

electronics today

INTERNATIONAL

MARCH 1985 99p

LEAD THE WAY!

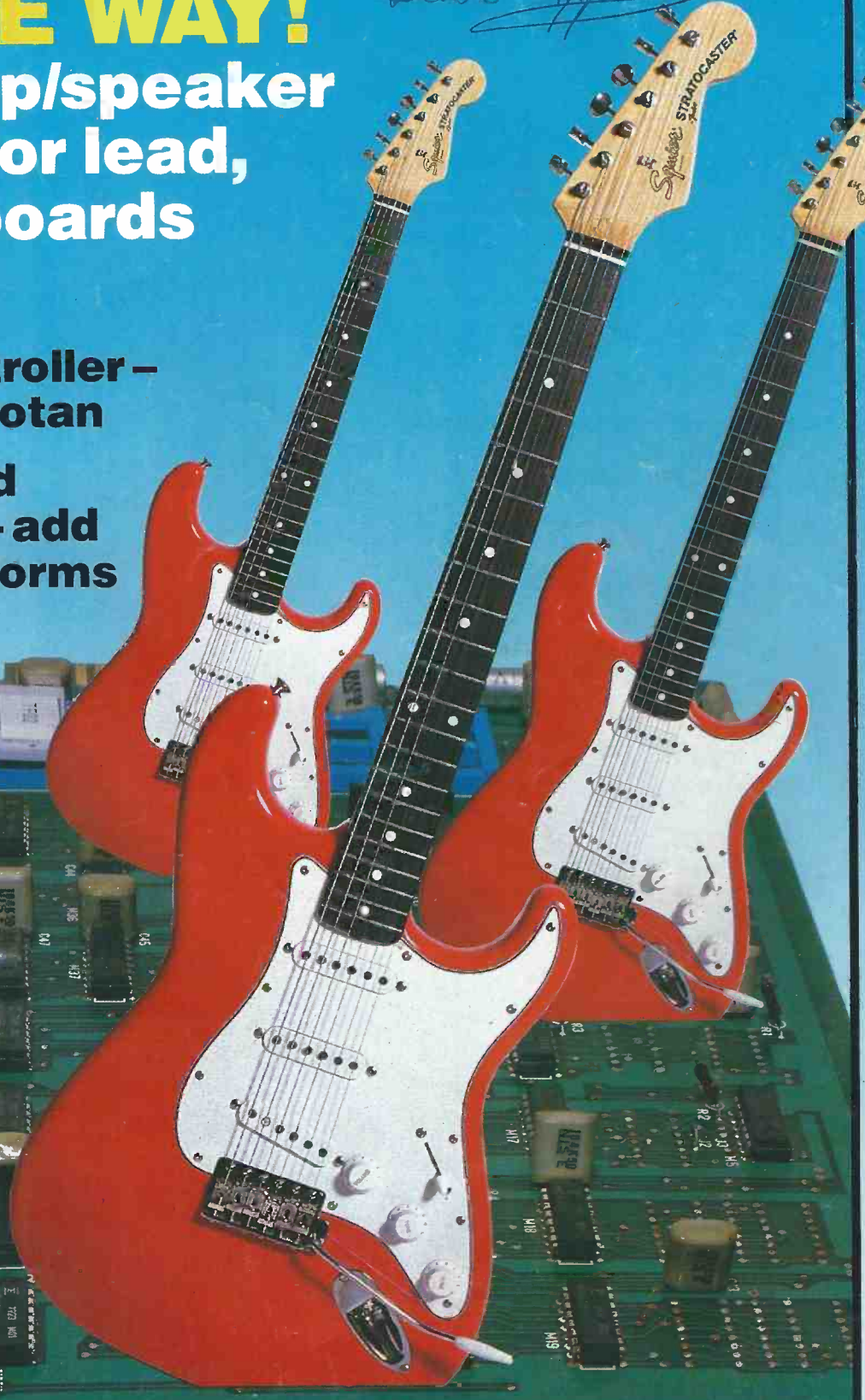
Build our amp/speaker
combo unit for lead,
bass or keyboards

PLUS

Single Board Controller –
based on the Microtan

Voltage Controlled
Digital Oscillator – add
extra synth waveforms
cheaply

Deane Apple



New Series – what the text
books don't tell you
about components

...AUDIO....MUSIC....RADIO....ROBOTICS.

Featured in Electronics
& Music Maker

TAKE COMPLETE CONTROL OF YOUR MUSIC with the

MCS-1

professional quality MIDI-controlled sampling unit

Once again, Powertran and E&MM combine to bring you versatility and top quality from a product out of the realms of fantasy and within the reach of the active musician.

The MCS-1 will take *any* sound, store it and play it back from a keyboard (either MIDI or Iv/octave). Pitch bend or vibrato can be added and infinite sustain is possible thanks to a sophisticated, looping system.

All the usual delay line features (Vibrato, Phasing, Flanging, ADT, Echo) are available with delays of up to 32 secs. A special interface enables sampled sounds to be stored digitally on a floppy disc via a BBC microcomputer.

The MCS-1 gives you many of the effects created by top professional units such as the Fairlight or Emulator. But the MCS-1 doesn't come with a 5-figure price tag. And, if you're prepared to invest your time, it's almost cheap!

Specification

Memory Size: Variable from 8 bytes to 64K bytes.

Storage time at 32 KHz sampling rate: 2 seconds.

Storage time at 8 KHz sampling rate: 8 seconds.

Longest replay time (for special effects): 32 seconds.

Converters, ADC & DAC: 8 bit companding. Dynamic range: 72 dB.

Audio Bandwidth: Variable from 12 KHz to 300 Hz.

Internal 4 pole tracking filters for anti-aliasing and recovery.

Programmable wide range sinewave sweep generator.

MIDI control range: 5 octaves.

+1 V/octave control range: 2 octaves with optional transpose of a further 5 octaves.

Digital Delay Line



Introduced in 1982, Powertran's DDL has brought digital quality effects to thousands of musicians. Still available in kit form at only £179.00 + VAT.

KIT
£499
+ VAT

BUILT
£699
+ VAT



Write or phone now to place an order
Powertran Cybernetics Limited,
Portway Industrial Estate,
Andover, Hants SP10 3ET.
Telephone: 0264 64455



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cybernetics Ltd

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INTERNATIONAL MARCH 1985 VOL 14 NO 3



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PUBLISHED BY:
Argus Specialist Publications Ltd.,
1 Golden Square, London W1R 3AB.
DISTRIBUTED BY:
Argus Press Sales & Distribution Ltd.,
12-18 Paul Street, London EC2A 4JS
(British Isles)
PRINTED BY:
The Garden City Press Ltd.
COVERS DESIGNED BY:
MM Design & Print.
COVERS PRINTED BY:
Alabaster Passmore.

OVERSEAS EDITIONS and their EDITORS
AUSTRALIA — Roger Harrison
CANADA — Halvor Moorshead
GERMANY — Udo Wittig
HOLLAND — Anton Kriegsman



Member of the
Audit Bureau
of Circulation

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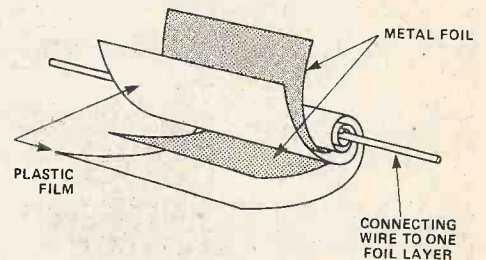
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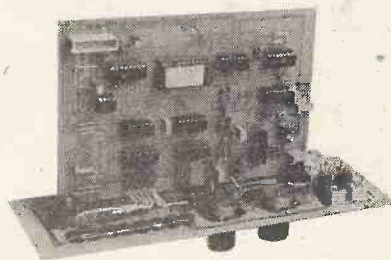
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DIGEST

System on a Chip? Well, Perhaps

Rapid Recall has just announced a new Intel software-on-silicon product which features a full BASIC interpreter in ROM on a single chip.

Known as the 8052 AH-BASIC, this 40-pin device is specifically designed for process control,

measurement and instrumentation applications. It consists of an 8052 AH micro-controller with a full-feature BASIC interpreter resident in the 8K bytes of available ROM. The interpreter allows 8052 AH users to write programs in BASIC instead of assembly language.

MCS BASIC-52 contains all the standard BASIC commands and functions, including BCD floating point arithmetic and transcendental operations. It also has many unique features to perform tasks that usually require assembly language programming. Bit-wise logic operators

(such as AND, OR and EXCLUSIVE-OR) are supported, as is hexadecimal arithmetic.

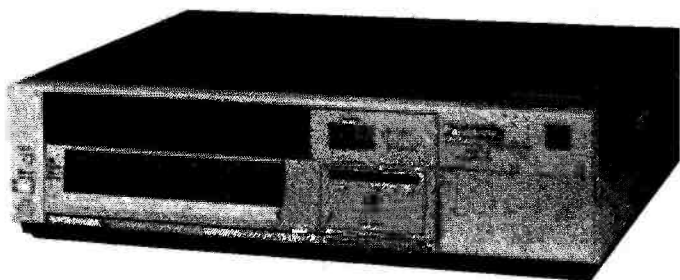
Additionally, almost all of the 8052 AH's special function registers can be accessed with MCS BASIC-52, allowing the user to set the timer or interrupt modes within the constructs of a BASIC program. MCS BASIC-52 also has a built-in 5msec real time clock which can be enabled, disabled and used to generate interrupts. Interrupts can be handled either by BASIC or assembly language.

A powerful feature of MCS BASIC-52 is that it generates all the timing necessary to program any standard EPROM or E²PROM with the user's application program. All that is required to implement this feature is a transistor, a gate and two passive components. Very little external hard-

ware is required to construct small systems.

Unlike most other BASIC interpreters, MCS BASIC-52 allows programs to reside in both RAM and EPROM/E²PROM. With the additional facility that up to 255 programs may reside in EPROM/E²PROM. Programs can also be transferred from EPROM/E²PROM to RAM for editing purposes.

An interrupted language, MCS BASIC-52 allows the user to develop a program interactively without the tiresome processes required by assemblers and compilers. Its design permits a programmer to develop resident high-level language software using the 8052 AH micro-controller. Rapid Recall Limited, Rapid House, Denmark Street, High Wycombe, Bucks, HP11 2ER, tel 0494 26271.



Time Lapse VCR

The Video Systems department of Panasonic Industrial have introduced a video cassette recorder which provides all the features normally found on such machines but in addition has the facility to produce time lapse recordings. The machine can be used with a conventional TV set or as part of a closed circuit television system for use in security/surveillance, education and information applications.

The AG-6010 is a VHS machine which can make recordings of up to three hours in the normal way or over a continuous period of 18, 36 or 72 hours in time lapse mode. The three-head design is described as microprocessor con-

trolled and provides a wide range of functions including still, slow, frame shift, reverse play and high speed forward or reverse search. A built-in timer allows time and date to be superimposed upon the recorded images and timed recordings can be stopped and started within a 24-hour period. Other features include automatic repeat recording, automatic recording after a power failure and alarm recording at normal speed. It is designed to complement Panasonic's range of CCTV products, including the mini CCTV system which allows up to three low-cost cameras to be used with a 9" monitor which has a built in sequential decoder.

The AG-6010 is now available through Panasonic's CCTV dealer network and the recommended retail cost is £1295.00 plus VAT. Panasonic UK Ltd, 300-318 Bath Road, Slough, Berkshire SL1 6JB, tel 0753-34522.

● By the 1st of January 1986 almost every company in the country will be required to display the new, EEC approved safety signs. As a reminder, the British Safety Council have produced a full colour poster which features a sculpted figure not unlike the present occupant of 10, Downing

Street. The wording on the poster reads "How dare you ignore the new safety signs". Readers wishing to acquire a copy for correction/contemplation/worship/to throw darts at should write to the council at 62-64 Chancellors Road, London W6 9RS, tel 01-741 1231.



'Walker In Manchester' Shock

Pictured above in classic pose — praying that he won't get any more technical enquiries — is erstwhile ETI Project Editor Phil Walker. Unconfirmed reports suggest that he is now in the Manchester area, scene of many

previous exploits (no, of course we're not going to tell you; use your imagination).

Sensitive Mancunians are advised to approach with care as this man's jokes have been known to stun at twenty paces. Those encountering him should approach with care and, if verbally assaulted, utter the terrible cry 'technical enquiry'. That should send him packing!

P.S. Sorry, Phil. And best of luck in your new job.

ELECTRONIC SIREN KIT

Produces an extremely loud piercing swept frequency tone from a 9-15V supply. Enable input for easy connection to alarm circuits. Includes 5in. Horn Speaker.



£7.90

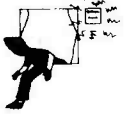
Mini Siren

As above, but with a small speaker (instead of horn speaker) for internal use. Complete with box

£4.30

SECURITY PRODUCTS

Protect your home and property and save by building your own burglar alarm system.



- Stair Mat 23 x 7 in (950 120) £1.70
- Floor Mat 29 x 16 in (950 125) £2.60
- Tamper-proof connecting block (950 110) £0.30
- Door/Window Contacts. Flush mounting, 4 wire, Magnet switch Per Pair (950 140) £1.05
- Window Tape 0.5" wide, 50m. (950 145) £2.50
- Window Tape Terminations Per pair. (950 150) £0.36
- Key-operated Switch, 1.5A 250V SPST Heavy chrome metal. (350 128) £4.50
- Passive Infra-Red Detector Detects intruder's body heat. Range 10 metres. 12V DC, n/o & n/c contact. (950 135) £40.00
- Alarm Control Unit. 4 input circuits, 2 instant and 2 delayed. Adjustable entry, exit and alarm times. Built and tested. Full instructions supplied. Size: 180 x 130 x 30mm. Supply: 12V DC. (950 160) £26.00
- Ultrasonic Burglar Alarm. Self-contained mains or battery powered unit complete with horn and AC adaptor. Impuls for pressure mats and other sensors together with exit/entry delays enable this unit to be used as a complete system. £45.00 + p&p £2.20
- BW Horn Speaker. 5.5 ins. 8 ohm. Ideal for sirens, etc. 2.5m lead and 3.5mm jack plug. (403 148) £6.15

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INFRA-RED REMOTE CONTROL KITS



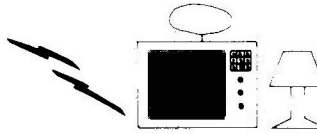
These kits are designed to enable infra-red remote control to be incorporated into virtually any application from switching car locks or alarms to controlling Hi-Fi or TV. The application will determine the interface circuitry between the receiver and the controlled device. General instructions and applications are supplied. The kits are coded and provide a high degree of security and noise immunity.

- MK18 Transmitter Kit** - for use with MK11/MK12 receivers. Requires PP3 battery. Size: 8 x 2 x 13cms. Range approx 60ft. £6.80
- Keyboards for MK18**
- MK9 4-way for use with MK12 £1.90
- MK10 16-way for use with MK12 £5.40
- MK13 11-way for use with MK11 £4.35
- MK11 Receiver Kit** - mains powered Provides 10 latched plus 3 analogue outputs ideal for controlling audio amplifiers, TV or lighting where control of light brightness is required £13.50
- MK14 AC Power Controller Kit** for (phase) controlling AC loads from MK11 analogue outputs, eg lamp dimming. £5.20

MK19 Stereo Amplifier Controller Kit - for remote control of bass, treble and volume (or balance) by MK11. Includes a one of 10 decoder remote channel or input selection. May be connected between the pre-amp and power amp of almost any audio system. £10.70

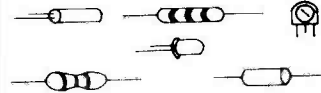
MK12 Receiver Kit - mains powered with 16 latched or momentary outputs. Latched version is for applications requiring one output on at a time, eg TV channel selection. Momentary type gives an output only during transmission. Lines may be latched as required. £13.50
Size: 9 x 4 x 2cms.

MK15 Dual Latched Solid State Relay - for switching mains loads such as lamps, TVs, etc. from the outputs of the MK12 (momentary). 15 items may be switched independently using 8 MK15s. Triacs (not supplied) switch at mains zero to reduce interference. £4.50



COMPONENT PACKS

- PACK 1 650 Resistors 47R 10M 10 per value £4.00
- PACK 2 40 - 16V Electrolytics 10-1000uF 5 per value £3.25
- PACK 3 60 - Polyester Capacitors. 0.01 1uF 250V 5 values £5.55
- PACK 4 45 Presets 100R 1M £3.00
- PACK 5 30 - Low Profile IC Sockets 8, 14 & 16 pin £2.40
- PACK 6 25 Red LEDs (5mm) £1.75



BT STYLE PHONE CONNECTORS

Line Jack Units
Master Unit (first line unit) has bell capacitor and surge arrester.
Flush or surface mounting. Screw connectors.

- Master (flush) (960 110) £3.00
- Master (surface) (960 112) £3.00
- Master (mini surface) (960 113) £3.50
- Secondary (flush) (960 114) £2.65
- Secondary (surface) (960 116) £2.65
- Secondary (mini surface) (960 117) £3.00
- Dual outlet adaptor (960 118) £4.20
- 4 way line cord with plug to spade terminals (960 120) £2.00
- 4 way line cord (960 130) £0.20 per m

LCD DIGITAL MULTIMETERS

LOW COST! 10M ohm, 3 1/2 digit 0.4 in display. Auto zero and polarity, low batt indication, overload protection. Includes test leads, battery, spare fuse, manual, carrying case.

- AC Volts: 0-200-500.
- DC Volts: 0-2-20-200-1000.
- DC Current: 0-20m-200mA.
- Resistance: 0.2k-20k-200k-2M.
- Size: 138 x 86 x 36mm. £25.95 (405 202)
- Professional** 10M, 0.5 in, 3 1/2 digit. Overrange and low battery indication. Overload protection: includes leads, spare fuse, battery, manual and case. Transistor Checker. Size: 175 x 93 x 42mm.
- AC Volts: 0-200-750.
- DC Volts: 0-200m-2-20-200-1000.
- DC Current: 0-20u-2m-20m-200mA, 0-10A.
- Ohms: 0-200-2k-20k-200k-2M, 0-20M. (405 204) £33.50



Auto Ranging. 3 1/2 digit 10mm display. Continuity buzzer, low battery, overload and range indication. 10A internal shunt for AC/DC current measurement. Carrying case supplied.

- AC Volts: 0-2-20-200-600.
- DC Volts: 0-0.2-2-20-200-1000
- AC Current: 0-200mA, 0-10A.
- DC Current: 0-200mA/0-10A.
- Resistance: 0-200.2k-20k-200k-0.2M.
- Size: 160 x 85 x 29mm. £44.85 (405 206)
- High Sensitivity Temperature Probe.** For use with a multimeter to measure temperatures from -50°C to +250°C. Accuracy: 1.5°C@25°C, 2°C@100°C. Response time (in water), 5 seconds. Includes case, calibrated scale and instructions. (405 220) £8.50

MICROPROCESSOR TIMER KIT

Designed to control 4 outputs independently switching on and off at preset times over a 7-day cycle. LED display of time and day, easily programmed via 20-way keyboard. Ideal for central heating control (including different switching times for weekends). Battery back-up circuit. Includes box. 18 time settings.



- CT6000K £39.00
- XK114. Relay Kit for CT6000 includes PCB, connectors and one relay. Will accept up to 4 relays. 3A/240V c/o contacts £3.90
- 701 115 Additional Relays £1.65

ELECTRONIC LOCK KIT

With hundreds of uses indoors, garages, car anti-theft devices, electronic equipment, etc. Only the correct easily changed four-digit code will open it! Requires a 5-15V DC supply. Output 750mA. Fits into standard electrical wall box. Complete kit (except front panel)

- XK101 £11.50
- Electric Lock Mechanism** for use with existing door locks and the above kit. (Requires relay.) 12V AC/DC coil. (701 150) £14.95

HOME LIGHTING KITS

These kits are designed to replace a standard wall switch to control up to 300w of lighting



- TDR300K Remote Controlled Light Dimmer £14.95
- MK6 Transmitter for above £4.50
- TD300K Touch Dimmer £7.75
- TS300K Touch Switch £7.75
- TDE/K 2-way extension for above kits £2.50
- LD300K Rotary controlled Light Dimmer £3.95

DISCO LIGHTING KITS

DL1000K This value-for money 4-way chaser features bi-directional sequence and dimming. 1kW per channel. £15.95

DLZ1000K - A lower cost uni-directional version of the above. Zero switching to reduce interference. £8.95

Optional opto input allowing audio 'beat' light response (DLA/1) 70p

DL3000K - 3-channel sound to light kit features zero voltage switching, automatic level control and built-in microphone. 1kW per channel. £12.95

DVM/ULTRA SENSITIVE THERMOMETER KIT

Based on the ICL 7126 and a 3 1/2 digit liquid crystal display, this kit will form the basis of a digital multimeter (only a few additional resistors and switches are required - details supplied), or a sensitive digital thermometer (50°C to +150°C) reading 0.1°C. The kit has a sensitivity of 200mV for a full-scale leading automatic polarity and overload indication. Typical battery life of 2 years (IP3). £15.50

IR GARAGE DOOR CONTROLLER KIT

For controlling motorised garage doors and switching garage and drive lights on off up to a range of 40 ft



Lots of applications like controlling lights and TVs, etc. in the home. Ideal for aged or disabled persons, this coded kit comprises of a mains powered infra red receiver with a normally open relay output plus two latched transistor outputs, battery powered transmitter and opto-isolated solid state mains switch.

- XK103 £25.00
- XK105 Extra transmitters £10.50

PANTEC KITS

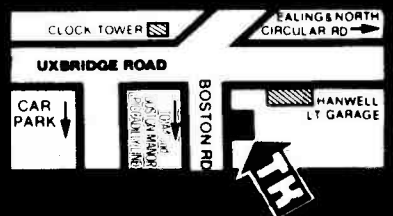
- PN2 FM Micro Transmitter £7.50
- PN3 Stabilised Power Supply £13.70
- PN5 2 - 10W Stereo Amplifier £14.50
- PN6 2 - 40W Stereo Amplifier £24.95
- PN7 Pushbutton Stereo Preamp £12.80
- PN8 Tone & Volume Control £13.60
- PN11 3w FM Transmitter £11.95
- PN13 Single Channel FM Transmitter £9.80
- PN14 Receiver for above £15.50

ELECTRONICS

11-13 Boston Road
London W7 3SJ

ORDERS 01-567 8910 ENQUIRIES 01-579 9794

01-579 2842 TECHNICAL AFTER 3pm



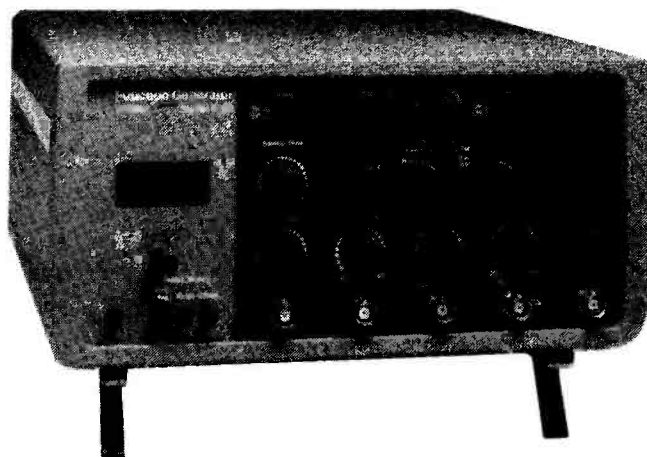
12 MHz AM/FM Sweep Function Generator

The series 8120 multipurpose function generator from Global Specialties Corporation provides sine, triangle, square, and pulse wave forms with variable amplitude, symmetry and offset over a frequency range of 1mHz to 12MHz. Frequencies can be amplitude or frequency modulated with an internal 1kHz sine signal or with an external signal or in a combination of both internal and external signal.

The output can be continuous, gated or triggered either by an

external switch or a front panel manual switch. The start phase of the output signal is continuously adjustable from -90° to $+90^\circ$. When used as a sweep generator, the series 8120 has an internal ramp with variable duration to provide a recurring linear sweep over a 100:1 frequency range or a 1000:1 range using an external signal.

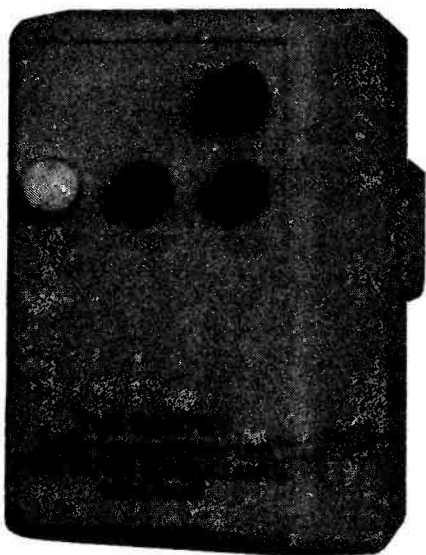
Other features include an output amplitude to 30V peak-to-peak, an attenuation and amplitude control to 80dB, a 20% to 80% variable symmetry and a DC/offset voltage adjustable from -7.5 to $+7.5$ V into 50R. A 3-digit LED display gives an automatic and convenient read-out of the frequency, output peak-to-peak voltage, output offset DC level and sweep stop frequency. This facility eliminates the need for external instruments such as oscilloscopes, digital multimeters, and counters, to monitor the output of the



function generator.

The 8120 series comprises ten different models, each weighing approximately 4.5kg and having an ambient operating temperature range of 0° to 40° C. Prices

range from £680.00 to £1,115.00 exclusive of VAT and postage. Global Specialties Corporation, Shire Hill Industrial Estate, Saffron Walden, Essex CB11 3AQ, tel 0799-21682.



Hicough Monitor

Could a hicough in the mains cause chaos with your micro or other gear? The answer is 'yes', but the problems only start there, because it's often impossible to tell what actually has caused the failure or latch-up, especially if you're testing out something new.

Enter Mektronic Consultants with 'The Sentry' mains monitor. You could use it just to indicate when a mains transient has occurred, so that, when your micro has gone down and taken 300 hours of diligent machine code graphics programming with it, at least you will know it wasn't

your fault. Alternatively, you could use 'The Sentry' to check the available supplies at your location to see which is cleanest. And by noticing what happens when a supply transient is generated, you could eventually isolate which items are causing the transients.

It plugs into a standard 13A socket and provides an indication if a transient is detected. It will indicate three levels of transient: slight, moderate and severe, and once a transient is detected the indicator lamp remains lit until the unit is reset. 'The Sentinel' costs £48.50 including P&P but excluding VAT (an extra £7.28) from Mektronic Consultants, Linden House, 116 Rectory Lane, Prestwich, Manchester M25 5DB, tel 061-798 0803.

TI Turn Their Hand To Diesel

As temperatures plunge well below freezing point, drivers of diesel-engined vehicles are finding that they can start up, but that their engines are running roughly, and frequently stalling two or three minutes down the road.

In sub-zero conditions, diesel engines suffer the problem of fuel "waxing", in which the paraffin crystallises. The engine will then usually run until the wax reaches the filter, which clogs up and

leads to stalling.

Truckers associations advise owners to garage their vehicles overnight, and to use diesel fuel heaters or fuel additives. But many do not have garages or even sheltered parking places, and the fuel mixtures available in any but the coldest countries cannot cope with such extremes.

In February 1984, the Materials and Controls Division of Texas Instruments launched an easy-to-use, semiconducting ceramic device which prevents the waxing of diesel fuel. This diesel fuel heater, known as the 30RT, uses ceramic elements as a heat source. Packaged in a highly-efficient heat exchanger, it is typically mounted between the filter head and the filter itself, or

alternatively in the fuel line.

The 30RT, in combination with an ambient temperature thermostat, switches on if the temperature falls below zero. The self-regulating nature of the ceramic means that it cannot overheat, and can be used on applications from 12-24V DC without any deterioration in performance.

Since the 30RT's introduction, many car, truck and filter makers have been evaluating it this winter or fitting it to their products. For example, it has recently been introduced on BMW's 300 series diesel models. Agricultural machinery maker International Harvester has been fitting 30RTs on its machines this winter, as has Fleetguard the truck maker on its

Cummins-engined vehicles.

However, at present the average driver is still having to contend with waxing problems because the automotive industry typically takes at least a year to complete its evaluation of new products, such as the 30RT. By next winter, however, this device should be moving down from the luxury end of car ranges. It will also become available through the retrofit/DIY after-market, helping to reduce the hazards of winter driving for many more motorists. In the meantime, the major UK filter manufacturer is presently adapting its range to provide compatibility with the 30RT. Texas Instruments Ltd, Manton Lane, Bedford, MK41 7PA, tel 0234 63211.

● Rapid Recall are making available a pamphlet written by two Digital Equipment Corporation engineers which outlines the more common microprocessor benchmarking techniques. The 8-page A4 pamphlet also describes the various areas of system performance and proposes a performance measuring system, and copies can be obtained free of charge from Rapid Recall, Rapid House, Denmark Street, High Wycombe, Buckinghamshire HP11 2ER, tel 0494-26271.

● British Telecom opened their first high-street shop at Southend on January 3rd. You can go in there, choose a new telephone, pay your bill... and two more shops will be opening in Newcastle and Plymouth later this year.

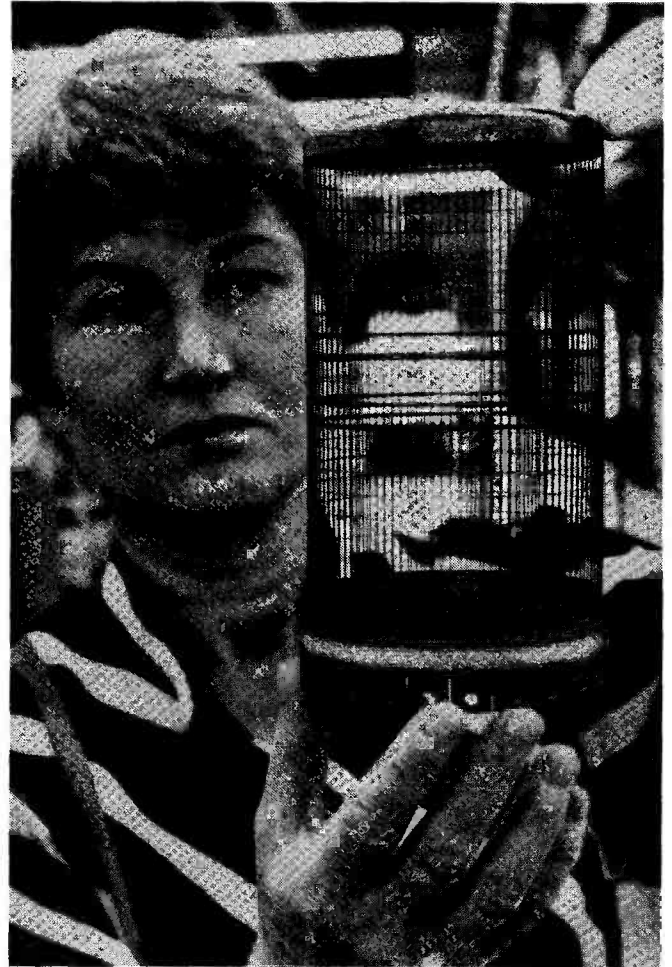
● Decospray have developed a process which allows molten zinc to be applied to the surfaces of plastic enclosures without deforming or weakening them. The coating provides a high level of shielding against radio frequency interference and will allow plastics to be used in many applications which currently demand the screening properties of a metal enclosure. For more information contact C.C. Hammond at Decospray Ltd, Eastmore Street, Woolwich Road, Charlton, London SE7 8NA, tel 01-858 5128.

● The British Standards Institution has published the following documents under the common title 'Harmonised system of quality assessment for electronic components':- BS9925 Inductor and transformer cores for telecommunications, part 0, geometric specification (£22.80); BS9925 part 01.0 Sectional specification of magnetic oxide cores for inductor applications (£16.20); BS CECC 11100 Sectional specification of display storage tubes (£16.20); BS CECC 1700 Generic specification of mercury wetted make contact units (£16.20); BS CECC 18000 Generic specification of dry reed change-over contact units, mechanically biased (£16.20); BS CECC 30400 Sectional specification of fixed metallised polyethylene-terephthalate film dielectric capacitors for direct current (£8.00); BS CECC 75100 Sectional specification of two part and edge socket connectors for printed board application (£22.80). All of these standards are available at 50% discount to members from the Sales Department, BSI, Linford Wood, Milton Keynes MK14 6LE.

Who's A Pretty Pyrographite Then?

High technology has been applied to some pretty mundane products but as far as we know no-one is yet using a laser to produce bird cages. The device shown is, in fact, the screen grid of a 100kW vapour-condensation cooled tetrode for medium and short wave radio transmitters. Manufactured by Siemens at their electronics tubes plant in Berlin, the grid was produced from a hollow cylinder of pyrographite using a laser as a precision cutting tool. The features are said to be remarkably smooth when compared with those of sand-blasted grids, and the material has excellent dimensional stability. In operation it will be loaded with as much as 24W per square centimetre and will run at temperatures as high as 2000 K.

Siemens Ltd, Siemens House, Windmill Road, Sunbury-on-Thames, Middlesex TW16 7HS, tel 09327-85691.



The Year To Go Bust

Last year, 1984, was the worst year on record for business failures in the electrical industry, according to the latest survey by Dun & Bradstreet Limited, the business information company. During the year company liquidations in the industry amounted to 793, an increase of 4.9 per cent over 1983 and representing 5.8 per cent of the total liquidations in England and Wales.

48.4 per cent of liquidations were recorded in London and the South East. A further 16.5 per cent occurred in the North West. Bankruptcies among firms, partnerships and individuals rose 19.8 per cent to 121 during the year.

In England and Wales as a whole, total company liquidations in 1984 reached 13,647 — an increase of 9.5 per cent on 1983. Bankruptcies among individuals, firms and partnerships rose to 8,035 during 1984 representing an increase of 17.8 per cent over the previous year.

Let's just hope that 1985 is better for us all.

Motor Control Chip

Plessey Semiconductors has introduced the TDA 2088, a bipolar phase control integrated circuit optimised for current feedback applications but which can also be used in the open loop mode.

The new circuit, now available from the company and its distributors, has been designed primarily for AC universal motor speed control in applications such as power drills and domestic appliances (foodmixers, etc). A high level of system integration has resulted in low external component count, thus ensuring a low cost solution to such applications.

Powered direct from the AC mains or a DC line, the TDA 2088 features an on-chip series regulator. This produces a smooth, low current (-5V) supply for the internal analogue control functions which may be used to power ancillary circuitry

usually associated with this type of control system.

Voltage and current synchronisation inputs ensure that the triac firing pulse is at precisely the right moment under any load conditions. The negative triac firing pulse (a drive polarity preferred by most triac manufacturers) has a minimum guaranteed drive current of 100 mA with a typical current of 125 mA which ensures reliable firing of triacs capable of handling up to 40 Amps.

The TDA 2088 phase controller also produces a well-defined control voltage/phase angle relationship by using the international -5V reference circuit as the charging voltage for both the pulse timing ramp capacitor and as the reference voltage for the speed input potentiometer.

Compensation of motor speed with varying load is achieved by sensing motor current. The circuit design allows simple optimisation of control loop parameters.

Currently available in a 14 pin plastic dual-in-line (DIL) package it is planned to supply the TDA 2088 in a SO 14 package. Further information will be provided by Plessey Semiconductors Limited, Cheney Manor, Swindon SN2 2QW, tel 0793 36251.

New 726 Information Technology Scheme

A new City and Guilds Information Technology scheme (726) was launched on 18 January. C&G say that this scheme represents a double breakthrough: it takes an entirely new approach to educational and training methods as well as a uniquely broad consideration of vocational training in the rapidly developing and changing field of

Information Technology.

The 726 series is intended to provide for very flexible study or training methods; it is entirely pupil paced, and the criterion referenced assessment is designed to ensure that successful candidates demonstrate an ability to do the job competently.

The approach is modular, but there are a limited number of modules and each is nationally devised so that employers will be able to assimilate and assess the content of each as well as deciding which combinations might best meet the needs of their workforce. Modules will relate to

and Guilds. This means that centre the three subject disciplines of: programming and software; electronics and hardware; and computer applications and operation. Module levels are defined as either introductory, elementary, intermediate or advanced. These levels relate to the subject matter and are not necessarily indicative of ability. C&G say that many of the modules will be equally suitable for a very wide range of candidates; some will ideally suit YTS trainees and others will be pitched at supervisory and management personnel.

The scheme may be offered by any centre approved by the City

and Guilds. This means that centres could be set up in schools, F.E. colleges, industrial premises, ITeC's or Skills Centres, etc — anywhere where the necessary hardware, training personnel and accommodation can be provided.

The scheme is initially released at the Introductory and Elementary levels, but Intermediate and Advanced level modules will be available very soon. Scheme notes are now available and further information can be obtained from: Section 18, City and Guilds of London Institute, 46, Britannia Street, London WC1X 9RG, tel 01-278 2468.

Digital Signal Processor For Audio Applications

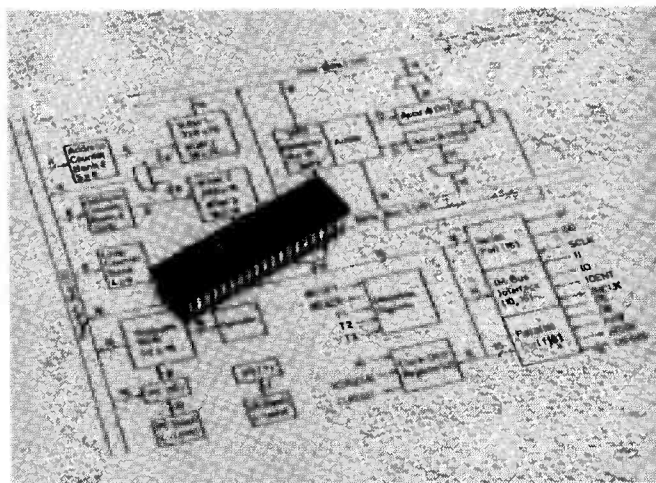
ITT Semiconductors have produced a digital signal processor chip which can be used instead of analogue devices in many audio-frequency applications. The advantages of using digital processing include higher noise immunity, true phase-linearity and freedom from component drift problems caused by temperature and ageing.

The UDP101 CMOS chip is based on the Harvard architecture, and comes in a 40-pin plastic package. Two data buses and pipelining are used for speed of execution, and the basic instruc-

tion cycle time is 100 nanoseconds which makes it suitable for use in a wide variety of audio processing applications. The basic arithmetic operation is multiply and add using twos complement with a results resolution of 31 bits. The data and instruction word-length is 16 bits and the internal memory comprises 1K 16-bit words of program ROM, 72 words of data ROM, and 440 words of data RAM. Subroutines can be nested at up to four levels.

Three separate I/O facilities are available: fast serial at rates up to 5 Mbits/second, slow serial I/O for communication with slave peripherals through the chip's IM bus interface, and a 16-bit parallel interface that's compatible with popular microprocessors, including the 68000.

The UDP101 operates on a single 5V supply and consumes about 80 mW. A ROMless version (UDP101-EC) is available for development. Software tools include a cross assembler and



simulator written in FORTRAN 77.

The device's bandwidth allows a wide range of applications. In the telecommunications field it could be used in DTMF receivers, modems, vocoders, scramblers and echo-cancelling systems, and in the consumer field it's suitable

for audio processing in a variety of TV, hi-fi and radio applications. General industrial uses include speech recognition.

For further information contact Georgina Cole at ITT Semiconductors, 145-147 Ewell Road, Surbiton, Surrey KT6 6AW, tel 01-390 6578.

Light And Colour Principles

A new volume — 'Light and Colour Principles' — has been published by the IBA as No. 22 in the series of occasional engineering texts under the general title of 'IBA Technical Review'.

Our sources say that this fully-illustrated 60-page book provides not only a clear introduction to aspects of photometry and colorimetry essential to the understanding and engineering of colour television but also describes the recent development by IBA engineers of new, microcomputer-based spectrometric equipment and its practical application to the analysis

and optimisation of television cameras and monitors.

Contributions include: "The Measurement of Light" by Professor R.W.G. Hunt (City University, London, formerly Kodak Research Laboratories) and P.J. Darby (IBA).

"Colorimetry" by Professor R.W.G. Hunt.

"Colorimetry in Television" by P.J. Darby.

"Computer-operated Spectrophotometric Analysis of Cameras (COSAC)" by P.A. King (IBA) and P.J. Marshall (HTV, formerly IBA).

"Computer-operated Spectrophotometric Analysis of Monitors (COSAM)" by P.A. King and P.J. Marshall.

In an introduction, J.B. Sewter, IBA's Assistant Director of Engineering (Network and Development), points out that

the IBA has overall responsibility for the maintenance of high technical standards in Independent Broadcasting. Its engineers are much concerned with the technical performance of studio centres although the equipping and operation of such centres and the creative content of the programmes is the concern of the individual programme companies. During recent years broadcasters have achieved a more widespread understanding of colorimetry and its importance to television. The availability of microcomputers now makes it possible to process multiple measurements and the complex calculations needed to analyse and optimise cameras and monitor display. Together with improvements in optical components this had led to the development of a transportable IBA test

rig capable of a wide range of colorimetric measurements.

The early sections provide clear, unambiguous definitions of units based on the latest CIE and CIELUV 76 recommendations. These volumes are intended only for engineers and students directly involved in the field of broadcasting. Subject to availability of limited stocks, single copies may be obtained without charge. Complimentary copies are also available, on request, to technical libraries and educational centres in the UK and overseas. IBA Technical Review No 22, 'Light and Colour Principles', technical editor Dr. Henry Palmer is published by IBA London. Enquiries to IBA Engineering Information Services, Crawley Court, Winchester, Hampshire, SO21 2QA, telephone Winchester (0962) 822444.

ETI

74 SERIES 4000 SERIES LINEAR ICs COMPUTER COMPONENTS

74 SERIES table listing various integrated circuits such as 7400, 7401, 7402, 7403, 7404, 7405, 7406, 7407, 7408, 7409, 7410, 7411, 7412, 7413, 7414, 7416, 7417, 7418, 7419, 7420, 7421, 7422, 7423, 7424, 7425, 7426, 7427, 7428, 7429, 7430, 7431, 7432, 7433, 7434, 7435, 7436, 7437, 7438, 7439, 7440, 7441, 7442, 7443, 7444, 7445, 7446, 7447, 7448, 7449, 7450, 7451, 7452, 7453, 7454, 7455, 7456, 7457, 7458, 7459, 7460, 7461, 7462, 7463, 7464, 7465, 7466, 7467, 7468, 7469, 7470, 7471, 7472, 7473, 7474, 7475, 7476, 7477, 7478, 7479, 7480, 7481, 7482, 7483, 7484, 7485, 7486, 7487, 7488, 7489, 7490, 7491, 7492, 7493, 7494, 7495, 7496, 7497, 7498, 7499, 7500

4000 SERIES table listing various integrated circuits such as 4000, 4001, 4002, 4003, 4004, 4005, 4006, 4007, 4008, 4009, 4010, 4011, 4012, 4013, 4014, 4015, 4016, 4017, 4018, 4019, 4020, 4021, 4022, 4023, 4024, 4025, 4026, 4027, 4028, 4029, 4030, 4031, 4032, 4033, 4034, 4035, 4036, 4037, 4038, 4039, 4040, 4041, 4042, 4043, 4044, 4045, 4046, 4047, 4048, 4049, 4050, 4051, 4052, 4053, 4054, 4055, 4056, 4057, 4058, 4059, 4060, 4061, 4062, 4063, 4064, 4065, 4066, 4067, 4068, 4069, 4070, 4071, 4072, 4073, 4074, 4075, 4076, 4077, 4078, 4079, 4080, 4081, 4082, 4083, 4084, 4085, 4086, 4087, 4088, 4089, 4090, 4091, 4092, 4093, 4094, 4095, 4096, 4097, 4098, 4099, 4100

LINEAR ICs table listing various linear integrated circuits such as LM733, LM734, LM735, LM736, LM737, LM738, LM739, LM740, LM741, LM742, LM743, LM744, LM745, LM746, LM747, LM748, LM749, LM750, LM751, LM752, LM753, LM754, LM755, LM756, LM757, LM758, LM759, LM760, LM761, LM762, LM763, LM764, LM765, LM766, LM767, LM768, LM769, LM770, LM771, LM772, LM773, LM774, LM775, LM776, LM777, LM778, LM779, LM780, LM781, LM782, LM783, LM784, LM785, LM786, LM787, LM788, LM789, LM790, LM791, LM792, LM793, LM794, LM795, LM796, LM797, LM798, LM799, LM800

COMPUTER COMPONENTS table listing various computer components such as CPU, MEMORY, ROMS/PROMS, DISC CONTROLLER, and INTERFACE ICs. Includes items like 1802CE, 2801, 2802, 2803, 2804, 2805, 2806, 2807, 2808, 2809, 2810, 2811, 2812, 2813, 2814, 2815, 2816, 2817, 2818, 2819, 2820, 2821, 2822, 2823, 2824, 2825, 2826, 2827, 2828, 2829, 2830, 2831, 2832, 2833, 2834, 2835, 2836, 2837, 2838, 2839, 2840, 2841, 2842, 2843, 2844, 2845, 2846, 2847, 2848, 2849, 2850

VOLTAGE REGULATORS table listing various voltage regulators such as 7805, 7806, 7807, 7808, 7809, 7810, 7811, 7812, 7813, 7814, 7815, 7816, 7817, 7818, 7819, 7820, 7821, 7822, 7823, 7824, 7825, 7826, 7827, 7828, 7829, 7830, 7831, 7832, 7833, 7834, 7835, 7836, 7837, 7838, 7839, 7840, 7841, 7842, 7843, 7844, 7845, 7846, 7847, 7848, 7849, 7850

OTHER REGULATORS table listing various other regulators such as 3150, 3151, 3152, 3153, 3154, 3155, 3156, 3157, 3158, 3159, 3160, 3161, 3162, 3163, 3164, 3165, 3166, 3167, 3168, 3169, 3170, 3171, 3172, 3173, 3174, 3175, 3176, 3177, 3178, 3179, 3180, 3181, 3182, 3183, 3184, 3185, 3186, 3187, 3188, 3189, 3190, 3191, 3192, 3193, 3194, 3195, 3196, 3197, 3198, 3199, 3200

OPTO-ELECTRONICS table listing various optoelectronic components such as 24L07, 24L08, 24L09, 24L10, 24L11, 24L12, 24L13, 24L14, 24L15, 24L16, 24L17, 24L18, 24L19, 24L20, 24L21, 24L22, 24L23, 24L24, 24L25, 24L26, 24L27, 24L28, 24L29, 24L30, 24L31, 24L32, 24L33, 24L34, 24L35, 24L36, 24L37, 24L38, 24L39, 24L40, 24L41, 24L42, 24L43, 24L44, 24L45, 24L46, 24L47, 24L48, 24L49, 24L50

OPTO-ISOLATORS table listing various optoisolators such as 6N137, 6N138, 6N139, 6N140, 6N141, 6N142, 6N143, 6N144, 6N145, 6N146, 6N147, 6N148, 6N149, 6N150, 6N151, 6N152, 6N153, 6N154, 6N155, 6N156, 6N157, 6N158, 6N159, 6N160, 6N161, 6N162, 6N163, 6N164, 6N165, 6N166, 6N167, 6N168, 6N169, 6N170, 6N171, 6N172, 6N173, 6N174, 6N175, 6N176, 6N177, 6N178, 6N179, 6N180

LEDs table listing various light-emitting diodes such as TL209, TL210, TL211, TL212, TL213, TL214, TL215, TL216, TL217, TL218, TL219, TL220, TL221, TL222, TL223, TL224, TL225, TL226, TL227, TL228, TL229, TL230, TL231, TL232, TL233, TL234, TL235, TL236, TL237, TL238, TL239, TL240, TL241, TL242, TL243, TL244, TL245, TL246, TL247, TL248, TL249, TL250

CHARACTER GENERATORS table listing various character generators such as MC1441, MC1442, MC1443, MC1444, MC1445, MC1446, MC1447, MC1448, MC1449, MC1450, MC1451, MC1452, MC1453, MC1454, MC1455, MC1456, MC1457, MC1458, MC1459, MC1460, MC1461, MC1462, MC1463, MC1464, MC1465, MC1466, MC1467, MC1468, MC1469, MC1470, MC1471, MC1472, MC1473, MC1474, MC1475, MC1476, MC1477, MC1478, MC1479, MC1480

ENCODERS table listing various encoders such as AY-5276, AY-5277, AY-5278, AY-5279, AY-5280, AY-5281, AY-5282, AY-5283, AY-5284, AY-5285, AY-5286, AY-5287, AY-5288, AY-5289, AY-5290, AY-5291, AY-5292, AY-5293, AY-5294, AY-5295, AY-5296, AY-5297, AY-5298, AY-5299, AY-5300

GENERATORS table listing various generators such as MC14411, MC14412, MC14413, MC14414, MC14415, MC14416, MC14417, MC14418, MC14419, MC14420, MC14421, MC14422, MC14423, MC14424, MC14425, MC14426, MC14427, MC14428, MC14429, MC14430, MC14431, MC14432, MC14433, MC14434, MC14435, MC14436, MC14437, MC14438, MC14439, MC14440

UHF MODULATORS table listing various UHF modulators such as BMH2UHF375, BMH2UHF450, BMH2UHF525, BMH2UHF600, BMH2UHF675, BMH2UHF750, BMH2UHF825, BMH2UHF900, BMH2UHF975, BMH2UHF1050, BMH2UHF1125, BMH2UHF1200, BMH2UHF1275, BMH2UHF1350, BMH2UHF1425, BMH2UHF1500, BMH2UHF1575, BMH2UHF1650, BMH2UHF1725, BMH2UHF1800

CRYSTALS table listing various crystals such as AD561, AD562, AD563, AD564, AD565, AD566, AD567, AD568, AD569, AD570, AD571, AD572, AD573, AD574, AD575, AD576, AD577, AD578, AD579, AD580, AD581, AD582, AD583, AD584, AD585, AD586, AD587, AD588, AD589, AD590, AD591, AD592, AD593, AD594, AD595, AD596, AD597, AD598, AD599, AD600

DISC CONTROLLER table listing various disc controllers such as 6843, 6844, 6845, 6846, 6847, 6848, 6849, 6850, 6851, 6852, 6853, 6854, 6855, 6856, 6857, 6858, 6859, 6860, 6861, 6862, 6863, 6864, 6865, 6866, 6867, 6868, 6869, 6870, 6871, 6872, 6873, 6874, 6875, 6876, 6877, 6878, 6879, 6880

DIODES table listing various diodes such as 2N2219A, 2N2222A, 2N2290, 2N2344, 2N2369, 2N2430, 2N2450, 2N2459, 2N2460, 2N2461, 2N2462, 2N2463, 2N2464, 2N2465, 2N2466, 2N2467, 2N2468, 2N2469, 2N2470, 2N2471, 2N2472, 2N2473, 2N2474, 2N2475, 2N2476, 2N2477, 2N2478, 2N2479, 2N2480, 2N2481, 2N2482, 2N2483, 2N2484, 2N2485

PLASTIC table listing various plastic components such as BY127, BY128, BY129, BY130, BY131, BY132, BY133, BY134, BY135, BY136, BY137, BY138, BY139, BY140, BY141, BY142, BY143, BY144, BY145, BY146, BY147, BY148, BY149, BY150, BY151, BY152, BY153, BY154, BY155, BY156, BY157, BY158, BY159, BY160, BY161, BY162, BY163, BY164, BY165, BY166, BY167, BY168, BY169, BY170

BRIDGE RECTIFIERS table listing various bridge rectifiers such as 1A, 1.5A, 2A, 3A, 4A, 5A, 6A, 7A, 8A, 9A, 10A, 11A, 12A, 13A, 14A, 15A, 16A, 17A, 18A, 19A, 20A, 21A, 22A, 23A, 24A, 25A, 26A, 27A, 28A, 29A, 30A, 31A, 32A, 33A, 34A, 35A, 36A, 37A, 38A, 39A, 40A, 41A, 42A, 43A, 44A, 45A, 46A, 47A, 48A, 49A, 50A

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VOLTAGE CONTROLLED OSCILLATOR

Tired of the same old sounds from your synth? Bring a new variety to its waveforms with the VCDO! Design by Richard Thorp, development by Simon Bailey.

A conventional VCO can produce several waveforms, rich in harmonics, which may be filtered in order to alter the timbres. This is quite satisfactory for a wide range of musical requirements but the small range of waveforms available (usually sawtooth, square and triangle) and the coarse effects of analogue filters mean that it is impossible to produce many of the delicate, natural sounds which are so characteristic of modern digital synthesis. This module adds some exciting new possibilities to existing synthesizers by combining the flexibility of analogue voltage control with the clarity and realism of digitally generated waveforms.

As a unit, the voltage-controlled digital oscillator (VCDO) may be regarded as an ordinary VCO, but with a far greater range of waveforms. The design is fully compatible with existing synthesiser systems (1V/octave frequency control, 10V peak-to-peak output, linear and exponential modulation inputs) and offers the versatility of 32 different waveforms covering a wide variety of sound textures. A particular waveform can be selected either with push-button switches using a simple incremental system or by a combination of a push-button switch and suitable electronic pulses to the input provided. The module has a wide frequency range (approximately 30Hz to 10kHz) which allows it to be used as either an audio or modulation source.

Design

The VCDO works on a very simple principle. The 32 waveforms are encoded in a 2716 EPROM. Each waveform is represented

as a series of 64 8-bit numbers (a wavetable). A binary counter is made to run at a frequency generated by a VCO and to count through the waveform data. A DAC converts each item of data into an analogue voltage.

The VCO is based on the familiar CEM 3340 from Curtis Electromusic Specialties. In this case, the frequency range has been shifted upwards by altering the timing components. Accurate calibration of the oscillator is

HOW IT WORKS

IC1 is a CEM 3340, which with the addition of a few external resistors and capacitors functions as a high quality VCO, featuring accurate exponential and linear control of frequency. Three output waveforms are provided (triangle, sawtooth and pulse), but in this application only the pulse output is required, which is available at pin 4. A positive-going control voltage to pin 5 allows adjustment of the duty cycle of the pulse wave from approximately 0% to 100%. Frequency control is by means of timing capacitor C4 (10pF in this application) and multiple voltage control via resistors R8-11 to pin 15, which is a virtual earth summing node. Additionally, pin 13 may be employed as a linear frequency control input, providing the facility of linear frequency modulation. The VCO is configured such that it may be calibrated for an accurate +1V/octave response using presets RV1 and RV3. Provision has also been made for connection to an external VC clock via SK4 which, if permanently connected, allows the removal of the CEM 3340 and associated circuitry.

The pulse output is suitably attenuated to 5V by R17/ZD1 and is further processed by a Schmitt trigger (1/6 of IC2). Squaring of the pulse output is necessary as at extremely high frequencies an unacceptable amount of slewing is present, which inhibits operation of the next circuit block, a frequency doubler. The frequency doubling circuitry configured around IC3a and IC3b is included to provide an extra octave range. It functions by separately differentiating both edges of the square wave — C6/R18 differentiate negative edges and C7/R19 differentiate positive edges. The output of IC3b is then a series

of narrow pulses corresponding to both edges of the original square wave clock signal.

Ripple counter IC4 steps through the lower six address bits of IC9, a 2716 EPROM suitably programmed with wavetables. The data outputs at pins 9-17 of the 2716 go directly to IC10, which is a high speed multiplying digital-to-analogue converter (DAC 0800). The data is thus converted to an analogue voltage which is buffered by IC11. The same IC also scales the output to 10V peak-to-peak.

Ripple counter IC7 and IC8 are used to select the required waveform Number and Group respectively. Their clock inputs (pin 1) are fed by IC3c and IC3d which invert and debounce the switches SW1 and SW2. Additionally, an external input is provided so that a suitable waveform or pulse train may be used to advance the waveform Number in a particular Group. ZD2/R20 are included to limit an incoming externally generated pulse to +5V. R24 and C10 form a power-on reset network to take the reset inputs of the select counters high at switch-on in order to start at waveform Number 1 in Group 1.

IC5 and IC6 are BCD to decimal converters and LED drivers, displaying two decimal equivalents present on the upper five address lines of the 2716. Thus the two highest address lines A9 and A10 are decoded to light one of four green LEDs representing the waveform Group whilst control lines A6 to A8 light one of eight red LEDs representing the waveform Number.

Power supply requirements to the VCDO are +/-15V at approximately 40mA per rail and a separate +5V rail at 500mA.

LLED DIGITAL

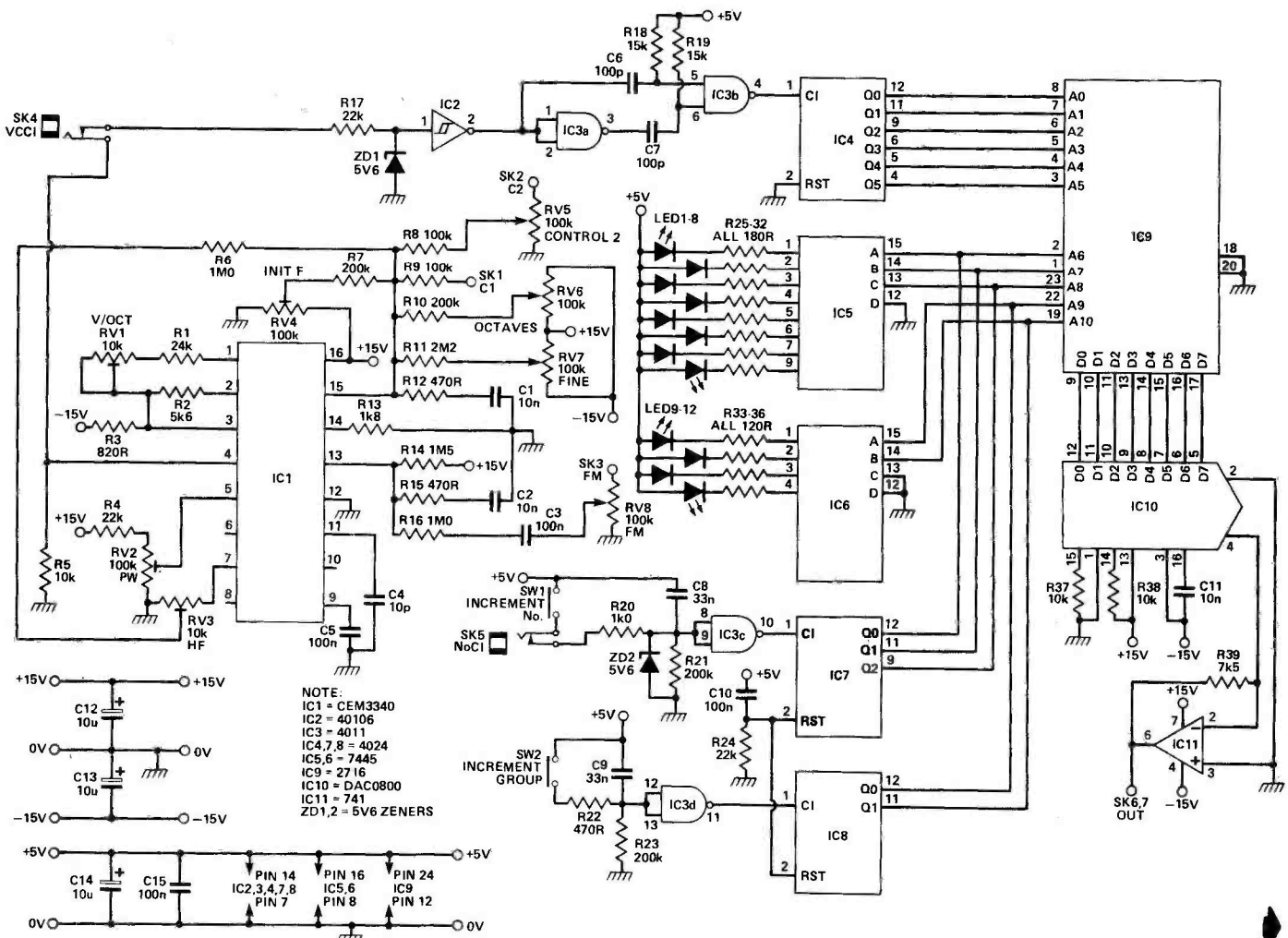
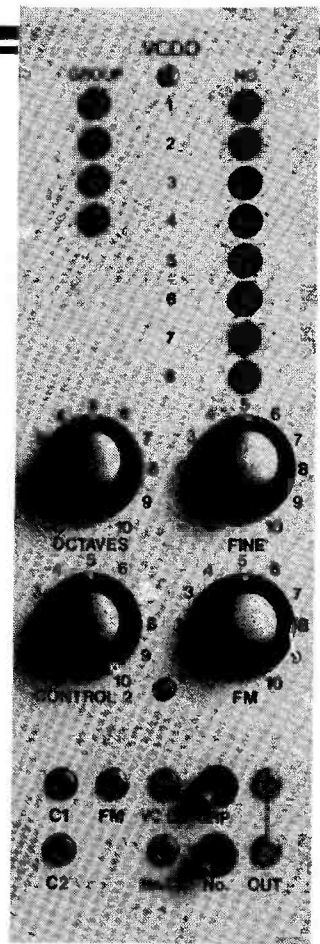
achieved by means of four presets. Coarse and fine frequency controls are available as well as depth controls for exponential and linear modulation (Control 2 and FM).

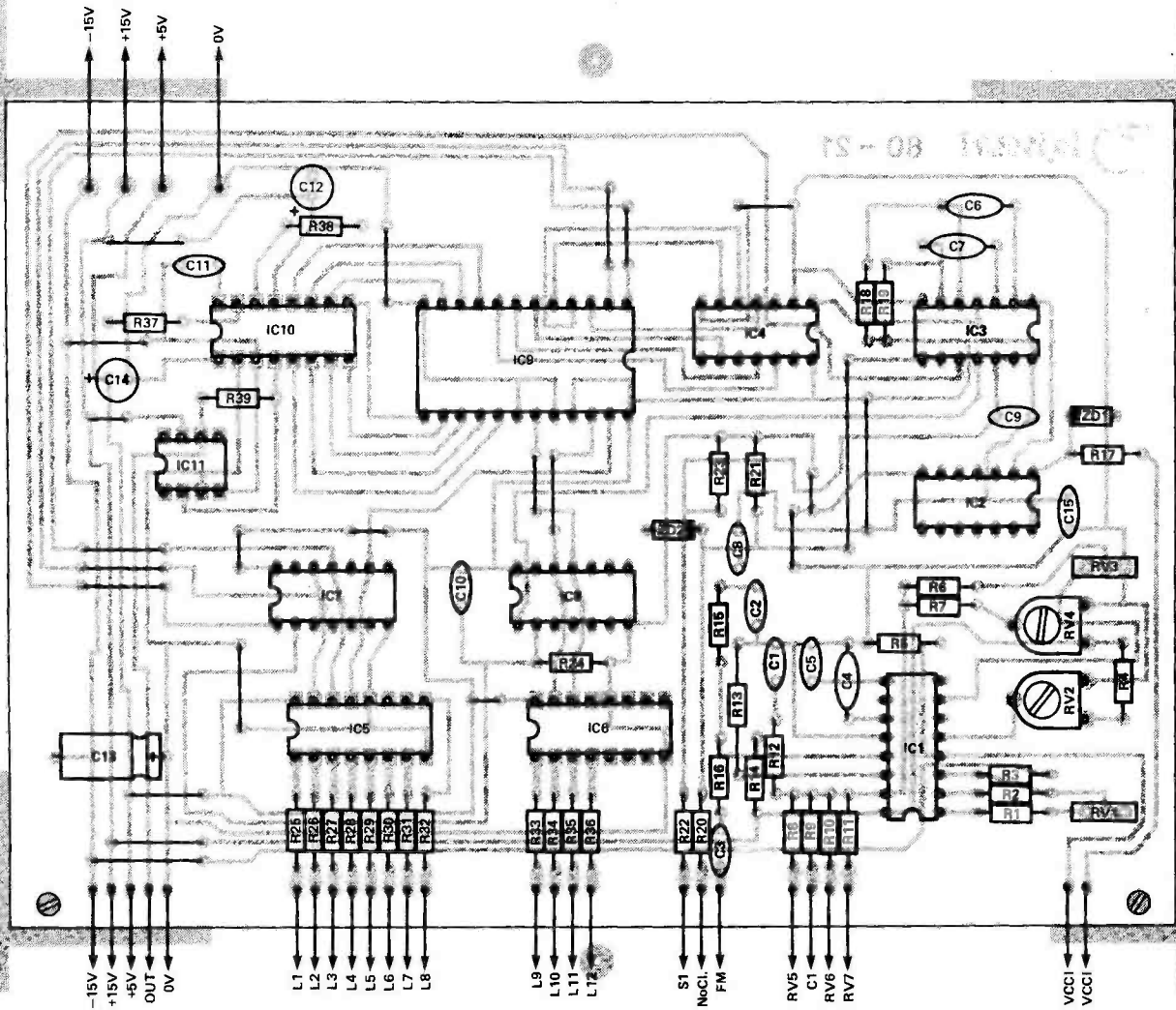
The pulse output of the 3340 is used as the clock for the waveform generation circuitry. After being cut down to 5V and passed through a Schmitt trigger to improve the shape, it is doubled in frequency by edge differentiation to give an extra octave range. Subsequently, a binary counter is incremented by the pulses and this steps through the 6 least significant address lines of the EPROM. A simple DAC and buffer convert the data outputs into voltages between 0 and +10V.

The remaining circuitry is concerned with the waveform selection. Two push-buttons are de-bounced and used to clock a pair of binary counters. One controls

the 2 most significant address lines of the 2716 and thus splits it into 4 groups designated Groups 1 to 4. The other counter controls a further 3 address lines and thus can select one of eight waveforms. The combination of two counters means that any particular waveform is quickly accessible. Inserting a jack plug into the waveform select (No. Cl.) input enables electronic control of the incrementation, opening up the possibility of timbral modulation and sequencing etc.

Indication of the waveform selected is by means of 4 green LEDs and 8 red LEDs, representing wave Group and wave Number respectively. These are driven by BCD-to-decimal converter/drivers which monitor the address lines. A simple RC network ensures that Group 1, Waveform 1 (a sine wave) is selected at switch-on.





PARTS LIST

RESISTORS (¼W, 5% unless otherwise stated)

R1	24k 1%
R2	5k6 1%
R3	820R
R4,17,24	22k
R5	10k
R6,16	1M0 1%
R7,10	200k 1%
R8,9	100k 1%
R11	2M2
R12,15,22	470R
R13	1k8 1%
R14	1M5 1%
R18,19	15k
R20	1k0
R21,23	200k
R25-32	180R (8 off)
R33-36	120R (4 off)
R37,38	10k 1%
R39	7k5
RV1,3	10k min multiturm
RV2	10k horiz preset
RV4	100k horiz Cermet preset
RV5-8	100k lin rotary pots

CAPACITORS

C1,2,11 10n min polyester

C3,5,10,15

C4 10p polystyrene

C6,7 100p polystyrene

C8,9 33n min polyester

C12,14 10u 35V radial electrolytic

C13 10u 25V axial electrolytic

SEMICONDUCTORS

IC1	CEM 3340
IC2	40106
IC3	4011
IC4,7,8	4024
IC5,6	7445
IC9	2716
IC10	DAC0800
IC11	741
LED1-8	5mm red LED
LED9-12	5mm green LED
ZD1,2	5V6 400mW zener

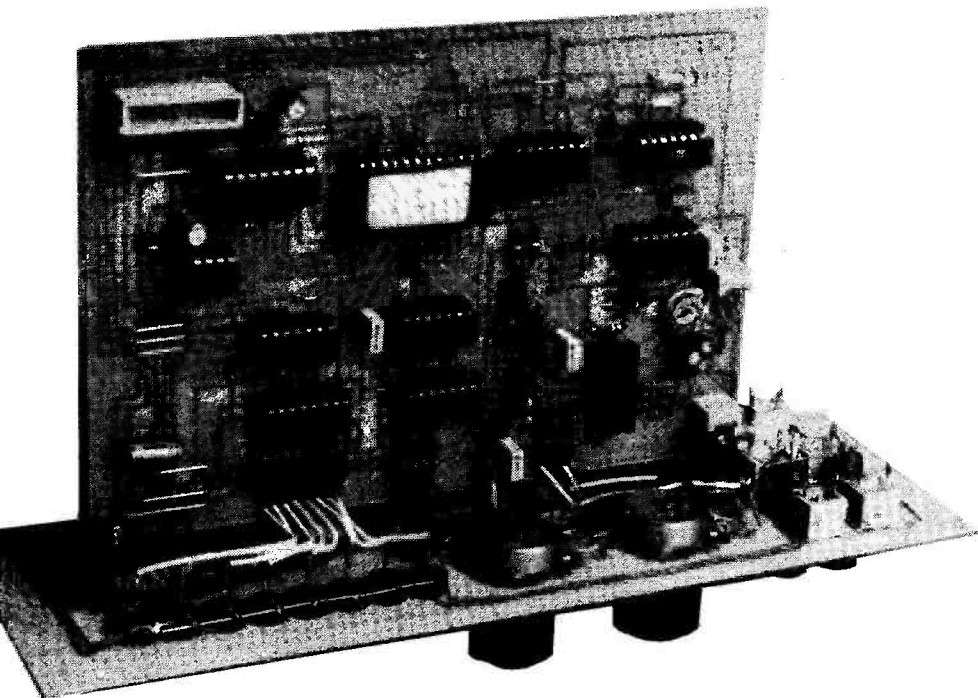
MISCELLANEOUS

SW1,2 momentary push-button switches, SK1-7 3.5mm min jack sockets (SK4,5 with break contacts), DIL Sockets (1 x 8 pin, 5 x 14 pin, 4 x 16 pin, 1 x 24 pin); PCB; wire, solder, knobs, etc.

Construction

There are a number of wire links to be made on the board and these should be inserted first. The rest of the components should then be fitted onto the PCB in order of increasing height (i.e. zener diodes, resistors, IC sockets, presets and capacitors). Note the orientation of the electrolytic capacitors and ensure that all the ICs are inserted as shown on the component overlay as they do not all have the same orientation. The use of a PCB solvent cleaner to remove residual flux is recommended.

Off the board, there are 12 LEDs, four potentiometers, seven jack sockets and two push-button switches to be wired up. These components may be mounted on a front panel as shown or in any other format that individual constructors may wish to use. The actual connections to be made are readily ascertained by using the circuit diagram and component overlay together.



The PCB has a space for a four pin CHIRI-type connector which may be used for the power supply connections rather than hardwiring them to the board.

Calibration

Once construction is complete and the unit has been carefully checked, set all presets to mid-position and power up. Calibration of the VCO circuitry is by way of four presets and is carried out as follows.

Firstly, RV2 is adjusted so that the unit operates over a frequency range from approximately 30Hz up to 30kHz. The correct setting of RV2 is likely to be slightly anti-clockwise from mid-way and can be recognised when the frequency may be increased (e.g. by RV6) without any noticeable sudden jumps.

The two multiturn presets, RV1 and RV3, are used to achieve a precise 1 volt/octave CV to frequency relationship and may be calibrated in a number of ways. The most convenient method is to use a previously calibrated keyboard, but failing this a variable voltage source which can be increased by precisely one volt may be used. Also required is some means of checking the output frequency. The simplest way is to take the output through an amplifier and speaker and to calibrate it by ear, providing the ear concerned has had some musical training. Alternatively, a frequency

meter or oscilloscope may be used to visually display the frequency.

Proceed with the calibration as follows: firstly, adjust RV3 so that its wiper is at the earth end of the track. With the oscillator set at some point on the range 150 to 500 Hz (set by RV4/6/7), check that when the control voltage input at C1 is increased by exactly 1V, the output frequency increases by one octave (ie, doubles). If not, adjust RV1 until it is. Repeat this check over the range 150 to 500 Hz.

Next, readjust the initial frequency to about 5kHz. Adjust RV3 until increasing the control voltage at C1 produces the required doubling of frequency.

Once these two adjustments have been done, the unit should track accurately over its entire range. Obviously, it is important that you should be able to measure the increase in the input control voltage accurately.

The final step in the calibration sequence is to adjust RV4 to give a convenient initial frequency when no inputs are connected, which to a large degree is a matter of personal taste. It may, for example, be set to 65.4Hz, which is the lowest note on a four octave C-C keyboard.

In Use

The VCDO kit (see Buylines) is supplied with a pre-programmed EPROM containing the data for 32 64-byte waveforms. Organised in 4

groups, these are as follows:-

1. Starting as a sine wave, this group progresses with the addition of extra harmonics in varying quantities, though none above the sixth are added.
2. The waveforms of this group contain some higher harmonics, and as a result sound brighter.
3. With lots of high harmonics and subdued lower harmonics and fundamental, these waveforms sound characteristically sharp and metallic.
4. This group contains some of the basic waveforms to be found on a conventional VCO (sawtooth, square, triangle, pulse etc.) plus one or two more unusual waveforms.

With suitable filtering and envelope shaping, a wide variety of sounds can be produced, both imitative and innovative. On the imitation side, Groups 1 and 2 can provide some very good church organs as well as xylophone, electric piano etc. Group 3 is ideally suited for bells, gongs, chimes and so on. Group 4 enables you to use the VCDO for conventional synthesis but it also includes some unusual waveforms unavailable on a standard VCO. As might be expected, the use of several VCDOs in a polyphonic system sounds especially impressive.

One or two unusual modes of operation yield some novel effects. Use of a linear FM patch produces sounds similar to those obtained from the recently popularised FM synthesisers. The waveform select input provides the possibility of cycling through any particular group, which can be quite dramatic when free-running or in time with the EG trigger from a sequencer/arpeggiator.

Additionally, the VCDO can operate as a modulation source. However, the output is stepped, and if being used as a frequency modulator for a VCO, for example, some form of filtering should be used in order to "smooth out" the waveform. This would be unnecessary for amplitude modulation.

BUYLINES ETI

A complete kit for the Voltage Controlled Digital Oscillator including all components noted in the parts list and a suitably programmed EPROM is available from Digisound Limited, 14/16 Queen Street, Blackpool, Lancs. FY1 1PQ for £47.75 inclusive of P&P and VAT. A front panel as featured is available for £3.80 fully inclusive.

THE ETI "SONNETI" COMBO



This month sees the departure of ETI Project Editor Phil Walker, who will shortly be returning to the electronics industry complete with his undisputed talents and indecipherable puns. But not before he's told us about the Sonneti, a combo unit guaranteed to turn anybody's farewell performance into the start of a new career.

The ETI Sonneti is an instrument amplifier suitable for use with lead guitar, bass guitar or keyboards. It doesn't have too many frills but it is capable of turning in a good performance without unnecessary fuss. The pre-amplifier and power supply have been designed to permit the simple addition of an echo

unit or similar effect, and whilst distortion-type effects are not specifically catered for there is no reason why they should not be included if desired.

The aim was to keep things as simple as possible, and to this end we have used a commercially-available combo cabinet and a ready-built power amplifier mod-

ule. There is nothing to stop ambitious constructors building their own cabinets, but it was not felt to be worthwhile designing and building a power amplifier for so basic an application.

We used a Crimson Elektrik CE1008 module, mostly because we happened to have one lying around, but there are many other modules on the market which would be suitable. The CE1008 is capable of 100W into an 8 ohm load when fed from a $\pm 45V$ supply and quite adequate power for the present purpose when supplied with $\pm 25V$. The output power can be increased by raising the supply voltage but the pre-amp regulator arrangements will have to be modified if more than $\pm 35V$ is used.

The power supply is a straightforward centre-tapped transformer feeding a bridge rectifier to give the split-rail supply. The transformer secondary voltage is 18-0-18 to give the $\pm 25V$ required and with a rating of 80VA is under very little strain. For 100W you would need 30-0-30V at around 120 to 150VA and C21 and 22 would have to be 63V types. You would also need pre-regulators for the pre-amp power supply to drop it down to about $\pm 30V$ — a simple resistor, transistor and zener diode arrangement would do.

The pre-amp section is

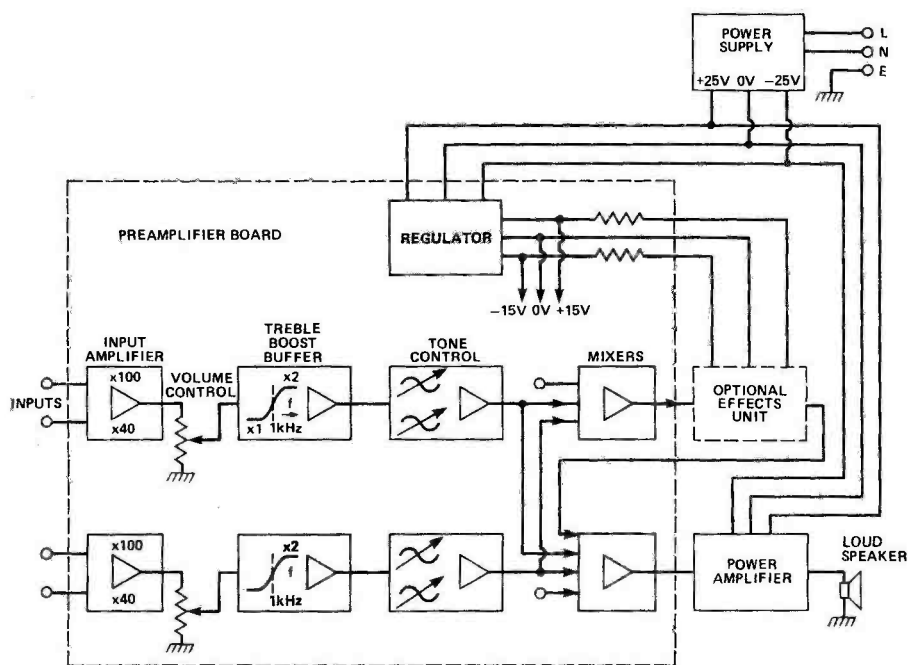


Fig.1 Block diagram of the combo unit.

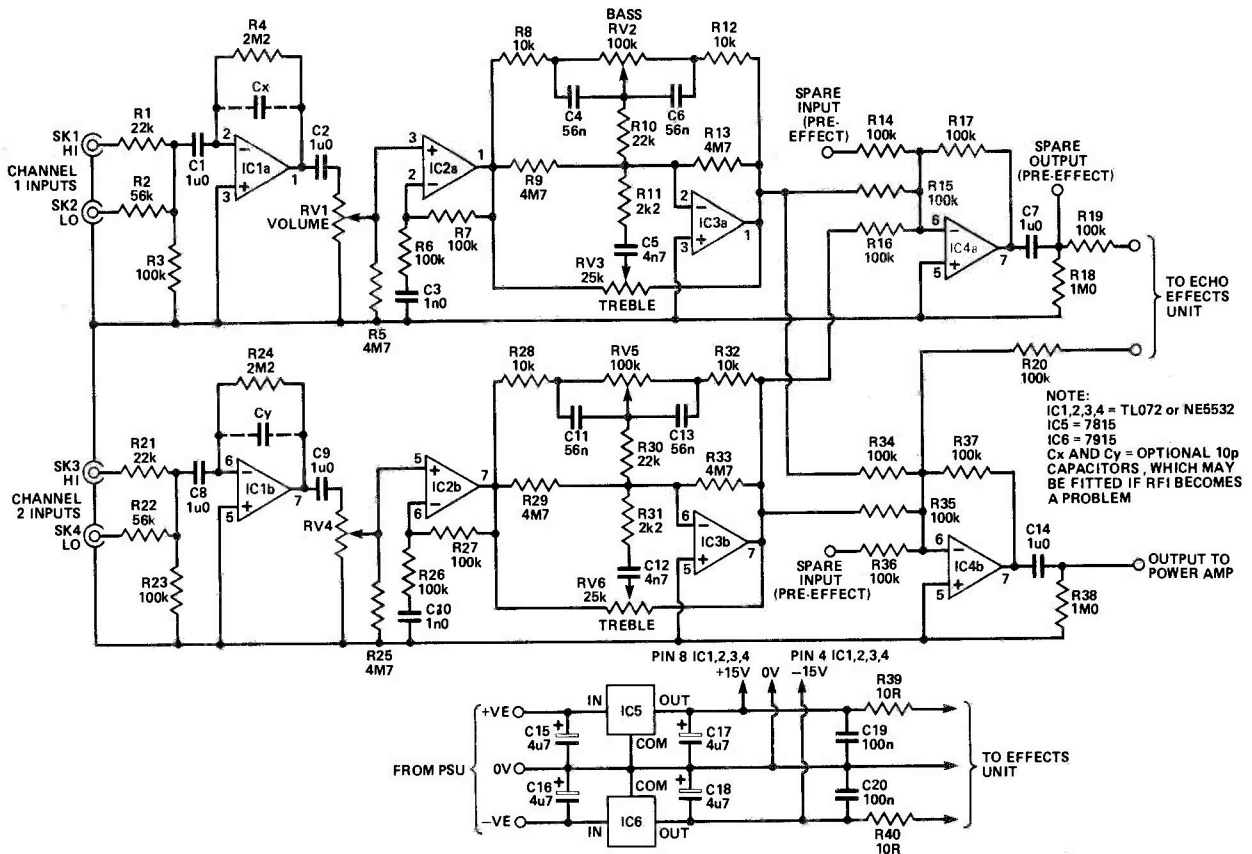


Fig.2 Circuit diagram of the preamplifiers and regulators.

designed as two identical channels each with hi and lo level inputs and volume, treble and bass controls. Both channels feed into the two mixer stages, one of which is designed to feed an echo or similar effects unit while the other drives the power amplifier input. This latter stage also has an input for a return signal from the optional effects unit, a configuration which reduces the possibility of electrical feedback through the effects unit. The preamplifiers are designed to give sensitivities of around 4 and 10mV on the hi and lo inputs respectively.

When this project was first assembled and tested using the author's guitar the sound produced was very muddy and "plonky". The guitar was known to produce a very wide range of sounds when used with commercial amplifiers, so the frequency response of the whole unit was tested and found to be flat to about 40kHz. It was decided to change the circuitry around IC2 to give a boost to the higher frequencies. Some component values in the tone control section were adjusted to improve the treble and expand its control range, and the final circuit gives a very good sound.

HOW IT WORKS

The preamplifier is the only part of this project which needs much explanation. It consists of two virtually identical channels. The inputs are connected via R1 and R2 and C1 to the input of IC1a. The values of R1 and R2 are such that the R1 input is about 2.5 times more sensitive than the other. The value of R4 connected as a negative feedback element round IC1a sets its gain to 100 from R1 input and 40 from the R2 input.

The output from this stage is coupled via C2 to the volume control RV1. From here the signal passes to IC2a which is configured such that it has a gain of 1 at low frequencies and 2 at high frequencies, the change in gain occurring between about 800 and 1600Hz.

The output from IC2a is a convenient low impedance drive for the tone control stage which follows. This is a familiar feedback configuration which is fairly simple but gives adequate results. Extra resistors have been incorporated in this and the previous stages so that the inputs to the op-amps will always have a DC path for their bias current should a potentiometer wiper become open circuit. This should prevent any alarming noises resulting from dirty contacts. The resistor R3 at the input prevents static build-up.

The outputs from the tone control stage of each channel are applied to the inputs of two mixer stages. The output of one of these is intended to drive an echo

or similar special effect circuit while the output of the other mixer drives the power amplifier. This second mixer has an extra input to take the return signal from the effects unit.

The power amplifier can be considered as a single, rather expensive, component. All that needs to be done is to supply suitable voltages and signal input and take the output to a loud-speaker. The specified module is capable of supplying 100W into an 8 ohm load but in this application the maximum output is somewhat less since the power supply voltage is only about 50 volts in total. The resulting output will be around 30 to 35 watts but could be raised by using a higher voltage transformer with appropriate modifications to associated components.

The power supply is a straightforward split rail configuration which gives about 25-0-25V from the 18-0-18V transformer. This is smoothed by C21 and C22 and applied to the power amplifier module. Integrated regulators IC5 and IC6 reduce this to the $\pm 15V$ required by the preamplifier and small capacitors connected across the supplies ensure stability and reduce the impedance at high frequencies. The regulated supply is made available to the effects card via the same connector which carries the effects input and output, and the 10R resistors R39 and R40 reduce the level of any noise produced on the card.

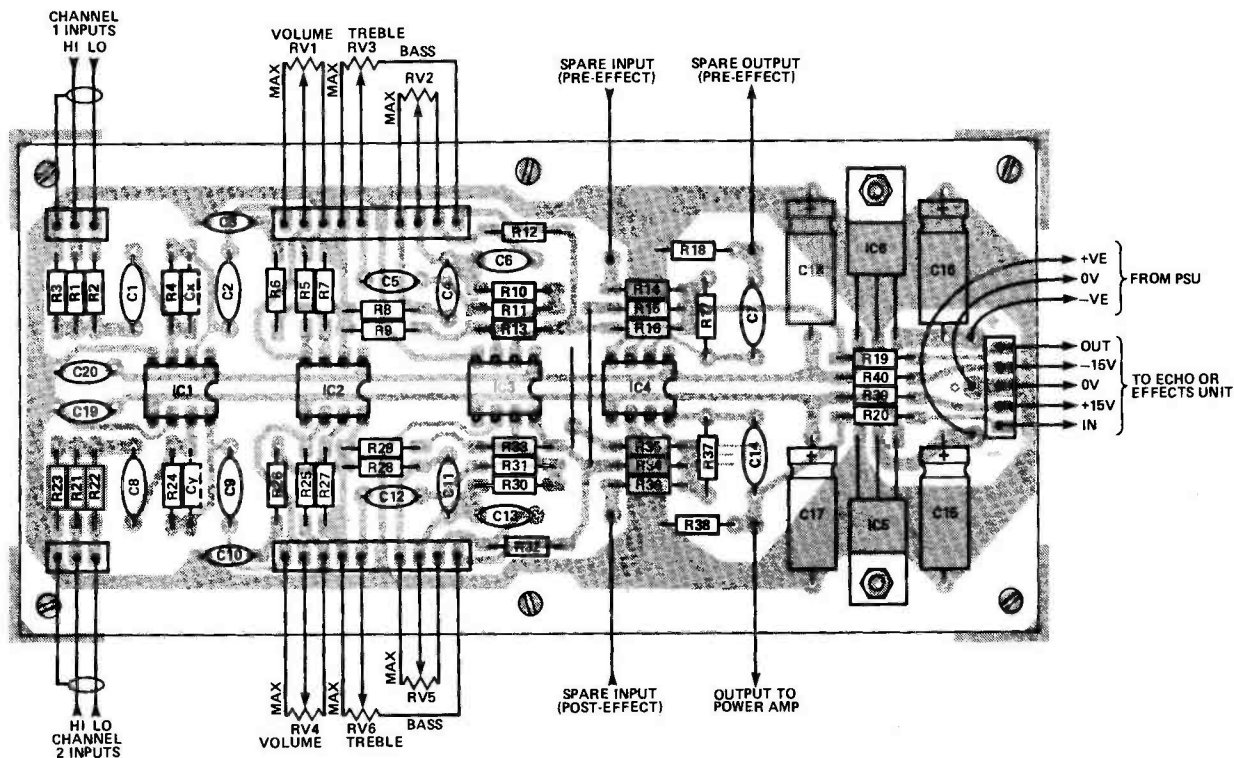


Fig.3 Component overlay of the preamplifier and regulator board.

PARTS LIST

RESISTORS (¼W carbon film 5%)

R1,10,21,30	22k
R2,22	56k
R3,6,7,14,15,16,17, 20,23,26,27,34,35, 36,37	100k
R4,24	2M2
R5,9,13,25,29,33	4M7
R8,12,28,32	10k
R11,31	2k2
R18,38	1M0
R19	100R
R39,40	10R
RV1,4	100k logarithmic potentiometer
RV2,5	100k linear potentiometer
RV3,6	25k linear potentiometer

CAPACITORS (layer type PCB mount polyester unless stated)

C1,2,7,8,9,14	1µ0 100V
C3,10	1n0 250V
C4,6,11,13	56n 250V
C5,12	4n7 250V

C15,16

4µ7 63V axial

electrolytic

C17,18

4µ7 25V axial

electrolytic

C19,20

100n 100V

C21,22

4700µ 40V can

electrolytic

SEMICONDUCTORS

IC1-4

TL072 or NE5532

— see text

IC5

7815

IC6

7915

BR1

200V 6A bridge

rectifier

MISCELLANEOUS

FS1

1A anti-surge
20mm fuse and
holder

LP1

240V neon
indicator,
panel-mounting

LS1

8R, 85W, 12"
McKenzie
C1285GP or similar

SK1-4

¼" chassis-
mounting jack
sockets

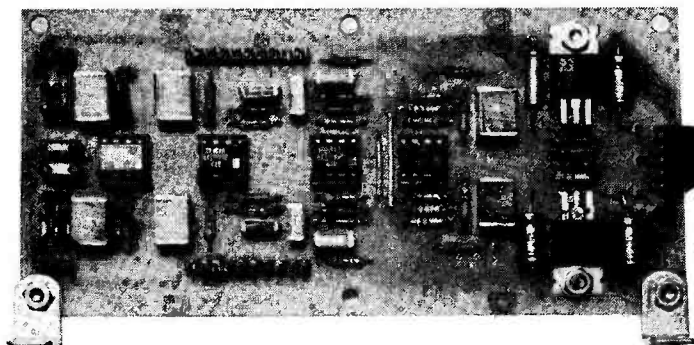
SW1

DPST mains toggle
switch

T1

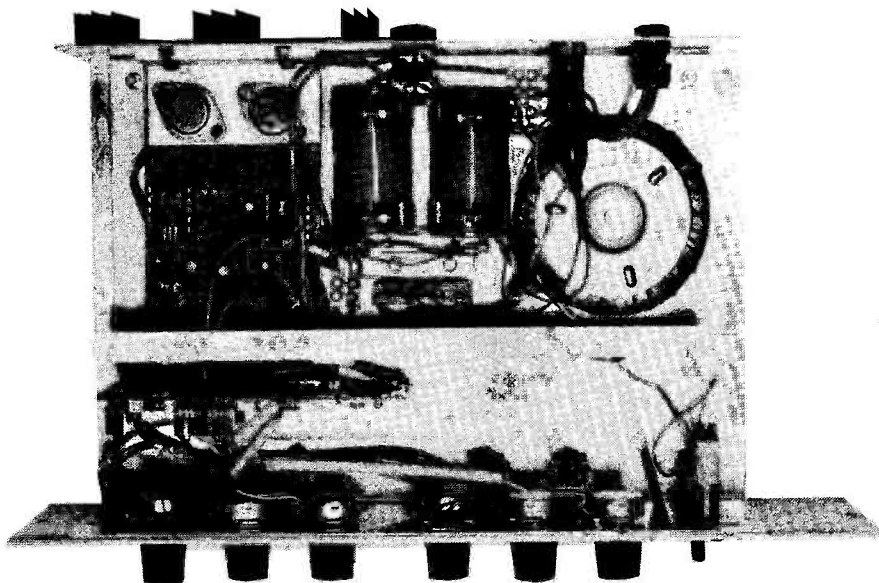
0-18 + 0-18V,
80VA toroidal
transformer

PCB; Crimson Elektrik CE1008 amplifier module or similar; two heatsinks, Maplin type FL42V or equivalent; PCB connectors if desired — 2 × 3 way, 2 × 10 way and 1 × 5 way plug and socket pairs; 4 × 8 pin DIL sockets; six knobs; Newrad NB19 or similar aluminium case; sheet aluminium for sub-chassis/screen, preamplifier screen and dummy front panel; ready-built combo cabinet or wood, cloth, etc to build; clamps for C21 and 22; strain relief bush for mains cable; two grommets for wires passing through internal screen; grommet for loudspeaker cable or ¼" jack socket and plug; brackets, nuts, bolts, solder tags, wire, etc.



Construction

The preamplifier PCB should be assembled first. The board has been designed so that PCB-type connectors can be used for the wiring to the potentiometers, input sockets and the optional effects card, and if you plan to use this system you should begin construction by soldering the appropriate connector halves to the PCB.



Plugs should be used for the potentiometer and input socket connections but the wiring to the effects card includes the supply rails and a socket should therefore be used so that there is no risk of bare pins being accidentally short-circuited. If you do not wish to use connectors simply poke the wires through the holes and solder in the usual way when the rest of the board has been assembled. If you intend using sockets for the ICs these should also be soldered into position before the rest of the components are installed.

Continue assembly by installing the two wire links and the solder pins and then the resistors and capacitors, taking particular care with the electrolytic capacitors C15-18 which may be damaged if they are not wired the correct way around. Pads are provided on the PCB for two 10p capacitors, Cx and Cy, in the feed-

back loops around IC1a and b. These will reduce the risk of radio frequency interference (RFI) and need only be installed if you have good reason to expect RFI problems. It is easy enough to add them later if you encounter problems when the unit is finished.

The last items to be soldered into position are the ICs. We used TL072 dual op-amps for ICs 1-4 but the more expensive NE5532 could be used if you require lower noise. A reasonable compromise would be to use an NE5532 in the IC1 position and TL072s in the other positions. If you use sockets it will be easy to swap ICs over to compare the performance of different types.

The amplifier is built into an aluminium box which is a little smaller than the slot at the top of the combo cabinet. An enlarged front panel, cut to suit the recess on the front of the cabinet, is

attached to the amplifier box by means of the potentiometer securing nuts, the jack socket bushes and two small screws. The complete unit is then held in place by two self-tapping screws which pass through either end of the panel and into the wooden uprights of the cabinet.

The internal layout of the amplifier is shown in Fig. 4. The power supply and the power amplifier module are mounted on a sub-chassis which is bent up at the front so as to form a screen between these components and the preamplifier. The advantages of using the sub-chassis are that it reduces the number of holes required in the bottom of the case and that this section can be built and wired up before being bolted into place. If you can't find anything that will serve as both sub-chassis and screen you could simply mount the components onto the bottom of the case and then use a piece of aluminium supported on brackets as the screen.

The preamplifier board is mounted vertically on two right-angle brackets immediately behind the front panel. This allows the input sockets and control potentiometers to be connected up using very short lengths of cable. By positioning the preamplifier board to one side, sufficient space is left to accommodate an effects board at a later date. A second screen is placed between the preamplifier and input circuitry and the mains switch and indicator at the far end of the panel. A small piece of thin aluminium is sufficient, bent at a right angle and held in place by the toggle switch.

Two heatsinks are bolted onto the rear of the case in line with the aluminium bracket on the power amplifier module. If the Newrad NB19 case is used as in our prototype, the heatsinks will project slightly beyond the back of the cabinet when the amplifier is slotted into place. This helps ensure a good flow of air for cooling but might be considered undesirable. Using a slightly shallower box will reduce or remove the projection, and if you can find one made from heavy gauge aluminium or bend one up yourself you might find that you don't need the heatsinks anyway. Whichever method you use, don't forget to smear some heatsink compound between the surfaces before assembly.

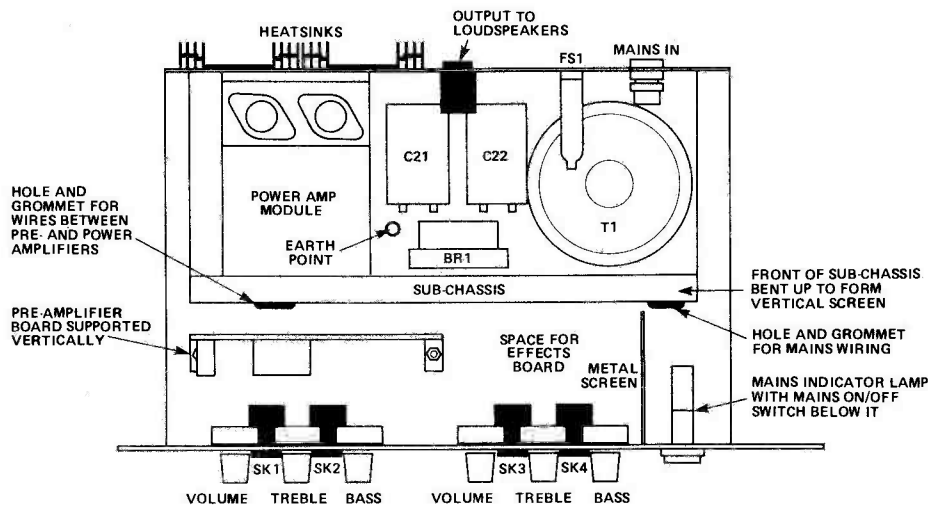


Fig.4 Layout of the major components within the amplifier case.

The wiring should present no problems provided the arrangement shown in Fig. 5 is followed closely. All of the earths are returned to one point so as to prevent the formation of hum loops, and care should be taken to ensure that no earth connection is inadvertently made elsewhere. The 1/4" jack sockets which are generally available have no connection between the earth tag and the mounting bush, but if for any reason you decide to use different sockets you should make sure that they are insulated from the panel.

Twin screened cable should be used for the connections to the volume controls and the input sockets, and single screened cable for the signal connection between the pre- and power amplifiers. The rest of the wiring, including the tone control connections, can all be made using un-screened wire. The short connections between the reservoir capacitors, the bridge rectifier and the earthing tag and the link between the earth connections on each pair of input sockets can all be made using tinned copper wire of a suitably

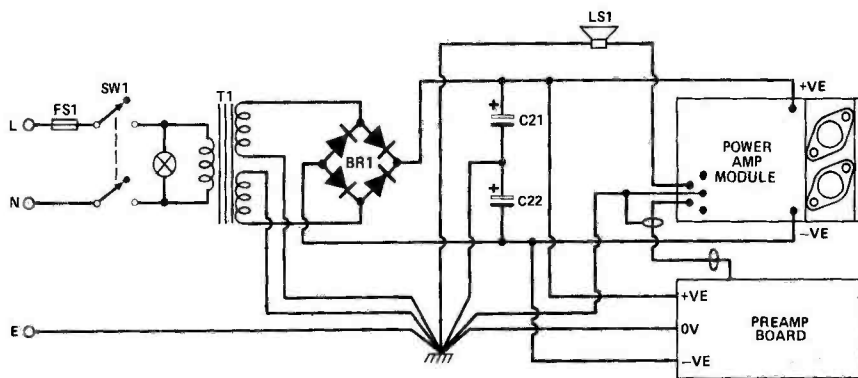


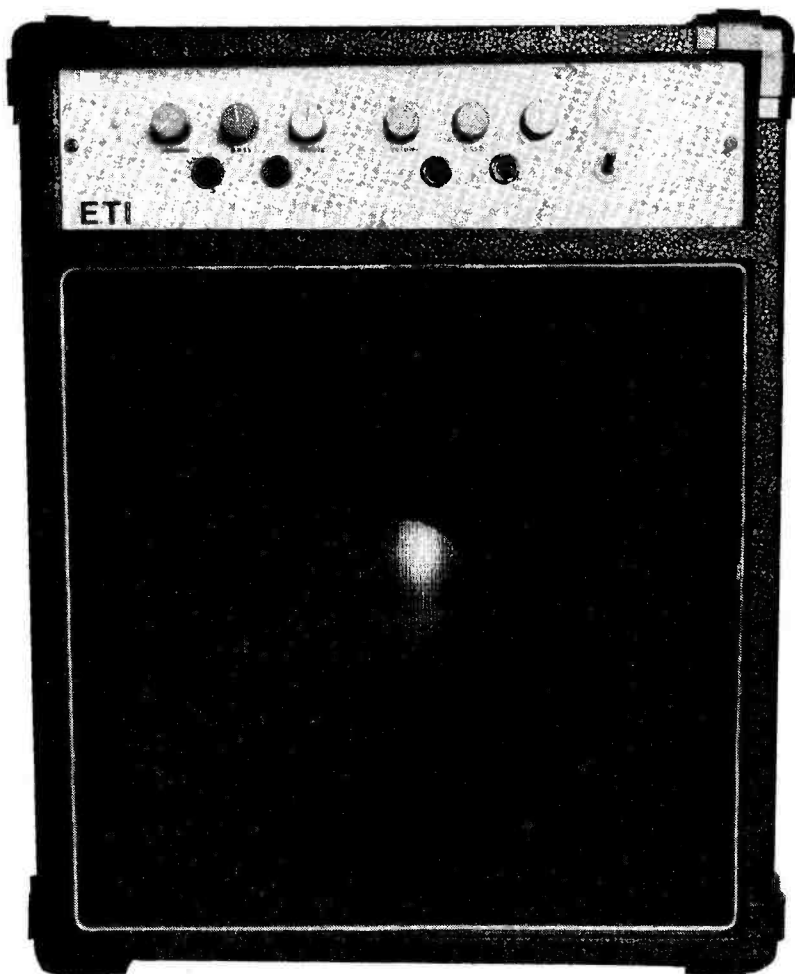
Fig.5 Wiring diagram. Note that all the earth connections are brought to one point.

heavy gauge.

The leads are brought out from the loudspeaker enclosure through a small hole in the bottom of the amplifier space. Rather than attach the leads permanently to the amplifier, we left a length hanging from the back of the cabinet, fitted it with a jack plug and provided a corresponding socket on the back of the amplifier. This allows the amplifier to be removed easily from the combo and used on its own.

BUYLINES

The cabinet we used was supplied by Wilmslow Audio, 35-39 Church Street, Wilmslow, Cheshire SK9 1AS, and they also stock a loudspeaker which is suitable but has a higher power rating than is needed for this project. The most recent prices we have are £35.75 inclusive for the cabinet and £32.45 for the C12 100GP loudspeaker, but we suggest you check with them before ordering; their telephone number is 0625-529599. We obtained the McKenzie loudspeaker used in the prototype from B.K. Electronics and you will find the price and other information you need in their advertisement elsewhere in this magazine. Crimson Elektrik amplifier modules are available from Bradley Marshall at their shop in London's Edgware Road, from Wilmslow Audio at the address above, or direct from the manufacturers at their Phoenix Works, 500 King Street, Longton, Stoke-on-Trent ST2 1EZ, tel 0782-330520. The most recent price we have for the CE1008 is £27.50 inclusive but again we recommend that you check this before ordering. The metal case for the amplifier was obtained from Newrad whose address and telephone number you will find in their advertisement. The only other items likely to cause any problems are the aluminium panels. If you live in the London area you could try H.L. Smith in the Edgware Road who will supply aluminium panels cut and bent to customer's requirements for a small charge. If you live elsewhere you will have to try local hardware shops or salvage some scrap aluminium and brush up your metal-bashing skills. The PCB is available from our PCB Service.



A CCD-delay line effects board for this project is currently under development, and we hope to bring you constructional details of it in a month or two. It will of course, require controls, so readers who intend building it are advised to postpone painting and lettering the front panel until it is published.

ETI

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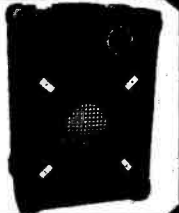
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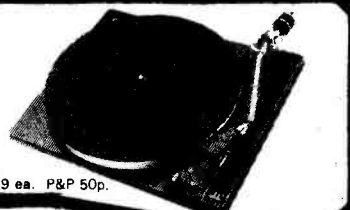
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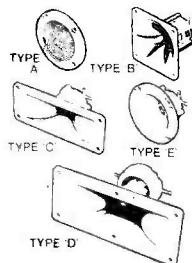
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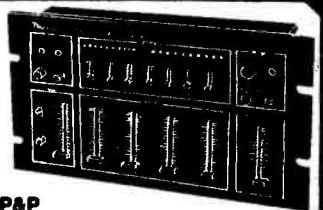
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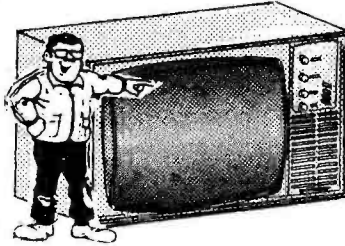
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THE REAL COMPONENTS

In this short(ish) series, John Linsley Hood will be looking at a range of components and their unwelcome characteristics.

It is becoming popular, among the lugubrious 'things aren't what they used to be' fraternity, to complain that Electronics Engineers are degenerating into technicians who merely connect 'black boxes' together, without any particular concern about what is in them or how they are made. But hasn't this always been true, to some extent, and isn't it also true of most other technical or engineering occupations?

In practice, everyone who uses bits and pieces provided by other people will be more concerned about how these are used, and how well they will work in that use, than about what they are. One doesn't expect an architect to be an expert in the manufacture of glass in order to be able to design windows, so why expect an electronics engineer to know just what is inside an 'op-amp IC' or a 'MSI CMOS gate'? Perhaps the mere fact that he can understand the jargon is an adequate qualification.

However, having set up the argument, I now want to nibble away at its foundations by saying that an architect who knows the relative qualities and costs of a borosilicate and a lead glass will be a better architect for this knowledge, and the mechanical engineer who knows the difference between EN20 and EN36 in steels will also be a more effective engineer because of that understanding.

So — how about our own bits and pieces, like the humble resistor and capacitor?

For a long time now, electronics engineers who have worked at the limits of this field, in very low noise systems, or at very high frequencies, or where high discrimination is needed between adjacent signals, have needed to be very fussy about component quality. Thanks to their efforts we now have some superb components at our disposal, whose qualities have come more into popular view because of the activities of the 'Ultra-Hi-Fi' buffs, who are very much sold on the need to use the most exotic things they can lay their hands on. But are these always as good for our purposes as the 'U-H-F' brigade would have us think. Let us have a look.

Resistors

These are made in a variety of kinds, and their purpose is to cause a voltage drop when current flows through them (remember $V=I \times R$). They will get hot if the current or voltage is high enough (heat, in watts = $V \times I$ or $I^2 R$). With transistor circuitry, the dissipation will usually be pretty small, so the 1/4 watt resistors are usually quite adequate, and will fit more tidily onto a printed circuit board. However, if one is in doubt, it is easy enough to check, using the formulas above, and a pocket calculator to ease the strain on the brain.

Wire Wound Types

For higher powers, it is most common to use 'wire-wound' resistors (which range from a watt or two as far

upwards as one has the strength to carry them). These are, as their name suggests, made by winding wire around a suitable fire-proof former, and joining a connector wire (or terminal, if they are big ones) on to the end, as I've sketched in Fig. 1. Obviously, if they are likely

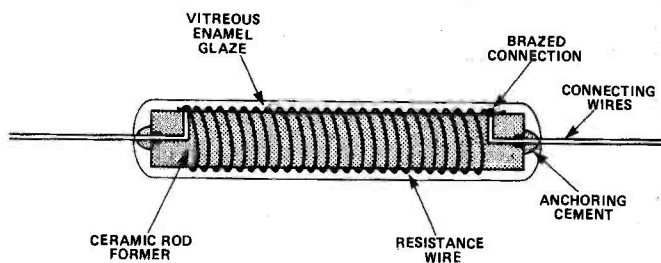


Fig. 1 A good quality wire-wound resistor (2–25W).

to get hot, and we want them to have the same resistance value when they are hot as when they are cold, the wire must have a low temperature coefficient of resistance. This usually means that they are wound from 'Eureka' or 'Constantan' wire. This a copper-nickel alloy, whose resistance doesn't change very much as it gets hot.

The snag with wire-wound resistors is that they have inductance, and the higher the value, and the more turns of wire that have to be wound round the former to get that resistance, the bigger the inductance will be. It is possible to make 'non-inductive' resistors by winding the wire in a zig-zag manner, so that there are just as many turns wound anti-clockwise, as there are wound in a clockwise rotation, but these are pretty rare.

A further point which has to be watched is that the former shouldn't expand as it warms up and stretch the wire wound round it, which would cause its resistance to increase — as in a strain gauge. Also, the wire has to be protected, to prevent it tarnishing or corroding, which would make it thinner. A layer of some heat-resistant vitreous enamel is usually fired on for this purpose, in the better WW resistors.

Apart from these snags, this is a pretty good type of resistor, which usually behaves in a nearly ideal manner.

Metal Glaze Types

These are made by firing onto a ceramic former a pottery type glaze, containing metallic salts, which make it

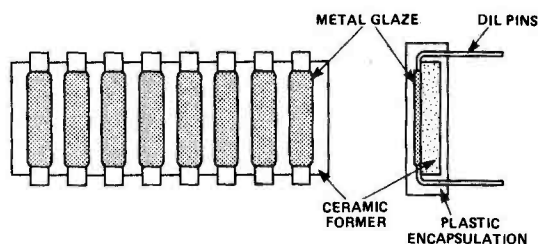


Fig. 2 Plastic encapsulated DIL metal glaze resistor array.

conductive. With proper composition these can have a low temperature coefficient, and can be made as non-inductive high-wattage replacements for WW types. However, you are most likely to find them as the single or dual-in-line devices I have sketched in Fig. 2, where they are plastic moulded like ICs, though some of these are carbon-film varieties.

Carbon Rod Types

These are the real grand-daddies of small power electronics resistors. They were around when I was a kid, and that was a good few years ago!

Their method of manufacture is to extrude a rod of mixed clay and graphite, in a combination which it is hoped will give the right sort of value. This is then chopped up into lengths, dried, fired in a kiln, and an end connection made by spraying it with metal, onto which a wire or other fixing can be soldered. I have shown the general scheme in Fig. 3. After the process is completed, the resistor will be impregnated with wax, and painted to say what value it is (for the time being).

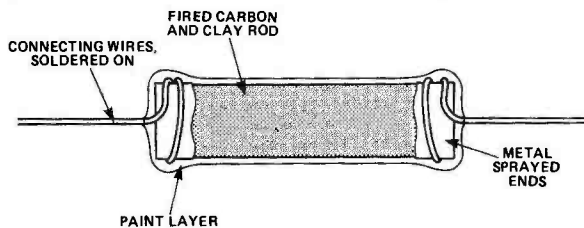


Fig. 3 Carbon rod-type resistor (½W–2W).

There are a lot of problems with these resistors, the first of which is that no-one really knows what sort of value is likely to happen after the firing process, and no two resistor rods are going to be the same anyway. The manufacturers got around this problem by automatic sorting machines, which measured the resistance value, and dropped the resistor into the appropriate box. A consequence of this was that if one wanted a 10k 20% tolerance resistor, it might be 8k or it might be 12k, but the only value it certainly wouldn't be is 10k, because these would have been sorted out for the 5% tolerance cut!

Another snag, which I recall from my early days in messing around with valves and 'steam' radios, was that if the resistor got a bit hot in use, when it cooled down again, it would have a different value. These are not now thought to be very good resistor types to use, unless one isn't very fussy, since they have a pretty poor noise figure — more about that later.

Carbon Film Types

These were the first of the really high quality low wattage resistors to be made, and for quite a long time commanded a premium price. They are made by depositing a thin layer of graphite on to the surface of a smooth ceramic rod, affixing end caps, which are usually crimped into position, as shown in Fig. 4, and then feeding them into an automatic machine, which measures their resistance, and then grinds a spiral groove through the film with a diamond cutter wheel, until the value has reached the required level, when the rod is dropped in to a collection chute.

The accuracy of these is as high as the accuracy of setting of the machine which made them, and it is quite common these days to find that a $\pm 5\%$ carbon film resistor is, on measurement, within 1% of the quoted value. As with other types, the resistor will be given a coat of a hard protective lacquer, usually epoxy based, prior to the paint rings which denote its value being applied.

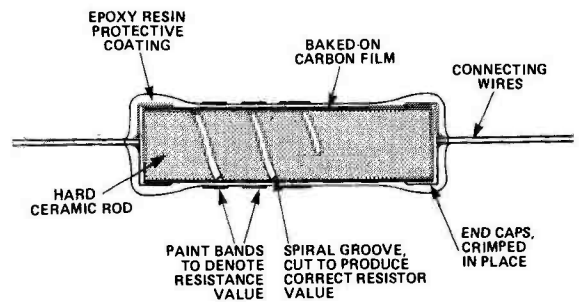


Fig. 4 Miniature carbon film high stability resistor (½W–2W).

Metal Oxide Types

These are usually made by firing a layer of thin oxide, which allows a low temperature coefficient, on to a 'Pyrex' glass rod former. Grooves are then ground, in spiral form, as in the carbon film types, to give the correct final value. They are then finished as the carbon film ones, though with rather more care. These were the first resistor types, I recall, to get the prestigious BS9000 approval, and, to my mind, are still the 'Rolls-Royce' of these components.

Metal Film Types

These are much like the carbon film ones except that a thin film of vacuum evaporated resistor alloy metal has been deposited on the surface, instead of a thin carbon layer. They are a bit more robust than carbon film types, and are available to very close tolerances.

Cermet Types

This is really just another name for 'metal glaze', though it is mainly used when this kind of resistor layer is going to be used in a potentiometer.

Some General Snags

Apart from the problems of inductance, temperature coefficient and instability of resistor value, mentioned above, there is also the snag about noise. This is partly a characteristic which is inherent in resistors, as the clouds of electrons inside them mill around, like crowds in a tube station at going-home time. Because, statistically, there will at any given moment be more going in one direction than in the other, and vice-versa, the net result is a 'noise' voltage which appears across the resistor, and is proportional to the square-root of the resistor value. As the temperature increases, the crowds of electrons become more agitated, and mill about more, so the noise voltage increases. So, in very low noise circuits, it is necessary to keep the resistance values as low as possible.

However, in addition to this, there is also the problem of 'excess noise', which is a function of the way the resistor is made, and the composition of the materials, and is due to a variety of causes, from the trapping of electrons by impurity 'holes' to spurious electrochemical potentials, or to piezo-electric or tribo-electric effects. Our old friend the carbon rod resistor is the worst offender here.

An additional problem which would worry an audio amplifier designer, is the voltage dependence of resistance. By this I mean the sort of change in resistance value which can occur as a function of the voltage applied across it — regardless of its change in temperature. This can generate odd harmonics in the signal waveform.

The final problem is that of asymmetry in resistance, due to slight rectification effects. Happily this is rare.

Looking at these problems, which is the best resistor to use. Well, apart from inductance, the wire-wound ones are very snag free. Next, in descending order of goodness come the metal oxide or metal film, the carbon film the metal glaze, and a long way behind, the carbon rod types.

Capacitors

These are best divided into 'polar' (ie, electrolytic) and 'non-polar' (ie plastic film or ceramic) types. The polar ones are those which will give a lot of capacitance in a small space, but need, generally, to be connected the right way round or they become either medium value resistors, or miniature canons, depending on the voltage and current available. More fun to watch from the other side of a stout window, in someone else's amplifier.

Plastic Film Dielectric Types

The plastic film dielectric types — they used to be made from waxed paper, but happily no longer, except in some exotic polychlorinated biphenyl impregnated systems, for power use — are not fussy about which way round they are connected, but tend to be a bit bulky and dear if one wants much in the way of microfarads. These will normally use polystyrene, polyester, polycarbonate or polypropylene films as the insulating dielectric between the two 'plates' to which one makes the electrical connections.

The best kind of 'plate' in a plastic film capacitor is a thin foil of high conductivity aluminium. Two of these will normally be wound up in a 'swiss roll' fashion, sandwiched between a pair of strips of plastic film, as I have shown in Fig. 5. One or more conducting wires or

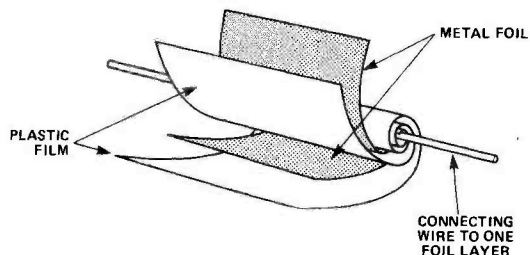


Fig. 5 The construction of 'film-foil' capacitors.

strips will then be led out of the body before it is wound, or perhaps while it is being wound, to make contact with the foils, and in the case of a polystyrene film capacitor, for example, the whole lot is then heated in an oven to make the plastic shrink and fuse, to give the shape shown in Fig. 6. Note at this point that one end will be identified, often with red dye, to tell you which is the outside layer of foil. If this is earthed, perhaps, it will screen the inner one.



Fig. 6 Finished 'film-foil' capacitor.

If one applies too high a voltage, the insulating film will puncture, and the capacitor will become 'short circuited'. This snag is avoided by using a vacuum evaporated, thin, layer of aluminium, on both sides of the film dielectric, as the conducting 'plate'. If the dielectric breaks down, in this case, the discharge of the capacitor through the pin-hole will blast away the evaporated metal layer around the puncture, and the

capacitor will 'self heal'. The price which is paid for this, is that the metal plate, being much thinner, hasn't got as good a conductivity, so an attempt to keep the internal resistance of the capacitor low is made by sputtering or spraying metal all over the exposed ends of the evaporated layer, as I have sketched in Fig. 7.

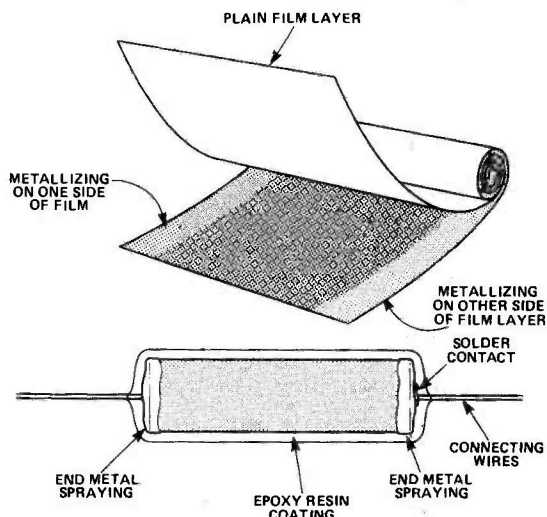


Fig. 7 'Metallised film' capacitor.

Because the evaporated metal 'plate' is so much thinner than a foil plate, these capacitor types give a bigger capacitance for the same physical size, and with the very thin film polycarbonate types, quite high capacitances, up to, say, 10uF, can be obtained in relatively small packages. The most common capacitor of this type is the 'polyester' one, usually based on a 'mylar' or 'melinex' polyethylene terephthalate film. This is thin because it is stretched in both directions, like the soap film in a bubble.

Ceramic Capacitors

Ceramic dielectric capacitors take advantage of the fact that some fired materials, like titanium dioxide, barium titanate, or barium titanate-zirconate, can have dielectric constants anywhere between 90 and 45,000, as compared with 2.2-4 for plastic films. Since the capacitance of a capacitor (its ability to store charge) depends directly on the dielectric constant of the insulation (the formula is $C(\text{uf}) = 0.225AK/D$, where A is the area of each plate, in sq. in., K is the dielectric constant and D is the separation between the plates), the higher the dielectric constant the more uFs in a given size.

Well, what's the snag? It is that the dielectric constant of these ceramic materials is wildly temperature dependent. The capacitor will usually have its characteristics printed on the side; for example, N750 means a temperature coefficient which is negative, and to the tune of 750 parts per million, per degree centigrade. Similarly, P100 is positive (ie., the capacitance increases with temperature) to the tune of 100 ppm°C. NPO means that it doesn't change at all, but you'll only find these in values up to about 100pF. The large capacitance, small size ones, like the pea sized 0.1uF/60V types, will all be N750 or maybe even N4500. Also, when they say '0.1uF' they mean somewhere in the range of 0.25uF-0.1uF!

Electrolytics

The electrolytic types, nowadays either aluminium or tantalum, rely on the formation of a thin continuous film of an insulating oxide layer on the 'anode', the +ve plate of the capacitor, as a result of electrolytic action occurring in the 'electrolyte'. Not only is the layer very thin, but

it has a fairly high dielectric constant, and if the 'plates' are etched to give a high effective surface area too, very high capacitance values can be obtained in small packages. Also, since the oxide film is formed by the passage of current through the unit, it follows that if it punctures, it will soon heal again by growing itself a bit of replacement oxide where the hole was.

The big problems with the electrolytic types, apart from some other more exotic defects which I will leave to later, were that they leaked (all the time!), they had a fairly high internal inductance, because of the way the plates were wound, and in use, they tended to behave as though they had a small resistor always connected in series with them, especially at higher frequencies. The big advantage of tantalum electrolytics is that their internal leakage can be exceedingly small, and they can even survive a small reverse voltage, say up to 1.5V. Aluminium electrolytics will survive up to about only 0.5V.

Recent developments have led to some very low leakage aluminium electrolytics too, and a big effort has been made to produce low 'equivalent series resistance' (low ESR) aluminium types. These are not yet quite in the league of tantalums for μFs per ml, but they are catching up.

Snags

Some people (not me this time, I spent many years working on, and designing instruments to test, plastics films for capacitor dielectrics) consider the capacitor to be the weakest link in most electronics — especially Hi-Fi — and think that the ideal audio amp. would be one without capacitors. Certainly, they have a lot of problems.

Consider how a capacitor works. A layer of some insulating material has a metal plate on either side, schematically shown in Fig. 8a. When a voltage is applied, the dielectric polarises, and negative and positive charges effectively move towards the two charged plates, giving the 'charging current', as in Fig. 8b. If the applied voltage is reversed the charges will require to

move towards the other plate, as in Fig. 8c. The movement of these charges may, in reality, be occasioned by the physical rotation of a molecule with a lop-sided charge as part of its structure.

There may then be some frictional energy losses in its rotation, and the higher the frequency, the worse these may be. These are known as the 'dielectric losses' of the capacitor, or ' $\text{Tan } \delta$ ', (an expression of the ratio, as an angle, between the capacitive and resistive parts of the capacitor). But maybe not all of the molecules reorient on the change of charge, this leads to what is known as stored charge, or 'hysteresis'. Or, again, what if the extent of polarisation is a bit non-linear with applied voltage. This would lead to the capacitance being voltage dependent, as well as being temperature and frequency dependent, which it will be anyway.

Voltage dependence of capacitance leads to the generation of harmonics in the current flow through the component, and is a well known trouble to power station engineers. Stored charge and hysteresis lead to lots of odd nasties. Internal series and leakage resistances lead to other problems, which the designer has to note. Finally, unlike resistors, capacitors don't usually have a precisely specified value: $\pm 20\%$ is usually a fair average, apart from polystyrene ones, which are quite precisely specified. Electrolytics may be anywhere between $+100\%$ and -25% in value. Fortunately, the actual value often doesn't matter all that much.

The stability of the capacitance value depends on a lot of factors. In the case of the plastic film types, it is mainly a question of the stability of the physical structure, though if there is a lot of self-healing, in metallised types, the available plate area will get less.

In electrolytics, the stability depends mainly on loss of electrolyte, and one should expect a steady and continuing decrease in capacitance with time. Advice here is to be generous in chosen values to begin with.

So — how does one choose the best capacitor for the job? The main moral is to use the biggest capacitor, physically, that you have room for. Usually small size implies a price which has to be paid somewhere. For HT supply decoupling, use a 'low ESR' type electrolytic, if one is available, and by-pass it by a suitable, low inductance non-polar type, say $0.22\mu\text{F}$ or $0.1\mu\text{F}$. If you are really fussy, you can by-pass this by a smaller value (hence lower internal inductance) capacitor yet again, to make sure your HT lines offer as low an impedance to higher frequencies as they do to 50–60Hz.

In audio systems, choose the capacitor with the dielectric having the lowest dielectric loss, which will probably also be the one with the lowest hysteresis, since it implies either no charge movement, or little friction in this. Polypropylene is the best here, followed by polystyrene (a close second), polycarbonate, polyester, low k ceramics and high k ceramics. Finally, if it is essential to use an electrolytic at all in the signal path, use an aluminium electrolytic. Tantalums have a rather bad image, nowadays, in respect of sound clarity. Also, between capacitors having the same dielectric, metal foil plates are preferable to evaporated metal film ('metallised') types.

Also, be generous in respect of the voltage and, in power supplies, the ripple current ratings of your capacitors. Electrolytics may survive brief voltage overloads; foil types will not.

Nowadays, capacitors don't usually introduce much circuit noise, apart from the thermal noise associated with their effective impedance, but, remember, in an electrolytic, if there is current flow, that current will be discontinuous, and very noisy.

Next month, bipolar transistors.

ETI

ETI MARCH 1985

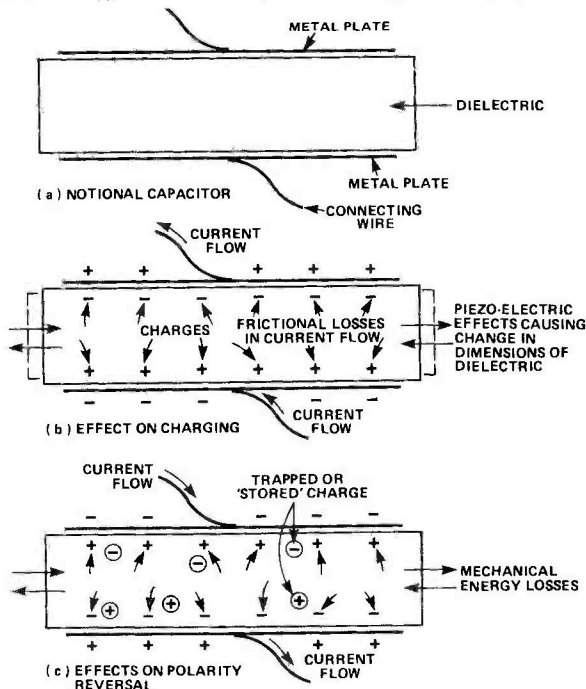


Fig. 8 Physical effects within a capacitor: (a) notional capacitor; (b) effect on charging; (c) effects on polarity reversal.

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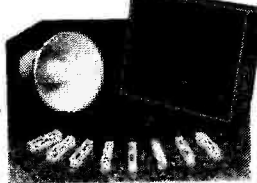
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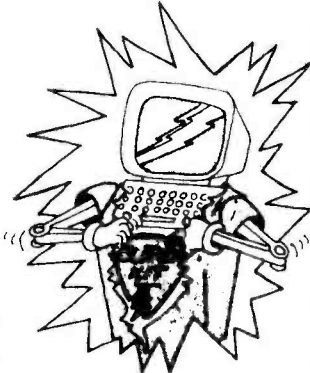
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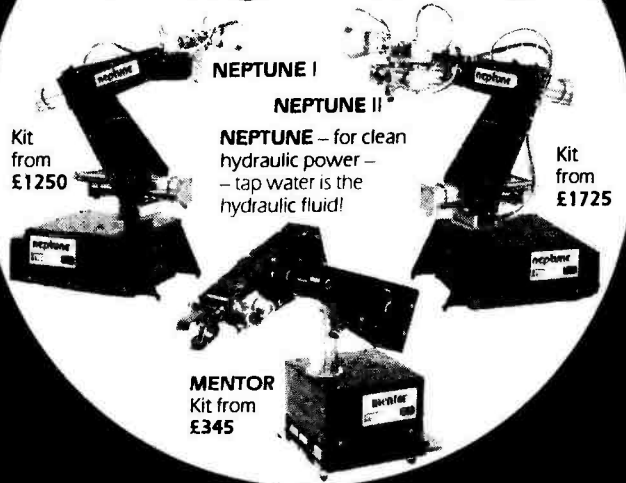
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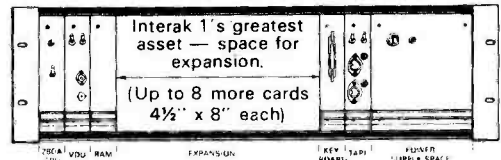
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SINGLE BOARD CONTROLLER

Mike Bedford considers the new Single Board Controller from Microtan Computer Systems Ltd and describes some simple modifications which will allow it to be used as a low-cost control computer.

Despite the increasingly large number of home computers on the market there are still surprisingly few which are aimed at the electronics enthusiast. Most machines are entirely suitable for game playing and BASIC programming, having such facilities as medium resolution colour graphics and sound effects, but they do not lend themselves to learning about the hardware or machine code programming. One product which has become known as a "hardware man's machine" is the Microtan 65, a number of add-ons for which have been featured in ETI. One drawback of the Microtan 65 is that the design is now somewhat dated, the single board having very little memory and being based upon the 6502 processor.

Out of the same stable has now come the Single Board Controller, which is being marketed by Microtan Computer Systems Ltd. This board uses the same bus specification as the Microtan 65 and can therefore be interfaced with previous Tangerine peripheral boards, but it can also be configured to use the 6809, regarded by many as the most powerful 8 bit processor. Other suitable processors are the 6802 and the 6808 which are versions of the 6800 with on-chip clock and RAM, but in this article the discussion will be restricted to the 6502 and 6809. The controller can also take up to 56K of memory on the one board.

The controller is available either as a complete board, as a kit of parts or as a bare PCB, monitor EPROMs being available separately if this latter option is chosen. As such, the controller forms the basis of an attractive

system for the more serious home computing enthusiast and especially those with a hardware bias.

The System

The single board controller has been artworked in such a way that it may take either a 6502 or 6809 processor, so the types of system which may be built around it fall into two categories. A 6502-based system will be similar in many ways to a system built around the original Microtan 65, although clock frequencies up to 1.5 MHz may be used which is twice the speed of the Microtan. The CBUG monitor will be used and will give

all the usual facilities of display/modify memory, setting breakpoints, etc, plus a line assembler and disassembler. This system will also allow BASIC resident in EPROM to be added.

A 6809 based system may be run at 1MHz or 2MHz and will use a system monitor called TVBUG. Monitor facilities are similar to those in CBUG except that the line assembler/disassembler is not included but routines for booting from disc and writing MIKBUG compatible records via the serial port are. It should be noted that the single board does not include any video circuitry, so a minimum system must either include the VDU card marketed by MCS Ltd or alternatively some sort of computer terminal interfaced via the RS232 port.

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P	TOGGLE PRINTER OUTPUT
R	DISPLAY/MODIFY REGISTER
S	DISPLAY STACK CONTENTS
V	COMPARE MEMORY BLOCK
W	WARM START FLEX OPERATING SYSTEM
X	REMOVE BREAKPOINTS
b	BUILD S1-S9 TAPE BLOCK
l	LOAD TAPE
s	SAVE MEMORY AS TAPE FILE
v	VERIFY TAPE

Table 1. Commands available with CBUG (6502).

M	MEMORY MODIFY/EXAMINE
L	LIST MEMORY
G	GO (EXECUTE PROGRAM)
R	REGISTER MODIFY/EXAMINE
S	SINGLE STEP MODE
N	NORMAL (NON SINGLE STEP) MODE
P	PROCEED (IN SINGLE STEP MODE)
B	SET/CLEAR BREAKPOINTS
O	OFFSETT CALCULATION
C	COPY MEMORY BLOCK
BAS	BASIC COLD START
WAR	BASIC WARM START
D	DUMP TO CASSETTE TAPE
E	EXAMINE CASSETTE TAPE
F	FETCH FROM CASSETTE TAPE
T	TRANSLATE (SINGLE LINE ASSEMBLER)
I	DIS-ASSEMBLER

Table 2. Commands available with TVBUG (6809).

PARTS LIST

RESISTORS

R1	220R	only for 20mA C/L
R2	220R	only for RS232
R3	4k7	only for RS232
R4	1k0	only for RS232
R5,11,12,14	4k7	
R6	120k	only for cassette interface
R7,8	10k	only for cassette interface
R9,13	470R	only for cassette interface
R10	10k	only for 20mA C/L
RP1	4k7 SIL pack	(7 commoned)
RP2	1k0 SIL pack	(7 commoned)
RP3	10k SIL pack	(4 separate resistors)
RP4	1k0 SIL pack	(4 separate resistors)

CAPACITORS

C1,7-14	100n	
C2,15	10n	
C3	100p	
C4,6	47n	only for cassette interface
C5	100u	

DISCRETE SEMICONDUCTORS

Tr1,3	BC184*	only for RS232
Tr2	BC184*	only for cassette interface
* NOTE BC184 HAS DIFFERENT PIN OUT TO BC184L		
D1	1N4001	only for serial I/O
D2	1N4001	
D3	1N4001	
XTAL 1	8.0MHz or 6.0MHz	8.0MHz for 1 or 2MHz operation 6.0MHz for 0.75 or 1.5MHz
XTAL 2	1.8432 MHz	only for serial I/O

INTEGRATED CIRCUITS

B1	6522	Always fitted for use in computer.
B2	6522	For control applications one or two 6522s may be fitted depending on application. May be replaced by 6821s as described in text. For frequencies above 1MHz use 6522A/68B21.
C1	74LS393	
C2	874LS04	
C3	LM358N	Only for cassette interface
D1	6551	Only for serial I/O. For frequencies above 1 MHz use 6551A.
D2	6809	Either D2 or D3 should be selected.
D3	6502	For frequencies above 1MHz use 68B09/6502A.
D4	75150	only required for RS232
E2	74LS244	May be replaced by wire links for single board control application (see text).
E3	74LS244	
F3	74LS139	
G3	74LS00	
H3	74LS266	
J3	74LS12	
K3	74LS10	
L3	74LS08	
M3	74LS138	
N2	74LS245	
N3	74S288	Not required for single board applications. Memory mapping PROM. Must be programmed as described in text or obtained from MCS. An alternative for simple control application is described in the text.
E1,F1,F2,H1,H2		Memory fitted as required
K1,K2,L1,L2		For 6502 computer system the minimum configuration is CBUG(2732) in E1, 6116 in F2. For 6809 computer system the minimum configuration is TVBUG(2732) in E1, 6116 in L1.

MISCELLANEOUS

PCB; edge connector 2X32 way A+B DIN Euro-connector; IC sockets as required.

From these minimal systems, which will allow 6502 or 6809 machine code programming and may well be adequate for those whose main interest is computer hardware, many upgrade paths are available. Hundreds of K of RAM or EPROM may be added in paged memory configuration. The addition of a disc controller and disc drives allows the FLEX or OS/9 operating system to be run on the 6809 board or TANDOS on the 6502 controller. Alternatively a Z80 card is available and allows the industry standard CP/M disc operating system to be run on systems with either processor. Other options include high resolution colour graphics, sound effects, serial and parallel I/O, EPROM programmers, real time clocks etc. Table 1 and Table 2 list the commands available under CBUG and TVBUG respectively.

The Board as a Controller

Some months ago, the author started to design a minimum configuration 6809 card to control the ETI Universal EPROM programmer in a stand-alone situation. It soon became clear that this was unnecessary because a board which would do this task at a reasonable cost was already available. Admittedly the 6502/6809 single board controller was not designed for this type of application, and it could be argued that it is a waste to use a board of this complexity for a pure control function.

This would be true if the board was only available fully built, but the fact that a bare board can be obtained and populated only as required for the particular application makes it quite suitable. The cost for control applications can be further reduced by some slight circuit modifications which remove the need for some of the more expensive components. For logic designs of reasonable complexity, the cost of a minimum configuration single board controller will be less than the component cost of a design using discrete TTL devices without even considering the time and expense of PCB artwork and manufacture.

The Circuit

The object of this section, How It Works and the constructional details is to open the board up to the electronics enthusiast. The

documentation currently provided by MCS Ltd does not really do justice to the product, a circuit diagram having only just been released, and the one presented here is more comprehensive being the result of many hours tracing the circuit from a bare PCB.

The circuit consists of:

- a) The processor, which may be either a 6502 or a 6809 running at a variety of clock frequencies.
- b) 9 sockets which will take standard JEDEC packages, allowing 2K, 4K or 8K RAMs or EPROMs to be used depending on link selection.
- c) One 6551 configured to provide TTL serial, 20mA current loop or RS232 I/O at various baud rates.
- d) Two 6522 VIAs giving 40 bits of parallel I/O, 2 counter/timers and 2 shift registers, one of which controls a cassette interface. When used in a computer system these VIAs provide interfacing for a parallel keyboard and a Centronics printer. When used as a controller, a slight circuit modification allows the 6522s to be replaced by the less expensive 6821 PIAs.
- e) A bipolar PROM controlling the memory mapping of the board.
- f) Signal buffering and implementation of various TANBUS signals to allow the board to be used as part of a large system by means of a system motherboard.

Construction

It is not the intention of this article to duplicate the information supplied by MCS Ltd, and this will mainly cover those points not covered by the instructions which accompany the PCB or kit. The only point to make is that the task should cause no problems to anyone familiar with the fundamentals of electronic construction. This section will cover the programming of the address decoding PROM and the ways in which the board may be modified slightly to reduce the cost of a minimum configuration system for control applications.

MCS Ltd supply a number of memory mapping PROMs for various applications but do not give instructions on how to work out the programming required to achieve a specific mapping configuration. The 74S288 PROM has a capacity of 32 bytes and, in this application, each of these bytes controls the memory configuration of a 2K block of addressing space within the 64K map. In other words, the first byte affects 0-2K

74S288 PIN No.	74S288 BIT No.	FUNCTION
9	7	A 0 IN THIS BIT ENABLES MEMORY SOCKETS 1-8. THIS IS FURTHER DECODED BY BITS 4, 5 & 6.
7	6	WHEREVER A 0 OCCURS IN BIT 7 A THREE BIT BINARY NUMBER SHOULD BE WRITTEN TO THESE BITS TO INDICATE WHICH OF THE EIGHT SOCKETS IS TO BE ADDRESSED. THE SOCKET NUMBER = 1 + THE THREE BIT NUMBER e.g. 000 ADDRESSES SOCKET No.1.
6	5	
5	4	
4	3	A 0 IN THIS BIT ENABLES MEMORY SOCKET No.8. THIS IS A SPECIAL SOCKET UNAFFECTED BY CLOCK ENABLE etc. AND IS USED FOR THE MONITOR EPROM.
3	2	WHEREVER A 0 OCCURS IN BIT 7 ONE OF THESE TWO BITS SHOULD BE SET TO INDICATE WHETHER THE MEMORY SOCKET SPECIFIED BY BITS 4, 5 & 6 IS TO BE CONSIDERED AS RAM OR EPROM FOR BLOCK ENABLING AND MEMORY INHIBITING PURPOSES. BIT 2 = 1 FOR RAM BIT 1 = 1 FOR EPROM
2	1	
1	0	A1 IN THIS BIT ENABLES THE TOP HALF OF THE 2K BLOCK TO BE THE I/O AREA

Table 3. Memory mapping PROM bit designations.

(0000-07FF), the second byte 2K-4K (0800-0FFF) etc.

Table 3 shows the significance of each bit within these bytes, bit 0 in this illustration being the least significant and bit 7 the most significant. As an example, Table 4

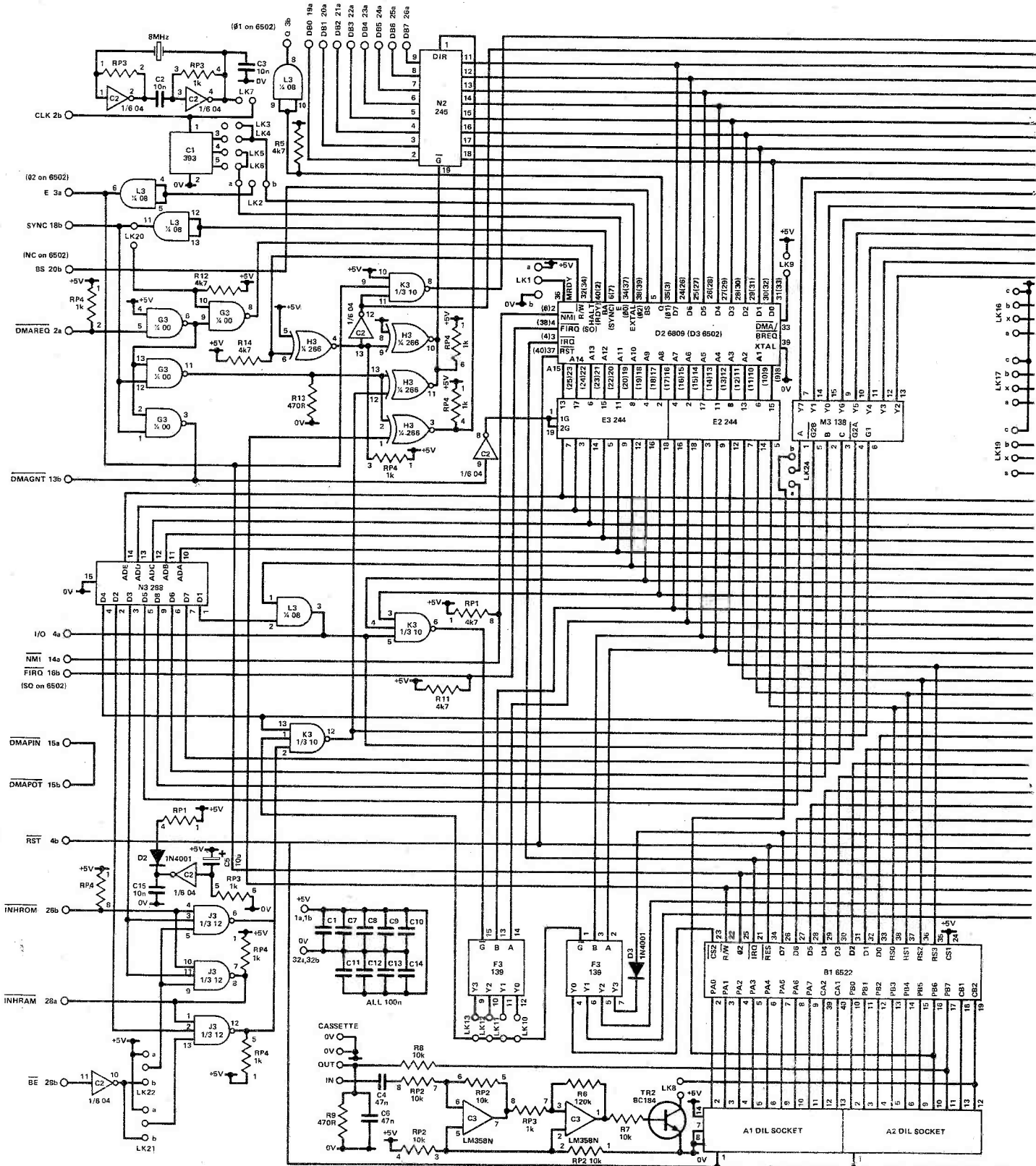
shows the programming of the standard memory map PROM for a 6502 CBUG system. Looking at the bit 7 column it is clear that the sockets 1-8 are enabled for addresses 0000-2000 and C000-EFFF, these blocks being the only ones where a 0 is programmed. The columns for bits 4, 5 and 6 indicate that sockets 1, 2, 3, 4, 7 and 8 are configured for 2K devices as each of these sockets is addressed for only a single 2K block and sockets 5 and 6 are addressed for 2 blocks each and are therefore 4K devices. It can be seen that 0000-07FF addresses socket 1, 0800-0FFF — socket 2, 1000-17FF — socket 3 up to E800-EFFF — socket 8.

By looking at the bit 1 and 2 columns we can see that, of these 8 sockets, the first four have a 1 for bit 2 and are therefore RAMs and the second four have a 1 for bit 1 and are therefore EPROMs. The last two 2K blocks have a 0 in bit 3 which selects socket 0, the monitor EPROM which is obviously a 4K device, and to complete the map, a 1 in bit 0 for the block B800-BFFF indicates that the I/O area is in the top half of this block ie BC00-BFFF.

ADDRESS BLOCK	EPROM ADDRESS	DATA BITS								HEX
		7	6	5	4	3	2	1	0	
0000-07FF	00	0	0	0	0	1	1	0	0	0C
0800-0FFF	01	0	0	0	1	1	1	0	0	1C
1000-17FF	02	0	0	1	0	1	1	0	0	2C
1800-1FFF	03	0	0	1	1	1	1	0	0	3C
2000-27FF	04	1	0	0	0	1	0	0	0	88
2800-2FFF	05	1	0	0	0	1	0	0	0	88
3000-37FF	06	1	0	0	0	1	0	0	0	88
3800-3FFF	07	1	0	0	0	1	0	0	0	88
4000-47FF	08	1	0	0	0	1	0	0	0	88
4800-4FFF	09	1	0	0	0	1	0	0	0	88
5000-57FF	0A	1	0	0	0	1	0	0	0	88
5800-5FFF	0B	1	0	0	0	1	0	0	0	88
6000-67FF	0C	1	0	0	0	1	0	0	0	88
6800-6FFF	0D	1	0	0	0	1	0	0	0	88
7000-77FF	0E	1	0	0	0	1	0	0	0	88
7800-7FFF	0F	1	0	0	0	1	0	0	0	88
8000-87FF	10	1	0	0	0	1	0	0	0	88
8800-8FFF	11	1	0	0	0	1	0	0	0	88
9000-97FF	12	1	0	0	0	1	0	0	0	88
9800-9FFF	13	1	0	0	0	1	0	0	0	88
A000-A7FF	14	1	0	0	0	1	0	0	0	88
A800-AFFF	15	1	0	0	0	1	0	0	1	88
B000-B7FF	16	1	0	0	0	1	0	0	0	88
B800-BFFF	17	1	0	0	0	1	0	0	1	89
C000-C7FF	18	0	1	0	0	1	0	1	0	4A
C800-CFFF	19	0	1	0	0	1	0	1	0	4A
D000-D7FF	1A	0	1	0	1	1	0	1	0	5A
D800-DFFF	1B	0	1	0	1	1	0	1	0	5A
E000-E7FF	1C	0	1	1	0	1	0	1	0	6A
E800-EFFF	1D	0	1	1	1	1	0	1	0	7A
F000-F7FF	1E	1	0	0	0	0	0	1	0	82
F800-FFFF	1F	1	0	0	0	0	0	1	0	82

Table 4. Memory mapping PROM for 6502 CBUG configuration.

Fig. 1 Circuit diagram of the Single Board Controller. The numbers in brackets are the pin numbers of alternative devices, the 6502 which can be used instead of the 6809 and the 6526 instead of the 6522.

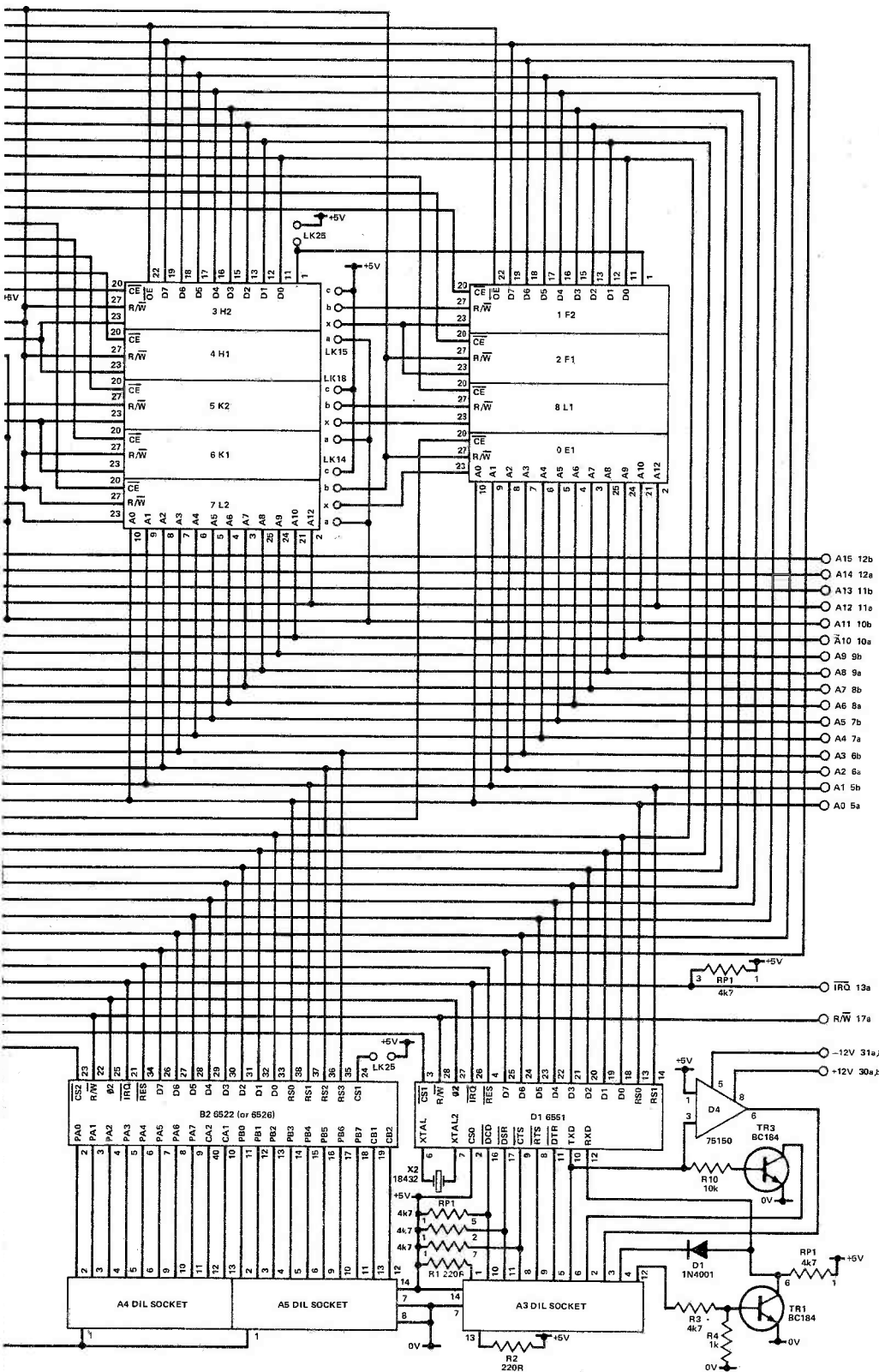


WORKS

The heart of the circuit is either D2, the 6809 processor or D3, a 6502 (6802 or 6808) processor, these two using slightly offset sockets. On the circuit diagram (Fig. 1) the two possible pro-

cessors are shown as one block, the pin numbers and functions for the 6502 option being shown in brackets (where different from the corresponding 6809 functions) next to the 6809

pin numbers and functions. LK1 is used for enabling or disabling on chip RAM if the 6802/6808 is in use and LK9 allows a battery supply to be used with this same processor for power down data retention. The processor clock is provided by the circuitry around C1, a binary counter and its associated crystal oscillator. LK7 selects either the on-board crystal oscillator or an off-board master clock. LK3, LK4, LK5 and LK6 select the processor frequency and LK2 alters the clock configuration depending on the type of processor in use. The power-on reset circuit is the portion including one-sixth of C2, D2 and capacitors C5 and C15. Buffering of the address bus is provided for on-board and external use by E2 and E3 whereas N2 buffers the data bus for off board peripherals only. E1, F1, F2, H1, H2, K1, K2, L1 and L2 are sockets for JEDEC memory devices, the specific type of device in use being specified by links LK14-19, some of which control a single socket and some of which affect a pair of memory sockets. The chip select decoding of these memories comes from M3, a 3 to 8 line decoder which is used in conjunction with N3, a bipolar PROM which controls the memory mapping of the complete board. LK24 allows a 2 page memory configuration to be implemented on board, the page selection being controlled from B1, a 6522 VIA. The circuitry around J3 allows on board memory to be enabled or disabled via the external BE (block enable) signal which is generated on the system mother board and allows a paged memory configuration greater than 64K to be achieved. LK21 and LK22 allow this facility to be disabled for on-board EPROM or RAM respectively. The same circuitry is sensitive to the Tanbus Inhibit RAM and Inhibit ROM signals which other boards may generate under various circumstances to disable portions of on-board memory. B1 and B2 are the 6522 VIAs, connection to the outside world being made via the D11 sockets A1, A2, A4 and A5. Socket B2 can take a 6526 in place of the 6522; this device has time of day registers and requires a 50Hz clock which may be connected via LK25. The cassette interface is driven from B1 and the circuitry round C3, an LM358N op-amp. D1 is the 6551 UART, access to which is provided via D11 socket A3 and the circuitry around D4, T33 and Tr1 provides RS232 (transmitted and received data only — not modem control lines) and 20mA current loop signal levels. The address decoding for the I/O devices is provided by F3 while links LK10-13 allow four optional addresses for the on-board portion of the I/O area. The I/O area select signal is also made available to off-board devices via the edge connector. Provision is made for DMA, the circuitry comprising G3 and H3 taking DMA request and generating DMA granted.



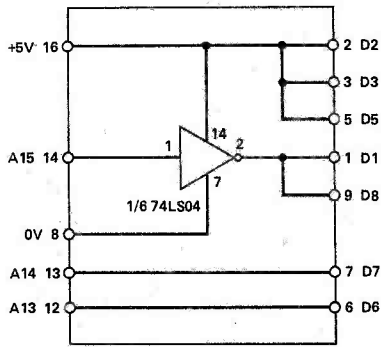


Fig. 2 The circuit which may be used for memory mapping instead of a PROM in control applications.

From the foregoing information it should be clear that virtually any memory map in 2K steps can be specified by the programming of the PROM. However, for a minimal configuration as used for control applications, a cost reduction can be made by replacing this component with a number of wire links and a simple TTL device which could be soldered onto a DIL header and inserted into the PROM socket. Figure 2 shows the circuit diagram of such an arrangement which gives a crude but effective memory map for many control applications. In this map the I/O area repeats sixteen times in 2K steps starting at 0400-07FF: socket 5 is addressed at 8000-9FFF, socket 6 at A000-BFFF, socket 7 at C000-DFFF and socket 8 at E000-FFFF. Obviously if 4K devices are used they will repeat twice within the 8K block and 2K devices will repeat four times. It should be noted that this configuration does not give RAM at address 0 and accordingly will be more practical for a 6809 application than for the 6503 which generally requires zero page memory at this address.

The memory mapping PROM does not dictate the mapping of the various I/O devices within the I/O area. This is partially fixed by the hardware and partially a function of LK10, LK11, LK12 and LK13, only one of which will be fit-

ted. Table 5 shows the I/O memory map.

When used as the basis of a computer system the 6522 VIAs will be required as their facilities are made use of by the system software, but in many control applications all that is required is the parallel I/O capability so the less expensive 6821 PIAs could be used. Unfortunately the pin-outs of the two devices are not identical, which means that a few tracks need cutting and few wire links require adding to the back of the board. Figure 3 shows the details of this modification. The 6821 only occupies an addressing space of 4 compared to the 16 bytes of the 6522 which means that, once the modification has been carried out, the 6821 registers will be spaced at intervals of 4 bytes. This need present no problem so long as it is not overlooked when writing the firmware.

To achieve further cost reductions for control applications it is merely necessary to omit those components which are not required for the particular application. One RAM and one EPROM will obviously be required as will at least one of the 6522 VIAs (or 681 PIAs). If no RS232 facility is required then D1, D4, Tr1, Tr3, X2 and their associated passive components may be left out. If the cassette interface is not to be used C3 and Tr2 together with their passive components can be omitted. As a final cost reducing exercise, assuming that no other boards are to be connected to the bus, the address and data bus buffers may be omitted. The data bus buffer N2 may be simply left out, but the address bus buffers E2 and E3 will require linking across as they supply on-board as well as off-board devices. This linking is done by omitting the chips in question and linking each input to its corresponding output, as may be seen from the circuit diagram (ie pins 13 to 7, 17 to 3, etc).

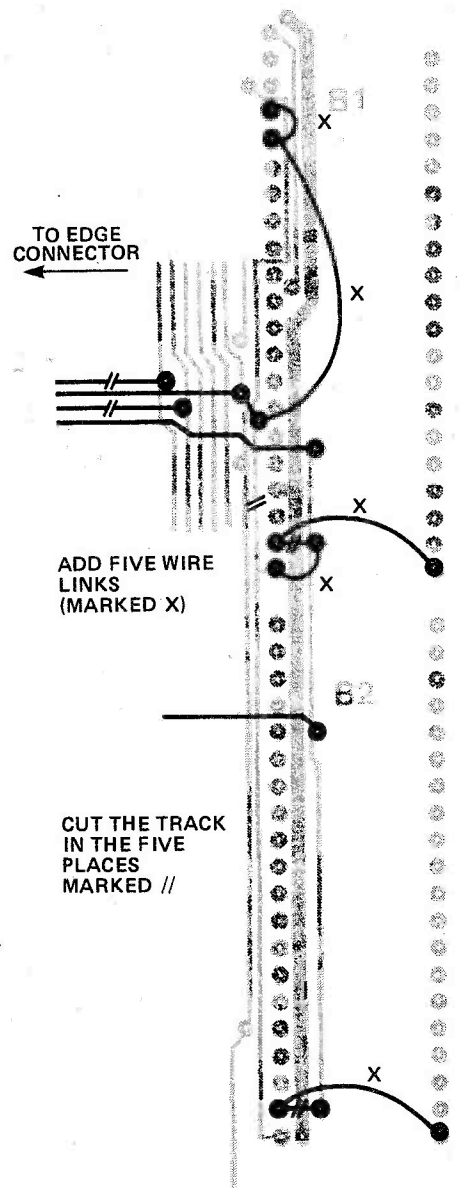


Fig. 3 PCB modification to enable 6821s to be used in place of 6522s.

BUYLINES

The PCB is not available from the ETI PCB service but may be obtained from Microtanic Computer Systems Ltd, 102, Lordship Lane, Dulwich, London SE22, tel 01-299 1419. MCS Ltd also supply complete kits of parts for various 6502 and 6809 configurations, ready built boards and pre-programmed memory mapping PROMs and monitor EPROMs. For those obtaining just the PCB from them there should be few problems finding the necessary components from standard sources.

ETI

LINK FITTED	6522 B1	START ADDRESS 6551 D1	6522 B2
LK10	I/O+00H+00H	I/O+00H+10H	I/O+00H+20H
LK11	I/O+40H+00H	I/O+40H+10H	I/O+40H+20H
LK12	I/O+80H+00H	I/O+80H+10H	I/O+80H+20H
LK13	I/O+C0H+00H	I/O+C0H+10H	I/O+C0H+20H

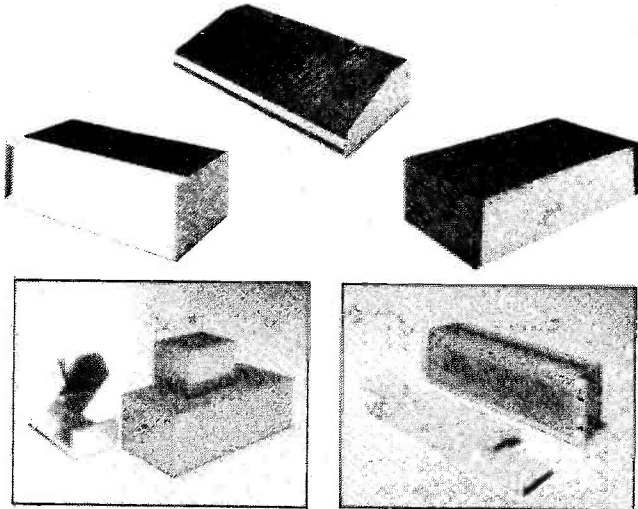
Table 5. Memory map of I/O area.

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74LS08	20p	74LS248	103p
74LS09	20p	74LS251	53p
74LS10	20p	74LS257	53p
74LS11	20p	74LS259	88p
74LS12	20p	74LS266	26p
74LS13	32p	74LS273	78p
74LS14	43p	74LS367	40p
74LS15	20p	74LS373	78p
74LS20	20p	74LS374	78p
74LS21	20p	74LS393	80p
74LS22	20p		
74LS27	20p		
74LS28	22p		
74LS30	20p		
74LS32	20p		
74LS33	22p		
74LS37	20p		
74LS38	20p		
74LS42	48p		
74LS48	76p		
74LS73	26p		
74LS74	26p		
74LS75	36p		
74LS76	26p		
74LS78	26p		
74LS83	66p		
74LS85	73p	74LS240	78p
74LS86	33p	74LS241	78p
74LS90	38p	74LS242	78p
74LS92	33p	74LS244	78p
74LS93	43p	74LS245	86p
74LS95	56p	74LS247	75p
74LS107	42p	74LS248	103p
74LS109	38p	74LS251	53p
74LS112	40p	74LS257	53p
74LS113	30p	74LS259	88p
74LS123	68p	74LS266	26p
74LS124	123p	74LS273	78p
74LS125	35p	74LS367	40p
74LS126	35p	74LS373	78p
74LS132	51p	74LS374	78p
74LS133	48p	74LS393	80p
74LS138	46p		
74LS139	46p		
74LS151	53p		
74LS153	63p		
74LS154	158p		
74LS155	53p		
74LS156	63p		
74LS157	46p		
74LS161	58p		
74LS163	58p		
74LS164	73p		
74LS165	93p		
74LS166	86p		
74LS173	78p		
74LS175	58p		
74LS181	188p		
74LS192	73p		
74LS193	75p		
74LS197	73p		
74LS221	76p		

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2532	340p
2764	470p
27128-25	1500p

CPU	
Z80	275p
6502	345p
6800	200p
6802	277p
6809	645p
8080	420p
8085	640p

CMOS	
4001	16p
4013	24p
4016	24p
4017	41p
4019	33p
4020	46p
4024	33p
4027	18p
4029	43p
4042	43p
4047	38p
4049	24p
4051	46p
4060	66p
4066	22p
4069	16p
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4078	23p
4081	16p
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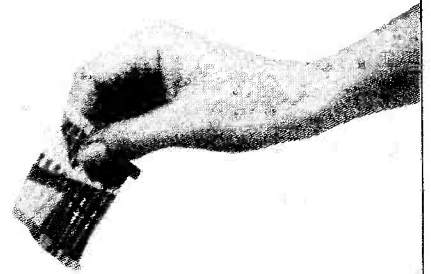
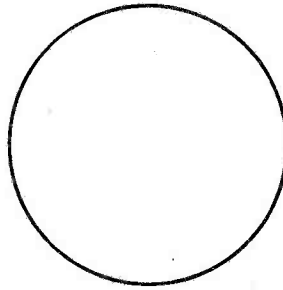
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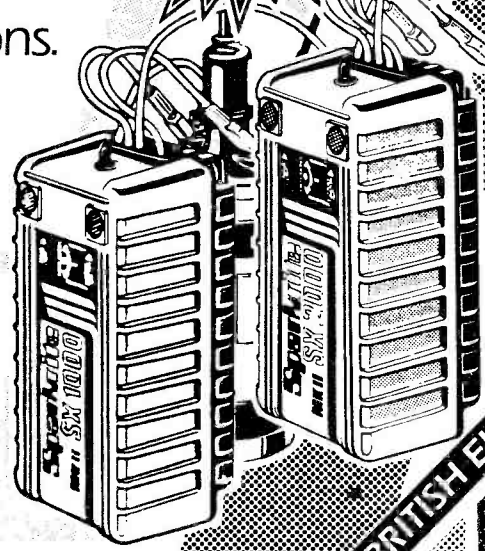
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DISTORTION METER

In the third and final part of this series, John Linsley Hood describes the construction and use of the instrument.

The THD meter is built on two main PCBs, one carrying the circuitry for the distortion meter itself and the millivoltmeter while the other carries the oscillator circuitry. A further PCB is required for the stabilised mains power supply or the dual-rail circuit if a single battery is to be used. No power supply circuitry is required if the distortion meter is to be operated directly from twin batteries. The mains power supply circuit is so standard that we have re-used an existing PCB rather than lay out a new one.

Assembly of the PCBs should present no problems if the overlay diagrams are followed carefully, and the only points to watch are the usual ones concerned with the orientation of ICs, electrolytic capacitors, diodes and any other polarity-conscious components. If you are planning to use IC sockets these should be soldered onto the boards first of all, followed by the resistors and capacitors and then the diodes. The ICs can then be inserted in their sockets when the soldering is complete. If you are not using sockets, solder the passive components into place first, then the diodes, etc, and last of all the ICs.

The choice of case will be largely determined by the method of powering you intend to employ. The single battery option will fit into a fairly small case,

especially since there will be no problems of mains pick-up. The twin-battery option will require a slightly larger case but is otherwise as compact as the first type, while the mains-powered version will require extra space for the transformer plus enough clearance between this and the main circuitry to prevent the risk of hum pick-up. Whichever system you are using, it is advisable to choose a die-cast box rather than a pressed-steel or other metal one, and you should certainly not use a plastic box.

The PCBs are mounted below the front panel using stand-off pillars, and the total depth of the finished unit should be about two inches. This allows plenty of room for a metal screen and a mains power supply to be mounted in

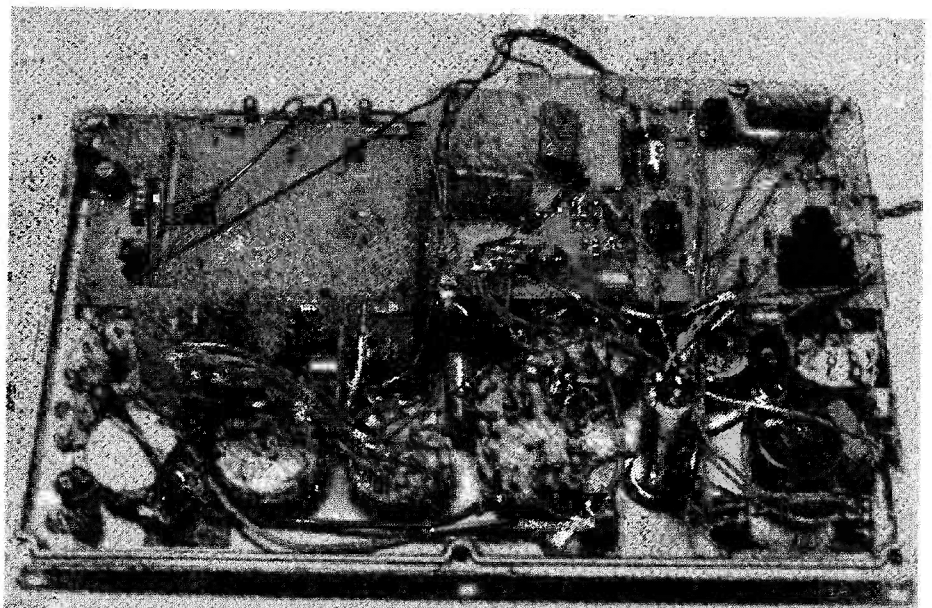
the base of a suitable box without making the completed instrument unduly deep. It is a good idea, however, to give yourself plenty of room even if you are not building the mains version. Too tight a construction may lead to capacitive coupling between various parts of the circuit and this will introduce a number of problems. One particular example is the effect of coupling the feedback signal from the millivoltmeter into the early stages of the THD meter circuit. This gives rise to a spurious crossover distortion effect which mysteriously vanishes when the instrument is nulled.

The input attenuator resistors can be mounted between the tags of the rotary switch. If you are using the specified values this

OOPS!

The formula for calculating the null frequency of a Wien network, given in the first part of this series on page 58 of the January issue, was incorrect. It should be

$$F_o = \frac{1}{2\pi \sqrt{C_1 C_2 R_3 R_4}}$$



Internal view of the prototype. A number of modifications have been incorporated in the final version, so don't try and follow this wiring too closely!

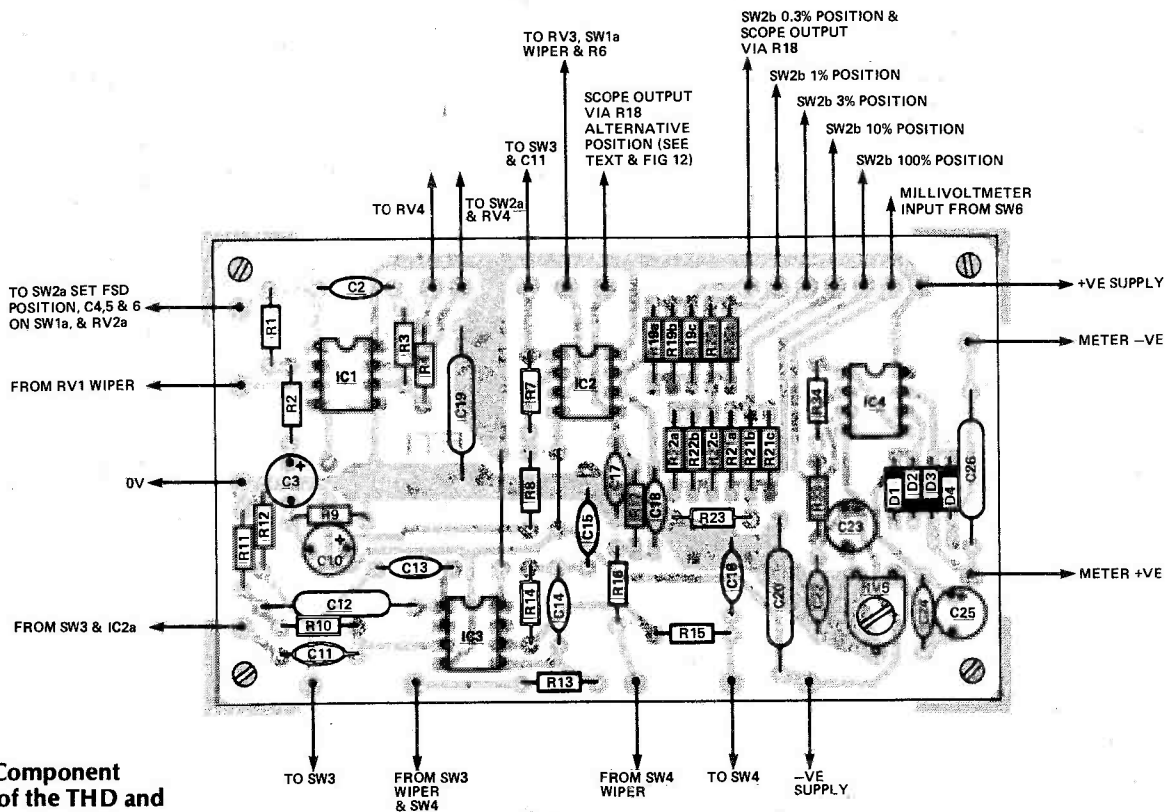


Fig. 13 Component overlay of the THD and millivoltmeter PCB.

PARTS LIST — THD METER AND MILLIVOLTMETER

RESISTORS (all 1/4W carbon or metal film)

R1	12k
R2	3k9
R3	5k6
R4	10k
R5	470R
R6	560R
R7, 15, 18	2k2
R8	220R
R9	47R
R10, 11, 12	6k8
R13	39k
R14, 33	2k7
R16, 17	3k3 (see text)
R19, 27	2k33 (see text)
R20, 28	666R (see text)
R21, 29	233R (see text)
R22	90R (see text)
R23, 32	10R (see text)
R24	66k6 (see text)
R25	23k3 (see text)

R26	6k66 (see text)
R30	66R6 (see text)
R31	23R (see text)
R32	10R (see text)
R34	68k
RV1	10k
RV2	10k dual gang
RV3	100R
RV4	2k2
RV5	2k7

CAPACITORS

C1, 4, 7, 12, 19, 20, 21, 24, 26	470n
C2	1u0
C3	2u2 electrolytic
C5, 8, 13	47n
C6, 9	4n7
C10, 23, 25	47u electrolytic
C11	22n
C14, 15	3n3
C16	33n

C17	470p (see text)
C18	1n0 (see text)
C22	100n

SEMICONDUCTORS

IC1 - 4	TL072
D1 - 4	1N4148

MISCELLANEOUS

M1	100uA meter
SK1 - 3	co-axial socket, panel mounting
SW1	2 pole, 3 way rotary switch
SW2	2 pole, 6 way rotary switch
SW3, 4, 6	SPDT toggle switch
SW5	1 pole, 9 way rotary switch
PCB.	

arrangement is not too critical, but if, as discussed earlier, you decide to use higher values to increase the input impedance, you may find it necessary to screen the switch to prevent pick-up. Note that a number of other components are also mounted on or between switches and potentiometers rather than on the PCBs. These include R5, 6, and 18 and C1, C4-9 and C21. Because we have re-used an existing PCB rather than design one specifically

for this project, R54 and R55 in the mains power supply must also be mounted off of the board.

Connecting up the PCBs and the various controls should present no problems provided you adopt a fairly methodical approach, but don't make the wiring any longer than you absolutely have to. This is particularly important with the mains wiring if you are building a mains-powered instrument.

When the unit has been

completed and appears to be working correctly, the sensitivity of the basic meter amplifier should be adjusted to 10mV FSD. This is probably best done, if appropriate calibration gear is not available, by setting up a small mains transformer to give a 50Hz output in the range 5-20V, as measured by a multi-meter with an AC range. You can then adjust meter sensitivity by means of RV5, on an appropriate range setting, until it gives the same reading.

PROJECT : Distortion Meter

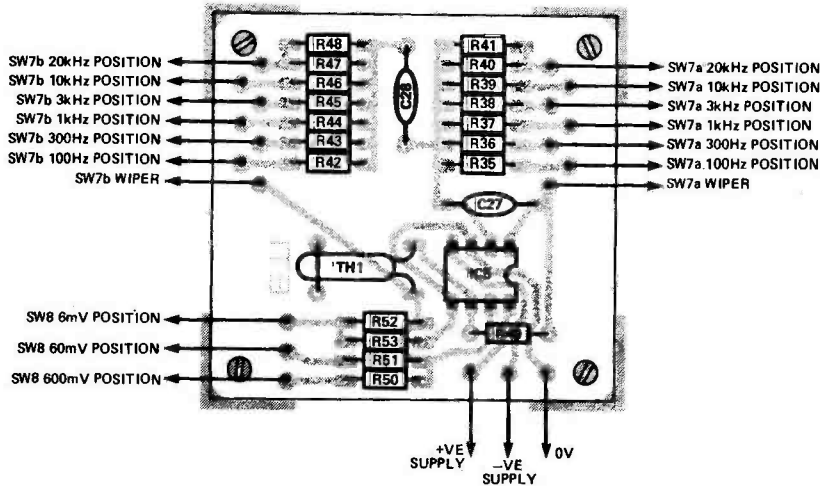


Fig. 14 Component overlay of the spot frequency oscillator PCB.

PARTS LIST — OSCILLATOR

RESISTORS (all 1/4W carbon or metal film)		CAPACITORS	
R35, 42	330k	C27, 28	4n7
R36, 43	100k	SEMICONDUCTORS	
R37, 44	33k	IC5	TL072
R38, 45, 52	10k	MISCELLANEOUS	
R39, 46	3k3	SK4	co-axial socket, panel mounting
R40, 47	1k8	SW7	2 pole, 6 way rotary switch
R41, 48	27k	SW8	1 pole, 3 way rotary switch
R49	1k5	TH1	RA53
R50	220R	PCB.	
R51	22k		
R53	100R		
RV6	2k5		

PARTS LIST — MAINS PSU

RESISTORS		LED1	
R54	470R	panel mounting	
R55	1k0	LED	1N4001
CAPACITORS		MISCELLANEOUS	
C29, 31	100u 16V electrolytic	SW9	mains toggle switch
C30, 32	1000u 25V electrolytic	T1	15-0-15V 3VA mains transformer, PCB mounting
SEMICONDUCTORS		PCB.	
IC6	7815		
IC7	7915		

Using The Distortion Meter

While the major application which will occur to the reader will undoubtedly be that of testing audio amplifiers, for example, to see whether the quiescent current setting of a transistor amplifier output stage is correct or to check that one is getting the results one should from a DIY unit, there are other uses.

There are three particular applications which are especially valuable. One is to check that the alignment of a pick-up cartridge on its arm is correct. For this one needs a test record with a track of 1 kHz or 3 kHz (the higher, the more difficult for the cartridge) recorded at, say, 5 cms/sec. If the cartridge is properly aligned, the THD should be in the range 0.4 to 1.2%, depending on cartridge quality. A worn stylus will worsen these figures rapidly, especially at higher frequencies, so if one checks the 'off-record' THD from time to time, one can monitor the health of the stylus.

A second useful application is to check the correct recording and bias levels on a tape or cassette recorder. With the latter, on a reasonable machine, the THD should be of the order of 0.3% at -5VU. This will worsen with increasing signal level, becoming perhaps 3% just below the recording overload level, which will allow the overload level to be determined for a particular machine/tape combination. A reel-to-reel machine, at 7.5 ins/sec, should have THD levels of about half these values.

Since the bias level settings on a tape recorder are a compromise between flatness of frequency response and THD, the combination of oscillator, millivoltmeter and THD meter should allow one to check or reset

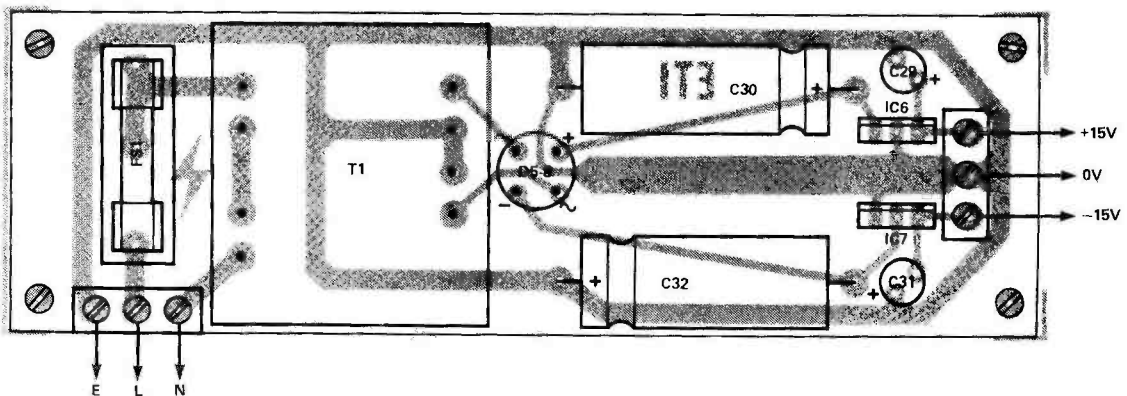


Fig. 15 Component overlay of the mains power supply PCB.

PROJECT : Distortion Meter

this level if it is not ideally chosen.

The final additional use for a THD meter is in setting up FM tuners. The THD of these depends on the alignment of the IF tuning coils and also upon the setting of the quadrature coil on the demodulator IC. By using the BBC test tones which are sometimes broadcast after the finish of programmes, the THD of the signal can be measured and optimised by adjustments to the controls.

I ought at this stage to sound a small note of warning in that one should be reasonably sure what one is doing before coil-twiddling inside an expensive and complicated commercial FM tuner. If it is a DIY job, one should be able to get back to square one if things go wrong.

In all of these applications, the method of operation is the same:

1. Set the THD meter input sensitivity to zero, and switch out both of the filter stages.
2. Set the mV/THD switch to THD, and set the Mode switch to Set FSD.
3. Connect the input of the meter to the output of the system under test, and gradually increase the input sensitivity control until the output meter reads full scale.
4. Switch the mode switch to 100% and alter the setting of the Coarse tune (RV2a and 2b) and Trim (RV4) controls, at an appropriate choice of frequency range (set by SW1). Adjust until the best practicable notch is obtained with the mode settings adjusted to the 10% and 3% positions.
5. Progressively increase the sensitivity given by the mode

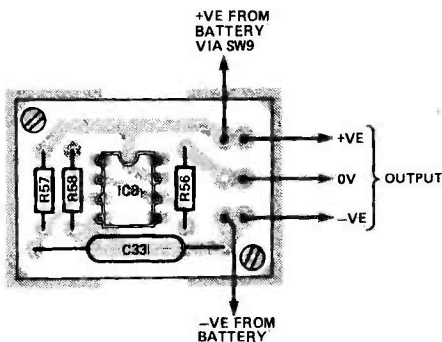


Fig. 16 Component overlay of the single battery supply PCB.

PARTS LIST — SINGLE BATTERY PSU

RESISTORS	
R56	100R
R57, 58	1M0
CAPACITOR	
C33	1u0
SEMICONDUCTOR	
IC8	TL071
MISCELLANEOUS	
SW9	SPST toggle switch

switch setting until the highest practical value is obtained, with the fine tune (RV3) and trim pots adjusted alternately until no lower value of residual reading can be obtained. Although the use of a single gang pot as RV3 is practicable, it does mean that it is necessary to try trim settings on either side of the apparent minimum position before adjusting the fine tune pot.

If the constructor uses the completed instrument to assess

the quality of the built-in oscillator, the THD values obtained should be similar to those shown in Table 1 for the prototype. This is a useful first test, serving both to confirm that all is well with the meter and also giving some practice in using the instrument.

Interpreting The Results

In spite of all the publicity which attends the introduction of new, very high quality audio amplifiers, and in spite of the continuing efforts of designers — me included — to produce very low distortion systems, I think a lot of the effort devoted to getting more 0s after the decimal point is of small value to the user. Even with modern designs, in which most of the residual distortion will be due to crossover type defects which lead mainly to audibly unpleasant high-order harmonics, I do not believe it is possible to hear the difference between nil and 0.05%. For myself, I am convinced that if an amplifier doesn't sound well and the THD is less than 0.05%, the problem lies elsewhere, possibly in its transient response or maybe in incipient instability or overload hang-up effects.

I say this to save users from needless anxiety if, in testing a well loved unit, they find it has, say, 0.04% THD — or maybe even more. Most of that could be low order distortion which isn't audible, or even hum and noise. The corollary is also true, that an instrument with a lower THD limit of, say, 0.03% will still be a valuable aid in making sure that the domestic hardware isn't letting the side down!

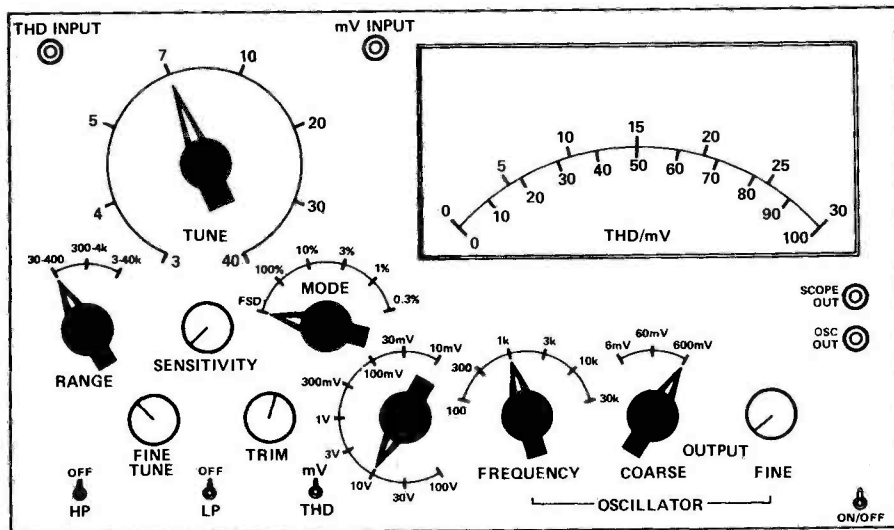


Fig. 17 The front panel layout used in the prototype.

ETI

BUYLINES

Metal film and carbon film resistors are available from many of the companies who advertise in ETI, as are all of the semiconductors and capacitors used in this project. Suitable rotary switches are sold by Electrovalue, Cricklewood, Maplin and others and Maplin also supply the RA53 thermistor. Large diecast boxes are not widely available but West Hyde Developments of 9-10 Park Street Industrial Estate, Aylesbury, Buckinghamshire, supply a range of sizes including one which measures 188 x 120 x 78mm which might be suitable. The PCBs are available from our PCB service.

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PARAGRAPH EQUALISER

Are Barry Porter's paragraphs equal to the task of describing the construction of this innovative project? Read on and find out.

By now, it must be obvious that the ParaGraph need not be limited to the suggested ten frequency bands, but this number does seem to give the best opportunity of applying just about any required response characteristic. A suggested panel layout is shown in Fig. 14, based on standard 19" rack

OOPS!

There were a number of errors in the first part of this project published last month. On page 31, in the formula for resonant frequency which appears towards the bottom of the third column under the heading 'Principle Of Operation', the bottom line should read $2\pi R_c C$.

In Fig. 5, the input stage circuit diagram, pin 2 of IC1b should be taken from the wiper of RV1 only. The link shown between this pin and the junction of RV1/R8 should not be there. There are also two resistors marked R10 on the diagram: the lower one, in the -15V supply line, should be R11.

In Fig. 7, the main signal path circuit diagram, there are two capacitors marked C24: the one connected between ground and the junction of R28/C27 should be C29.

In Fig. 8, the state variable filter circuit diagram, the IC supply pin numbers are missing. The +15V supply via R39 connects to IC6 & 7 pin 7 and the -15V supply via R40 connects to IC6 & 7 pin 4.

In Fig. 9, the balanced output stage diagram, the numbering of pins 2 and 3 on IC11 is reversed; the + and - signs on the two pins are correct. The input to R41/C42 should be marked "FROM SW2b" and C42 should be 330n, not 330k. The 'SET OUTPUT SYMMETRY' preset between R54 and R55 should be marked RV5, not RV4.

mounting dimensions, so there is a wide choice of suitable cabinets available.

Each filter stage is built onto a separate circuit board, which is attached to the front panel by the frequency and Q adjustment potentiometers. The board layout is shown in Fig. 11. The cut-out area allows different types of slide fader to be used and ensures that the rotary controls can be in line with the fader. Remember to purchase sliders which can be mounted by screws from the front, and use a dummy front panel if you don't want the screw heads to show.

The only components that differ between one filter board and another are the integrator capacitors, and plenty of space has been left for these. Instead of

attempting to mount the various capacitor types and sizes in the normal way, small terminal pins should be pressed through the capacitor mounting holes, and the components soldered to these from the top of the board.

Once the boards have been assembled, they should be attached to the front panel making sure that they are in the correct order. The busses which carry the various common connections should be fed through the circled holes and continued to the circuit board that contains the main signal path components (Fig. 12). A suitable gauge of tinned copper wire should be used for the busses and this may be insulated with short lengths of sleeving if it is felt that there is any danger of short circuits occurring.

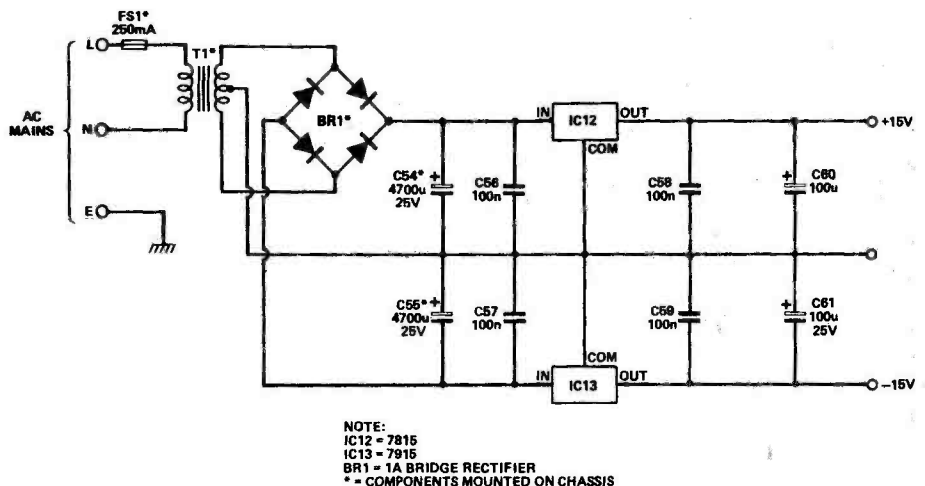
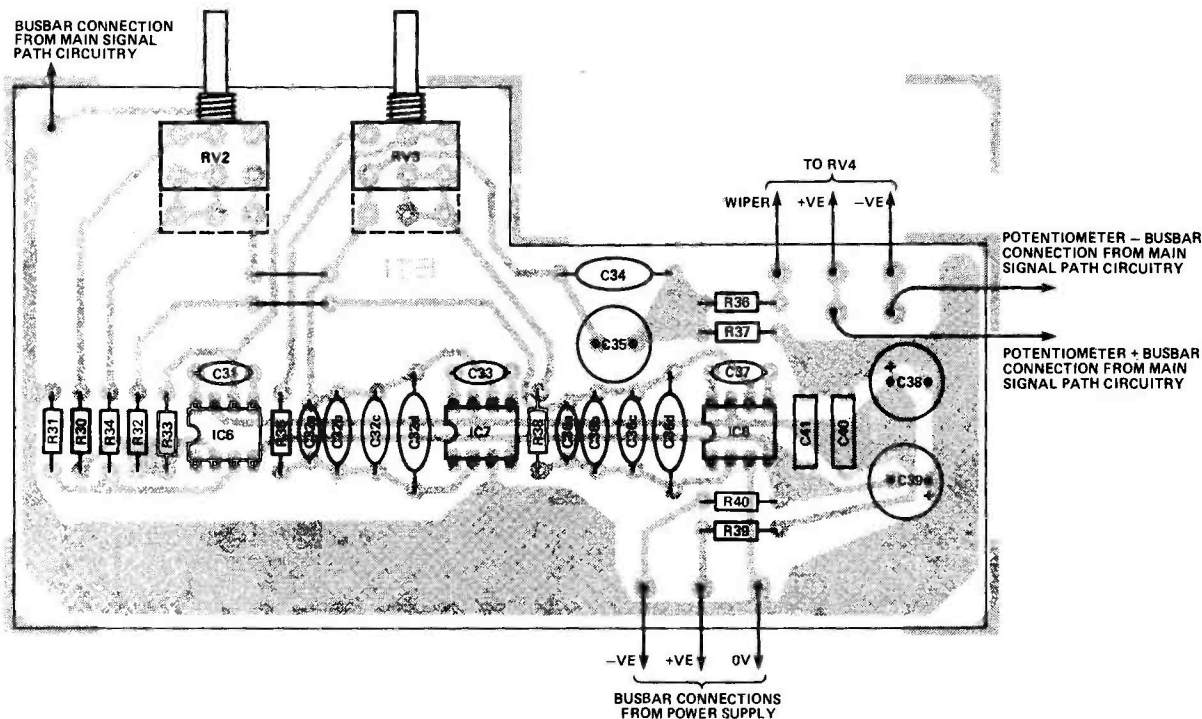


Fig. 10 Circuit diagram of the stabilised power supply.



PARTS LIST — FILTER BOARD

RESISTORS (all 1/4W 1% metal film)

R30, 31, 34	10k
R32, 33	20k
R35, 38	11k
R36	4k3
R37	47k
R39, 40	10R
RV2	100k linear dual gang rotary potentiometer
RV3	22k linear dual gang rotary potentiometer
RV4	10k linear slider potentiometer

CAPACITORS

C31, 33, 37	22p polystyrene see Table 1
C32, 36	
C34	100n polycarbonate
C35	22u 16V non-polarised radial electrolytic
C38, 39	100u 25V radial electrolytic
C40, 41	100n polyester

SEMICONDUCTORS

IC6, 7, 8	NE5534
-----------	--------

MISCELLANEOUS

PCB; IC sockets if desired; terminal pins for C32 and C36.

Fig. 11 (above) Component overlay of the filter PCB. Note that you will need one filter board for each channel of the ParaGraph.

PARTS LIST — INPUT AND MAIN SIGNAL PATH BOARD

RESISTORS (all 1/4W 1% metal film)

R1, 2	1k8
R3, 4	8k2
R5, 6, 23-26	10k
R7, 8	4k7
R9, 22, 27	47k
R10, 11, 28, 29	10R
RV1	10k linear rotary potentiometer

CAPACITORS

C1, 2	1n0 polystyrene
C3, 21, 25	100n polycarbonate
C4, 22, 26	22u 16V non-polarised radial electrolytic
C5, 6, 27, 28	100u 25v radial electrolytic
C7, 8, 29, 30	100n polyester
C23, 24	22p polystyrene

SEMICONDUCTORS

IC1	NE5532
IC4, 5	NE5534

MISCELLANEOUS

SK1 XLR or other three-pole connector to choice — see text
PCB; IC sockets if desired.

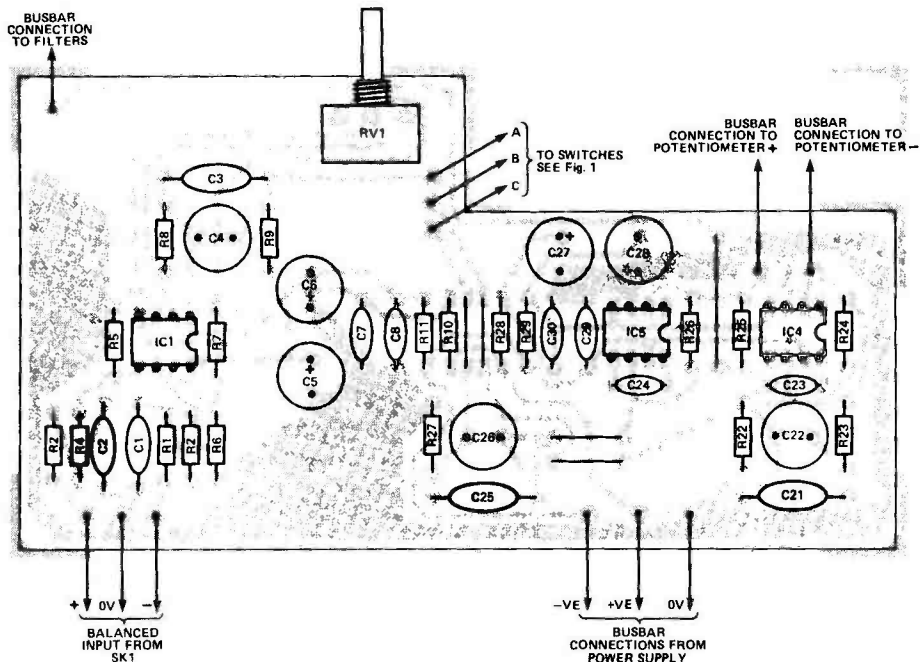


Fig. 12 (left) Component overlay of the input stage and main signal path PCB.

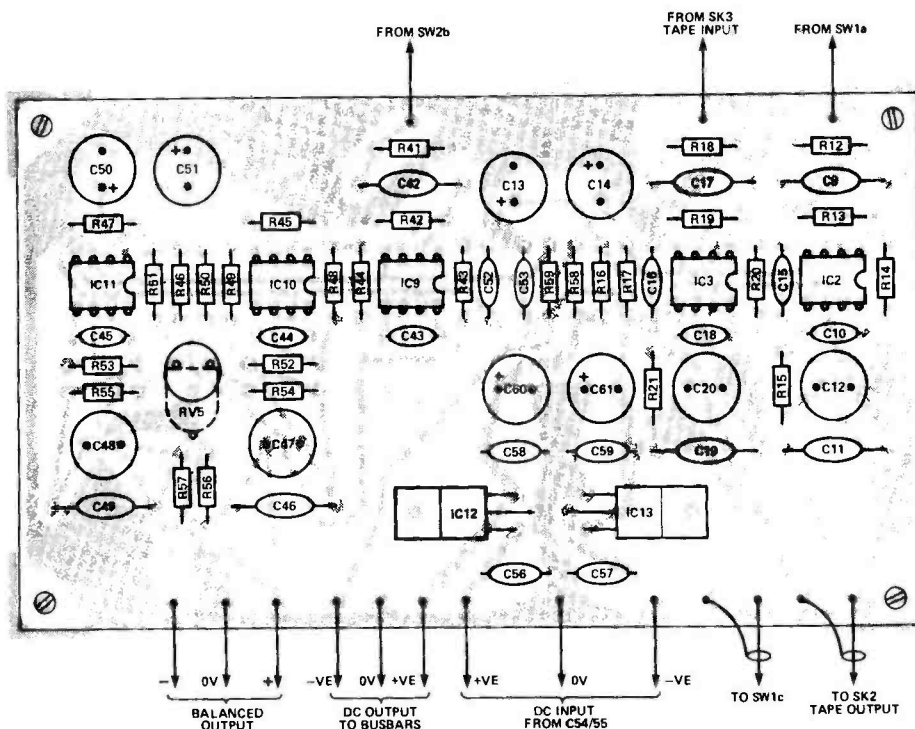


Fig. 13 Component overlay of the tape buffer, balanced output and PSU board.

The output stage and tape buffer amplifiers are on a separate circuit board, together with the power supply stabilizers (Fig. 13). This board may be mounted at any convenient point within the cabinet, but should be kept as far away as

possible from the mains transformer and any mains wiring. Connections between the circuit boards and function switches should prove quite straightforward, using Fig. 1 as a reference. Due to the low impedance of the switched conec-

PARTS LIST — TAPE BUFFERS, BALANCED OUTPUT AND PSU BOARD

RESISTORS (all 1/4W 1% metal film)

R12, 18, 41	100k
R13, 19, 42	330k
R14, 16, 17, 20, 43, 58, 59	10R
R15, 21, 56, 57	47k
R44 - 51	3k3
R52, 53	33R
R54, 55	1k0
RV5	10k moulded preset

CAPACITORS

C9, 17, 42	330n polycarbonate
C10, 18, 43, 44, 45	22p polystyrene
C11, 19, 46, 49	100n polycarbonate
C12, 20, 47, 48	22u 16V non-polarised radial electrolytic
C13, 14, 50, 51, 60, 61	100u 25V radial electrolytic
C15, 16, 52, 53, 56 - 59	100n polyester
C54, 55	4700u 25V can electrolytic

SEMICONDUCTORS

IC2, 3, 9, 10, 11	NE5534
IC12	7815
IC13	7915
BR1	1A bridge rectifier

MISCELLANEOUS

FS1	250mA anti-surge fuse and chassis-mounting holder
SK2, 3	phono or other sockets to choice — see text
SK4	XLR or other three-pole connector to choice — see text
SW1	4-pole 2-way toggle switch
SW2	DPDT toggle switch
SW3	SPDT toggle switch
T1	15-0-15V 25VA mains transformer, preferably toroidal

PCB; IC sockets if desired; 4U height 19" rack-mounting case or similar; mounting brackets or stand-off pillars for the tape buffers, balanced output and PSU board; mains input connector or cable strain-relief bush; knobs for rotary and slider potentiometers; tinned copper wire for busbars; nuts, bolts, etc.

tions, unshielded wire may be used throughout.

If the recommended balanced inputs and outputs are employed, it is suggested that professional XLR 3 pin connectors are used. These can be obtained at a reasonable price from a number of sources, and will remain reliable for many years — unlike some of their lesser brethren. There is a permanent confusion, even in the professional world, over the correct wiring of these connectors, so the generally accepted standard is given here:-

all signal inputs — via XLR 3 way chassis mounting sockets (termed female)

all signal outputs — via XLR 3 way chassis mounting plugs (termed male)

wiring to both plugs and sockets

- Pin 1 — Earth
- Pin 2 — Signal +
- Pin 3 — Signal -

For unbalanced inputs or outputs, connect pin 3 to pin 1.

Unbalanced versions may be fitted with DIN or Phono sockets. If the latter are used it is well worth tracking down some gold plated ones, and be sure to mount them with insulation bushes so there is no electrical contact between the cabinet metalwork and the socket body.

For safety reasons, the metal cabinet must be connected to earth via the mains lead. If the signal earth is connected to the cabinet in any way, a nice juicy hum loop will probably be formed whenever the ParaGraph is used with other equipment which has common mains and signal earths. The best approach to this problem is to experiment once the unit is working correctly, so as an interim measure, make sure that the signal earth is floating at this stage.

Testing

Once the construction and internal wiring is complete, the moment has arrived for power to be applied for the first time. The ParaGraph should be connected to an oscillator and an oscilloscope, so that when the initial switch-on takes place an immediate indication

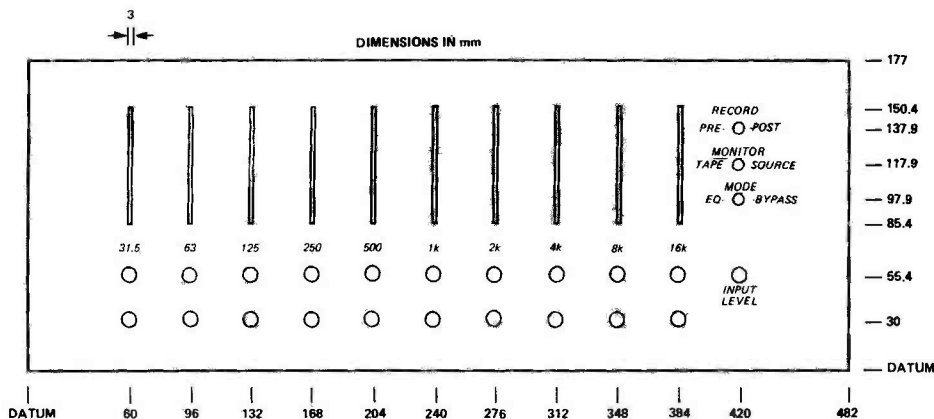


Fig. 14 Suggested front panel layout for the ParaGraph based on a 4U (7") height 19" racking case.

is given of the unit's correct operation — or otherwise. If signal does not appear at the output, the golden rule is: Do Not Panic. Assuming that the unit is located behind the regulation 6ft wall of sandbags, crawl around and look for signs of smoke. You will probably find that in your excitement, you have forgotten to switch on the oscillator, but if, after taking a handful of Valium, you convince yourself that everything is as you

intended and that your new example of turbo-technology really is not working, carry out the usual checks for correct DC voltage rails and IC inputs and outputs. If all appears healthy the signal should be traced, using your oscilloscope, from the input socket through the circuitry until it disappears.

Once any faults have been located and rectified the correct operation of all the control functions should be checked, and

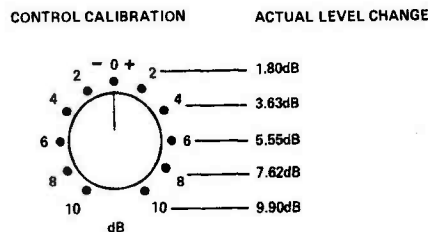


Fig. 15 Calibration of the input level control.

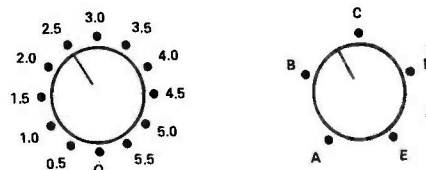
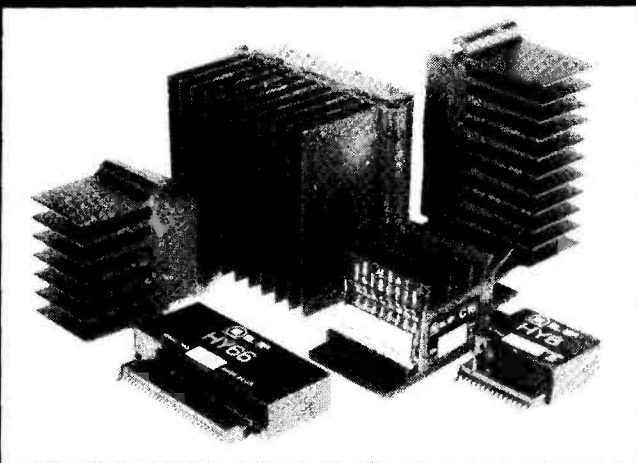


Fig. 16 Calibration of the Q and frequency controls.

once you are satisfied that everything is working as intended, your ParaGraph may be fed its first dose of musical signal. You can then spend a pleasant hour twiddling the controls and discovering whether all the effort has been worthwhile. If so, you may wish to sally forth and build yourself another one, so that you can at least equalise yourself to distraction in stereo. **ETI**

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MOS248	120	4-8	£39.95				

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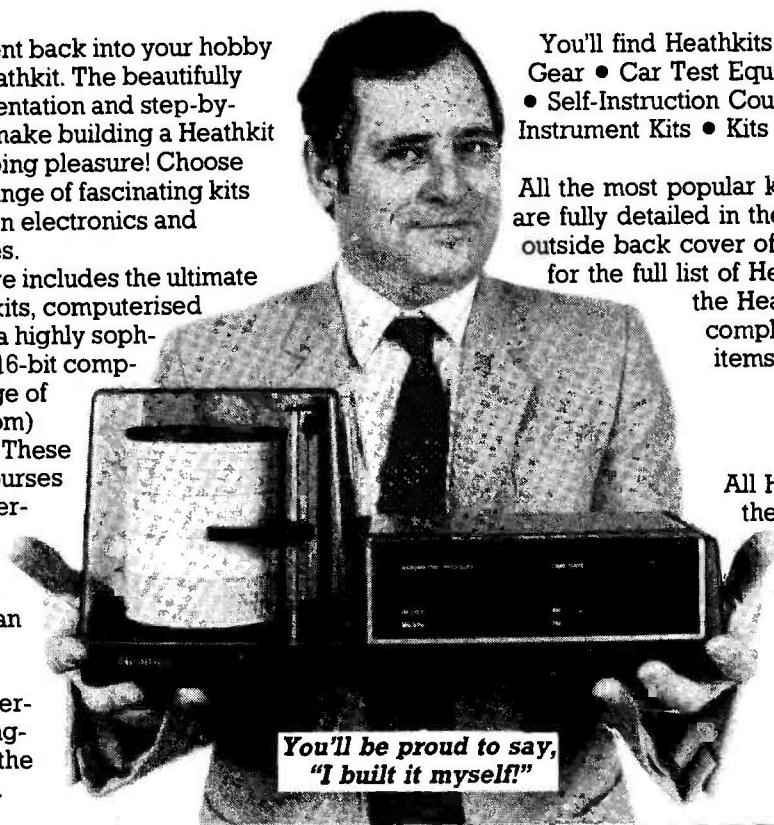
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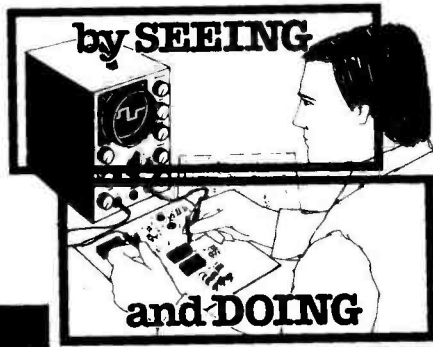
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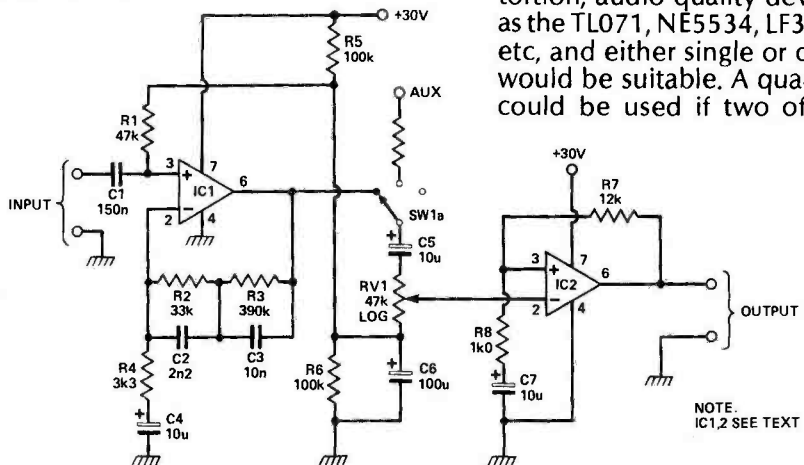
TECH TIPS

Pick-up Pre-amplifier

Jeff Macaulay, Crawley

Over the last few years, two schools of thought have emerged on the subject of audio pre-amplifier design. The 'British' approach, as it is sometimes termed, favours designs with the minimum of frills on the grounds that tone controls and the like introduce unnecessary distortion and phase shifts. The design described here is an example of this minimalist approach and possesses sufficient dynamic range to handle direct-cut and digitally mastered records without problems.

The circuit may be considered in two parts, each built around one of the op-amps. IC1 functions as an RIAA equaliser with R2, R3, C2 and C3 in the feedback loop providing



the correct response. R4 sets the midrange gain at 10 while C4 prevents the stage amplifying DC. The input overload factor is greater than 40dB and this, combined with a signal to noise ratio of more than 70dB gives the circuit a dynamic range of 110dB.

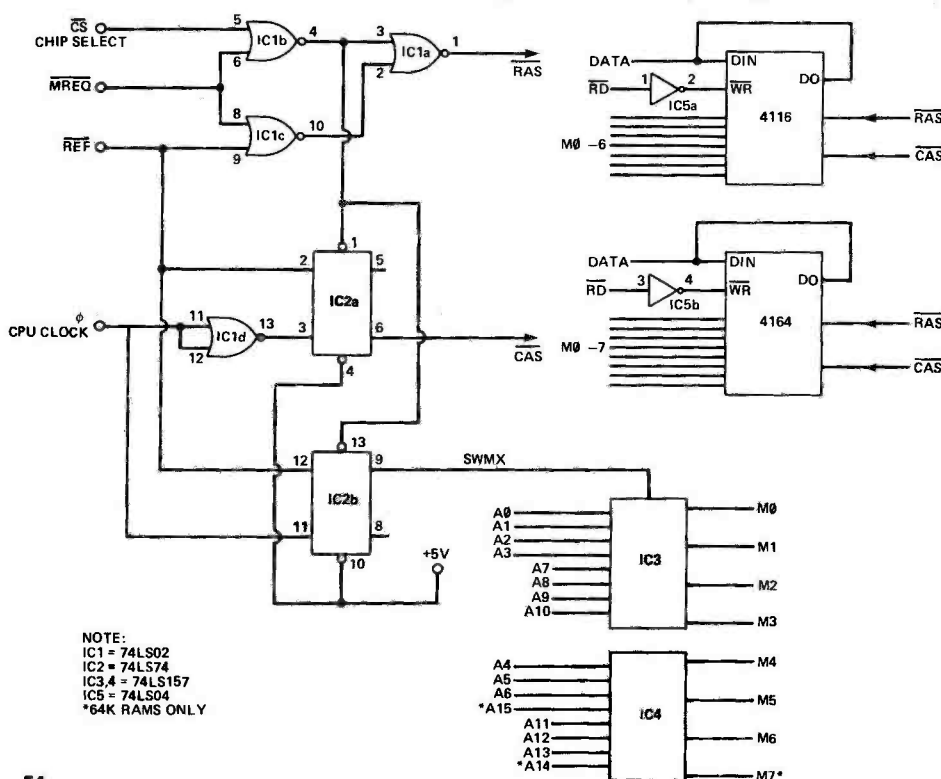
IC2 has a flat frequency res-

ponse and provides extra gain for the equaliser stage or for an auxiliary input selected by SW1. Both op-amps should be low noise, low distortion, audio quality devices such as the TL071, NE5534, LF351, OP27, etc, and either single or dual types would be suitable. A quad op-amp could be used if two of the pre-

amplifiers were to be combined in a stereo arrangement. The pin numbers given are correct for 741-type single-packaged op-amps but it is advisable to check carefully the pin-outs of the device you plan to use, and the arrangement will obviously be different if dual or quad devices are employed.

Low Cost Z80 DRAM Drive & Refresh

D. Allen Bolton



NOTE:
IC1 = 74LS02
IC2 = 74LS74
IC3,4 = 74LS157
IC5 = 74LS04
*64K RAMS ONLY

This circuit provides address multiplexing & refresh for 16K or 64K DRAMs using only four chips and one inverter.

Memory Cycle: In a normal memory access the cycle is started by MREQ & CS going low. This causes RAS to go low and the flip-flops are no longer held in reset. RAS gates the lower

seven (or eight) row address lines into the memory. On the first positive going clock edge after MREQ the SWMX flip-flop IC2b clocks. The D input is REF which will be high during memory cycles. Therefore the SWMX signal goes high and switches the column address lines to the DRAM. On the next negative going clock pulse CAS goes low and gates in the column address. Data can then be written to or read from memory depending on the Z80 RD line. The WR line is not used. The cycle ends when MREQ goes high causing both flip-flops to reset.

Refresh: Dynamic RAMs require RAS low and CAS high and only the lower 7 address lines are used to refresh. The Z80 counts through the lower 7 address bits after each instruction fetch and sets REF low. MREQ and REF are gated together to produce RAS. Clock cycles do not change the state of IC2a because the D input is REF which is low. Therefore the multiplexer is not switched and CAS is not generated.

Addressing: For 16K DRAMs A14 & A15 are not connected to the multiplexer and will normally be gated to provide Chip Select (CS). In this case ground the inputs to the multiplexer.

When 64K DRAMs are used the CS input may be a disabling signal to avoid double addressing with ROMs.

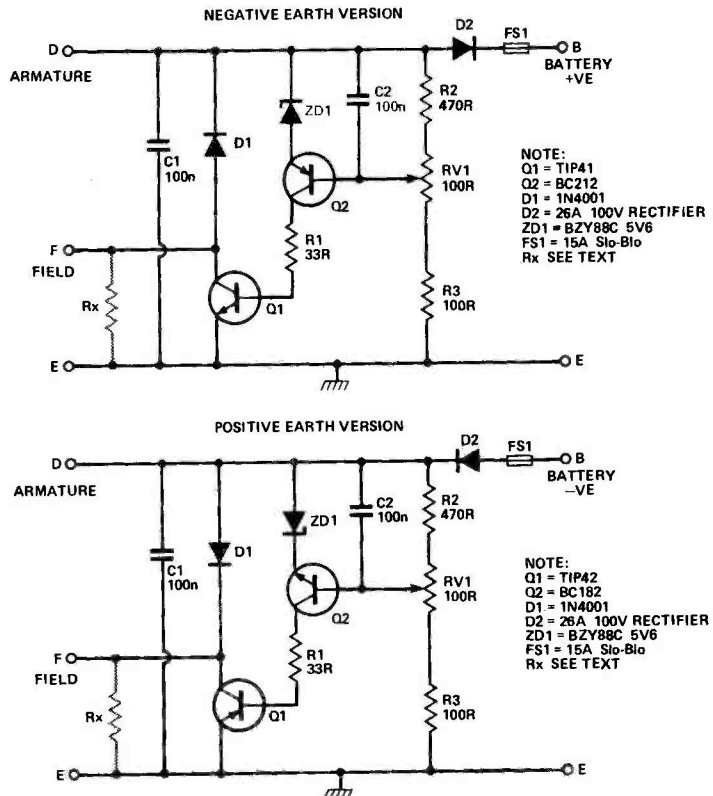
Regulator For DC Generators

J. Michael,
Broadstone,
Dorset

This circuit was developed to replace the regulator on a motorcycle when the original component failed and a replacement proved impossible to obtain. It is designed to control the output voltage of a 6V dynamo used for charging a lead-acid battery but it could easily be adapted to suit other voltages. Both positive and negative earth versions are illustrated and in either case the circuit will replace the original regulator without modification of the existing wiring.

Rx is the field current control resistor. On the original unit this was incorporated in the dynamo, but for most applications a separate resistor will have to be fitted in the regulator. A 10W wirewound type should be used. The series diode D2 replaces the cutout in the original regulator. D2 and Q1 should be mounted on a small heatsink.

To set up the desired charging voltage (6.9V in the case of a 6V lead-acid battery) set RV1 fully clockwise and run the dynamo at maximum speed with a fully-charged battery connected. RV1 should then be adjusted until the battery voltage is correct.



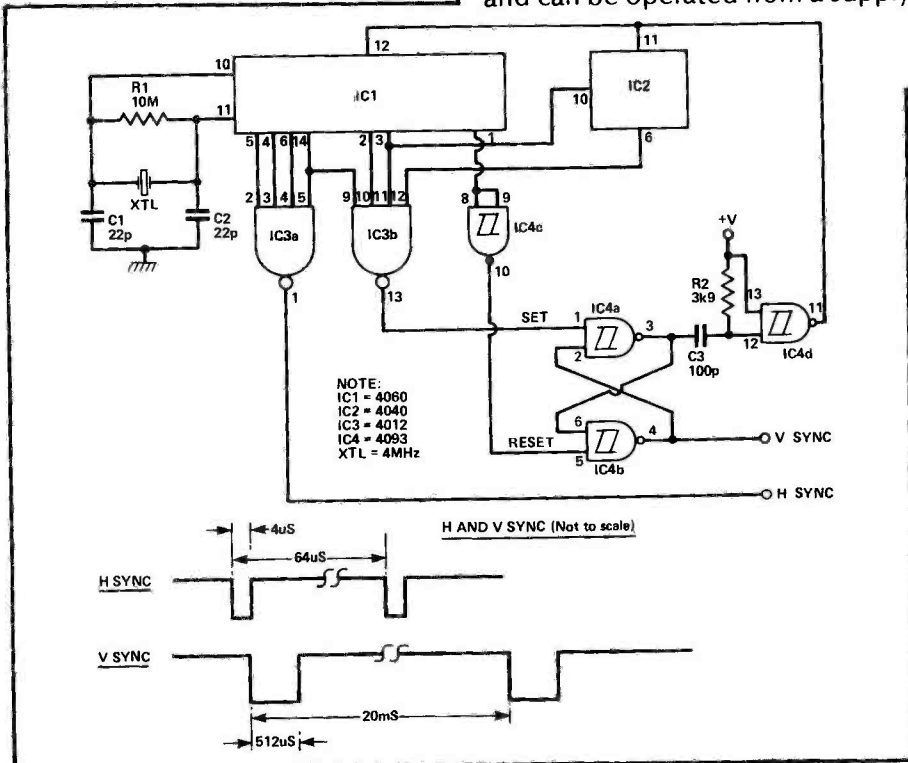
TV Sync Generator

J. C. Barker,
Morley

This crystal controlled sync generator uses only four cheap CMOS ICs, a 4MHz crystal and a few Rs and Cs, and can be operated from a supply

of between 5 and 15V.

IC3a gates the Q5, Q6, Q7 and Q8 outputs from IC1 to generate the H sync pulses. The V sync is generated by IC3b which gates Q8, Q13, Q14 and Q17 (the third output of IC2) to set the latch IC4a and b after 19.488 ms. The latch is reset 512us later by the Q12 output of IC1 via IC4c. IC4d then generates a positive going pulse to reset the two counters and start the cycle all over again.



Attention!

Would the authors of the following Tech tips please get in touch with us:-

CRU Interface For The Cortex Caravan Indicator Warning Light
In each case the address of the author has been mislaid and we need to contact them before using the items.

May we also take this opportunity of advising all Tech Tips authors to write their names and addresses on each sheet of their submissions rather than just on the title page. This ensures that, even if the sheets get separated, we will still know what belongs where. This is especially important with drawings which are treated separately from the text and therefore stand the most chance of going astray. With luck, if this advice is followed, even we won't be able to lose things!

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THE SECRETS OF TELECINE

It's not that easy to turn 'Towering Inferno' from a wide-screen epic into a small-screen Sunday matinee, and not all the difficulties are those of imagination. We'll be looking at the technicalities involved.

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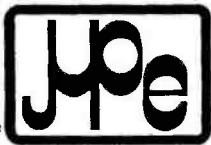

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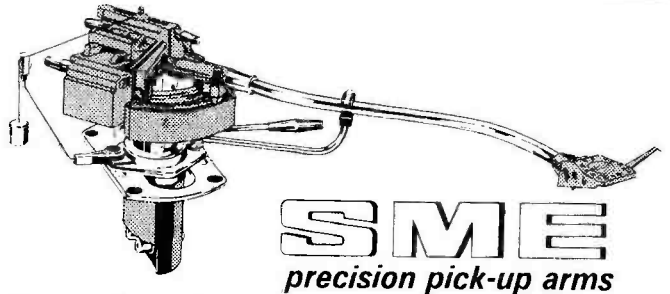
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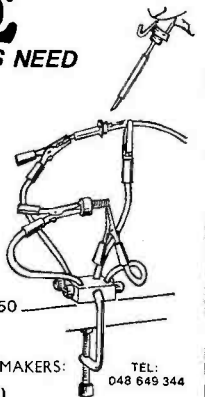
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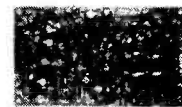
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DIGITAL FRAMESTORE

The project draws to a close with the last of the constructional details, suggestions on how to link the unit to a home micro and what to do with it when you've done this, and a mod to use an external sync source. All by Daniel Ogilvie.

Essentially the framestore is a large piece of memory. Various bits and bobs have been added to it to format the memory so that it can be easily written to and read from in a format compatible with a raster-scanned TV system. However at the heart of it all is a large piece (512K) of dynamic RAM just waiting to be got at by your home computer. The home computer itself can perform some quite powerful image processing routines.

We have seen that grey level manipulations can be performed by the lookup table and for the type of thing discussed that offers us a faster non-destructive method. It could equally have been performed by the home micro. Indeed, a micro with access to the framestore memory was essential to construct the grey level histogram. Image storage is another area where the home computer can be of some use, although your average floppy disk will throw a fit at having to cram on the 393K bytes necessary to store just one image. However parts of images may be stored and the more adventurous may choose to write some image compression routines, a 10:1 reduction being possible on simple images.

Getting At The RAM

Most home computers are based on either the 6502 or Z80 MPU's, with a smattering of 6809

and 68008 (just), amongst them. Mr Sinclair has chosen the right road with the QL for our average image processing buff, in that the 68008 can address 1Mbyte of memory directly. The 512K of the framestore can slot in nicely. Most micros are restricted to 64K and by the time we have added an operating system or two and some of its own RAM there may be little left to access the framestore. There is a lot to be said, therefore, for a dedicated micro providing a serial or, preferably, a faster parallel interface to the home computer, or providing a DMA interface to shift chunks of the framestore memory's data to and from the micro's own RAM.

We will not take this approach, however, but will make the assumption that at least a 16K block can be freed through which we can access the framestore RAM by bank selection. The popularity of the home micros has been reflected in two designs recently in ETI for dynamic RAM controllers for the 6502 and Z80. Also recommended is the excellent Texas TMS4500A DRAM controller user manual, which provides circuits to interface some other microprocessors to DRAM, including the 68000, 8085 and TMS9995.

Other DRAM controllers are available, from AMD and Intel amongst others, with exhaustive application notes. We will concentrate therefore on the bank select logic and particular points regarding the interface to the

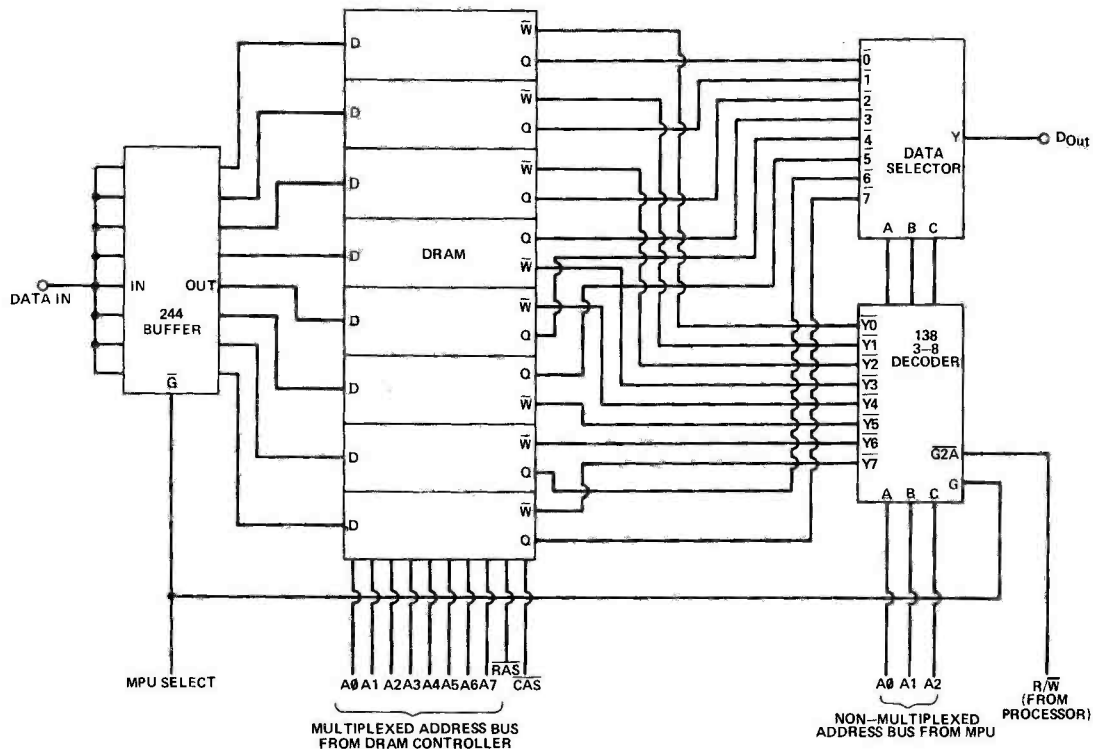
framestore RAM.

You will remember that each RAM card stores one bit of data. There are eight 64K X 1 DRAMs on each card, which is configured to store 512K X 1 of data. We provide an eight bit shift register on the card which temporarily stores the incoming data before we parallel load this 8-bit byte into the RAM. This overcomes the relatively slow access time of the DRAM. Each DRAM therefore stores every eighth bit of the same DRAM address.

The facility has been provided on the card to turn off the drivers to the RAM address and control inputs. This allows access to an external DRAM controller. When the MPU line is pulled low (and MPU is high) the DRAM address multiplexors and W, RAS and CAS drivers are turned off, (high impedance) as is IC17, the latch that drives the data lines to the RAM.

We now have complete access to the RAM on the card and are free to access any of the 64K bits of RAM. We do, however, have to perform some multiplexing of the data and control lines to enable us to sequentially access pixels from the DRAM and not have to worry about the complications caused by the shift register. Were we not to do this, and, for example, tied each data line of the DRAMs to a separate MPU line, sequential pixels would appear on each line of the MPU data bus.

To access any of the remaining five data bits we would need to



select a separate part of memory. For example, assume we wish to read from the framestore memory. First set up the most significant address lines of the micro-processor bus (latching them into a port), then perform a memory read operation at the address we want to access. The DRAM controller performs the multiplexing of all but the lower three address lines and then strobes \overline{RAS} and \overline{CAS} low in turn. When \overline{CAS} is strobed low, all eight dynamic RAMs turn on their output drivers and, after the \overline{CAS} access time, the data at the address we have selected becomes valid.

In fact we access eight sequential pixels worth of data at the same time. The data outputs from the DRAM are taken to the eight to one multiplexor IC19. We select one of the eight DRAM outputs by means of the three lower address lines: the data bit appearing on the MPU data bus is thus just one of the selected pixels. If we wish to access the next sequential pixel we increment the address line by one. The address loaded in to the RAM is the same but the lower three address lines select the next bit from the next DRAM. This is performed on all six boards simultaneously — each board drives a separate MPU data line — only D0-D5 of the MPU data bus are used. This process is illustrated diagrammatically in Fig. 17.

This method is not the most efficient to access the RAM, but it is simple. By strobing all of the \overline{CAS} lines simultaneously (and thus turning on all of the RAM drivers simultaneously) maximum current is taken. We are turning on eight RAMs to access one per board. Ideally we should multiplex the \overline{CAS} lines to the RAM's using the same method we use for writing.

Writing to the RAM is performed much the same as reading. The DRAM controller responds to a write access request by strobing \overline{RAS} and \overline{CAS} low to latch the two eight bit address inputs. Because the R/\overline{W} arrives before \overline{CAS} (read/write is set up with the address lines by the MPU) the DRAMs perform an early write and the Q outputs will remain in a high impedance state. When R/\overline{W} is low and a valid \overline{CS} has been received, the 74LS138 (IC14) decodes the lower three address lines and the appropriate Y output is strobed low driving the DRAM write line low, and latching in the data that has been set up on the D inputs (and buffered by IC18).

Although slightly more complicated, this method of accessing the DRAMs allows the MPU to "see" a logical memory map. The first pixel stored (top left of field 1) is at address 00000H, the next along the line is at 00001H, etc. The end of the first line (pixel

number 639) is at 0027FH. The next line starts at address 640=00280H and ends at 004FFH=640+639. The end of the first field is at (640X-256)-1=27FFFH. The next field starts at 28001H and ends at (640X512)-1=327679=4FFFFH.

In this way, any dynamic RAM controller can access the framestore as if it were a conventional piece of memory. We have also seen that it is necessary to be able to address 327,679 bytes to have access to all of the framestore and this is beyond the addressing

PARTS LIST MEMORY CARD

RESISTORS (all 1/4W 5%)

R1-10 33R
R11 2k2

CAPACITORS

Unmarked decoupling — all 100n ceramic

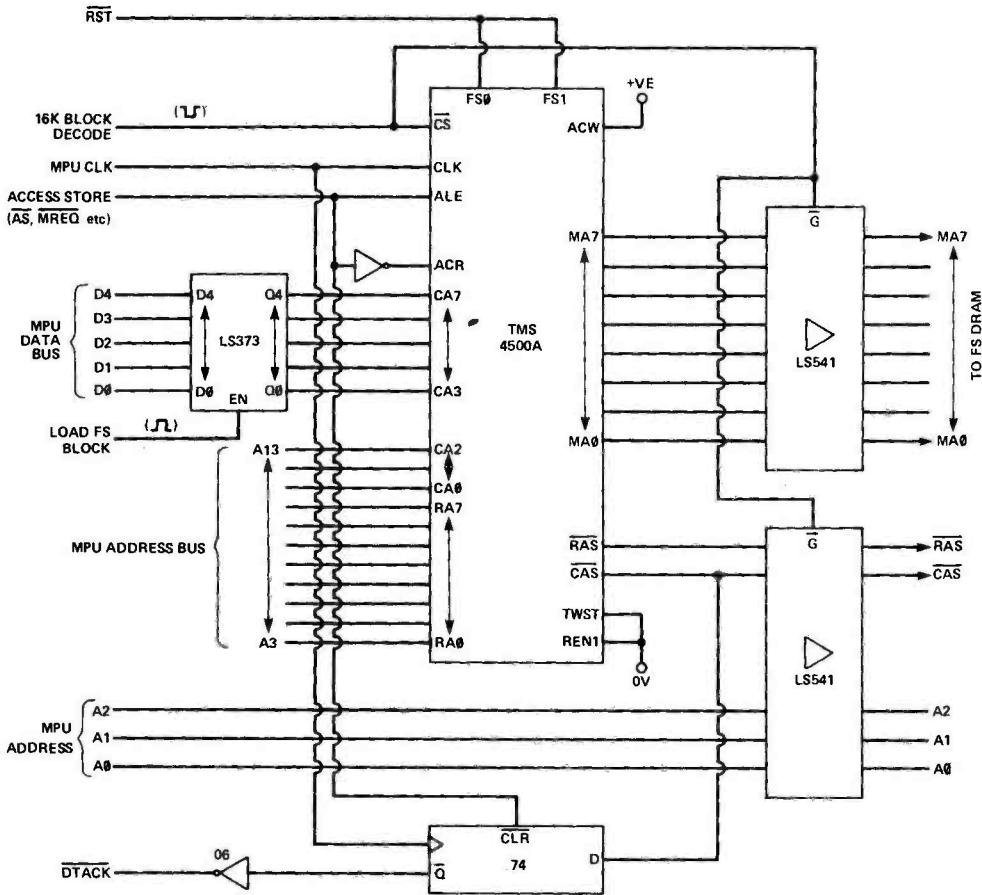
SEMICONDUCTORS

IC1, 10 74LS257N
IC2-9 MCM666L20
(64K X 1 200ns
DRAM — see text)
IC11,12 74LS08N
IC13 74LS244
IC14 74LS367 (8T97)
IC15 74LS138
IC16 74LS138N
IC17,18 74LS195N
IC19 74LS374N

MISCELLANEOUS

PCB: wire solder, etc.

PROJECT : Framestore



plete framestore (20 X 16K = 327,679). The additional upper address lines we require can be stored in a latch by an additional MPU load instruction to select one of the twenty 16K blocks before we perform a memory read or write. Normal read or write operations can now be performed within the block selected.

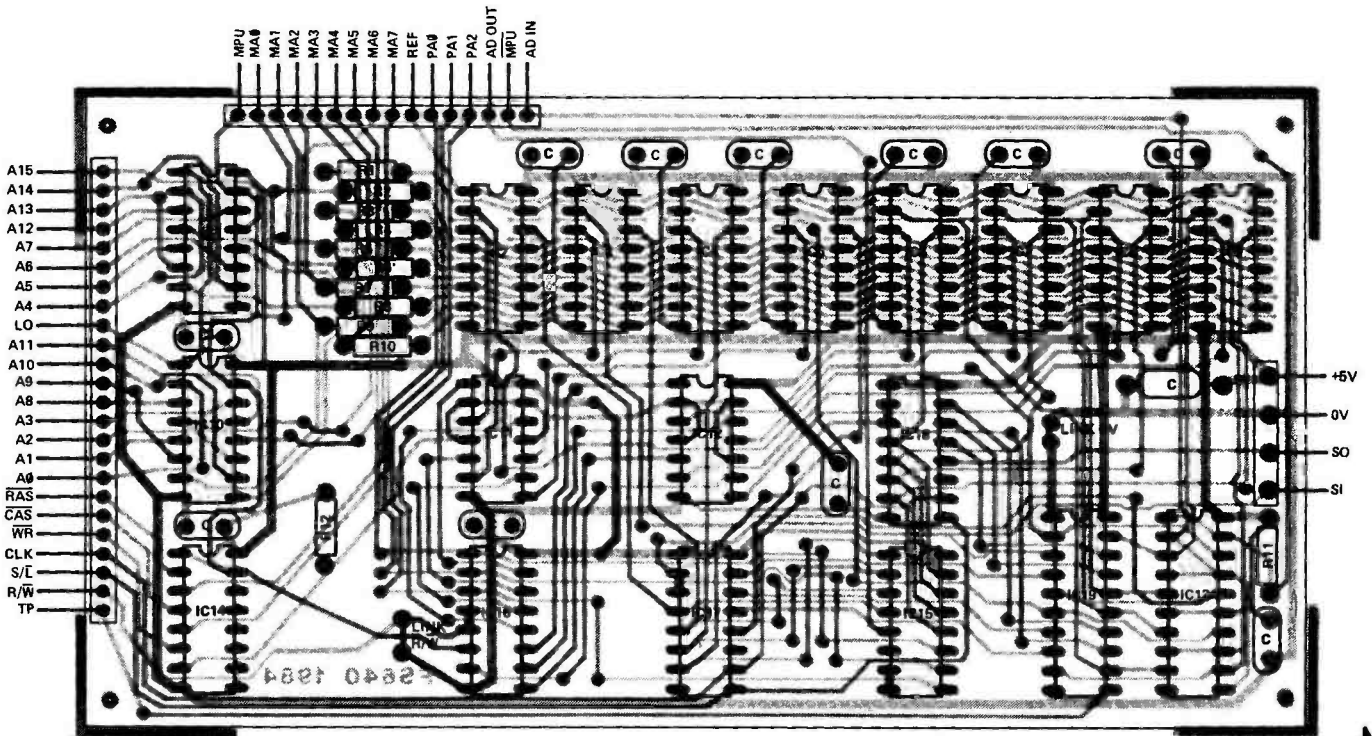
Synchronising The Framestore

The framestore as it stands is intended to be the master sync generator, ie, it will provide the synchronisation for all the other units in the system connected to it. However, this is not always possible, for example, when using video recorders, off-air broadcasts and some cheap video cameras. The modification described here allows the framestore to be externally synchronised.

The modification works by replacing IC5 on the control card; IC5 is the sync pulse generator IC. The heart of the replacement circuitry is the TA6993W, which is itself a sync pulse generator, but with the facility to synchronise to an external reference. This IC normally runs off the 500kHz clock input to pin 23 (this should be derived from the 25MHz clock already on the control card). The TA6993W generates an odd field pulse instead of an even field pulse (as with IC5, ZNA134) but

range of most 8-bit micro-processors, which makes it necessary to implement a bank selection technique to enable us to peer through a movable window at the framestore.

A suggested circuit for this is shown in Fig. 18. If we have, for example, only 16K of memory available in the micro, we will need to be able to select one of twenty blocks to access the com-



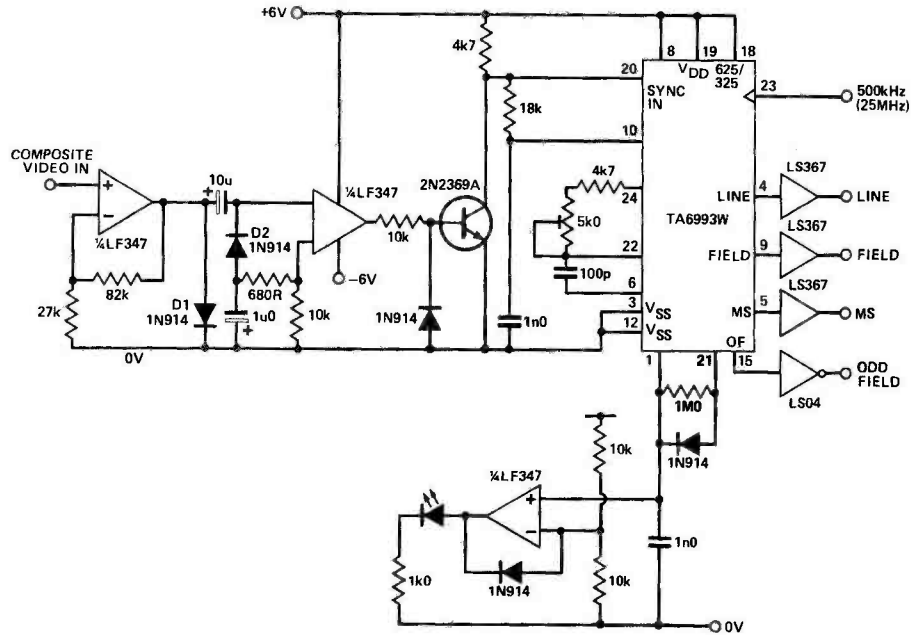
NOTE:
ALL UNMARKED C's = 100n

this is not important, it just shifts our reference point.

The TA6993W contains a phase comparator and a phase-locked loop. When negative going mixed sync pulses are presented on its pin 20 it switches over from the external oscillator to an internal voltage controlled oscillator formed by the RC network on pins 6,22,24. The frequency of this oscillator is varied until the internally generated line and external line input are locked in phase.

The vertical synchronization is achieved by integrating the mixed sync input via the 18k and 1nF capacitor, which generates a field pulse, and using this to reset the vertical line counter. This method produces a quite effective external lock but it will never be as stable as the original method. The trimmer should be adjusted until a stable lock is obtained; be careful to avoid twice line frequency. The switch over between internal and external oscillator is performed automatically and the sync source is indicated by detecting the voltage level on pin 1 and lighting an LED (+6V = external sync).

The front end of the circuit is a



sync separator which strips the syncs from the composite video input. The composite video is amplified and clamped by diode D1. This is fed to a comparator formed by the op-amp. The other terminal of the op-amp is fed with a proportion of the signal from the

peak detector formed by diode D2 and the capacitor. The comparator threshold is therefore set just up from the sync tips, preventing false triggering due to noise.

ETI

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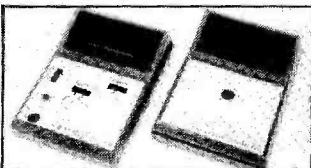
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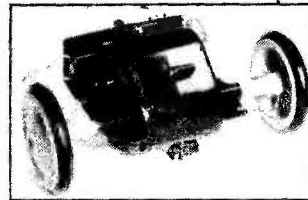
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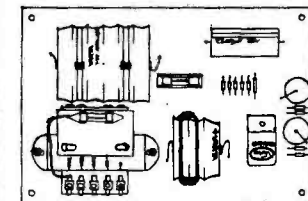
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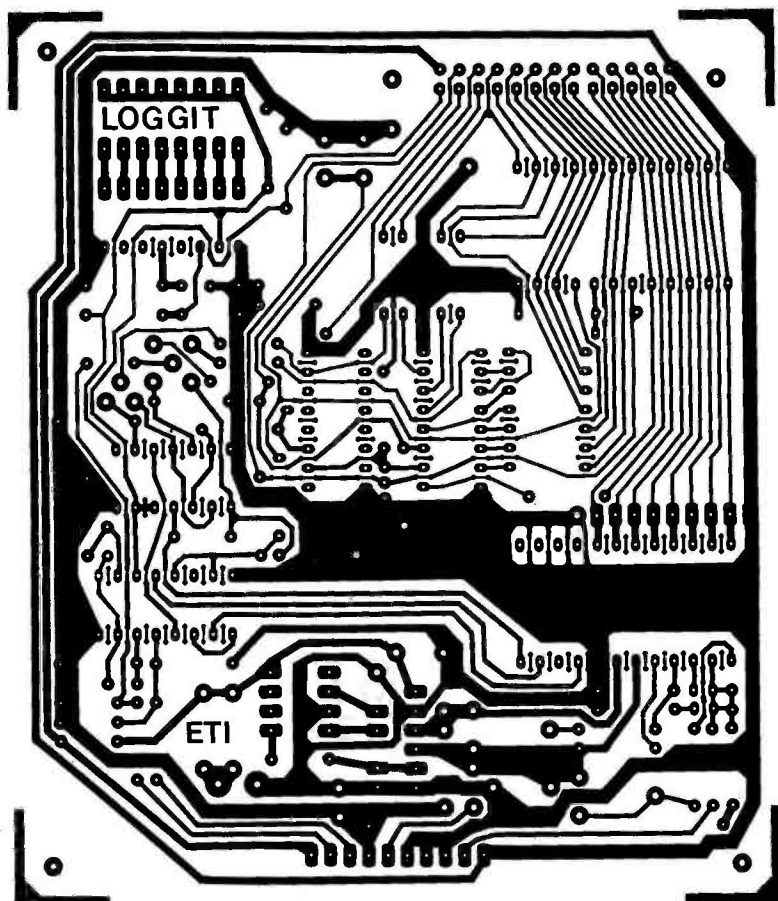
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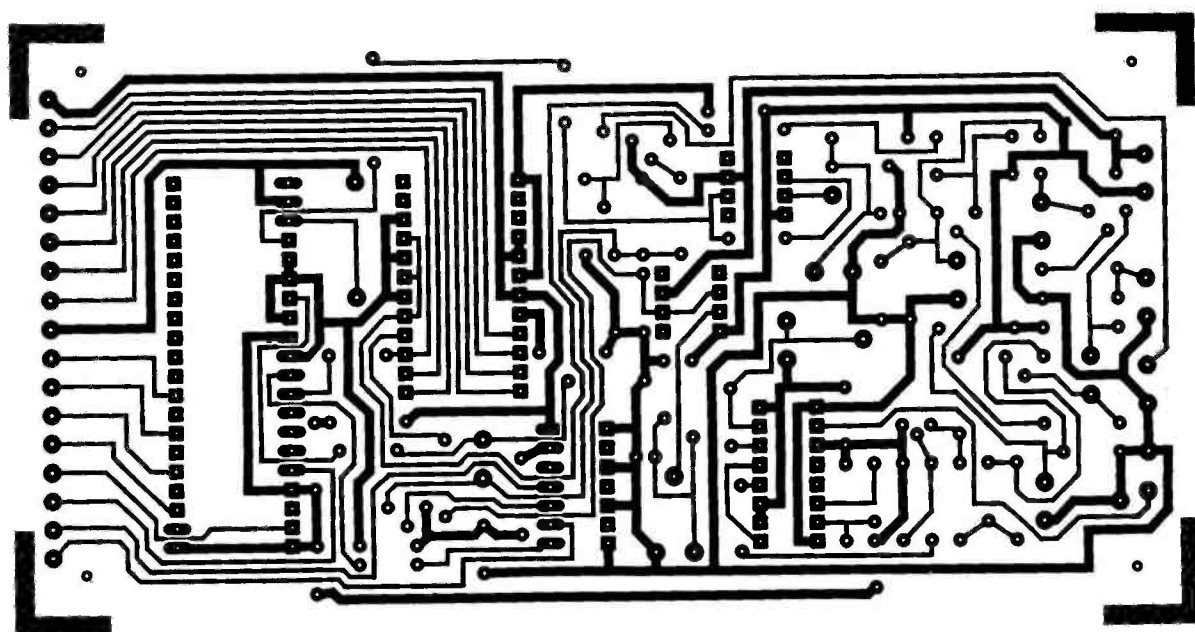
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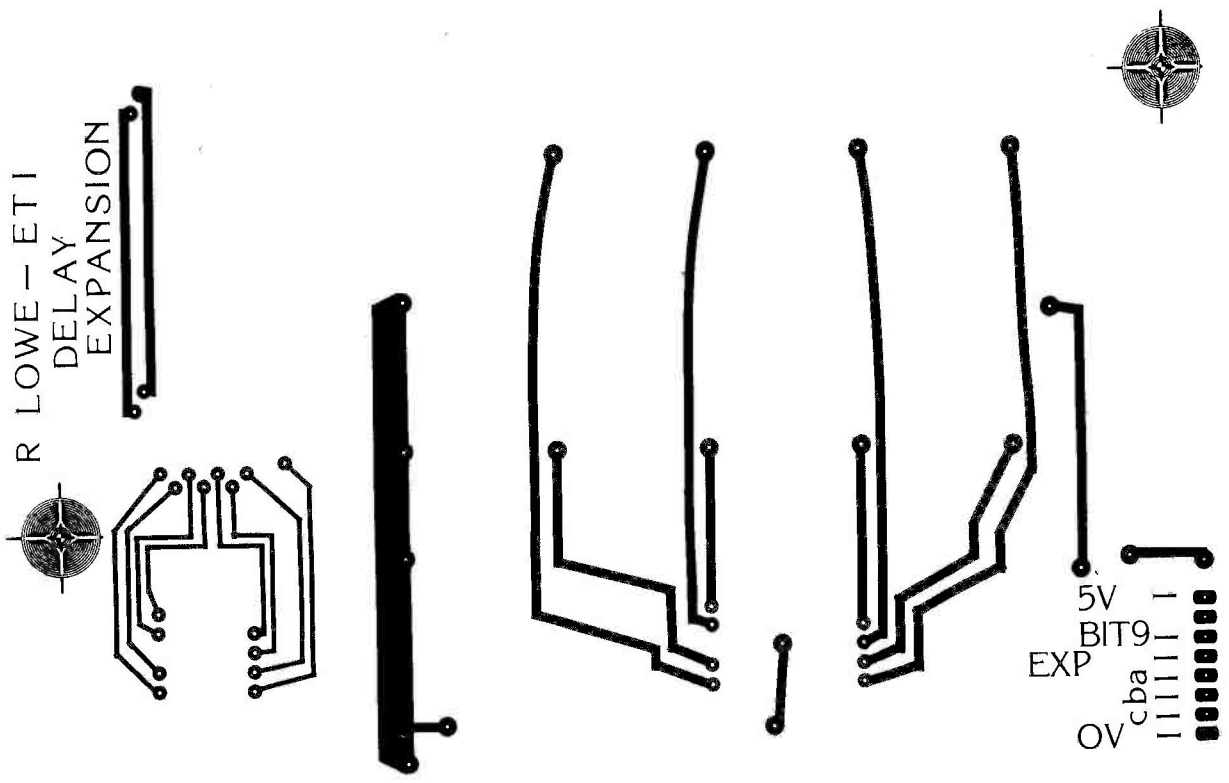
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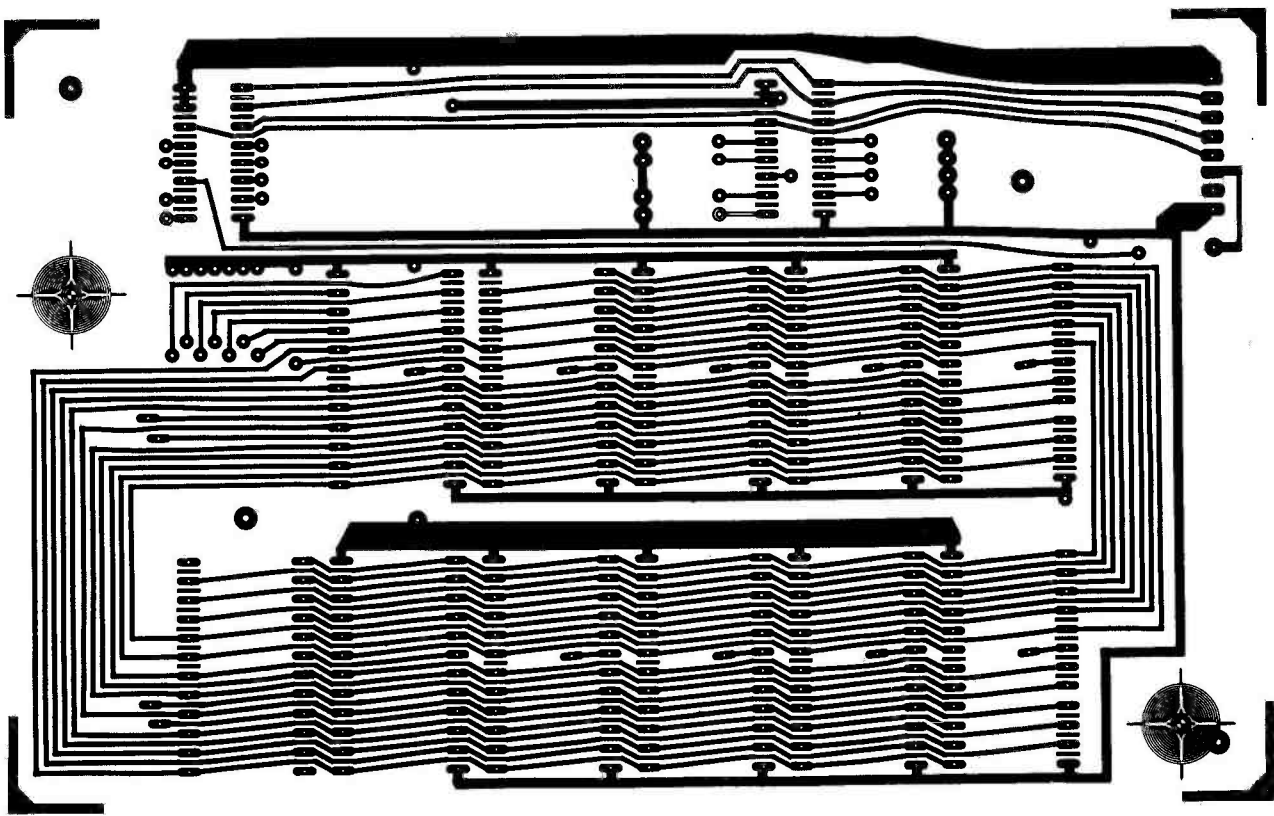
Two of the foil patterns held over from last month, the Data Logger board (left) and the Digital Framestore ADC/DAC board (below).

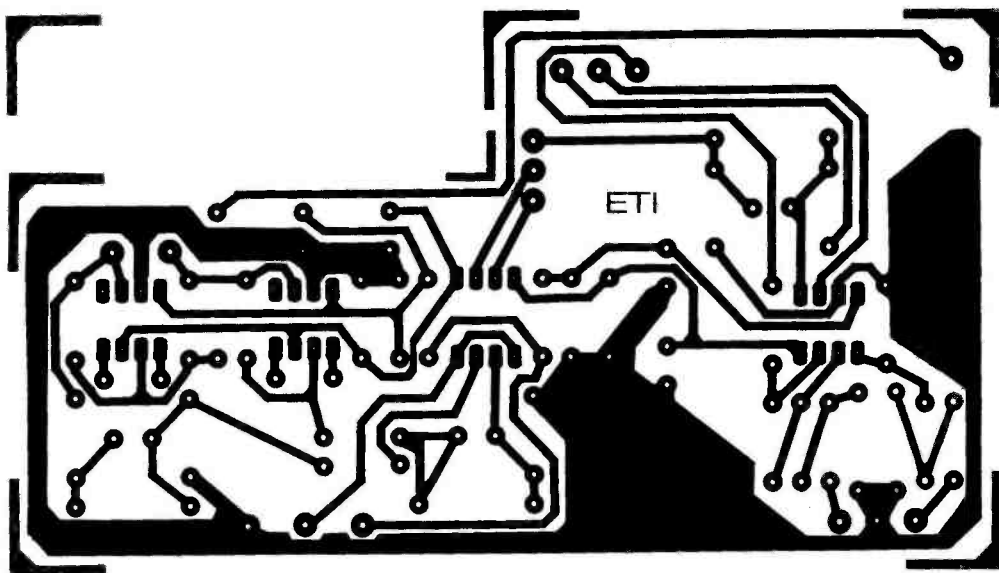


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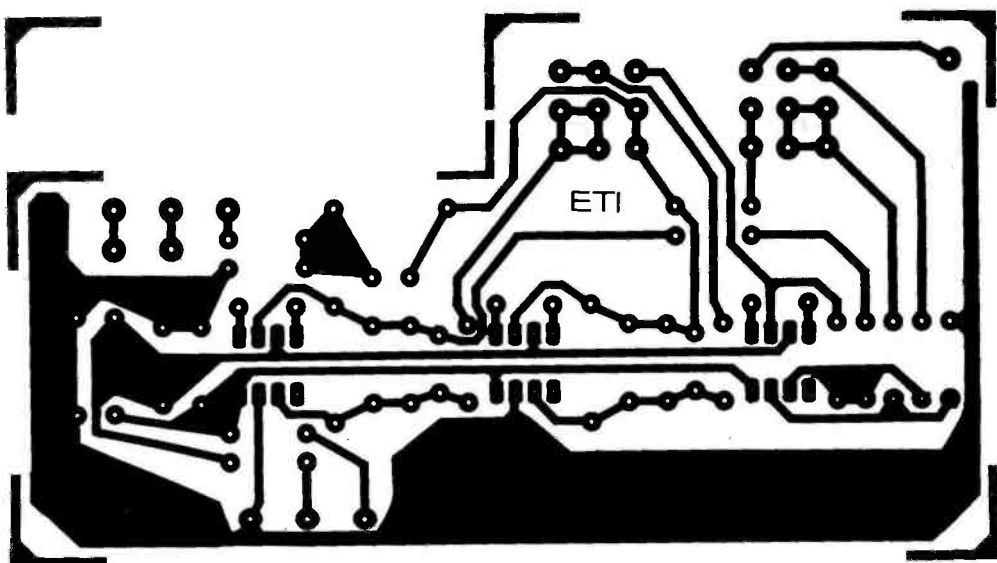


The top and bottom foils of the Digital Delay Line Expansion board, held over from last month.

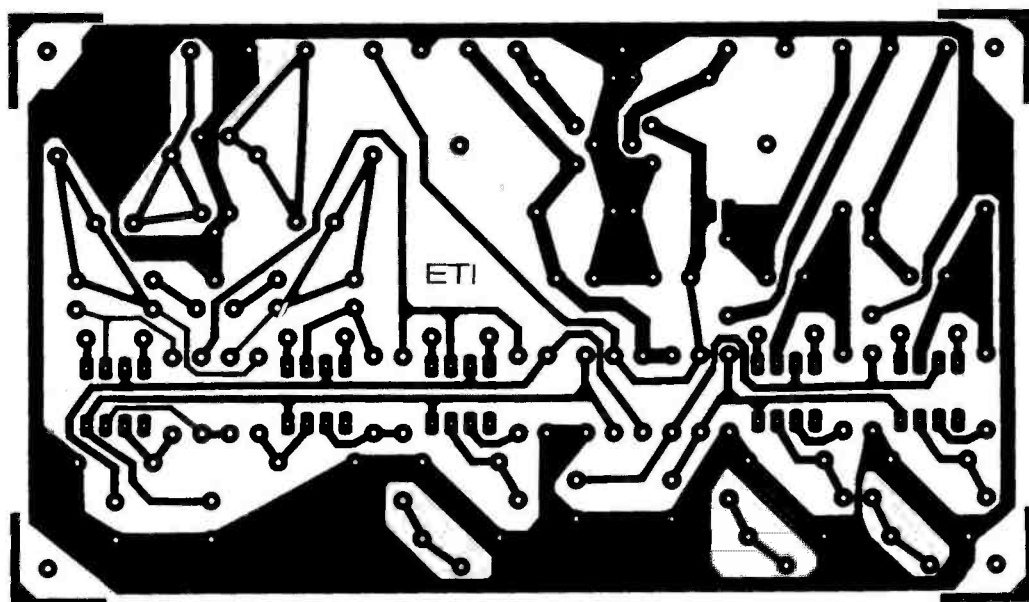




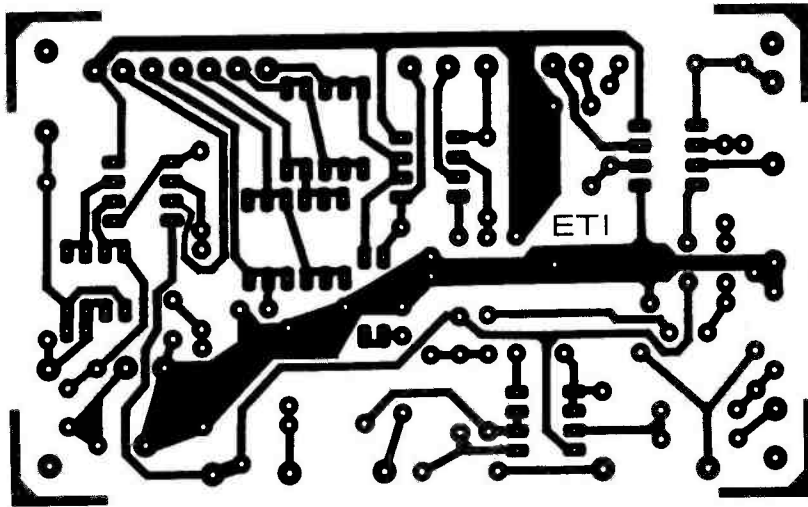
The ParaGraph Equaliser input stage and main signal path board.



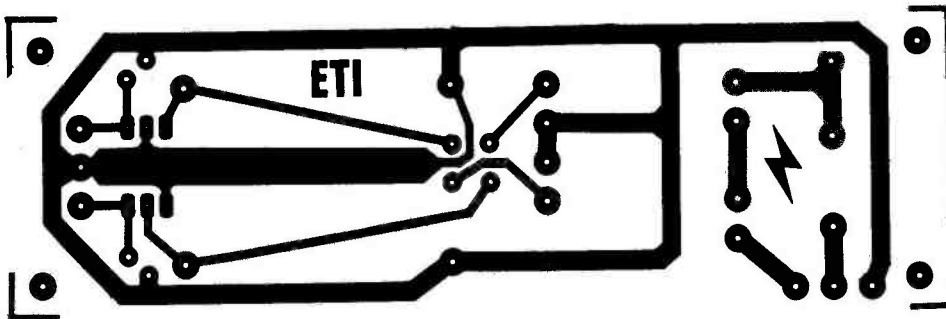
The ParaGraph Equaliser filter board.



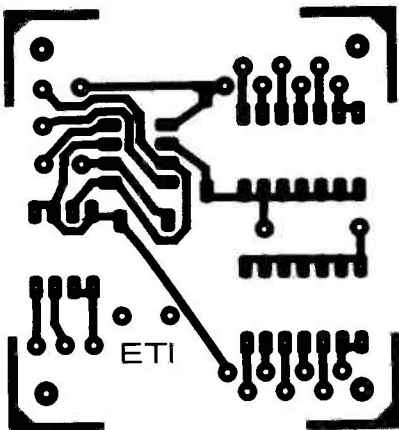
The ParaGraph Equaliser balanced output, tape buffers and regulated supply board.



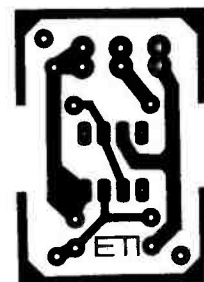
The THD and millivoltmeter board for the Distortion Meter.



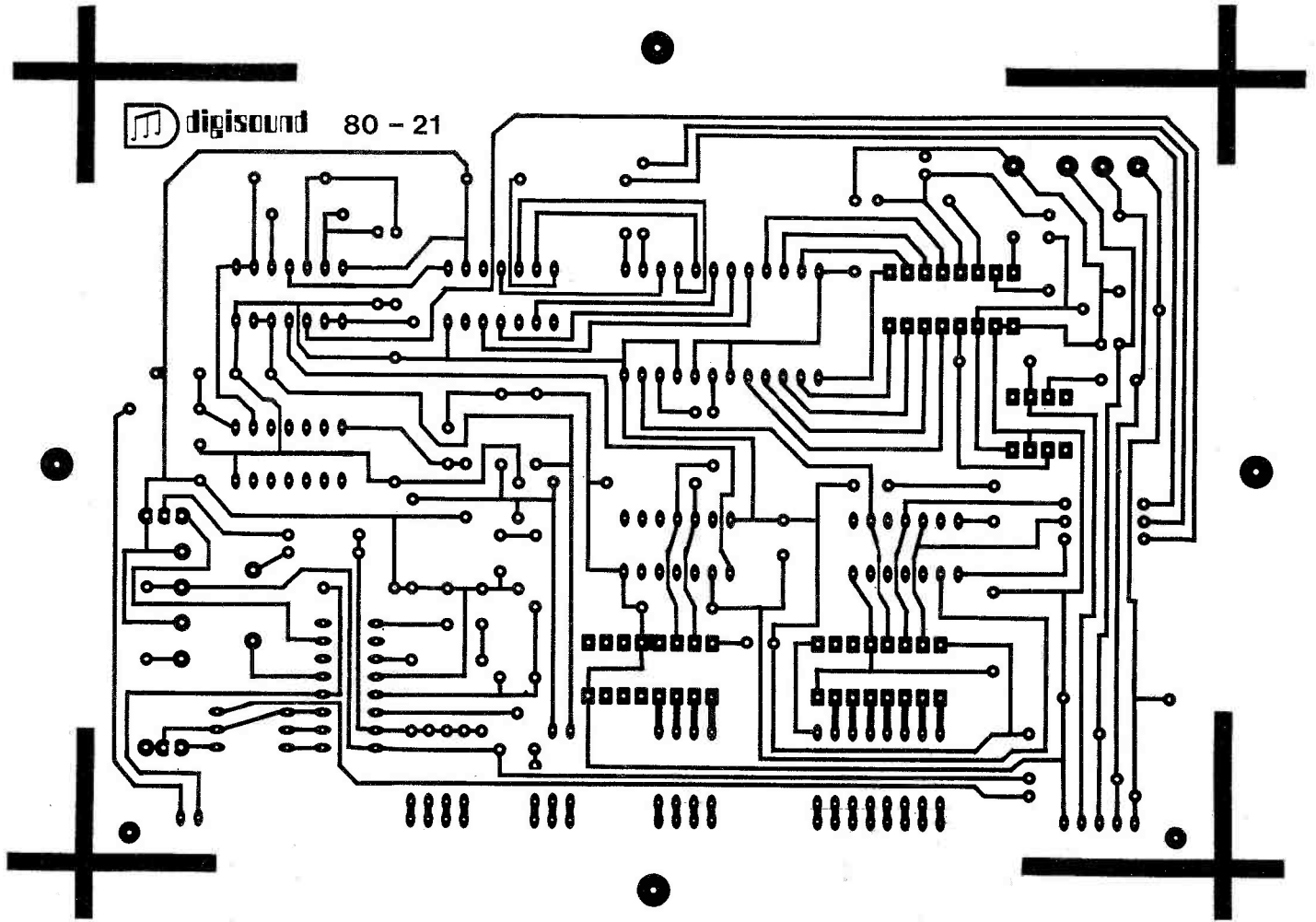
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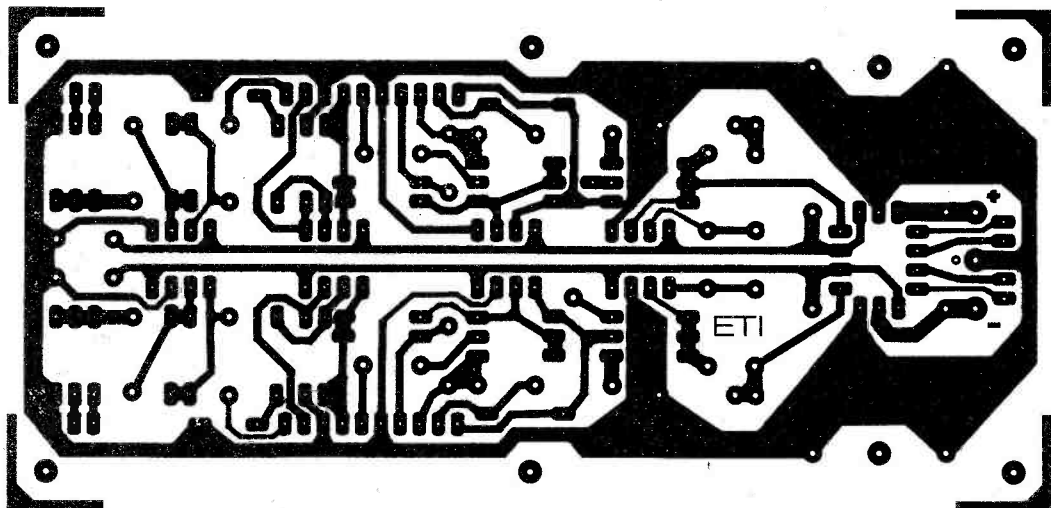
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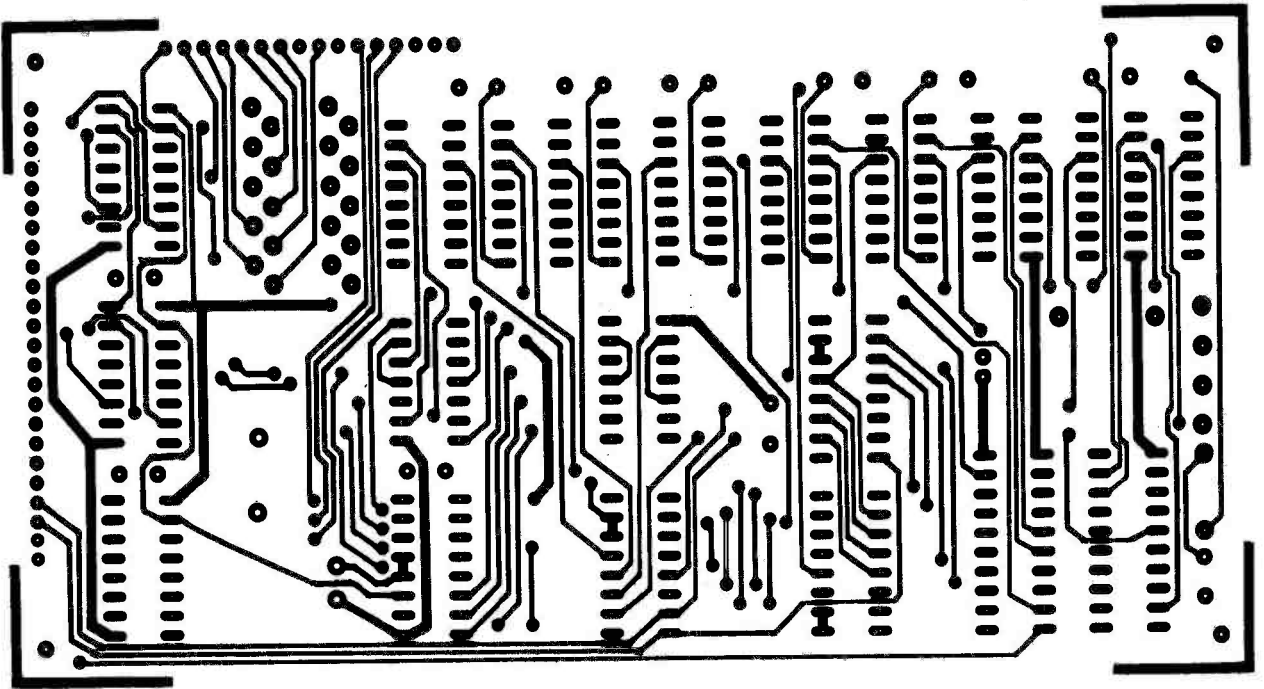
The Distortion Meter single battery supply board.



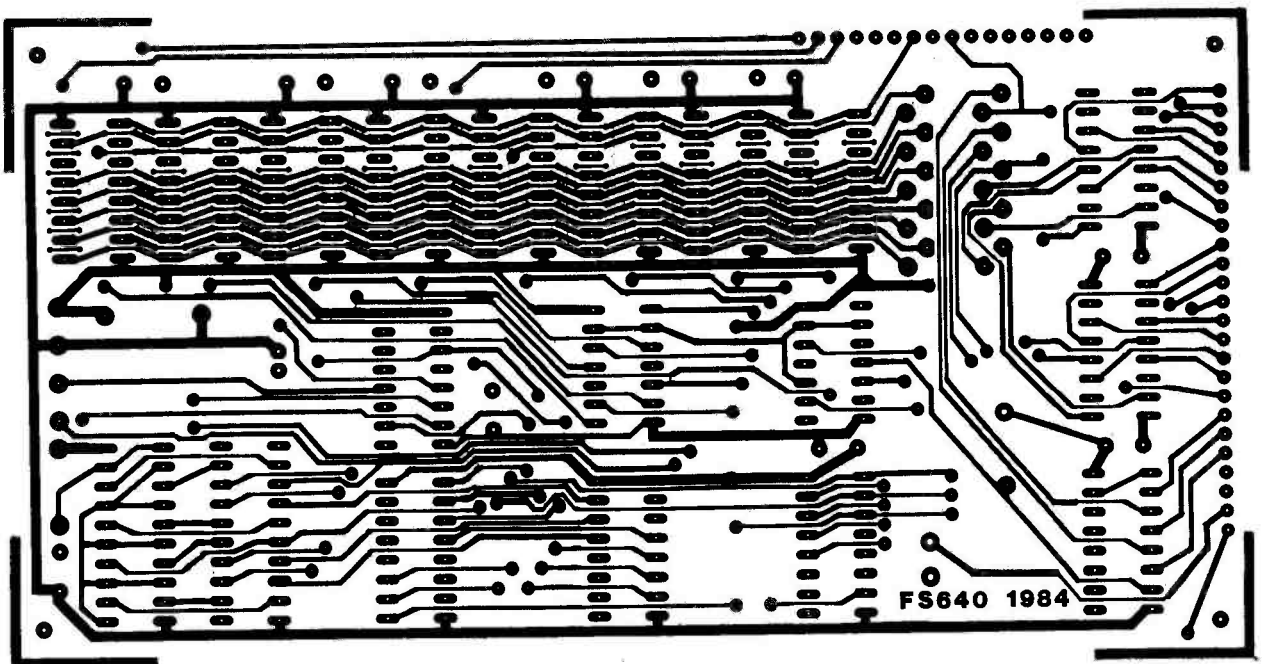
The Voltage Controlled Digital Oscillator board.



The preamplifier and regulator board for the combo.



The top and bottom foils for the Digital Framestore memory card.



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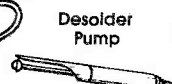
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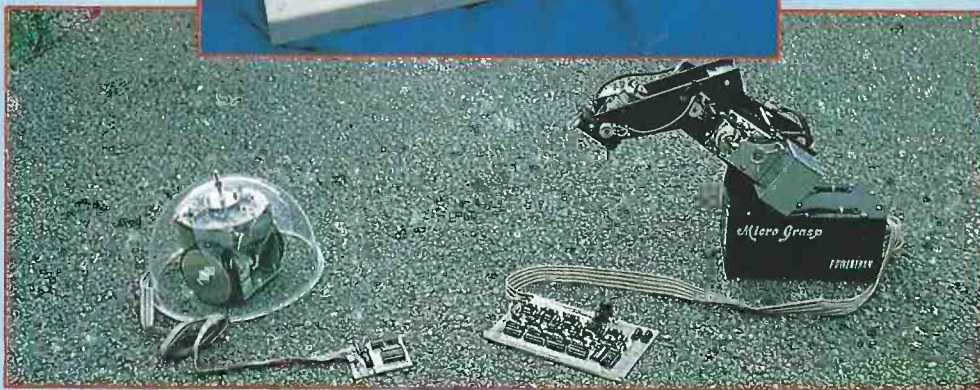
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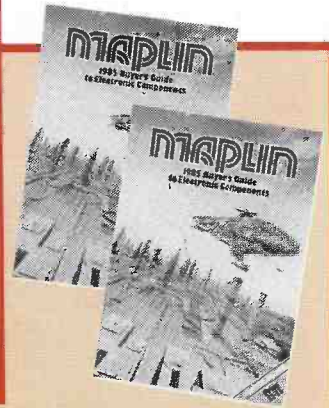
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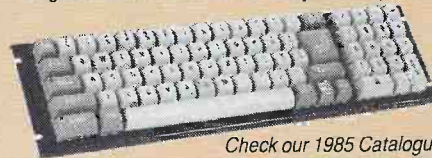
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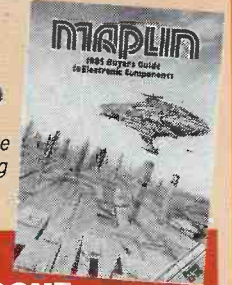
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