads ( $\mu \mathrm{F}$ ), nanofarads ( nF ) and picofarads ( pF ). The wall chart gives the values of these sub-divisions and should be consulted as necessary until the terms and their meanings are thoroughly familiar.

## CAPACITANCE VALUE

At this stage the reader may be wondering how the capacitance value is related to the basic parallel plate system of Fig. 3.2, and the answer lies in the relationship between the charge transferred and the voltage $V_{\text {all }}$. The capacitance of a given capacitor, or system of plates, is in fact a measure of the amount of charge transfer necessary to produce a voltage difference ( $V_{\mathrm{AB}}$ ) across the capacitor, of 1 volt .

The greater the charge that has to be moved to produce one volt difference, the larger the capacitance of the system considered. In practice the capacitance is determined by the dimensions and separation of the two plates and also the type of material used to fill the space between them. This material is known as the dielectric. Increasing the plate area and/or reducing the plate separation, lead to an increase in capacitance. The above relationships are conveniently summarised:
(a) charge (in coulombs)=capacitance (in
farads) $x$ voltage (in volts) or $Q=C V_{A B}$
(b) capacitance of parallel plate capacitor $=$

$$
\text { constant } \times \frac{\text { plate area }}{\text { plate separation }}
$$

The constant in (b) depends on the material used for the dielectric.

## DISCHARGED AND STORED ENERGY

If the capacitor Cl in Fig. 3.3 was ideal it would remain charged, with a voltage difference $E$, even if removed from the rest of circuit. providing no external connection is made between the plates. If such a connection is made. say with a resistor R1 and a switch S1 as shown in Fig. 3.4, the charge would be "restored" when the switch closes and a current would flow during this process. The new equilibrium condition would be when $V_{A B}$ and $I$ are both zero. The energy lost as heat in the resistor represents the energy that was stored in the previously charged capacitor and it can be shown that this energy is given by:

$$
\text { energy }=\frac{1}{2} C\left(V_{\mathrm{AB}}\right)^{2} \text { joules. }
$$

In this equation $C$ is in farads and $V_{A B}$ is in volts. For a given capacitance the energy stored rises as the square of the voltage, so doubling the voltage increases the energy by four times. The resistor R1 limits the initial discharge current and the curves in Fig. 3.4 illustrate the variation of $I$ and $V_{A B}$ during the discharge period.

## time CONSTANT

The time to fully charge or discharge an ideal capacitor is theoretically infinite but in practice the process can be considered complete when the voltage or current change is within l per cent of the final equilibrium value. The rate at which a given capacitor can alter its state of charge is determined by the circuit "time constant" which is given by the product $C \times R$.


Fig. 3.5. Time constant graph.

If $C$ is in farads and $R$ is in ohms the product $C R$ gives the time constant in seconds.

Two interpretations of the meaning of "time constant" are possible: If the capacitor charge (or discharge) rate is maintained constant at the initial value then the process would be complete in a time equal to the circuit time constant. Alternatively the time constant is the time required for approximately 63 per cent of the full change to actually take place. Both interpretations are illustrated in Fig. 3.5.

To reach the point at which the charging is 99 per cent complete a time equal to approximately $5 C R$ is required. The charge and discharge curves are often called "exponential" and are very important-many changes that occur in nature follow the same law of variation. A large number of electronic circuits employ capacitor/resistor combinations for timing and pulse generation and we shall come across these later in the series.

## CAPACITOR TYPES

A wide choice of different types of capacitor exists and the circuit symbols used are shown on the wall chart. In addition to the capacitance value and associated percentage tolerance, it is normal to quote a maximum working voltage rating. The use of very thin dielectrics allows large capacitance values to be achieved within a reasonable volume but the voltage rating falls as the plate separation is reduced.

Some dielectrics can yield high capacitance values but are not perfect insulators and this introduces an internal leakage path between the plates which allows the charge to leak away within the capacitor itself. A further point is that the larger values of capacitance may only be available with a polarised type of capacitor, which implies operation with one voltage polarity only. Many so called electrolytic capacitors are of this form and these components often have very wide tolerances, typically +100 per cent and -50 per cent.

In some applications the temperature variation of capacitance may also be of interest. The common capacitor types and their main characteristics are listed in Table 3.1. For general circuit applications the polyester and polycarbonate types wil be quite suitable. Electrolytic types are invariably used for power supplies, decoupling and similar applications requiring large values, say $10 \mu \mathrm{~F}$ or more.

When a particular type of capacitor is specified it is unwise to use another type without first considering its suitability in the given application. This is especially true when operation at high frequencies is involved.

## SERIES AND PARALLEL

Capacitors of similar voltage rating can be connected in parallel and this gives a total

Table 3.1 Capacitors

| Type of Dielectric | Typical Range of Capacitance Values | Typical Voltage Rating | Main Characteristics |
| :---: | :---: | :---: | :---: |
| Silver Mica | 1 pF to $10,000 \mathrm{pF}$ | 300 V | Close tolerance $\pm 1 \%$. Stable, low loss. Low leakage. Used at high frequencies. |
| Polystyrene | 50 to $10,000 \mathrm{pF}$ | $30-500 \mathrm{~V}$ | $\pm 2 \%$ or better if required. Relatively bulky. Low loss. Good insulation. |
| Ceramic | $1 \cdot 0-10,000 \mathrm{pF}$ | $30-1500 \mathrm{~V}$ or more for special "suppressor" types. | Tolerance $\pm 20 \%$. R.F. applications, decoupling. Some types have controlled temperature characteristics. |
| Polyester <br> Polycarbonate | $\begin{aligned} & 0 \cdot 01-1 \cdot 0 \mu \mathrm{~F} \\ & 0.01-10 \mu \mathrm{~F} \end{aligned}$ | 50-250V | $\pm 20 \%$ or better. General purpose applications. Larger values relatively expensive. |
| Tantalum | $0 \cdot 1-500 \mu \mathrm{~F}$ | $\begin{aligned} & \text { 5-100V (Observe } \\ & \text { polarity) } \end{aligned}$ | Low leakage; polarised; stable; low voltage ratings, small size. |
| Electrolytic | Up to $10,000 \mu \mathrm{~F}$ or more. | 5-500V (Observe polarity) | High values, mainly polarised. Wide tolerance $+100 \%-50 \%$ Poor stability. |
| Variable Types | 500 or 1000 pF max. (10 : 1 max/min ratio.) Low values available for trimmers e.g.: $0 \cdot 5 / 5 \mathrm{pF}$. | 500 V or more | Air insulation types-low loss, stable. Silvered ceramic, P.T.F.E. or mica compression types for low value trimmers. |

capacitance equal to the sum of the separate components. Thus a $250 \mu \mathrm{~F}$ and a $500 \mu \mathrm{~F}$ capacitor will give $750 \mu \mathrm{~F}$ when joined in parallel (like polarity ends together-positive to positive, negative to negative when electrolytics are involved). Connection in parallel gives an effective increase in plate area, hence the increase in capacitance.

Series connection is also possible but this gives a capacitance less than the smallest value used. The rule for calculating the effective capacitance is simply

$$
\frac{1}{\mathrm{C}_{\text {effective }}}=\frac{1}{\mathrm{C} 1}+\frac{1}{\mathrm{C} 2}+\frac{1}{\mathrm{C} 3}+\text { etc. }
$$

A $1 \mu \mathrm{~F}$ in series' with a $0.5 \mu \mathrm{~F}$ would give an effective value of $0 \cdot 33 \mu \mathrm{~F}$. If the capacitors are polarised the positive of one capacitor must be joined to the negative of the next and the individual voltage ratings must be adequate, since high leakage in one component will affect the voltage distribution across all elements.

It is also possible to series connect electrolytics, back to back, to simulate a non-polarised (i.e. reversible) electrolytic but the effective value may be somewhat indeterminate as one capacitor is always effectively the wrong way round and may not yield its specified capacitance under these conditions. The voltage rating is also ill-defined with this connection.

## LEAKAGE CURRENT

The leakage current of electrolytic capacitors can be a nuisance if not allowed for in the circuit design stage. When these types are subjected to normal voltage levels, after periods "out of service", the leakage current may initially rise well above the normal leakage current level. The current eventually decreases as the electro-chemical action rebuilds the dielectric barrier.

In general the leakage current depends on the capacitance and voltage and is sometimes specified as a certain maximum current level per unit $C V$ product (farad $x$ volt). For lon leakage applications tantalum types are extremely useful but usually have a very lon reverse voltage limit above which current fion increases rapidly.

## COLOUR CODES

Some capacitors, usually below $1 \mu \mathrm{~F}$, have the capacitance, tolerance and voltage rating given by a colour code. The illustrations on the chart give details of two fairly common codes. Ceramic, tantalum bead and polyester types are often colour coded.

Next month we shall begin our study of the behaviour of the BC107 transistor and introduce some experiments using this device.

## Test No. 7

Devise a suitable layout for the circuit shown in Fig. 3.1 and wire up the components on the Tutor Board in a neat manner. Connect the voltmeter across points $A$ and $D$ and with the switch open turn the 100 ohm potentiometer to point $A$. Close the switch and check that the voltmeter reads zero. Slowly turn the potentiometer whilst observing the meter. The voltage rises at first and then remains almost constant at about $4 \cdot 7$ volts even though the potentiometer is turned fully towards point $B$.

Repeat the procedure with the voltmeter connected across the 1 kilohm resistor (point $C$ and $D$ ). In this case the meter will only begin to show an appreciable reading when the diode begins to break down. By studying the circuit and the test results, show that when connected across the 1 kilohm resistor, the voltmeter behaves as though it was a $0-10 \mathrm{~mA}$ meter in series with the diode.

## Test No. 8

This test illustrates the charge-discharge mechanism covered in this month's part. Build the circuit shown in Fig. 3.6 with the capacitor $\mathrm{Cl}=250 \mu \mathrm{~F}$. Observe correct polarity. With the switch initially in position $A$ connect the 0 to 10 V voltmeter circuit across the capacitor and check that the capacitor is uncharged.

Operate the switch to position $B$ whilst still observing the meter. 'Satisfy yourself that the operation of the circuit is correct and that the discharge occurs more quickly than the charge. Why is this so? (A charged capacitor can be discharged by returning the switch to position A.)


Fig. 3.6. Circuit for use with Test No. 8.

## Test No. 9

Repeat Test No. 8 using the $1000 \mu \mathrm{~F}$ capacitor. Using the "seconds hand" of a clock or wristwatch measure the time taken for the capacitor to charge to 63 per cent of its final voltage. To perform this test it is necessary first to determine the voltage across the $1000 \mu \mathrm{~F}$ capacitor when fully charged. This reading should be approximately 8 volts, which is less than the total battery voltage. (If you have remembered
your earlier tests you will know why this is so -if not, go back over the earlier work to find the answer!)

Work out the voltage equivalent to the 63 per cent point which should come somewhere near to five volts. This is half full scale deflection on the meter. The timing is best done with the help of a friend who can note the time elapsed when you call out that the 63 per cent point has been reached. It helps if the switch is moved to position $B$ when the seconds hand is at a convenient point on the clock face.

Use the results to estimate the actual capacitance value, which has a wide tolerance on the $1000 \mu \mathrm{~F}$ nominal value. Due to the shunting effect of the voltmeter the effective charging resistance is about 9 per cent less than the 10 kilohm resistor i.e. about $9 \cdot 1$ kilohm.

To help check your results note that a capacitor of exactly $1000 \mu \mathrm{~F}$ would take $9 \cdot 1$ seconds to charge to 63 per cent of its final voltage, irrespective of the actual battery voltage in use.

## Test No. 10

Modify the circuit wiring on the Tutor Board to match the schematic circuit of Fig. 3.7. This is very similar to the previous circuit but allows for rapid charging of the $1000 \mu \mathrm{~F}$ when the switch is in position $B$. With the switch in position $A$ the only discharge path is via the 100 kilohm and meter and the time constant is now much greater than before ( 100 seconds for a nominal capacitor value of $1000 \mu \mathrm{~F}$ ).


Fig. 3.7. Circuit for use with Test No. 10
Using this arrangement try to plot a discharge curve by taking meter readings every 10 seconds after switching to position A. Don't forget that the rate of fall of voltage (or current) will become less as discharge takes place. Several minutes will be needed for a complete discharge with the given values, as using the $5 C R$ factor, mentioned earlier, 99 per cent discharge will take 500 seconds!

After recording all the important points, dismantle the circuit and reconnect the protective meter shorting lead.
See page 686 for a progress check.


By GORDON J. KING

For record reproduction three main items besides amplifiers and speakers are involved, (i) the pickup cartridge (ii) the pickup arm and (iii) the turntable unit. The complete unit is usually finished off nowadays with a wooden plinth and tinted Perspex dust cover.

Sometimes the plinth is made sufficiently large to carry the amplifier, it then being necessary to connect a couple of loudspeaker systems and the mains supply to this. The alternative is for the amplifier to be a separate unit designed to accept the signals from the gramophone pickup.

One would rarely nowadays expect to see the loudspeakers in the same cabinet as the record playing equipment and amplifier-at least not when good quality stereo reproduction is the order of the day.

The encased three items are often referred to collectively as the record playing unit which, from a spinning stereo record, yields left and right audio signals for applying to the pickup sockets of the amplifier; this in turn driving the left and right loudspeaker systems to reproduce the two-channel stereo information.


The Toshiba SR-870 stereo deck with belt drive turntable and electret condenser cartridge.
into this in a manner where any speed change produces a control parameter change in the direction required to correct the speed-a sort of feedback system.

## V-SHAPED GROOVE

An ordinary stereo disc carries the left and right signals on the two walls of a common V . shaped groove, which means that the two lots of information are recorded mutually perpendicular and each in a plane 45 degrees to the surface of the record. The wall nearest to the centre of the disc carries the left channel signals and the other wall the right channel signals.

It is the job of the pickup cartridge to extract the signals and to present them in isolation to the left and right channels of the amplifier. For the best stereo effect it is important for the signal "leakage" from one channel to the other channel, to be as small as possible. This channel separation is given in terms of a decibel ratio, the higher the decibel value the better. The reciprocal term is crosstalk, also presented as a decibel ratio, indicating how much signal in one channel is getting into the other channel.

Any pick-up cartridge is thus expected to "trace" the modulation on the two walls and to present it in two isolated channels in an electrical form corresponding to the left and right signals which originated the modulation from the microphone system.
A pick-up cartridge, therefore, can be regarded as a generator which is powered by the mechanical energy coupled from the moving, modulated groove via the vibrating stylus assembly.


The Toshiba SR-510 stereo deck featuring direct drive turntable and condenser cartridge. Suitable for playing CD4 four channel discs.

## GENERATING SYSTEMS

The two main generating systems are piezoelectric and electromagnetic. The former is
based on the fact that an electric charge is produced when certain kinds of natural and man-made crystals are bent or stressed. The amount of electricity so yielded depends on the degree of stress.

It is noteworthy that gas and cigarette lighters are now using this principle, whereby the lighting action is arranged to bend a crystal sufficiently to produce enough electricity to cause a spark to ignite the gas!

Piezoelectric pick-ups, though, only produce a low output-often less than 1 V . This is because only relatively small stresses occur from the deflection of the stylus coupling under the control of the groove modulation. Generally, the better the overall quality of the cartridge the smaller the electric output.

As piezoelectric crystals are not very resilient it is necessary to "gear-down", so to speak, the stylus-to-crystal coupling, which means that the effective deflection at the crystal is less than that at the stylus.

The majority of early piezoelectric cartridges and pickups employed the crystal, Rochelle salt. This is rather fragile and is sensitive to temperature and humidity changes.

Recent years have seen a change from this sort of crystal to a man-made crystal based on a ceramic material. The piezoelectric effect is introduced during manufacture by an electrostatic polarizing process which orientates the crystalline structure of the ceramic so that it exhibits similar characteristics to Rochelle salt. However, the crystal is harder, chemically inert and immune to humidity and other atmospheric conditions.

It produces less output than Rochelle salt and is used mostly in the better quality piezoelectric cartridges which would normally be connected to an amplifier having sufficient input stage (preamplifier) gain to step-up the weak signals to operate the power amplifier.

A couple of well known ceramic species among the many available are the Decca Deram and the Goldring CS91E, yielding respective perchannel outputs of some 35 millivolts and 20 millivolts into 2 megohm loads.


The Decca Deram ceramic stereo cartridge is the most popular budget model ever produced; available with both spherical and elliptical stylus assemblies.

# .SPECIAL <br> JFFER! п н 

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## The Kit

To help new readers and established constructors, the staff of E.E. in conjunction with a leading supplier of tools, have put together four tools of high quality that form the basis of any constructor's tool kit. The tools are not cheap but, together with a strong, woven, greaseproof nylon "roll" are offered to readers at a saving of approximately 80 p on the recommended retail price.

The kit would make an excellent Christmas present for anyone just starting electronic con-struction-but be sure to order immediately to avoid disappointment.


## Batteries

I recently bought a transistor radio that needed 9 volts to run it. As I did not have the right physical sized batteries I temporarily wired up six HP\%s to give the right voltage and the radio did not work. Eventually
when I got the right batteries (HP11s) all was well. The original smaller batteries were new and gave the right voltage so why wouldn't they run the radio?

Assuming you did not make a mistake in wiring up the batteries we suspect that the small HP7s were current limiting. This means in simple terms that they did not have enough guts to do the job properly. Because of their small size there is not a very large area of chemically active surface within them; when you draw current from a battery, gases are generated at one of the electrodes and there is a material put in the battery especially to absorb these gases -called a depolariser.

Probably you were trying to draw a high current from the battery and the depolariser was not able to keep up with the gas generation - consequently the battery would cease to pass current. As soon as you switched off and removed the batteries the depolariser would start to have an effect and the battery would appear perfectly normal again.

## CSRs

What are the differences between a thyristor, triac and diac?

The thyristor and triac are both used to control high power alternating currents in applications such as light dimmers and motor speed controllers. The thyristor will never let more than half the total mains energy pass through it because it has rectifier properties; the triac, on the other hand, will control both positive and negative going mains excursions.

You can seldom substitute one for another in circuits because the driving circuits usually have to be different. The diac is sometimes called a trigger diode because it is a device that will not conduct current in either direction until a certain voltage is developed across it; when that voltage has been reached the device goes into conduction (in either direction) until the current that is flowing falls below a certain level and then it drops back out of conduction until it is triggered by another high voltage.


A retailer discusses component supply matters.

I suppose in other trades with the approach of Christmas the retailer has a fairly clear idea what stock he must lay in. Whether it be Teddy Bears, Socks, or Light Ale, he can judge on past experience his probable needs. The component dealer has no such yardstick. True he may sell a few more soldering irons, or multi-meters but on the whole it will depend, on what the projects are in the magazines and also whether they "catch on". Alas the line-hold on, my crystal ball is slipping so I can only cross my fingers and hope!

## Width or Depth

In addition one of the major difficulties facing the retailer is the proliferation of all types of electronic components, and he is faced with the invidious choice of stocking in width (i.e. a large variety) or depth (i.e. a smaller variety but greater quantity) and
it is becoming more and more obvious that in order to give his customers good service he will have to settle for the latter! We must trust that between all of us everything will be covered.

To accentuate the problem the manufacturers themselves are dictating terms which rule out any alternative. Only recently we had a notification from Repanco stating that in future in their "transistor coil" range not less than 100 of any type of coil could be supplied at one time. They do not supply through wholesalers and there are 16 different varieties of coil. On a quick calculation, it meant an outlay of nearly $£ 600$ in order to sell a few dozen coils. I have no doubt they can justify their decision on economic grounds, but I am sure the sober truth is that they have been wooed by the colour T.V. manufacturers.

We joined a buying group several years ago and it was
hoped that between all the members we might buy them, each member buying one range but there was insufficient interest, and so one more component bites the dust. I would like to be able to tell you that this is an isolated case, but unfortunately I cannot. I could quote probably another six examples at least. So when you ask your supplier for an XYZ coil and he tells you he has not got one, do not think he is too lazy to pick up the phone and order some!

## Asides

Being near Christmas I was hoping to tell you about the Indian who walked into our shop one day and asked us to make him a lalking kettle, and about the Pussian chauffeur who used to come down to our shop once a week in an embassy car, complete with a hammer and sickle flag on the front. He would enter and stand stiffly to attention and say "Me Sokolov, me want 7 lamp Philips'! but this would be deviating too far from the straight and narrow, so you will have to read my memoirs. Good Christmas shopping.

An effects unit for use with electric guitar or organ.

THE tremolo effect is one electronic musical effect which has become extremely popular with electric guitar and organ players, but for the average amateur user, the drawback is that commercial units are very expensive to buy. The effect of tremolo is to vary the amplitude of the input signal at a rate determined by the setting of the speed control.


## CIRCUIT ACTION

The "electronics" part of the circuit is simply an oscillator producing a sine wave voltage variation of frequency bettween about 3 Hz and 15 Hz . This varying signal is then used to modulate the signal input from the instrument. The oscillator configuration used is known as a twin $T$ bridge (Fig. 1). which gives a 180


Fig. 1. Complete circuit diagram of the Tremolo Unit.
degrees phase shift at a frequency set by the values of C2, C3, C4 and R2, R3, R1 and VR1. This shift, when added to the 180 degrees phase shift produced by TR1, connected as a common emitter amplifier, gives a total 360 degrees shift, or positive feedback, which results in oscillation.

The slowly varying signal appearing at TRI collector is taken via C6 and R8 to the "depth" control, VR2, which determines how much of this alternating voltage is fed to the base of TR2, connected as an emitter follower to buffer the relatively high impedance output from TRI against possible low impedances at the input jack sockets.

The values of Cl and C 5 are not critical, and may be anything between $40 \mu \mathrm{~F}$ and $200 \mu \mathrm{~F}$, the main consideration probably being the physical size of the components. Also Dl may be any germanium diode, TR2 should be one of the higher gain groupings of the BCl 09 , i.e. BCl 09 B or C, while TRI should be a lower gain grouping of BC107, i.e. unclassified or BC107A.

## VEROBOARD WIRING

The piece of Veroboard may be cut from a standard strip of 65 mm width ( 16 holes). Capacitors and resistors should be mounted first after making the necessary breaks in the strip and mounting holes of 4 BA or 6 BA clearance to preference, see Fig. 2. The transistors may be mounted next, and the diode last, using a heatsink on the leads of these components, especially the germanium diode.

The best way of connecting the wires, which run between the front panel and the board, to the Veroboard is to use Veropins or short pieces of stiff wire at these points, and then make the connections later, soldering the wires to the pins.

## CASE CONSTRUCTION

The front panel lid should be drilled first, as indicated in Fig. 3-the round holes are most easily and neatly made with chassis punches. A 6 mm hole should be drilled and the remainder

filed out to form the 12 mm by 6 mm rectangular hole for S1. The switch, controls and sockets can now be mounted and interwired.

The box part of the case is drilled to take the Veroboard, and in one corner, to take a Terry clip or similar for the battery mounting. When positioning these holes, make sure, of course, that none of the top panel components are fouled in any way by components on the Veroboard or by the battery.

The circuit board is mounted on spacers which are of sufficient height to ensure that the copper side of the board is clear of the metal case. The board and clip are best secured using countersunk screws, so that the base of the unit is left fairly flat. The final assembly is completed by wiring the front panel to the Veroboard. Wires between the lid and the board should be of reasonable length to facilitate removal of the lid for battery changing, etc.

## THE UNIT IN USE

As the circuit diagram shows, it does not matter which way round the amplifier and instrument are connected to the unit, which is connected between the instrument and the amplifier. It is suitable for use with guitar or organ

## Components ....

## Resistors

| R1 | $2 \cdot 2 \mathrm{k} \Omega$ | R6 |
| :--- | :--- | :--- |
| R2 | $220 \mathrm{k} \Omega$ | R $\Omega 2$ |
| R3 | $220 \mathrm{k} \Omega$ | R |
| R4 | $330 \mathrm{k} \Omega \Omega$ |  |
| R5 $100 \mathrm{k} \Omega$ | R8 | $680 \mathrm{k} \Omega$ |
| All $\frac{1}{4} \mathrm{~W}+10 \%$ carbon | R9 | $27 \mathrm{k} \Omega$ |
| R | R10 | $10 \mathrm{k} \Omega$ |
| R11 | $1 \mathrm{M} \Omega$ |  |

## Capacitors

C1 $64 \mu \mathrm{~F}$ elect. 9 V
C2 $\quad 0.22 \mu \mathrm{~F}$
C3 $0.47 \mu \mathrm{~F}$ polyester
C4 $0.22 \mu \mathrm{~F}$
C5 $100 \mu \mathrm{~F}$ elect. 9 V
C6 $4 \mu$ F elect. $9 V$
C7 $1 \mu \mathrm{~F}$ elect. 9 V
Potentiometers
VR1 $25 \mathrm{k} \Omega$ carbon log. VR2 $500 \mathrm{k} \Omega$ carbon lin.

## SE SHOP TALK

Semiconductors
TR1 BC107 or BC107A silicon npn TR2 BC109B or BC109C silicon non
D1 OA91 germanium diode
Miscellaneous SK1 standard jack socket SK2 standard jack socket S1 s.p.s.t. slide or toggle switch B1 9V PP3 battery
Battery connectors, Veroboard 14 holes by 16 strips $\times 0.15$ inch matrix, aluminium case $138 \mathrm{~mm} \times 74 \mathrm{~mm} \times 40 \mathrm{~mm}$ (approx), knobs for VR1 and VR2.


## TREMOLD UNIT

Fig. 2 (above) Layout and wiring of the components mounted on the Veroboard.

Fig. 3 (right) Layout and wiring of the complete unit.


#  By GEORGE HYLTON 


#### Abstract

"How is it that carbon resistors, all about the same size, can have quite different power ratings?"


Traditionally, carbon resistors come in standard wattage ratings such as ${ }_{2} W, 1_{4} W,{ }_{8}^{1} W$ and so on. In recent times, however, resistor makers have taken to quoting power ratings which take into account the ambient temperature in which the resistor has to work. The basis of power ratings for resistors is temperature.

There is always some temperature which is high enough to damage the materials from which a resistor is made. One source of heat is the power dissipated in the resistor when current flows through it. Even if there were no other source of heat, this selfheating would impose a limit to the power which could safely be dissipated in the resistor.

In practice, the resistor has to operate in surroundings which may raise its temperature even when no power is being dissipated. This explains those puzzling differences in power ratings.

## AMBIENT TEMPERATURE

To illustrate the point, let's conduct an imaginary experiment with a resistor. This resistor has a maximum safe operating temperature of exactly 100 degrees centigrade. Anything higher will destroy it. We now pop it into the oven with the thermostat set to 100 degrees centigrade. Our resistor is kept at its upper temperature limit by the ambient temperature inside the oven alone. Any more heat and it will die.

If, keeping it in the oven, we pass any current through it at all, its temperature will pass the safe limit and the resulting chemical changes will destroy it. Our resistor may, in ordinary circumstances, be $1_{2}$ watt type,
but in the oven, to all intents and purposes, it's a zero-watt type.
If we relent a little, and turn the oven down to 90 degrees C, we can pass a little current through the resistor without damaging it. But only enough to raise its temperature by 10 degrees $C$, that is, from 90 degrees $C$ back to 100 degrees $C$ again. Any more, and it's finished. So it's still far from being a $1_{2}$ watt resistor.

If we go on turning down the oven, to 80 degrees C, 70 degrees $C, 60$ degrees $C$ and so on, at each new lower temperature we can safely put more electrical power into the resistor. Eventually we shall have reduced the temperature so much that our "1 2 watt" resistor will really be able to dissipate ${ }^{1_{2}}$ watt of electrical power without coming to grief.

## ACTUAL DISSIPATION

How do you know what temperature allows the full power rating to be achieved? You don't, without consulting the maker's data on the particular type of resistor you are using. If the resistor happens to be a type made for military use the rated ambient temperature may be quite high, say 70 degrees $C$.

It will be obvious from our oven experiment that such a resistor, if rated at $1_{2}$ watt at 70 degrees C, will safely dissipate more than $1_{2}$ watt at room temperatures of $20-25$ degrees $C$. By the same token, a resistor intended for use in domestic equipment and rated to dissipate ${ }^{1} 2$ watt at 25 degrees C will certainly not stand up to $1_{2}$ watt at 70 degrees $C$. On the other hand, it will probably be much smaller than its military, high-temperature counterpart, of
the same apparent power rating.
Our "resistor - in - the - oven" example was highly artificial and unrealistic in one respect. We assumed for the purpose of the argument that a sharp dividing line could be drawn between a safe operating temperature and a lethal one. Real life isn't like that, and the dividing line is blurred. As the temperature is raised, the destructive chemical reactions are speeded up, but they still go on, slowly, at lower temperatures, gradually destroying the resistive "track" and so altering the resistance. If your particular application can tolerate a 10 per cent change of resistance over the lifetime of your equipment, then you can work your resistors harder than if only a one per cent change can be tolerated.

## SPECIFICATIONS

This idea of the allowable change of resistance over a period of time is built into some makers' specifications. The Mullard CR25 resistor is an example. Graphs are published which enable the user to select an operating power which ensures that the resistance stays within known limits.

You can now see why some makers quote several ratings for the same resistance. A resistor with, say, 0.5 per cent tolerance may be expected to stay within, say, one per cent of its nominal value for 1000 hours at one dissipation, within five per cent at another, higher dissipation, and within 10 per cent at a still higher one-all at a specified maximum ambient temperature,

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When desoldering printed circuit boards one frequently comes across multi-terminal components such as integrated circuits and transformers which defy desoldering owing to the small size of the average soldering iron bit. To effectively increase the area of the bit a few turns of heavy gauge wire round the soldering iron bit will allow such components to be desoldered. A similar extension, with a protruding wire, can be used for cutting through thermo-plastics, which tend to mess-up a soldering iron bit if used directly.

> N. Howard, Rutland.

This idea came to me while I was trying to find my solder reel in amongst the pile of "junk" accumulating on my workshop bench. At that time my components were stored in plastic interlocking storage drawers often advertised in this magazine. My solder reel fits neatly in the smallest of these drawers. To make the solder run freely a hole must be drilled slightly larger than the diameter of the solder in the middle of one side of the drawer and the case. I have since made a wire feed based on this same principle.
A. Freed,

Bucks.

I have found a useful and inexpensive way of making microphone or earpiece holders. A plastic, one ounce ground pepper container obtainable from nearly all food stores is ideal from the point of view of size and the perforations in the lid avoid the necessity of making further holes. The microphone or earpiece is easily mounted with adhesive, in the lid behind these holes and the flex can be brought through the bottom of the container which, although quite strong, is light and very easy to cut.

> S. M. Poultney, Bath, Somerset.

[^2]

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T was interesting to see one reader commenting in a recent letter that if we published any more audio effects units he would go mad and start pulling his hair out-I hope he does not as we don't like losing regular readers. The comment is of course a valid one but with fantastic interest in audio and special effects it is difficult for us not to publish such items regularly. A case of providing designs for the majority. Anyway there are always one or two other items in each issue that are aimed at different fields and this one is no exception.

## Baby Snatch Alarm

Although basically simple the Baby Snatch Alarm does incorporate one or two rather unusual components such as the pressure mat, key operated switch and the illuminated sign, apart from these three items the components are quite straight forward.

Taking the switch first, a basic switch is available from Home Radio or Henry's Radio but the ignition switches in cars are rather better as they use a better type of key and are thus less easily "picked". A breakers yard should be able to provide the switch but you may need to get the key from a garage. The pressure mat is only available from J. Bull as far as we know.

The lamp has proved rather more difficult to get-a suitable one is available from Home Radio but can only be supplied with the wording engraved and these are thus rather expensive (about $£ 1 \cdot 25$ ). Various types are available from smaller suppliers-particularly ex-equipment types. If you cannot get a similar one it is possible to mount a piece of opaque Perspex on the front panel and use two "L" bracket type lamp holders behind it to illuminate the lettering.

Incidentally, the lettering is best added using Letraset and spraying over with clear varnish to protect it.

## Tremolo

The Tremolo can be dealt with very quickly by saying that all the components should be readily available. If necessary a footswitch may be added in parallel with the on/off switch, so that the unit can be foot operated when required.

The values of the electrolytic capacitors are not critical.

## Auto-water

Once again few component buying problems for the Autowater but some comment on one or two parts may be useful. The integrated circuit used is available in two types of case; this project uses the 14 pin dual in line (d.i.l.) type and, if the wiring diagrams are to be followed this type should be obtained-it is also a good idea to get a socket for the i.c. to prevent damage when soldering.
The relay must work mechanically and must possess at least two sets of contacts-so that it operates correctly-the contacts are not used for electrical connections and can thus be of any type.

Finally an unusual item, the drainpipe, this should be available from most d.i.y. shops-the diameter will need to be about 6 inches, we think this is more correctly called sewer pipe.

## T:MDI-11'74 Qustion TME

IF
F you wish to test your progress in the Teach-In '74 series so far, why not have a go at answering the following questions. The questions are based on the material presented in the first three parts. Answers next month.

1. Are electrons positive or negative?
2. How are current and charge related?
3. What does Ohm's law state?
4. What is the effective value of $10 \mathrm{k} \Omega$ in parallel with $22 \mathrm{k} \Omega$ ?
5. What is the maximum current allowable for a 1 watt, $1 \mathrm{k} \Omega$ resistor?
6. What colours represent $\pm 1 \%, \pm 5 \%$ and $\pm 10 \%$ in the resistor code?
7. What resistance value is coded Red, Violet, Yellow, Gold?
8. If the negative terminals of two 4.5 V batteries are connected together what is the voltage difference between the remaining two terminals?
9. If the dielectric of a capacitor is made thinner what happens to the capacitance?
10. What is the time constant for $R=10 \mathrm{k} \Omega$ and $C=$ $22 \mu \mathrm{~F}$ in series?
11. What energy can be stored in a $1000 \mu \mathrm{~F}, 100 \mathrm{~V}$ working voltage, capacitor?
12. When constructing the $0-10 \mathrm{~V}$ voltmeter must the resistor always be connected in the positive lead?
13. Does the band marking on a diode indicate the anode or the cathode connection.
14. A battery, resistor and diode are connected in series. The voltage across the diode is approximately the same as the battery. Is the diode (a) forward biased, (b) reverse biased, (c) damaged?
15. What is the maximum current allowable via a $10 \mathrm{~V}, 400 \mathrm{~mW}$ Zener diode?
16. What value results from $1 \mu \mathrm{~F}$ in series with $5 \mu \mathrm{~F}$ ?
17. Does a lamp bulb have a constant resistanice?

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# Demo circurs (II) ${ }^{\text {By Mixiz miatils }}$ <br> <br> The Hartley Oscillator 

 <br> <br> The Hartley Oscillator}

To look at the conventional way a Hartley oscillator circuit is drawn it is rather difficult, at first, to grasp what is going on. In an attempt to simplify the explanation of how it works we have started off with a circuit that is more in keeping with the type of transistor stage we have come across so far. In actual fact there is no difference whatsoever between the circuits of Figs 11.1 and 11.2

## BASIS OF OPERATION

Anyway, look at Fig 11.1 for astart! Transistor TR1 is basically a grounded emitter amplifier stage but instead of a resistor as a collector load we are using the primary winding of a transformer T1. Resistors R1, R2, and R3 are the normal biasing resistors we have come across before and C3-if we were to use it-would be the emitter decoupling capacitor to prevent negative feedback between emitter and base. More about C3 later.

Notice that Tl is wound so that the signal at point $B$ is out of phase with that at point $A$ (relative to the common point $C$ ). You can tell that there is a phase reversal between primary and secondary of the transformer by noting the


Fig. 11. 1. A basic Hartley circuit with the circuit layout slightly modified to ease the explanation.
dots that show the starts of the respective windings.

Forgetting Cl for a moment, consider what is happening if we assume that the transistor is working as an amplifier that has its output signal fed back (in phase) to the input. When the circuit is switched on for the first time the bias current into the base of TRI will make the voltage at $A$ fall slightly; this induces a rising voltage at $B$ and this is fed back to the input via C2 to point $D$. The effect of this rising voltage across C2 injects extra base current and the transistor conducts more making the voltage at A fall further.

If this argument is continued it can be seen that there is a form of positive feedback which continues until the transistor is fully conducting. When this happens there will be no further change in voltage at $A$ and hence no induced voltage at $B$; consequently the feedback signal falls and this makes the transistor cease conducting and the voltage at $A$ rises. Again positive feedback assists because the rise in potential at $A$ makes the voltage at $B$ fall-this reverses the direction of the feedback current which now opposes the bias current; this process continues until the transistor is turned off.

## WAVESHAPE

One of the features of the Hartley oscillator is that it produces a very stable sinusoidal waveform but to achieve this end there are two points to consider. Firstly how do we prevent the transistor going from fully conducting to totally cut off (to get a pure sinewave we must not clip the waveform); secondly how do we control the frequency?

We will deal with the waveshape first as it is the simplest problem. The answer is to control the amount of positive feedback so that it is sufficient to maintain oscillation but not so high that clipping occurs. This can be done in one of two ways; either by reducing the turns ratio between primary and secondary of Tl or by deliberately introducing an amount of negative feedback that will negate the positive feedback to some degree. The latter technique is preferable because by its very nature it is self compensating to a fair degree.

In our example we are going to use a transformer with a 1 to 1 turns ratio, so we have ample feedback signal, and to keep this in bounds we can inject a considerable amount of negative feedback by totally removing the normal emitter decoupling capacitor C3 (that is why it is shown dotted). Later on if you make the circuit you can experiment with fewer turns on the secondary and you may have to reduce the amount of negative feedback to maintain oscillation; this is done by introducing progressively larger values of capacitance for C 3 .

## FREQUENCY CONTROL

To see how the frequency is controlled it might be better to look at Fig 11.2.' First, assure yourself that it is identical to Fig 11.1 except that instead of a symbol for a transformer we have used a single winding inductor, centre tapped. Don't worry though, this is identical to T1 of Fig 11.1. Point $C$ is the same common point which is connected to the positive rail and you can, if you like, consider the single winding as being two adjacent windings on the same core having the start at $A$ for the winding between $A$ and $C$ and the start at $C$ for the winding between $C$ and $B$. The reason for using a single winding is that in this instance we can dispense with one of the four lead out wires shown in Fig 11.1 (it is easier to make!).
Having sorted out the circuit now look at the position of our Cl ; it is across the terminals of inductor Ll. This forms a tuned circuit that has maximum impedance when the reactance of Cl equals the reactance of Ll and this can only occur at one frequency,

$$
\text { i.e. when } 2 \pi \mathrm{fL}=\frac{1}{2 \pi \mathrm{fC}}
$$

where $f$ is in Hz , L in henries and C in farads.


Fig. 11. 2. A more conventional schematic for a Hartley Oscillator.

By doing a little algebra it can then be shown that maximum impedance is obtained at a frequency given by:

$$
\mathbf{f}=\frac{1}{2 \pi \sqrt{ } \mathrm{LC}}
$$

When the tuned circuit Ll Cl shows maximum impedance maximum voltage drop across it will be obtained. Thus, in simple terms, it can be seen that the feedback signal amplitude at $B$ will be maximum for only one frequency and it is at this frequency that the circuit will prefer to oscillate. If, however the amount of positive feedback is too great, not only will this distort the waveshape but also incite the circuit to oscillate at other frequencies-it is quite common to encounter a phenomenum called "squegging" when the circuit tries to oscillate at two frequencies at the same time. In audio circuits this sometimes sounds like an outboard motor ticking over (depending on the frequencies involved) and is known as "motor boating".

Fig. 11. 3. A practical Hartley Oscillator.


## PRACTICAL CIRCUIT

A practical demonstration circuit is shown in Fig 11.3, this will oscillate quite happily in the upper audio frequencies. L1 has an inductance of about 1.5 mH and can be made by winding 350 turns of 32 to 36 s.w.g. enamelled wire onto about 75 mm of $3_{\text {ginch }}$ diameter ferrite aerial rod. At 175 turns, a length of the wire should be looped out of the windings to form the centre tap.

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## Beta Down Under

Having been interested in electronics for only a short while, I have found Everyday Electronics and more especially the Teach-In '74 series, to be most useful and informative for beginners like myself, and without it I probably would have given up long ago. Thank you.

For quite some time now I have wanted an electric guitar, but could never find sufficient finance to buy one commercially, so I was highly delighted when the project on the Beta Electronic Guitar was announced. I waited until I had all three issues concerning the Beta before embarking on my first electronic project.

I realised I would have trouble obtaining the transformer type M218 and probably the jack socket without sending. to England for them, but decided to go ahead anyway and make as many of the parts as I could, including the pick-ups.

The materials and components were gathered together from three different states of Australia, and with the help of friends and an understanding wife, the guitar was manufactured on the kitchen bench.

All was completed and ready to go except for the transformer, and all enquiries for a 5 ohm to 50 kilohm matching transformer
turned up zero, so with the help of a very good friend and technician, a single transistor pre-amp circuit was developed to take its place, which, with a few modifications to original circuits, has done the job very well.
I am so pleased with the performance and sound of the guitar, plus the big saving in cost, that if anyone else in Australia is building or wanting to build the same, and is having the same difficulties as I had, I would be only too pleased to be of any assistance with information if they care to write to me.
Thank you once again for helping me get started in electronics through your magazine.

T Holmes,
152 Heber St.,
Moree, 2400
N.S.W.

Australia.

## Battleground

I was interested in Mr. R. Macdonnell's letter, Everyday Electronics July 1973, which mentioned various kits. He seems to have enjoyed a great deal of success with his equipment which functions correctly after being assembled and wired. My own experience however is that correct assembly and wiring with good soldered joints does not guarantee satisfactory operation of
electronic equipment.
Some years ago I caught the radio bug and decided to put together a t.r.f. radio or "straight" set as it is sometimes called. This receiver was a three valve plus rectifier set in a cream plastic case, and it produced a mains hum when switched on.

I then went to work on it by removing the metal rectifier and fitting a double-diode valve in its place. My joy was short lived lowever, because having removed the mains hum I now had a modulation hum from the loudspeaker.

Two 0.02 microfarad 1000 V capacitors connected to each anode of the rectifier cured this trouble. Then transistor radio's appeared and I simply had to have a shot at these not knowing what lay in wait for me.

The first attempt was a complete failure and it was sent back from whence it came, my own fault of course, printed circuit soldering had defeated me (incorrect soldering iron-too large) produced many dry joints.

At present I have a transistor radio waiting for a new volume control because the one sent had faulty switch contacts. Has any other reader found it a battleground of electronics.
W. J. Mitchell

Lancs.

## Price

As a schoolboy, I would like to thank you for putting your magazine and your projects within both the scope and pocket-money of the schoolboy enthusiast; I have already constructed quite a few of your ideas, and still find money for more!
N. D. Tyrrell,

Nr. Bristol.


## COMPETITION WINNER

The first prize-winner of EVERYDAY ELECTRONICS soldering competition Mr. David Riley (right of our picture) with the Viscount Audio System donated by Radio and T.V. Components (Acton) Ltd. On the left are Editor Fred Bennett who made the presentation, and Assistant Editor Mike Kenward. Mr. David Riley whose home is at Orpington, Kent, has just entered University to study medicine.

One hundred runners-up have been awarded prizes consisting of soldering equipment donated by Adcola Products Ltd., Antex (Electronics) Ltd., and Multicore Solders Ltd.

EVERYDAY ELECTRONICS thanks all firms concerned for their valuable support for this contest.

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## RECORD PLAYBACK HEADS

## （TRUVOX）

2 treck record playback heads bop each．
A track record playback heads 7 tip each．
Erae heads are aleo avallable eeparately 2 track 88－4trect 85
TINIEST AUDIO UNIT
Althougb only the name slye an an oxo cubo them are completely self contained and en mprise microphone， 3 transiator ampliner with voluthe control and battery compartment and Anally a dynanile earplece．All in on plattic cane．Mado by Anient（gold，we belleve at over 850 each）．Thene ear tubl bat we are not melling these as bearing alds only for the mitero miliget parta they contali． belleved to be in perfect worting order but not testen．Price A5s 50 emeb．


## MAINS MOTOR

Precimitu mode－an used In dern－bleal alwo for extr actor fan，blower，heaters，etc．New and perfect．Snlp at 6p． Pontare $90 p$ for frat one then 10p for each one ordered
1 ntock motor $94 p$ ．
NEED A SPECIAL SWITCH

both contect 10 for 10 p ．Plantic puah rod uitable for uperating．©

## Resettable fuse

How lone does it take you to renow a fuve？Time yuurmelf when next one
blowa．Then reckoning zour time t il per hour nee now quickiy our remettable fuse tanto circrat breaker， will pay for itealh．Prioe ouly $\mathrm{E} 1 \cdot 10$ each or 212 per dozen，specify 5,10 or 10 amp－simeny
At im slen of swifich．

MAINS OPERATED CONTACTOR
$380 / 240 \mathrm{v}$ ． 50 ofye colenold With lamingted core so very alroult anch ratid at 10 ampa Extramely well made by Extrumen Flectrical Company． Overall alre $21 \times 2 \times 2$ an． se8 ench．
1 REV．PER MINUTE MOTOR

## WITH GEAR－BOX

Mede by the famous Cbamberian \＆Hookhant Ltd．These could be made to drive clock or similer．Really robust relimble unit

## Price 1.10 each

AUTO－ELECTRIC CAR AERIAL Whth dawhoard control swith－fully extendable to 40 in or fully retrac Leble．Bulteble for 12 V poaitive or megative earth．sapplied complet Whed diting inilructions and ready $25 p$ poot and lnmurance．


## MAINS TRANSISTOR POWER

## PACK

Dengmed to operate transistor acta and ampllaers． Adjustable output $6 \mathrm{v} ., 9 \mathrm{v}$ ．， 12 volte for up to 800 mA （clan B working）．Taken the place of any of the following betteries：PP1，PP3，PP4，PP6． PP7，PP9 and othere Kit compises：mains tranaformer rectiter，smoothing and lasd reaistor， $81 \cdot 10$ ．plus 20p poatage．

AFER SWITCHES 2 pole， 2 way－4 pole， 2 way－ pole 4 way－9 pole， 4 way－ 2 pole each．

DRY FILM LUBRICANT Dry Film Libricmat．In acromol can for lubricant tato places where the nor． mal ofl can cannot mach．Home and
everyday uses．We have purchened －large quantlly of theoe from the
Dopyill to yof for sbout half of the original list price．野p per（ 8 oz ．）can or 12 canst for 85 poet pald．The lubricant io I．C．l．tuon Ll69．

## MUETI．SPEED MOTOR

 Bix apeods are available 500,850 and 1.100 r．p．tn．End $8,000,12,000$ dianeter sud approximetely 1 in longe $250 / 240 \mathrm{v}$ ．It apeed may b farther controlled with the use of our Thryrfter controller．Very powerful and uaeful motor alre approx． 2 in．dla．$\times 8 \mathrm{im}$ ．long． Price 97 plus 2 pp postage and
## SLIDE SWITCHES

滒lide 8witch． 2 －pole changeover panel approx．In $x$ in rated 200 V limp． 8 p each． 10 for Thp．Ditto an abnve but lab 1 in approx．）between fixing centres．20p each or 10 for 11.90 ．BP Change over apring return 250 v 1 amp． 110


15A ELECTRICAL PROGRAMMER
Learn in your aleap： Have radio playing and kettle boiltay as you awake－swich on IIGht解 an othical promeminar do if you inveat in an elsctrical programmer Clock by famous maker with is amp，on／ou otay on up to 6 houra．Independent 60 minate memory jogger．A besutiful unit．Price fers 15 20 p \＆ P or with glaw front chrome besel 831 extra．

## CHIP RADIO

Ferrantis latent device ZN414－riven remalte etter than superhet．Bupplied complete with echnical notee and circults． 31.25 each． 10 for 118.
Hi－＠TUNER COMPONENTS
Por experimenting with the zN414．
IT m，Pleseyy Minhatare Tuntig Condenset itu wound $W$ coll and wave changer elab and IIT $\mathbf{5 0 . 8}$ ．Air apaced tuning condenser $6^{\circ}$ ferrti rod litx wound MW and LW colls and wave hange awlich， 94 p ．
ITT 10 ．8．Air spaced TC with slow motion rive $8^{\prime \prime}$ lerrit rod，with litz wound LW and MW colle and wave change awitch， $82 \cdot 20$ ． CT NO．4．Permenblity tuner with fant and dow notion drive and LW Joanding coils and


HONEYWELL PROGRAMMER
This is a dram type turs ing dovice，the or stiteh etains promeen fith tripe which are Infinitely adjuatebie for podtion． They are aleo erringed to allow 2 opera－ tions per awltch per rotation．There are 15 changeover mloro awtiches ench of 10 amp trpe oparated by the tripe thop 15 edreulta may be changed per revolution．Drive motor is malne operated 5 reve per min．Bome of the many une of thio timer are Ypechloery control，Boller ffring，Dispensing and Vending machines，Dlsplay $11 g h t i n g$ animsted and efsus，8ignalling，tc．Frioe from aakers probably over 110 each．Bpeclal enip price $38-33$ plun 25 p poot and ineurance．Don＇t mise thic terrtic barrain．

## THIS MONTH＇S SNIP

Wah TEREMOETATE．Made by the famon Bmith Inatrument Co called Colourtat．Wall mounting and io a handsome plastic case．（Cream and belfe）．Adjastable by ilider（lockable）and nay be eet to contro temperaturen from around freezing throngh to $50^{\circ} \mathrm{C}$ ．The elide panel it engraved and indicaten（froot）（warin）（very warm），etc．The thermostat －Ill control heatern，etc．up to 15 mmp at normal maipi voltage and fo Idea for living foom，bedroom and freenhouse，etc．Price $s 1$－Es．Don＇t mise this

TEACH IN＇74
Anew beginnera aeries started with the October inme of thin magatine，we will be mupplying all tbe parta for this．The inhial kit covering all component required for the frat 6 monthe is avallable post and VAT incieded－price a7 A spectal feature about our veraion of this kit la the $41^{\circ} \times 9^{\prime \prime}$ meter $0-1000$ A meter．As the author says，a large meter ja so much easer to resd than mall one．

## BABY SNATCH ALARM AUTO－WATER FOR PLANTS

 TREMELO UNITTo recelve parta for these and other feature projecta，aend the quoted approxinate arnounts and any cauh adjustment can be nuade later．

## TANGENTIAL HEATER UNIT

Thle heater ualt if the very lateat type， moot emelient，and gulet running．Is as contlig in Hoover and biower heater only．Comprises motor，impeller， 2 LW only．Comprises motor，impelier，2kW whithing 1， 2 and $8 \leq w$ ．and with thermal satety cut－out．Can be otted into any metal line case or cabinet． Only needs control switich，83．85． 2 WW．Model as shove except 2tw． 29．75．Don ${ }^{\circ}$ mise thlm．Control 8 witch 44 plun VAT P．© P． 40 p

PORTABLE RADIO CASE DE•LUXE A similar size to the above but a nore expenalve destrn． plite sop pone and Insurance．


24hr．REPEATING TIME SWITCH
Made by Bmiths then are A．C．melins operted．NOT CLOCKWORK．Ideal for poountiog on reck or shelf or can be hullt into box with 18A socket． 2 completely sdjustable time perlods per 24 hourt． 6 amp omaryeover contectic will ine．23p．Additional time contacte हैp p

## SWITCH TRIGGER MATS

8o thin in undetectable under carpet but will wwitch on with allehtest premure．For burglar alarms，mop doorn． with slifhtest premure．For burtiar alarma


HORSTMANN＂TIME E SET＂SWITCH
 Aso Amp B itah．）Just the thing if you want co a warm houe without it conting you is fortune．Tou can deley the ewitch on time of your eleotric fires，blo．up to 14 hours from entting time of you can uee the ewitch to five boont on perlod of up to 3 houra．kiqnally suikable 45 Bpecial andp price il 4 Post and ins．28p．

## KETTLE ELEMENTS

Made by tha fanous A．s．I．Co．Complete with wacher and combined fixing ring and plug obroud．Normal 2 rousd pin and fat pio barth connection and overioed reat push hutton． 2 Models－1 th（epprox．）maileble for 8 wan and other similar models－18in（approx．）auileble for C．E．C．，Hot point etc．All quick boll 2hlw eloment it 240 V ．Price si ． 88.


## BATTERY CONDITION TESTER

Made by Mallory but auitable for all batterles made hy Rver Feady and othore，mont of which are sine carbon Tpe but aleo mercury manganeen－alced－ailver oxide dummy loed on the battery and the matar seste fndicates tbe condition depending upon which soction the polater reate．The atection reade＂replece＂＂wath＂or＂good＂．The tester to completo in ito cepe，slise $31^{\circ} \times 6 \frac{1}{*}^{\circ} 2^{\circ} x$ with lemde and prode．Price 4.50 plat 20 p pontage．

## －I2WAYSUR－

MULTHCORE CABLE 7.0076 oopper coree each core P．V．C． insulated and of different colour． P．V．C．covered overall and approx．


SNAP ACTION SLIDE SWITCH
Rated 5 s .240 v ．Miede bs Arrow．Type titied in the handles of electric drills， vacuums，etc． 51 each． 10 for 84 p ．

EDUCATIONAL KITS－all with pictorial instructions


THIS BALAN KIT FREE． Regde educational tits．Japanem insde，thewe are excellent valua do not expect to be able To Tepert fin ofter once atocks are wolld． Brief dencription of each kit in given below and with 3 kils or more we give PREE an accurate peld，Epeclal price for all 7 kits $38-00$－ith pree pold．Epecis price for sll 7 kits $2-00$ with free EAR Lons
CAL Lons Eit．Bleven perte，including candle， one concave lens，one convex lens，atage and all through difterent lenses．Thirteen parts．Top of pump in transparent no that operating parta may be obeerved．Sniall parts are brightly coloured to be meen easily while worklig．Three typea of pump nisy be made：Liti Pump，Porce Pumy and Porce Pump with renetvoir and nosale． EA4 Beaser Eth，Bleven parth．Transparent covers allow the operation of buzser to be neen．Hilustralen and taaches how electromagnetlatm，with an EA7 Electro－tegnet Eit．Pifteen partu，includea SA7 siectro－Legnet Eit．Fifteen parti，inciodes compasa．Makes two electro－niaguets，one with
one layer of wire and une with weveral layera of one layer of wire and one with wera iayers of
wire．Pick up tackn，nalis and any anial parta showlag how magnetiman work．
KA8 Curgent and Desimtanoe Kit．Twanty－nime parts．including bench and light bulb．Conduct interecting and edocational projecte to learn the application of＂OHMB LAW＂and see the vifiler ence in current sul resistance with difterent typee and lengthy of wire．
EA9 Bell Eit．Eight parta，incloding bell and puah button switch．Build a consplate electric bell and mee bow the hammer ln trigered to make the bell ring． klt，easy to conatruct，simple to operate．

MINIATURE SEALED RELAY Anverican insde．Our Ref．No．
REL A！．Measures only $f^{\prime \prime}$ wide
$\times$ im

 fon＇t know the rontact rating
but estimate this at $s / \delta$ emps The coll realiatance in 600 ompase and 9－1＇2 rolt will clowe It．Ideal for models and mululaturined equipunent． $1 t^{\circ}$ n a pluy in melay buf we rupply complete with base．
Price 88 jincluding bare．

## TELEPHONES

Complote is ithutrated．Save
 your legs，time nad temper， elmply by putting in somat
telaphonen，Ex．G．P 0 ．not uow－but guaranteed in good condition and servicesble Bupplled witb diagram and
 tlluatrated lene Interna）bel！ 81 each．Ditto with bell but lions dial 81.58 each As illurtrated with disl and bell 81.50 each． Post etc．50p each

BAKELITE INSTRUMENT CASE
RIzo approx． $6!^{\prime \prime} \times 31^{\circ} \times 2^{\prime \prime}$
deep with bray inuart in deep fith brasy ingarth in
fomr cornery and bakelite panel．This fis and vary etrone case rulteble to hound instru． givesend special righ，tc．Prioe pax lid 110

## TELESCOPIC AERIAL

Ior portable，car radlo of tranmitter．Chrorne plated－ 7th．Holo in bottom for 6BA 7 terew 47 kn ．Hole in bottom for 6BA crew．
KNUCKLED MODEL FOR F．M．SSp

TREASURE TRACER Complete KIt（except wooden battens）to make the mete detector as the circuit In Praction Wiraleen，August Isure． 88.80 plus 20p poet and ineurance

## MMEHAON HEATERS BY

REMPLOY
Standard fitting for comentic water tanown Remploy Company，Complete
 A．C．Depth into tant wilm ole for $200-240$ volt


## MAINS OPERATED

 OLENOIDS


 21․ $31 \cdot 98$ plus 20 p post and insurance．

## 

AUOIDTRONIC MODEL ATM.I
pocket multimeter. AC and DC Renlistance $0.1 \mathrm{~mA} / 100 \mathrm{~m}$. Deciliance oflotr ohms. slye $90 \times 10$ to +22 d 13 . Complete will teat fead 82.95. Post 15 p .

RUSSIAN 22 RANGE MULTIMETER A firnt class veratlle
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nabufartured U.B.B.R. to the haghent atabiarif. Range.
$80 / 250 / 500 / 1000 \%$ 10/80/250/500/1000 100 m Curtent $100 \mathrm{wa} / 1 / 10 /$ 300 ohmal3/30/300K $/ 3 \mathrm{ma}$ Complete with baticries teat leads, instructions and f485. P. \& P. 23 p
MODEL TE-200

## Mrrloat protection. 0/5/2s/125 l.000V. DA: 0/10/50/250 

## MODEL TE-300



## U4312 MULTIMETER



Model s-100TR MULTIMETER TRANSISTOR TESTER 100,000 o.p.v. mirror scale/
overioad protection. $0 /-12 /$ 8/3/12/30/120/800 $0 / 60 / 120 / 800$. V AC. $0 / 12$ DC: $0 / 10 \mathrm{~K} / 1 \mathrm{MEO} / 100 \mathrm{MEO}$ -20 to a 50 db . $0.01-.2$ MPD Alpha, mer teater measures fith inate and Ico. Complete and fade. 81495 . P/P 25 p .

## AMODEN 72.200

MULTITESTER
Itish wenaltivity tester.
200,000 o.f.x. Overlosd pro-
rection. 3lirror meale. Rangea: / / 0ff /-3/3/30/120/600 /3/12/60/300/11.200v / $6 \mu \mathrm{~A} / 1 \cdot 2 \mathrm{~mA} / 120 \mathrm{~mA}$ /loa. A. D.c.
-20 to +63 d . $0 / 2 \mathrm{~K} / 200 \mathrm{~K} / 2 \mathrm{meg} /$

## ALL PRICES ARE SUBJECT TO $10 \%$ VAT

## TMK LAB TESTER.



KAMODEN HM. 350 TRANSISTOR TESTER


## LB4 TRANSISTOR

 TESTERTents PNP or NPN tran-
alntorn. Audio
Indication. alntornt Audio Indication.
Opreraten on two l-wiv bat. eries. Complete with al P. \& P. 20p.


TE 40 HIGH SENSITIVITY

able.
22.50.
MDOEL AT2OI DECADE ATTENUATOR Frequency range 0 200 KHz . Attenustor 0 111db, 0.1 db step.
1mpedance 600 ohma.
Maz. input power Maz. Input power
30 dbm . Aize $180 \times 90 \times 58$ £12.50. Pont 37p.

KAMODEN HM. 720B F.E.T. V.O.M
 f14.98. Pont 30 p

## TMK MODEL 117 F.E.T. ELEOTRONIO VGLTMETER <br>  <br> DC VOLTS O-3- 1200 V <br> AC YOLTG $3-300 V$ DC CURRENT $12-$ to 2000 M ohm. Declbele -20 to $+81 d B$ Complete with leada/inetructlona. 217.60 . $\mathbf{P}$ \& P. 200 . <br> KAMODEN HMG. 500 INSULATION RESISTANCE TESTER <br>  <br> neter $44^{\prime \prime} \times 4^{\prime \prime}$ <br> Complete with de-

batteries instruc-

BELCO AF.5A SOLID STATE SINE
SQUARE WAVE C.R. OSCILLATOR
Aine $18 \times 200,000 \mathrm{~Hz}$; Bquare $18 \times 20.000 \mathrm{H}$


TO.3 PORTABLE OSCILLOSCOPE 3 in. tube, Yimp. Benaitivity $0-1 V$
$1.5 \mathrm{cps}-1.8 \mathrm{CM}$ siHz. Input imp. $\begin{array}{lll}2 \text { meq } \Omega & 25 \mathrm{pH} & X \text { amp } \\ \text { senaltivity } & 0.9 \mathrm{p} & \mathrm{p}-\mathrm{p} / \mathrm{CM}\end{array}$ $\begin{array}{lll}\text { Bandwith } & 0.9 \mathrm{~F} \text {. P-p/CM } \\ \text { Bepa-8004 }\end{array}$ nput tmp. 2 thep $\Omega 20 \mathrm{pF}$ Time base. 5 ranaes 10 cp
300 kilz. Branchronization.


Internal/externnl. Illuminated
acale $140 \times 215 \times 330 \mathrm{~mm}$. Weight 154 th . $220 / 240 \mathrm{~V}$. A.C. Bupplied brend new with handbook. 55250 . Carr. 6

## CI- 5 PULSE

 OSCILLOSCOPEFor dinplay of puleed and periodic waverormn in electronic circults.
VERT. AMP. Band. width 103 Mz . Benel tivity at 100K Hz VRME fitn. $1+25 ; \mathrm{HOR}$. AMP. Bandwidth 500 KH Senaltivity at 100 KHz , $\mathrm{BM} / \mathrm{mm} .3 \cdot 2 \mathrm{~m}$ Preset triggered aweep $1-3,000 \mu s e c$.: free runaing $20-200,000 \mathrm{~Hz}$ in nine raliges. Callbretor pipa. $220 \times 360 \times 430 \mathrm{~mm}$.

## RUSSIAN CI. 16 DOUBLE

 BEAM OSCILLOSCOPE ${ }_{6} \mathrm{Mc} / \mathrm{M}$ Pawn Band. Beparat Rectangular $\sin$ amplthers. C.R.T. Callbrated triz. gered aweep from -2 thec to 100 meep from $-2 \mu / 1$ nee. Free running time bane $50 \mathrm{~cm} / \mathrm{m}$ mols. Bullt In thrue bare callbrator and amplitude callbrator. Bupplied complete wlith all accesmorien and inatruction inanual287. Carf, Pald


MODEL U431: SUB.STANDARD MULTI. RANGE VOLT AMMETER

 760 V aC. Automatic cut out. Supplied com. pleto with test leads, manual and test certif. -
TMK MODEL TW-50K
46 ranges, mirror meale
$50 \mathrm{~K} / \mathrm{Vol}_{\text {ol }} \mathrm{D} . \mathrm{C} . ~$
$\mathrm{~K} / \mathrm{V}$ olt A.O
 10K, Weck, MER, 10 MEO ©8.50. Decibels: -20 to +81.5 db

## MODEL TE. 15 GRID DIP METER



## TE22 SINE SQUARE WAVE AUDIO GENERATORS

 Blne: 20 cps to 200$\mathrm{kc} / \mathrm{l}$ on 4 bands. kryare: 20 cpn to 30 kcr. Output impe. $200 / 250 \mathrm{~V}$. A.C. ob. erstion. Supplied brand new and Ruaranteed with instruction manual end $240^{\circ}$ Wide Angle ImA Meters
$\begin{array}{ll}\text { MW } 1.6 \text { 60man square } & \text { £3.97 } \\ \text { MW 1-8 80mm squate }\end{array}$ MW 1-8 80 mm square


POWER RHEOSTATS

## High quality ceramic

 meruction. Windingsbedded in vitreous bedded in vitreoun ensmel
Meavy duty brush wiper
Contlinuous Continuous rating. Single hole nxing. fin. dia.
shafts. Bulk quantiles gyall.
shatis.
25 WATT. 10/25/50/100/250/600/1000 ohma 1.15 P. \& P. 10p.
50 WATY
of WATT. $10 / 25 / 50 / 100 / 260 / 600 / 1000 / 2500$
or $\delta(60)$ whms. $£ 1-62$. $P$. \& $P$ P 10 p 100 WATT. 1/5/10/25/50/100/250/500/1000

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## Fully

 $18 p$$18 p$
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11

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Amateur Electronica＇－The profesalonal from basle principles to anvanced clectronic lechniquea．
OUR PRICE 88.80 ，complete with circult board for maling the Intim lirtell helom AE1 100 mW output ntage
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A F9 Treble Alter
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EFLEX HORN SPEAKER RUH． 6 Built In driver unit．
Impedence 16 ohm．
Power ratigg 10 whtt． Power ratlng 10 watt．
Reaponve $390-7000 \mathrm{~Hz}$ ． Reapone $380-7000 \mathrm{~Hz}$.
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OUR PRICE 14.97 P．＊P．30p

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Approx．7－1 ratlo planetary drive vernier dials．Log male $0-180$ degrees．Blank
scales 1 to 5 ．Bcale width overall ize a ${ }^{\prime \prime} \times 41^{\prime \prime} \times 11^{\prime \prime}$ deep including snob and corpllag． $8^{* \prime}$ dla，ahatt．
OUR PRICE 11.62
MP7 MIXER PREAMPLIFIER


E microphone inpute each with indlvidute gain controls enabling
complete mix intlea．Buttery oper－ ated． $9 t^{\prime \prime} \times 5^{\prime \prime} \times 3^{*}$
$\mathrm{nv} 50 \mathrm{~K}: 2 \times 3 \mathrm{mv} 600$ Input Mics： $3 \times 3 \mathrm{mV} 50 \mathrm{~K}: 2 \times 3 \mathrm{mV} 600$
ohin．Phono meg． 4 mV 80K．Phono ceramic 100 mV 1 meg．Output 250 mv 100 K ．

Our Price E8．97 P．\＆P． 200

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USED EXTENSIVELY BY INDUSTRY，GOVT．DEPTS．，EDUCATIONAL AUTHORITIES，ETC．
Over 200 ranges in stock－other ranges to order，Quantity discounta available． Send for fully illustrated brochur

| Trpe SW． 100 | $100 \times 80 \mathrm{~mm}$. | Type MR．SSP． 41 in ．$x$ 4iln．fronts |
| :---: | :---: | :---: |
| ธоцA ．．．．．． |  |  |
|  |  | 500 mA ．．． |
| $100 \mu \mathrm{~A}$ |  | $1 \mathrm{amp} . . . . . .$. tien |
| 100－0－100 4 4 38 |  | 5 amp．．．．．．．．t．00 |
| $\begin{array}{lll} 800 \mu \mathrm{~A} \\ 1 \mathrm{~mA} & . . . \\ \hline \end{array}$ |  |  |
| $\operatorname{limA}_{20 \mathrm{~V}, \mathrm{DC}}^{\mathrm{c}} . . .$ |  | $\begin{aligned} & 30 \text { arp. } . . . \\ & 10 \mathrm{~V} \text { D.C. } \end{aligned}$ |
| s0V．D．C．．－${ }_{\text {ce }}$ | 5 amp．1．c． 4.60 | 20 V ．D．C． |
| 300 V ．D．C． | 300 V ．A．C．．．\％870 | B0MA ．．．．． 8440 B0V．D．C． |
| 1 emp．D．C．etere | VU Meter ．．8．50 | 80－0－50 A A st 150 V. D．C． |
| Trpe SD． 830 3．5mm $\times 110 \mathrm{~mm}$ Fronts |  |  |
|  | $10 \mathrm{~mA} \quad . . .88 .10$ |  |
|  | 50 ma ． 3.10 |  |
|  | 100 ma A $\quad . .$. |  |
|  | 500 mA ．．． |  |
|  |  |  |
|  | $10 \mathrm{mmp} . . . .88 .10$ | 10 mA |
| b0ma | BV．D．C．．． 5 S． 10 |  |
| 50－0－50 | 10V．D．C．．． 8.10 |  |
| 100\％A | 30V．D．C．．． $5 \cdot 10$ | Type MR．S2P．2tin．square fronts |
| 100－0－100 $\mu \mathrm{A}$ 粏－25 | S0V．D．C．． 88.10 |  |
| $200 \mu \mathrm{~A}$ … 23.20 | $300 \mathrm{~V} . \mathrm{D} . \mathrm{C} \text {. } 88.10$ | $50-0-60 \mu \mathrm{~A}$ 18．03 20V．D．C．．－ |
| 600\％A ．．．．．${ }^{8.15}$ | $15 v . \text { A.C. . . } 58.80$ |  |
|  | 500V．A．C．．．ASter |  |
| Trpe SD． 640 \＄3．5mm $x$ ESmm Fronts |  |  |
|  |  |  |
| 60xa | 800 mA 年 |  |
| 50－0－80pa | 1 amp．．．．．．．5．00 |  |
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## DEPT. E.E., ELSTOW STORAGE DEPT. KEMPSTON HARDWICK BEDFORD.

## RESISTORS

W lskra high seability carbon film-very low noiso-ceapless construction. W Mullard CR25 carbon film-very small body size $7.5 \times 2.5 \mathrm{~mm}$. W $2 \%$ ELECTROSIL TRS.

| Power water |  |  | Valuas |  | Price |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { erance } \\ & 5 \% \end{aligned}$ |  | available | 109 | ${ }_{100}^{10+}$ |
|  | 10\% | 3.3M0-10M0 | E12 | Ip | 0.80 |
|  | $2 \%$ | $100-1 \mathrm{MO}$ | E24 | $3.5 p$ | 3p |
| 1 | $10 \%$ | $10-3 \cdot 90$ | E:2 | 1 p | $0 \cdot 6$ p |
| t | 5 | $4.70-1 \mathrm{Ma}$ | E12 | 1 p | $0 \cdot 8 \mathrm{p}$ |
|  | 10\% | $10-100$ | E12 | ${ }^{6 p}$ | 5.50 |

## DEVELOPMENT PACK

0.5 watt $5 \%$ lskra resistors 5 of each value 4.70 to IMO.
EI2 pack 325 resistors $\$ 1.40$. E24 pack 650 resistore 4.70.

## POTENTIOMETERS

Carbon track $5 k a$ to $2 M$ o, log or linear (log tW, lln tW).
Single, l2p. Dual tang (stareo), 40p. Single D.P. switch, 24p.
.
SKELETON PRESET POTENTIOMETERS
Linear: $100,250,500 \mathrm{Q}$ and decsdos so 5 M O . Horizontal or vertical P.C. mounting ( $0 \cdot 1$ matrix).
Sub-miniature $0.1 \mathrm{~W}^{2}$. Sp each. Miniature 0.25 W . 7p each.

## TRANSISTORS

| AC107 | 15p | AFI 26 | 20p | 8 FIIS | 25p | OC42 | 12p | 2N3707 | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ACl 26 | 12p | AFI 39 | 32p | BFi73 | 20p | 0 O 4 | 12p | 2N3708 | 10p |
| ACl27 | 15p | AFi78 | 32p | 8 Fi 77 | 28p | OC45 | 12p | 2N3709 | $11 p$ |
| AC128 | $15 p$ | AF180 | 40p | BFI78 | 32p | OC70 | 12p | 2N3710 | $11 p$ |
| ACl31 | 12p | AFl81 | 40p | BF179 | 32p | OC71 | 12p | 2N3711 | $11 p$ |
| ${ }_{\text {ACl }}{ }^{\text {c }}$ | 12p | BC107 | 12p | BFI80 | 32p | OC72 | 12p | 2N3819 | 32p |
| AC176 | 15p | 8C108 | 12p | BFI81 | 32p | OC81 | 12p | 2N4062 | 12p |
| AC187 | 22p | BC109 | 12p | $8 \mathrm{8F194}$ | $14 p$ | OC82D | 12p | 2N4286 | 20p |
| AC188 | 22p | $8 \mathrm{8C1} 17$ | 12p | $8 F 195$ | $14 p$ | 2N2646 | 60p | 2N4289 | 20p |
| ADI 40 | $50 p$ | BC148 | 12p | BF197 | 15p | 2N2904 | 20p | 40360 | 35p |
| ADI49 | 45p | 8 Cl 149 | 12p | BF200 | $32 p$ | 2N2926 | 10p | 40361 | 35p |
| AD161 | $31 p$ | BC157 | 14p | BFY50 | 20p | 2N3054 | 58p | 40362 | 40p |
| AD162 | 36p | BC158 | 14p | BFY51 | 20p | 2N3055 | $60 p$ | 40408 | 40p |
| AFII4 | 20p | BC159 | 14p | 8FY52 | 20p | 2N3702 | $13 p$ | ZTX108 | 15p |
| AFIIS | 20p | BC187 | 22p | BUYI05 | 225p | 2N3703 | 12 p | Z $\mathrm{T} \times 100$ | 15p |
| AFII6 | 20p | BD131 | 75p | OC26 | 45p | 2N3704 | 13p | ZTX302 | 20p |
| AFII7 | 20p | BD132 | 750 | OC28 | 50p | 2N3705 | 11p | $2 \mathrm{~T} \times 500$ | 15p |
| AFIIB | 38p | BDI33 | 75p | OC35 | 50p | 2N3706 | $11 p$ | ZXT503 | 20p |

$\left.\begin{aligned} & \text { ZENER DIODES } \\ & 400 \mathrm{~mW} 5 \% 3.3 V \text { to } 30 \mathrm{~V}, 12 \mathrm{p} .\end{aligned} \right\rvert\, \begin{aligned} & \text { WIRE WOUND POTS, } 3 W, 10,25, \\ & 50 \mathrm{a} \text { and decades to 100k }, ~ 35 p .\end{aligned}$

## DIODES

| RECTIFIER |  |  |  | SIGNAL |
| :---: | :---: | :---: | :---: | :---: |
| BY127 | 1250 V | IA | 12p | OA85 |
| IN4001 | 50 V | 14 | $7 p$ | OA90 |
| IN4002 | 100 V | IA | 8 p | OA91 |
| IN4004 | 400 V | 14 | 8 p | OA202 |
| IN4006 | 800 V | IA | 10p | IN4148 |
| IN4007 | 1000 V | 14 | 10 p | BAlla |

BRUSHED ALUMINIUM PANELS
$12 \mathrm{in} \times 6 \mathrm{in}, 25 \mathrm{p}$; $12 \mathrm{in} \times 2 \mathrm{yin}, 10 \mathrm{p}$; $9 \mathrm{in} \times 2 \mathrm{in}, 7 \mathrm{p}$
SLIDER POTENTIOMETERS
$86 \mathrm{~mm} \times 9 \mathrm{~mm} \times 16 \mathrm{~mm}$, length of track 59 mm ,
NUAL GANG $10 K$ K $+10 K$ etc. lot or
KNOB FOR ABOVE, 12 p .
FRONT PANEL, 65p.
18 Gaute panel $12 \mathrm{in} \times 4 \mathrm{in}$ with slota cut for use with slider pota. Grey or matt black finish com. plete with fixings for 4 pots.

MULLARD POLYESTER CAPACITORS C2OS SERIES
$00 V ; 0.001 \mu F, 0.0015 \mu F, 0.0022 \mu F, 0.0033 \mu F, 0.0047 \mu F, 21 P, 0.0068 \mu F, 0.01 \mu F$ $0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F},{ }^{3} \mathrm{p} .0 .047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 4 \mathrm{p}, 0.15 \mu \mathrm{~F}, 6 \mathrm{p}, 0.22 \mu \mathrm{~F}$, 160V: $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 3 \mathrm{p}, 0.1 \mu \mathrm{~F}, 34 \mathrm{p}, 0.15 \mu \mathrm{~F}$ 4p. $0.22 \mu \mathrm{~F}, ~ 5 \mathrm{p} .0 .33 \mu \mathrm{~F}, 6 \mathrm{p} .0 .47 \mu \mathrm{~F}, ~ 7$ tp. $0.68 \mu \mathrm{~F}$, $11 \mathrm{p} .1 .0 \mu \mathrm{~F}, 13 \mathrm{p}$.
MULLARD POLYESTER CAPACITORS C280 SERIES
250V P.C. mounting: $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 3 \mathrm{~J} .0 .033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}$,
 3p. $0.1 \mu \mathrm{~F}, 4 \mathrm{p}$. $0.15 \mu \mathrm{~F}, 0.22 \mu \mathrm{~F}$,
13p. $5 \mu \mathrm{~F}, 20 \mathrm{p} .2 \cdot 2 \mu \mathrm{~F}, 24 p$.
MYLAR FILM CAPACITORS IOOV CERAMIC DISC CAPACITORS $0.001 \mu \mathrm{~F}, 0.002 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.02 \mu \mathrm{~F}, \quad 100 \mathrm{pF}$ to $10,000 \mathrm{pF}, 2 \mathrm{p}$ each.
2 f . $0.04 \mu \mathrm{~F}, 0.05 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 3 \mathrm{l}$
ELECTROLYTIC CAPACITORS
$(\mu F / V) 1 / 63,1 \cdot 5 / 63,2 \cdot 2 / 63,3 \cdot 3 / 63,4 \cdot 7 / 63,6 \cdot 8 / 40,6 \cdot 8 / 63,10 / 25,10 / 63,15 / 16,15 / 40$, $\begin{array}{llll}15 / 63,22 / 10, & 22 / 25,22 / 63, & 33 / 6 \cdot 3,33 / 16,33 / 40,47 / 4,47 / 10,47 / 25,47 / 40,68 / 6 \cdot 3, \\ 68 / 16,100 / 4 & 100 / 10,100 / 25,150 / 6 \cdot 3,150 / 16,20 / 4\end{array}$ $68 / 16,100 / 4,100 / 10,100 / 25,150 / 6 \cdot 3,150 / 16,220 / 4,220 / 6 \cdot 3,220 / 16,330 / 4,6 p$, $47 / 63$. $470 / 10,680 / 6+3$, $11 \mathrm{p} .100 / 63$, $150 / 63,220 / 63,1000 / 10,120,470 / 25,680 / 16$ is00/6. 3, 13p. $470 / 40,680 / 25,1000 / 16,1500 / 10,2200 / 6 \cdot 3,18 \mathrm{p} .330 / 63,680 / 40,1000 / 25,1500 / 16$, $2200 / 10,3300 / 6 \cdot 3,4700 / 4,21 \mathrm{p}$.


| VEROBOARD 0.1 O.IS\\| JACK PLUGS AND SOCKET |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $21 \times 340.1$ | 0.15 | Standard screened | 18p | 2.5 mm in | insulated | ${ }^{\text {b }}$ |
| $21 \times 34$ | 16p | Standard insulated | 12p | 3.5 mm in | nsulated | $0_{0}$ |
| $2 \mathrm{x} \times 5$ 24p | 24p | 5 sereo screened | $35 p$ | $3 \cdot 5 \mathrm{~mm}$ sc | creened | 13 p |
| $3 \mathrm{y} \times 38$ | 14p | Standard socket | 45p | 2.5 mm soc | ocker | 8 |
| $\begin{array}{rr}37 \times 5 \\ 17 \times 24 & 77 p \\ 75 p\end{array}$ | 27p | Stereo socket | 18p | 3.5 mm | ocket | $\mathbf{1}^{\text {d }}$ |
| $17 \times 31100 p$ | $78{ }^{\circ}$ | D.I.N. PLUGS | ND | OCXETS |  |  |
| $17 \times 5$ (plain) | $82 p$ |  |  |  | $0^{\circ} .6$ |  |
| $17 \times 3:$ (plain) | 60 p | Plug 12p. Socke | 8 p. |  | . |  |
| $17 \times 21$ plain | 42 p | 4 way icreened c |  |  |  |  |
| $21 \times 5$ (plain) | $12 p$ | 6 way screened ca |  | p/mesre. |  |  |
| pi, $\times 34$ (piain) | $11 p$ |  |  |  |  |  |
| Spot face cutter 42p | 42p | BATTERY ELIM | NAT |  |  |  |
| Pkt. 50 pins 20p | 20p | mains power sup | ly. 5 | me size a | as PP9 b |  |

LARGE (CAN) ELECTROLYTICS

| $1600 \mu \mathrm{~F}$ | 64 V | 74p | 2500 uF | 64V | 80p | 4500 ${ }_{\text {u }}$ | 16 V | 50p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2500 $\mu \mathrm{F}$ | 40 V | 74p | $2800 \mu \mathrm{~F}$ | 100 V | 42.60 | 4500uF | 25 V | C1. 68 |
| $2500 \mu \mathrm{~F}$ | 50 V | 58p | $3200 \mu \mathrm{~F}$ | 16V | 50p | $5000 \mu \mathrm{~F}$ | 50 V | CI. 10 |

HIGH VOLTAGE TUBULAR CAPACITORS-I,000 VOLT
$\begin{array}{llllll}0.01 \mu \mathrm{~F} & 10 p & 0.047 \mu \mathrm{~F} & 13 p & 0.22 \mu \mathrm{~F} & 20 p \\ 0.022 \mu \mathrm{~F} & 12 p & 0.1 \mu \mathrm{~F} & 13 p & 0.47 \mu \mathrm{~F} & 22 p\end{array}$ POLYSTYRENE CAPACITORS $160 \mathrm{~V} 2 \not 2 \%$
10pF to 1,000pF El2 Series Values, 4p each.
SMOKE AND COMBUSTIBLE GAS DETECTOR-GDI
The GDI is the world's first semiconductor that can convert a concentration of gat or smoke into an electrical signal. The sensor decreases iss electrical resistance when it absorbs deoxidizint or combustible gases such as hydrogen, carbon monoxide. methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or smoke. This decrease is usually large enough to be utilized without amplification. Full details and circuita are supplied with each detector,
excludin case. Mains operated detector C5-20. 12 or 24 V bateery operated audibla axarm C7.30. As above for PP9 battery, 46.40.
PRINTEO BOARD MARKER
Draw the planned circuit onto a copper laminate board with the P.C. Pen, allow to drypief. immerse the board In the etchant. On removal the circuit remains in high

## LARGE RANGE ITT/TEXAS IC'S NOW IN STOCK




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    Everyday Electronics, Fleetway House, Farringdon Street, London, E.C.4. Phone: Editorial 01-634-4452; Advertisements 01-634-4202.

[^1]:    Publisher's Annual Subscription Rate, including postage to any part of the world, £2.35. International Giro facilities Account No. 5122007. State reason for payment "message to payee". Address to Everyday Electronics, Subscription Department, Carlton House, Great Queen Street, London, WC2E 9PR. Binders for volumes 1 and 2 (state which) and indexes for volume 1 available for 97p and 11p respectively. including postage, from Binding Department, at the above address.

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