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## 1

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10 TRANSISTORS. 9 TUNABLE WAVEBANDS, MW1, MW2, LW, SW1, SW2, SW3, TRAWLER BAND. VHF AND LOCAL STATIONS ALSO AIRCRAFT BAND Bult in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated 7 section Teleacopl Aerial, can be angled and rotated for peak short wave and VHF listening. Push Pull output Dioden. Fine tone moring coll apeaker. Gatiged Tuning Condenser with Yif aection. Separate coil for Alrcraft Band. Volurne on/onl. Ware Cliange and tone Control Attractlye Ceat in black with allver blocking. Bize $9^{\prime \prime} \times 7^{\prime \prime} \times 4^{\prime \prime}$. Eany to follow tnetructions and diagrams. Parta price list and plans 30 p (FREE with parts).

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7 Tunable Wavebanda: MWI, MW2, LW, sWl, 8W'2 8W3 and Trawler Band. Bullit in Ferrlte Mod Aerle for MW and LW. Retractable chrome plated Tele. acoplo aerial for Short Waren. Pubh pull ontput uaing 600 m W tranimintors. Car aerial and Tape record sockete. Belectrity switch. 8 tranoiators plus 3 doden. Fine tone moving coll speaker. Alr apaced ganged tuning con-
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7 stages- 5 traneintore and 2 dlodes,
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Turable Ware bands: MW, LW BW1, 8W2, 8W3 Trawler, band plue on exira Medlum easler tunlag tc. Sensitive fero rlte rod aerlal and telescopic merial for Short Wavea.
3 in. Epeaker.
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TRANSONA FIVE

5 TRANSISTORS AND 2 DIODES


Tunable Warebands: MW, LW and Trawler Band 7 stage-5 transistorn and 2 diodes, ferrito rod aerial. tuning condenser volume control, ane tone grille. Bize $61 \times$ it $\times 1$ if. Plane and parti price list $15 p$ (FREE with perta).

 bends: MW, LW, and Truwler Band.
gensitive ferrite roi aerial for M.W. and L.W. Telescopic serial for Short Waves. 3 in . Speaker. 8 Improfed type transletors plus 3 dioden. Atractive case in black with red grilie, dislend blark knobs with pollahed metal inserts, size $9 \times 8: \times 2 i \mathrm{in}$. approx. Puab pull
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## THE HY41



The HY41 supersedes the populan HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distontion liypically $0.05 \%$ at 1 KHz into 8 ohms!) and is electronically and mechanically comoatible with the HY40.

With this important improvement the HY4 $1^{1}$ ' retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sulficiently versatile to provide power not merely for Hi.Fi bat atso for public address systems and industry

The free manual gives a full circuit diagram of the HY41 and its varlous applications including a complete stereo ampliffer.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent vears.
OUTPUT POWER: British Rating so WATTS PEAK, 20 wats
R.M.S. continuous.

LOAD IMPEDANCE: 4-16 ohms.
INPUT IMPEDANCE: 30 K ohms at 1 KHz .
VOLTAGE GAIN: 30 db at 1 KHz
TDTAL HARMONIC DISTORTION: tess than $0.15 \%$ (iypical $0.05 \%$ ) at 1 KHz
FREQUENCY RESPONSE: $5 \mathrm{~Hz}-50 \mathrm{KHz} \& 1 \mathrm{db}$
SUPPLY VOLTAGE: +22.5 volts D.C.
SUPPLY CURRENT: 0.8 amps maximum.
PliICE: inc. comprehensive manual, P.C. board, five extra companents and P. \& P.:MONO: $£ 4.90$

STEREO: $£ 9.80$

## UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an Integrated preamolifier circuit.

Supplied with the HY5 are two stabilizing capactions and by the addition of volume, treble and bass potentiometers it is ready for use

Internally the HY5 provides equalization for almost every conceivable input, the desired function is achieved by use of a multi-way switch or by direct interconnection.

Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing if to be run off any unregulated power supply from 16-25 Volis and a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo preamplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

## INPUTS

Magnetic Pick-up (within $\ddagger 1 \mathrm{db}$ RIAA curve) $2 \mathrm{mV} .47 \mathrm{~K} \Omega$
Tape Replay lexternal components to suit head). $4 \mathrm{mV} .47 \mathrm{~K} \Omega$
Microphone (flat) $10 \mathrm{mV} .47 \mathrm{~K} \Omega$
Ceramic Pick-up (equalized and compen
satable) $20-2000 \mathrm{mV}$. variable.
Tuner (flat) 250 mV . $100 \mathrm{~K} \Omega$ Auxiliary $1250 \mathrm{mV} .47 \mathrm{~K} \Omega$
Auxiliary $22-20 \mathrm{mV}$. $100 \mathrm{~K} \Omega$

OUTPUTS
Main Pre-amp output 500 mV Direct tape output 120 mV .
ACTIVE TIDNE CONTROLS (Bexendall)
Treble $\pm 12 \mathrm{db}$
Bass + ${ }^{12 d \mathrm{do}}$.
INTERNAL STABILIZATION
Enables the HY5 to share an unregulated
supply with the Power Amplifier.
SUPPLY VOLTAGE
16-25 volts
PRICE
MONO: £3.60
STEREO: $£ 7.20$

## POWER SUPPLY PSU45

The versatile P.S.U. 45 is designed to supply your HY41's 4 HY5's in stereo or mono format.

Specification
Input: 200-240 Volts.
Output: $\pm 22.5$ Volis at 2 amps.
Overall Dimensions: L. $7^{\prime \prime}$; D. $3.8^{\circ \prime} ;$ H. $3.1^{\circ}$
PRICE: £4.50 inc. P. \& P

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## MAINS OPERATED CONTACTOR 220/240v. 50 cyela solenold with laminated cort co very alrouthe each rated at 10 ampe Ercuita each reled at 10 ampe. German Electrical Compans Orerall aize $21 \times 2 \times 2 \mathrm{in}$ 11 -8 esch. <br> NEED A SPECIAL SWITCH Double Las! Contact. Very elight prearure clowes等 both contacte. $8 p$ each 10 for 60 . Platic puhhrod cultabla for operating. ip esch. 10 for $64 p$.

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## AERIAL

with dabbboard control switch-fully ertendable to 40 in or fully retractable. Buitable for 12 V poaltive or negative earth. Bupplied complete with fitting instructions and ready 25 p pont and insurance.
MAINS TRANSISTOR POWER Dealoned to pACK


Dealgned to operste transistor weta and amplifiera. Adjurtable output 6v.. 9 v.. 12 volta for up to 500 mA (clans B working). Takes the place of any of the following batteries: PP1, PPS, PP4, PP8 PP7. PP9 and others. Klt comprinea: matas trantormer rectiter, amoothigg atd load redistor,
condenmera and inatructions. Real onip at only 1010, plus 20p portege.


## MINIATURE

WAFER SWITCHES 3 pole, 2 way-4 pole, $3^{2}$ way3 pole. 3 way-4 pole, 3 way- 2
pole 4 way- 3 pole, 4 way 2 pole
8 way-1 pole, 12 way. All at 28 p each.

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 Dry Film Labricant. In aerosol can for easy application and for putting mal oil can cennot reach. Home "and UBRNM everyday usea. We have purchaed alarge quantity of these from the Lalquidator and are able to ofler them to you for wbout half of the original list price. lubricant jo i.C.I. fuon L169.MULTI-SPEED MOTOR Siz upeed are vallable 500,880 and $1,100 \mathrm{r} . \mathrm{p} . \mathrm{m}$. and $8.000,12,000$ dameter and approrimately 1 in . long. $250 / 240 \mathrm{v}$. It apeed inay be further controlled with the use of our Thryrinter controller. Very poweriul and useful motor alze approx. $2 \mathrm{in}. \mathrm{dia}$.$\times i in. long.$
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15A ELECTRICAL PROGRAMMER Learn in your aleep: Gave radio plaging and
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Ferrantid latent device ZNist-givea resulta better then auperhet. Bupplied complete with Hi-Q TUNER COMPONENTS
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XIT MO. 1. Pleswey Miniature Tuning Condenser With built in LW awitch and $3^{* N}$ ferrit alah and KIT 110.2. AIr apaced tuning condenter $6^{\circ}$ ferrit roll litz wound $M W$ and $L W$ collh and wave change switch. 94p.
EIT MO, S. Alr spaced TC with elow nootion drive $8^{\circ}$ ferrit rod, whith litz wound LW and MW colls and wave change ewitch, sl-10.
KIT 110. 4. Permeabulty tuner with fant and alow motion drive and LW loading coilm and wave change awlith. BOp
HOUR MINUTE TIMER Made by Amiths. Complete With conirol wnob and call office, dark-room, tto. Bargain at E5j.
 asea of this timer are Machinery control, Boiler fring, Dlopenaing and Vending
machines, Display Mighing animated and algne, Bifnalling, otc. Price from machines, Dlaplay lighting animated and algne, Blfaalling, itc. Price from makers probably over $\ell 10$ each. Spectal andp price 36.88 plan 20 p poat and nsurance. Don't mien this territic bergain.

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Probably the tiniest ponathle radio, as described in Practical Wireleas January 73. All electronica parta 航. 20 poat pald. $^{2}$

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Juat what you need for work beach or lab.
standard 13 amp fured pluga and onfott awl
complete with 6 feet of dez eable. Wired up reet wheon warning light. Bupplled


HORSTMANN "TIME \& SET" SWITCH (ASO Amp Bwich.) Juth the thing if you want to come home to a warm house without it conting gon a fortuna. You can delay the switch on time of your electric fres, to. up to 14 hours from setting time or you can une the awlich to give - boost on Deriod of up to 3 hours. Equally saitsble to


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40 tacent lightiag unita with polyostar choke and Antohed white ename tonembled ready to inntall, te-80. poat 40p.

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 MULTI-CONE CABLE 7.0076 copper cores each core P.V.C. ingulated and of diterent colour. $3 / 16 \mathrm{in}$. thick. Price 28 p per yard.
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 SWITCHReted Ba. 240v. Made by Arrow. Type thted in the handles of electric drills. 10 for 64p.


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Complate as Illuatrated. Bave jour legs, time and temper smply by putting in sotm telephones. Ex. G.P O. not now- but graranteed in good conditlon and aervicesble. Bupplied with diagram and Instructlonn abowing how to connect. 3 types avallable na 1 each. Ditto with bell but less dial 11.25 each As illustrated with dita and bell $\$ 1.50$ each. Post etc. 50 p each.


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A must for every busy man, fives almost inatant hert aleo illumi-
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 Complete Kit (except wooden battens) to make tbe metal detector an the circrit in Practical Wirelena, Auguat isarue. $\mathbf{8} \mathbf{8} .20$ plue 20 p poot and InsuranceIMMERSION HEATERS BY
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How long doen it tak gou to renew fuse: Time yourself when next ona blows. Then reckoning your time at 41 per hoar see how qualclily our remotiable fum (auto circuit breaker) or 112 per dozen, epecify $\mathrm{B}, 10$ or 15 amp -simply of in place nf arfiel.

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Mede by the famoun Smithe Company． 240 v elock mechaniema．Price 21.10 each or 10 for 210 ．

ROCKER SWITCH
13 anip self－ixing into an ohlong hole． Bise appro
10 for $8 \mathrm{E} p$ ．


## SLIDE SWITCHES


slide 8witch．2－pole changeover panel mounting by two 6B．A．screws．Size op each． 10 for $84 \mathrm{~g}, 100$ for $85 \cdot 10,500$ for tea．Ditto an above but for printed 8ub lilnistare 8lide 8wlich，DP1）T 19 mm in approz．）between fixing centrea．18p each or 10 for $\mathbf{1 1}$－08．SP Change over spring return 250v 1 amp． 10 p ．
HIGH ACCURACY THERMOSTAT Unen difterential comparator 1．C．With thermbeter so probe．Denjger claims temperature control to pack $86 \cdot 10$ ．

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Makere Ref．KMKs Our number Rel．As．Open type maine operated coll－ 3 pairm changeoover Contactar rated at 6 ampa each．Mounted by Ditto but 12 V ．Our Ref．Rel A4．Price 55 p esich．

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 ELEMEMT26 garde length 70W．Self－regulating
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## SPEAKER

Marketed by Britten Relay under the name Lurintor．This io in a very neat looking cablaet and In ideal around the home or in the workabop for trouble ahooting or for testing out a quick lash up．Size approx． $9 y^{\circ}$ I $67^{\circ}$ I $3 y^{\circ}$ dmep．Input and amplliter may be powered by an tuternal $9 v$ and ampliner ingy be powered by on internsi 97 R－A eliptical $6^{\circ}$ I $3 \frac{y}{*}^{\circ} 10,000$ gatian，The minplitier


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EAR Laus Elf．Ploven parin，including candle one concave lena，one conver lena，stage and all reme，etc．watch light reys bead an they pae through difterent lensect．
EA\＆Wiatar Pump Eit．Thirteen parta．Top of pomp is tramparent so that operating parta may be obmersed．Bmall parts are brightly coloured to be seen enally while working．Three typen of pump may be maife：Lift pump．Force Pimp and
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EAS Curront ard Roalitance Eit．Twenty－nine partn，including hench and Jight bulh，Conduct interating and educational projecta to learn the application of＂OHMS LAW＂and wee the difter－ once in current and resistasce with diferent gpea and lengths of wire．
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75 ；cerriage up to 200 miles then 50 p per 100 mlles 75 p carriage up to 200 miles then 50 p per 100 miles

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 CONTROLVary mpeed of your wiper to mult conditions All parts and lontrucilos to make．fill 48

HORSTMANN 24－HOUR TIME SWITCH With 6 position programmer．When fitted to hot water ngatemn thas could programme to tolloza：－

| Programme | Hot Water | Central Feating |
| :---: | :---: | :---: |
| 0 | Off |  |
| 1 | Twice Daily | Of |
| 2 | All Day | Ot |
| 3 | Twice Datly | Twlce Datly |
| ${ }_{5}$ | Continuously | Continuo |

Suitahle，of courae．to rropramme other than central heating and hot water，for instance，programme upatalra and down－ and radio．In fect there is no ilmit to the veratilits of this Programmer Mains operated Bize 3 in．$\times 3$ in．$\times 2$ in deep Price 89．85 as Hllustrated but leas case．


## STANDARD WAFER SWITCHES

standard alis $11^{\circ}$ wafer－ailver－plated s－amp content standard $8^{\circ}$ splorlle $2^{-}$loos－with locking wabar and nat．

| No．of Polea | 2 way | 5 way | 4 way | 5 way | 6 way | \％${ }^{7}$ | 9 way | 0way | 12\％＊5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 pole | 44p | 440 | 44p | 44p | $44^{1}$ | 44p | $4{ }^{4} \mathrm{D}$ | 44 | 44 |
| 2 polen | 448 | 440 | 440 | 440 | 440 | 445 | 440 | 77. | 77 |
| 3 poles | 40． | 440 | 44 | 44 | 779 | 770 | 770 | 11.04 | 11.04 |
| 4 pole | 44p | 440 | 440 | 770 | 779 | 770 | 779 | 31.8 | 81－58 |
| 5 polea | 440 | 44p | 77 p | 77 p | 18.04 | 11.04 | 81．04 | 1.00 | 11－60 |
| 6 polea | 440 | 770 | 770 | 77 p | 81.04 | 81．04 | E1．04 | 11．87 | E1．${ }^{5}$ |
| 7 poles | 770 | 770 | 770 | 11.04 | 11－82 | 21．88 | 81.29 | ce． 15 | $2 \cdot 15$ |
| 8 poles | 770 | 779 | 770 | 81.04 | －1－82 | 81．88 | E1－82 | 58．48 | 22－48 |
| 9 polen | 778 | 77 | 81.04 | 31.04 | 81.60 | $31-60$ | 81－60 | 鯥．70 | 18－70 |
| 10 prolen | 77 p | 770 | 81.04 | 21．82 | \＄1－60 | $11-60$ | \＄1－60 | 33．00 | 88．00 |
| 11 poles | 770 | 51.04 | 81.04 | 11.2 | 11.87 | 11.87 | －11．87 | 43 ${ }^{\text {d }}$ | 4．25 |
| 12 pole | 77 | 11.04 | 11.04 |  | 11.87 | E1．87 | 11－87 | 新•㒾 |  |

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1 3is deep．Cadmium plated punched in the centre to Lake 3 P．O．
sooo type relayn．There ta aloo semoveabie cover
 over this section mearur． ing $41^{\prime \prime}$ long $\left.\times\left. 3\right|^{\prime \prime} \times 2\right\}^{\prime \prime}$ ． The chandin alao has a few holes and could take a amall tranaformer and／or valve holders alno monse $3 / 8^{2}$ hules for controlk，pote etc．This be an idea chased for making up a relay unit or similar Thene are ex－equlpment but in excellent condi－ thoo and may have a few reaintora etc．atill
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| U 8 | 60 | 200 mA 8 sub -3tin. Bilicon |  |
| U 6 | 30 | PN | 0.55 |
| U 7 | 16 | ectifler |  |
| 118 | 50 | 8il. Pianar Dioden DO-7 Glane 250 mA Alke OA200/202 |  |
|  |  | Mlzed Voltagen. I Watt Zener Dloriea |  |
|  |  | AY50 charge stora |  |
| U11 |  | FP811. Plan |  |
| 2 |  | Bllicon Reclltera Epory 800 mA up to 800 PIV |  |
| 3 | 30 | P'NP-NPN Bll. Tranalators 0C200 \& 28104 |  |
| 4 |  | Mized Eillinon and Germanium Dioden |  |
|  |  | NPN Bll. Planar Trane. TO- |  |
| U16 |  | 3 Amp silicon Rectifters Btud Type up to 1000PIV |  |
| U17 |  | Giermanlum PNP AF Tranalatorn TO-5 Jjke ACy 17-22 |  |
|  |  | A Amp Sllicon Rectifers BYZ.13 Trpe up to 600 FIV |  |
| 19 |  | Bilicon NPN Tranamators like BC108 |  |
| U20 |  | 15 Amp Sillcon Rectlfers Top Hit up 101000 PIV |  |
| 1 |  | AF. Germmilum Allos Transintors 201300 Serles \& OC71 |  |
|  |  | MAnT* like MHz Serles PNT Trensietors |  |
|  |  | Germanlum 1 Amp Rectiflern GSM Serlen up to 300 PIV |  |
|  |  | 300 MHz NPN (iltcon Tranmiators $2 \mathrm{~S} 70 \mathrm{~A}, \mathrm{B8} \mathrm{~V}^{\circ} 27$ |  |
|  | 30 | Past Ewitching gitleon Dioden like IN914 Micro-3iln. | 55 |
| 7 |  | NPN Germanlum AF Tranilatorn TO-1 flke AC127 | 0.55 |
|  |  | 1 A moselen TO-5 cmn, vo to 600 PlV CRE1/26.60n | 0 |
|  |  | Plantle 8illcon Planar Trans. NPN 2N292n |  |
| 1 |  | Sllicon Planer Plantic NTN Trann. Jonw Nolee Amp |  |
| US2 |  | Zener Diorten 400 mW W DO. 7 came $3-18$ rolin inlued |  |
| U33 |  | Plantic Cane 1 Amp Slicon Rectifera 1N 4000 Seriea | 5 |
| U34 |  | 8ilicon PNP Alloy Trann. TO-6 RCY26 $28302 / 4$ |  |
| U35 |  | Slilicon Planar Transletors PNP TO-18 2N2006 |  |
| ¢ |  | Allicon Planar NPN Tranalatorn TO-6 BPY80/61/62 |  |
| U37 |  | 8ilicon Alloy Transistors 80-2 PNP OC200, 28322 |  |
| 1138 |  | Fant Ewltching gilicon Trank. NPN 400 MHz | 0.88 |
| U39 |  | RF. Germ. PNP Tranmiators $2 \mathrm{~N} 1303 / 6$ T0-5 | S |
| U40 |  | Duai Tranmintorn 6 lend TO-5 2 N 2060 | 0.8 |
| U +1 |  | RFFGermantun Tranaint ore TO-1, OC45, NKT72 | 0.55 |
| U42 |  | VIf Gernanium PNP Tranoletors TO-1 NKT667, Arll7 | 0.85 |
| U43 |  | Bil. Trann. Plantic TO-18 A.F. BC113/114 | 0.55 |
| U44 |  | 811. Trann. Plastle TO-5 BC115/116 | 0.85 |
| U45 |  | A 8CR. TO86 up to 600PIV | 1.20 |
| Code No'n, mentsoned abore are given an a guide to the type of device in the pak. The devices themelves are normally unmarked. |  |  |  |

U23 30 MAnT" llke MHz Serles PNT Trensletors


U27 12 NPN Germinlum AF Transintorn TO-1 like AC127


$$
\text { U31 } 20 \text { Sulicon Planar Plastic NPN Trann. Jonw Nolee Amp 2N3707 }
$$

$$
\text { Us } 25 \text { Zener Dionten } 400 \mathrm{~mW} \text { WO. } 9 \text { came } 3-18 \text { rolin inlied }
$$

U33 15 Plantic Cane 1 Amp Blicon Rectifera 1N 000 Series

-

QUALITY TESTED SEMICONDUCTOR
Pak M
Q1

90 Red spot tranalatore PNE
4216 White npot R. F. Ifanglatora PN 43 OC 77 type transhators 6 OC 77 type tranatators atched tranalstors OC44/45/81/8in 0.55
$0 C 75$ B OC 72 transintor
AC 128 trannintora PNP high gala AC 126 trathistors PNP
OC 81 type transintors
AC $127 / 128$ Complementary palr 3 AF 116 type translatorn
3 AF 117 type transintors
3 OC $171 \mathrm{H.F}$. type transintor

$$
\begin{aligned}
& \text { OC } 171 \text { Hiv. type transintors } \\
& \text { 2N2926 sil. Epory tran } \\
& \text { mixed colours }
\end{aligned}
$$Q23 10 OA 202 gillcon dlocles sub- coded Q23 10 OA 202 gillicon dlodes sub-min.0.55 500 MHI (code P397) NPN tranalntors $4 \times 2$ N3703. 2N3702

## ELECTRONIC SLIDE-RULE

$$
2 \text { GETB80 }
$$

$$
\begin{aligned}
& \text { GET880 low nolae Germanlum } \\
& \text { transistorn }
\end{aligned}
$$

tranaistornQ19 3 MADT'S $2 \times$ MAT 101 \& $1 \times$ MATQ20 OC 4t Germanum irahalntors A.F.
Q21 4 AC 127 NP (iermaniumQ21 20 AC 127 NPS (iermanium tramalatora Q25 15 IN914 8llicon dloden 78 Piv $78 \mathrm{~mA}{ }^{\circ}$ Q26 0 0a9s Germanlum diodes aub-min Q27 2 10A PIV sllicon rectitiers 18425 R . $\begin{array}{llll}282 & 2 & \text { sillcon power rectillern BYZ } 13 & \ldots \\ 0.65 \\ 029 & 0.65\end{array}$ Q29 4 Allicon tranaistora $2 \times 2 \mathrm{~N} 696$, Q30 7 Allicon bifteh translators 2N708 0.85 Q31 6 alllcon auftch transiators 2 N 子o Q32 3 NPN Billent transistors $2 \times 2$ Nili

Q33 $\times 2 \mathrm{~N} 1132$ Q34 7 8illcon NPN transialors $2 \mathbb{N} 2369$

## Q35 3 sllicon PNP TO.B \& 2 N2904 \& 0.55

 0373 2N3053 NPN Sillicon tranaletors $\quad 0.65$

The NK Blide Rule, desleged to simplify Elec tronic calculations features the following scales:Conversion of Prequency and Wavelength. Reactance and Belf Inductance. Area of Cliscles. Volume of Cylladers. Resietsnce of Condurtors. Weight of Condurtors. Decibel Culculations. Anple Functions. Natural Loge and 'e' Functions. Multiplication and Divislon. Squaring, Cubling and Bquare Roofs. Convepalon of $k$ w and itp. A must for every electronle engloeer and enthuil. ant. Size: $22 \mathrm{~cm} \times$ tem. Complete with case and
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| :--- | :--- |
| UICO7 | 0.85 |
| U | 0.85 | $\begin{array}{ll}\text { UIC07 }=8 \times 7407 & 0.85 \\ \text { UIC10 }=12 \times 7410 & 0.85\end{array}$ $\begin{array}{ll}\text { UIC13 } & 8 \times 7413 \\ \text { UIC20 } & 0.85 \\ & 0.8520 \\ 0.85\end{array}$ UIC20 $=12 \times 7420$ $\mathrm{UIC} 30=12 \times 7430$

$\mathrm{UIC} 40=12 \times 7440$ U1C4 $=5 \times 7441$ UIC42 $=5 \times 744$

 | $\mathrm{UIC4B}$ | $=5 \times 7445$ | 0.55 |
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SN7406 BN7408
GN7407 BN7408
BN7409 BN7410 QN741 BN74 SN74 BN74
BNT4 QNT4t
QN74? BN7425
BN742 BN742 SN742 BN7430 $\begin{array}{ll}\text { BN77322 } & 0.50 \\ \text { GN7733 } & 0.80\end{array}$ BN743 BN7438 BN744 8 N 744 8N7442 0.74 BN744 BN7444 BN7445 21. 8N7446 \&1 07 BN7447
GN7448
81.10



 $\begin{array}{llllll}17 & 0.16 & 0.138 N 7460 & 0.17 & 0.16 & 0.1 \\ .17 & 0.16 & 0.13 & \text { RN7470 } & 0.32 & 0.29 \\ 39 & 0.34 & 0.31 & 0.2 \\ 39 & 0.34 & 0.31 & \text { SN7473 } & 0.32 & 0.28 \\ 0.41 & 0.3 & 0.3\end{array}$ $\begin{array}{lllllll}39 & 0.34 & 0.31 & \text { HN7473 } & 0.41 & 0.39 & 0.3 \\ 0.18 & 0.18 & \text { RN7474 } & 0.41 & 0.39 & 0.3 \\ 0.18 & 0.18\end{array}$ $\begin{array}{lll}0 & 0.18 & \\ 0 & 0.19 & 0 \\ 0.18 & 0\end{array}$ | 16 | 0 |
| :--- | :--- |
| 0.1 |  |
| 0. |  | 0.18

0.18
0.28
0.31 $\begin{array}{lll}.32 & 0.29 & 0.2 \\ .88 & 0.44 & 0.4 \\ .8 & 0.44 & 0.4\end{array}$ $\begin{array}{lll}7 & 0.18 & 0 \\ 5 & 0.53 & 0\end{array}$


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TAA 350 E1.87p 83p 77 p B.G.8. EA1000 22.90D

No.
BP930 BP932 BP933
BP935 BP935
BP938 BP938
BP944 $\mathrm{BP}^{4} 44$
$\mathrm{BP945}$ BP945
BP948 BP948
BP948 BP948
BP951 BP9812
BP9093 BP962
BP9093 BP9094 BP9097
BP9099 BP9099
 quantity price. Larger quantiky price
on application. (DTL 930 Beries onlf). on applicatlon. (DTL 930 Eeries obls).

\section*{NUMERICAL INDICATOR TUBES <br>  <br> | MODEL | Cder | OR116 | 3018 F mintion |
| :---: | :---: | :---: | :---: |
| Anode voltage (Vdc) | 170 min | 175 min | 5 |
| Cathode Current (mA) | $2 \cdot 3$ | 14 | 8 |
| Numerical Height (mm) | 16 | 13 | 9 |
| Tube Helsht (mm) | 47 | 32 | 22 |
| Tube Diameter (mm) | 19 | 13 | 12 wide |
| I.C. Driver Rec. | ${ }_{141}$ | $\begin{gathered} \text { BP41 or } \\ 141 \end{gathered}$ | BP47 |
| PRICE EACH | 21.87 | 41.70 | 21.60 |

RTL MICROLOGIC CLRCUITS
Price esch
Eposy TO-5 case 1-24 25-99 100 up uL900 Buffer 38D 36p 290 $\underset{\text { gate }}{\text { ul914 Dual21/D 38p } 38 \mathrm{p}} 29 \mathrm{p}$ $\begin{array}{cccc}\text { Gate } & \text { 38p } & \text { 36p } & \text { 29p } \\ \text { UL023J-K fip-top } & 55 \mathrm{~g} & \text { 51p } & \text { 49p }\end{array}$ Date and Circuits Booklet for IC's Price 8p.
DUAL-IN-LINE SOCKETS. 14 \& 16 Lead Sockets for nse पltb PROFESSIONAL ANEW LOW COST PROF. TYPE No. 1-24 25-99 100up. $\begin{array}{lllll}\text { T80 } 14 \text { pintype } & 330 & 300 & 28 \mathrm{D} \\ \text { T80 } 16 \text {, } & 39 \mathrm{D} & 350 & 33 \mathrm{p}\end{array}$
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BPS 16
$\begin{array}{lll}170 & 130 & 180 \\ 180 & 130 & 180\end{array}$

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15 mA
Qulescent current 15 mA
Nolter than -75 dB
Supply voltage
SA35 $25-45$ volts
Supply voltage $\quad$ SA35 $25-45$ volts
Size
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## INTEGRATED CIRCUIFS

There is a remarkable and noteworthy contradiction in present day electronics. While circuit designs are tending to increase in complexity and in variety of functions offered, in terms of actual hardware electronic equipments are tending to become less complicated and consequently simpler to build.

The explanation to this apparent paradox is to be found in the integrated circuit. This is a small component hardly larger than a conventional transistor, but containing a complete circuit arrangement incorporating a number of semiconductor devices as well as other circuit elements. As constructors, we don't really have to concern ourselves with the internal details of these remarkable devices. It is sufficient for many purposes to consider the integrated circuit (i.c.) as just another component, or as a "black box".

Integrated circuits have been around for many years, but Everyday Electronics has so far concentrated upon discrete semiconductor devices. This makes sense, because it is our belief that a true understanding of electronics can only stem from an awareness of the discrete transistor and familiarity with its function as gained through practical constructional and experimental work.

But to ensure that our readers reap all possible advantages from modern developments, we shall make increasing use of integrated circuits in future designs. For a start, this month we include two quite dissimilar projects that

Our October issue will be published on Friday, September 21
are based upon different examples of these miniature marvels of current technology.

## DON'T MISS THE BUS!

Great news for all those wishing to learn the basics of electronics from scratch. Here is their BIG OPPORTUNITY. An entirely new series Teach-In '74 will be launched next month in Everyday Electionics. This series has been carefully and expertly planned to meet the need of the ordinary person, man or woman, boy or girl, who wishes to acquire an understanding of electronic circuit principles without delving deeply into mathematics.

No previous experience or knowledge is required! Easy to follow text will be accompanied by easy to perform practical exercises requiring the very minimum of tools and components.

Regrettably it is our duty once again to advise readers that the supply of back numbers of Everyday Electronics is not possible. So all budding enthusiasts please do take heed of this advance notice and friendly word of advice. Opportunities for the layman to learn the fundamentals in such an enjoyable and painless way in his own home as we have planned are all too rare, and of necessity come at infrequent intervals.


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[^0]
# EASY TO CONSTRUCT SIMPLY EXPLAINED 

VOL. 2 NO. 9



## CONSTRUCTIONAL PROJECTS

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Everyday Electronics, September 1973



Although it is very difficult to define what fascinates so many people about a miniature radio receiver, the fact remains that a great many people enjoy "messing about" with radio on this scale, and derive many hours of enjoyment (and learn a great deal of physics) from constructing these devices.

## CRYSTAL SETS

The crystal set is the most basic receiver possible, Fig. 1 shows a typical simple crystal set using a tuned circuit, and a diode to detect the modulation-the audio part of the waveform which drives the earpiece. A long aerial wire and an earth are essential if any volume is to be expected, and unless very high impedance headphones are used the programmes will all merge into one. This is because a low impedance across the tuned circuit will damp it and increase the bandwidth or range of frequencies received.

If one perseveres with the crystal set shown, one will notice that it possesses one or two fine

Fig. 1. A typical, simple crystal set.

qualities. These are:

1. The sound quality is very good (if a good ear piece is used).
2. The background noise is very low.

These are the basic requirements for a quality radio receiver. Unfortunately, the receiver has some bad qualities too. These are:

1. The volume is very low.
2. The large aerial necessary is somewhat cumbersome for a portable receiver.

## THE I.C.

Now, if we could add between the tuned circuit and the earpiece a circuit which possessed r.f. gain, low distortion and high input impedance, we would maintain the good qualities above and eliminate the bad qualities.

Using modern semiconductor processes it is now possible to achieve just this and the Ferranti ZN414 offers us complete radio tuner in a 3 pin "transistor" package. If the circuit of Fig. 1 is re-drawn using ZN414 we have an earpiece radio which has real advantages over existing types (Fig. 2). The very high input resistance (greater than 4 megohms) of the ZN414 ensures that the tuned circuit is virtually undamped by the device. Thus very high selectivity, low bandwidth operation is possible. The output of the ZN414 can now drive a lower impedance earphone.

If this circuit is built remember that although layout is not too important leads should be kept as short as possible. When the unit is operating the effects of varying Ll (unwinding turns) and Cl can be noted. Also, if one deliberately damps the tuned circuit by adding a resistor (say 10


Fig. 2. The basic set using the ZN414.
kilohms) across it, it can be shown that the selectivity is reduced.

It does not need much imagination to realise that the radio shown in Fig. 2 could fit into a very small case. In practise, the size is limited by the ferrite rod which should not be reduced below about one inch in length.

A diagram of the connections to the ZN414 is shown in Fig. 2. Fig. 3 shows the internal circuitry of the ZN414 and is included for reference.

The basic receiver shown in Fig. 2, whilst capable of good results, lacks certain refinements which are desirable if optimum performance is to be achieved under all conditions. For this reason a further receiver circuit has been developed. This can have the refinement of volume control (or preset) volume control and a sensitivity control if wanted, and can be used to drive an amplifier (of input impedance greater than 20 kilohms) if necessary.

The circuit is shown in Fig. 4, the layout for printed circuit board in Fig. 5 and the wiring for the p.c. board in Fig. 6. One advantage of the crystal earpiece used is that two can be "paralleled" up to make a headphone. It is a lot less tiring to listen with both ears than one, and crystal earpieces are much cheaper than other

## Components

```
Resistors
    R1 100k\Omega
    R2 3.3kS
    R3 250\Omega
    R4 560\Omega
    R5 100\Omega
    All }
```

Capacitors
C1 100 pF to 200 pF miniature variable
C2 $0.01 \mu \mathrm{~F}$ miniature ceramic
C3 0.1 or $0 \cdot 22 \mu \mathrm{~F}$ miniature ceramic
C4 $0.05 \mu \mathrm{~F}$ miniature ceramic
Semiconductors
IC1 ZN414 integrated circuit
TR1 ZTX300 silicon npn
$\left.\begin{array}{l}\text { D1 ZS120 } \\ \text { D2 ZS120 }\end{array}\right\}$ or any small signal silicon diode
Miscellaneous
L1 Ferrite rod $2 \frac{1}{2} \times \frac{1}{\ddagger}$ inch diameter and
length of $30 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. enamelled copper
wire
TL1 Crystal earpiece
B1 3-6V battery (comprised of four RM
675's)
Jack socket to suit TL1 incorporating an
on/of switch (S1), 6BA fixings and stand-off
pillars, plastic case approx. $3 \times 1 \frac{3}{4} \times \frac{3}{4}$ inches.
types. The quality of reproduction from two crystal earpieces using this circuit is astonishingly good.

The circuit now includes certain desirable features such as much higher volume (with optional control) and sensitivity control if required. This latter feature is vital for an experimenter, as it enables a much wider range of ferrite rod sizes and/or earphones to be used without making the receiver difficult to operate.

The prototype receiver used miniature "button" batteries which, although expensive, give extensive life and enable a fairly small receiver to be constructed. The voltage is not critical, the higher ranges will give higher volume without distortion.



Fig. 4 (left). The complete circuit diagram of the Personal Receiver.

Fig. 5 (below). The printed circuit layout for the receiver shown full size.


A magnetic earpiece may be used in place of the crystal one, by substituting it for the 560 ohm resistor R 4 soldered between the collector of TR1 and the positive supply rail; its impedance should be similar (about 500s).

If during experimentation one finds earpiece listening tiring (continual removal and replacement of an earphone can be very irritating) the earphone can be replaced by a connecting lead to an amplifier, which has a high input impedance. Most transistor amplifiers are suitable, and no damage will be incurred if the circuit in Fig. " ${ }^{\prime \prime}$ is used.

## CASE CONSTRUCTION

The constructional details given are not for a micro-miniature set. They are intended for an easily built receiver. The set is small and yet avoids very "fiddly" working. The complete unit is housed in a transparent Perspex box size 3 inches $x 1^{3_{4}}$ inches $x^{3_{4}}$ inches shown in Fig. 8. Perspex is glued internally with polystyrene cement to provide a battery compartment, and a clamp for the ferrite rod.

The bottom of the box slides out for battery replacement. The batteries are held together by a small spring, laterally they are held by a piece of neoprene tubing slit across to allow the batteries to be inserted easily. The earpiece is connected by means of a jack socket and this also carries an on/off switch. Thus the set is turned on when the earpiece is plugged in.

Care is needed in drilling Perspex; if too much pressure is put on the drill it will crack the Perspex. Slow steady drilling is best.

## VARIATIONS

A volume control can be added by inserting a 250 ohm potentiometer (a preset type could be used) in series with the emitter of TR1 e.g.
between the junction of R5/C4 and the emitter. This control will only reduce the output power from the circuit as shown and was not found to be essential in the prototype. Resistor R5 should not be omitted or have its value reduced.

Diodes D1 and D2 are used to form a voltage stabiliser for the supply to the ZN414. These diodes can be any small signal silicon types, for these the forward voltage drop is about 600 mV to 700 mV each, giving a supply of about 1.4 V .

The sensitivity control, if required, can be obtained by adding a 1 kilohm preset in place of DI.

The acrial coil should be wound using 30 s.w.g. enamelled copper wire. Start winding at about $3_{8}$ inch from one end of the rod and wind on 85 turns. The turns should be touching each other and not crossed or overlapping, insulation tape can be used to secure each end.

Any small (physically) tuning capacitor of value 100 pF to 200 pF may be used. A few more turns will be needed on the coil if lower values (less than 100 pF ) of capacitance are used. The internal layout of the prototype receiver is shown in Fig. 8.

Fig. 7. Additional components and connections for use with an external amplifier.


Everyday Electronics, September 1973

Fig. 6. Wiring of the printed circuit board.




UP to the last two or three years many keen yachtsmen and small workboat owners such as inshore fishermen with 40 foot boats were heard to complain of the lack of a suitable "mini" radar. After all, big ship radar had been with us since the early days of the last war, the world's leading manufacturer was about to clock up his 40,000 th order, and radar for small craft, as opposed to "very" small boats, had been available since 1963 (in one case a small boat radar had first appeared in 1966, but the smallest boat which could use this is about 40 feet).

Suddenly there was a proliferation of sets suitable for "very" small craft but this was followed immediately by the failure, or at least lack of obvious success, of some of them. What is there to mini radars generally and why do the manufacturers appear to find this particular market so difficult? In answering these questions, it is hoped that old radar hands will forgive a description of basic principles.

## BASIC OPERATION

Radar is easily understood, once comparisons are made with sound waves, and the echoes which return from them. We know that sound travels through the air at the rate of about 1100 feet per second. Until radar was developed skippers of boats working near cliffs or up rivers used sound waves to determine distance away from bluffs, buildings and so on. A short blast on the whistle would be sounded, and the seconds counted until the echo was heard. If it took five seconds for the echo to return it meant that the sound waves had travelled a total distance out and back of approximately 5,500 feet; therefore the target was a little over half a mile away.

Now it happens that if you send out radio waves at a suitable frequency (the standard
" X " band is 9380 to 9440 MHz ) with sufficient energy, they actually bounce back to you from hard objects in exactly the same way. As the speed of both the emission and the returning echo is similarly constant, all you have to do to measure the distance of the hard object is to record the time taken for the entire operation. A marine radar incorporates many refinements to this principle but basically that is all there is to it.

Taking things a stage further: a radar set consists essentially of the following elements; the transmitter to generate short bursts of radio-frequency energy; a rotating scanner to radiate the radio waves in a narrow beam around the horizon and pick up the returning echoes; a receiver to detect and amplify these echoes; and a display tube to visually present them, with facilities for measuring range and bearing. The transmitter and the receiver are combined in one unit, which for convenience is called the transceiver, and there is an extra unit -making a total of four-for the power supply (all radars work off standard voltages from 12 V upwards, but this has to be changed into a form acceptable to the radar, usually by a static inverter).

## BASIC SYSTEM

Coming from the general to the particular, these four elements still exist but in recent years have been telescoped into three units, and lately into only two. This naturally simplifies and cheapens installation and there is a useful saving in wheelhouse space, particularly important in workboats which may already have much other instrumentation. The compression from four to three units came about by installing the transceiver immediately under the scanner in a form of a streamlined pod. With the transceiver below-where it still has to be in the case

Everyday Electronics, September 1973


The "exposed" scanner of the Decca 101 radar.
of larger big ship sets-it is joined to the scanner by an expensive and energy losing waveguide of rectangular copper tubing. The obviation of this, not only simplifies installation but allows a smaller power output for the same radar performance. This again results in a smaller power requirement from the boat's supply, usually a matter of great significance.

Further miniaturisation through the adoption of solid-state techniques (an ill-defined phrase but here taken to mean the latest micro-circuit and other solid-state devices) has enabled the power supply to be incorporated in either the scanner/transceiver assembly or in the display, or shared between the two. This results in a total of only two units, and is standard with mini-radars. With so much of the electronics of the system built into a scanner assembly which may be several feet up in the air, it is important that the different elements are designed on a modular plug-in principle as far as possible, for easy removal below.

## TRANSCEIVER

The transmitter and receiver are in appearance almost a unity as the name transceiver implies, but in reality have, of course. very distinct functions. The transmitter and receiver circuits are provided with a means of isolating one from the other, so that when transmitting, none of the energy goes into the receiver; and only when the transmitter has stopped its emission is the receiver on and enabled to receive the reflected echoes. To measure the time lag between emission of a radio wave and its reflected echo obviously requires electronic switching on and off of the transmitted radio waves at a rate so rapid that it nearly defies comprehension.

The bursts of power, or pulses, are timed in two ways. First, the lengths of time measured in fractions of a microsecond that the transmitter is on. This is termed pulse length. Second, the number of times per second that the pulses are repeated. This is termed pulse repetition frequency.

There are short and long pulse lengths automatically controlled by the range to which the radar is set. Usually shorter pulse lengths are used on short ranges for optimum range discrimination between objects; longer pulse lengths for longer ranges because of the need for a greater amount of power to create an echo. These pulse lengths typically vary between 0.05 and 1.5 microseconds.

## SCANNER

It is logical to consider the scanner next. As many readers may have noticed, in a large vessel, it consists of a horizontal bar from 4 feet to 9 feet long and about 6 inches deep. This is mounted on a pillar or other support and made to revolve at about 30 r.p.m. by a small motor mounted beneath. In mini-radars this assembly is invariably cased in a glass-fibre "radome", resulting in a mushroom appearance. The predominant reason is reduction in cost. The radome itself is not expensive and permits the scanner inside to be lighter, easier to rotate-since wind resistance is removed-not weatherproofed, and so cheaper and requiring less electrical power. As we have seen the radome houses the transceiver, and in one design the power stipply as well.

Design of the scanner itself is always important but particularly in very small boats. Obviously, the smaller it can be the lighter and cheaper, but there is a limit below which performance in the form of discrimination (the ability to separate adjacent echoes) and freedom from side lobes, suffers unduly (it is impossible to direct all the energy into the desired beam and a small amount will be radiated to

Scanner unit of the Decca 050 radar showing the transmitter and turning assembly.



The two points of the Electronic Laboratories Seascan small boat radar.
either side, this is known as sidelobes and, if excessive, will create highly undesirable false echoes on the display).
The minimum size of scanner would appear to be 30 inches. The actual design of the aerial itself is another important point. Up to the late fifties the cheese type aerial was standard, where the end of the waveguide is positioned at the focal point of a parabolic reflector; the width of the latter has to be large in comparison with the wavelength so that transmission can be made in the form of a narrow beam. It is bulkier and not so efficient as the slotted waveguide scanner now universal in commercial and most other radars.

In the slotted waveguide type a bar aerial has slots cut in the vertical face through which pulses can be transmitted and echoes received. The disadvantage is that the slots have to be cut extremely accurately according to a mathematical formula and a slotted waveguide aerial is considerably more expensive than a cheese type.

## DISPLAY

The echoes are handled in the receiver portion of the transceiver. Obviously they vary greatly in strength; a nearby ship produces an extremely strong echo, while a buoy some distance away produces only a faint one. All are very greatly amplified to bring the weak ones to a level that can be seen on the display. The echoes are then levelled to a common value, so that the echo created by a nearby ship will bear a reasonable relationship in size to that created by a buoy. All this is done electronically and may answer some queries as to why radars are not as cheap as washing machines!

To understand the working of the display,


The Decca Super 101, this is a three unit system suitable for boats down to about 40 feet.
simple comparison with a searchlight may be made. Imagine yourself directly above the boat's searchlight which is being rotated 360 degrees. As it revolves the beam of light crosses boats close by and you see each of these objects momentarily. Consider now the radar's cathode ray tube, the circular extremity of which forms your radar display. As with the searchlight, your position is in the centre of the circle and the display shows all "radar conspicuous" objects within the range set at the time.

There is a difference, however, in that the inside of the tube is treated with a special material that continues to glow for a considerable period after the echo has been passed; in addition, each time the scanner directs the radio waves to cross a target (which it does about every two seconds) the echo is re-illuminated. In this way the entire radar scene is permanently visible, though the targets currently being swept show up more brightly than the remainder.

By courtesy of certain elements in both the receiver and the display any one boat mentioned above will be shown on the display as a bright spot at a range and bearing from the centre (which represents own ship) exactly corresponding to its true position. Radars have several range scales whereby, at the turn of a knob, the radius of the display can be taken to represent different distances from, say, half a mile to 18 miles. Concentric illuminated rings on the display represent increasing distances from the centre; as the range scale is changed the previous rings disappear, to be replaced by new rings in different positions, and it is always easy to gauge the range of an echo by its position relative to the nearest ring.


The display unit of the Decca 050 radar mounted in front of the "helmsman".

The relative bearing of an echo is read off the circumference of the display, with the aid of a revolving transparent disc. Modern big ship sets have more sophisticated facilities whereby, as controls manipulate a variable ring for range, and a radial line for bearing, the two readings come up simultaneously on digital readouts.

## QUALITY, PERFORMANCE, PRICE

So much for the general principle of marine radar. At the outset of this article-which concentrates on mini-radars as being of interest to the widest circle of boat-owners-it was stated that, judging by results, many manufacturers find this is a very difficult market; not so much in selling the finished product but in getting its original design right. Why is this?

The basic reason is that the three-sided equation between quality, performance and price is a very awkward one. The price ceiling simply must be low, bearing in mind the likely pocket of the prospective owner and the danger of being undercut by a competitor. The manufacturer's outlets, usually agents in the case of pleasure craft and his own depots in the case of work-boats will have no chance (particularly with cost-conscious fishermen who form a very large section of the market) if the price is too high.

Performance in the form of maximum range, minimum range, definition (sharp, clear-looking echoes) discrimination, power required and so on must be adequate in view of competition. Last, but by no means least, there is quality; quality of electronic design, mechanical design and materials used; these are the basis of reliability. Contrary to general belief, the smaller the radar, the more hostile an environment it will be in. For example, a 30 foot family cruiser which is shipping a lot of water and spray and vibrating from the action of its engine is probably providing rougher treatment than that experienced by the radar of a large merchant ship on a sturdy bridge high above the
waves and which is being operated by professional mariners.

The manufacturer has an agonising balancing act to perform between performance, extra ruggedness plus highly reliable material leading to high cost on the one hand and the necessity to keep the price down on the other. Some have failed to solve this equation first time, one large company having to dispose of its mini-radar altogether, and at least one other bringing out a second mark with major modifications.

## CHOOSING

When choosing a radar it cannot be stressed too highly that reliability is the first thing to look for. As this is not assessable for any particular set in advance the best thing to do is enquire of existing owners. Performance is naturally important-but is of no account if the set won't work-and in the context of a very small boat it should be realised that theoretically long range may be unattainable in practice. This is because radar sees almost directly like the human eye (the radar horizon exceeds the optical horizon by 6 per cent).

There is little point in buying a 20 mile range radar if you are only going to mount it 18 feet above the water, because its "horizon" at that height will be only five miles. To be fair it will pick up high land at a greater range, but somewhat disappointing since the distance at which a feature will be on the horizon of a radar is found by adding the aerial's horizon to that of the feature. The following aerial heights (in feet) are followed by the corresponding radar horizon (in nautical miles) in brackets: 10 (4), $15\left(4{ }^{1}{ }_{2}\right), 18(5), 24(6), 32(7)$, so that land at 32 feet will begin to appear above the horizon of an aerial at 10 feet, at $7+4=11$ miles.

Another aspect that prospective owners should look into most carefully is the service organisation of the manufacturer. In spite of what the brochures claim (so often "a new concept in radar reliability") radars do break down, and the proximity of a manufacturer's service depot or trained agent-there are few aboutcan make or mar a sailing holiday in certain circumstances. This is actually a factor in the price of the radar, since widespread service organisations are not maintained for nothing, and charges must be realistic.

## USE

A brief look at what radar will do for you. Collision avoidance was its original object and still holds pride of place in the minds of most people. On a dark night or in fog, the possession of radar confers peace of mind, in that it should be impossible for anything bigger than a football, providing it is projecting far enough, to come dangerously close undetected. And if you want to see whether another vessel will hit you
if both stand on, it is only necessary to take successive bearings of her when your own boat is dead on course. If they do not alter considerably she will at least pass close. This check is more easily performed than with a compass.

However, study of an article that appeared some time ago in the yachting press on the uses for which radar was put throughout a seven port cruise, showed that collision avoidance came up only once in half a dozen times. Why do virtually all Scottish motor fishing vessels fit a radar when the instance of fog on the North East coast of Scotland is in fact slight? They use it for a multitude of small tasks from locating the small dan buoy which marks the end of their net, to fixing their position. Most radars are efficient, in calm conditions, down to about 20 yards and this can be a great help in locating your moorings or picking your way into harbour among lines of moored yachts.

Coastal navigation is a subject in itself, but basically, everything that the navigator does to fix his craft by cross bearings can be emulated and more quickly, with radar. In addition, a range facility is added, enabling 'range and bearing' fixes to be obtained as well. Is important of course that the point you are taking on the display is exactly identifiable on the chart; this is not difficult with experience but it is advisable to practice in good conditions when checking is easy.

## CONCLUSION

In conclusion, a quote from an american enthusiast, which is being proved by more and
more British owners: "Since the fitting of radar we have cruised thousands of miles more safely and without the anxiety that is ever present when compelled to operate in thick weather, or to enter a strange harbour at night."


## What doyouknow?

1 You want a transformer to supply 24 volts at 1 amp . You have a 24 volt 500 mA , a $12-0-12 \mathrm{~V} 2 \mathrm{~A}$ and 30 V 1 A which one would you use, and how would you connect it.
2 A coil and a capacitor are used to form a tuned circuit in a project you are building. The coil you have is slightly higher in inductance than that required, you cannot alter its value so what could you do to get the correct resonant frequency.
3 What does the following circuit symbol represent:


4 The impedance of a coil is stated as being

400 ohm, when you measure its resistance on a multimeter it is only 100 ohm. Say if you think this is correct and why.

## ANSWERS

II!M pue kouanbol! dejno!qed e fe peanseaw
$\forall 1$ әчł Kiddns uej damsofsueł әчł pue бu!ped

# Bothered by <br> Basics? <br> <br> Confused by <br> <br> Confused by <br> Current? <br> <br> Troubled by <br> <br> Troubled by <br> <br> Transistors ? 

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# Aquarium TH ERMOSTAT 

 BY MIKE KENWARD
## A unit for accurate temperature control of liquids.



roprietary thermostats for fish tanks and other heat control and monitoring applications are available and many of them are simple and cheap. However it has long been the requirement of many tropical fish keepers and others to have a more reliable, more accurate thermostat that can be set to the required temperature and that will maintain the temperature of a liquid to within ${ }^{1}$ degree centigrade.

The thermostat to be described in this article was designed for this purpose and was found in practice to be extremely accurate, once set, and able to keep the temperature to within less than ${ }^{1} 2$ degree should this be required.

## CIRCUIT

The circuit diagram of the thermostat is shown in Fig. 1. Transistor TR1 is operating in the emitter follower mode, the output of which is determined by the setting of VR1 and VR2, and by the resistance of thermistor RTH1 which is determined by its temperature. The output from TRI emitter is fed, via a current limiting resistor R2, to a Schmitt trigger formed by TR2 and TR3. The use of TR1 prevents undue loading of the Schmitt by the thermistor.

The thermistor RTHl is located in the liquid, the temperature of which is to be controlled. With a fall in temperature the resistance value of RTH1 rises and causes TR1 to pass less current through its collector emitter junction. Thus the voltage at TR2 base falls and TR2 begins to turn off, at a certain level (set by R3, R4 and R6, TR3 turns on and forces TR2 to
turn completely off (Schmitt action). This switching of states happens very quickly and TR3 switches from off to fully on with only a slight change in the value of RTH1.

Transistor TR3 operates a relay which is used to switch the mains supply to a tank heater. Thus when TR3 turns on the heater is turned on and the liquid begins to warm up. When the required temperature is reached the fall in the resistance of RTH1 causes TR1 current to rise and the Schmitt to revert to its original state (TR2 on TR3 off) thus turning off the heater via RLA1.

## HYSTERESIS

Although the above action is straightforward one problem is encountered-the hysteresis present in the Schmitt trigger circuit. This means that the unit would only switch with a


Fig. 1. The complete diagram of the Aquarium Thermostat.
rise and fall in temperature of about 3 degrees centigrade which is greater than the required temperature control.
To overcome this VR3 has been incorporated in the Schmitt circuit and this resistor is used to "balance" the two transistors and thus reduce the amount of hysteresis. Thus this potentiometer can be used to vary the sensitivity of the thermostat and can be set to keep the temperature to within about plus or minus 5 degrees centigrade down to less than plus or minus ${ }^{{ }^{1}} 2$ degree centigrade. In actual fact the prototype was able to maintain the temperature to a very high degree of accuracy-higher than is practically useful in an aquarium and higher than we were able to measure by conventional means.

## SUPPLY

Power for the circuit is derived from the mains via the bell transformer T1, the rectifier D2 and smoothing capacitor C1. This very basic half wave supply was found to be quite adequate in practice. Diode D1 is incorporated to prevent the back e.m.f., caused by RLA1 switching off, from damaging TR3.

## CONSTRUCTION

Commence construction by cutting and drilling the circuit board as shown in Fig. 2. Mount all the components-soldering in the transistors and diodes after the other components and flying leads.

Next mount all the components in a suitable metal or plastic case as shown in Fig. 3 and wire up the complete unit. Note that if a metal case is used a three core mains lead should be provided and the box should be earthed by means of a tag bolted to the inside.

The themistor must be isolated from the water and can be mounted in any convenient way. The prototype used a thermistor mounted on the end of a short length of plastic tube (ball pen case) and covered in Araldite to insulate and protect it. Take care not to use too much Araldite on the thermistor as this may prevent it from reacting quickly to temperature changes.

Fig. 2. Layout and wiring of the components mounted on the Veroboard.


# Aquarium TH:ZMOSAT 



Fig. 3. Layout and wiring of the componenfs mounted in the case.

## Components.... <br> Resistors

| R1 | $56 \mathrm{k} \Omega$ |
| :--- | :--- |
| R2 | $10 \mathrm{k} \Omega$ |
| R3 | $22 \mathrm{k} \Omega$ |
| R4 | $1 \mathrm{k} \Omega$ |
| R5 | $22 \Omega$ |
| R6 | $10 \mathrm{k} \Omega$ |

## SEHOD <br> TALK

Capacitor
C1 $100 \mu \mathrm{~F}$ elect. 15 V
Variable Resistors
VR1 $2 \mathrm{k} \Omega$ carbon linear
VR3 25082 carbon linear
VR3 500S2 carbon linear
Semiconductors
D1 Any small signal silicon diode
D2 IN4148 or any 50 V 200 mA silicon diode
TR1 2N2926 (any colour) silicon npn
TR2 2N2926 (green) silicon non
TR3 2N2926 (green) silicon non
Miscellaneous
RTH1 VA 1005 thermistor
RLA 2000 s2 P.O. type 3000 relay with one set of normally open contacts
T1 Friedland bell transformer $(200-250 \mathrm{~V}$ primary, 8 V secondary)
LP1 Neon indicator lamp with built in resistor Veroboard $2 \frac{1}{2} \times 1 \frac{1}{8} \times 0.15$ inch matrix, small aluminium bracket for RLA, mains lead, materials for mounting RTH1 (see text), plastic case approx. $7 \times 4 \times 3$ inches, $4 B A$ fixings, mains plug, knobs as required.

## TESTING

Connect the unit to the heater and mains and with RTH1 in free air and VR3 fully clockwise switch on. Turn VRI (coarse temperature) through the range and check that RLAl clicks in and out as you do this, LPl is incorporated to show when the relay is operating (ie. heater on). Next set VR2 (fine temperature) fully clockwise and VR1 so that RLAl has just operatedswitched on the heater-now turn down VR2 and check that as it nears its minimum value RLAl drops out-turn up VR2 until RLA.l just operates.

By breathing on the thermistor it should now be possible to cause RLAl to drop out and switch off the heater. Now test the function of VR5 (sensitivity) by turning it fully anticlockwise and resetting the unit as above. It should now take a greater rise in temperature to make RLAl operate.

If all is well place RTH1 in the tank and turn VR1 up, when the required temperature of the liquid is reached back off VR1 and adjust both VR1 and VR2 until RLA1 just drops out. Leave the unit set and observe the rise and fall in the
temperature.
By adjustment of VR3 and the two temperature controls the correct temperature and controlled level (rise and fall) can be set. This may take a little time but once set will remain constant. Any latter alteration of VR3 (sensitivity) may also mean slight adjustment of VR2 and possibly VR1 to maintain the correct temperature.

The thermostat can be used to maintain the temperature of other liquids-such as used in colour photographic work-but for accurate control the thermistor should be mounted away from the heater and some means of "stirring" the liquid introduced.

Photograph of the conpleted Veroboard with the components mounted on it.


The connections to VR1 and B1 positive on the Waa Waa Veroboard layout (page 439, August '73) should each be moved one place to the left to position A9 and A8 respectively. The wiring diagram of Fig. 6 with reference to these connections is correct. The connection from A2 to SK1 should be omitted and the screen from C2 should be connected to SK1 auxiliary tag.

In the Electronic Dcorbell article (August '73) transistor TR5 was incorrectly shown as an AC 126. This should have been an AC 176.

Under What Do You Know it was stated that the AC 127 could not be used in place of the BC 109 because it is a pnp device. It is an non device but it would not be as likely to work as the 2N2926 because it has a much lower gain.

We apologise for any confusion caused by these mistakes.

$W^{\text {e }}$continue this month with further properties and theory of the transistor and introduce some transistor types which will be completed in Part 5.

## COMMON EMITTER CURRENT GAIN

The a.c. current gain of a transistor in the common emitter circuit is usually designated $\beta, \gamma^{\prime}, h_{21}$ or $h_{\text {f.. }}$ It is given by the equation:

$$
\beta=\frac{\text { change in collector current }}{\text { change in base current }}
$$

The current gain of typical transistors in the common emitter circuit varies from about 5 to 1,000 . It varies from one type of transistor to another, but even amongst transistors of the same code number there are variations in the current gain of between about two times to five times (depending on type). The current gain is temperature dependent.

The common emitter current gain usually rises at first with increasing collector current until it reaches a maximum, after which it falls again (see Fig. 4.1).


Fig. 4.1. Variation of current gain with collector current in a typical transistor.

Some transistors (such as the 2 N 2484 ) are designed so that they provide a high current gain even at very low collector currents (perhaps 0.01 mA ), whilst other transistors provide a high gain in the medium current range (typically 1 mA to 100 mA ) and yet others in the high current range (perhaps 5A to 10 A ).
The common emitter circuit not only provides a current gain of over unity, but it also provides a voltage and a power gain when used in a suitable circuit. The power gain provided is normally greater than that obtainable using the same type of transistor in either of the other basic circuits.

## LEAKAGE CURRENT

In Fig. 4.2a, a transistor is biased in the normal way with the collector positive with respect to the base, but the emitter is left unconnected so that the emitter current is zero.

Although the collector/base junction is reverse biased, a small current will pass, since both of the materials contain limited numbers of minority carriers which are attracted across the junction (as in the reverse biased diode). This small current is known as the leakage current.

(a)

(b)

Fig. 4.2. Measurement of leakage current.
The leakage current in the common base connection is designated $I_{\text {cbo }}$ (or sometimes $I_{\text {co }}$ ). The subscrip "cb" indicates that the current flows between the collector and base, whilst the third subscript, "o", shows that the current passing to the third electrode is zero.
The leakage current in Fig. 4.2a is that of the collector/base diode and is therefore much smaller in the case of silicon transistors than in germanium devices.

The common emitter leakage current is measured with the base open circuited as shown in Fig. 4.2b. It is normally given the symbol $I_{\text {ceo }}$, but is sometimes designated $I_{c o}$.
The value of the common emitter leakage current is much larger than that of the common base leakage current. The leakage current of the collector/base diode acts as the base current and is therefore amplified by the current gain of the transistor concerned.
In a germanium transistor $I_{\text {ceo }}$ may be some hundreds of microamperes, increasing slightly with applied voltage over the working range of the transistor.

The leakage current of any transistor increases rapidly with temperature for the same
reason that the leakage current of a diode increases with temperature.

## PNP TRANSISTORS

The principles of operation of $p n p$ transistors are exactly similar to those of $n p n$ transistors, but the polarities of the applied voltages are reversed and the charge carriers are of the opposite polarity.
As shown in Fig. 4.3, the base is forward biased with respect to the emitter, so in this type of transistor the base must receive a negative bias (as opposed to the positive base bias of the npn type). Similarly, a negative voltage is applied to the collector so that the collector/ base junction is reverse biased.

The $n$-type base is lightly doped, so the emitter/base current consists mainly of holes moving from the emitter to the base with only a few electrons moving in the opposite direction.

Most of the holes passing from the emitter into the base reach the depletion region of the collector/base junction and they are then swept into the collector to form the collector current in the external circuit.


Fig. 4.3. Flow of charge carriers in the $p n p$ transistor.

## SYMBOLS

The normal symbol for an $n p n$ transistor is shown in Fig. 4.4a. Sometimes the circle is omitted for simplicity, since it is only used to indicate that the device is sealed in a suitable encapsulation.

The direction of the arrow shows the direction in which conventional current flows in the emitter circuit. (Conventional current flows from the positive to the negative terminal of a
battery in the opposite direction to the flow of electrons.)

Fig. 4.4b shows the symbol used for a $p n p$ transistor. It is similar to that of the $n p n$ transistor, except that the direction of the arrow is changed.

Alternative symbols for the $n p n$ and $p n p$ transistors are shown in Figs. 4.4c and 4.4d respectively.


Fig. 4.4. Symbols for $n p n$ and $p n p$ transistors.

## baSE VOLTAGES

The forward bias applied to the base of a silicon $n p n$ transistor results in this electrode being about 0.5 to 0.6 V positive with respect to the emitter.

This follows from the fact that a forward biased silicon diode does not pass very much current until this forward voltage is reached, but the current then increases very rapidly with forward voltage (refer to Fig. 2.8 in Semiconductors Part 2).

Similarly, the base of a germanium $n p n$ transistor operates at about 0.15 V positive with respect to the emitter.

The base operating voltages of silicon and germanium pnp transistors are about -0.5 to -0.6 V and about -0.15 V respectively relative to the emitter.

## COLLECTOR VOLTAGES

If the collector of a transistor is operated from too low a supply voltage, the maximum outpu: voltage swing will be limited and the gain may be reduced. Generally, supply voltages below about 3 V are seldom used. The upper limit depends on the type of transistor used for the reasons discussed below.

Some silicon transistors are designed to operate with collector voltages well above 100 volts, but most types are only capable of satisfactory operation at lower voltages.

Germanium pnp transistors are seldom
designed to operate with their collector voltages more than 80 V negative with respect to their emitter voltage.
If the collector/base voltage is made greater than the maximum permissible value quoted in the manufacturer's data sheet, avalanche breakdown of the collector/base junction may occur. (The doping level in transistors is usually greater than that at which true Zener breakdown takes place.)

A maximum permissible value of the collector/base reverse voltage, $V_{\text {cbo }}$ (or, sometimes, $V_{c b}$ ), is therefore quoted in the data sheet. This is the collector/base maximum voltage when the emitter current is zero.

The maximum permissible collector/emitter voltage with the base open circuited (that is, with zero base current) is designated $V_{\text {ceo }}$ and is often lower than $V_{\text {cbo }}$, since the collector/base leakage current is multiplied by the current gain of the transistor.

In addition to normal avalanche breakdown, an effect known as second breakdown can occur in which some parts of the junction become hotter than others. If any part tends to become hot, conduction in that part may become more like conduction in a metal, so that the current concentrates there and makes it hotter still.

A voltage applied between the collector and emitter (but not between the collector and base) can lead to an effect known as punch-through.

In this case the collector/base depletion region becomes so deep that it encompasses the whole of the base region and enters the emitter. When this occurs, a large current can flow between the collector and emitter.

The punch-through voltage depends mainly on the base width and resistivity; in many transistors the punch-through voltage is arranged to be of the same order as the avalanche breakdown voltage of the collector/ base junction.

Although avalanche breakdown and punch through do not in themselves destroy the transistor, in most circuits they would cause such a high current to flow that the power dissipation in the device would be great enough to destroy it. The manufacturer's limiting values of $V_{\text {ebo }}$ and $V_{\text {cbo }}$ should therefore be strictly observed.

## FREQUENCY LIMITS

The amplification given by a transistor falls off at high frequencies, the symbol $f_{T}$ is used as a meaure of this fall in modern transistors; it is the gain-bandwidth product or, more precisely, the common emitter current gain multiplied by the bandwidth measured in the frequency region where the gain is falling fairly rapidly.
It must be stressed, however, that the high frequency performance is dependent on the circuit in which the transistor is used as well as on the properties of the transistor itself.

It is not always wise to use a transistor with a good high frequency performance in a circuit where this property is not really needed, since oscillation at a very high frequency may occur. The latter may not be easy to detect.
It should be remembered that the value of $f_{\mathrm{T}}$ quoted by most manufacturers is the minimum value and many specimens of their transistors of a specified type number may have a far higher value of $f_{\mathrm{r}}$.

## TRANSISTOR TYPES

The number of transistor types on the market is extremely large. It is obviously necessary to have many different types available for various purposes but the profusion of type numbers now available tends to confuse not only the beginner, but also the somewhat more experienced designer.
This series will give some information on the ways in which some types of transistor provide the characteristics required by the circuit designer, but it is obvious that this account cannot be a comprehensive review or even cover the majority of the types in normal use. In general only the more common types will be considered and no attempt will be made to include details of transistors suitable for operation at $\mathrm{GHz}(1,000$ million Hz ) frequencies or of any radio frequency power transistors.


Photograph showing some of the various transistors available:
(a) AD149 (b) BC107 (c) OC72 (d) AC128 (e) AD161
(f) BD201 (g) BC147-Lockfit.
(Mullard)

## TOLERANCES

Manufacturers can produce cheap transistors only if they can sell huge quantities of each type and if they do not have to carry out long testing procedures or guarantee that their products have very close tolerances.

The most expensive devices have tended to be used in the military and space research fields where human lives may depend on the satisfactory operation of a large number of devices over a long period.

Somewhat cheaper transistors have been used for general industrial purposes and in instrument manufacture, whilst the cheapest devices are used in the domestic entertainment field where wide tolerances are of no great disadvantage if one allows for them in the circuit design.

## REPLACEMENT TYPES

Although this article may help readers to choose a suitable replacement type for a defective transistor, it cannot be stressed too strongly that the manufacturer's data sheet should always be examined in detail before any transistor is used to replace another type or is used in a new circuit.

In many cases modern epoxy encapsulated silicon transistors can be used as a cheap (but perfectly satisfactory) replacement for some of the types supplied in metal cans. Epoxy encapsulation is a kind of plastic material and can be used for silicon (but not normally germanium) device manufacture.

Germanium devices were developed before the more modern silicon types and will therefore be covered first.

## PNP ALLOY JUNCTION GERMANIUM TYPES

Some of the earliest transistors were produced by the alloy junction process. If a $p n p$ ger-
manium transistor is to be made, pellets of the $p$-type additive are placed on each side of a wafer of lightly doped $n$-type material.

In the case of the 0C71 transistor, for example, the size of the $n$-type wafer is $4 \times 2 \times$ 0.12 mm .

After suitable heat treatment, the $p$-type additive diffuses into the wafer to form a pnp device with a lightly doped base. The cross section of such a transistor is shown in Fig. 4.5.


Fig. 4.5. The structure of an alloy junction transistor.

Transistors manufactured by this technique are suitable for use only at audio and low radio frequencies. For example, the $p n p$ audio frequency transistor type OC7l has a typical common emitter cut off frequency of 11 kHz (minimum 5 kHz ) and a common base cut off frequency of 600 kHz .

The pnp OC45 has a thinner base and can be used as a 475 kHz intermediate frequency amplifier in radio receivers, since the thinner base raises its common base cut off frequency to about 6 MHz .

The pnp OC44 has about the optimum high frequency performance possible with transistors manufactured by the alloy junction technique; it has a common base cut off frequency of typically 15 MHz (minimum $7 \cdot 5 \mathrm{MHz}$ ) and is often used as a self oscillating mixer in radio receivers for the medium and long wavebands. Various other types, such as the OC42, are similar to the OC44.

Table 4.1: Germanium Alloy Junction Transistors

| Device | $V_{\text {cbo }}$ <br> (V) | $\begin{aligned} & V_{\text {ceo }} \\ & (V) \end{aligned}$ | $\begin{aligned} & I_{c_{\text {max }}} \\ & \left(\mathrm{mAA}^{2}\right. \end{aligned}$ | $\begin{aligned} & \mathbf{P}_{1} \max \\ & \left(\mathbf{M W}^{2}\right) \end{aligned}$ | $\mathrm{h}_{\text {fe }}$ | $\begin{gathered} \mathbf{f}_{\mathrm{T}} \\ (\mathrm{MHz}) \end{gathered}$ | Application |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| pnp |  |  |  |  |  |  |  |
| OC71 | -30 | -20 | 10 | 75 | 50 | $0.6$ | Medium gain general purpose |
| OC75 | -20 | -20 | 10 | 75 | $90$ | $0 \cdot 6$ | High gain general purpose |
| OC45 | -10 | -10 | $5 \cdot 0$ | 43 | 50 | $6 \cdot 0$ | I.F. amplifier in medium frequency receivers |
| OC44 | -10 | -10 | $5 \cdot 0$ | 43 | 100 | 15 | Mixer/oscillator in medium łrequency receivers |
| OC72 | -16 | -16 | 125 | 75 | 70 | $>0.35$ | Low power output transistor |
| OC77 | -60 | -60 | 125 | 75 | $>45$ | $>0.35$ | High woltage low power switch |
| 2N1309 | -30 | -15 | 200 | 150 | 60-120 | 15 | General purpose |
| npn |  |  |  |  |  |  |  |
| OC139 | 20 | 15 | 250 | 145 | 20-84 | $3 \cdot 5$ |  |
| OC140 | 20 | 15 | 400 | 145 | 20-150 | $4 \cdot 5$ | Medium current transistors |
| OC141 | 20 | 15 | 400 | 145 | 80-200 | $9 \cdot 0$ |  |
| 2N1308 | 25 | 15 | 200 | 150 | 80-300 | 15 | General purpose |

Returning to audio transistors, the 0C71 has a common emitter current gain of 30 to 75 at a collector current of 3 mA . The OC75 is a high gain version with a current gain $h_{\text {fr }}$ or $\beta$ of 60 to 130 at a collector current of 3 mA .

The 0C71 has a collector voltage rating of 20 V , but the thinner base of the OC44 and OC45 involves a reduction of the collector rating to 10 V .

All of the above types except the OC42 are encapsulated in a small, black painted, glass tube with the three leads emerging from the one end, as shown in Fig. 4.6.


Fig. 4.6. The OC71 type transistor showing stages of production.
(Mullard)


Fig. 4.7. The OC72 type transistor.
The $0 C 71$ is rated at a maximum average collector current of 10 mA . The $0 C 72$ has a maximum average collector current rating of 125 mA and has been much used in the past in the output stages of small radio receivers. It is encapsulated in a metal tube, as shown in Fig. 4.7, so that the heat will be conducted away if it is placed in a small heat sink.

The 0C77 is essentially a high voltage version of the OC72.

Low noise types, such as the ACl 07 , are available, but one can obtain a better low noise performance with a modern silicon planar type.

## PNP ALLOY DIFFUSED GERMANIUM

The pnp alloy diffused germanium transistors have been widely used in the radio and inter-
mediate frequency sections of radio receivers.
A cross section of such a transistor is shown in Fig. 4.8.

The manufacturing technique employed enables a base width of a few thousandths of a millimetre to be obtained. A drift field is developed by adding both $n$ - and $p$-type impurities to the emitter pellet and allowing the $n$-type material to penetrate more deeply into the crystal than the $p$-type at a high temperature so that a graded base layer is formed.

Such transistors have a high gain at a low collector current and a low collector base feedback capacitance.


Fig. 4.8. The structure of an alloy diffused germanium transistor.

The 0 Cl 170 and OCl 17 are two well known types manufactured by this technique. They have an $h_{\text {f. }}$ value of about 100 (minimum 20) and a cut off frequency of around 70 MHz .

In current radio receivers these transistors have been repiaced by the AF114 to AF117 series. The AF114 is a v.h.f. amplifier for f.m. receivers, the AF115 a mixer/oscillator for a.m./f.m. and short wave receivers, the AF116 an i.f. amplifier for f.m. receivers and the AF117 a mixer/ oscillator and i.f. amplifier for the long, medium and short wave bands.

Another use for alloy diffused transistors is as video amplifiers in television receivers and the AF118 has been designed especially for this purpose.

All of the alloy diffused transistors mentioned above have the type of construction shown in Fig. 4.9. The shield electrode is connected to the metal case and should be earthed.

Alloy diffused $n p n$ germanium transistors do not appear to be available.


Fig. 4.9. The OC170 and OC171 types of transistor.
Next month: Moie types, manufacture of planar devices and testing.


T he initial purchase of model train equipment is often in the form of a "set" with train, track and a plastic battery box fitted with an on-off-reverse switch only.

The absence of any form of speed control and the expense of frequent battery replacement soon leads to the acquisition of some form of resistive controller and, either a proprietary mains transformer/rectifier unit, or a battery charger.

Those with a little know-how elect to construct their own mains supply unit using a heavy duty variable resistance of $100-200$ ohm as the controller. Only a little experience is needed to show that a variable resistance controller is not really satisfactory and to counter the effects of uneven running, indeterminate starting, etc., the enthusiast begins to consider the purchase of an electronic control unit.

This article details the construction of an electronic speed control incorporating short circuit protection and a facility for automatically giving a gradual and realistic speed change to stop and start at signals and stations.

POWER SUPPLY
The unit operates fromi an approximate 12 V reasonably smooth d.c. supply. If such a supply is not readily available the novice is strongly advised to purchase a proprietary unit or to obtain expert help in building a mains transformer/rectifier unit since it is vital that safety requirements are met and that children cannot gain access to high voltages.

The transformer rating should be approximately 14 V a.c. at 2 amps , though it is well to consider the advantage of a slightly more expensive one rated at 4 amps preferably with two sets of windings to provide tivo independent


BY A. J. DUNN

Gives realistic performance to your electric model train
d.c. supplies and ample unrectified a.c. for electric point operation, lamps, etc.

A smoothed supply is essential.
Many proprietary units have no smoothing since the action of the train's motor is to average out the waveform. If such a supply unit is available it may be used if an electrolytic capacitor of approximately $2000 \mu \mathrm{~F}$ is connected across its terminals.

The working voltage of such a capacitor should be at least 20 V since it will charge up to the peak value when not connected to a load; when on load the voltage will fall to a lower voltage with a waveform as in Fig. 1.


Fig. 1. Shows the voltage increase for no load condition.

Such a smoothing capacitor will take a momentary large charging current, possibly in excess of a fitted current trip. In such a case the trip should be wired after the supply has been smoothed. Should it be intended to use an unprotected d.c. supply other than for the short circuit protected circuit to be described, it would be necessary to provide a means of short time constant overload protection such as a quick acting magnetic cut out. Similarly, any a.c. output could be protected by a thermal cut out.

## DESIGN REQUIREMENT

The starting performance of a loco is a common source of dissatisfaction; unless the resistive controller is well advanced it is often found that the loco will not move at all and then it suddenly speeds up, requiring immediate controller adjustment to avoid excess speed at points, curves, etc.

This effect is comparable to attempting to start off and drive a car in top gear; obviously the equivalent of a gear box is required, or a means to change the torque/speed characteristic.

In this design, this effect is achieved by switching the supply on and off at a fast rate; the ratio of the time it is switched on to the time it is switched off (the mark-space ratio) is varied by a control so that the extreme ends of the control range corresponds to the supply being virtually fully on or off.

In the condition of starting from rest, the supply is switched on for brief periods only (Fig. 2a), each period being long enough to develop the maximum torque from the motor but not long enough to allow for much movement so the loco moves in a series of almost undetect-


Fig. 2. Shows that the average value is proportional to the mark-space ratio.
able jerks, slowly increasing speed.
In the half-way position, the controller creates an equal mark-space ratio or on for half the time (Fig. 2b) and the inertia of the motor integrates this and runs as if powered by half the supply volts.

In the fast position the controller switches the supply on for most of the time (see Fig. 2c) and the loco rail voltage is therefore the supply voltage ( $12-14 \mathrm{~V}$ d.c.) less a $0 \cdot 7 \mathrm{~V}$ drop across TR 1 and less the small voltage drop across R6 dependent upon the current taken.

## TRAIN MOTOR

Consider the loco motor as shown in Fig. 3 here the resistance of the motor windings is shown as $R_{\mathrm{m}}$ in series with a generator-this being the back e.m.f. generator with an output proportional to speed.

At rest, when the supply is connected, the current that flows is the supply voltage $V_{n}$ divided by $R_{\mathrm{m}}$ plus the control resistance $R_{\mathrm{c}}$ (including the supply resistances). The torque caused by the current causes the motor to revolve and overcome initial or static friction whereupon the motor runs faster and the back e.m.f. increases..

The current taken is now

$$
\frac{V_{\mathrm{s}}-V_{\mathrm{g}}}{R_{\mathrm{c}}+R_{\mathrm{m}}}
$$



Fig. 3. The equivalent circuit of the loco motor in circuit.
and the torque is reduced accordingly. It is obvious that if $V_{\mathrm{s}}$ and $R_{\mathrm{c}}$ are both made very large and constant (normal constant current circuit) the motor speed will vary as a function of the load and, in cases of indeterminate frictional effects, will vary wildly.

From this consideration, the series resistance should be reduced as far as possible and the motor speed controlled by either a variable voltage low impedance source or by a fixed voltage and switched time division.

## CIRCUIT

The complete circuit diagram of the train controller is shown in Fig. 4. Transistors TRA and TRB (inside the integrated circuit) form a multivibrator whose period is determined by the values of the capacitors C1, C2, R1 and (R2+ VR1). The mark-space ratio is approximately $1: 1$ with the wiper of VR1 in the central position, and the collector of TRB (pin 5) is alternately at the supply voltage or approximately +0.2 V when TRB is turned on hard or saturated. This square wave signal is applied via R4 to TRC which is switched on or off.

For the moment leaving aside transistor TRD, the collector of TRC is connected to the base of TRE which forms, with TR1, a compound emitter follower giving a large current low impedance square wave output.

Diode D2 is wired in the circuit, reverse
biased, to protect TRl from transient reverse voltage produced by the inductance of the motor winding and commutator switching.

## SHORT CIRCUIT PROTECTION

Short circuit protection is provided by the use of R6 (approximately 0.5 ohm ), the connections to TRD being so arranged that if a current in excess of 1.5 amps flows through R6, the voltage across it will turn on TRD.

The base current of TRD is limited by R7, but it will saturate and the collector of TRD will fall to approximately +0.2 V pulling down the base of TRE and virtually turning off TR1.

Accidental short circuits are thereby limited to approximately 1.5 mpss though this figure may be readily changed by changing R6 such that,
(short circuit current in amps) $\times($ R6 in ohms $)$

$$
\bumpeq 0.7 \mathrm{~V} .
$$

## AUTOMATIC CONTROL

Automatic control is achieved by replacing R7 with D1, C3 and R8 as shown in Fig. 4.

Consider first that S2 is open: if a short circuit is applied to the output, the voltage across R6 will be applied via D1 to the base of TRD. The voltage that must be produced across R6 to saturate TRD is now approximately 1.4 V made up of 0.7 V to turn on D1, and 0.7 V the voltage dropped across the base/emitter junction of TR1.

Fig. 4. The complete circuit diagram of the Train Controller.


# TRAN CONTROLLER 



Fig. 8 (below). Details of the heatsink bracket for securing TR1. Mica washer and insulating bushes must be used.


Fig. 7 (above). The layout of the components on the top side of the printed circuit board. Note the polarity of the diodes and the integrated circuit.

The value of R6 should be selected accordingly.
Assume that the control VRl is adjusted centrally to give a $1: 1$ mark-space ratio and that a train is running to a signal set at stop.
If S 2 is closed, C3 will charge slowly via R8. The time constant of C3, R8 is given by t (secs) $=(\mathrm{R} 8$ in ohms $) \times(\mathrm{C} 3$ in farads $)$
With R8 at 100 kilohm this gives $\mathrm{t}=10$ secs.
However, this corresponds to approximately 60 per cent of the charge voltage, or 7 V from a 12 V supply and only approimately 1 V is necessary to operate TRD. The relationship between time and charge is approximately linear so IV will be obtained in one-seventh of the time for 7 V or $10 / 7 \operatorname{secs} \bumpeq 1^{1}{ }_{2}$ secs.
As C3 charges, TRD will gradually pass more current, limiting the pulses from TR1 and after $1^{1}{ }_{2}$ seconds TR1 will be cut off and the train stopped.

Consider now that the signal aspect is changed and that by the use of a parallel switch or a relay, S2 is opened. The charge on C3 cannot pass via DI (reverse biased) and so must dissipate by providing the base current to TRD. As the charge on C3 falls, so the current taken by TRD falls and output pulses from TR1 increase and start the train. After a short period C 3 is virtually discharged and the train runs as in the original condition.

## PRINTED CIRCUIT BOARD

The unit is to be constructed on a piece of printed circuit board the full-size drawing of which is shown in Fig. 5. The component layout on the top side of the board is shown in Fig. 6. the only critical positioning being the holes for VR1 and the integrated circuit, ICI via its holder.

Note that R7 is shown (dotted) for initial testing; automatic control is obtained (if desired) by replacing R7 after testing with D1 and C3 wired as shown.


Fig. 5. The full-size master of the printed circuit.

## CONSTRUCTION

The printed circuit board should be produced as described in the article Making Printed Circuit Boards, E.E. June 1973.

When the board is ready, drill all the holes with a No. $62-68$ drill bit and then enlarge the holes to take the potentiometer VR1 with a larger drill or small file so that a snug fit is
obtained.
Next solder VR1, the i.c. holder, the resistors and capacitors in position as indicated in Fig. 6. If the automatic control is to be installed leave the leads of R7 long for easy removal later. When this has been done plug in 1 Cl ensuring that it is the correct way round; this is done with reference to the notch at one end of the integrated circuit.

Next make the aluminium heatsink bracket as shown in Fig. 8 for the power transistor TR1 and fix the latter to the bracket via a mica washer and insulating bushes.

Secure the solder tag to the case of TRI via one of its fixing bolts; this is the connection to the collector of TR1 since the casing is internally connected to the collector.

Put some heatsink compound on the bracket where it is to be in contact with the diecast case and tightly bolt the bracket in position.

Fix the other components to the case and wire up as shown in Fig. 9.

## Components....



Printed circuit board, size $58 \times 32 \mathrm{~mm}$; etchant -ferric chloride; diecast aluminium case or similar metal case; knob; 16 s.w.g. aluminium; mica washer and bushes for TR1; 14 pin dual-in-line socket.

## TESTING

The board should be carefully examined to ensure that the components have been wired up correctly paying particular attention to the polarity of D2 and the wiring to TR1.

Check for short circuits, solder bridges, etc., and that the polarity of the supply is correct.
falls towards zero-and this encourages more current to flow in from the emitter which again makes $R_{\mathrm{b} 1}$ reduce in value. We have, in effect, a sort of positive feedback reaction. The current flowing into the emitter flows out of Cl and the potential at $B$ falls rapidly towards zero. When it reaches almost zero the inflow of current reduces and the resistance of $R_{\mathrm{bl}}$ rises back to its original level; the diode again becomes reverse biased and Cl is free to charge up again.

## OUTPUTS

The nice thing about a unijunction oscillator is that we have two possible waveforms at our disposal; one approaching a sawtooth at point $B$


Fig. 10.3. Practical circuit used to demonstrate the operation of the unijunction oscillator. Alteration of C1 varies the frequency, as does VR4 or PCC1, whichever is in circuit. Potentiometer VR1 will also alter the frequency but this will affect the amplitude of the output.

Fig. 10.4. The circuit of Fig. 10.3 wired up on the Demo Deck.


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## EXPERIMENTAL CIRCUIT

The experiment-shown in Fig. 10.3 will operate very slowly (several seconds per cycle) if Cl is made to be $50 \mu \mathrm{~F}$ and thus it is possible to monitor the exponential waveform at the emitter on the 1 mA meter movement of the Demo Deck. Alternatively insert a lower value capacitor (two alternative values are suggested) and listen to the sound on Demo Deck's loudspeaker. Fig. 10.4 shows the experimental circuit with audible and visual monitoring wired up on the Demo Deck.

Potentiometer VR1 is included to alter the quiescent potential at the point originally called A. Start with VR1 set with the wiper nearest the positive supply rail and then reduce this voltage by turning the potentiometer down; the
frequency of the oscillator will increase because the level to which the capacitor has to charge is being reduced-the amplitude of the signal will, however, reduce. Adjustment of VR4 will modify the frequency over a very wide range without altering the amplitude.

Substitute PCCl for VR4 and it is possible to make a light controiled oscillator-the basis for an interesting musical instrument if you shade the cell with your hands! An interesting feature of the unijunction is that bl can be interchanged for b2 and the device will still work, but this will be turning the intrinsic stand off ratio on its head and the amplitude of signal will be nothing like as great-try it and see!

Next part: The Hartley Oscillator


B
ecause the electronic component industry is booming private constructors are having difficulty in obtaining some components. It sounds stupid but it's true, the manufacturers have trouble in keeping up with the demands of industry and very often cannot supply the smaller customer. At the present time a number of capacitors are difficult to get and we know some firms have been quoted delivery times months away.

Unfortunately there is nothing that either we or the retailer can do about this situation other than be aware of it and try to help you overcome the problems by finding alternative components. So don't always blame the shop-
keeper-remember that in this business he is at the bottom of a very long list when it comes to supply deliveries from the big companies.

## Personal Receiver

The Personal Receiver is likely to fall foul of the problems mentioned above-two of the capacitors may be difficult to get (C3 $0 \cdot 1 \mu \mathrm{~F}$ and $\mathrm{C} 40.05 \mu \mathrm{~F}$, miniature) to overcome these problems we have given an alternative for $\mathrm{C} 3(0.22 \mu \mathrm{~F})$ and we suggest that you use the receiver without C4 until this can be purchased. This will result in some loss of volume as the audio signal will have to pass through R5 instead of being decoupled by C4 but the receiver will work quite well like this.

A marked and drilled printed circuit board for the receiver is available from Valance Electronics, 2A Canel St., Droglesden, Manchester. We believe this firm may also be able to supply the plastic case used.

Finally, remember that this project is fairly small and all the components used should be miniature or very small types as listed in the components box.

## Train Controller

It seems strange that this issue contains two projects which use integrated circuits, perhaps it's a sign of the times--no doubt these devices will be feazured more and more in our projects as
the months go by. We suggest that you use a socket for mounting the ic. in the Train Controller so that this can be soldered in without fear of damage to the i.c.

The electrolytic capacitor used should be a printed circuit type and the right size component is available from Electrovalue, 28 St . Judes Fioad, Englefield Green, Egham, Surrey.

It is mentioned in the text that a metal case should be used as this forms a heat sink for the power transistor. Diecast boxes of the appropriate size are available and should make excellent cases for this project. If you pa.nt the case remember that darker colours dissipate the heat better.

## Aquarium Thermostat

We had better not praise the Aquarium Thermostat too much, someone might notice who wrote the article! In fact, it is difficult to say much about it since most of the components are generally available. The transformer should be available from most electrical shops or Woolworths. The thermistor can be obtained from most of the larger suppliers, while the relay is available from G. W. Smith should other sources fail.

The heater used with the prototype was a standard one sold for aquarium use. Incidentally, too large a neater (wattage size that is) will result in a poor constant temperature.


## Bulb Resistance

I measured the resistance of a $6 \mathrm{~V}, 0.04 \mathrm{~A}$ bulb and was surprised to see it was much lower than expected. To pass 40 mA with 6 V applied, it should have a resistance of $\frac{6}{0.04}=150 \mathrm{ohm}$ but mine was round about 80 ohm. Is this a "rogue" lamp?

No. The tungsten filament in the bulb has what is called a "positive temperature coefficient of resistance". This means that when it is cold it has a lower resistance than when hot. The current stated for the bulb is that which it draws when it has got up to its working temperature-well over 1,000 degrees Centigrade.

## Screening

Could you explain-in simple terms-how a screened lead pre. vents hum pick up?

Hum pick up is often caused by capacitive coupling between a wire and mains wiring in the same area. If you surround the wire in question with a shield (the screen) capacitive coupling will be between the mains lead and this screen. If the latter is connected to ground the potential of the screen remains constant and the capacitively induced current runs straight to ground. According to Faraday (his ice pail experiment) no charge can be induced on a totally enclosed body and as the conductor wire
is now totally enclosed by the screen it will pick up no hum.

## Output Stage

In the days of valves we had to drive loudspeakers with trans. formers but it seems as though this is not necessary with transistors. Why is this so?

Valves operated by controlling quite high voltages at small currents while loudspeakers - because of their low coil resistances need high current at quite low voltages. If you assume that there is conservation of power between input and output of a transformer it is an excellent device for converting from high voltage swings at low current to low voltage swings at high current. This is why they are used in valve circuits.

On the other hand transistors are basically current controllers and consequently are able to handle low voltages at reasonable currents directly and there is no need to use transformers in most cases. It is, of course, highly desirable to remove transformers from circuits because they are bulky and are never perfectly efficient: they also introduce a degree of distortion that had to be overcome with quite complicated circuitry in the old valve days.

## Smoothing

In the old days I used to use chokes for smoothing but never see these in modern equipment. Are they not as good as the modern approach-which seems to use a resistor?

The resistor between the two capacitors in a smoothing circuit is not as good as the "old fashioned" choke because it is inefficient (wastes power) and the smoothing effect is not so good.
However, these days when we use transistors in most equipment the current that is drawn from the power supply tends to be very high (compared with that taken by equivalent valve circuitry) and to prevent the core of the choke becoming "saturated" it would be necessary to have a large amount of iron. Not only this but the windings would have to be of stouter wire to carry the higher current. Consequently chokes would be very expensive and far too cumbersome in modern systems. One
of the sacrifices in quality we have to make for the convenience of modern living?

## Wiring Layout

Why is it that some of your articles say "layout" is important? Surely a wire is a wire and provided it goes to the right placeirrespective of position-then all is correct.

Layout is not always important but in some cases it is. More particularly when the circuit is dealing with high frequencies. All connecting wire-even if it is straight-has a small amount of inductance. This can modify the tuning of radios and introduce reactance where it is not wanted.

There is always a degree of capacitance between a wire and neighbouring components-it may only be small but at very high frequencies this small capacitance can transmit small a.c. currents. These currents might cause positive feedback-making the circuit oscillate-or negative feedback which reduces the gain of the system. You can also get inductive coupling.

In a.c. circuits it is good practice to keep wire lengths as short as possible and to separate input circuits from output circuits. Sometimes neat "loomed" wiring makes matters worse because the bundling together of the wires makes the inter-wire capacitive coupling greater. Generally speaking there are no problems with simple d.c. and logic circuits unless they are operating at very high speeds.

"But dad, the article in here says it's so simple to strip down that even a child could do it."

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#### Abstract

"In published circuits a volume control is sometimes connected as in Fig. la, with the input to the slider, and sometimes as in Fig. lb, with the output from the slider. Which method of connection is correct?"


The short answer is: when the output from the volume control is connected to a low impedance load, use Fig. la. For high impedance load, use Fig. lb.

The essential point is that a volume control doesn't exist in isolation. The way it works in a practical circuit depends on what comes before it and what goes after it. Disregard this simple fact and you may end up with a control which has no effect as it is turned until the slider is very nearly at the end of the track, whereupon the volume suddenly changes from minimum to maximum. What's known to the trade as a "fierce" control.

## ENDS AND MEANS

The circuit of Fig. 2a is a case in point. With the slider at the start (s) of the track, the signal (here 1 volt from a source of 100 ohms) is shorted, so the output is zero-the output in this case being the voltage which appears across the 1 megohm load resistance. With the slider at the finish ( $f$ ) of the track, the signal source is connected to the total resistance of the track (100 kilohms) in parallel with the load ( $1<$ megohm ), i.e. about 90 kilohms.

When current flows, only a small amount of the 1 volt signal is lost in the signal-source's own internal impedance of 100 ohms (it might be a 100 ohm micro.


Fig. 1. Two common ways of connecting a volume control.
phone, for instance) and practically the whole 1 volt appears across the load $R_{\mathrm{L}}$. In a word, volume is maximum.
So the volume is zero with the slider at $s$ and maximum with the slider at $f$. This is alright if you only want to operate your equipment at maximum volume, but not for intermediate settings.

## CALCULATE

First, calculate, or at any rate get a rough idea of the current through the load when tne slider is at $f$. As we saw, the voltage across the load is almost 1 volt, so 1 micramp flows. Now move the slider back to the bottom (s) of the track and then adjust it so that there's just 1 kilohm between slider and earth. What current flows?
Well. obviously the current from the source divides at the slider, part flowing up and through the load and part down to earth. But since there's nearly 1100 kilohm in the upper path ( 1 megohm plus 100 kilohm) and only 1 K in the lower, we can safely say that the lower path has the controlling effect and forget about the upper.

For practical purposes, the signal "sees" a load of its own 100 ohms plus the 1 kilohm between slider and earth: in other words, the total resistance is 1100 ohms, which with 1 volt gives a current of 0.9 milliamps


Fig. 2. Fierce ( a and c ) and gentle ( $b$ and d) volume controls.

## REiviember TO USE THE POSTCOLE Readers Letters

## Simplified

Would it be possible to give me a brief description of the Demo Deck as I unfortunately missed that particular issue. I am now taking EE regularly, and I find it more suitable at my age (I am 75 yrs old), having started back in the old cat whisker days. 1 find the other publications a bit too complicated but interesting, what with all this hifi etc.. which is a vast improvement on the old methods of valves and corner wall baffles etc. The explanations in EE are also much plainer, this must suit the younger people
also, making it easier to grasp. The gadgets for the home are a great attraction for experimenting with, and your simple circuits require less time to make. Hoping you will carry on providing even more simplified versions.
E. Skidmore

Birmingham.
The Demo Deck will no longer feature in our pages. It has been used since December '71 and can still be used by readers for experimenting. The new beginners series Teach-In '74 will not be based on the Demo Deck.

## Radio Amateurs

I write to ask that a brief item be inserted in Everyday Elec. tronics re. the amateur radio course run by the Northumberland County Education Dept., at Gosforth, very near to Newcastle upon Tyne.
The course to prepare students for the R.A.E. (Radio Amateurs Examination) in May/June 1974 will be run at the Grammar School, Gosforth, Northumberland, commencing in September 1973.

Held on Tuesday/Wednesday of each week from 7 pm to 9 pm . candidates may sit the R.A.E. at the School.

Enquiries should be addressed to the Principle. Gosforth Grammar School, Northumberland, who will forward a prospectus. Or further information can be had by telephoning Gosforth 851000 .
I take the class and your cooperation in this matter would be appreciated.
D. R. Loveday.

Newcastle upon Tyne.


1 find etching p.c. (printed circuit) boards takes a long time, to speed up the process all that is needed are two match sticks. Make up the etchant in the usual way, but before putting the p.c. board in the etchant dish, put the two match sticks in, parallel but some distance apart. The board rests on the match sticks keeping it away from the bottom of the dish.
The dish can now and again be rocked gently to and fro, all the dissolved particles of copper fall to the bottom of the dish and fresh etchent can start to dissolve the rest of the copper away.

> J. Majchrowski.
> Ayr.

Having made nu nerous projects I always find that the front panel or fascia presents a problem with respect to labelling. Engraving and "silk screen printing" being very expensive for the home builder and Dymo labels not giving a suitable appearance. I think the method I have adopted might be of interest to many other readers.

The process is as follows:

1. Drill all holes and slots in the required positions.
2. Spray the panel the desired colour using an aerosol spray.
3. Add the lettering using Letraset or Magic Letters, these need no more than placing on the panel and rubbing with a ball point pen to transfer each letter to the panel. A sheet of graph paper suitably placed and tacked in position lightly with sellotape, helps in keeping letters in alignment.
4. When satisfied that all is correct, a sheet of clear self adhesive film (available at W. H. Smiths) is rolled onto the panel starting at one end and making sure no air bubbles are left. If, accidentally an air pocket is made do not attempt to pull the film of but carefully pierce the bubble with a pin and roll again from the edges of the bubble towards the pin hole. The edges of the film should be left large enough so that they can be turned over and stuck to the reverse side of the panel so that with use the edges will not curl.
The finished panel viewed from a foot or so cannot easily be distinguished from a panel which has been silk screen printed. The surface is easily cleaned with a damp cloth and gives projects the professional finish.

> A. Evans,
> Portsmouth.

## ALL PRICES SHOWN INCLUDE V.A.T.

## SWITCHES

Standard roegle awitches: $5 W 20$
5.P.S.T. 20 : $5 W 21$-DPD. 2540 . Miniature tosgle witcher: SW18Sliderawitches: SW3-D.P.D.T., Istp. Miniature puah butzon: SWI-5.P. 14 $\ddagger \mathrm{p}$.
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SWS-2 pole, 8 way.
SW6-3 pole. 4 way.
SW7-4 pole, 2 way
SW8-4 pole. 3 war

## GROOV-KLEEN

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#### Abstract

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lokg for low $40-16,000 \mathrm{~Hz}$. Output: 3-8-18 1 Power Supply 12 V 44.70 plus $24 p$

PANEL NEON INDICATORS 240 V
N1-Round, 9 mm diameser, 33 p . N3-Round, 18 mm diameter, $28+\mathrm{p}$

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34p.
Cassette rack with teak ends, holds 10 cassetres in library cases. 72p, plus 12p

## CONNECTING WIRE PACK

Contains 30 feet of stranded wire. colours per pack. I 1 p

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In plain aluminium, ideal for mixers.


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Coiled screened loads, 20 feet long \&l.os each.

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Car aerial
Co-axial
D.I.N. 2 pin (speaker)
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DIIN. 5 pin. $180^{\circ}$
DIIN 5 pin,
erases a whole reel of
lape in seconds. 240 V
C2.20, Flus instructions.

Jack, $2 \not \mathrm{~mm}^{6}$
Jack, $2 \not 2 \mathrm{~mm}$ unscreened
Jack, 3 mm screened
Jack, 34 mm unscreened
Jack, 3fmm screened
Jack, tin unscreene


SOCKETS
Jack, sereo. unsereened
Jack, stereo, screened
Phono, plastic top
Phono, plazed metal
Warider, red or black
LINE SOCKETS
Car aerial
Co-axial
D.i.N. 2 pin (apeaker)
D.I.N. $\frac{2}{3}$ pin
DI.N. 5 pin, 180
D.i.N. 5 pin, 240
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Jack, stereo, screened
Phono. plated mezal



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## Sinclair Project 60

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Such are the results of using a PZB Mk. 3 to drive iwo $Z .50 \mathrm{Mk} .2$ power amplifiers. Developed from the original 250 . the Mk 2 has improved thermal stability, better regulated D.C. limiting to ensure more symmetrical output voltage swing with sill less distortion at lower outputs and automatic transient overload protection. The PZ.8 Mk. 3 is the most advanced power supply unit ever to be made at a reasonable price. It cannot be damaged by direct shorting. nor witl it fall through overloading. because of an ingenious re-entrant current limiting principle used usually only in expensive laboratory equipment. Because output voltage is variable, the PZ8 Mk. 3 makes a worthwhile alternative where PZ 5 and PZ.6 are recommended for Project 60 applications. particularly since this most powerful of all Sinclair supply units can be operated from a smaller mains transformer. Together, the Z 50 Mk 2 and PZ8 Mk 3 provide new standards of performance and reliability and these modules are compatible with earlier types in the Project 60 range.
Z.50 Mk. 2 SPECIFICATIONS

Input impedance $100 \mathrm{~K} \Omega$
Input (for 30 w into 8 亿) 400 mV
Signal to noise ratio, referred to fult o/p at $30 v \mathrm{HT} 80 \mathrm{~dB}$ or better
Distortion $0.02 \%$ up to 20 W af 8 . .
See published curve
Frequency response 10 Hz to more than 200 KHzt 1 dB
Max. Supply voltage $45 v$ ( $4 \Omega$ to $8 \Omega$ speakers) ( 50 V 15 n speakers only)

Min. supply voltage 9 v
Load impedance - minimum: $4 \Omega$ at $45 v \mathrm{HT}$
Load impedance - maximum: safe on open circuit

C5.48- V.A
PZ.8 Mk. 3 SPECIFICATIONS
Nominal working output 45 V . Adjustable between 20 \& 50 V

Mains Transformer E5.98 + VA T. 59p


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| 12W. RMS continuous sine wave stereo amp. for average needs | $\begin{aligned} & 2 \times 2.50, \text { Stereo } \\ & 60: P \mathbf{Z . 5} \end{aligned}$ | Crystal, ceramic or mag. P.U., F.M. Tuner, etc. | $\begin{aligned} & £ 25.92 \\ & \text { VA } 59 \end{aligned}$ |
| 25W. RMS continuous sine wave stereo amp using low efficiency (high performance) speakers | $\begin{aligned} & 2 \times 2.50 . \text { Stareo } \\ & \text { 60;PZ. } 6 \end{aligned}$ | High quality ceramic or magnetic P.U. F.M Tuner, Tape Deck, etc | $\begin{aligned} & £ 28.92 \\ & \vee A T \\ & £ 289 \end{aligned}$ |
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POTENTIOMETERS gINOLES and DUAL 6K Log or 8K ${ }_{25 \mathrm{~K}}^{10 \mathrm{~K}}$ Lin Less ${ }_{20 \mathrm{~K}}^{10 \mathrm{~K}}$ Less 50K 12 pea, 500 K switch 250K Double 250 K 40 p . 500 K Pouble 300 K each

2 M Switch 2 M
$24 \mathrm{pea}, \quad 2$

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& \text { Sp. P. \& }
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 MULLARD POLYESTER CAPACITORS C296 SERIES


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MINIATURE ELECTROLYTIC MULLARD C426 SERIES (6p each) ( $\mu$ FIV) $1 / 63,4 / 40,8 / 40,10 / 40,10 / 64,16 / 40,20 / 64,25 / 25,32 / 10,40 / 16,64 / 10$ MULLARD C437: $(\mu \mathrm{F} / \mathrm{V})$ 64/64, 10p: $160 / 25$, $10 p ; 160 / 40,12 p ; 640 / 6 \cdot 4$ MOp; 1600/6.4, 16p.

ELECTROLYTIC CAPACITORS. Tubular and large can ( $4 F / V$ ) $2.5 / 50,3 p, 4 / 10,10 / 25,16 / 15,20 / 25,25 / 15,25 / 25,40 / 6,64 / 10,200 / 6$,
$250 / 10,5 p: 10 / 6,10 / 50,25 / 50,32 / 50,50 / 10,64 / 25,100 / 25,6 p ; 50 / 50,64 / 40$, $250 / 10,5 p ; 1 / 6$. $10 / 50,25 / 50,32 / 50,50 / 10,64 / 25,100 / 25,6 p ; 50 / 50,64 / 40$, 500/25, 11p: 500/50, 14p; 1,000/12. 11p; 1,000/25, 2.000/12, 2,500/12. $17 p$ $1.000 / 50,39 p ; 2,000 / 25,27 p ; 2,50025,31 p ; 2,500 / 50,62 p_{i}, 3,000 / 50,72 p$ $5,000 / 50,94 p ; 1,000 / 100,66 p ; 8 / 350,14 p ; 16 / 350,19 p: 32 / 350,25 p$.
50 V : (pF) $22,27,33,39,47,56,68,82,100,120,150,180,220,270,330,390$ 470, 560, 680, 820, IK, IK5, 2K2, 3K3, 4K7, 6K8. ( $\mu F$ ) $0.01,0.015,0.022$. $0.033,0 \cdot 047,2 \frac{1}{2} ; 0.1,30 \mathrm{~V} .4 \frac{4}{2} \mathrm{p}: 0.1 .100 \mathrm{~V}$, $5 \frac{1}{2} \mathrm{p}$.
CAREON FILM RESTSTORS $\ddagger W 5 \% 10 \mathrm{ohms}-2 \cdot 2 M .+W 5 \% 10 \mathrm{hms}-$ IM. In each or 100 for $62 p$ : 1,000 for 64.50.
METAL FILM RESISTORS IW $5 \% 10$ ohms-IOM. Ito each or 100 for K1-10. 55 EI2 KIT ( 15 each value 10 ohms-IOM) EB .

| Veroboard | 0.1 | 0.15 | IN4001 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $2+\times 5 \mathrm{Sin}$ | 28p | 28p | IN4002 |  | 5PEC |  | JLK |  |  |
| $21 \times 3$ in | 26p | 19p | 1N4003 |  | ARE |  | AIL |  |  |
| $3 \pm \times 5$ in | 32p | 33p | IN4004 |  |  | A | ON FO |  | GE |
| $3{ }^{3} \times 3$ in | 28p | 28p | IN914 | $7 p$ | PROIE |  | AND |  |  |
| 21 $\times$ lin | 7p | 7p | 46914 | 35p |  |  |  |  |  |
| $2 \mathrm{~F} \times \sin$ (plain) | - | $14 p$ | OC71 | 13 p |  |  | S.C.R. |  |  |
| $2 \mathrm{t} \times 31 \mathrm{in}$ (plain) |  | 12 p | $0 C 75$ | 17p | 100 V |  | 29p | 3 3A | 31p |
| $5 \times 3 \tan$ (plain) Insertion sool |  | 22p |  | 20p | 400 V |  | 50p | 3 3A | 40p 80 |
|  | 4.p | 44p |  |  |  |  |  |  |  |
| Pins. pkt. 25 | 10p | 10p | Twin sc |  | wire |  |  |  |  |
| pin DIN Plug. | 12 | Skt., | Stereo Connec | c. W | re, m. |  |  |  |  |
| $10 p .3$ pin DIN | Plug | 13p: | onnec | 1 c | wir |  | rs, |  |  |
| Sket. 10p. 5 pin | DIN | Plug, | Preset | eler | n pors | IK | M. |  |  |
| tor Equiv. |  |  |  |  | CES | CLU | DE |  |  |
| rbon | 2 M |  |  | V. | \& $P$. | OD | on ord |  | (5. |
| , single 16 | , | gle |  |  | (10 |  |  |  |  |
| with swirch 26p. | du | 46p. | Expore | roe | enaui | S | elcom |  | e) |
| Dept. E | E. |  | DINGT | ON | $\begin{aligned} & \text { ROA } \\ & \text { BED } \end{aligned}$ | $\boldsymbol{P}$ |  |  |  |
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| AAY42 | 160 | BC169C | 12p | BY100 | 150 | OCAS | 150 | V408A | 250 | 2N3440 | 750 |
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 Input 220／240V AC， | Nae $185 \times 85 \times$ |
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| 105 mmi. |
| 88 | PS． 200 REGULATED P．S．U．

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| pe SW． $100100 \times 80 \mathrm{~mm}$ | Typa MR．esp． 4 isin．$x$ tiln．fronts |  | Tyoe MR．38P．I 21／32in．square fronts |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| ${ }^{80-0-60 \mu A ~}$ |  | 100 mA A $\cdots \cdots$. |  | 300ma |
| ${ }_{1000-0-100 \mu \mathrm{~A}}^{100}$ |  |  |  | 500mA ．．．．48．45 |
| $800 \mu \mathrm{~A}$ ．．．${ }^{3}$ |  |  |  |  |
|  |  | 18 map．．．．． |  |  |
|  |  |  |  |  |
|  |  | 20V．D．C．${ }^{\text {ate }}$ |  | 10 amp．．．．．． 40.4 |
|  |  |  |  |  |
|  | sopa |  |  | 10V．D．C．．．29．4 |
|  |  | 18 V A．C．．．${ }^{\text {a }}$ |  |  |
| Type SD．830 $82.5 \mathrm{~mm} \times 110 \mathrm{~mm}$ Fronts |  | 200v．A．C．．．As．\％ | 100－0－100 1 A | 60V．D．c．．．${ }^{\text {a }}$ |
|  | 200 | 8 Metar 1 mA Es．e0 | $200 \mu \mathrm{~A}$ ．．．．erers | 100V．D．C． 40.4 |
| 50 mA ．．．． 88.10 |  | VU Metor．$\because 4.68$ |  | 150 V ．D．C． 4.85 |
| $\underline{1000 \mathrm{~mA}}$ |  |  | 800－0－600 1 Al A |  |
| ${ }^{5000 m A}$ | $1-0-1 \mathrm{~mA} . .588$ | 10 mmp ．A．C． | $\operatorname{lma}_{10-1 \mathrm{ma}} \times$ ．．． | ${ }_{750 \mathrm{~V} \text { ．D．C．}}$ |
| 5 emp．．．．．．．．\％${ }^{5} 10$ |  |  | 2 ma ．．．．．． 8 ．25 | 16V．A．C．．． 43.20 |
| 10 mpp．．．．．限10 |  | 80 mmp A．C．${ }^{\text {a }}$ at． 0 |  | 50V．A．C．．－ 4 － 80 |
| 8v．D．C．．．23．10 |  |  | $10 \mathrm{~mA} \mathrm{...}. \mathrm{28.2}$. | 160V．A．C．．．48－30 |
|  | Trde MR．52P． 21 in ．square fronts |  |  | 300 V ．A．C．．－ 28.30 |
| 100 A A ．．．． 29.25 20V．D．C．．． |  |  | 50 mA ．．．． | ${ }^{500 V}$ V．A．C．． 23.80 |
|  | $\begin{aligned} & 60 \mu \mathrm{~A} \\ & 80-0-00 \mu \mathrm{i} \end{aligned}$ |  |  |  |
|  |  |  |  | VU Moter ．．2seds |
| 1 ma ．．．．．． 43.10 300V．A．c．．． 81.20 | 100－0－100 $\mu \mathrm{A}$ 迷 | 300 V ．D．C． 88.50 |  |  |
| 5 mA ．．．．．83－10 VU meter ．． 88.50 |  | $18 \text { V.AC. . A }$ | Type MR．45P．2in．square fronts |  |
|  |  |  | A ．．．．．．，能 | 6 amp．．．．．．．es．40 |
| Type $50.64063 .5 \mathrm{~mm} \times 85 \mathrm{~mm}$ Fronts | 10 mA …． |  |  | 10V．D．C．．． 5 － 40 |
|  | 80ma … ater | 1 amp．A．C．－ 43.50 |  | 20V，D．C．．． 240 |
| ${ }^{5000}{ }_{50-0-50 \ldots}$ | 100ma … | 5 mmp A．C． AL 50 | 100－0－100 A A 8 E6 |  |
|  | 600ma … 5 Eso |  |  |  |
|  |  | 20 mmp ．A．C．${ }^{2}$ He 50 |  |  |
| $200 \mu \mathrm{~A}$ ．．．． 1800 bV．D．C．．． |  | $80 \mathrm{mmp}. \mathrm{A.C}. \mathrm{-}{ }^{\text {a }}$－ 50 | $\operatorname{lma}$ …… | －Meter lma |
| $500 \mathrm{\mu A}$ ．．．． 20.96 20V．D．C．．． |  |  | 3 ma ．．．．． 8. |  |
|  | Trpe MR．65P． $34 \mathrm{in} . x^{3} \mathbf{3 i n}$ ．frents |  | 10mA $\ldots . . .8 .40$ | 1 mmp A．C．－${ }^{\text {a }}$－ 40 |
|  |  |  |  | 5 mmp. A．C．－ate 40 |
|  |  | 20V．D．C．．． 88.50 | $\begin{array}{llll}100 \mathrm{ma} & \cdots . & 88.40 \\ & 100 \mathrm{ma}\end{array}$ | 10 ninp．A．C．： 88 |
|  |  |  |  | 20 amp A．C．$=18.40$ |
| $100 \mathrm{~mA} . .$. ． 8.60 VU Meter $\quad 3.15$ | 100－0－100 $A$ A | 150V．D．C．$\quad 3.60$ |  |  |
| Trpe SD． $460 \mathbf{4 6 m m} \times 59.5 \mathrm{~mm}$ Fronts |  |  | ＂SEW＂BAKELITE |  |
|  | 800－0－800\％i |  |  |  |
|  | 1ma $\cdot$ ．．．． | 160 V. A．C．．． 48.40 | PANEL METERS <br> Type MR．65．Jfin．square fronts |  |
| 50－0－50нA |  | 300 V. A．C．． 88.0 |  |  |
|  | 10ma.. .9 ． 8.60 | $600 \mathrm{~V}, \mathrm{A.C}$. 43．00 |  |  |
|  | 80 ma A ．．．．${ }^{\text {a }}$ | －Metar lma mate | Type MR．65．Jfin．square fronts |  |
|  | 100ta A ．．．． 88.60 | VU Metar ．． 88.70 |  | 6 amp．．．．．．．${ }^{\text {a }}$－ 0 |
|  |  | 50 ma A．C．－ 48.80 |  | 15 amp．．．．．${ }^{\text {ate }} 60$ |
|  | 1 map．．．．．．． | 100 max A．C． |  | 30 amp．．．．． 2.40 |
| OmA ．．．．．se．60 300v．D．C． 88.60 | $8 \mathrm{mmp} . . . . .1$ ar | 200 mA A．C． |  |  |
|  | 10 amp．．．．． | 600mA A．C．－ 3.0 |  | bV．D．C．．．A8＊0 |
|  | 20 amp．．．．．， |  |  |  |
|  |  |  |  | Sov．D．C．$\because .$. |
|  |  |  |  |  |
|  |  |  | $25 \mu \mathrm{~A}$ ．．．．．． 84.60 |  |
|  | ＂EEW＂EDUCATIONAL METERS |  |  |  |
|  |  |  | 50 |  |
|  |  |  |  |  |
|  |  |  | 800， |  |
|  |  | rall 100 mm | 500－0－500 |  |
|  |  | ， |  | mp．A．C．－ 60 |
|  |  | befiv ranite of |  | $\begin{aligned} & 60 \\ & 60 \end{aligned}$ |
|  |  | traments moving | 10 |  |
| ＂SEW＂EDGWISE METERS |  |  |  |  |
| Troe PE．70． $\begin{gathered}\text { 3 } \\ \text { 2tin．deep } \\ \text { 2 }\end{gathered}$ |  | net and othe | 100 mA   <br> 500 mA $\cdots .$. 8.80 <br> 88 80  | － |
|  |  |  |  | VU Meter ．．as．es |
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|  | demonatrate internal worting．Available In the following rangea： |  |  |  |  |
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| AAZ17 |  |  |  |  |  |  |  | $\begin{array}{llllllll}\text { AD1s0 } & \text { 60p } & \text { BC212L } \\ \text { AD161 } & \text { 28p } & \text { BC213L 11p } & \text { MP8122 } & \text { 44p } & \text { 2N1131 } & \text { 22p } & \text { BA } 100\end{array}$








 | AF＇139 | 39 p | BC303 | $\mathbf{5 0 p}$ | NKT275 25p | 2 N 2926 | 10 p | BAY31 | 9 p |
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| AF＇239 | 41p | BC304 | 40 p | NKT403 71p | 2 N 3053 | 26 p | BY 100 | 29 p |










 | BC116 | $18 p$ | Br 173 | $29 p$ | OC23 | 33 p | $2 N 3710$ | 日p | OAB1 |
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