

Ctro

An exciting hobby .... for everyone

**SEPT. 73** 

15p

Reurit Del

An integrated circuit ensures excellent results and simplifies construction.

# Aquarium Thermostat

A simple unit that will maintain a set temperature accurately.

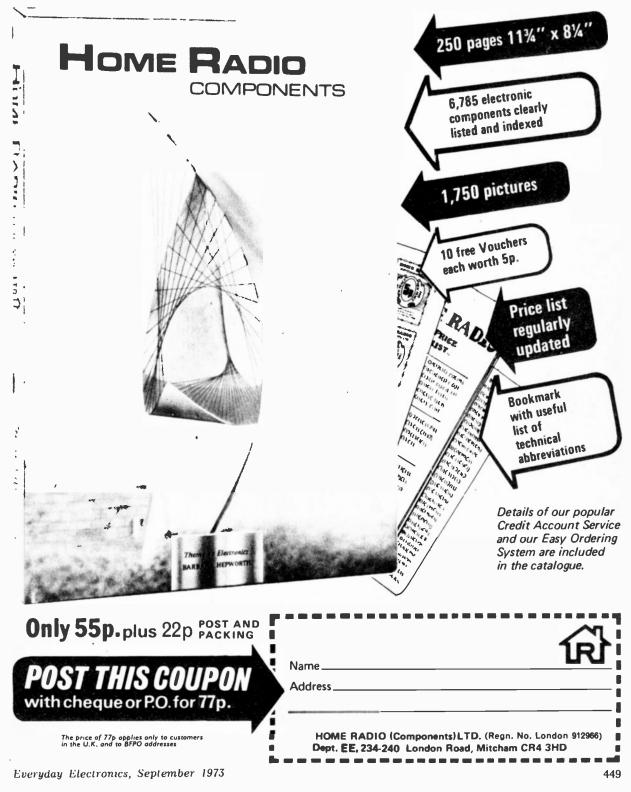
# CHIS Train Controller

Provides automatic, gradual speed change for stopping or starting, together with a manual facility to provide realistic speed control.



HOME RADIO (Components) LTD, Dept. EE, 234-240 London Road, Mitcham, CR4 3HD. Phone 01-648 8422

# The Catalogue you MUST have!



# SANSEI TEST EQUIPMENT

SIG MITTER Powerful trouble

shooting signal injector. Model

SF260

including

VAT &

**D D** 



10 Instruments in one. Including AC & OC Voltmeter, Ohm Meter

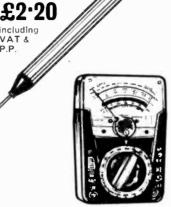
#### £11.95 VAT & P.P.



SIGNAL TRACER/ INJECTOR Designed to receive audio frequency, built in amplifier with high gain of 60dB.



Associates Ltd.





DC POWER SUPPLIES Regulated power supply variable up to 15V 0.5A. Model SE800 . . . ideal for development work.

£11.00 including VAT & P.P. NEW HIGHLY SENSITIVE MULTITESTERS Model M650 with mirror scale. £7.70 including VAT & P.P.

#### Cricketfield Lane, Bishops Stortford, Herts. Tel. 0279 56347



FIC

 $2 \times 4$  in. packed with semiconductors and top quality resistors, capacitors, diodes, etc. Guaranteed min. 35 transistors plus data. 10 boards 50p (9p). SPECIAL BARGAIN PACK 25 boards £1 (25p). Panels with 4 power transistors sim. OC28 50p (9p) FLECTROLYTICS

ELECTROLYTICS  $68,000\mu$  16v,  $4\frac{1}{2} \times 2$  in. dia.,  $25,000\mu$  25v,  $20,000\mu$  30v,  $5,000\mu$  90v,  $35,000\mu$  15v,  $8,000\mu$  55v,  $4\frac{1}{2} \times 3$  in. dia., 50p (12p).  $15,000\mu$  15v,  $10,000\mu$  35v,  $5,000\mu$  75v,  $4\frac{1}{2} \times 2$ in. dia., 30p (10p).  $2,000\mu$  25v wire ends 15p (5p), 12 for  $\pounds 1$ -50 (15p).

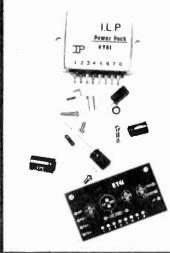
4 for £1 (7p) 4 for 50p (5p) **3A DIODES** 8 BLACK TOGGLES dpst 250 MIXED CAPACITORS 250 MIXED RESISTORS 50p (8p) 60p (8p) 60p (8p) 150 HI-STAB RESISTORS 60p (8p) 200 SI PLANAR DIODES 50p Sub min. co-ax. plugs & skts

August Antipage (2014) A pairs 50p (5p) REED RELAYS MIXED 10 for 50p (5p) MICROS MIXED 8 for 50p (8p) ASSORTED RELAYS 8 for 61 (12p) MIN. GLASS NEONS 12 for 50p (5p) O WAY TERMINAL BLOCKS 10 WAY TERMINAL BLOCKS

ID for 55p (5p) QH BULBS 12V 55W 50p (5p) PAPST EXTRACTOR BLOWER FANS 100 cfm 41 x 41 x 2in. £3-50 (28p) Postage and packing shown in brackets. Please add 10% V.A.T. to prices.

KEYTRONICS (Mail Order only) 44 EARLS COURT ROAD LONDON W8. 01-478 8499

## L.P. (Electronics) Ltd



#### THE HY41

1KH2

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05% at 1KHz into 8 ohms!) and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry.

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years.

OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts

R.M.S. continuous. LOAD IMPEDANCE: 4-16 ohms. INPUT IMPEDANCE: 30K ohms at 1KHz. VOLTAGE GAIN: 30db at 1KHz.

TDTAL HARMONIC DISTORTION: less than 0.15% (typical 0.05%)

FREQUENCY RESPONSE: 5Hz-50KHz + 1db. SUPPLY VOLTAGE: + 22.5volts D.C. SUPPLY CURRENT: 0.8 amps maximum.

PRICE: inc. comprehensive manual, P.C. board, five extra components and P. & P.:-MONO: £4.90 STEREO: £9.80

#### UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an Integrated pre-amplifier circuit.

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use. Internally the HY5 provides equalization for almost every conceivable input, the

desired function is achieved by use of a multi-way switch or by direct interconnection. Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing it to be run off any unregulated power supply from 16-25 Volts and a balance circuit

to be run off any unregulated power supply from 16-25 Volts and a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo pre-amplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HYS combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely integrated system.

OUTPUTS

#### INPUTS

Magnetic Pick-up (within ±1db RIAA curve) 2mV, 47K Ω Tape Replay (external components to suit

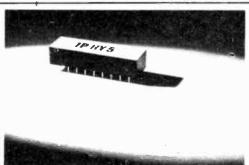
head}. 4mV, 47KΩ Microphone (flat) 10mV, 47KΩ

Ceramic Pick-up (equalized and compensatable) 20--2000mV. variable. Tuner (flat) 250mV 100K 0

Tuner (flat) 250mV. 100K  $\Omega$ Auxiliary 1 250mV. 47K  $\Omega$ Auxiliary 2 2–20mV. 100K  $\Omega$  Direct tape output 120mV. ACTIVE TONE CONTROLS (Bexendall) Treble + 12db. Bass + "12db. INTERNAL STABILIZATION Enables the HYS to share an unregulated supply with the Power Amplifier.

Main Pre-amp output 500mV

SUPPLY VOLTAGE 16-25 volts PRICE MONO: £3.60 STEREO: £7.20



SUPPLY CURRENT 6mA approx. OVERLOAD CAPABILITY better than 26db on most sensitive Input infinite on tuner and auxl, OUTPUT NOISE VOLTAGE: 0.5mV.



#### POWER SUPPLY PSU45

The versatile P.S.U.45 is designed to supply your HY41's +HY5's in stereo or mono format.

Specification

Input: 200–240 Volts. Output: <u>+</u> 22.5 Volts at 2 amps. Overall Dimensions: L. 7''; D. 3.8''; H. 3.1''

PRICE: £4.50 inc. P. & P.

#### CROSSLAND HOUSE · NACKINGTON · CANTERBURY · KENT

#### CANTERBURY 63218

Please note we reserve the right to substitute at our discretion updated versions of advertised designs where applicable.

#### MAINS OPERATED CONTACTOR

220/240v. 50 cycle solenoid with laminated core so very silent in operation. Closes 4 sirouits each rated at 10 amps. Extremely well made by a German Electrical Company. Overall size 21 × 2 × 2in each



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**NEED A SPECIAL SWITCH** 

Double Leaf Contact. Very slight pressure closes both contacts. 8p each 10 for 60p. Plastic pushrod suitable for operating. 6p 0 each. 10 for 54p.

AUTO-ELECTRIC CAR AFRIAL

AEWIAL with dashboard control switch-fully extendable to 40in or fully retrac-table. Buitable for 12V positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. 28-35 plus 25p post and insurance.

MAINS TRANSISTOR POWER

MAINS TRANSISTOR POWER PACK Designed to operate transistor sets and amplifiers. Adjustable output 6\*., 9\*., 12 volts for up to 500m A (class B working). Takes the place of any of the following batteries: PPI, PPS, PPA, PPG, PP7, PP9 and others. Kit comprises: maina transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip at only 81-10. Disa 20to noctage. \$1.10, plus 20p postage. ------

#### MINIATURE WAFER SWITCHES

2 pole, 2 way-4 pole, 2 way-3 pole, 3 way-4 pole, 3 way-2 pole.4 way-3 pole, 4 way-2 pole 6 way-1 pole, 12 way. All at 23p each



DRY FILM LUBRICANT

DRY FILM LUBRICANT Dry Film Lubreant. In serveoi can for easy application and for putting lubricant into places where the nor-mal oil can cannot reach. Home and everyday uses. We have purchased a large quantity of these from the Liquidator and are able to offer them to you for about half of the original list price. 88p per (6 oc). can of 2 cans for 55 post paid. The lubricant is I.C.I. fluon L169.

#### MULTI-SPEED MOTOR

PULTI-SPEED MOTOR Bit speeds are available 500, 850 and 1,100 r.p.m. and 8,000, 12,000 4 15,500 r.p.m. Shati is 1 in. dnameter and approximately 1 in. long. 230/240v. Its speed may be further controlled with the use of our Thyrister controller. Very powerful and useful motor size approx. 2 in. dias. x 5 in. long. Price 979 plus 23p postage and imaurance.



MAINS MOTOR Precision made-as used in record decks and tape recor-ders-ideal also for extractor fan, blower, heaters, etc. New and perfect. Snip at 650, Pootage 200 for first one then 00 for each one ordered. 1° stackmotor 949, 1° stackmotor 91-10.



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PROGRAMMER Learn in your sleep: Have radio playing and kettle boiling as you to ward off intrudera—bave warm house to come home to. All these and many other things you can do if you invest in an electrical programmer Clock by famous maker with 15 amp. on/off witch. Bwitch-on time can be set anywhere to stay on up to 6 hours. Independent 60 minute memory jogger. A beautiful unit. Price \$2:15 + 20p p 4 p or with glass front chrome bezel 83p extra.

I CHIP RADIO Ferranti's latest device ZN414-gives results better than superhet. Supplied complete with technical notes and circuits. \$1:35 each. 10 for \$12. **Hi-Q TUNER COMPONENTS** 

Hi-Q TUNER COMPONENTS For experimenting with the ZN414. MIT MO. 1. Plessey Miniature Tuning Condenser with built in LW switch and 3° territ slah and litz wound MW coil and wave change switch, 290 KIT MO. 2. Air spaced tuning condenser 6° ferrite rod litz wound MW and LW coils and wave change switch, 949. KIT MO. 3. Air spaced TC with slow motion drive 8° ferrit rod, with litz wound LW and MW coils and wave change writch, 31-0. KIT MO. 4. Permeability tuner with fast and alow motion drive and LW loading coils and wave change switch, 509.

wave change switch, 50p.

HOUR MINUTE TIMER Made by Smiths. Complete with control knob and cali-brated dial. Useful in kitchen, office, dark-room, etc. Bargain at 55p



### HONEYWELL PROGRAMMER

HONEYWELL PROGRAMMER This is a drum type timing device, the drum being calibrated in equal divisions for switch setting purposes with trips which are infinitely adjustable for position. They are also arranged to allow 2 opera-tions per switch per rotation. There are 15 changeover micro switches each of 10 amp be changed per revolution. Drive motor is mains operated 5 revs per min. Some of the many uses of this timer are Machinery control, Bolier firing, Dispensing and Vending mackers probably over 210 each. Bycclai and price \$6:83 plus 26p post and naurance. Don't mise this terrific bargain.



Probably the tinjest possible radio, as described in Practical Wireless January 73, All electronics parts £2-20 post paid.

**DISTRIBUTION PANELS** 



Just what you need for work bench or lab. 4 x 13 amp acckets in metal box to take standard 13 amp funce fugs and ong/off awitch with neon warning light. Supplied complete with 6 feet of Sex cable. Wired up ready to work. \$2.50 plus 33 p. & I



HORSTMANN "TIME & SET" SWITCH (A30 Amp Bwitch.) Just the thing if you want to come home to a warm house without it costing you a fortune. You can delay the switch on time of your electric fires, etc. up to 14 hours from setting time or you can use the switch to give a boost on period of up to 3 hours. Equally suitable to control proceeding. Regular price probably around 45° Bpecial snip price §1-65 Fost and ins. 23p.

#### MULLARD UNILEX

This D.I.Y. Stereo Amplifier is still available complete at \$7-06 for the four Mullard Modules, or Modules can be bought separately as follows: --4 watt amplifier module (2 required) Mullard Ref. No. E.7.9000--21.60 each. Pre amp module Mullard Ref. No. E.7.9001--\$198 each. Power module-Mullard Ref. No. E.7.9002--\$28 each. In addition and made to Mullard Specification we offer:--Standard Control Unit with excutcheon and knobs--\$38.90 Knobs--Set of 4-509

SPECIAL OFFER the complete Unilex with control panel at PRE VAT PRICE. £10 post

#### **RADIO STETHOSCOPE**

RADIO STETHOSCOPE Easiest way to fault fload-traces signal from serial to speaker-when signal stops you've found the fault. Use it on Radio, TV amplifier, anything -- com-plete kit comprises two special transistors and all parts inclu-ding probe tube and crystal explece. £2:20-twin stetho-set instead of earpices £35 extra-post and ins. 20p.



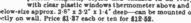
24hr. REPEATING TIME SWITCH Made by Smiths these are A.C. mains operated. NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be built into box with 13A socket. 2 completely adjustable time periods per 24 hours. 5 amp change-over contacts will switch circuit on or off during these periods \$2.75 poet and ins. 23p. Additional time contacts 55p pair.

TWENTYLITE

()-----Fluorescent lighting units with polyester choke and finished white enames, 40 ins model, ideal kitchen, bedroom, hallway, porch, loft etc. With tube sasembled ready to install, \$2:20, post 40p.



HONEYWELL THERMOSTAT Made by Honeywell for normal air temperatures 40°-80°P (6-28°C). This is a precision instrument with a differential which can be adjusted to better than 1-8°P. A mercury awitch breaks on temp. rise-the awitch is operated by a could di metal element and adjustable beater is incorporated for heat antici-pation. Elegantity styled and encased in an ivory plastic case with clear plastic windows thermometer above and awitch acting scale below-36° ± 3° ± 3° ± 3° ± 4° deep-can be mounted on conduit box or directly on wall. Price \$1.87 each or ten for \$12-58.



#### **KETTLE ELEMENTS**

Made by the famous A.E.I. Co. Complete with washers and combined fixing ring and plug shroud. Normal 2 round pin and flat pin earth connection and overload reset push button. 2 Models-rijin (approx.) suitable for Swan and other similar models--lin (approx.) suitable for G.E.C., Hotpoint, etc. All quick boll 24k elements at 240V. Price 21.38.

#### **BATTERY CONDITION TESTER**



BAILERT CONDITION IESTER Made by Mallory but suitable for all batteries made by Ever Ready and others, most of which are zine carbon types but also mercury manganese—nicad—silver oxide and alkaline batteries may be tested. The tester puts a dummy load on the battery and the meter scale indicates the condition depending upon which section the pointer rests. The section reads "replace" "weak" or "good". The tester is complete in its case, size  $3J^* \propto 6J^* 2^* x$  with leads and prode. Price 63.50 but 2000 postage. and prods. Price \$2.50 plus 20p posts

12 WAY SUB-MINIATURE MULTI-CORE CABLE 7.0076 copper cores each core P.V.C. insulated and of different colour. P.V.C. covered overall and approx. 3/16in. thick. Price 22p per yard.



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CONTROL

DRILL

SPEEDS

EXTRACTOR FAN Cleans the air at the rate of 10,000 cubic ft. per hour. Suitable for kitchens, bath-Suitable for kitchens, bath-rooms, factories, changing rooms, etc., it's so quiet it can hardly be heard. Compact, 5§' casing with 53' fan blades. Kit comprises motor, fan blades, abset steel casing, pull switch. mains connector, and fixing brackets. \$3'75 + 20p P. & P.

DRILL CONTROLLER NEW IKW MODEL Electronically changes speed from approxi-mately 10 revs. to maximum. Full power at all

watimum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instruc-tiona. &1-65 plus 13p post and insurance. Made up model also available. \$2-50 plus 13p post a p.

#### TELEPHONES

TELEPHONES Complete as illustrated. Save your legs, time and temper, simply by putting in some telephones. Ex. G.P.O. not new-but guaranteed in good condition and serviceable. Supplied with diagram and instructions showing how to connect. A trues available as

connect. 3 types available as illustrated less internal bell \$1 each. Ditto with bell but less dial \$1.25 each. As illustrated with dial and bell \$1.60 each. Post etc. 50p each.

#### BAKELITE INSTRUMENT CASE



CASE Rize approx. 6<sup>4</sup> × 3<sup>4</sup> × 2<sup>7</sup> deep with brass inserts in four corners and bakelits panel. This is a very strong case suitable to house instru-ments and special rigs, etc. Price

pax lld 11p extra.

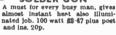
#### SPIT MOTOR



200-250V induction motor, driving a Carter gearbox with a 14" output drive shaft running at 5 revs p.m. Intended for roasting chickens, also for driving modela-windmilla, colour-

ed disc lighting effects, etc. 22 05 plus 20p post

#### SOLDER GUN



TELESCOPIC AERIAL

for portable, car radio or transmitter. Chrome plated-six sections, extends from 74 to 47in. Hole in bottom for 6BA serew. KNUCKLED MODEL FOR F.M. 559 42n.



#### TREASURE TRACER

Complete Kit (except wooden battens) to make the metal detector as the circuit in Practical Wireless, August issue, \$3-30 plus 20p post and insurance

#### IMMERSION HEATERS BY

REMPLOY Standard fitting for Standard fitting for Stanka, made by the famous Remploy Company, Complete

company. complete with scaling washers suitable for 200-240 volts A.C. Depth into tank  $11^{\circ}$ . 2kw or 3kw \$1.65 plus 20p each post and insurance.

#### MAINS OPERATED

MAINS OPERATED SOLENOIDS Model TT2-small but power-ful 1' pull-approx. size Model 400/1  $\frac{1}{4}$  pull. Size  $2\frac{1}{4}$  x 2' x 1/\*. 889. mil. Size 3' x 2 $\frac{1}{4}$  x 2 $\frac{1}{4}$ . 8298. 2]' x 2' Model TT10 1]' puil. Size 3' plus 20p post and insurance



## RESETTABLE FUSE RESETTABLE FUSE how long doe it take you to renew a fuse? Time yourself when next one biows. Then reckning your time at at a per hour see how quickly our restable fuse (auto cirouit braker) will pay for itself. Frice only \$1:00 each or \$12 per dozen, specify 5, 10 or 15 amp-simply fit is place of switch.

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#### RECORD PLAYBACK HEADS (TRUVOX) Individual prices of these are:

2 track record playback heads 50p each.

2 track record playback neads 600 each. 4 track record playback neads 720 each. Erass heads are also available separately— 2 track 330 - 4 track 530 Mu-metal mounting shields 390 each. 2 track record, playback and erase heads already fixed on heavy mounting plate with shield \$1:\$35

I R.P.H. MOTOR Made by the famous Smiths Company. 240v 80 cycle maine working. Ideal motor to drive elock mechanisms. Price \$1.10 each or 10 for \$10.

#### ROCKER SWITCH

13 anip self-fixing into an obiong hole. Bize approximately  $1^{\circ} \times \frac{1}{2}^{\circ}$  Sp each 10 for S2p.

#### SLIDE SWITCHES

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SLIDE SWITCHES Bilds Switch. 2-pole changeover panel mounting by two 6B.A. acrews. Bize approx. In x lin rated 250V lanup. 6p each. 10 for 54p, 100 for 25-10, 500 for 224. Ditto as above but for printed circuit 5p each. 10 for 65p, 100 for 34-25. Sub Ministure Bilds Switch. DPDT 19mm pprox.) between fixing centres. 15p each or 21-09, SP Change over apring return 250v 1 10m.

(žin appro 10 for £1.0 amp. 10p.

HIGH ACCURACY THERMOSTAT Uses differential comparator 1.C. with thermister as probe. Designer claims temperature control to within 17th of a degree. Complete kit with power pack £6 10.

#### RELAYS BY KEYSWITCH

Makers Ref.KMK3 Our number Rel. A3. Open type mains operated coil—3 pairs change-over contact rated at 6 annes each. Mounted by 1 serew. Solder tag connections. Price 60p each. Ditto but 12V. Our Ref. Rel A4. Price 55p each.

WATERPROOF HEATING ELEMENT 26 yards length 70W. Self-regulating temperature control. 55p post free.

#### AMPLIFIER IN CASE WITH SPEAKER

**SPEAKER** Marketed by Britlah Relay under the name Luristor. This is in a very next looking cabinet and is ideal around the home or in the workshop for trouble shooting or for testing out a quick lash up. Size approx.  $91^{\circ} \times 64^{\circ} \times 34^{\circ}$  deep. Input is via a natching itanaformer and volume control and amplifier may be powered by an internal  $9^{\circ}$ battery or an external 110° source. Speaker is an R-A eliptical 6' x 34' 10.000 gauss. The amplifier proper is a Newmarket model ref. P.C.A. Price \$3-85 each, 10 for \$31:50. Post and insurance 20p.

EDUCATIONAL KITS-all **pictorial** instructions



KIT FREE Eagle educational kits. Japanese made these are excellent value for money. We for money. do not e to money. We do not expect to be able to repeat this offer once stocks are sold. Brief description of seck hit is given below and with 3 kits or more we give FREE an accurate 11 piece balance kit. Frie of kits 446 each poot paid. Apecial price for all 7 kits \$3-00 with free balance kit.

THIS BALANCE KIT FREE

11 piece ba paid. Specia balance kit. **EA2** Less Eit. Eleven parts, including candle one concave lens, one convex lens, stage and alit frame, etc. Watch light rays bend as they pase through different lenses.

through dimershi lenses. MAS Waisr Pump Ed. Thirteen parts. Top of pump is transparent so that operating parts may be obserted. Smail parts are brightly coloured to be seen easily while working. Three types of pump may be made: Lift pump. Force Pump and Force Pump with reservoir and noxile.

EA4 Busser E4: Eleven parts. Transparent covers allow the operation of buzzer to be seen. Illustrates and teaches how electromagnetism, with an automatic switch results in an operating buzzer. EA7 Electro-Hagnet Elt. Fifteen parts, inhibde compase. Makes two electro-magnets, one with one layer of wire and one with several layers of wire. Ficks np tacks, nails and any small parts showing how magnetism works.

scowing how magnetism works. EAS Carrest and Resistance Eit, Twenty-nine parts, including bench and light bulb, Conduct interesting and educational projects to learn the application of "OIIMS LAW" and see the differ-ence in current and resistance with different types and lengths of wire.

**EA9** Bell Kit, Eight parts, including bell and push button switch. Build a complete electric bell and see how the hammer is triggered to make the bell ring.

KA10 Morse Key busser and hell hit, 25 part kit easy to construct, simple to operate.

TERMS :-- 10% discount if ten of an item ordered, send postage where quoted -other items, post free if order for these over £6:00 otherwise add 20p.



TAPE PLAYBACK UNITS Mains operated. Made by Reditune the famous "music in, background people". These are complete units ready to work. Have a superior motor driven flywheel in control the tape through the capstag and also an ven equally useful valve amplifier with ELB4 output. In a steel case with carrying handle. Two models offered, good as new 36.50 and somewhat used at 38.50, 75p carriage up to 200 miles then 50p per 100 miles vira. 90 minutes casetties plain 72p recorded 41. extra. 90 minutes cassettes plain 77p recorded \$1.

#### THYRISTOR LIGHT DIMMER

Domestic model for any lamp up to 250 watt. Mounted on wwitch plate to fit in place of standard switch. Virtually no radio interferences. Price 22:95. Industrial model 5 amp module with control knob \$3:80.





PSYCHEDELIC LIGHTING can be yours with our manns motor driven can awitch.<sup>4</sup> cans drive 8 awitches alots in cans make and break 10 aimp contacts as they rotate. Hundreds of combinations possible to give all sorts of effects. Switches can handle more than 10kW of lighting. \$3-85 each plus 20p post and insurance.

### I.C. RADIO **AOUARIUM THERMOSTAT** CONTROLLER

To receive parts for these and other projects featured in this issue send quoted approximate amount any cash adjustment can be made later.



WINDSCREEN WIPER CONTROL Vary speed of your wiper to suit conditions. All parts and instructions to make. \$2.48.

Central Heating Progra

mme	Hot Water	
	no	
	Twice Daily	
	All Day	
	Twice Daily	
	Ali Day	
	Continuously	

Suitable, of course, to programme other than central heating and hot water, for instance, programme upstairs and down-stairs electric heating and cooling or taped music and radio. In fact there is no limit to the versatility of this Programmer. Maina operated. Sinc Sin. × Sin. × 2in. deep. Price \$3.85 as illustrated but less case.

#### STANDARD WAEER SWITCHES

	314	INDA		MILE	n 31		FIE3		
	81	landard	eize 1	≩" wai	lerail	ver-pla	ted 5-	amp e	ontact,
	st	andard	₹″ spin	dle 2″ l	0 <b>0g</b> w	ith loc	king w	asher a	nd nut.
No. of Poles	2 way	Sway -	4 way 5	5 way (	Sway 8	way .	9 way	10way	12way
l pole	44p	44p	44p	44p	44p	44p	44p	44p	44p
2 poles	44p	44p	44p	44p	44p	44p	44p	77p	775
3 poles	44p	44p	44p	44p	779	779	77p	-\$1-04	41 D4
4 poles	44p	44p	44p	77p	779	77p	779	\$1-88	\$1.88
5 poles	44p	44p	77p	77p	#1.04	\$1.04	#1-04	£1-60	\$1-60
6 poles	44p	770	77p	77p	£1-04	81.04	\$1.04	\$1.87	\$1.87
7 poles	77p	77p	77p	\$1.04	#1 . 88	£1·82	41-32	\$2·15	\$2.15
8 poles	779	77p	77p					12-42	
9 poles	77p	779	11.04	\$1.04	£1-60	£1 ·60	£1.60	\$2-70	\$2-70
10 poles	77p	77p							00 · 82
11 poles	77p	£1-04							\$ <b>1</b> 25
12 poles	779	\$1-04	#1-04	41 - 32	\$1.87	\$1.87	41 . 87	48-58	\$3-52

#### BURGLAP ALARM KIT

Protect your home & family by frightening away the intruder. With our circuit, a mains door bell rings directly the door or window is opened. Kit comprises 10 reed switches, 10 magnets, relay, mains transformer and bell with circuit. Price \$7.65.

#### INTEGRATED CIRCUIT BARGAIN

INTEGRATED CIRCUIT BARGAIN A parcel of integrated circuits made by the famous Plessey Company. A once-in-a-lifetime offer of Micro-electronic devices well below cost of manufacture. The parcel contains 5 ICs all new and perfect, first-grade device, definitely not sub-standard or seconds. 4 of the ICs are single silicon chip GP amplifiers. The 5th is a monolithic NPN matched pair. Regular price of parcel well over 35. Full circuit details of the ICs are included and in addition you will receive a list of many different ICs araitable at bargain prices 25 upwards with curcuits and technical data of each. Complete parcel only \$1 post pad. DON'T MISS THIS TERRIPIC BARGAIN.

#### GOOD COMPANION

wood cabinet. Ca × 3in. deep. Co 25p post and Ins.

We can now offer these again in i.c. version using Ferranti ZN414 and Mullard AP Modules 1172. Excellent tone wood cabinet. Cabinet size approx. 11in wide x 81n. high x 31n. deep. Complete assembly instructions \$5-75 plus



#### MINIATURE SEALED RELAY



RE SEALED RELAY American made. Our Ref. No. REL A1. Measures only #" wide x #" thick and #" high and it's a double change over, we don't know the contact rating but estimate this at 3/5 amps. The coil resistance is 600 ohms and 9-12 roit will close it. Ideal for models and ministuriade for models and miniaturised equipment, It's a plug in relay but we supply complete with base. Price 28p including base.

**METAL CHASSIS** 14 gauge sheet steel— size approx.  $7'' \times 3j''' \times 1$ 3/8''' deep. Cadmiumplated punched in thecentre to take 3 P.O.centre to take 3 r.O. 3000 type relays. There is also a removeable cover over this section measur-ing  $4|^{2}$  long  $\times 3\frac{1}{3} \times 2\frac{1}{3}$ . The chassie also has a few holes and could take a



small transformer and/or valve holders also some small transformer and/or valve molters also some 3/8" holes for controls, pots etc. This is an ideal chassis for making up a relay unit or similar. There are ex-equipment but in excellent condi-tion and may have a few resistors etc. still attached. Price 40p each.

#### **CLOCKWORK TIME SWITCH**

For delaying the switching on for up to 12 hours. Being clockwork this is independent of the mains and is therefore useful for remote operation or for hattery appliance. The front dial which is calibrated in hours is turned through the required revolution then after pre-set time double pole 15 a switch operates. Made by Smiths. Price \$1-65.

#### MAINS TRANSFORMER

Our Ref. MTJ1. Drop through chassis-open construction. 240v Primary-9v 1A Secondary. Price 77p each.

#### MAINS TRANSFORMER

MAINS TRANSFORMER Our Ref. MT2. Parneko Neptune series. This is a totally enclosed 'C' core construction, upright mounting and black enamelied. Por 230/2409 Sec. 25-0-25v at 50mA. Ideal for mounting on metal chassis mentioned above. Ex-equipment but unused. 779 each.

3 POST OFFICE TYPE 3000 RELAYS SPOSI OFFICE TIPE 3000 RELATS Ex-equipment but guaranteed perfect—any not so would be changed. 1.—Ref. REL JI. Haw 6 sets of change-over contacts and 2000 ohm coil. 55p each. 2.—Ref. REL J2. 2 pairs that close when relay energized and 2000+1000 ohm coil. Price 44p. Ref. PET 13.0. Pairs contracts that close the set of the set

- 3.-Ref. REL J3. 2 pairs co and 6.4. K ohm coll. 44p. contacts that close

#### **REV. PER MINUTE MOTOR**

WITH GEAR-BOX Made by the famous Chamberlain & Hookham Ltd. These could be made to drive clock or similar. Really robust reliable unit. Price 999 each

#### **110 REV. PER MINUTE MOTOR**

110 REV. PER FILES. WITH GEAR BOX Good American make. Operates from mains and will drive awitch mechanism or other medium service Rize approx. 4" x 3" x 2|" with 4" Write 49.20.

#### **12V CAR BLOWERS**

IZV CAR BLOWERS Units made by Delco. 6 bladed 5" dls. fan inside beavy duty cylinder. These have really powerful series wound motors giving a terrific air flow solitable for ventilating or heating a car, boat, caravan etc. Price £28 op jus 400 post and insurance. (Note these are intended for 13V D.C. but can be run from A.C. up to 30V. The higher the voltage the more the air flow.)

13 AMP SWITCHED SOCKETS By G.E.C. Standard type for fused pluga. Brown bakelite. 17p each or \$1.50 for 10.

SPECIAL SUMMER OFFER Mullard Unitex at Pre V.A.T. price. You want a good storeo syntem—well here's an offer you should not mise! The four Mullard modules all in eriginal manufacturer's carions and with original maker's guarance. ST the lot. Control unit with name plate and 4 spun aluminium faced control knobs 83. Total \$10 post and VAT paid. \$ Goodman's Speakers \$3.00.

#### V.H.F. AMPLIFIERS

With built in mains power pack, these are valve amplifiers, are metal cased and co-ax inputs and outputs. Optimum amplification at T.V. fre-quency. Useful also for re-building into another unit which needs a mains power pack. Price 89.75.

#### CORE MAROON COTTON

COVERED FLEX Very best makers but old coloured code. 6 amp-23/36 × 100 yd. coll \$3 plus 56p. 15 amp-70/38 × 50 yd. coll \$3 94s plus 50p post. Kits of parts avsilable for most previous EE projects send SAE for inst.

Everyday Electronics, September 1973

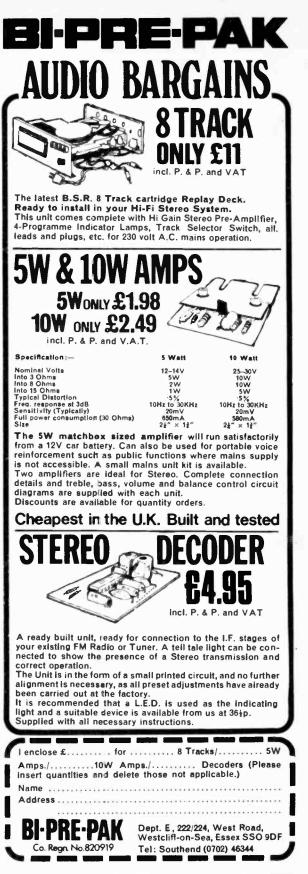


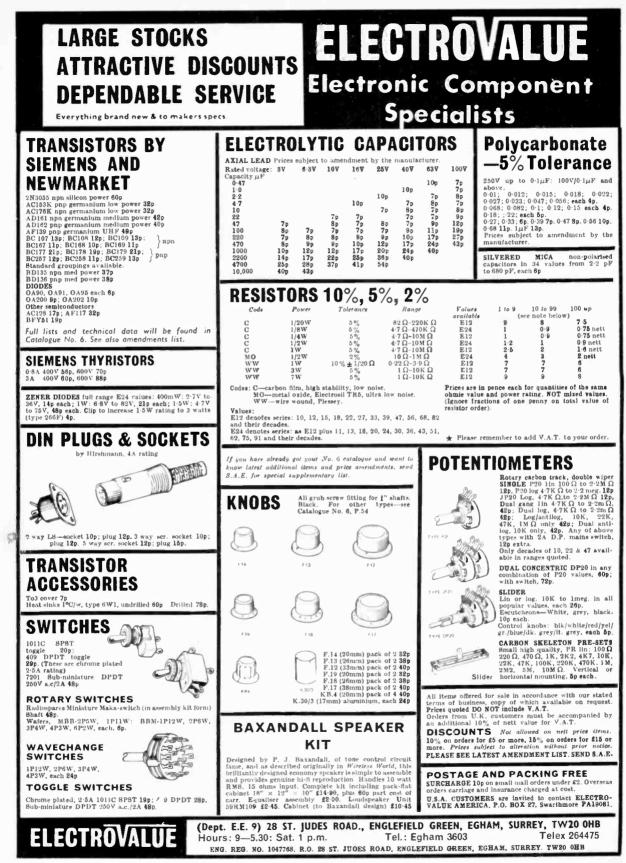


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50 0·26 0·28 0·39 0·3	064 T048 T048 T048 T048 39 0.52 0.55 0.59 1.27 52 0.55 0.64 0.70 1.54	SUPER PAKS NEW SEN	BI-PAK UNTESTED	Q1 20 Red spot transistors PNP 0.55
200 0-39 0-41 0-54 0-6	54 0 63 0 67 0 83 1 76 62 0 74 0 83 1 03 1 93	Money back refund if not satisfied	ICONDUCTORS	Q2       16 White spot R.F. transistors PNP       0.55         Q3       4 OC 77 type transistors       0.55
600 0.59 0.63 0.75 0.7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			Q4         6 Matched transistors OC44/45/81/81D 0.55           Q5         4 OC 75 transistors         0.55           Q6         4 OC 75 transistors         0.55
800 0.10 0.11 0.88 0.8	38 0.39 1.32 1.05 4.40	Pak No. Description	Price £p	Q7 4 AC 128 transistors PNP bigh gain 0.65
	IS. TESTED	U 1 120 Glass Sub-Min. General Purj U 2 60 Mixed Germanium Transisto	pose Germanium Diodes . 0.55	Q8         4 AC 126 transistors PNP         0.55           Q9         7 OC 81 type transistors         0.55
PIV 300mA 750mA 1A 50 0 04 0.06 0.0	06 0.08 0.16 0.23 0.66	U 3 75 Germanium Gold Bonded Su	b-Min. like OA5, OA47 0.55	Q10 7 OC 71 type transistors 0.55 Q11 2 AC 127/128 Complementary pairs
100 0 04 0 07 0 0 200 0 06 0 10 0 0	06 0-15 0-18 0-26 0-83 07 0-16 0-22 0-27 1-10	U 4 40 Germanium Transistors like U 5 60 200mA Sub-Min. Billeon Die	OC81, AC128 0-85	PNP/NPN 0.55 Q12 3 AF 116 type transistors 0.55
400 0.07 0.15 0.0 600 0.08 0.18 0.1	08 0·22 0·30 0·41 1·38 11 0·26 0·38 0·50 2·05	U 6 30 Bil. Planar Trans. NPN like	dea 0.55 B8 ¥95A. 2N706 0.55	Q13 3 AF 117 type transistors 0.55 Q14 3 OC 171 H.F. type transistors 0.55
1000 0.12 0.28 0.1	12 0-28 0-41 0-61 2-20 16 0-33 0-51 0-70 2-75	U 7 16 Sil. Rectifiers TOP-HAT 750 U 8 50 Sil. Planar Diodes DO-7 Gla	mA VLTG. RANGE up to 1000 0.55 as 250mA like QA200/202 . 0.55	Q15 7 2N2926 Sll. Epoxy transistors mixed colours 0.55
1200 - 0.37 -	0.42 0.63 0.83 -	U 9 20 Mixed Voltages, 1 Watt Zen-	er Dlodes	Q16         2 GET880         low noise         Germanium           transistors         0.55         0.55         0.55           Q17         5 NPN 2 × ST.141 & 3 × ST.140         0.55
TRIACS	FULL RANGE OF ZENER DIODES	U10 20 BAY50 charge storage Diode U11 25 PNP Sil. Planar Trans. TO-5	es DO-7 Glass 0.55 Hke 2N1152, 2N2904 0.55	Q18 4 MADT 8 2 x MAT 100 & 2 x MAT
VBOM 2A 6A 10A TO-5 TO-66 TO-48	VOLTAGE RANGE 2-33V. 400mV (DO-7	U12 12 Silicon Rectifiers Epoxy 500	mA up to 800 PIV 0.55	Q19 3 MADT'S 2 × MAT 101 & 1 × MAT
£p £p £p	Case) 15p ea. 11W (Top- Hat) 20p ea. 10W (SO-10	U13 30 PNP-NPN SIL Transistors O U14 150 Mixed Silleon and Germaniu	m Diodea	121         0.55           Q20         4 OC 44 Germanium transistors A.F.         0.55           Q21         4 AC 127 NPN Germanium transistors         0.55
100 83 55 83 200 55 66 99	Stud) 33p ea.	U15 25 NPN Sil. Planar Trans. TO-	5 like BFT51, 2N697 0 55	Q22 20 NKT transition A.F. R.F. coded 0.55 Q23 10 OA 202 Silicon diodes sub-min 0.85
400 77 821 1-21	10 amp POTTED	U17 30 Germanium PNP AF Transis		Q24         8         OA         202         shiftin indees         0.85           Q24         8         OA         8         diades         0.85           Q25         15         IN914         8         diades         75         PIV         75         MA         0.65
DIACS FOR USE WITH	BRIDGE RECTIFIER on heat sink.	U18 8 6 Amp Silicon Rectifiers By U19 25 Silicon NPN Transistors like	213 Type up to 600 PIV 0-55	Q26 8 OA95 Germanium diodes sub-min 1N69 0.55
FOR USE WITH TRIACS BR100 (D32) 41p each	100PIV. 99p each	U20 12 15 Amp Silicon Rectifiers To	np Hat up to 1000 PIV 0.55	Q27 2 10A PIV Silicon rectifiers 18425 R. 0.65 Q28 2 Silicon power rectifiers BYZ 13 0.65
	2 Amp. BRIDGE RECTS.	U21         30 AF. Germanium Alloy Trans           U23         30 MADT's like MHz Series PN		Q29 4 Silicon transistors 2 × 2N696, 1 × 2N697, 1 × 2N698 0.85
FREE One 50p Pak of your	50 v RMS 35p each	U24 20 Germanium 1 Amp Rectifier	GJM Berles up to 300 PIV 0.85	Q30 7 Billeon switch transistors 2N706 NPN 0.55
own choice free with orders valued £4 or over.	100 v RMS 41p 400 v RMS 51p Size 16 mm x 16 mm.	U25 25 300 MHz NPN Bilteon Trans U26 30 Fast Switching Silleon Diode		Q31 6 Sillcon switch transistors 2N708 NPN 0.55
BRAND NEW TEXAS	Size in min x in min.	U27 12 NPN Germanium AF Transis	ators TO-1 like AC127 0.55	Q32 3 PNP Silicon transistors 2 × 2N1131, 1 × 2N1132 0.55
GERM. TRANSISTORS	UT 46 UNIJUNCTION TRANSISTORS	U29 10 I Amo SCR's TO-5 can, up t U30 15 Plastic Silicon Planar Trans.		Q33 3 Billeon NPN transistors 2N1711 0-55 Q34 7 Silleon NPN transistors 2N2369.
Coded and Guaranteed Pak No. EQVT	Direct replacement for T18 43rand BEN 3000	U31 20 Silicon Planar Plastic NPN T U32 25 Zener Diodes 400mW DO-7 c	rans. Low Noise Amp 2N3707 0.55 mas 3-18 volts mixed 0.55	500MHz (code P397) 0.55 Q35 3 Silicon PNP TO-5. 2 x 2N2904 &
T1 8 203713 OC71	also electrically equiva- lent to 2N2646	U33 15 Plastic Case 1 Amp Silicon F		1 × 2N2905 0.55 Q36 7 2N3646 TO-18 plastic 300 MHz NPN 0-55
T2 8 D1374 OC75 T3 8 D1216 OC81D	1 25 100 4 0 · 30 0 · 28 0 · 22	U34 30 Bilicon PNP Alloy Trans. TO U35 25 Bilicon Planar Transistors P1		Q37 3 2N3053 NPN Silicon transistors 0.55 Q38 7 NPN transistors 4 x 2N3703, 3 x
T4 8 2G381T OC81 T5 8 2G382T OC82		U36 25 Silicon Planar NPN Translat	ors TO-5 BFY50/51/52 0.55	2N 3702
T6 8 2G344B OC44 T7 8 2G345B OC45	CADMIUM CELLS ORP12 480	U37 30 Silicon Alloy Transistors 80- U38 20 Fast Switching Silicon Trans	2 PNP OC200, 28322 0.55 NPN 400 MHz 2N3011 0.55	ELECTRONIC SLIDE-RULE
T8 8 2G378 OC78 T9 8 2G399A 2N1302 T10 8 2G417 AP117	ORP60, ORP61 44p each	U39 30 RF, Germ. PNP Transistors U40 10 Dual Transistors 6 lead TO-5		The MK Blide Rule, designed to simplify Elec- tronic calculations features the following scales: Conversion of Frequency and Wavelength.
All 55p each pak	GENERAL PURPOSE	U41 25 RF Germanium Transistors 7		Calculation of L. C and fo of Tuned Circuita. Reactance and Self Inductance. Area of Circuita.
D1699 NPN SILICON	NPN SILICON SWITCH- ING TRANS, TO-18	U42 10 VHF Gernanium PNP Trans U43 25 Sil. Trans. Plastic TO-18 A.F	BC113/114 0.55	Volume of Cylinders. Resistance of Conductors. Weight of Conductors. Decibel Calculations.
DUAL TRANSISTOR (Similar to 2N2060)	SIM. TO 2N706/8. BST- 27/28/95A. All unable	U44 20 Bil. Trans. Plastic TO-5 BC11	5/116 0.55	Angle Functions. Natural Logs and 'e' Functions. Multiplication and Division. Squaring, Cubing
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	devices no open or short circuits. ALSO AVAIL-	U45 7 3A SCR. T066 up to 600PIV		and Square Roots. Conversion of kW and Hp. A must for every electronic engineer and enthusi-
ND 120 NIXIE DRIVER	ABLE in PNP 8im. to 2N2906, BCY70, When	Code No's, mentioned above are given a the pak. The devices themselves are nor		ast. Size: 22 cm x 4cm. Complete with case and instructions. Price each: £3-69
TRANSISTOR. Suitable replacement for	ordering please state preference NPN or PNP.	SILICON PHOTO TRAN-	INTEGRATED CIRCUIT PAKS	
BSX 21, C 407, 2N 1893 120veb.	20 For 0.55 50 For 1.10	SISTOR. TO-18 Lens end NPN Sim. to BP x 25 and P21.	Manufacturers "Fall Outs" which	ch include Functional and Part-Functional Units.
1 25 100+ 0·19 0·17 0·18	100 For 1.92 800 For 8-25	BRAND NEW. Full data available. Fully guaranteed.	These are classed as 'out-of-spec are ideal for learning about I.C's	c' from the maker's very rigid apecifications, but
Sil. trans. suitable for	1000 For 14-30	Qty. 1-24 25-99 100 up Price each 49p 44p 38p		No. Contents Price   Pak No. Contents Price
P.E. Organ. Metal TO-18 Eqvt. ZTX300 51p each.	SIL. G.P. DIODES #p		UIC00-12×7400 0-55 UIC UIC01-12×7401 0-55 UIC	246 - 5 × 7446 0.55 U1C86 - 5 × 7486 0.55 247 - 5 × 7447 0.55 U1C90 - 5 × 7490 0.55
Any Qty.	300mW 300-55 40PIV(Min.) 100 1-85	F.E.T.'S	UIC02-12×7402 0-65 UIC UIC03-12×7403 0-65 UIC	248 = 5 × 7448         0.55         U1C91 = 5 × 7491         0.65           250 = 12 × 7450         0.65         U1C92 = 5 × 7492         0.65
GP 100 TO3 METAL CASE GERMANIUM	Sub-Min. 500 5-50 Full Tested 1,000 9-90	2N3819 81p 2N5458 35p 2N3820 85p 2N5459 44p	UIC04=12×7404 0-55 UIC	C51-12×7451         0.55         U1C93-5×7493         0.55           C53-12×7453         0.55         U1C94-5×7494         0.55
Vebo=80V. Voco=50V. I.C.=10 amps. Ptot=	Ideal for Organ Builders.	2N3821 89p BFW10 66p 2N3823 81p MPF105 41p	U1C06-8×7408 0.55 U1C U1C07-8×7407 0.55 U1C	C54 - 12 × 7454         0 · 55         U1C95 - 5 × 7495         0 · 55           C60 - 12 × 7460         0 · 55         U1C96 - 5 × 7496         0 · 55
30W. hfe=30~170. Replaces the majority of	R 2400 TO3 NPN		UIC10=12×7410 0-55 UIC UIC13=8×7413 0-55 UIC	C70=8x7470         0.55         UIC100=5x74100         0.55           C72=8x7472         0.55         UIC121=5x74121         0.55
Germanium power tran- eistors in the OC, AD	SILICON HIGH VOLTAGE	NEW 6th EDITION	UIC30-12×7430 0.55 UIC	$773 - 8 \times 7473$ 0.55 U1C141 - 5 $\times 74141$ 0.55 $74 - 8 \times 7474$ 0.55 U1C151 - 5 $\times 74151$ 0.55
and NKT range. 1 25 100+	Vebo=250V. Vceo= 100V. 1.C.=6 amps.	TRANSISTOR EQUIVALENTS	UIC40 = 12 × 7440 0.55 UIC UIC41 = 5 × 7441 0.55 UIC	C75 = 8 × 7475         0 · 55         U1C154 = 5 × 74154         0 · 55           276 = 8 × 7476         0 · 55         U1C193 = 5 × 74193         0 · 55
0-48 0-44 0-40	Ptot = $30W$ . hfe = typ.20 fT = $5M$ Hz.	BOOK. A complete cross reference and equivalents book for European, American and Japanese Transis	UIC43=5×7443 0.55 UIC	280 = 5 × 7480         0 · 55         U1C199 = 5 × 74199         0 · 55           281 = 5 × 7481         0 · 55
GP 300 TO3 METAL CASE SILICON	1 25 100+ 0·55 0·50 0·44	American and Japanese Transis- tors. Exclusive to BI-PAK 99p each.	UIC45-5×7445 0-85 UIC	382-5×7482         0.55         UICXI=25 Assorted           383-5×7483         0.55         74's 1.65
Vebo = 100 V. Vceo = 60 V I.C. = 15 amps. Ptot =			Packs cannot be split, but 25 asso	rted pieces (our mix) is available as PAK UIC X1.
115W. hfe=20. 100fT. = IMHz. Suitable replace-	2N3055	A LARGE RANGE OF TECHNICAL	BI-PAKS NEW COMPONENT SI	HOP NOW OPEN WITH A WIDE RANGE OF
ment for 2N 3055, BDY 11 or BDY 20.	115 WATT SIL	AND DATA BOOKS ARE NOW AVAILABLE EX. STOCK.		D ACCESSORIES AT COMPETITIVE PRICES
1 25 100+ 0.55 0.53 0.51	POWER NPN 55p EACH	SEND FOR FREE LIST.	TEL. (STD 0920) 6159	ET (Alo), WARE, HERTS. 3.
				6 p.m., FRIDAY UNTIL 8 p.m.
AD161/162 PN1	Vebo=100V, Vo	PN PLASTIC SILICON co=50V I.C.=10 amps. Ptot=50W.		d packing per order. Cosh with order
M/P COMP GERM TRANS OUR LOWEST PRICE O	8. hfe=typ. 100 fT DF 1 25	3MHz B1P 19/20 Matched Pair. 100+ 1 25 100+		SEMICONDUCTORS, P.O. BOX 6,
60p PER PAIR	0.871 0.35	0.82 0.66 0.61 0.55		WARE, HERTS.
Contraction of the local division of the loc		ومناوية الأناملي ويردد والأحي	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	

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BP933	14p	13p	12p
BP935	14p	13p	12p
BP936	14p	135	12p
BP944	14p	130	12p
BP945	28p	270	24p
BP946	13p	120	110
BP948	28p	270	24p
BP951	72p	66a	61p
BP962	13p	120	11p
BP9093	44p	420	39p
BP9094	44p	420	39p
BP9097	44p	425	39p
BP9099	44p	420	39p

Devices may be mixed to qualify for quantity price. Larger quantity prices on application. (DTL 930 Series only).

### NUMERICAL INDICATOR TUBES

MODEL	CD66	OR116	3015F Minitron	
Anode voltage (Vdc)	170min	175min	5	
Cathode Current (mA)	2.3	14	8	All indicator
Numerical Height (mm)	16	13	9	point. All sid
Tube Height (mm)	47	32	22	data for al types availabl
Tube Diameter (mm)	19	13	12 wide	on request.
I.C. Driver Bec.	BP41 or 141	BP41 or 141	BP47	
PRICE EACH	£1-87	£1-70	\$1.50	

RTL MICROLOGIC	CIRCUITS Price	DUAL-IN-LINE SOCKETS. 14 & 16 Lead Sockets for use with DUAL-IN-LINE 1.C's. TWO Range				
Epoxy TO-5 case	1-24 25-99	100 up	PROFESSIONAL	A NE	WLOW	COST.
uL900 Buffer uL914 Dual 21/p gate uL923 J-K flip-flop	38p 36p 38p 36p 55p 51p	299	PROF. TYPE No. TSO 14 pin type TSO 16	1-24 33p 39p	25-99 30p 35p	100up. 28p 33p
Date and Circuit Price 8p.			LOW COST No. BPS 14 BPS 16	17p 18p	13p 18p	12p 18p

Everyday Electronics, September 1973

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Volts.

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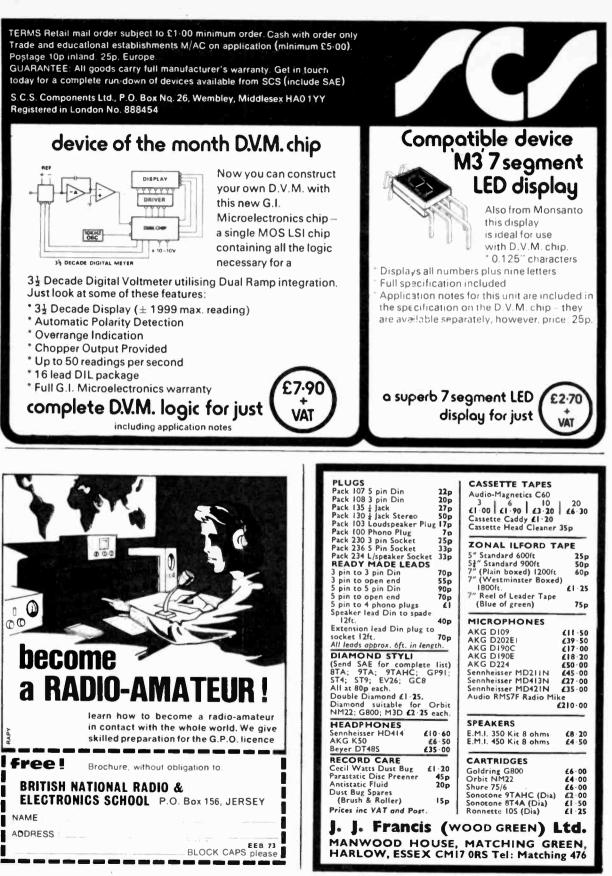
Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 storeo pre-amplifier has been conceived from the latest circuit technique. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPM devices for use in the input stages. Three awliched storeo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.



 $\begin{array}{l} 20\,Hz\,-\,20\,K\,Hz\,\pm\,1dB\\ better\,than\,0\cdot1\%\\ 1\cdot25\,mV\,into\,50K\,\Omega\\ 35\,mV\,into\,50K\,\Omega\\ 1\cdot5\,mV\,into\,50K\,\Omega \end{array}$ All input voltages are for an output of 250mV. Tape and P.U. inpute equalised to RIAA curve within  $\pm$  1dB. from 20Hz to 20KHz. ± 15dB at 20Hz ± 15dB at 20KHz 100Hz 8KHz better than - 65dB better than -+ 26dB + 35 volts at 20mA 292mm × 82mm × 35mm ONLY £13 15

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- 6. Printed circuit board.
- 7. Keyboard panel.
- Electronic components pack (diodes, resistors, capacitors, transistor).
- Battery clips and on/off switch.
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producing and marketing electronic kits. You may have used one, and you've almost certainly heard of them – the Sinclair Project 60 stereo modules. It seemed only logical to combine the knowledge of do-it-yourself kits with the

It seemed only logical to combine the knowledge of do-it-yourself kits with the knowledge of small calculator technology. And *you* benefit !

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Ī	To : Sinclair Radionics Ltd, London Road, St Ives, Huntingdonshire, PE174HJ	
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i	*Delete as required.	

# everyday electronics

PROJECTS .... THEORY.....

#### INTEGRATED CIRCUITS

There is a remarkable and noteworthy contradiction in present day electronics. While circuit designs are tending to increase in complexity and in variety of functions offered, in terms of actual hardware electronic equipments are tending to become less complicated and consequently simpler to build.

The explanation to this apparent paradox is to be found in the integrated circuit. This is a small component hardly larger than a conventional transistor, but containing a complete circuit arrangement incorporating a number of semiconductor devices as well as other circuit elements. As constructors, we don't really have to concern ourselves with the internal details of these remarkable devices. It is sufficient for many purposes to consider the integrated circuit (i.c.) as just another component, or as a "black box".

Integrated circuits have been around for many years, but EVERYDAY ELECTRONICS has so far concentrated upon discrete semiconductor devices. This makes sense, because it is our belief that a true understanding of electronics can only stem from an awareness of the discrete transistor and familiarity with its function as gained through practical constructional and experimental work.

But to ensure that our readers reap all possible advantages from modern developments, we shall make increasing use of integrated circuits in future designs. For a start, this month we include two quite dissimilar projects that are based upon different examples of these miniature marvels of current technology.

#### DON'T MISS THE BUS!

Great news for all those wishing to learn the basics of electronics from scratch. Here is their BIG OPPORTUNITY. An entirely new series *Teach-In* '74 will be launched next month in EVERYDAY ELECTRONICS. This series has been carefully and expertly planned to meet the need of the ordinary person, man or woman, boy or girl, who wishes to acquire an understanding of electronic circuit principles without delving deeply into mathematics.

No previous experience or knowledge is required! Easy to follow text will be accompanied by easy to perform practical exercises requiring the very minimum of tools and components.

Regrettably it is our duty once again to advise readers that the supply of back numbers of EVERYDAY ELECTRONICS is not possible. So all budding enthusiasts *please* do take heed of this advance notice and friendly word of advice. Opportunities for the layman to learn the fundamentals in such an enjoyable and painless way in his own home as we have planned are all too rare, and of necessity come at infrequent intervals.

Feel Bennet

Our October issue will be published on Friday, September 21

EDITOR F. E. Bennett 

ASSISTANT EDITOR M. Kenward 

B. W. Terrell B.Sc.

ART EDITOR J. D. Pountney 

P. A. Loates

ADVERTISEMENT MANAGER D. W. B. Tilleard

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## .. EASY TO CONSTRUCT ...SIMPLY EXPLAINED



VOL. 2 NO. 9

### SEPTEMBER 1973

### CONSTRUCTIONAL PROJECTS

PERSONAL RECEIVER	Medium wave receiver to suit the pocket by F. R. Heath	464
AQUARIUM THERMOS	TAT For accurate temperature control of liquids by Mike Kenward	474
TRAIN CONTROLLER	For electric model trains, featuring automatic control by A. J. Dunn	483

#### GENERAL FEATURES

EDITORIAL	462
RADAR FOR SMALL BOATS by G. A. G. Brooke	468
WHAT DO YOU KNOW? Inductors	472
PLEASE TAKE NOTE	477
SEMICONDUCTORS Four—The Transistor by J. B. Dance	478
RUMINATIONS by Sensor	488
DEMO CIRCUITS 10 The Unijunction Oscillator by Mike Hughes	489
SHOP TALK Component buying problems solved by Mike Kenward	493
HELP! Answers to some of your problems	494
DOWN TO EARTH The fierce volume control by George Hylton	497
READERS LETTERS Your news and views	498
BRIGHT IDEAS Reader's constructional hints	498

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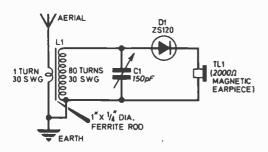
A LTHOUGH it is very difficult to define what fascinates so many people about a miniature radio receiver, the fact remains that a great many people enjoy "messing about" with radio on this scale, and derive many hours of enjoyment (and learn a great deal of physics) from constructing these devices.

#### **CRYSTAL SETS**

The crystal set is the most basic receiver possible, Fig. 1 shows a typical simple crystal set using a tuned circuit, and a diode to detect the modulation—the audio part of the waveform which drives the earpiece. A long aerial wire and an earth are essential if any volume is to be expected, and unless very high impedance headphones are used the programmes will all merge into one. This is because a low impedance across the tuned circuit will damp it and increase the bandwidth or range of frequencies received.

If one perseveres with the crystal set shown, one will notice that it possesses one or two fine

#### Fig. 1. A typical, simple crystal set.



qualities. These are :

- 1. The sound quality is very good (if a good ear piece is used).
- 2. The background noise is very low.

These are the basic requirements for a quality radio receiver. Unfortunately, the receiver has some bad qualities too. These are:

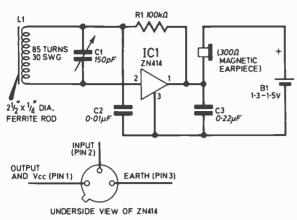
- 1. The volume is very low.
- 2. The large aerial necessary is somewhat cumbersome for a portable receiver.

#### THE I.C.

Now, if we could add between the tuned circuit and the earpiece a circuit which possessed r.f. gain, low distortion and high input impedance, we would maintain the good qualities above and eliminate the bad qualities.

Using modern semiconductor processes it is now possible to achieve just this and the Ferranti ZN414 offers us complete radio tuner in a 3 pin "transistor" package. If the circuit of Fig. 1 is re-drawn using ZN414 we have an earpiece radio which has real advantages over existing types (Fig. 2). The very high input resistance (greater than 4 megohms) of the ZN414 ensures that the tuned circuit is virtually undamped by the device. Thus very high selectivity, low bandwidth operation is possible. The output of the ZN414 can now drive a lower impedance earphone.

If this circuit is built remember that although layout is not too important leads should be kept as short as possible. When the unit is operating the effects of varying L1 (unwinding turns) and C1 can be noted. Also, if one deliberately damps the tuned circuit by adding a resistor (say 10



#### Fig. 2. The basic set using the ZN414.

kilohms) across it, it can be shown that the selectivity is reduced.

It does not need much imagination to realise that the radio shown in Fig. 2 could fit into a very small case. In practise, the size is limited by the ferrite rod which should not be reduced below about one inch in length.

A diagram of the connections to the ZN414 is shown in Fig. 2. Fig. 3 shows the internal circuitry of the ZN414 and is included for reference.

The basic receiver shown in Fig. 2, whilst capable of good results, lacks certain refinements which are desirable if optimum performance is to be achieved under all conditions. For this reason a further receiver circuit has been developed. This can have the refinement of volume control (or preset) volume control and a sensitivity control if wanted, and can be used to drive an amplifier (of input impedance greater than 20 kilohms) if necessary.

The circuit is shown in Fig. 4, the layout for printed circuit board in Fig. 5 and the wiring for the p.c. board in Fig. 6. One advantage of the crystal earpiece used is that two can be "paralleled" up to make a headphone. It is a lot less tiring to listen with both ears than one, and crystal earpieces are much cheaper than other

Compone	SEE
Resistors	SHOP
R1 100kΩ	
R2 3·3kΩ	TALK
R3 250Ω	
R4 560Ω	
R5 100Ω	
All <b>W</b> ±10% ca	rbon
Capacitors	nE miniatura variable
C2 0.01 µF minia	pF miniature variable
	F miniature ceramic
C4 0.05µF minia	ture ceramic
Semiconductors	
IC1 ZN414 integ	rated circuit
TR1_ZTX300 sili	con <i>non</i>
D1 ZS120)	ny small signal silicon diode
D2 ZS120 Cora	iny small signal silicon diode
Miscellaneous	
L1 Ferrite rod	21 x linch diameter and
length of 3	0 s.w.g. enamelled copper
wire	
TL1 Crystal earp	
	y (comprised of four RM
675's)	

types. The quality of reproduction from two crystal earpieces using this circuit is astonishingly good.

The circuit now includes certain desirable features such as much higher volume (with optional control) and sensitivity control if required. This latter feature is vital for an experimenter, as it enables a much wider range of ferrite rod sizes and/or earphones to be used without making the receiver difficult to operate.

The prototype receiver used miniature "button" batteries which, although expensive, give extensive life and enable a fairly small receiver to be constructed. The voltage is not critical, the higher ranges will give higher volume without distortion.

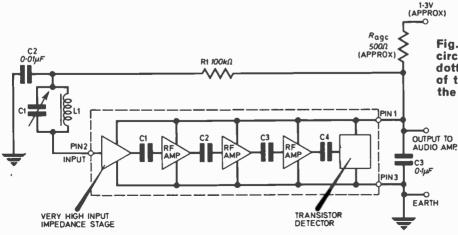


Fig. 3. The ZN414 in a basic circuit. The area inside the dotted line shows the basis of the internal circuitry of the i.c.

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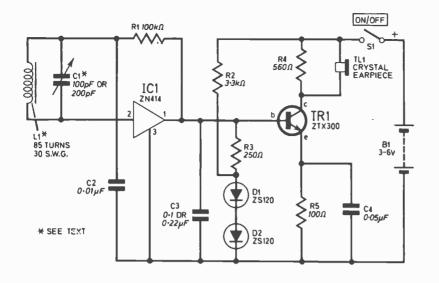
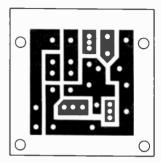


Fig. 4 (left). The complete circuit diagram of the Personal Receiver.

Fig. 5 (below). The printed circuit layout for the receiver shown full size.



A magnetic earpiece may be used in place of the crystal one, by substituting it for the 560 ohm resistor R4 soldered between the collector of TR1 and the positive supply rail; its impedance should be similar (about  $500\Omega$ ).

If during experimentation one finds earpiece listening tiring (continual removal and replacement of an earphone can be very irritating) the earphone can be replaced by a connecting lead to an amplifier, which has a high input impedance. Most transistor amplifiers are suitable, and no damage will be incurred if the circuit in Fig. Fis used.

#### **CASE CONSTRUCTION**

The constructional details given are not for a micro-miniature set. They are intended for an easily built receiver. The set is small and yet avoids very "fiddly" working. The complete unit is housed in a transparent Perspex box size 3 inches x  $1_{4}^{3}$  inches x  $3_{4}$  inches shown in Fig. 8. Perspex is glued internally with polystyrene cement to provide a battery compartment, and a clamp for the ferrite rod.

The bottom of the box slides out for battery replacement. The batteries are held together by a small spring, laterally they are held by a piece of neoprene tubing slit across to allow the batteries to be inserted easily. The earpiece is connected by means of a jack socket and this also carries an on/off switch. Thus the set is turned on when the earpiece is plugged in.

Care is needed in drilling Perspex; if too much pressure is put on the drill it will crack the Perspex. Slow steady drilling is best.

#### VARIATIONS

A volume control can be added by inserting a 250 ohm potentiometer (a preset type could be used) in series with the emitter of TR1 e.g.

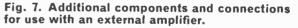
between the junction of R5/C4 and the emitter. This control will only reduce the output power from the circuit as shown and was not found to be essential in the prototype. Resistor R5 should not be omitted or have its value reduced.

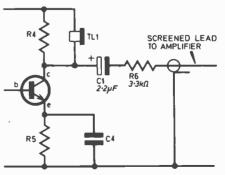
Diodes D1 and D2 are used to form a voltage stabiliser for the supply to the ZN414. These diodes can be any small signal silicon types, for these the forward voltage drop is about 600mV to 700mV each, giving a supply of about 1.4V.

The sensitivity control, if required, can be obtained by adding a 1 kilohm preset in place of D1.

The aerial coil should be wound using 30 s.w.g. enamelled copper wire. Start winding at about  ${}^{3}_{8}$  inch from one end of the rod and wind on 85 turns. The turns should be touching each other and not crossed or overlapping, insulation tape can be used to secure each end.

Any small (physically) tuning capacitor of value 100pF to 200pF may be used. A few more turns will be needed on the coil if lower values (less than 100pF) of capacitance are used. The internal layout of the prototype receiver is shown in Fig. 8.





Everyday Electronics, September 1973

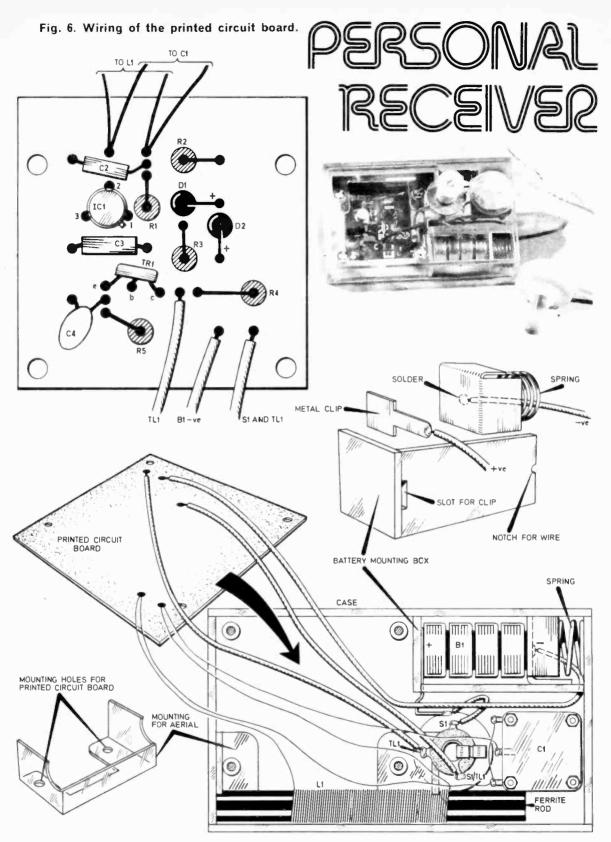


Fig. 8. Layout and General construction of the Personal Receiver.

# Small By G.A.G. Brooke

UP to the last two or three years many keen yachtsmen and small workboat owners such as inshore fishermen with 40 foot boats were heard to complain of the lack of a suitable "mini" radar. After all, big ship radar had been with us since the early days of the last war, the world's leading manufacturer was about to clock up his 40,000th order, and radar for small craft, as opposed to "very" small boats, had been available since 1963 (in one case a small boat radar had first appeared in 1966, but the smallest boat which could use this is about 40 feet).

Suddenly there was a proliferation of sets suitable for "very" small craft but this was followed immediately by the failure, or at least lack of obvious success, of some of them. What is there to mini radars generally and why do the manufacturers appear to find this particular market so difficult? In answering these questions, it is hoped that old radar hands will forgive a description of basic principles.

#### **BASIC OPERATION**

Radar is easily understood, once comparisons are made with sound waves, and the echoes which return from them. We know that sound travels through the air at the rate of about 1100 feet per second. Until radar was developed skippers of boats working near cliffs or up rivers used sound waves to determine distance away from bluffs, buildings and so on. A short blast on the whistle would be sounded, and the seconds counted until the echo was heard. If it took five seconds for the echo to return it meant that the sound waves had travelled a total distance out and back of approximately 5,500 feet; therefore the target was a little over half a mile away.

Now it happens that if you send out radio waves at a suitable frequency (the standard "X" band is 9380 to 9440 MHz) with sufficient energy, they actually bounce back to you from hard objects in exactly the same way. As the speed of both the emission and the returning echo is similarly constant, all you have to do to measure the distance of the hard object is to record the time taken for the entire operation. A marine radar incorporates many refinements to this principle but basically that is all there is to it.

Taking things a stage further: a radar set consists essentially of the following elements: the transmitter to generate short bursts of radio-frequency energy; a rotating scanner to radiate the radio waves in a narrow beam around the horizon and pick up the returning echoes; a receiver to detect and amplify these echoes; and a display tube to visually present them, with facilities for measuring range and bearing. The transmitter and the receiver are combined in one unit, which for convenience is called the transceiver, and there is an extra unit -making a total of four-for the power supply (all radars work off standard voltages from 12V upwards, but this has to be changed into a form acceptable to the radar, usually by a static inverter).

#### BASIC SYSTEM

Coming from the general to the particular, these four elements still exist but in recent years have been telescoped into three units, and lately into only two. This naturally simplifies and cheapens installation and there is a useful saving in wheelhouse space, particularly important in workboats which may already have much other instrumentation. The compression from four to three units came about by installing the transceiver immediately under the scanner in a form of a streamlined pod. With the transceiver below—where it still has to be in the case



The "exposed" scanner of the Decca 101 radar.

of larger big ship sets—it is joined to the scanner by an expensive and energy losing waveguide of rectangular copper tubing. The obviation of this, not only simplifies installation but allows a smaller power output for the same radar performance. This again results in a smaller power requirement from the boat's supply, usually a matter of great significance.

Further miniaturisation through the adoption of solid-state techniques (an ill-defined phrase but here taken to mean the latest micro-circuit and other solid-state devices) has enabled the power supply to be incorporated in either the scanner/transceiver assembly or in the display, or shared between the two. This results in a total of only two units, and is standard with mini-radars. With so much of the electronics of the system built into a scanner assembly which may be several feet up in the air, it is important that the different elements are designed on a modular plug-in principle as far as possible, for easy removal below.

#### TRANSCEIVER

The transmitter and receiver are in appearance almost a unity as the name transceiver implies, but in reality have, of course, very distinct functions. The transmitter and receiver circuits are provided with a means of isolating one from the other, so that when transmitting, none of the energy goes into the receiver; and only when the transmitter has stopped its emission is the receiver **on** and enabled to receive the reflected echoes. To measure the time lag between emission of a radio wave and its reflected echo obviously requires electronic switching **on** and **off** of the transmitted radio waves at a rate so rapid that it nearly defies comprehension.

Everyday Electronics, September 1973

The bursts of power, or pulses, are timed in two ways. First, the lengths of time measured in fractions of a microsecond that the transmitter is on. This is termed pulse length. Second, the number of times per second that the pulses are repeated. This is termed pulse repetition frequency.

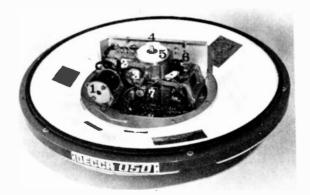
There are short and long pulse lengths automatically controlled by the range to which the radar is set. Usually shorter pulse lengths are used on short ranges for optimum range discrimination between objects; longer pulse lengths for longer ranges because of the need for a greater amount of power to create an echo. These pulse lengths typically vary between 0.05and 1.5 microseconds.

#### SCANNER

It is logical to consider the scanner next. As many readers may have noticed, in a large vessel, it consists of a horizontal bar from 4 feet to 9 feet long and about 6 inches deep. This is mounted on a pillar or other support and made to revolve at about 30 r.p.m. by a small motor mounted beneath. In mini-radars this assembly is invariably cased in a glass-fibre "radome", resulting in a mushroom appearance. The predominant reason is reduction in cost. The radome itself is not expensive and permits. the scanner inside to be lighter, easier to rotate-since wind resistance is removed-not weatherproofed, and so cheaper and requiring less electrical power. As we have seen the radome houses the transceiver, and in one design the power supply as well.

Design of the scanner itself is always important but particularly in very small boats. Obviously, the smaller it can be the lighter and cheaper, but there is a limit below which performance in the form of discrimination (the ability to separate adjacent echoes) and freedom from side lobes, suffers unduly (it is impossible to direct all the energy into the desired beam and a small amount will be radiated to

Scanner unit of the Decca 050 radar showing the transmitter and turning assembly.



469



The two points of the Electronic Laboratories Seascan small boat radar.

either side, this is known as sidelobes and, if excessive, will create highly undesirable false echoes on the display).

The minimum size of scanner would appear to be 30 inches. The actual design of the aerial itself is another important point. Up to the late fifties the cheese type aerial was standard, where the end of the waveguide is positioned at the focal point of a parabolic reflector; the width of the latter has to be large in comparison with the wavelength so that transmission can be made in the form of a narrow beam. It is bulkier and not so efficient as the slotted waveguide scanner now universal in commercial and most other radars.

In the slotted waveguide type a bar aerial has slots cut in the vertical face through which pulses can be transmitted and echoes received. The disadvantage is that the slots have to be cut extremely accurately according to a mathematical formula and a slotted waveguide aerial is considerably more expensive than a cheese type.

#### DISPLAY

The echoes are handled in the receiver portion of the transceiver. Obviously they vary greatly in strength; a nearby ship produces an extremely strong echo, while a buoy some distance away produces only a faint one. All are very greatly amplified to bring the weak ones to a level that can be seen on the display. The echoes are then levelled to a common value, so that the echo created by a nearby ship will bear a reasonable relationship in size to that created by a buoy. All this is done electronically and may answer some queries as to why radars are not as cheap as washing machines!

To understand the working of the display,



The Decca Super 101, this is a three unit system suitable for boats down to about 40 feet.

simple comparison with a searchlight may be made. Imagine yourself directly above the boat's searchlight which is being rotated 360 degrees. As it revolves the beam of light crosses boats close by and you see each of these objects momentarily. Consider now the radar's cathode ray tube, the circular extremity of which forms your radar display. As with the searchlight, your position is in the centre of the circle and the display shows all "radar conspicuous" objects within the range set at the time.

There is a difference, however, in that the inside of the tube is treated with a special material that continues to glow for a considerable period after the echo has been passed; in addition, each time the scanner directs the radio waves to cross a target (which it does about every two seconds) the echo is re-illuminated. In this way the entire radar scene is permanently visible, though the targets currently being swept show up more brightly than the remainder.

By courtesy of certain elements in both the receiver and the display any one boat mentioned above will be shown on the display as a bright spot at a range and bearing from the centre (which represents own ship) exactly corresponding to its true position. Radars have several range scales whereby, at the turn of a knob, the radius of the display can be taken to represent different distances from, say, half a mile to 18 miles. Concentric illuminated rings on the display represent increasing distances from the centre; as the range scale is changed the previous rings disappear, to be replaced by new rings in different positions, and it is always easy to gauge the range of an echo by its position relative to the nearest ring.

Everyday Electronics, September 1973

470



The display unit of the Decca 050 radar mounted in front of the "helmsman".

1

The relative bearing of an echo is read off the circumference of the display, with the aid of a revolving transparent disc. Modern big ship sets have more sophisticated facilities whereby, as controls manipulate a variable ring for range, and a radial line for bearing, the two readings come up simultaneously on digital readouts.

#### QUALITY, PERFORMANCE, PRICE

So much for the general principle of marine radar. At the outset of this article—which concentrates on mini-radars as being of interest to the widest circle of boat-owners—it was stated that, judging by results, many manufacturers find this is a very difficult market; not so much in selling the finished product but in getting its original design right. Why is this?

The basic reason is that the three-sided equation between quality, performance and price is a very awkward one. The price ceiling simply must be low, bearing in mind the likely pocket of the prospective owner and the danger of being undercut by a competitor. The manufacturer's outlets, usually agents in the case of pleasure craft and his own depots in the case of work-boats will have no chance (particularly with cost-conscious fishermen who form a very large section of the market) if the price is too high.

Performance in the form of maximum range, minimum range, definition (sharp, clear-looking echoes) discrimination, power required and so on must be adequate in view of competition. Last, but by no means least, there is quality; quality of electronic design, mechanical design and materials used; these are the basis of reliability. Contrary to general belief, the smaller the radar, the more hostile an environment it will be in. For example, a 30 foot family cruiser which is shipping a lot of water and spray and vibrating from the action of its engine is probably providing rougher treatment than that experienced by the radar of a large merchant ship on a sturdy bridge high above the

Everyday Electronics, September 1973

waves and which is being operated by professional mariners.

The manufacturer has an agonising balancing act to perform between performance, extra ruggedness plus highly reliable material leading to high cost on the one hand and the necessity to keep the price down on the other. Some have failed to solve this equation first time, one large company having to dispose of its mini-radar altogether, and at least one other bringing out a second mark with major modifications.

#### **CHOOSING**

When choosing a radar it cannot be stressed too highly that reliability is the first thing to look for. As this is not assessable for any particular set in advance the best thing to do is enquire of existing owners. Performance is naturally important—but is of no account if the set won't work—and in the context of a very small boat it should be realised that theoretically long range may be unattainable in practice. This is because radar sees almost directly like the human eye (the radar horizon exceeds the optical horizon by 6 per cent).

There is little point in buying a 20 mile range radar if you are only going to mount it 18 feet above the water, because its "horizon" at that height will be only five miles. To be fair it will pick up high land at a greater range, but somewhat disappointing since the distance at which a feature will be on the horizon of a radar is found by adding the aerial's horizon to that of the feature. The following aerial heights (in feet) are followed by the corresponding radar horizon (in nautical miles) in brackets: 10 (4), 15 (4<sup>1</sup><sub>2</sub>), 18 (5), 24 (6), 32 (7), so that land at 32 feet will begin to appear above the horizon of an aerial at 10 feet, at 7+4=11 miles.

Another aspect that prospective owners should look into most carefully is the service organisation of the manufacturer. In spite of what the brochures claim (so often "a new concept in radar reliability") radars do break down, and the proximity of a manufacturer's service depot or trained agent—there are few about can make or mar a sailing holiday in certain circumstances. This is actually a factor in the price of the radar, since widespread service organisations are not maintained for nothing, and charges must be realistic.

#### USE

A brief look at what radar will do for you. Collision avoidance was its original object and still holds pride of place in the minds of most people. On a dark night or in fog, the possession of radar confers peace of mind, in that it should be impossible for anything bigger than a football, providing it is projecting far enough, to come dangerously close undetected. And if you want to see whether another vessel will hit you if both stand on, it is only necessary to take successive bearings of her when your own boat is dead on course. If they do not alter considerably she will at least pass close. This check is more easily performed than with a compass.

However, study of an article that appeared some time ago in the yachting press on the uses for which radar was put throughout a seven port cruise, showed that collision avoidance came up only once in half a dozen times. Why do virtually all Scottish motor fishing vessels fit a radar when the instance of fog on the North East coast of Scotland is in fact slight? They use it for a multitude of small tasks from locating the small dan buoy which marks the end of their net, to fixing their position. Most radars are efficient, in calm conditions, down to about 20 yards and this can be a great help in locating your moorings or picking your way into harbour among lines of moored yachts.

Coastal navigation is a subject in itself, but basically, everything that the navigator does to fix his craft by cross bearings can be emulated and more quickly, with radar. In addition, a range facility is added, enabling 'range and bearing' fixes to be obtained as well. Is important of course that the point you are taking on the display is exactly identifiable on the chart; this is not difficult with experience but it is advisable to practice in good conditions when checking is easy.

#### CONCLUSION

In conclusion, a quote from an american enthusiast, which is being proved by more and more British owners: "Since the fitting of radar we have cruised thousands of miles more safely and without the anxiety that is ever present when compelled to operate in thick weather, or to enter a strange harbour at night."



<u>What do you know?</u>

- 1 You want a transformer to supply 24 volts at 1 amp. You have a 24 volt 500mA, a 12-0-12V 2A and 30V 1A which one would you use, and how would you connect it.
- 2 A coil and a capacitor are used to form a tuned circuit in a project you are building. The coil you have is slightly higher in inductance than that required, you cannot alter its value so what could you do to get the correct resonant frequency.
- 3 What does the following circuit symbol represent:



4 The impedance of a coil is stated as being

400 ohm, when you measure its resistance on a multimeter it is only 100 ohm. Say if you think this is correct and why.

#### ANSWERS

core and a screen between the windings. This could well be correct, the impedance is measured at a particular frequency and will always be higher than the d.c. resistance.

is increased, reduce C for the same f. 3 A transformer with two windings, a laminated

frequency  $f = \frac{2\pi\sqrt{LC}}{1}$  thus if L (the inductance)

may be slightly high). 2 Reduce the capacitor value slightly. The resonant

Use the 12-0-12V 2A, connect across the two tags marked 12V (this gives a 24V winding) ignoring the 0V tag. The 2A is a maximum rating and the transformer can supply the 1A required without trouble (although the voltage

Everyday Electronics, September 1973

7

Bothered by Basics ? Confused by Current ? Troubled by Transistors ?



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October issue on sale Friday, September 21



# Aquarium THERMOSTAT

## **BY MIKE KENWARD**



# A unit for accurate temperature control of liquids.

**P**ROPRIETARY thermostats for fish tanks and other heat control and monitoring applications are available and many of them are simple and cheap. However 'it has long been the requirement of many tropical fish keepers and others to have a more reliable, more accurate thermostat that can be set to the required temperature and that will maintain the temperature of a liquid to within  $^{1}_{2}$  degree centigrade.

The thermostat to be described in this article was designed for this purpose and was found in practice to be extremely accurate, once set, and able to keep the temperature to within less than  $1_2$  degree should this be required.

#### CIRCUIT

The circuit diagram of the thermostat is shown in Fig. 1. Transistor TR1 is operating in the emitter follower mode, the output of which is determined by the setting of VR1 and VR2, and by the resistance of thermistor RTH1 which is determined by its temperature. The output from TR1 emitter is fed, via a current limiting resistor R2, to a Schmitt trigger formed by TR2 and TR3. The use of TR1 prevents undue loading of the Schmitt by the thermistor.

The thermistor RTH1 is located in the liquid, the temperature of which is to be controlled. With a fall in temperature the resistance value of RTH1 rises and causes TR1 to pass less current through its collector emitter junction. Thus the voltage at TR2 base falls and TR2 begins to turn off, at a certain level (set by R3, R4 and R6, TR3 turns on and forces TR2 to



turn completely off (Schmitt action). This switching of states happens very quickly and TR3 switches from off to fully on with only a slight change in the value of RTH1.

Transistor TR3 operates a relay which is used to switch the mains supply to a tank heater. Thus when TR3 turns on the heater is turned on and the liquid begins to warm up. When the required temperature is reached the fall in the resistance of RTH1 causes TR1 current to rise and the Schmitt to revert to its original state (TR2 on TR3 off) thus turning off the heater via RLA1.

#### HYSTERESIS

Although the above action is straightforward one problem is encountered—the hysteresis present in the Schmitt trigger circuit. This means that the unit would only switch with a

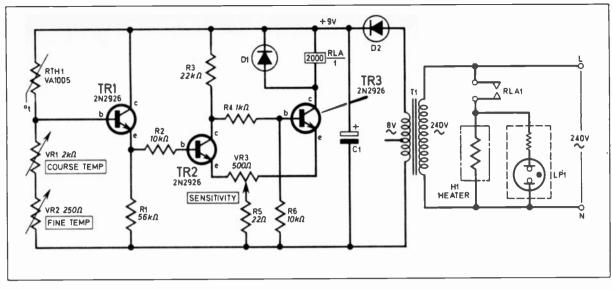


Fig. 1. The complete diagram of the Aquarium Thermostat.

rise and fall in temperature of about 3 degrees centigrade which is greater than the required temperature control.

To overcome this VR3 has been incorporated in the Schmitt circuit and this resistor is used to "balance" the two transistors and thus reduce the amount of hysteresis. Thus this potentiometer can be used to vary the sensitivity of the thermostat and can be set to keep the temperature to within about plus or minus 5 degrees centigrade down to less than plus or minus  $^{1}_{2}$  degree centigrade. In actual fact the prototype was able to maintain the temperature to a very high degree of accuracy—higher than is practically useful in an aquarium and higher than we were able to measure by conventional means.

#### SUPPLY

Power for the circuit is derived from the mains via the bell transformer T1, the rectifier D2 and smoothing capacitor C1. This very basic half wave supply was found to be quite adequate in practice. Diode D1 is incorporated to prevent the back e.m.f., caused by RLA1 switching off, from damaging TR3.

#### CONSTRUCTION

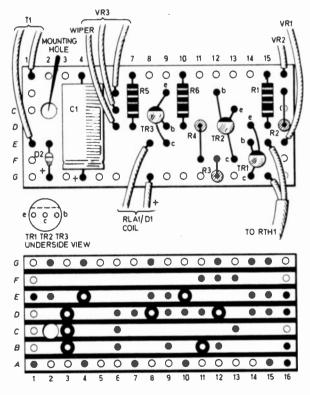
Commence construction by cutting and drilling the circuit board as shown in Fig. 2. Mount all the components—soldering in the transistors and diodes after the other components and flying leads.

Next mount all the components in a suitable metal or plastic case as shown in Fig. 3 and wire up the complete unit. Note that if a metal case is used a three core mains lead should be provided and the box should be earthed by means of a tag bolted to the inside.

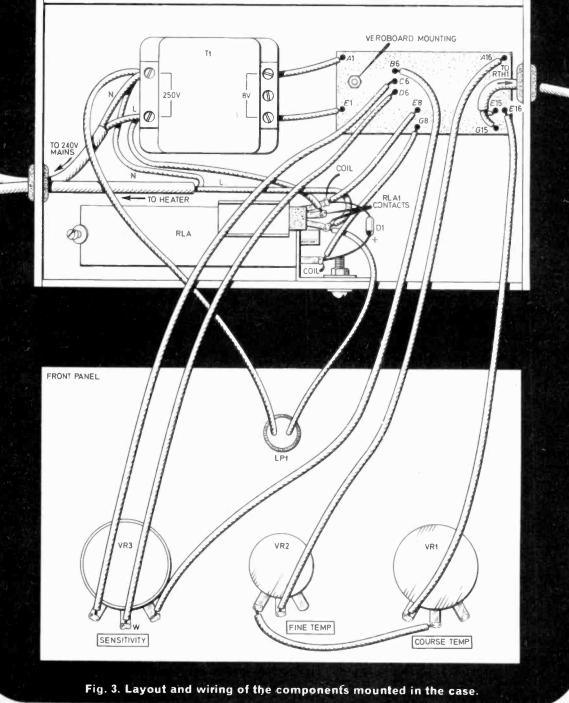
Everyday Electronics, September 1973

The themistor must be isolated from the water and can be mounted in any convenient way. The prototype used a thermistor mounted on the end of a short length of plastic tube (ball pen case) and covered in Araldite to insulate and protect it. Take care not to use too much Araldite on the thermistor as this may prevent it from reacting quickly to temperature changes.





# Aquarium THERMOSTAT



	_
Components	
Resistors	
R1 56kΩ SEE	
R2 10kΩ	
R3 22kΩ	
$\begin{array}{c} R4 & 1k\Omega \\ R5 & 22\Omega \end{array} \qquad $	
R5 22Ω	
R6 10kΩ	
Capacitor	
C1 100µF elect. 15V	
Variable Resistors	
VR1 2kΩ carbon linear	
VR3 250Ω carbon linear	
VR3 500Ω carbon linear	
Semiconductors	
D1 Any small signal silicon diode	
D2 IN4148 or any 50V 200mA silicon diode	- {
TR1 2N2926 (any colour) silicon npn	
TR2 2N2926 (green) silicon npn	
TR3 2N2926 (green) silicon npn	
Miscellaneous	
RTH1 VA 1005 thermistor	
RLA 2000Ω P.O. type 3000 relay with one set o	f
normally open contacts	
T1 Friedland bell transformer (200–250)	'
primary, 8V secondary)	
LP1 Neon indicator lamp with built in resistor	
Veroboard $2\frac{1}{2} \times 1\frac{1}{6} \times 0.15$ inch matrix, small alumin	
ium bracket for RLA, mains lead, materials fo	
mounting RTH1 (see text), plastic case approx	
7 x 4 x 3 inches, 4BA fixings, mains plug, knobs	; )
as required.	Γ

#### **TESTING**

Connect the unit to the heater and mains and with RTH1 in free air and VR3 fully clockwise switch on. Turn VR1 (coarse temperature) through the range and check that RLA1 clicks in and out as you do this, LP1 is incorporated to show when the relay is operating (ie. heater on). Next set VR2 (fine temperature) fully clockwise and VR1 so that RLA1 has just operated switched on the heater—now turn down VR2 and check that as it nears its minimum value RLA1 drops out—turn up VR2 until RLA1 just operates.

By breathing on the thermistor it should now be possible to cause RLA1 to drop out and switch off the heater. Now test the function of VR5 (sensitivity) by turning it fully anticlockwise and resetting the unit as above. It should now take a greater rise in temperature to make RLA1 operate.

If all is well place RTH1 in the tank and turn VR1 up, when the required temperature of the liquid is reached back off VR1 and adjust both VR1 and VR2 until RLA1 just drops out. Leave the unit set and observe the rise and fall in the

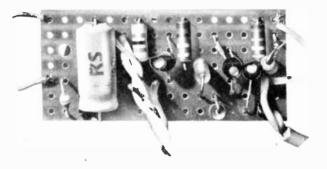
Everyday Electronics, September 1973

temperature.

By adjustment of VR3 and the two temperature controls the correct temperature and controlled level (rise and fall) can be set. This may take a little time but once set will remain constant. Any latter alteration of VR3 (sensitivity) may also mean slight adjustment of VR2 and possibly VR1 tc maintain the correct temperature.

The thermostat can be used to maintain the temperature of other liquids—such as used in colour photographic work—but for accurate control the thermistor should be mounted away from the heater and some means of "stirring" the liquid introduced.

Photograph of the completed Veroboard with the components mounted on it.





The connections to VR1 and B1 positive on the Waa Waa Veroboard layout (page 439, August '73) should each be moved one place to the left to position A9 and A8 respectively. The wiring diagram of Fig. 6 with reference to these connections is correct. The connection from A2 to SK1 should be omitted and the screen from C2 should be connected to SK1 auxiliary tag.

In the *Electronic Doorbell* article (August '73) transistor TR5 was incorrectly shown as an AC 126. This should have been an AC 176.

Under What Do You Know it was stated that the AC 127 could not be used in place of the BC 109 because it is a *pnp* device. It is an *npn* device but it would not be as likely to work as the 2N2926 because it has a much lower gain.

We apologise for any confusion caused by these mistakes.



W<sup>E</sup> continue this month with further properties and theory of the transistor and introduce some transistor types which will be completed in Part 5.

#### COMMON EMITTER CURRENT GAIN

The a.c. current gain of a transistor in the common emitter circuit is usually designated  $\beta$ , z',  $h_{21}$  or  $h_{1e}$ . It is given by the equation:

$$\beta = \frac{\text{change in collector current}}{\text{change in base current}}$$

The current gain of typical transistors in the common emitter circuit varies from about 5 to 1,000. It varies from one type of transistor to another, but even amongst transistors of the same code number there are variations in the current gain of between about two times to five times (depending on type). The current gain is temperature dependent.

The common emitter current gain usually rises at first with increasing collector current until it reaches a maximum, after which it falls again (see Fig. 4.1).

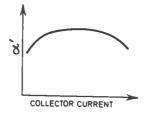


Fig. 4.1. Variation of current gain with collector current in a typical transistor.

Some transistors (such as the 2N2484) are designed so that they provide a high current gain even at very low collector currents (perhaps 0.01mA), whilst other transistors provide a high gain in the medium current range (typically 1mA to 100mA) and yet others in the high current range (perhaps 5A to 10A).

The common emitter circuit not only provides a current gain of over unity, but it also provides a voltage and a power gain when used in a suitable circuit. The power gain provided is normally greater than that obtainable using the same type of transistor in either of the other basic circuits.

#### LEAKAGE CURRENT

In Fig. 4.2a, a transistor is biased in the normal way with the collector positive with respect to the base, but the emitter is left unconnected so that the emitter current is zero.

Although the collector/base junction is reverse biased, a small current will pass, since both of the materials contain limited numbers of minority carriers which are attracted across the junction (as in the reverse biased diode). This small current is known as the **leakage** current.

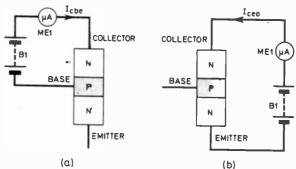


Fig. 4.2. Measurement of leakage current.

The leakage current in the common base connection is designated  $I_{cbo}$  (or sometimes  $I_{co}$ ). The subscrip "cb" indicates that the current flows between the collector and base, whilst the third subscript, "o", shows that the current passing to the third electrode is zero.

The leakage current in Fig. 4.2a is that of the collector/base diode and is therefore much smaller in the case of silicon transistors than in germanium devices.

The common emitter leakage current is measured with the base open circuited as shown in Fig. 4.2b. It is normally given the symbol  $I_{ceo}$ , but is sometimes designated  $I_{co}$ .

The value of the common emitter leakage current is much larger than that of the common base leakage current. The leakage current of the collector/base diode acts as the base current and is therefore amplified by the current gain of the transistor concerned.

In a germanium transistor  $I_{ceo}$  may be some hundreds of microamperes, increasing slightly with applied voltage over the working range of the transistor.

The leakage current of any transistor increases rapidly with temperature for the same

reason that the leakage current of a diode increases with temperature.

#### **PNP TRANSISTORS**

The principles of operation of pnp transistors are exactly similar to those of npn transistors, but the polarities of the applied voltages are reversed and the charge carriers are of the opposite polarity.

As shown in Fig. 4.3, the base is forward biased with respect to the emitter, so in this type of transistor the base must receive a negative bias (as opposed to the positive base bias of the npn type). Similarly, a negative voltage is applied to the collector so that the collector/base junction is reverse biased.

The *n*-type base is lightly doped, so the emitter/base current consists mainly of holes moving from the emitter to the base with only a few electrons moving in the opposite direction.

Most of the holes passing from the emitter into the base reach the depletion region of the collector/base junction and they are then swept into the collector to form the collector current in the external circuit.

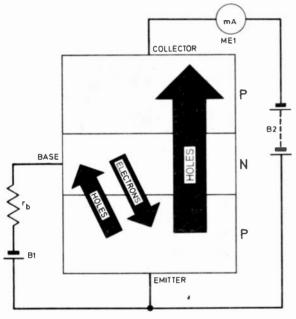


Fig. 4.3. Flow of charge carriers in the *pnp* transistor.

#### **SYMBOLS**

The normal symbol for an *npn* transistor is shown in Fig. 4.4a. Sometimes the circle is omitted for simplicity, since it is only used to indicate that the device is sealed in a suitable encapsulation.

The direction of the arrow shows the direction in which conventional current flows in the emitter circuit. (Conventional current flows from the positive to the negative terminal of a

Everyday Electronics, September 1973

battery in the opposite direction to the flow of electrons.)

Fig. 4.4b shows the symbol used for a *pnp* transistor. It is similar to that of the *npn* transistor, except that the direction of the arrow is changed.

Alternative symbols for the *npn* and *pnp* transistors are shown in Figs. 4.4c and 4.4d respectively.

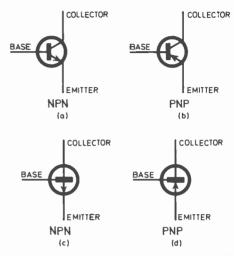


Fig. 4.4. Symbols for npn and pnp transistors.

#### **BASE VOLTAGES**

The forward bias applied to the base of a silicon npn transistor results in this electrode being about 0.5 to 0.6V positive with respect to the emitter.

This follows from the fact that a forward biased silicon diode does not pass very much current until this forward voltage is reached, but the current then increases very rapidly with forward voltage (refer to Fig. 2.8 in Semiconductors Part 2).

Similarly, the base of a germanium npn transistor operates at about 0.15V positive with respect to the emitter.

The base operating voltages of silicon and germanium pnp transistors are about -0.5 to -0.6V and about -0.15V respectively relative to the emitter.

#### COLLECTOR VOLTAGES

If the collector of a transistor is operated from too low a supply voltage, the maximum output voltage swing will be limited and the gain may be reduced. Generally, supply voltages below about 3V are seldom used. The upper limit depends on the type of transistor used for the reasons discussed below.

Some silicon transistors are designed to operate with collector voltages well above 100 volts, but most types are only capable of satisfactory operation at lower voltages.

Germanium pnp transistors are seldom

designed to operate with their collector voltages more than 80V negative with respect to their emitter voltage.

If the collector/base voltage is made greater than the maximum permissible value quoted in the manufacturer's data sheet, **avalanche breakdown** of the collector/base junction may occur. (The doping level in transistors is usually greater than that at which true Zener breakdown takes place.)

A maximum permissible value of the collector/base reverse voltage,  $V_{cbo}$  (or, sometimes,  $V_{cb}$ ), is therefore quoted in the data sheet. This is the collector/base maximum voltage when the emitter current is zero.

The maximum permissible collector/emitter voltage with the base open circuited (that is, with zero base current) is designated  $V_{ceo}$  and is often lower than  $V_{cbo}$ , since the collector/base leakage current is multiplied by the current gain of the transistor.

In addition to normal avalanche breakdown, an effect known as **second breakdown** can occur in which some parts of the junction become hotter than others. If any part tends to become hot, conduction in that part may become more like conduction in a metal, so that the current concentrates there and makes it hotter still.

A voltage applied between the collector and emitter (but not between the collector and base) can lead to an effect known as **punch-through**.

In this case the collector/base depletion region becomes so deep that it encompasses the whole of the base region and enters the emitter. When this occurs, a large current can flow between the collector and emitter.

The punch-through voltage depends mainly on the base width and resistivity; in many transistors the punch-through voltage is arranged to be of the same order as the avalanche breakdown voltage of the collector/ base junction.

Although avalanche breakdown and punch through do not *in themselves* destroy the transistor, in most circuits they would cause such a high current to flow that the power dissipation in the device would be great enough to destroy it. The manufacturer's limiting values of  $V_{\rm cbo}$ and  $V_{\rm cbo}$  should therefore be strictly observed.

#### FREQUENCY LIMITS

The amplification given by a transistor falls off at high frequencies, the symbol  $f_T$  is used as a meaure of this fall in modern transistors; it is the **gain-bandwidth product** or, more precisely, the common emitter current gain multiplied by the bandwidth measured in the frequency region where the gain is falling fairly rapidly.

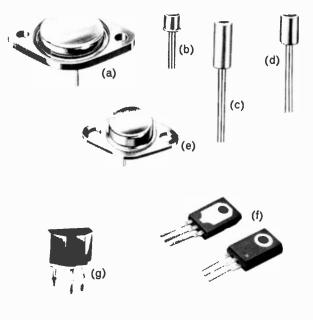
It must be stressed, however, that the high frequency performance is dependent on the circuit in which the transistor is used as well as on the properties of the transistor itself. It is not always wise to use a transistor with a good high frequency performance in a circuit where this property is not really needed, since oscillation at a very high frequency may occur. The latter may not be easy to detect.

It should be remembered that the value of  $f_{T}$  quoted by most manufacturers is the minimum value and many specimens of their transistors of a specified type number may have a far higher value of  $f_{T}$ .

#### TRANSISTOR TYPES

The number of transistor types on the market is extremely large. It is obviously necessary to have many different types available for various purposes but the profusion of type numbers now available tends to confuse not only the beginner, but also the somewhat more experienced designer.

This series will give some information on the ways in which some types of transistor provide the characteristics required by the circuit designer, but it is obvious that this account cannot be a comprehensive review or even cover the majority of the types in normal use. In general only the more common types will be considered and no attempt will be made to include details of transistors suitable for operation at GHz (1,000 million Hz) frequencies or of any radio frequency power transistors.



Photograph showing some of the various transistors available: (a) AD149 (b) BC107 (c) OC72 (d) AC128 (e) AD161

(f) BD201 (g) BC147—Lockfit. (Mullard)

Everyday Electronics, September 1973

480

#### TOLERANCES

Manufacturers can produce cheap transistors only if they can sell huge quantities of each type and if they do not have to carry out long testing procedures or guarantee that their products have very close tolerances.

The most expensive devices have tended to be used in the military and space research fields where human lives may depend on the satisfactory operation of a large number of devices over a long period.

Somewhat cheaper transistors have been used for general industrial purposes and in instrument manufacture, whilst the cheapest devices are used in the domestic entertainment field where wide tolerances are of no great disadvantage if one allows for them in the circuit design.

#### **REPLACEMENT TYPES**

Although this article may help readers to choose a suitable replacement type for a defective transistor, it cannot be stressed too strongly that the manufacturer's data sheet should always be examined in detail before any transistor is used to replace another type or is used in a new circuit.

In many cases modern epoxy encapsulated silicon transistors can be used as a cheap (but perfectly satisfactory) replacement for some of the types supplied in metal cans. Epoxy encapsulation is a kind of plastic material and can be used for silicon (but not normally germanium) device manufacture.

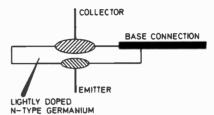
Germanium devices were developed before the more modern silicon types and will therefore be covered first.

## PNP ALLOY JUNCTION GERMANIUM TYPES

Some of the earliest transistors were produced by the alloy junction process. If a pnp germanium transistor is to be made, pellets of the *p*-type additive are placed on each side of a wafer of lightly doped *n*-type material.

In the case of the OC71 transistor, for example, the size of the *n*-type wafer is  $4 \times 2 \times 0.12$  mm.

After suitable heat treatment, the *p*-type additive diffuses into the wafer to form a *pnp* device with a lightly doped base. The cross section of such a transistor is shown in Fig. 4.5.



## Fig. 4.5. The structure of an alloy junction transistor.

Transistors manufactured by this technique are suitable for use only at audio and low radio frequencies. For example, the *pnp* audio frequency transistor type OC71 has a typical common emitter cut off frequency of 11kHz (minimum 5kHz) and a common base cut off frequency of 600kHz.

The *pnp* OC45 has a thinner base and can be used as a 475kHz intermediate frequency amplifier in radio receivers, since the thinner base raises its common base cut off frequency to about 6MHz.

The pnp OC44 has about the optimum high frequency performance possible with transistors manufactured by the alloy junction technique; it has a common base cut off frequency of typically 15MHz (minimum 7.5MHz) and is often used as a self oscillating mixer in radio receivers for the medium and long wavebands. Various other types, such as the OC42, are similar to the OC44.

Device	V <sub>cbo</sub> (V)	V <sub>ceo</sub> (V)	l <sub>c max</sub> (mA)	P <sub>t max</sub> (MW)	h <sub>fe</sub>	f <sub>T</sub> (MHz)	Application	
pnp				-	50	0.6	Medium gain general purpos	
OC71	-30	-20	10	75	50	• -		
OC75	-20	-20	10	75	90	0.6	High gain general purpose	
OC45	-10	-10	5.0	43	50	6.0	I.F. amplifier in medium frequency receivers	
OC44	-10	-10	5.0	43	100	15	Mixer/oscillator in medium frequency receivers	
OC72	-16	-16	125	75	70	>0.35	Low power output transistor	
0C77	-60	-60	125	75	>45	>0.35	High voltage low power swite	
			200	150	60-120	15	General purpose	
2N1309	-30	-15	200	150	00-120	15	Ocheral pulpose	
npn	00	45	250	145	20-84	3.5	1	
OC139	20	15			*** * * *	4.5	Medium current transisto	
OC140	20	15	400	145	20-150		Swedium current transisto	
OC141	20	15	400	145	80200	9.0	5	
2N1308	. 25	15	200	150	80-300	15	General purpose	

**Table 4.1: Germanium Alloy Junction Transistors** 

1

1

Returning to audio transistors, the OC71 has a common emitter current gain of 30 to 75 at a collector current of 3mA. The OC75 is a high gain version with a current gain  $h_{te}$  or  $\beta$  of 60 to 130 at a collector current of 3mA.

The OC71 has a collector voltage rating of 20V, but the thinner base of the OC44 and OC45 involves a reduction of the collector rating to 10V.

All of the above types except the OC42 are encapsulated in a small, black painted, glass tube with the three leads emerging from the one end, as shown in Fig. 4.6.

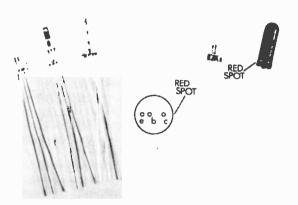


Fig. 4.6. The OC71 type transistor showing stages of production. (Mullard)

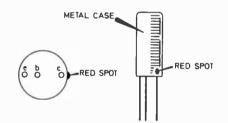


Fig. 4.7. The OC72 type transistor.

The OC71 is rated at a maximum average collector current of 10mA. The OC72 has a maximum average collector current rating of 125mA and has been much used in the past in the output stages of small radio receivers. It is encapsulated in a metal tube, as shown in Fig. 4.7, so that the heat will be conducted away if it is placed in a small heat sink.

The OC77 is essentially a high voltage version of the OC72.

Low noise types, such as the AC107, are available, but one can obtain a better low noise performance with a modern silicon planar type.

#### PNP ALLOY DIFFUSED GERMANIUM

The *pnp* alloy diffused germanium transistors have been widely used in the radio and inter-

mediate frequency sections of radio receivers.

A cross section of such a transistor is shown in Fig. 4.8.

The manufacturing technique employed enables a base width of a few thousandths of a millimetre to be obtained. A drift field is developed by adding both *n*- and *p*-type impurities to the emitter pellet and allowing the *n*-type material to penetrate more deeply into the crystal than the *p*-type at a high temperature so that a graded base layer is formed.

Such transistors have a high gain at a low collector current and a low collector base feedback capacitance.

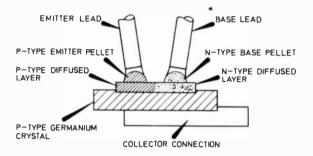


Fig. 4.8. The structure of an alloy diffused germanium transistor.

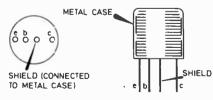
The OC170 and OC171 are two well known types manufactured by this technique. They have an  $h_{tr}$  value of about 100 (minimum 20) and a cut off frequency of around 70MHz.

In current radio receivers these transistors have been replaced by the AF114 to AF117 series. The AF114 is a v.h.f. amplifier for f.m. receivers, the AF115 a mixer/oscillator for a.m./f.m. and short wave receivers, the AF116 an i.f. amplifier for f.m. receivers and the AF117 a mixer/ oscillator and i.f. amplifier for the long, medium and short wave bands.

Another use for alloy diffused transistors is as video amplifiers in television receivers and the AF118 has been designed especially for this purpose.

All of the alloy diffused transistors mentioned above have the type of construction shown in Fig. 4.9. The shield electrode is connected to the metal case and should be earthed.

Alloy diffused *npn* germanium transistors do not appear to be available.



#### Fig. 4.9. The OC170 and OC171 types of transistor.

Next month: More types, manufacture of planar devices and testing.

HE initial purchase of model train equipment is often in the form of a "set" with train, track and a plastic battery box fitted with an on-off-reverse switch only.

The absence of any form of speed control and the expense of frequent battery replacement soon leads to the acquisition of some form of resistive controller and, either a proprietary mains transformer/rectifier unit, or a battery charger.

Those with a little know-how elect to construct their own mains supply unit using a heavy duty variable resistance of 100-200 ohm as the controller. Only a little experience is needed to show that a variable resistance controller is not really satisfactory and to counter the effects of uneven running, indeterminate starting, etc., the enthusiast begins to consider the purchase of an electronic control unit

This article details the construction of an electronic speed control incorporating short circuit protection and a facility for automatically giving a gradual and realistic speed change to stop and start at signals and stations.

#### **POWER SUPPLY**

The unit operates from an approximate 12V reasonably smooth d.c. supply. If such a supply is not readily available the novice is strongly advised to purchase a proprietary unit or to obtain expert help in building a mains transformer/rectifier unit since it is vital that safety requirements are met and that children cannot gain access to high voltages.

The transformer rating should be approximately 14V a.c. at 2 amps, though it is well to consider the advantage of a slightly more expensive one rated at 4 amps preferably with two sets of windings to provide two independent

BY A. J. DUNN

Gives realistic performance to your electric model train

HI



d.c. supplies and ample unrectified a.c. for electric point operation, lamps, etc.

A smoothed supply is essential.

Many proprietary units have no smoothing since the action of the train's motor is to average out the waveform. If such a supply unit is voltage available it may be used if an electrolytic capacitor of approximately  $2000\mu$ F is connected across its terminals.

The working voltage of such a capacitor should be at least 20V since it will charge up to the peak voltage value when not connected to a load; when on load the voltage will fall to a lower voltage with a waveform as in Fig. 1.

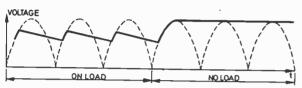


Fig. 1. Shows the voltage increase for no load condition.

Such a smoothing capacitor will take a momentary large charging current, possibly in excess of a fitted current trip. In such a case the trip should be wired *after* the supply has been smoothed. Should it be intended to use an unprotected d.c. supply other than for the short circuit protected circuit to be described, it would be necessary to provide a means of short time constant overload protection such as a quick acting magnetic cut out. Similarly, any a.c. output could be protected by a thermal cut out.

#### DESIGN REQUIREMENT

The starting performance of a loco is a common source of dissatisfaction; unless the resistive controller is well advanced it is often found that the loco will not move at all and then it suddenly speeds up, requiring immediate controller adjustment to avoid excess speed at points, curves, etc.

This effect is comparable to attempting to start off and drive a car in top gear; obviously the equivalent of a gear box is required, or a means to change the torque/speed characteristic.

In this design, this effect is achieved by switching the supply on and off at a fast rate; the ratio of the time it is switched on to the time it is switched off (the mark-space ratio) is varied by a control so that the extreme ends of the control range corresponds to the supply being virtually fully on or off.

In the condition of starting from rest, the supply is switched on for brief periods only (Fig. 2a), each period being long enough to develop the maximum torque from the motor but not long enough to allow for much movement so the loco moves in a series of almost undetect-

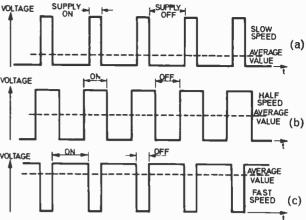


Fig. 2. Shows that the average value is proportional to the mark-space ratio.

able jerks, slowly increasing speed.

In the half-way position, the controller creates an equal mark-space ratio or on for half the time (Fig. 2b) and the inertia of the motor integrates this and runs as if powered by half the supply volts.

In the fast position the controller switches the supply on for most of the time (see Fig. 2c) and the loco rail voltage is therefore the supply voltage (12-14V d.c.) less a 0.7V drop across TR1 and less the small voltage drop across R6 dependent upon the current taken.

#### TRAIN MOTOR

Consider the loco motor as shown in Fig. 3 here the resistance of the motor windings is shown as  $R_m$  in series with a generator—this being the back e.m.f. generator with an output proportional to speed.

At rest, when the supply is connected, the current that flows is the supply voltage  $V_{\rm a}$  divided by  $R_{\rm in}$  plus the control resistance  $R_{\rm c}$  (including the supply resistances). The torque caused by the current causes the motor to revolve and overcome initial or static friction whereupon the motor runs faster and the back e.m.f. increases.

The current taken is now

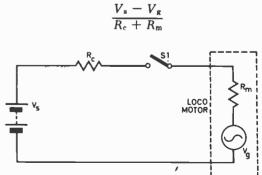


Fig. 3. The equivalent circuit of the loco motor in circuit.

Everyday Electronics, September 1973

484

and the torque is reduced accordingly. It is obvious that if  $V_s$  and  $R_c$  are both made very large and constant (normal constant current circuit) the motor speed will vary as a function of the load and, in cases of indeterminate frictional effects, will vary wildly.

From this consideration, the series resistance should be reduced as far as possible and the motor speed controlled by either a variable voltage low impedance source or by a fixed voltage and switched time division.

#### CIRCUIT

The complete circuit diagram of the train controller is shown in Fig. 4. Transistors TRA and TRB (inside the integrated circuit) form a multivibrator whose period is determined by the values of the capacitors C1, C2, R1 and (R2+ VR1). The mark-space ratio is approximately 1:1 with the wiper of VR1 in the central position, and the collector of TRB (pin 5) is alternately at the supply voltage or approximately +0.2Vwhen TRB is turned on hard or saturated. This square wave signal is applied via R4 to TRC which is switched on or off.

For the moment leaving aside transistor TRD, the collector of TRC is connected to the base of TRE which forms, with TR1, a compound emitter follower giving a large current low impedance square wave output.

Diode D2 is wired in the circuit, reverse

biased, to protect TR1 from transient reverse voltage produced by the inductance of the motor winding and commutator switching.

#### SHORT CIRCUIT PROTECTION

Short circuit protection is provided by the use of R6 (approximately 0.5 ohm), the connections to TRD being so arranged that if a current in excess of 1.5 amps flows through R6, the voltage across it will turn on TRD.

The base current of TRD is limited by R7, but it will saturate and the collector of TRD will fall to approximately +0.2V pulling down the base of TRE and virtually turning off TR1.

Accidental short circuits are thereby limited to approximately 1.5 amps though this figure may be readily changed by changing R6 such that,

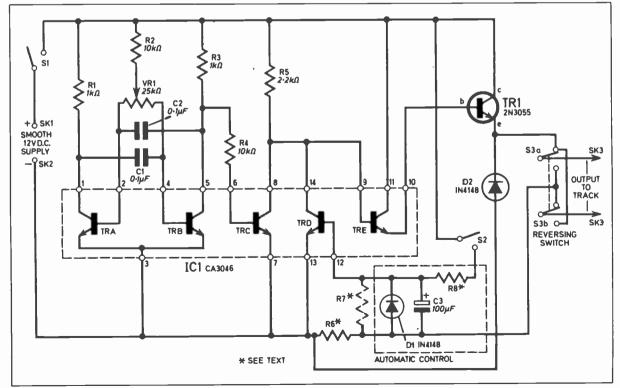
(short circuit current in amps)  $\times$  (R6 in ohms)  $\simeq 0.7V.$ 

#### AUTOMATIC CONTROL

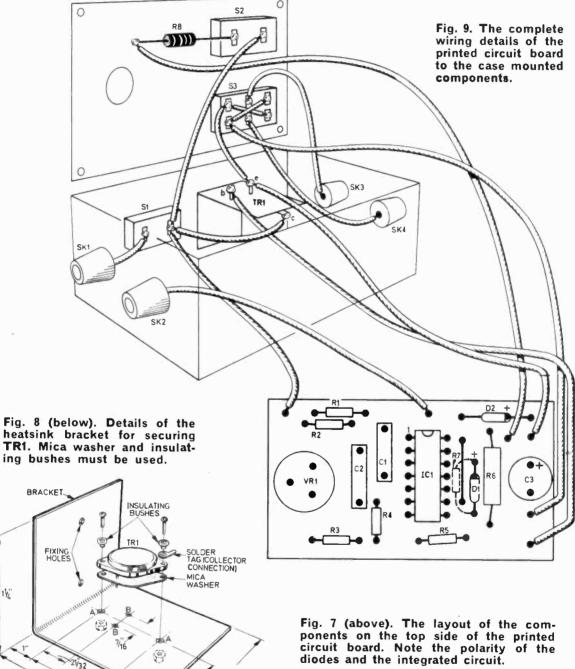
Automatic control is achieved by replacing R7 with D1, C3 and R8 as shown in Fig. 4.

Consider first that S2 is open: if a short circuit is applied to the output, the voltage across R6 will be applied via D1 to the base of TRD. The voltage that must be produced across R6 to saturate TRD is now approximately 1.4V made up of 0.7V to turn on D1, and 0.7V the voltage dropped across the base/emitter junction of TR1.

Fig. 4. The complete circuit diagram of the Train Controller.



# NTROLLE



11/2

132 13/16

5/8

2 HOLES A 5/32 DIA 2 HOLES B 1/8 DIA

14%

The value of R6 should be selected accordingly.

Assume that the control VR1 is adjusted centrally to give a 1:1 mark-space ratio and that a train is running to a signal set at stop.

If S2 is closed, C3 will charge slowly via R8. The time constant of C3, R8 is given by

 $t(secs) = (R8 \text{ in ohms}) \times (C3 \text{ in farads})$ 

With R8 at 100 kilohm this gives t = 10 secs.

However, this corresponds to approximately 60 per cent of the charge voltage, or 7V from a 12V supply and only approimately 1V is necessary to operate TRD. The relationship between time and charge is approximately linear so 1V will be obtained in one-seventh of the time for 7V or  $10/7 \text{secs} \simeq 1^{1}_{2} \text{ secs.}$ 

As C3 charges, TRD will gradually pass more current, limiting the pulses from TR1 and after  $1_{2}$  seconds TR1 will be cut off and the train stopped.

Consider now that the signal aspect is changed and that by the use of a parallel switch or a relay, S2 is opened. The charge on C3 cannot pass via D1 (reverse biased) and so must dissipate by providing the base current to TRD. As the charge on C3 falls, so the current taken by TRD falls and output pulses from TR1 increase and start the train. After a short period C3 is virtually discharged and the train runs as in the original condition.

#### PRINTED CIRCUIT BOARD

The unit is to be constructed on a piece of printed circuit board the full-size drawing of which is shown in Fig. 5. The component layout on the top side of the board is shown in Fig. 6, the only critical positioning being the holes for VR1 and the integrated circuit, ICI via its holder.

Note that R7 is shown (dotted) for initial testing; automatic control is obtained (if desired) by replacing R7 after testing with D1 and C3 wired as shown.

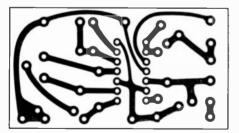


Fig. 5. The full-size master of the printed circuit.

#### CONSTRUCTION

The printed circuit board should be produced as described in the article Making Printed Circuit Boards, E.E. June 1973.

When the board is ready, drill all the holes with a No. 62-68 drill bit and then enlarge the holes to take the potentiometer VR1 with a larger drill or small file so that a snug fit is

Everyday Electronics, September 1973

obtained.

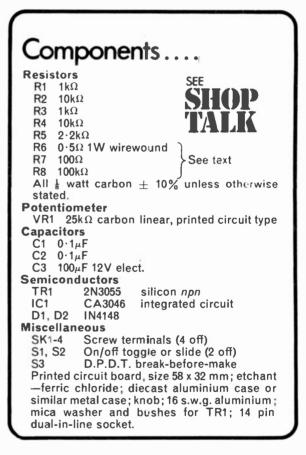
Next solder VR1, the i.c. holder, the resistors and capacitors in position as indicated in Fig. 6. If the automatic control is to be installed leave the leads of R7 long for easy removal later. When this has been done plug in IC1 ensuring that it is the correct way round; this is done with reference to the notch at one end of the integrated circuit.

Next make the aluminium heatsink bracket as shown in Fig. 8 for the power transistor TR1 and fix the latter to the bracket via a mica washer and insulating bushes.

Secure the solder tag to the case of TR1 via one of its fixing bolts; this is the connection to the collector of TR1 since the casing is internally connected to the collector.

Put some heatsink compound on the bracket where it is to be in contact with the diecast case and tightly bolt the bracket in position.

Fix the other components to the case and wire up as shown in Fig. 9.



#### TESTING

The board should be carefully examined to ensure that the components have been wired up correctly paying particular attention to the polarity of D2 and the wiring to TR1.

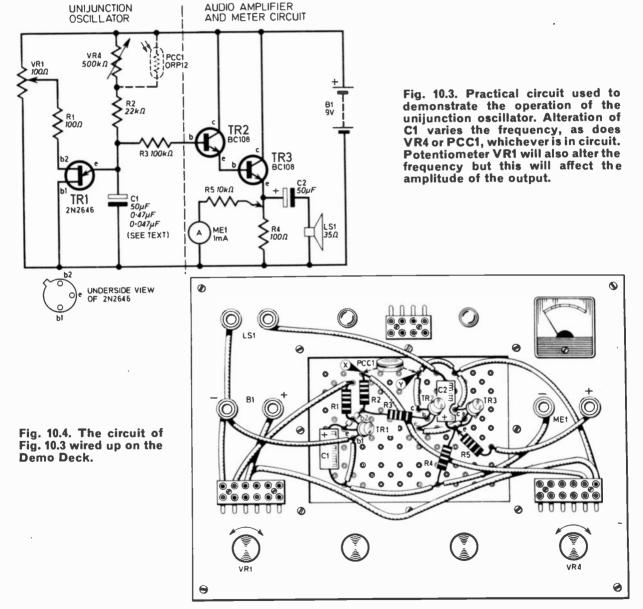
Check for short circuits, solder bridges, etc., and that the polarity of the supply is correct.

falls towards zero—and this encourages more current to flow in from the emitter which again makes  $R_{b1}$  reduce in value. We have, in effect, a sort of positive feedback reaction. The current flowing into the emitter flows out of C1 and the potential at *B* falls rapidly towards zero. When it reaches almost zero the inflow of current reduces and the resistance of  $R_{b1}$  rises back to its original level; the diode again becomes reverse biased and C1 is free to charge up again.

#### **OUTPUTS**

The nice thing about a unijunction oscillator is that we have two possible waveforms at our disposal; one approaching a sawtooth at point Bwhich rises—as the capacitor charges—along an exponential curve and then falls very rapidly to zero. While the feedback reaction is taking place extra current flows through R1 (because the internal resistance of the unijunction falls) and we will get very short duration negative going pulses at point A.

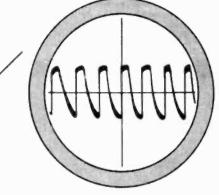
Resistor R2 should always be greater than a certain value otherwise sufficient emitter/base current could flow through it to maintain the unijunction in conduction. On the other hand it can be as high a value as you like—provided it does not approach the leakage resistance of the emitter base junction. Capacitor C1 can be of almost any value hence it is possible to get a tremendous range of frequencies with this very simple circuit by changing the value of C1 and making R2 variable—above a certain value.



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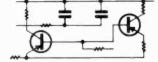


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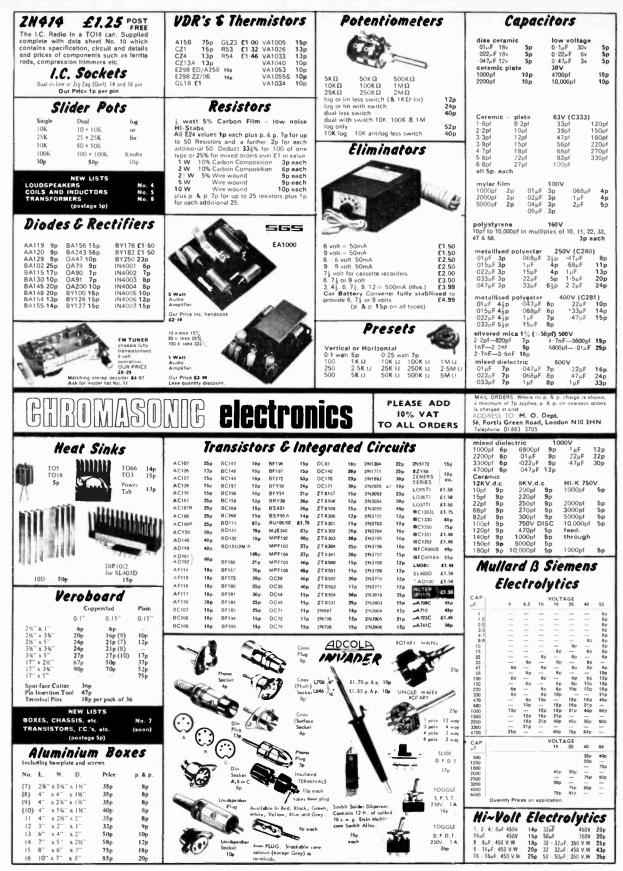
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#### EXPERIMENTAL CIRCUIT

The experiment—shown in Fig. 10.3 will operate very slowly (several seconds per cycle) if C1 is made to be  $50\mu$ F and thus it is possible to monitor the exponential waveform at the emitter on the 1mA meter movement of the Demo Deck. Alternatively insert a lower value capacitor (two alternative values are suggested) and listen to the sound on Demo Deck's loud-speaker. Fig. 10.4 shows the experimental circuit with audible and visual monitoring wired up on the Demo Deck.

Potentiometer VR1 is included to alter the quiescent potential at the point originally called A. Start with VR1 set with the wiper nearest the positive supply rail and then reduce this voltage by turning the potentiometer down; the

frequency of the oscillator will increase because the level to which the capacitor has to charge is being reduced—the amplitude of the signal will, however, reduce. Adjustment of VR4 will modify the frequency over a very wide range without altering the amplitude.

Substitute PCC1 for VR4 and it is possible to make a light controlled oscillator—the basis for an interesting musical instrument if you shade the cell with your hands! An interesting feature of the unijunction is that b1 can be interchanged for b2 and the device will still work, but this will be turning the intrinsic stand off ratio on its head and the amplitude of signal will be nothing like as great—try it and see!

Next part: The Hartley Oscillator



**B** ECAUSE the electronic component industry is booming private constructors are having difficulty in obtaining some components. It sounds stupid but it's true, the manufacturers have trouble in keeping up with the demands of industry and very often cannot supply the smaller customer. At the present time a number of capacitors are difficult to get and we know some firms have been quoted delivery times months away.

Unfortunately there is nothing that either we or the retailer can do about this situation other than be aware of it and try to help you overcome the problems by finding alternative components. So don't always blame the shopkeeper—remember that in this business he is at the bottom of a very long list when it comes to supply deliveries from the big companies.

#### **Personal Receiver**

The Personal Receiver is likely to fall foul of the problems mentioned above-two of the capacitors may be difficult to get (C3 0.1µF and C4 0.05µF, miniature) to overcome these problems we have given an alternative for C3  $(0.22\mu F)$  and we suggest that you use the receiver without C4 until this can be purchased. This will result in some loss of volume as the audio signal will have to pass through R5 instead of being decoupled by C4 but the receiver will work quite well like this.

A marked and drilled printed circuit board for the receiver is available from Valance Electronics, 2A Canel St., Droglesden, Manchester. We believe this firm may also be able to supply the plastic case used.

Finally, remember that this project is fairly small and all the components used should be miniature or very small types as listed in the components box.

#### Train Controller

It seems strange that this issue contains two projects which use integrated circuits, perhaps it's a sign of the times—no doubt these devices will be featured more and more in our projects as the months go by. We suggest that you use a socket for mounting the i.c. in the *Train Controller* so that this can be soldered in without fear of damage to the i.c.

The electrolytic capacitor used should be a printed circuit type and the right size component is available from Electrovalue, 28 St. Judes Road, Englefield Green, Egham, Surrey.

It is mentioned in the text that a metal case should be used as this forms a heat sink for the power transistor. Diecast boxes of the appropriate size are available and should make excellent cases for this project. If you pa.nt the case remember that darker colours dissipate the heat better.

#### Aquarium Thermostat

We had better not praise the Aquarium Thermostat too much, someone might notice who wrote the article! In fact, it is difficult to say much about it since most of the components are generally available. The transformer should be available from most electrical shops or Woolworths. The thermistor can be obtained from most of the larger suppliers, while the relay is available from G. W. Smith should other sources fail.

The heater used with the prototype was a standard one sold for aquarium use. Incidentally, too large a neater (wattage size that is) will result in a poor constant temperature.

Everyday Electronics, September 1973

493



#### **Bulb Resistance**

I measured the resistance of a 6V, 0.04A bulb and was surprised to see it was much lower than expected. To pass 40mA with 6V applied, it should have a resistance of  $\frac{6}{0.04} = 150$  ohm but mine was round about 80 ohm. Is this a "rogue" lamp?

No. The tungsten filament in the bulb has what is called a "positive temperature coefficient of resistance". This means that when it is cold it has a lower resistance than when hot. The current stated for the bulb is that which it draws when it has got up to its working temperature—well over 1,000 degrees Centigrade.

#### Screening

Could you explain—in simple terms—how a screened lead prevents hum pick up?

Hum pick up is often caused by capacitive coupling between a wire and mains wiring in the same area. If you surround the wire in question with a shield (the screen) capacitive coupling will be between the mains lead and this screen. If the latter is connected to ground the potential of the screen remains constant and the capacitively induced current runs straight to ground. According to Faraday (his ice pail experiment) no charge can be induced on a totally enclosed body and as the conductor wire is now totally enclosed by the screen it will pick up no hum.

#### Output Stage

In the days of valves we had to drive loudspeakers with transformers but it seems as though this is not necessary with transistors. Why is this so?

Valves operated by controlling quite high voltages at small currents while loudspeakers — because of their low coil resistances need high current at quite low voltages. If you assume that there is conservation of power between input and output of a transformer it is an excellent device for converting from high voltage swings at low current to low voltage swings at high current. This is why they are used in valve circuits.

On the other hand transistors are basically current controllers and consequently are able to handle low voltages at reasonable currents directly and there is no need to use transformers in most cases. It is, of course, highly desirable to remove transformers from circuits because they are bulky and are never perfectly efficient: they also introduce a degree of distortion that had to be overcome with quite complicated circuitry in the old valve days.

#### Smoothing

In the old days I used to use chokes for smoothing but never see these in modern equipment. Are they not as good as the modern approach—which seems to use a resistor?

The resistor between the two capacitors in a smoothing circuit is not as good as the "old fashioned" choke because it is inefficient (wastes power) and the smoothing effect is not so good.

However, these days when we use transistors in most equipment the current that is drawn from the power supply tends to be very high (compared with that taken by equivalent valve circuitry) and to prevent the core of the choke becoming "saturated" it would be necessary to have a large amount of iron. Not only this but the windings would have to be of stouter wire to carry the higher current. Consequently chokes would be very expensive and far too cumbersome in modern systems. One of the sacrifices in quality we have to make for the convenience of modern living?

### Wiring Layout

Why is it that some of your articles say "layout" is important? Surely a wire is a wire and provided it goes to the right place irrespective of position—then all is correct.

Layout is not always important but in some cases it is. More particularly when the circuit is dealing with high frequencies. All connecting wire—even if it is straight—has a small amount of inductance. This can modify the tuning of radios and introduce reactance where it is not wanted.

There is always a degree of capacitance between a wire and neighbouring components—it may only be small but at very high frequencies this small capacitance can transmit small a.c. currents. These currents might cause positive feedback—making the circuit oscillate—or negative feedback which reduces the gain of the system. You can also get inductive coupling.

In a.c. circuits it is good practice to keep wire lengths as short as possible and to separate input circuits from output circuits. Sometimes neat "loomed" wiring makes matters worse because the bundling together of the wires makes the inter-wire capacitive coupling greater. Generally speaking there are no problems with simple d.c. and logic circuits unless they are operating at very high speeds.



"But dad, the article in here says it's so simple to strip down that even a child could do it."



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Development Protocol Soft each value 4-7Ω to IMΩ. E12 pack 325 resistors £2-40. E24 pack 650 resistors £4-70. POTENTIOMETERS Carbon track 5kΩ to 2MΩ, log or linear (log ±W, lin ±W). Single, 12p. Dual gang (stereo), 40p. Single D.P. switch 24p. SKELETON PRESET POTENTIOMETERS	REPLACES C426, C487 RANGES (µF/V) 1-0(63, 1-5)(63, 2-2)(63, 3-3)(63, 4-7)(63, 6-8)(40, 10)(25, 10)(63, 15)(16, 15)(40, 15)(63, 22)(10, 22)(25, 22)(63, 33)(6-3, 33)(40, 47)(4, 47)(10, 47)(25, 47)(40, 47)(63, 68)(6-3), 68)(16, 100)(4, 100)(10, 100)(25, 100)(40, 150)(6-3, 150)(16, 150)(25, 220)(4, 220)(10, 220)(16, 30)(4, 330)(10, 470)(6-3, 5p each. 68)(63, 150)(40, 220)(25, 330)(16, 470)(10, 680)(6-3), 1000)(4 9p. 100)(3, 150)(3, 220)(40, 470)(25, 680)(16, 1000)(10, 1500)(6-3) 12p. 220)(51, 470)(40, 680)(25, 1000)(16, 1500)(10, 2200)(6-3, 15p. 330)(63, 680)(40, 1000)(25, 1500)(16, 2200)(10, 3300)(6-3, 4700)(4, 18p.
Linear: 100, 250, 500 $\Omega$ and decades to SM $\Omega$ . Horizontal or vertical P.C. mounting (0-1 matrix). Sub-miniature 0-1W, Sp each. Miniature 0-2SW, 6p each.	SOLID         TANTALUM         BEAD         CAPACITORS         12p           0 - 1 µF         35V         2 · 2µF         35V         22µF         16V           0 - 22µF         35V         4 · 7µF         35V         33µF         10V           0 - 47µF         35V         6 · 8µF         25V         47µF         6 · 3V           1 - 0µF         35V         .10µF         25V         100µF         3V
TRANSISTORS           AC107         ISp         AF124         22p         BD131         75p         OC26         45p         2N3702         13p           AC107         I2p         AF125         10p         BD132         75p         OC26         45p         2N3702         13p           AC126         12p         AF125         10p         BD132         75p         OC26         45p         2N3702         13p           AC137         13p         AF125         10p         BD133         75p         OC26         45p         2N3703         12p           AC131         13p         AF127         10p         BF115         25p         OC42         12p         2N3706         12p           AC131         13p         AF178         13p         BF173         12p         OC44         12p         N3706         12p           AC132         13p         AF180         40p         BF178         13p         OC70         12p         2N3708         12p           AC187         13p         AF180         40p         BF179         13p         OC71         12p         2N3709         11p           AC187         13p         AF180         <	VEROBOARD         0.1         0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	LARGE (CAN)         ELECTROLYTICS           1600µF         64V         74p         3200µF         16V         50p           2500µF         40V         74p         4500µF         16V         50p           2500µF         50V         58p         4500µF         25V         61-48           2500µF         64V         80p         5000µF         50V         61-10           2800µF         100V         42-60         5000µF         50V         61-10
DIODES RECTIFIER         SIGNAL           BY127         1250V         IA         12p         OA85         7p           BZY10         800V         6A         25p         OA90         5p           BZY13         200V         6A         25p         OA91         5p           IN4001         50V         IA         7p         OA202         7p           IN4004         400V         IA         8p         IN4148         5p           IN4007         1000V         IA         12p         BA114         8p	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
BRUSHED ALUMINIUM PANELS 12in x 6in = 25p; 12in x 2jin - 10p; 9in x 2in - 7p.         THERMISTORS VAI055S         ISp VAI055S         ISp VAI060S           SLIDER POTENTIOMETERS 86mm x 9mm x 16mm, length of track 59mm. SINGLE 10K, 25K, 100K 10g, or lin. 40p.         THYRISTORS VAI050S         THYRISTORS VAI050S         ISp VAI05S         ISp VAI05S           DUAL GANG, 10K + 10K etc. log. or lin. 60p.         ZNS060 50V 0.8A 30p, 2NS064 200V         THYRISTORS VAI05S         THYRISTORS VAI05S           Bidar pots. Gray or matt black finish complete with fixings for 4 pots.         The complete with fixings for 4 pots.         The complete with fixings for 4 pots.         The complete with fixings for 4 pots.	SMOKE AND COMBUSTIBLE GAS DETECTOR-GDI (2:00) The GDI is the World's first semiconductor that can convert a concentration of gas or smoke into an electrical signal. The sensor decreases its electrical resistance when it absorb deoxidizing or combustible gases such as hydrogen, carbon monoxide, methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or smoke. This decrease is usually large enough to be utilized without amplification. Detector GDI, £2. Kit of parts for detectors including GDI and P.C. board but excluding case, Mains operated detector 5:20. 12 or 24V battery operated audible alarm £7:30. As above for PP9 battery, £6:40. <b>PRINTED BOARD MARKER</b> . Draw the planned circuit onto a copper laminate board with the P.C. Pen, allow to dry, and immerse the board in the etchant. On removal the circuit remains in high relief.







"In published circuits a volume control is sometimes connected as in Fig. 1a, with the input to the slider, and sometimes as in Fig. 1b, with the output from the slider. Which method of connection is correct?"

The short answer is: when the output from the volume control is connected to a low impedance load, use Fig. 1a. For high impedance load, use Fig. 1b.

The essential point is that a volume control doesn't exist in isolation. The way it works in a practical circuit depends on what comes before it and what goes after it. Disregard this simple fact and you may end up with a control which has no effect as it is turned until the slider is very nearly at the end of the track, whereupon the volume suddenly changes from minimum to maximum. What's known to the trade as a "fierce" control.

#### ENDS AND MEANS

The circuit of Fig. 2a is a case in point. With the slider at the start (s) of the track, the signal (here 1 volt from a source of 100 ohms) is shorted, so the output is zero—the output in this case being the voltage which appears across the 1 megohm load resistance. With the slider at the finish (f) of the track, the signal source is connected to the total resistance of the track (100 kilohms) in parallel with the load (1 < megohm), i.e. about 90 kilohms.

When current flows, only a small amount of the 1 volt signal is lost in the signal-source's own internal impedance of 100 ohms (it might be a 100 ohm micro-

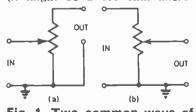


Fig. 1. Two common ways of connecting a volume control.

phone, for instance) and practically the whole 1 volt appears across the load  $R_{\rm L}$ . In a word, volume is maximum.

So the volume is zero with the slider at s and maximum with the slider at f. This is alright if you only want to operate your equipment at maximum volume, but not for intermediate settings.

#### CALCULATE

First, calculate, or at any rate get a rough idea of the current through the load when the slider is at f. As we saw, the voltage across the load is almost 1 volt, so 1 micramp flows. Now move the slider back to the bottom (s) of the track and then adjust it so that there's just 1 kilohm between slider and earth. What current flows?

Well. obviously the current from the source divides at the slider, part flowing up and through the load and part down to earth. But since there's nearly 1100 kilohm in the upper path (1 megohm plus 100 kilohm) and only 1K in the lower, we can safely say that the lower path has the controlling effect and forget about the upper.

For practical purposes, the signal "sees" a load of its own 100 ohms plus the 1 kilohm between slider and earth: in other words, the total resistance is 1100 ohms, which with 1 volt gives a current of 0.9 milliamps

(using ohm's law I = V/R). This 0.9 milliamps flows through the 1 kilohm, setting up a voltage drop of 0.9 volt between slider and earth.

#### LOAD VOLTAGE

Now we come to the important point of the voltage across the load. The 0.9 volt at the slider drives a small current up through the track and then on through the 1 megohim load and back to earth. The resistance in this loop is 1.1 megohm, near enough, so the current is 0.9/1100000 = 0.8microamps approx. Now, 0.8 microamp in 1 megohm produces a voltage of 0.8 volt, so, with the slider at the 1 kilohm point, the output is 0.8 volt. This, you'll note, is only 20 per cent less than the maximum output of 1 volt, and in terms of audibility is just perceptible.

So in moving the slider up to the 1 kilohm position we've changed the volume from zero to just below maximum. With a logarithmic law 100 kilohm volume control the 1 kilohm change calls for a rotation of about 10 per cent. The other 90 per cent produces hardly any further increase in volume.

The correct arrangement is as in Fig. 2b. But it's not universally correct. If you have a high impedance signal source Fig. 2c feeding a low impedance load, then this will now give a fierce control and the correct arrangement is as shown in Fig. 2d. These second two circuits are a complete reversal, in terms of fierceness or gentleness, of the first two, even though the volume control is 100 kilohm in every case.

A final tip. If, as sometimes happens, you are stuck with a particular value of volume control, then the best compromise is to use whichever of the two connections produces the least variation in the input signal current drawn as the control is turned from minimum to maximum volume.

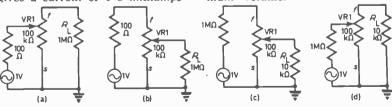


Fig. 2. Fierce (a and c) and gentle (b and d) volume controls.



#### Simplified

Would it be possible to give me a brief description of the Demo Deck as I unfortunately missed that particular issue. I am now taking EE regularly, and I find it more suitable at my age (I am 75 yrs old), having started back in the old cat whisker days. I find the other publications a bit too complicated but interesting. what with all this hifi etc., which is a vast improvement on the old methods of valves and corner wall baffles etc. The explanations in EE are also much plainer, this must suit the younger people

also, making it easier to grasp. The gadgets for the home are a great attraction for experimenting with, and your simple circuits require less time to make. Hoping you will carry on providing even more simplified versions.

> E. Skidmore Birmingham.

The Demo Deck will no longer feature in our pages. It has been used since December '71 and can still be used by readers for experimenting. The new beginners series Teach-In '74 will not be based on the Demo Deck.

## **Radio Amateurs**

I write to ask that a brief item be inserted in EVERYDAY ELEC-TRONICS re. the amateur radio course run by the Northumberland County Education Dept., at Gosforth, very near to Newcastle upon Tyne.

The course to prepare students for the R.A.E. (Radio Amateurs Examination) in May/June 1974 will be run at the Grammar School, Gosforth, Northumberland, commencing in September 1973.

Held on Tuesday/Wednesday of each week from 7 pm to 9 pm. candidates may sit the R.A.E. at the School.

Enquiries should be addressed to the Principle, Gosforth Grammar School, Northumberland, who will forward a prospectus. Or further information can be had by telephoning Gosforth 851000.

I take the class and your cooperation in this matter would be appreciated.

> D. R. Loveday. Newcastle upon Tyne.



I find etching p.c. (printed circuit) boards takes a long time, to speed up the process all that is needed are two match sticks. Make up the etchant in the usual way, but before putting the p.c. board in the etchant dish, put the two match sticks in, parallel but some distance apart. The board rests on the match sticks keeping it away from the bottom of the dish.

The dish can now and again be rocked gently to and fro, all the dissolved particles of copper fall to the bottom of the dish and fresh etchent can start to dissolve the rest of the copper away.

> J. Majchrowski, Ayr.

Having made numerous projects I always find that the front panel or fascia presents a problem with respect to labelling. Engraving and "silk screen printing" being very expensive for the home builder and Dymo labels not giving a suitable appearance. I think the method I have adopted might be of interest to many other readers. The process is as follows:

- 1. Drill all holes and slots in the required positions.
- 2. Spray the panel the desired colour using an aerosol spray.
- 3. Add the lettering using Letraset or Magic Letters, these need no more than placing on the panel and rubbing with a ball point pen to transfer each letter to the panel. A sheet of graph paper suitably placed and tacked in position lightly with sellotape, helps in keeping letters in alignment.
- 4. When satisfied that all is correct, a sheet of clear self adhesive film (available at W. H. Smiths) is rolled onto the panel starting at one end and making sure no air bubbles are left. If, accidentally an air pocket is made do not attempt to pull the film off but carefully pierce the bubble with a pin and roll again from the edges of the bubble towards the pin hole. The edges of the film should be left large enough so that they can be turned over and stuck to the reverse side of the panel so that with use the edges will not curl.

The finished panel viewed from a foot or so cannot easily be distinguished from a panel which has been silk screen printed. The surface is easily cleaned with a damp cloth and gives projects the professional finish.

A. Evans, Portsmouth. MAIL ORDERS: Some items have a postage and haridling charge shown against them. Where p. & p. is not shown the charge is 13p for any selection. When both classes of goods are ordered the charge is 13p plus any p. & p. charges shown. (Overseas extra). Telephone 01-692 4412.



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October issue on sale September 14, 1973



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Everyday Electronics, September 1973

# Sinclair Project 60

# New performance standards ....new safety margins

Such are the results of using a PZ8 Mk.3 to drive two Z.50 Mk.2 power amplifiers. Developed from the original Z 50, the Mk 2 has improved thermal stability, better regulated D.C. limiting to ensure more symmetrical output voltage swing with still less distortion at lower outputs and automatic transient overload protection. The PZ.8 Mk.3 is the most advanced power supply unit ever to be made at a reasonable price. It cannot be damaged by direct shorting, nor will it fail through overloading, because of an ingenious re-entrant current limiting principle used usually only in expensive laboratory equipment. Because output voltage is variable, the PZ8 Mk.3 makes a worthwhile alternative where PZ 5 and PZ.6 are recommended for Project 60 applications, particularly since this most powerful of all Sinclair supply units can be operated from a smaller mains transformer. Together, the Z 50 Mk 2 and PZ8 Mk 3 provide new standards of performance and reliability and these modules are compatible with earlier types in the Project 60 arage.

Z.50 Mk.2 SPECIFICATIONS

Input impedance 100 KΩ Input (for 30w into 8Ω) 400mV Signal to noise ratio, referred to full o/p at 30v HT 80dB or better Distortion 0.02% up to 20W at 8Ω. See published curve Frequency response 10Hz to more than 200 KHz i 1dB Max. supply voltage 45v (4Ω to 8Ω speakers) (50v 15Ω speakers only)

Other power supplies

In addition to the remarkable Sinclair PZ.8 Mk.III as described, there are two other power units available, which should be chosen according to their types in order to buy to best advantage. All are for operation from A.C. mains 240V.

PZ.5 30 volt, unsta	abilised £4.9	86
	+ VAT 4	9p
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IC.12).	£7.5	
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#### Guarantee

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Sinclair Radionics Ltd Each Project 60 module is tested before leaving our factory and guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you. A small charge may be made in those cases where damage arises through miss-use. No charge is made for postage by surface mail. Air Mail charged at cost.



Min. supply voltage 9v Load impedance – minimum; 4Ω at 45v HT Load impedance – maximum: safe on open circuit £5.48 <sup>- V,A T</sup> 54p PZ.8 Mk.3 SPECIFICATIONS

PZ.8 Mk.3 SPECIFICATIONS Nominal working output 45V. Adjustable between 20 & 50V £7.98 <sup>+</sup> VAT. 79p Mains Transformer £5.98 + VAT. 59p



Mk 2



# Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.50	Crystal P.U., 12V battery volume control, etc.	£5.48 + VAT 54p
Mains powered record player	Z.50, PZ.5	Crystal or ceramic P.U. volume control, etc.	£10.46 + V.A.T.£1.04
12W. RMS continuous sine wave stereo amp. for average needs	2 x Z.50, Stereo 60; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£25.92 VAT £2.59
25W. RMS continuous sine wave stereo amp using low efficiency (high performance) speakers	2 x Z.50, Stereo 60 ; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£28.92 + VAT £289
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W, RMS into 8 ohms)	2 x Z.50 Mk.2, Stereo 60 ; PZ.8 Mk.3 transformer	As above	£34.90 + VAT £3.49
Indoor P.A.	Z.50 Mk.2, PZ.8 Mk.3 transformer	Mic., guitar, speakers, etc., controls	<b>£19.44</b> + V.A.T. £1.94

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## Stereo 60 pre-amp/control unit

Designed specifically for Project 60 systems, the Stereo 60 is equally suitable with any high quality power amplifier. Silicon epitaxial planar transistors used throughout ensure high signal to-noise ratio and excellent tracking between channels. Input selection is by press buttons, with accurate equalisation on all input channels. The unit is easy to mount.

SPECIFICATIONS—Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A. curve = 1dB: 20 to 25,000Hz. Ceramic p.u. – up to 3mV: Aux – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE + 12 to —12dB at 10KHz: BASS + 12 to —12dB at 100Hz. Front panel; brushed aluminium with black knobs and controls: Size: 6-40+-20-20-20-66 × 40 × 207mm. + V.A.T. £9.98

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For use between Stereo 60 and two 2.30's or 2.50's in stereo formation. Cut off frequencies are continuously variable, with 12dB/octave cut in the rejection band. Two stages of filtering – rumble (high pass) and scratch. (low pass). Amplitude and phase distortion are negligible, supply voltage needed – 15–35V. H.F. cut-off (1–3dB) 28KHz to 5KHz, L.F. (–3dB) 25Hz to 100Hz. For Project 60 or any good stereo system. Built pertent and represented Built, tested and guaranteed



99p

# Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-fi constructors with the IC.10, which was the first time an IC had ever been made available for such purposes, we followed it with an even more efficient version, the Super IC.12. This needs very few external resistors and capacitors to make an exceedingly efficient high fidelity amplifier for pick-up, F.M. radio or small P.A. amplifier for pickup, risk ratio of similar risk, set up etc. The free 40 page manual supplied details many other applications which this remarkable IC make possible, The Super IC.12 is the equivalent of a 22 transistor circuit

contained within a 16 lead DIL package, and the finned heat sink is sufficient for all likely require-ments. The Super IC.12 is also compatible with those Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board

#### SPECIFICATIONS

Output power: 6 watts RMS continuous (12 valts peaks into 6-8 O. Frequency Response: 5Hz to 100KHz ⇒1dB. Total Harmonic Distortion: Less than 1%. (Typical 0.1%) at all output powers and frequencies in the audio band (28V). Load Impedance: 3 to 15 ohms. Input Impedance: 250. Kohms norminal. Power Gain: 90dB (1.000.000,000 times) after feedback. Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V Size: 22 45 × 28mm cluding pins and heat sink

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Everyday Electronics, September 1973

# **Project 605**



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 50V: (p): 22, 27, 33, 94, 75, 66, 80, 20, 100, 120, 150, 180, 220, 270, 130, 390, 470, 580, 680, 820, 101, 120, 150, 180, 220, 270, 130, 390, 470, 350, 461, 40; 10, 01, 150, 001/2, 150, 1100, 150, 0022, 003, 0047, 24p; 0.1, 130V, 41p; 0.1, 100V, 51p.

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Veroboard         0.1         0.15           2½ x Sin         28p         28p           2½ x 3½in         26p         19p           3½ x 5in         32p         33p           3½ x 3½in         28p         28p           2½ x 3½in         28p         28p           3½ x 3½in         28p         28p           3½ x 3½in         7p         7p	IN4001 IN4002 IN4003 IN4004 IN914 #L914	6 p 7 p 9 p 9 p 7 p 35 p	SPECI A R E QUOT	AL B	TY DIS ULK BU AILA DN FO AND	JY PR BLE R LA	B Y RGE
21/2 x 1in     /p     /p     /p       21/2 x 5in (plain)     -     14p       21/2 x 32in (plain)     -     12p       5 x 32in (plain)     -     22p       Insertion tool     59p     59p	OC71 OC75 OC83	13p 17p 20p	50V 100V 400V			3A 3A 3A	33p 40p 60p
Track cutter 44p 44p Pins, pkt, 25 10p 10p	Screened Twin scr	eeneo	d wire,	m			. 10p
2 pin DIN Plug, 12p; Skt., 10p. 3 pin DIN Plug, 13p; Skt., 10p. 5 pin DIN Plug, 180°, 15p; Skt., 12p, Tran-	Stereo s Connect Neon bu Preset s	ing W Ib 90	Vire. all V wire	ende	d	.5 for	21p 24p
sistor Equiv. Book, 40p. Carbon pots 5K-2M log. & Iln. single 1612p, single with switch 26p, dual 46p.	C.W.O. d	count	. & P. : (10-	100 0	. 620-	s below 15%.	
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BN7422         0         20         18         0         16         BN7486         0           BN7422         0         48         0         44         0         877470         0           BN7423         0         48         0         44         0         877470         0           BN7423         0         48         0         40         877470         0           BN7423         0         48         0         40         877470         0           BN7427         0         42         0.39         0.35         BN7492         0           BN7427         0         42         0.39         0.35         BN7493         0           BN7428         0.50         0.46         0.40         8         87494         0           BN7428         0.50         0.48         0.38         BN7495         0         8           BN7433         0.70         0.18         0.16         BN7496         1           BN7433         0.70         0.65         0.60         0.50         BN74106         1           BN7433         0.65         0.60         0.50         BN74106         2         BN743	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	04202 10p 1000 + 8p 04202 10p 100 + 7p 100 + 7p 1000 + 5p 0005 + 5p 0005 Mullard 50p 25 + 45p	$\begin{array}{c} 25 + 32p\\ 100 + 28p\\ 500 + 25p\\ 1000 + 22p\\ \hline 1000 + 22p\\ 25 + 18p\\ 100 + 15p\\ 500 + 12p\\ 1000 + 10p\\ \hline 2N3055  55p\\ 25 + 50p\\ 100 + 45p\\ \hline \end{array}$	BC50A         100         £1-25           BC50B         200         §1-35           BC50B         500         \$1-85           BC50B         500         \$1-85           DIAC D32         25p         TRIACS-           Additional Types         40430         (T065)         85p           40669         (Plastic)         £1-00         40486         (T05)         80p           NEW BRIDGE         RECTIFIERS         \$100         \$100         \$100         \$100         \$100	15 Am T048
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A SELECTION OF SEMI-CO           AAY30         10p         BC147         12p           BC147         12p         BU105         2-25           AAY32         16p         BC169C         12p         BV100         125           AC13         10p         BC121         10p         BV102         15p           AC124         16p         BC127         75p         BV213         35p           AC124         26p         BCY32         75p         BV213         35p           AC127         25p         BCY34         85p         C106D         65p           AC127         25p         BCY42         30p         GET111         55p           AC176         25p         BCY42         30p         GET111         55p           AC187         25p         BCY42         30p         GET111         55p           AC187         25p         BCY43         35p         GET3140         50p           AC187         25p         BCY43         35p         GET3140         50p           AC187         30p         BCY17         15p         MAT1212         55p           AC180         50p         BCY17         15p	DNDUCTORS         FROM         STOCK           0C44         16p         T1843         35p         2X3055         55p           0C45         16p         T1843         35p         2X3045         75p           0C45         16p         T1843         35p         2X3440         75p           0C57         26p         ZTX300         12p         2X3624         75p           0C73         25p         ZTX301         12p         2X3624         75p           0C73         25p         ZTX301         12p         2X3614         5p           0C77         45p         ZTX301         12p         2X3614         5p           0C31         25p         ZTX301         12p         2X3614         5p           0C38         25p         ZTX301         12p         2X3704         10p           0C43         25p         ZTX401         12p         2X3704         10p           0C140         65p         ZTX500         15p         2X3704         10p         10c           0C170         25p         2X4027         35p         2X3773         200         117         2X3705         22x300         2X3773         200	10p each. 25+ 9p 100+ 8p 600+ 650 1000+ 5p Any one type. 1} Watt 5% Wire Ends Metal Case All voltages 6:8 - 100 Volts 20p each 25+ 18p 1000+ 10p Any one type. 3 Watt Plastle Wire Ends 5% 8EZ Range	741C         T0095         557           741C         D.I.L.         659           747C         T0095         81-16           747C         D.I.L.         617           81NCLAIR         607         618           708HIBA         T0013P         20           20         WATT AMP         61-86           DATA AND         61-96         105           CIRCUITS REP.         42 105           PREE WITH         PURCHA8E8           TRANSISTORS,         IC's. TRIACS,	₩005         50         80p           ₩01         100         85p           ₩02         200         40p           ₩06         600         45p           ₩07         200         40p           ₩06         600         45p           ₩07         50         85p           ₩07         100         40p           №03         100         40p           ₩2/100         100         60p           ₩2/100         1000         60p           ₩2/100         1000         60p           ₩2/100         100         70p           ₩4/400         800         \$1.00           \$24/800         800         \$1.00           \$24/800         200         75p           \$24/800         200         75p           \$24/800         200         75p           \$24/800         200         75p           \$26/200         200         75p      >>	
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	TAA263 75p         2N1306 25p         2N5777 55p           TL209 35p         2N1301 200         2N001 1.00           TLP204 50p         2N1671 1.00         28012 10-00           TLP304 60p         2N1671 7.5p         28018 6.25           TLP31A 60p         2N2167 75p         28018 6.25           TLP31A 60p         2N217 25p         28301 65p           TLP34A 70p         2N2217 25p         28303 66p           1.00         2N2224 20p         28303 66p           1.00         2N2224 20p         28303 66p           1.80         2N2224 20p         28303 66p           1.80         2N2224 20p         28303 66p           1.80         2N2234A         40360 40p           2.850         20p 40362 50p         1.648 50p           2.80         2N2906 20p         40362 50p           3.00         cols) 10p         40486 75p           3.00         cols) 10p         40486 75p           11P41A 75p         2N354 50p         40430 1.00	All voltages 68-100 Volta 30p each. SILICON EECTIFIERS WIRE ENDED PLASTIC Type P.L.V.1-11 1 amp miniature IN4001 50 6 IN4402 100 7 IN4003 200 8 IN44004 400 8 IN44004 600 18	BRIDGES, SCR's, LDR's	SILICON CONTROLLED RECTIFIERS Type Volta Price P.I.V. 1.11 OFE AMP P.I.V. 1.11 OFE AMP P.I.V. 1.11 OFE AMP P.I.V. 1.11 OFE AMP 200 80p CR8 1/40 100 80p CR8 1/40 400 45p CR8 3/40 100 80p CR8 3/40 400 45p CR8 3/40 400 45p CR8 3/40 400 45p CR8 3/40 400 45p	1 Ami To5
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 20,000
 0.9. V.
 Overload
 protection, Bilde awitch selector

 0/25 / 25 / 10 / 50 / 250 /
 1000 V.
 1000 V.
 100 / 250 / 250 /

 1000 V.
 1.0. 0 / 10 / 50 / 250 /
 1000 V.
 25 / 20 / 250 /

 1000 V.
 1.0. 0 / 0 / 250 /
 250 mA.
 D.C.
 0 / 3K / 30K /

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 25 / 1 / 25 / 1 / 20

 25 / 10
 J60 / 250 / 1000 / 5000Y.
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USED EXTENSIVELY BY INDUSTRY, GOVT. DEPTS., EDUCATIONAL AUTHORITIES, ETC. Over 200 ranges in stock-other ranges to order. Quantity discounts available. Send for fully illustrated brochure. Type SW.100 100 x 80 mm. Type MR.85P. 4 Jin. x 4 Jin. fronts Type MR.38P, 1 21/32in, square fronts ... \$4-15 50mA .... \$8-90 100mA .... \$8-90 200mA .... 48-25 300mA .... 52-25 V 41.05 شعر و 500mA .... 500mA .... 750mA .... 1 amp..... 2 amp..... £1 25 £1 25 £1 25 £1 25 500mA 43-95 43-90 43-70 43-80 43-80 43-60 43-60 43-60 .... 43-90 -4 43-90 43-90 43-90 43-90 43-90 43-90 ∎,A 1 6/00 1 amp..... 5 amp..... 15 amp..... 30 amp .... 20V. D.C. 50V. D.C. 150V. D.C. 150V. D.C. 150V. D.C. Y 212. R 21 ar.;= \$2-25 \$2.95 5 amp..... 5 amp, ... 10 amp, ... 3V, D.C. 10V, D.C. 15V, D.C. 20V, D.C. 50V, D.C. 100V, D.C. 160V, D.C. 5 amp. D.C 23. 29-95 300V. A.C. VU Meter 43-70 \$3.90 \$3.90 \$3.90 \$3.96 \$3.95 \$3.95 \$3.90 49-85 84-34 50µА ..... £4-40 50-0-50µА £4-85 100µА .... 54-85 100-0-190µА £4-05 200µА .... \$4-05 50µA ..... 82:55 50-0-50µA 82:60 100µA .... 82:45 100-0-100µA 83:40 £3-55 52-25 . . 
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 0 Amp. A.C.\*
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 20 amp. A.C.\*
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 30 amp. A.C.\*
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 30 amp. A.C.\*
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 100μ Α .... 100-0-190μΑ 200μΑ .... 500μΑ .... 500μΑ .... . . \$2-25 Type SD.830 82.5mm x 110mm Fronts \$2-25 \$2-25 10m A 50m A £3-10 £3-10 2004A 42-25 500μA 500-0-500μA \$3-90 49.95 41.95 £3-26 £2-25 £2-25 £2-25 £2-25 £2-25 £3-25 00mA .... 100mA .... 500mA .... 1 amp..... \$3-10 \$3-10 800V. D.C. 800V. D.C. 800V. D.C. 780V. D.C. 13 10 13 55 13 55 12 55 12 55 12 30 41-90 lmA ..... 1-0-1mA ... 43-90 41-90 lmA ...... 1-0-1mA ... \$3.10 \$3.10 5mA ..... \$3.90 10mA .... \$3.90 780V. D.C. 15V. A.C. 50V. A.C. 150V. A.C. 300V. A.C. 500V. A.C. 8 Meter 1m VU Meter 5 amp..... 2m A 5mA 10 amp. 5V. D.C. 88-10 42-30 £3-40 41.10 L0m A 42-25 42-20 

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 43-16 43-10 43-10 43-10 20mA 50mA 100mA 150mA 42-25 42-25 42-25 42-25 42-25 49.30 Type MR.52P. 24in. square fronts £3.40 £3.25 £3.25 £3.25 £3.20 £3.15 £3.10 £3.10 41.30 
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 \$2:80

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 \$2:75

 100-0-100μA
 \$2:75

 200μA
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 500μA
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 5mA
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 10 amp. 5V. D.C. 10V. D.C. 20V. D.C. 50V. D.C. Type MR.65. 34in. square fronts 12-60 10mA 12 60 12 60 12 60 1 amp...... 48-60 δ amp...... 42-60 15 amp...... 42-60 50m A 42-60 100mA .... 500mA .... 1 amp..... δ amp..... 53-50 52-50 52-60 52-60 52-60 52-60 52-60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 12:60 15 amp. .... 30 amp. .... 50 amp. .... 20 x D.C. 10 V. D.C. 20 V. D.C. 50 V. A.C. \*. 50 V. A.C. \* 42-60 300V. D.C. \$2-60 10 amp. 15V. A.C. 22.70 41-60 \$2-60 15 amp. 300V. A.C. . . \$2.70 \$2.60 20 amp. .... 42-60 42-60 VU Meter .. \$2.90 30 amp. 50 amp. 5V. D.C. £1-50 £1-60 £1-60 55µА .... 80µ.А .... 80-0-50µА \$4-60 \$3-55 "SEW" EDUCATIONAL 48-06 100μA 100-0-100μA 48-00 42-65 METERS 50V. A.C. • 150V. A.C. • 300V. A.C. • 500mA A.C. • 1 amp. A.C. 5 amp. A.C. Type ED.107. Size overall 100mm x 70mm x 108mm 100mm x 70mm x 100mm x 100mm x 70mm x 100mm x 100mm x 70mm x 100mm 48-00 41-64 ۱. 11-65 11-65 11-65 11-60 11-60 500uA 41.70 500-0-500µA £2-70 £2-50 £2-60 1mA ..... 1-0-1mA ... 5mA ..... 10mA .... 22-60 0 amp, A.C. \* 22:60 10 amp, A.C. \* 23:60 20 amp, A.C. \* 23:60 30 amp, A.C. \* 23:60 50 amp, A.C. \* 23:60 VU Meter ... \$3:65 12 60 12-30 12-60 12-60 "SEW" EDGWISE METERS 50mA 100mA 100mA .... \$2.60 500mA .... \$2.60 Type PE.70. 3 17/32in. x | 15/32in. x 21in. deep \$3.15 500µA .... \$3.20 \$3.60 1mA ..... \$3.20 Type S-80 80 mm. square fronts 
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 50μΑ ..... \$3-50 50-0-50μΑ \$3-40 100μΑ .... \$8-40 50µA ..... \$6-90 100µA .... \$6-90 1mA .... \$6-40 1mA .... \$5-96 50-0-50µA \$0-40 1-0-1mA \$5-96 1A d.c. \$5-96 20V. d.c. .. \$5.96 50V. d.c. .. \$5.96 300V. d.c. .. \$5.95 100-0-100µA \$8-80 ad. 100-0-100μ 500μA .... 20V. D.C. 50V. D.C. 300V. D.C. 1 amp. D.C. \$3.00 \$2.00 \$2.00 \$3.00 \$3.00 \$3.00 \$3.00 **\*MOVING IRON---**Dual range 500mA/5A d.c \$7:00 5V/50V d.c. \$7:00 1A d.c. .... 5A d.c. .... ALL OTHERS MOVING COIL 15 96 15 96 SOOV. A.C. VU Meter #3-00 £3-70 Please add postage 10V de HAND HELD 2-WAY WALKIE 240° Wide Angle SEND SAE FOR NEW 8 PAGE LIST ImA Meters SEMI CONDUCTORS & VALVES ۵ Battery operation. Volume and squelch controls. Call button and press to talk button. Telescopic aerial. Complete carrying MW 1-6 60mm square \$3-97 \$4-97 1-8 80mm square P. & P. extra **ALL PRICES ARE** SUBJECT TO 10% VAT 100mW £24.95 Pair. Post 50p. 230 VOLT A.C. **SO CYCLES** 2 channel £52.50 Pair. 300mW £52.50 Post 50p. RELAYS Brand new. 5 sets of channel £71.25 Pair. Post 50p. changeover contacts at 5 amp rating. 50p each. P. & P. 10p (100 lots \$40) Quantities available. 2 watt Licence required for operation in U.K. FOLLOWING

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Everyday Electronics, September 1973

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CS35 STEREO CASSETTE RECORDER	RECORD DECK PACKAGES	Ideal for	6 TRAN- SISTUR
For conventional or Chronium Dioxide tape. 4 track record/playback. Volume and		office, stores,	ULC HIGH
tone controls. Frequency response 40- 16kHz (using CrO2 tape),		factories, etc. com-	TUNER.
distortion better than 2%, wow and futter better than 0.2% RMS.	S Card An	plete with batteries, cable and instructions.	ONLY
Complete with pair of matching		2 Station £2.97, P. & P. 15p. 3 Station £5.25, P. & P. 15p.	6 × 4 × 2jin. 3 I.F. stages. Double tuned discriminator. Ample
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Rec. Price 268:30         E44:45         50p           GWS PRICE (P. & P. 50p)         MICROPHONES (P. & P. 50p)           CASSETTE (P. & P. 50p)         MICROPHONES (P. & P. 50p)	Complete units with Stereo cart- ridge ready wired in plinth cover.	Outstanding value. Soft	Price 12p Stereo multiplex adaptors £4-97.
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GXC40T Deck/Receiver GXC45 Deck	2025 TC/9TAHCD £10-65 8P25 111/G800 £15-95 8P25 111/M44E £16-45	headband, 8.16 *hms. 20.20,000	SPECIAL PURCHASE!
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TAPE/CASSETTE         (P. & P. 75p)         A8E11         £4.75           A8E20         £7.30	GL75/G800E £39-15	TEIOIS DE-LUXE MONO HIGH	
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