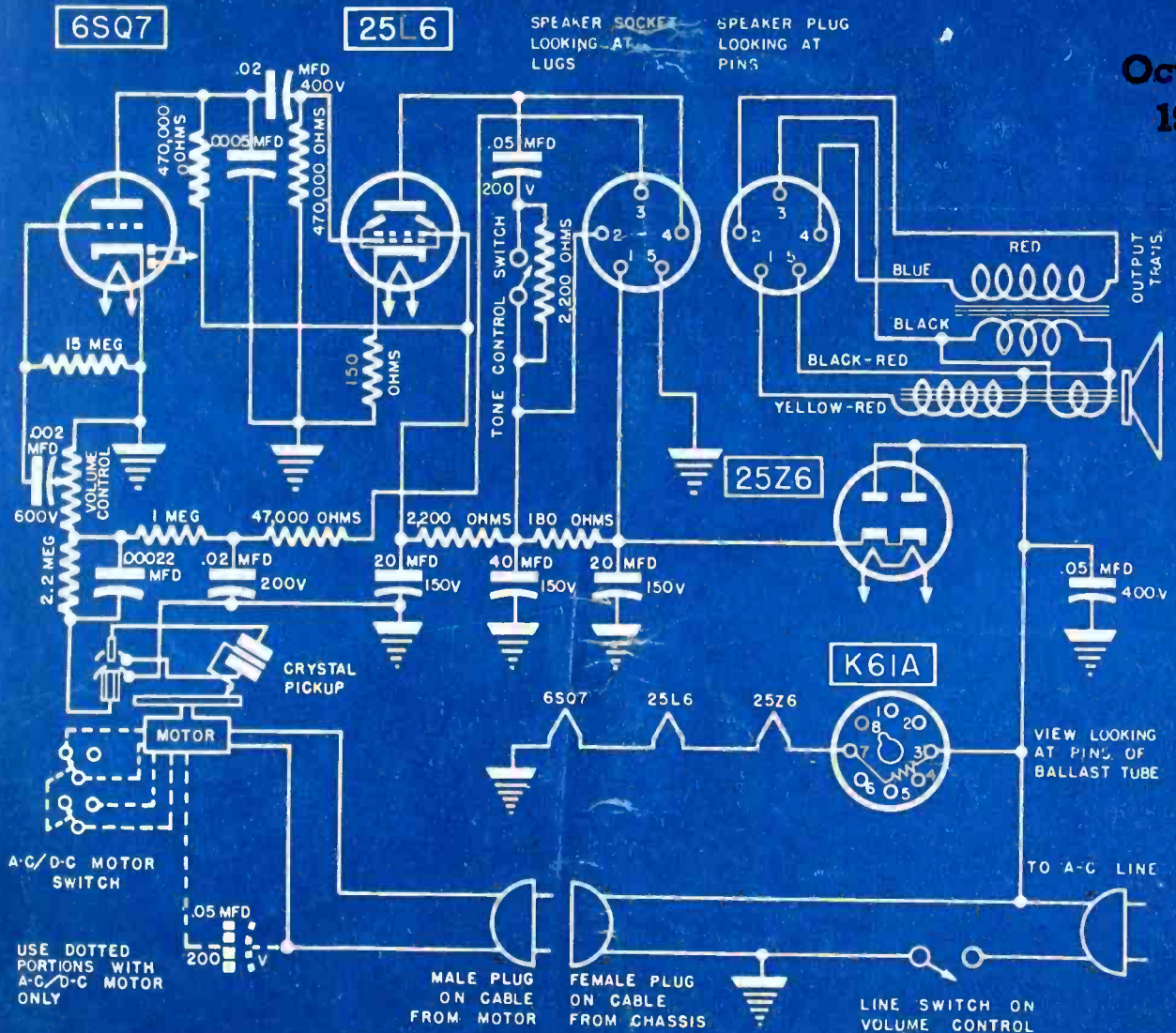


SERVICE

October
1945



A self-contained tube-watt phone amplifier featuring a rumble attenuator. (See page 57.)



busy as a beaver?

Telephones buzzing...shopping for parts...accounts to balance...and jobs lined up 10 deep. Doubling on "desk duty" sure cuts into a fellow's at-the-bench time, but not the smart servicer's. He gets extra working mph (minutes per hour) by buying replacement parts he can trust...parts that do the job right first shot.

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Ken-Rad Tubes have played a vital part in bringing about higher standards of home radio reception . . . Now, to tube quality already foremost, are added great new research and engineering facilities . . . Ken-Rad Radio Tubes consequently are *better than ever*, increasing the desirability and profit opportunities of the Ken-Rad sales franchise.

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KEN-RAD

DIVISION OF GENERAL ELECTRIC COMPANY

OWENSBORO, KENTUCKY

THE multi-million dollar community-housing developments recently announced for New York City and also scheduled for other cities throughout the nation, have alerted many Service Men to the large-scale servicing possibilities of these programs. To provide expert radio maintenance and repair for the thousands of tenants who will occupy these buildings, some Service Men have projected group servicing plans and submitted them to the multiple building owners. The plans have included complete single-manned shops for each building to larger shops that can service a series of buildings. In the larger shops Service Men assigned for each building would repair the receivers. In addition, the shops would feature a specialist on a-m, f-m, television and antennas, so that it would be simple to cope with any particular receiver problem in any of the buildings. Since servicing would actually be on the premises, balky repairs could be completed with a minimum of delay. And since in many instances the same antennas could be used for on-the-air testing, the field tests would be more accurate too. Where the repair would require the receiver to be kept in the shop for more than a day, a loan set service is planned. This plan was utilized quite successfully during the war.

Since servicing many receivers simultaneously requires quite a complex instrument setup, a simplified portable-fixed arrangement has been planned by several Service Men. In this setup, the instruments would be housed in a rack mounting and arranged so that they could be plugged into position for fixed use, or removed via a multi-pin plug jack for portable work. Thus, full utilization of the instrument would be possible at all times. In addition, a practical housing would be provided and there would be less possibility of damage. All instruments would be properly identified and supplied with top and side folding handles that would sit in recesses when not in use so as to permit compact mounting.

Novel ideas that merit close study!

MANY letters received recently have contained intriguing questions with problems that should be of interest to all Service Men. We plan to publish these letters and invite solutions to the problems presented. For every question published, we will pay \$1.00 and for every answer submitted and published, we will offer \$2.00. So Service Men if you have a question, send it in. Not only will you receive an effective answer to your problem, but a reward if it is published. Let's hear from you!

THE new year will probably see many novel receivers, particularly of the miniature type. Several now planned fit into a coat pocket and use hearing-aid ear pieces. With these units the Service Men will meet for the first time the popular use of the hearing-aid type tubes; tubes that will undoubtedly be used in a variety of receivers and test devices next year. To acquaint Service Men with these tubes and their unusual circuit possibilities, we have scheduled a series of analysis papers. The first installment will appear in December. Be sure to read this series!

A Monthly Digest of Radio and Allied Maintenance

Reg. U. S. Patent Office

Vol. 14, No. 10

October, 1945

LEWIS WINNER

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Advisory Editor

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The Reader's Digest, in its Aug., 1941 issue, ran an article saying that investigators on its staff found that radio service-dealers cheated the public on 64 out of 100 repair jobs. After citing several examples, the article ended with a warning that radio owners should "beware" of the repair man.

N. Y. HERALD TRIBUNE
JANUARY 24, 1945

City License Law Urged For Radio Repair Men

Magistrate James A. Blanchfield declared yesterday in Flatbush Court that he would ask the City Council for a law requiring

SHOULD RADIO SERVICE DEALERS BE LICENSED?

THE NEW YORK TIMES
JANUARY 24, 1945

RADIO RACKETEERS ASSAILED BY COURT

City Repair Men Should Be Licensed

bonded in order to do business.

N. Y. WORLD-TELEGRAM
JANUARY 23, 1945

Irked Magistrate Lashes at Racket in Radio Repairs

Declaring that radio repairmen were fleecing customers by charging all the traffic would bear, Magistrate James A. Blanchfield in Flatbush Court, Brooklyn, took up the issue.

RAYTHEON
HAS THE ANSWER!
watch for announcement
to be made soon

No intelligent radio service-dealer will deny the fact that the reputation of his industry has suffered in recent years.

Unethical servicemen who have taken advantage of manpower and parts shortages have done great damage to public opinion. They have caused so much adverse publicity in national magazines and influential newspapers that dealer-licensing, federal regulation and even finger-printing are being suggested for the public's protection.

Raytheon began many months ago to remedy this situation, and now has the answer in a strong merchandising program to be announced soon.

It will be revolutionary in every respect, enabling the public to tell which service-dealers deserve complete trust and confidence.

Dealers who can qualify will immediately have a tremendous competitive advantage. Watch for our announcement!

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RADIO RECEIVING TUBE DIVISION
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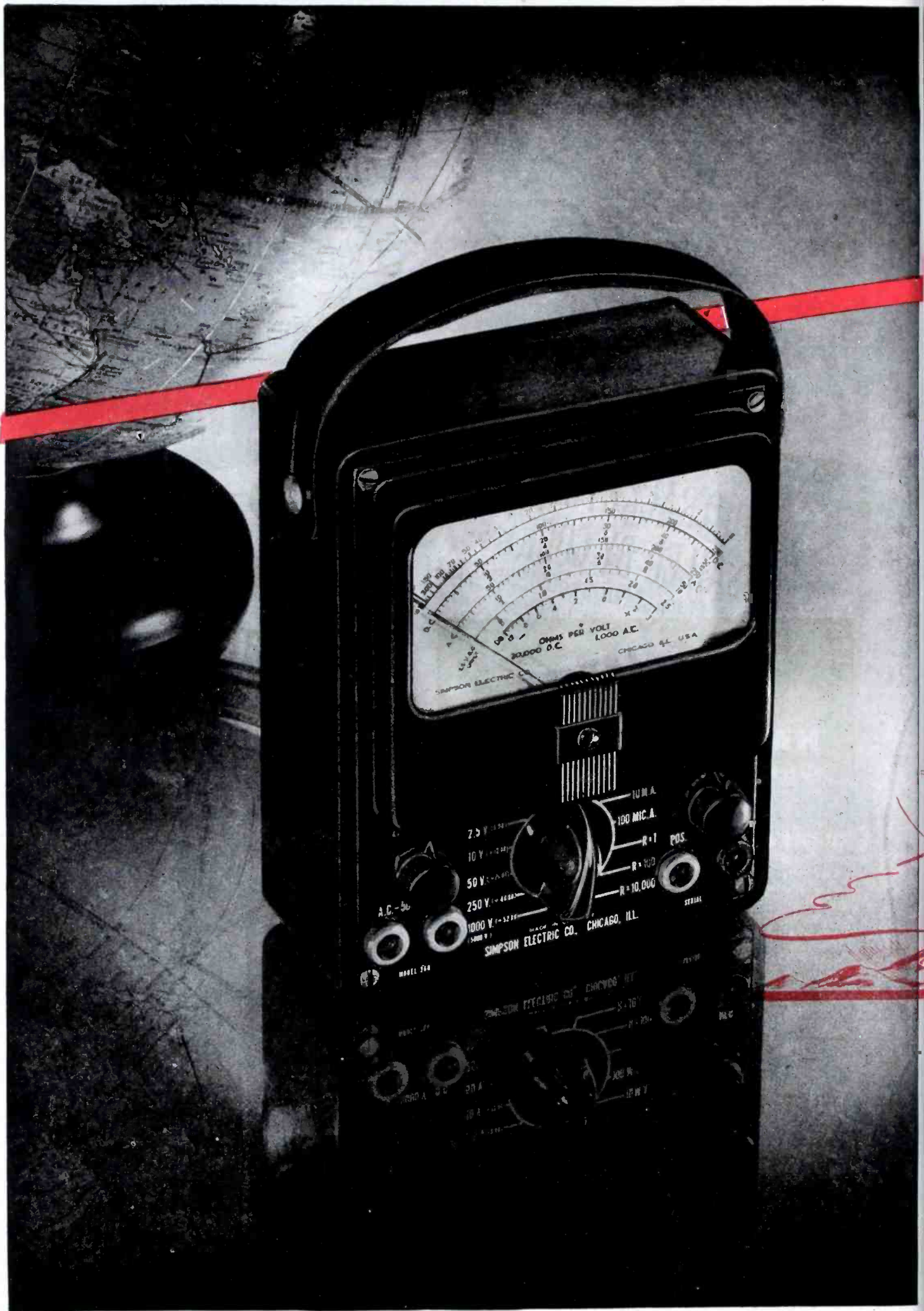
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The most honored instrument of the war

This is not our own appraisal of the Simpson 260. We knew, before the war, that it was a fine instrument but, frankly, we didn't know *how* good it was until war wrote the record. Now the story of the 260 is written into the records of such wartime industrial developments as that of synthetic rubber, and into the vast and secret research and servicing of radar.

branch of the armed services—Army, Navy, Marines, Coast Guard—carried them to the far ends of the earth. They were compelled to perform under conditions often so arduous that testimonials of amazement at their ability to function at all became commonplace as the record grew.

Chosen on its merits, the Simpson 260 became uniquely *the* test instrument of the war.

Originally designed as a radio serviceman's test unit, the Simpson 260, because of its sensitivity and wide range was found adaptable to general service duties in the entire electronics and electrical fields. Not a warborn instrument, the 260 was given thousands of essential war jobs in the production and servicing of communications equipment. It made a vital contribution to the success of tactical operations.

AVAILABLE NOW TO YOU

Now the Model 260, always the preferred instrument of radio servicemen, is available again to a widened field of peacetime services. We ask you to remember its record as an example of the quality and advanced engineering that goes into all Simpson instruments, as evidence that other new Simpson developments are well worth waiting for. They will be released as soon as Simpson standards for their manufacture are satisfied. They will continue the leadership that has given Simpson a world-wide reputation for "instruments that *stay* accurate" with ideas that *stay* ahead.

Over 300 government agencies and university laboratories of the United States and Canada procured every one of these test instruments Simpson could deliver on an expanded war production schedule. They were turned out by the thousands. Every

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At 20,000 ohms per volt, this instrument is far more sensitive than any other instrument even approaching its price and quality. The practically negligible current consumption assures remarkably accurate full scale voltage readings. Current readings as low as 1 microampere and up to 500 milliamperes are available.

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Price, complete with test leads.....\$33.25
Carrying case 4.25

ASK YOUR JOBBER

WATCH FOR NEW SIMPSON DEVELOPMENTS. THEY WILL BE WORTH WAITING FOR!

Volts D.C. (At 20,000 ohms per volt)	Volts A.C. (At 1,000 ohms per volt)	Output	Milliamperes	Microamperes	Ohms
2.5	2.5	2.5 V.	D.C.	10	0-1000 (12 ohms center)
10	10	10 V.	100	100	0-100,000 (1200 ohms center)
50	50	50 V.	500	500	0-10 Megohms (120,000 ohms center)
250	250	250 V.			
1000	1000	1000 V.			
5000	5000	5000 V.			

(5 Decibel ranges: -10 to +52 DB)

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READ WHAT THESE SERVICEMEN SAY!

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"Thanks a million! I only hope I can again sell and install your excellent products after this emergency!" Cpl. S.S., Louisiana.

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"Thanks for running my ad. It was very successful. This service of yours should and will keep Sprague in the minds of all radio men after the war!" C.J.S., New York.

"My ad brought 12 replies to date. Thanks for this service—and I, for one, am going to use all the Sprague parts I can!" E.R.S., Kentucky.

"I used Sprague Condensers before the war, and intend using them as long as I can get them during the war and after it!" E.A.F., Georgia.

"Thank you again—and be assured I'll not forget this favor when making my purchases!" L.G., Miss.

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"I couldn't name another service that benefits the radio trade at this time like your Sprague Trading Post." F.M.M., Kans.

WANTED—Hallcrafters Super Skyrider SX9 or Sky Champion S-20R. Matthew Healey, 681 Harris ave., Providence 9, R. I.

FOR SALE—Philco 077 sig. gen.; Million tube tester; Superior #1230 sig. gen.; shop made multi-meter 3 1/2" meter with precision resistors; 6 to 250 d-c volt. generator; 6A7, 6AB7, 1619 tubes; tube tester transformers, and Stewart Warner #G8243 vibrators. Radio Center, 111 S First st., Tucuman, N. Mex.

SELL OR TRADE—Philco VTVM and circuit tester #028 with diagram, \$25; signal tracer CA-10 with audio stage, \$15. Both portable. Also Riders & Corne's books and all numbers of Radio Craft, 1/2 off. Edwin Larason, Martinsburg, Ohio.

FOR SALE—Used record player in good condition. \$50. J. R. Whitaker, Farmersville, La.

WILL TRADE—Navy radio with power supply. Want Hallcrafters S-29 Sky Traveler or S-39 Sky Ranger. Will accept cash. Donald E. Griffith, 51 Ridge road, Quonset Point, R. I.

FOR SALE—Jensen high-f. 8" p.m. speaker PM8CT, \$6; Cinacograph heavy 8" p.m. speaker, \$6; 5" RCA speaker, \$2, and 5" p.m. speaker, \$1.50. Also used 57, 58, 2A5, 2A4, 35, 80, and 5Y3 tubes; used power transformer 2 1/2 w. fil., 5v rectifier, and 300-0-300 at 70 mil windings and used crystal pickup. Herbert Jacobowitz, 1412 Franklin ave., Bronx 56, N. Y.

FOR SALE—Rider's #3 and #6 manuals, \$6 ea. B. & L. Radio, 112 Park st., N. Attleboro, Mass.

FOR SALE—Thoradson 60-watt booster amplifier with tubes suitable for any low power amplifier; also Audak magnetic pickup. Ed. Monahan, Shawomet, R. I.

SELL OR TRADE—Electro-dynamic speaker 6v field and two 6F6, one 6B5 and one 59 tubes. Want schematic of 1- and 2-tube short-wave recorder, 20m to 30,000 kc.; also need line cord resistance elements. Wierick Radio Service, Box 263, Warren, Mo.

WANTED—Sig. generator, Rider's chanalyst, scope or other similar testing eqpt.

L. C. Phelps, Sheridan Park, Bremerton, Wash.

FOR SALE—Rider's 1 to 11 new; RCP #312 tube tester; Electronic multi-tester R.C.P. #661; 800 1/2 & 1 & 2 watt resistors above, all new; 350 condenser filters & by passes assorted, some used in testing, and 60 tubes used only in testing. \$250 for lot. August Palermo, 223 S. Winebidde ave., Pittsburgh 24, Pa.

FOR SALE—Coyne books; Trouble Shooting Manual; Electricians Handbook; Electronics; 150 Shop Prints; Vols. 1, 2 & 3 of Electrical and Radio Reference set; Electrical and Radio Dictionary. All new. \$25. Woodrow Lewis, Bolinger, Ala.

WANTED—Rider's Manuals 6 to 14 inclusive—any or all. Ray Butts, 408 Thirty-fifth st., Cairo, Ill.

SELL OR TRADE—Complete radio shop and equipment. Write for full details. Warren Wigner, 1220 Fairview st., Fort Wayne 4, Ind.

FOR SALE—Hickok T-53P dynamic mutual conductance tube tester with built-in roll chart. Almost new. The Radio Laboratory, 912 W. 151st st., East Chicago, Ind.

WANTED—Inoperative G-E auto radio C-61 complete with tuning mechanism. William E. Mallory, 360 S. 40th st., Apt. 2A, Richmond, Calif.

WILL TRADE—Back issues Radio Craft; 1—Modern Servicing; 3 vol. Radio for Millions and Radio Electronic Manual. Want used phonograph. Henry Skoritowski, 828 Fig st., Scranton 5, Pa.

FOR SALE—Franklin D-33-A set analyzer; combination V-O-M, analyzer and tube checker, a-c operated with instructions \$20, or what have you? Need good signal generator. C. E. Brickley, Farm-land, Ind.

WILL TRADE—New 12B8GT tube for new 25B8 or 25B8GT and one 70L7 or 70L7GT. Both tubes must be new. S. Rosenwasser, 219 E. Jefferson, Mishawaka, Ind.

FOR SALE—Professional Federal recorder, dual-speed, 112 lines per inch, 12" weighted turntable, synchronous motor rim drive, overhead cutting mechanism. Built-in amplifier & T.R.F. tuner, with in-

dividual control of 2 mikes, 1 phono, 1 radio. Accessories include SR80 amperite mike & floor stand, 7JH amperite chest mike, 50" mike extension cord, speaker extension core, cutting needles. Don Ruskjer, 166 Lathrop ave., Battle Creek, Mich.

FOR SALE—01A, 19, 1G5, 22, 24A, 27, 30, 32, 34, 35, 40, 42, 47, 48, 58, 6C6, 6F6, 6K7GT/G, 6Q7G, 6SK7, 6U7, 76, 77, 70, 80, 12K7GT/G, 12Q7, 25L6, 1N5, 12J7, 35L6, 50L6 and other tubes. Write for complete list. Rayford's Radio Clinic, Brentford, S. Dak.

WILL TRADE—Two Leeds & Northrup, zero center galvanometers, with breakage guarantee; also 2-tube variable code practice oscillator in cabinet with key and buzzer attachment. Arthur Ginsberg, 1454 Grand Concourse, Bronx 57, New York, N. Y.

FOR SALE—Supreme 89 deluxe combination V-O-M and tube tester with schematic and tube test chart; also Readrite tube tester #430 with chart, \$40 for both. George Miller, 94 Holland ave., Elmont, Long Island, New York.

FOR SALE—New tubes, including 50L6, 35L6, 35A5, 35Z5, 12SA7, 1A7, 1A6, 75, etc. Write for details. Discounts to servicemen. Ben W. Mueller, North Tona-wanda, N. Y.

FOR SALE OR TRADE—P.A. amplifier tubes and transmitter eqpt. Want recording eqpt. and Abbott DK-2 or DK-3 transceiver. R. F. Peyton, 3306 Arch st., Little Rock, Ark.

FOR SALE—RCA oscillator, vibrator transformer; 5 adaptors, speaker cone; 80 new, in carton tubes; Official Radio Service, Supreme manual 1940 and 1941 Motorola manual, \$115. Stanley W. Dieroff, 3090 S. Custer road, Monroe, Mich.

WANTED—Green Flyer phono motor 115F, 60 cycle with 12" turntable or similar. Have for sale or trade, Silvertone automatic record changer with Astatic crystal pick-up. R. C. Gleiforst, 38 Howson st., Vallejo, Calif.

FOR SALE—RCA tube tester #156-B; Superior dynameter; Superior signal tracer CA-10; Superior signal generator #850 and set six Supreme circuit manuals. All A-1 condition with instructions and test leads. \$120. Gene's Electric Service, 108 Newhard st., Carey, Ohio.

FOR SALE—Supreme diagnetometer #585; Supreme sig. gen. #580; Monarch sig. gen. #12; Triplett tube tester #1213; 3" oscilloscope. H. D. Laurence, 3025 Elliza-beth st., Denver 5, Colo.

FOR SALE—Philco and Sprague resistors and condensers; also other radio parts and eqpt. Henry A. Czarkowski, 2620 Ash st., Phila., Bridesburg, Pa.

FOR SALE OR TRADE—Philco 5-tube a-c rec. table model 37-62, \$40; Freed-Eisemann 8-tube a-c broadcast and short wave, \$35; a-c-dc converter generator, \$20; and Majestic console 8-tube a-c receiver, \$45. Want precision VTVM or RCA junior voltohmmyst. Frnklin C. J. Slay, 243 West 107 st., New York 25, N. Y.

FOR SALE—Hallcrafters SX25, \$75 and 1000v 5amps d-c generator and 115v exciter generator. George A. Carroll, 70 Capistrano ave., San Francisco 12, Calif.

URGENTLY NEEDED—A-117Z4GT tube for soldier's radio. Paul W. Zoellner, 930 Adams st., LaCrosse, Wis.

FOR SALE—Eight radio and electronic books, 10% off. Write for list. Kenneth A. Stohl, 25 Wanamassa Pt. Rd., Wanamassa, N. J.

FOR SALE—Meissner 9-1040 analyst; RCA 195 voltohmmyst; Precision P-844 VOM; G-E TC-3 tube tester; Weston 772 VOM; Solar CE-1-60; Aerovox 75; Solar BQC, and C-D BF-50 cond. analyzers; RCP 492 VOM; Meissner 10-1199 6-tube kit; Precision 912-P tube tester and Weston 687 VOM. All new or in A-1 condition. Alexander A. Mogull, 300 Adams ave., West Hempstead, N. Y.

WANTED—Tube tester and multimeter. J. Dowdell, 3474 Milverton road, Cleveland 20, Ohio.

FOR SALE—Webster phono-record changer new, and rim-driven phono motor with 9" turntable. Reasonable. William Blaha, 2233 S. 59th ave., Cicero, Ill.

WANTED—Complete set Rider manuals; sig. gen. and tubes of 12, 25, 35 and 50v types. G. L. Conroy, Route 8, Box 231, Richmond, Va.

FOR SALE—Back-issues radio magazines. Complete volumes only. Write for list. Carl H. Fastie, Denison, Iowa.

SELL OR TRADE—New capacity bridge; Readrite 710A analyzer; late model tube checker; line cord resistors; condensers; 5 new Delco car radio vibrators; mounting kits for car radio and other misc. items. Earl Triplett, Route 2, Bizby, Okla.

WANTED—New 4-pronged plug-in coils for short-wave and broadcast bands. John Flaherty, 47 Mountain ave., Norwood, Mass.

FOR SALE—Three 35Z5; 2 ea. 50L6 and 6K7; one 25L6 used tubes, \$3. Bill Buehrle, Jr., 120 Apple Place, Ferguson 21, Mo.

WANTED—Used tube tester and V-O-M. Write details. J. N. Gibson, 110B, Concord st., North Charleston, S. C.

FOR SALE—New Starrett universal dial test indicator complete and Wollensak 250 power microscope. George Baum, Hagerman, New Mexico.

FOR SALE—Instruograph with 10 rolls of tape; oscillation and Pilot key. All like new, \$25. Eber E. Cline, 915 Sheridan road, Chicago 13, Ill.

FOR SALE—New tubes 20% off list, eight 6H6; six 6J5; five 6B7; four 6K6; four 6K8; four 6B37; fifteen 6BK7; four 78, and four 27. Also inverter 32v to 110, 100-watt capacity. Siefert Motor & Impl. Co., Utica, Minn.

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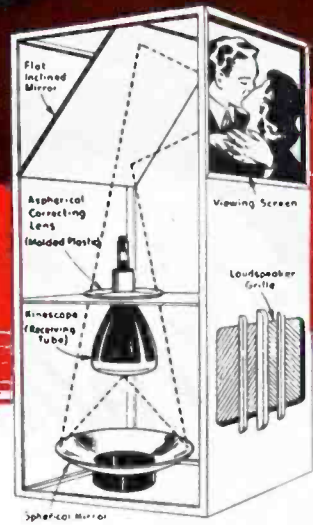
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HIGH RESOLUTION: Improved gun design provides high resolution.

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ERL

Division of **GLOBE-UNION INC.**, Milwaukee

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from Jensen



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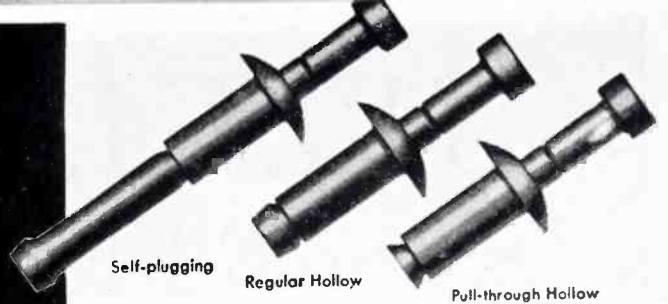
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SYLVANIA NEWS

RADIO SERVICE EDITION

OCTOBER Published by SYLVANIA ELECTRIC PRODUCTS INC., Emporium, Pa. 1945

PROFIT PERIOD FAST APPROACHING AS WHEELS OF RADIO INDUSTRY BEGIN TO TURN FOR PEACE

60 MILLION TUBES TO BE NEEDED, ESTIMATE SHOWS

Radio Servicemen May Double Prewar Business

In 1941, about 34 million replacement tubes were sold. In contrast to this is the recent authoritative report (from one of America's leading research organizations) that no fewer than 60 million replacement tubes will be required to handle the expanding radio market. This means that the Dealer and Serviceman can look forward to about doubling their prewar tube replacement business.

In addition to this, is the widespread acceptance of record players, FM and television. It has been estimated that within a few short years, approximately 75 million home radios plus 25 million auto sets will be sold.

These facts not only back up the estimated tube replacement sales, but indicate the extent to which the demand for electrical and mechanical parts will be boosted. As far as the radio tube market is concerned, the serviceman *knows* he can depend on the high quality standards and large production facilities of Sylvania Electric.

DID YOU KNOW...

Ninety per cent of Sylvania's radio tube production went toward hastening the day of total victory. (Each B-29 used 700 radio tubes!)

Radio Servicemen Assured Of Receiving Highest Quality Products To Meet Rising Demand

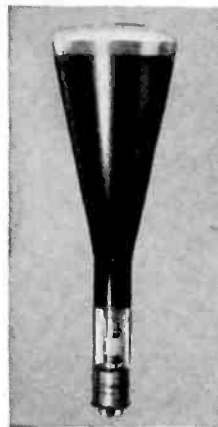
As the period of reconversion gradually takes active form and spreads over the nation, the radio industry can look forward to one of the most profitable spans in its history. Millions are waiting for radio sets of improved design. Meanwhile millions of sets are in need of repairs.

This peace-time expansion means a *profit* period for radio servicemen everywhere. Backed up by Sylvania's more than 40 years' research and experience in manufacturing, the radio serviceman can with confidence look forward to the expansion of his business. Note this list:

Television: experience in design and the production of untold thousands of Sylvania Cathode Ray Tubes for war requirements have contributed greatly to peace-time applications.

High frequency sets (FM, television): the Sylvania Lock-In Tube is so electrically and mechanically perfect in construction that it can handle ultra-high frequencies with ease.

Radio: manufacture and distribution of the famous high quality Sylvania lock-in "Glass" and miniature tubes will continue to satisfy the exacting circuit requirements



CATHODE RAY TUBES



LOCK-IN RADIO TUBES

of modern radio receivers.

Now that the go-ahead signal has been given to the radio industry, servicemen know they can depend on the Sylvania Electric wide-scale production facilities that have served our government so well.



"GLASS" RADIO TUBES

SYLVANIA ELECTRIC

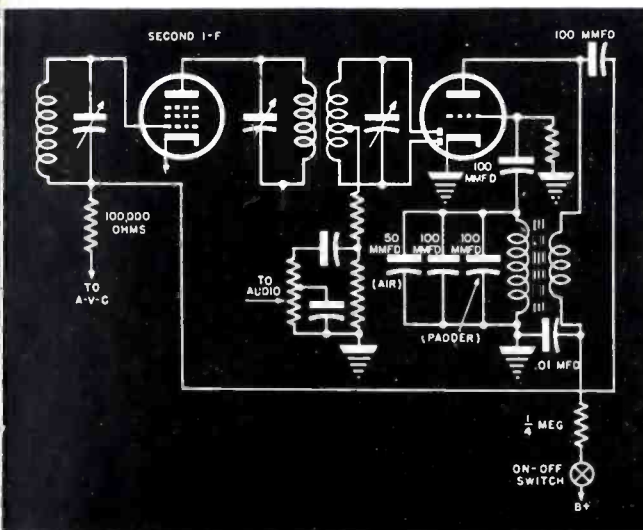
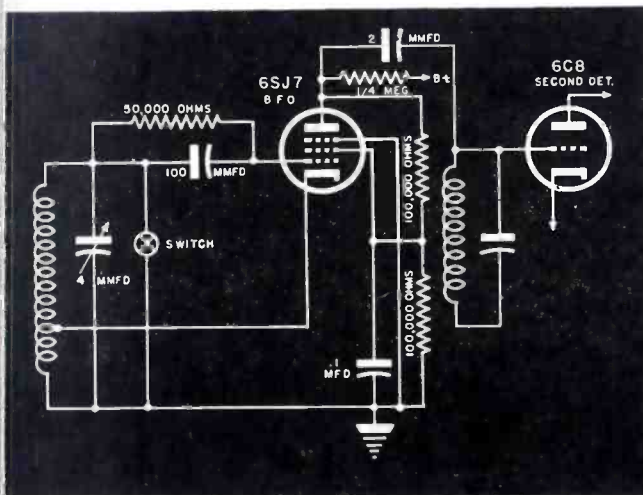
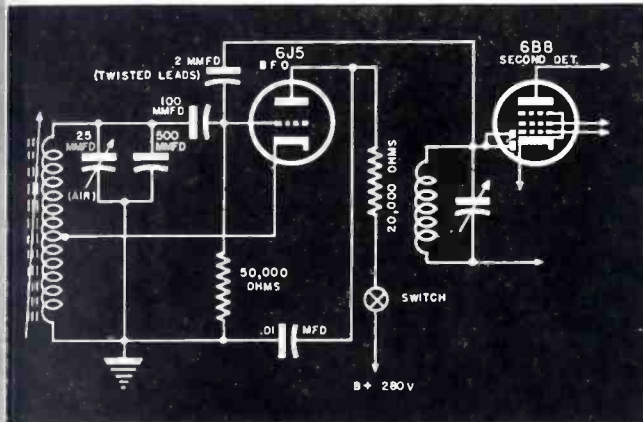
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COMMUNICATIONS RECEIVERS'

BEAT-FREQUENCY OSCILLATORS

by THOMAS T. DONALD



Figs. 1 (above), 2 (center), and 3 (below). Fig. 1 shows the b-f-o circuit of the Hallicrafters SX28. This circuit uses a 6J5 in a Hartley oscillator. The 25-mmfd capacitor, used for adjusting the beat note, is adjusted by a panel control. In Fig. 2 appears the b-f-o circuit of the National NHU. Here a pentode is used in a Hartley oscillator. To cut out the b-f-o, a shorting switch is used in shunt with the oscillator coil. Fig. 3 illustrates the b-f-o circuit of the RME 41-43. A duodiode-triode is used as a combination second detector and triode b-f-o oscillator. The b-f-o signal is fed back to the low side of the input of the second i-f.

THE extensive use of communications type receivers by the military during the war has alerted many to the versatility of this equipment. As a result we shall undoubtedly see quite a sales increase of these receivers. Service Men will therefore find it increasingly important to become acquainted with all of the models produced and being made now. In this and subsequent papers analyses of all types will be offered.

Communications type receivers are basically the same as home types, with such added features as b-f-o, a-n-l, crystal filters, S meters, variable i-f, separate r-f and audio volume controls, antenna tuning systems, and band-spread tuning. In addition, circuit values are kept to very close tolerances, and alignment is more complex.

One feature common to all communications receivers is the *beat-frequency oscillator*. A b-f-o is a tunable oscillator which generates a local signal within audio range of the frequency of the receiver's intermediate frequency. By mixing the b-f-o with any signal coming through the i-f amplifier, an audible tone is produced in the speaker. It is used for the reception of coded signals which are merely r-f carriers, interrupted in coded

(Continued on page 48)

PHOTOELECTRIC

by WILLARD MOODY

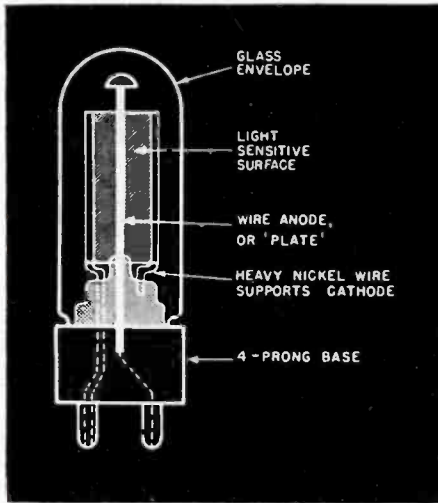


Fig. 1. A typical photoemissive cell. Light falling on the light-sensitive surface increases the emission and consequently the current flow. This variation in current flow may be used for the control of either visual or aural devices.

THERE are four main types of photoelectric cells . . . photoemissive, photoconductive, photovoltaic and electron-multiplier. All of them respond to light; more specifically they change light variations into electric variations.

Photoemissive Types

The photoemissive cell is sometimes identified as a photocell, or phototube. They depend upon electron emission for operation. That is, when light

shines on the cell, electrons are emitted from the cathode and move to the anode or plate which is at a positive potential with respect to the cathode. This is similar to the action that takes place in the usual vacuum tube. In Fig. 1 we have a drawing of a typical photoemissive cell. As the light intensity decreases, the emission is decreased and less current flows in the tube. In effect, the tube is a variable resistance, whose resistance decreases with an increase in light.

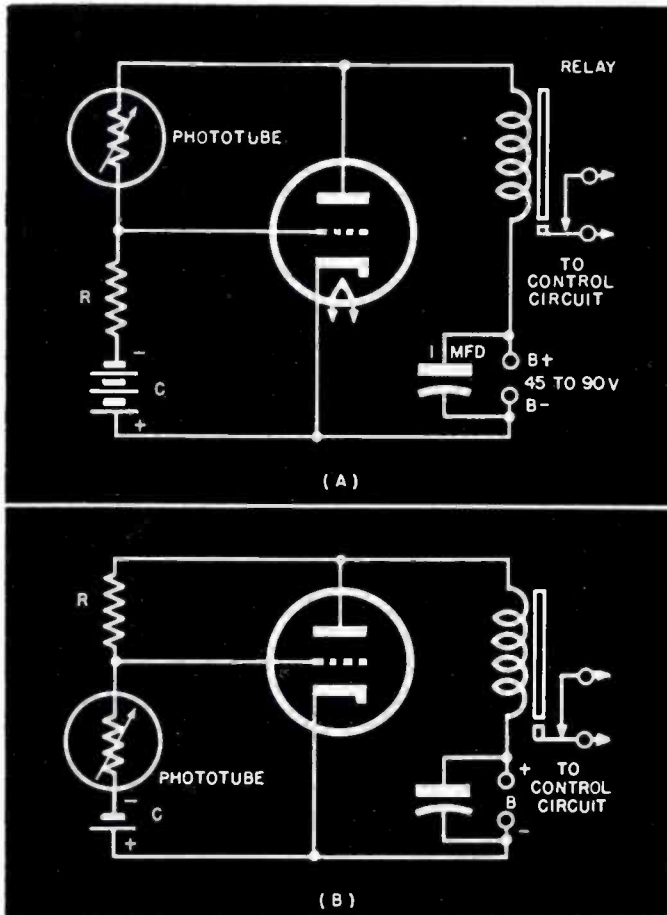
The cathode is a semi-circular cyl-

inder of oxidized silver, or some other suitable metal, supported by stiff wire leads of nickel. The surface of the cathode facing the plate is covered with a thin film made of caesium oxide, sodium, potassium, or lithium, or other light sensitive chemical compound. The plate is a plain nickel rod or wire placed in the center of the cylinder.

The glass envelope is soda-lime glass for many inexpensive cells, while higher priced cells may use pyrex or fused quartz, which have lower light losses and permit more ultra-violet light to pass through. Lead glass is not used, because it is a poor transmitter of light and reacts chemically in an undesirable way with the cathode materials, causing envelope discoloration.

The plate is the smallest electrode so that it won't cast a shadow on the cathode and reduce cell efficiency. Two types of cells are used; one is a high vacuum, the other gas filled. Using gas, increased output current for a given amount of light is obtained through gas ionization. The gas also reduces the effects of space charge.

Basic Control Circuit



Figs. 2 a and b. Here we have two electronic applications of the phototube. In the circuit in a light falling on the phototube increases the plate current, and closes the relay in the plate circuit. In b, we have a circuit performing the reverse action. When the light on the phototube is interrupted the plate current increases and closes the relay.

In Fig. 2 appears a typical application of a phototube, either high vacuum or gas filled. With no light on the cell, its resistance is high and the grid potential is negative. When light shines on the cell, the resistance drops and the grid of the control tube becomes less negative. The cell resistance is in series with R , the C battery, and the relay and B supply. The effect of the plate voltage on the grid becomes greater when the cell resistance is decreased. The operating conditions are usually set so that the grid is always negative, but is simply made less negative when light hits the cell. The tube plate current, which passes through the relay coil, thus increases. The result is a stronger magnetomotive force in the relay magnetic circuit, which attracts the armature, closing the contacts to the control circuit.

The reverse action can be obtained by placing the cell in the position now occupied by R , and placing R in the cell position, Fig. 2b. The two elements then form a voltage divider in the circuit. When no light shines on the cell, its resistance is high. This resistance is in series with the resistor, which is between plate and grid, using

C E L L S

versed arrangement. Accordingly, the grid becomes less negative and the plate current rises, causing the relay to close. When light hits the cell, the resistance drops, and less voltage is developed across the cell resistance. The grid, therefore, is highly negative, and the plate current correspondingly small, so that the relay is open. In this case, light failure, caused by the interruption of the beam would increase cell resistance, reduce the grid bias, increase plate current and thereby cause the control circuit to swing into action and sound the alarm.

Photoconductive Cells

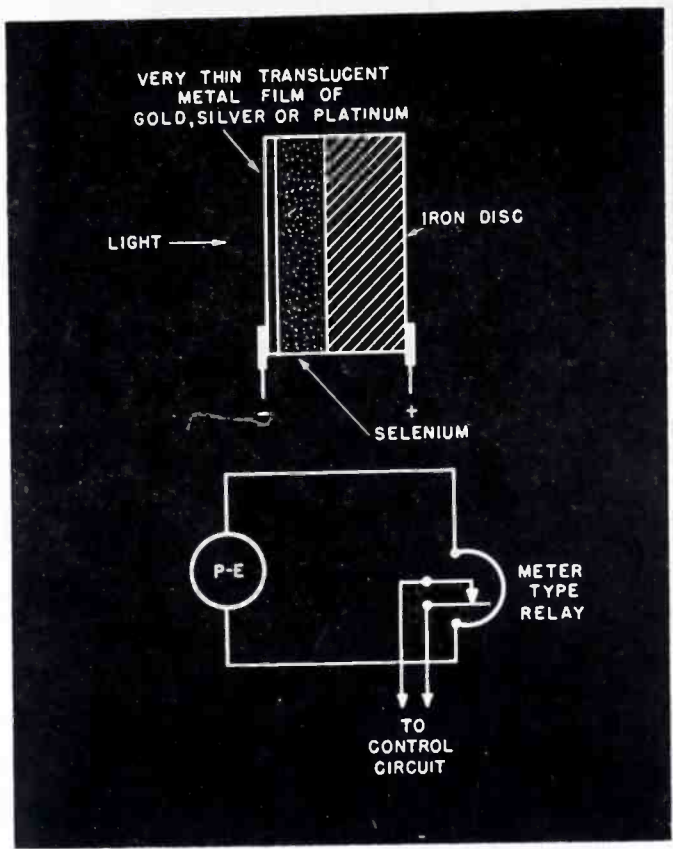
In the photoemissive cell there was electron emission. In the photoconductive variety, we have a variation in cell resistance, but no emission. Selenium cells are the most common types and consist basically of two electrodes having between them a deposit of selenium. The electrodes themselves may be of copper, iron, nickel, or other suitable conducting material. The counting block may be slate, mica, bakelite, or equivalent insulating material. Most selenium cells have a high sensitivity to red and infra-red (invisible) light. A typical cell may have a resistance of about 10 megohms dark and 2 megohms for an illumination of 1 foot candles. Since its action is similar to the photoemissive type it may be substituted, or used for similar application such as that shown in Fig. 2.

The cell must be kept cool and dry and not too much current can be passed through it; about 4 ma should be the maximum.

Photovoltaic Cells

The photovoltaic cell generates a voltage, while the previous types discussed developed electron emission and changed resistance. The fundamental construction of a photovoltaic type is shown in Fig. 3. The iron disc may be only $\frac{1}{8}$ " thick. It forms the positive terminal of the cell. The light causes electrons to be forced to the surface of the sensitized layer, to be collected by a thin translucent film which serves as the negative terminal. The loss of electrons in the metal disc makes it positive. The voltage difference between the terminals is used for control of a super-sensitive meter type relay, as shown in the lower part of the figure. When light shines on the cell, the control voltage is de-

Fig. 3. A cross-sectional view of a typical voltaic cell; a circuit application appears below. Light falling on the selenium through the thin translucent metal film generates a voltage, which may be used in control circuits.



veloped. The fact that the cell uses selenium does not mean it is a variable resistance type. The sensitive relay may, in turn, control a heavier relay which operates a control circuit to ring an alarm or perform some other operation. In one type, an output voltage of .15 volt for an illumination of 1 lumen is obtained. This is for a no-load condition. However, cells of this

type give a linear response when used in low resistance circuits. Thus, the resistance in Fig. 3 might be quite low in value to give a response directly proportional to the light, as in some photoelectric light-intensity meters. By putting cells in parallel, greater output current can be obtained. Photovoltaic cells are low-impedance
(Continued on page 49)

Fig. 4. An electron multiplier cell. This tube has not been used too widely, but may be used more extensively in the near future. The tube uses the principle of secondary emission for amplification, each successive plate amplifying from the previous one. High plate potentials are used, since each plate is at a higher voltage level than the previous one.

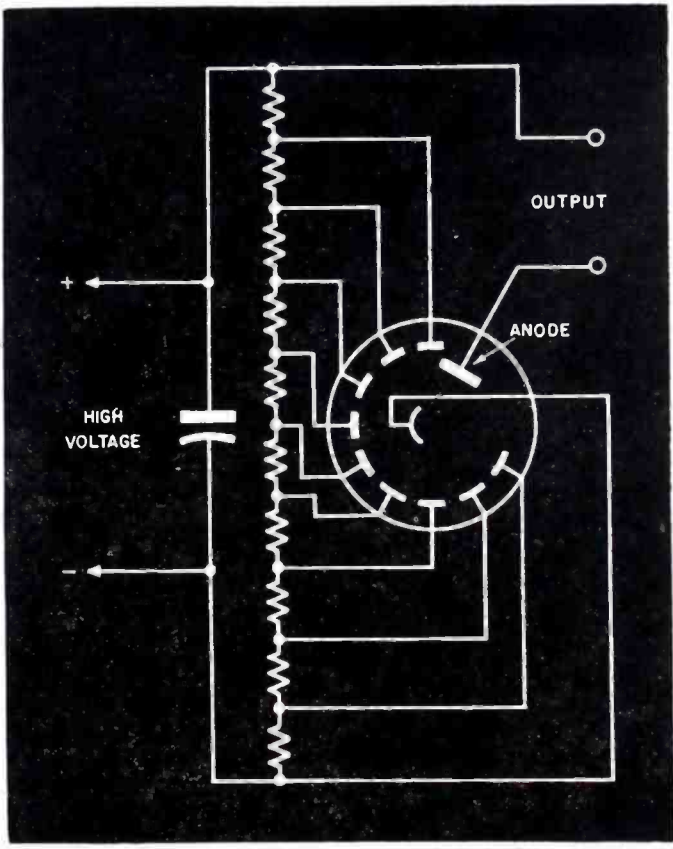


Fig. 1. Circuit of the electron-eye indicator. At zero bias the eye is open, closing as the bias is increased negatively.

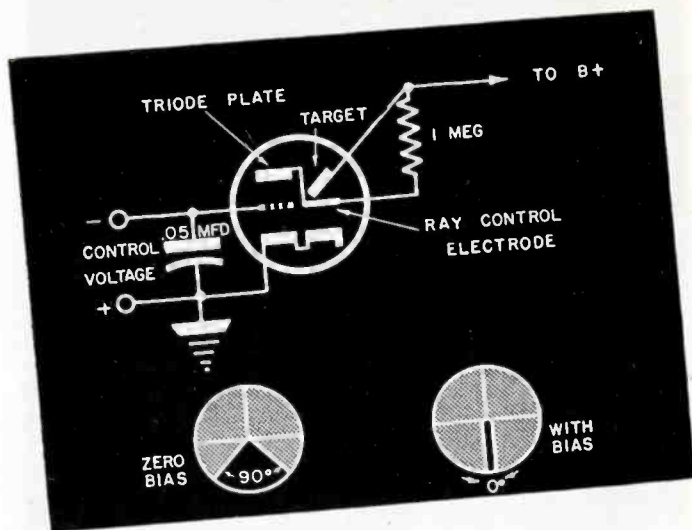
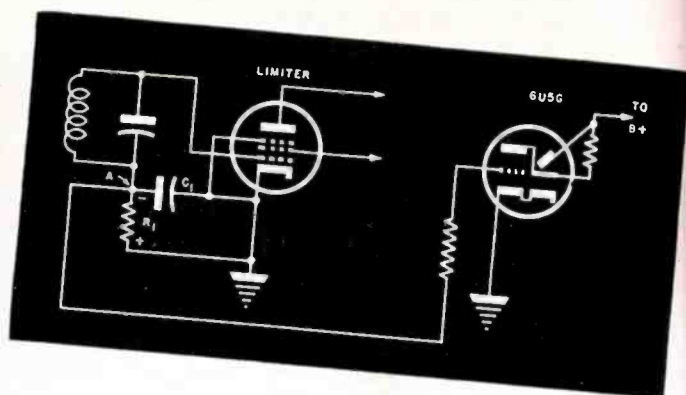


Fig. 3. Magic eye as used in an f-m receiver. The actuating voltage for the eye is supplied by the limiter stage. As the center frequency of the signal is approached the voltage across R_1 increases, biases the eye grid, and closes the eye.



F - M TUNING INDICATORS

ALL f-m receivers require some form of tuning indicator for proper reception of f-m signals. Two types are in general use; a meter to indicate that the station signal is properly tuned in, and a magic-eye tube such as the 6U5G for the same purpose.

The operation of a meter type indicator is quite simple to understand, since it involves a direct reading of some voltage or current, whose amplitude is a function of the correctness of alignment of the signal. The electron ray, or magic-eye tube serves the same purpose, electronically.

Magic Eye Tube Circuit

Fig. 1 shows a circuit diagram of a typical magic eye tube. It consists of a triode amplifier, and a cathode-ray indicator. In action, a variation in grid voltage changes the plate current of the triode portion of the tube. Since the plate is connected to the ray-control electrode, and since both are in series with the B+ through a 1-megohm resistor, the voltage drop across this resistor will also vary. The target is directly connected to the B+, so that variations in the triode's grid voltage will increase or decrease the voltage difference between the target and the ray-control electrode.

The fluorescence area of the target is a function of this voltage difference; the shadow angle decreases as the po-

by J. GEORGE STEWART

tential difference decreases. Or, stated another way, the shadow angle decreases with an increase in grid bias. An increase in bias will close the eye, and conversely, a bias decrease will open it.

Tube Types

In Fig. 2 appears a list of electron-ray tubes and their characteristics. The twin-indicator types have no internal triodes, but are operated with external amplifiers, in essentially the same circuit as that shown in Fig. 1. They are usually used where one indicator is for weak signals and the other for strong signals.

When used as a tuning indicator, the electron-ray tube is coupled to the

receiver at some point where a d-c voltage variation occurs upon tuning. Since the grid of the tube draws no current, it can be used at any point where a voltage change occurs, with no appreciable loading effect. The usual point of connection is the avc system in a-m receivers. However, due to the broad response of f-m receivers, this presents a problem, since the function of the tuning indicator is to indicate center frequency of the received signal.

F-M Eye Circuits

A popular hookup for f-m receivers is shown in Fig. 3. Here, the limiter stage is used to furnish the voltage for tuning indication. As the center frequency of the received signal is approached, the voltage across R_1 increases. This voltage is the result of the grid of the tube drawing current on positive pulses of the input signal. The action in the grid circuit of the limiter may be likened to that of the diode detector. Condenser C_1 acts as a filter condenser, smoothing out the resultant voltage. The polarity of the developed voltage is such that the ground end of the resistor is positive with relation to point A. Therefore, any increase in the developed grid voltage will bias the grid of the 6U5G more negative, causing the eye to close.

Another system is shown in Fig. 4. Here, the electron-ray tube is con-

Type	Bias for 0°	Plate Voltage	Plate Resistor (megohms)	Remarks
6AB5/6N5	-15.5v	135	1	Used in a-c/d-c models
6U5/6G5	-22 v	250	1	Remote cut-off type; increases sensitivity to weak signals
6E5	-7.5v	250	1	
6AD6G	150	..	Twin type, -75 v for 0°, -8 v for 90° on ray-control electrode
6AF6G	250	..	Twin type, -160 v for 0°, -0 v for 90° on ray-control electrode

Fig. 2. Electron-ray tube types and their applications.

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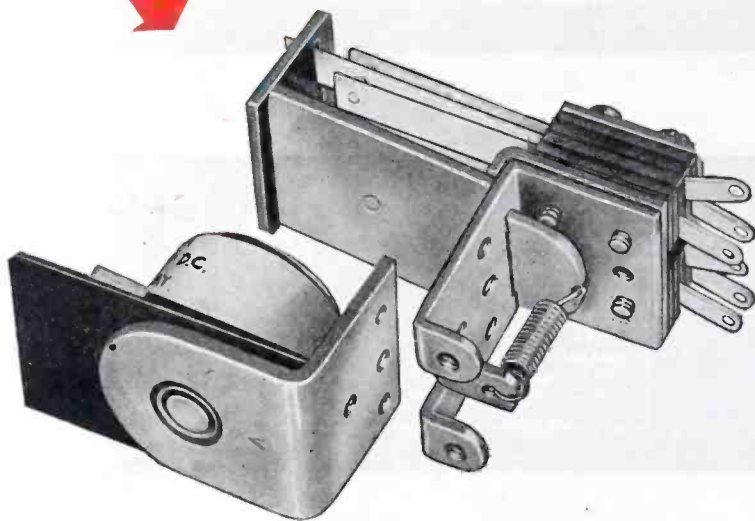
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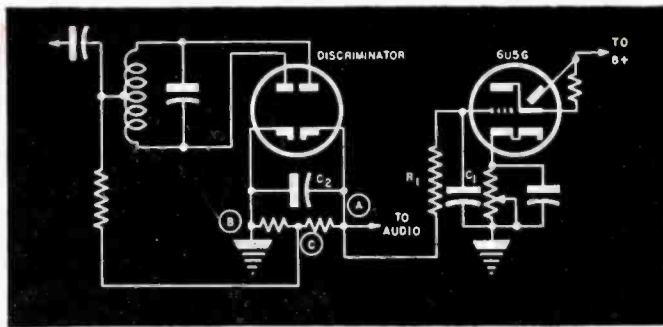


Fig. 4. A pentode magic-eye circuit. The voltage developed by the discriminator across points A, B, and C is used to actuate the eye.

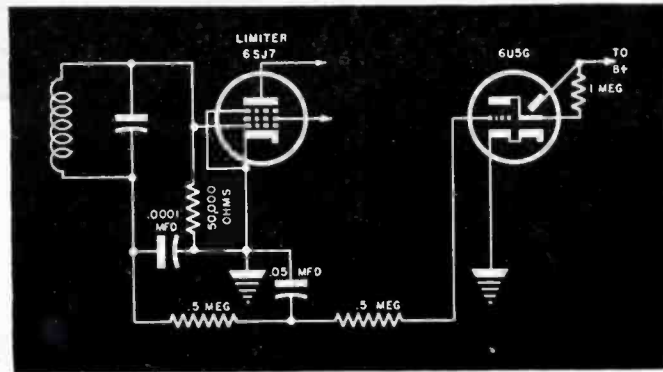
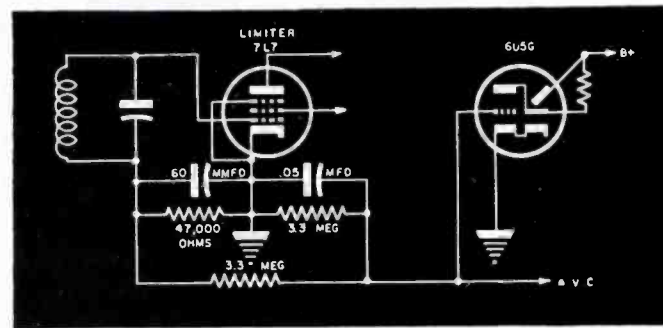
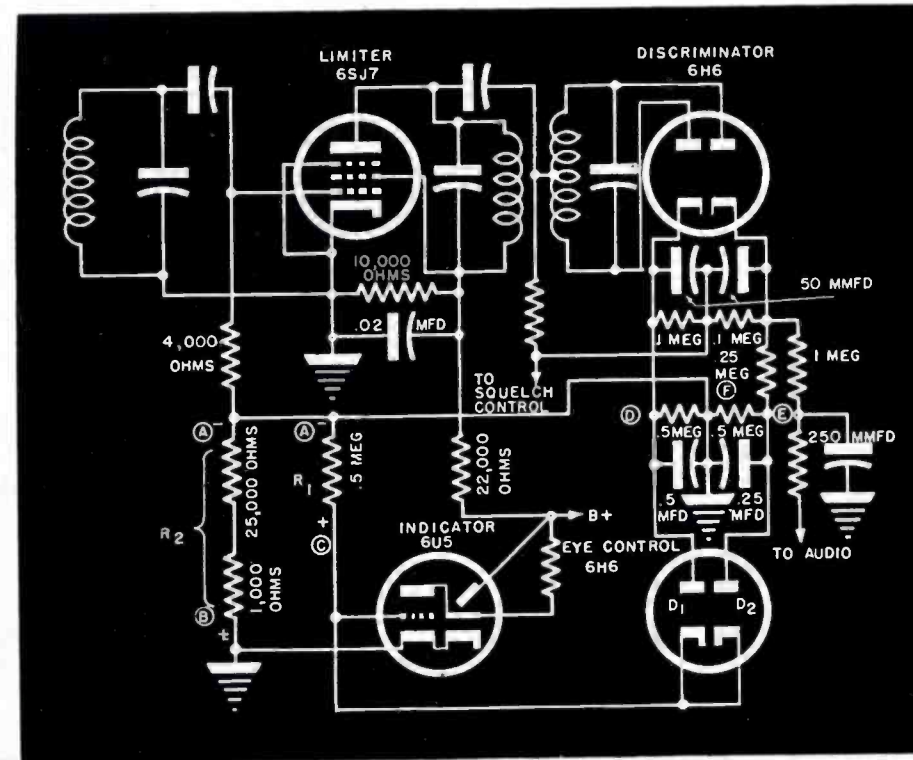


Fig. 5. Indicator system used in the Freed model 57-71. Since the discriminator is not used to supply the avc voltage, the action of the eye is sharpened.



Figs. 6 (left) and 7 (below). Fig. 6 shows the indicator circuit of the a-c/d-c Emerson FM 460. Fig. 7 is the magic-eye circuit of the Espey 2170. A diode-eye control tube is used to increase the efficiency of the tuning indicator. (See page 49 for complete circuit data.)



nected to the discriminator cathode which is above ground. The 6U5G is cathode biased, so that the eye remains closed when no signal is applied.

Discriminator Behavior

When no signal is being received no voltage exists across points A, B, and C. As a signal is approached point A becomes positive with relation to point B. When the receiver is tuned to the center frequency, the voltage between points A and C is equal to that between B and C. However, these voltages are opposite in polarity so that the net voltage between A and B is zero. As the dial passes the center frequency, B becomes positive with reference to A. The highest voltage difference is registered 75 kc away from the center frequency.

This voltage variation influences the action of the tuning indicator in the following manner. As the signal is approached, the positive voltage at point A cancels the self bias on the grid of the 6U5G. The eye, which is normally closed, therefore opens. As the center frequency is approached, the voltage between points A and B reduces to zero, and the eye returns to the closed position, due to the cathode bias voltage. As the center frequency of the signal is passed, point A becomes negative with respect to point B. This negative voltage, added to the cathode-bias voltage, causes the two images of the eye to overlap. Therefore, correct tuning is indicated by the point where the two images meet, just before they overlap.

Most f-m receivers use either the limiter- or discriminator-actuated indicator systems, or some combination of the two. Figs. 5 to 7 show some typical systems.

Freed 57-71

Fig. 5 shows the magic eye circuit used in the Freed model 57-71; note its similarity to Fig. 3. In this circuit the limiter is used to supply the indicator tube only, and is not used for a-v-c. This tends to sharpen the response of the 6U5G, since there is no signal-compensating voltage to reduce r-f gain.

Emerson FM 460

In Fig. 6 we have a similar system used in an a-c/d-c f-m receiver, the Emerson FM 460. Because of the reduced plate voltage available in a-c/d-c sets the 6U5G opens and closes at reduced grid voltages. This accounts for the divider network in the grid return of the 7L7, which reduces the

(Continued on page 49)

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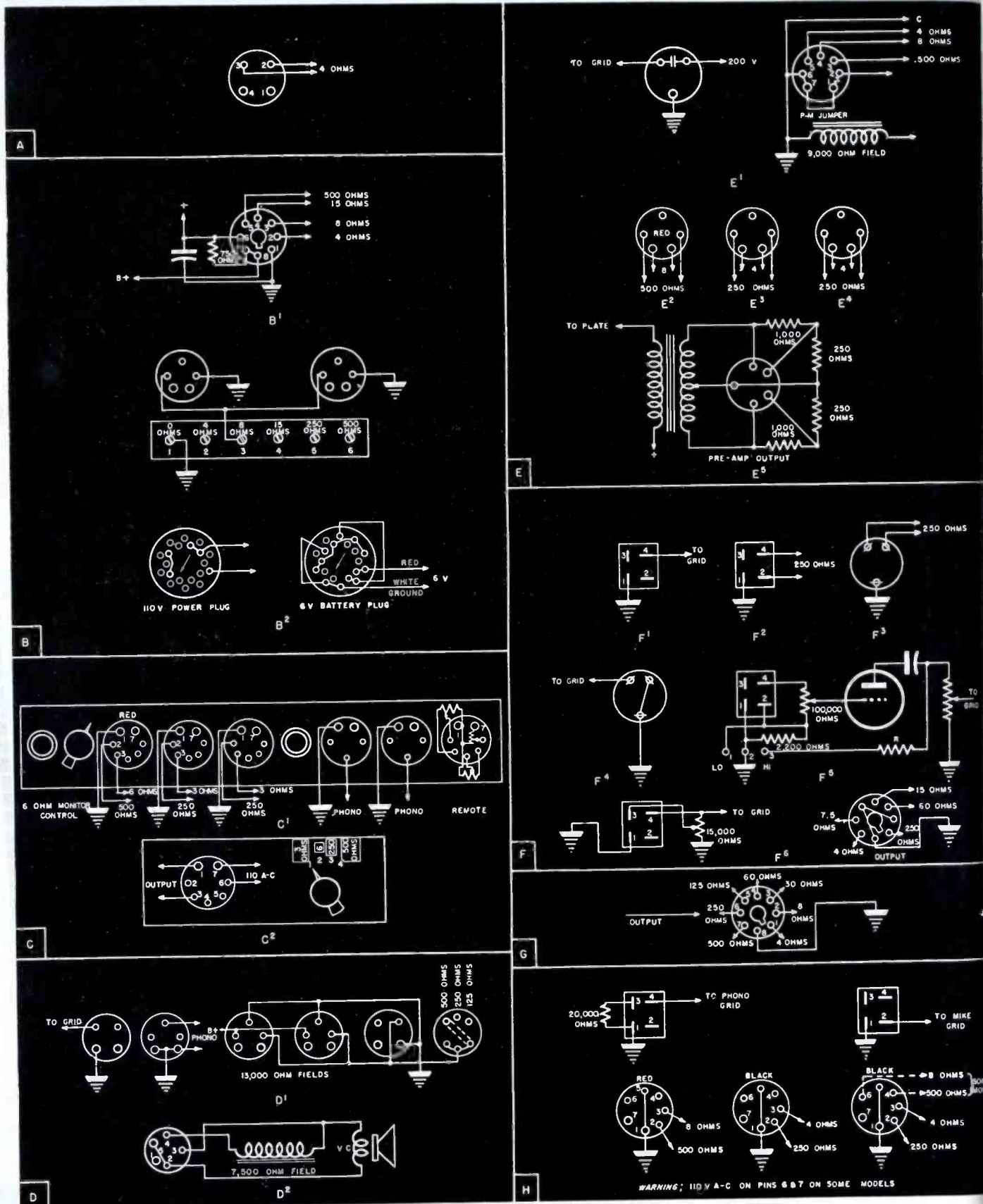
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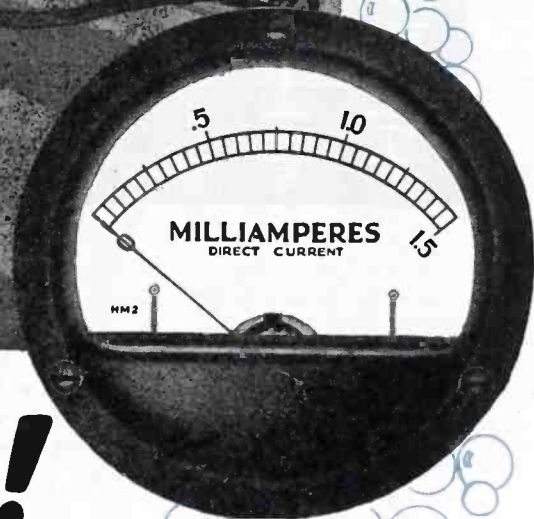
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CONNECTIONS FOR UNLABELED AMPLIFIER TERMINALS



Reference chart for unmarked amplifier connections; all views from outside. A, Audiograph AMR 15C. B¹, Bogen E-8. B², Bogen E-620. C¹, Erwood 35-watt deluxe. C², Erwood models 412 and 4120 with speaker plugs as above. D¹, Magnavox 3023. D², Magnavox 922. E¹, Operadio 108 (right 835 (left). E², Operadio 162. E³, Operadio 1010. E⁴, Operadio 1025. B³, Operadio 950 pre-amplifier output. F¹, RCA 12756. F², 12212,14,20. F³, RCA 12214,39. F⁴, RCA 12224,30,57. F⁵, RCA 12204,9. F⁶, RCA 12754 mobile. G, Stromberg-Carlson. H, Webster-Rauland. (Courtesy P. Sickie Radio Supply Co. . . . See page 51 for further data.)

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Production vacuum checking of Marion Glass-to-Metal Hermetically Sealed Electrical Indicating Instruments is no haphazard operation . . . After sealing in our dehydrating rooms, the instruments are submerged in glass jars which are partially filled with alcohol. A vacuum of 25 inches is drawn in accordance with newest JAN-1-6 specifications. During the test we watch for air bubbles — no bubble means no trouble. Spot checks for a period of four hours are made in a 29 inch vacuum.

The testing apparatus, illustrated above, is a Marion development, and demonstrates our sincerity of purpose in producing hermetically sealed instruments. We take nothing for granted — we neither suppose nor assume. Because imperfectly sealed instruments entrap condensation, we make certain that every hermetic instrument bearing our name is — perfectly sealed.

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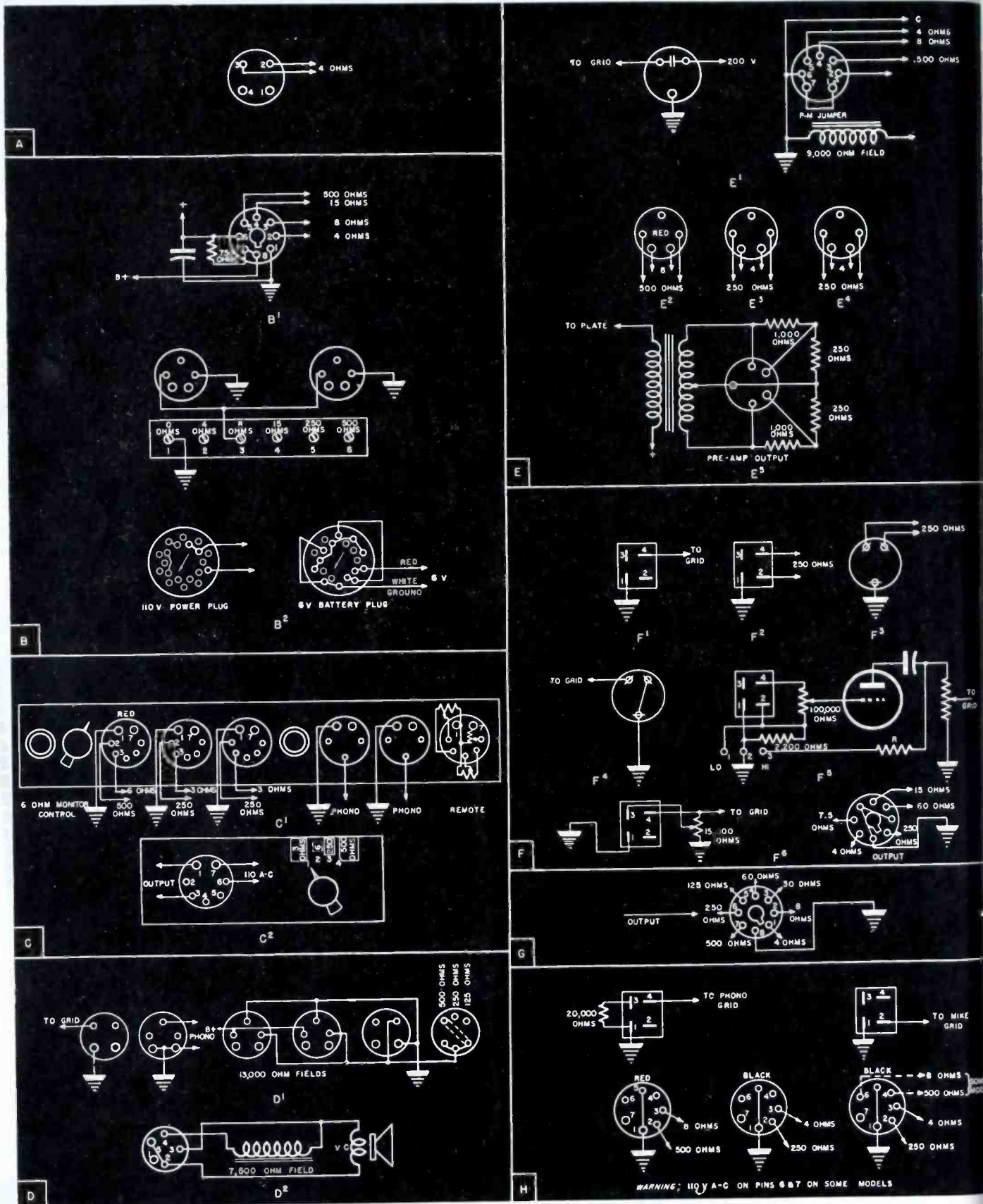
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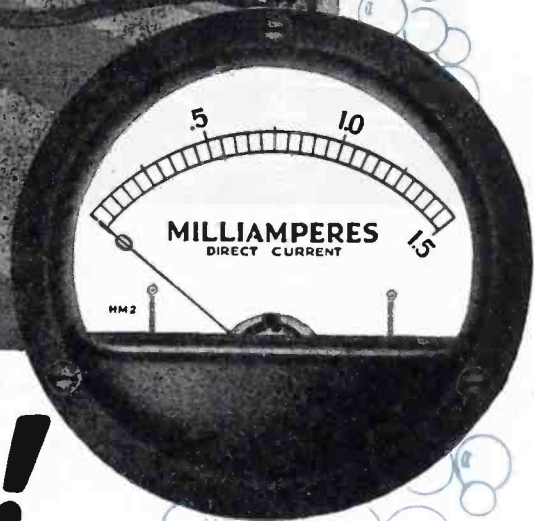
NEW YORK, N. Y.

CONNECTIONS FOR UNLABELED AMPLIFIER TERMINALS



Reference chart for unmarked amplifier connections; all views from outside. A, Audiograph AMR 15C. B¹, Bogen E-8. B², Bogen E-620. C¹, Erwood 35-watt deluxe. C², Erwood models 412 and 4120 with speaker plugs as above. D¹, Magnavox 3023. D², Magnavox 922. E¹, Operadio 108 (right) 835 (left). E², Operadio 162. E³, Operadio 1010. E⁴, Operadio 1025. E⁵, Operadio 950 pre-amplifier output. F¹, RCA 12756. F², 12212,14,20. F³, RCA 12214,39. F⁴, RCA 12224,30,57. F⁵, RCA 12204,9. F⁶, RCA 12754 mobile. G, Stromberg-Carlson. H, Webster-Rauland. (Courtesy Vaco Sickle Radio Supply Co. . . See page 51 for further data.)

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SUPERHETERODYNE

by MARTIN W. ELLIOTT

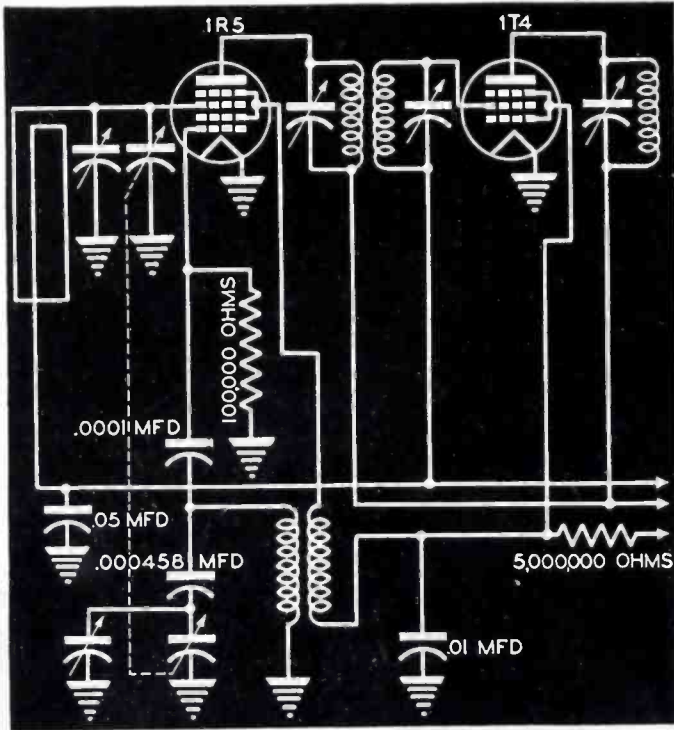


Fig. 1. Circuit of the converter and i-f stages of the Continental model G4. Since the entire receiver consists of four tubes, the converter stage must also supply high r-f gain. Avc is applied to the converter for uniform reception.

THE gain and selectivity of an r-f amplifier depends to a great extent upon the particular r-f of the signal, a high frequency allowing less gain and selectivity than a low frequency. This is due, in part, to the higher r-f losses at high frequencies. Hence, the popularity of the superheterodyne in which the signal frequency is converted to a desirable low frequency where optimum amplifying and selectivity conditions prevail. This desirable frequency is, of course, the i-f, and the frequency conversion is accomplished in the mixer stage by beating the signal with a local oscillator.

Producing I-F

The production of the intermediate frequency is not accomplished by the simple addition or subtraction of the two frequencies but, rather, by a modulating or detecting process in which the mixer tube operates on a non-linear part of its characteristic. A strong oscillator signal is applied to one of the mixer grids, usually grid 1, causing the tube to reach cut-off on the negative part of the oscillator cycle. This allows detection of a wide range of signal voltages with little change in mixer efficiency, the output i-f voltages being approximately proportional to the product of the oscillator and signal voltages.

I-F Transformers

In the detecting or modulating process the plate current of the mixer tube contains various modulation products in addition to the desired i-f. It contains the oscillator frequency, signal frequency, the sum and difference

Fig. 2 (below). Converter stage of the Garod IC712. The oscillator portion of the converter is a Hartley, with the cathode above r-f ground. A vacuum-tube voltmeter must be used to measure the cathode voltage, usually on the order of one volt.

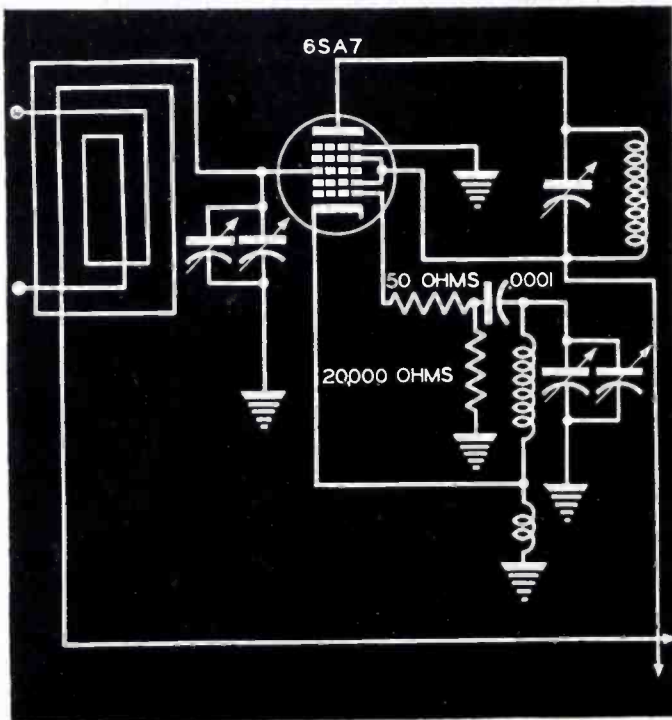


Table I (right). The more popular types of converters, together with their important operating characteristics, are presented in this table. Note the high conversion transconductance, which aids stage gain where no r-f stage is used.

	Plate Voltage	Screen Voltage	Control Grid Voltage	Plate Resistance (megohms)	Conversion Transconductance	Grid 1 Resistor	Total cathode current (ma.)
1A7	90	45	0	.6	250	20,000	2.5
1R5	90	45	0	.8	250	100,000	2.75
6A8	250	100	-3	.36	550	50,000	10.6
6K8	250	100	-3	.6	350	50,000	12.5
6L7	250	150	-6 over 1	.350	12.5
7A8	250	100	-3	.7	550	50,000	10.8
{ 6SA7	250	100	0	1	450	20,000	12.5
{ 12SA7							

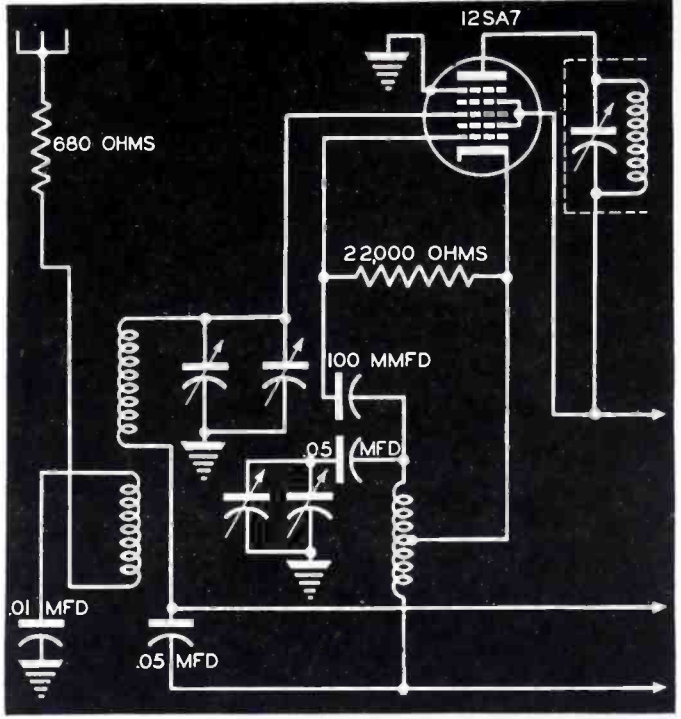
MIXERS

...eats and their integral multiples. It appears as if quite a filter would be required to select the correct i-f, and only the i-f. But the i-f is provided by a simple double-tuned i-f transformer operating at a selected low frequency favorable to sharp tuning. Since the detecting or mixing is accomplished in the grid circuit, the mixer tube acts as an amplifier at the intermediate frequency, but it is less efficient in this role than the conventional i-f amplifier because of the operation at cut-off during the negative half cycles.

Early superhets used triode mixers and separate oscillator tubes. This arrangement is still used by some manufacturers, notably Philco, but since this is not a typical practice, we shall bypass it. Most modern sets are designed around the series of high gain multi-grid converter tubes, whose characteristics appear in Table 1. Grids 1 and 2 usually serve as the oscillator grid and plate, respectively, so that a separate oscillator tube is not required. There are a few exceptions, where separate triode oscillators are employed. Special purpose short-wave and communications receivers often use separate oscillators for the very high frequencies and increased stability.

The new converter tubes use the electron stream as a mixing medium, eliminating the various types of ca-

Fig. 3. The converter stage of the G. E. model L540. The oscillator portion of the converter is a Hartley, with the cathode above r-f ground.



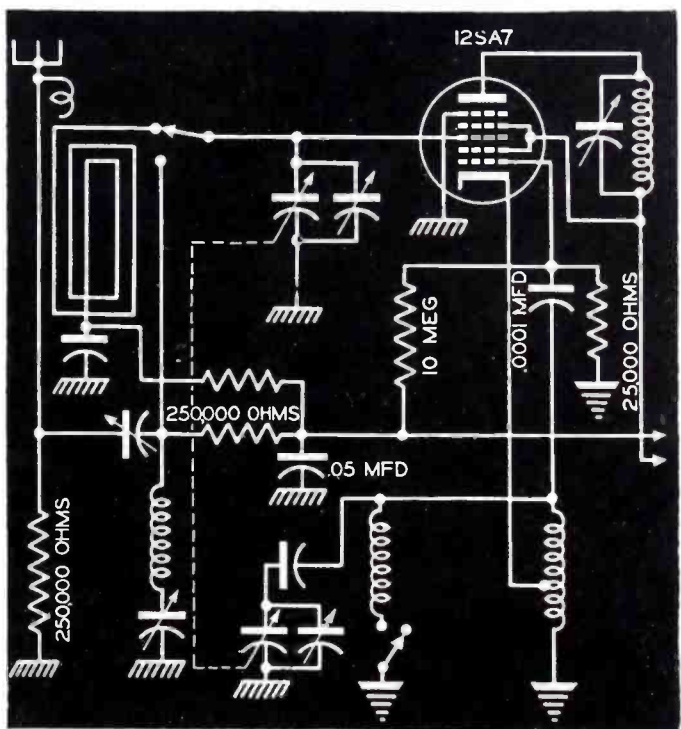
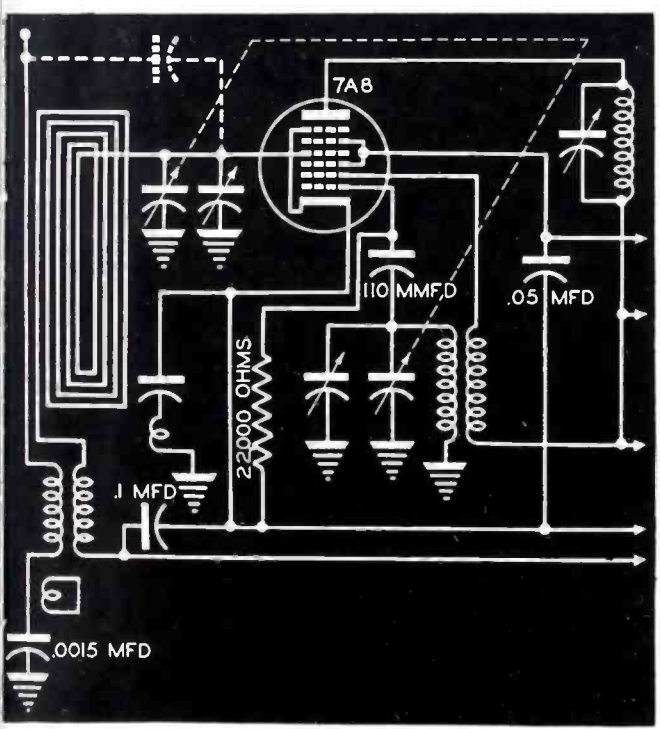
...pacity or inductive coupling which often were guilty of causing the receiver to radiate the oscillator frequency. The electron stream is modulated at the oscillator frequency by grid 1, the oscillator control grid. It is then intercepted by the signal grid which further modulates the stream, carrying to the plate the modulation products. This method of electron coupling causes negligible radiation

making an r-f stage buffer unnecessary to kill the radiation.

Continental Radio G4

Fig. 1 shows a typical 4-tube portable-battery receiver's (Continental Radio and Television G4) mixer and i-f circuits. This receiver uses a quadruple-grid 1.5-volt 1R5 converter tube which has a high conversion conductance, providing a high conversion

Figs. 4 (left, below) and 5 (right, below). Fig. 4. Philco 41 KR converter stage. A separate oscillator plate permits the use of a plate feedback type of oscillator circuit. In Fig. 5, the converter of the G.E. JCP-596 is shown. A shunt coil is used to increase the oscillator frequency for short-wave reception. Chassis ground and usual ground connections are shown.



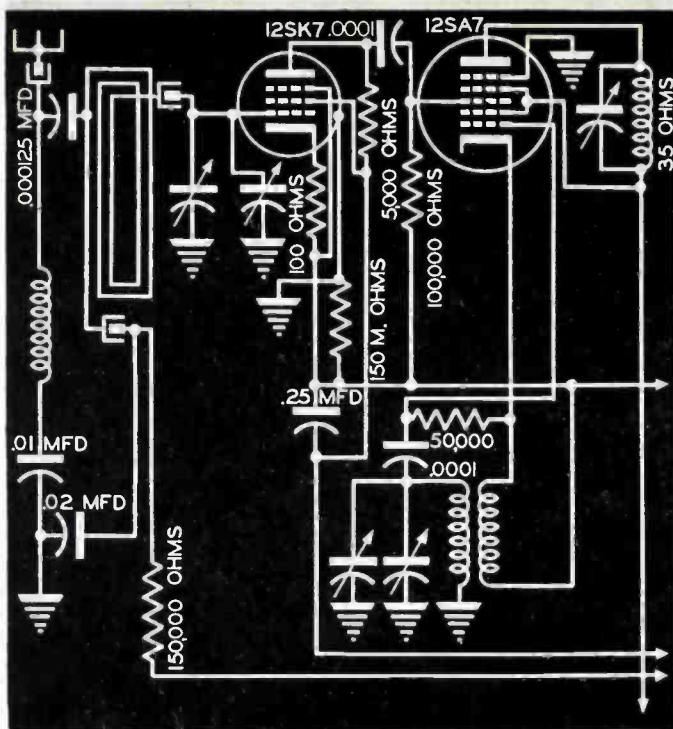


Fig. 6. R-f stage and converter of the Coronada C6D18. Here, the r-f stage is tuned, and resistance coupled to the converter stage. The use of the r-f stage does not increase the selectivity, but does improve the receiver gain, particularly at the low-frequency end.

gain. This is important because a small portable must use a small loop antenna with very limited pickup; therefore the overall gain must be very high. A substantial part of this gain must be furnished by the mixer stage. Modern mixer tubes also have remote cut-off characteristics making them adaptable for applying avc bias for controlling the gain in an inverse relation to the signal strength. This must be done with negligible detuning of the oscillator.

The low-potential end of the loop is tied to the avc system, returning to filament via a .05 mfd r-f bypass capacitor, C_1 . A high-frequency trimmer is connected in parallel with the tuning capacitor. A plate-tickler, tuned-grid oscillator circuit is used, the feedback winding being connected to grids 2 and 4, the oscillator plate and screen grid. No cut section is required in the tuning capacitor because of the low-frequency padding capacitor, C_2 , which has a capacity of .000485 mfd within 2%. A high-frequency trimmer is shown connected across the oscillator tuning capacitor. The grid capacitor, C_3 , has a capacity of .0001 mfd, typical values for battery portables, running from .00003 to .0001 mfd. The grid leak, R_1 , is of .1-megohm value, usual values running .1 to .25 megohms. Some battery sets have oscillators with screen grid or filament feedback. It is interesting to note that sets using the larger 1A7 converter tube have more freedom in oscillator circuits because the 1A7 has a separate grid, 2, for the oscillator plate.

Garod 1C712

A typical 6SA7 frequency converter

taken from a Garod, 1C712, is shown in Fig. 2. The loop is similar to that of Fig. 1 except that a primary turn is added for connecting an external antenna. The oscillator is a typical hot-cathode Hartley which uses either a tapped coil or two separate coils. The oscillator grid, 1, is at a high r-f potential, usually over 5 volts, while the plate, 2 grid, is at ground, or zero potential. The cathode is usually about 1 volt above ground, measured with a v-t voltmeter.

The cathode voltage of a 6SA7 must be limited to this value because over-voltage tends to block the tube, considerably reducing the gain. It should be noted that, in short-wave sets, the r-f voltage on the cathode across only $\frac{1}{2}$ turn will often be excessive with improper oscillator adjustment. This oscillator has a 50-ohm series resistor at the grid to limit the voltage developed at the high-frequency end of the range. The grid capacitor is .0001 mfd, usual values ranging from .00003 to .00012 mfd. The grid leak here has a value of 20,000 ohms while other receivers use 15,000 to 30,000 ohms. The grid leak is sometimes connected across the grid capacitor instead of the grid-to-cathode connection.

G. E. L-540

In Fig. 3 we have a typical 12SA7 mixer for 150-mil a-c/d-c compact sets, G. E. models starting with L-540. This is also a loop receiver with an antenna primary and 680-ohm series resistor which tends to give uniform antenna coupling throughout the band. The oscillator circuit is similar

to Fig. 2, using a tapped coil and the grid leak from grid to cathode instead of grid to ground. Note C_1 , a .05-mfd paper blocking capacitor used to satisfy underwriters' requirements that prohibit a B- connection on the top of the chassis. The capacity is large enough to prevent padder action, or detuning. The grid capacitor is a .0001 mfd; the leak, 22,000 ohms. Here, too, the loop is connected to the avc bus with a .05-mfd bypass to B-

Philco 41-KR

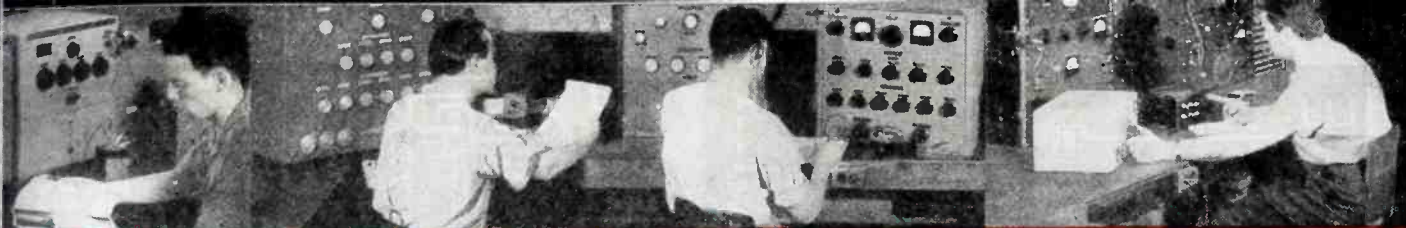
Philco uses a 7A8 converter in their model 41-KR, Fig. 4. This is a six-grid converter with a separate oscillator plate and requires a lower voltage on the screen grid than the plate for maximum conversion gain. Two separate types of antenna coupling are used; a small capacitor formed by a wire and eyelet which favors the high frequencies and an antenna transformer at the low potential end of the loop which favors the low frequencies. This makes an excellent flat-coupling system, but it is somewhat more expensive than the previous methods. Note the shorted tertiary winding on the transformer which reduces the Q , broadening the response and minimizing any resonant effects that may occur in the external antenna circuit.

A plate-tickler oscillator is used with a 110-mmfd grid capacitor and a 22,000-ohm leak. A series choke and capacitor connect the cathode with the chassis, instead of the usual capacitor. This innovation makes use of the common coupling that ordinarily exists from B- to chassis to make adjustments in the frequency response of the signal frequency circuits. This frequency converter is used only where no r-f stage exists.

G. E. JCP-596

Another 12SA7 mixer, this time with two wavebands, is shown in Fig. 5, G.E. model JCP-596. The antenna coupling to the loop is obtained by a small capacitor formed by a wire and the grid end of the loop. Coupling to the short-wave antenna coil is similarly obtained by means of a small capacitor. A 250,000-ohm resistor from antenna to chassis prevents building up of electrostatic charges on the antenna. The bandswitch is a simple d-p-d-t unit which connects the 12SA7 signal grid to loop or short-wave coil and also applies a shunt coil to the oscillation transformer in the short-wave position. This is, perhaps, the simplest means of switching oscillator frequency, no change being required in the feedback. An oscilla-

(Continued on page 26)



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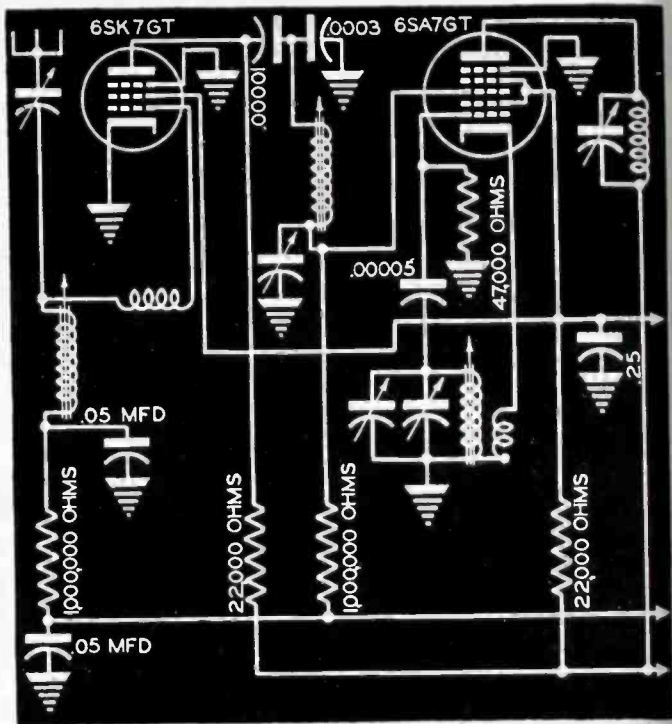
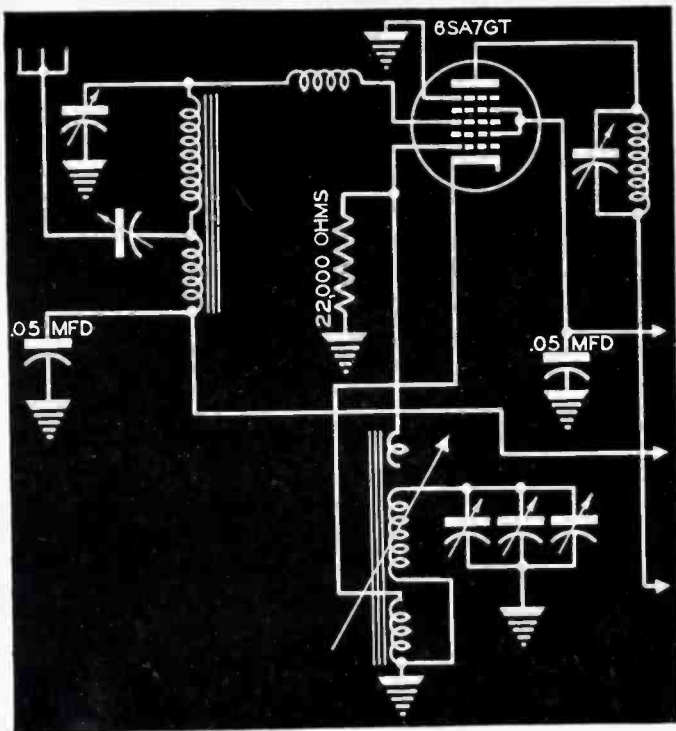
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ALL PLANTS





tor blocking capacitor is used for underwriters' approval.

Coronado C6D18

In Fig. 6 we have a tuned r-f 12SK7 amplifier which is resistance coupled to an untuned 12SA7 mixer, Coronado C6D18. In this design only a 2-gang condenser need be used and, while the extra stage contributes little in selectivity, it has a gain of about 11 on the low-frequency end and 5 on the high-frequency end. This model has combination coupling, both capacitive and magnetic, between antenna and loop. The coupling capacitor is large, .000125 mfd, but it is connected to a medium impedance tap on the loop. The other receivers used a much smaller capacitor connected at the grid end. T_2 is a high-impedance antenna primary isolated from the chassis by a .01-mfd capacitor. A 100-ohm degenerative cathode resistor supplements the avc bias on the r-f amplifier. The avc bus is connected to ground through 150,000 ohms.

The resistance coupling circuit is composed of a 5000-ohm plate load, .0001-mfd blocking capacitor and 100,000-ohm grid leak. The oscillation transformer has a separate cathode-feedback winding which permits grounding of the grid coil, eliminating the need for a grid-blocking capacitor. A .0001-mfd grid capacitor and 50,000-ohm leak are used. The latter value is unusually high.

Silvertone 7091-7093

Figs. 7 and 8 show mixers of a pair of Silvertone automobile receivers,

models 7091 and 7093, respectively. In Fig. 7 the oscillator has a separate feedback coil. In Fig. 8 wide spacing is used on the oscillator coil for proper tracking with the r-f stage.

ers, models 7091 and 7093, respectively. In Fig. 7 an iron-core antenna and oscillation transformer is used, the latter being adjustable for low-frequency ganging. The antenna is coupled through C_1 which is also the antenna trimmer provided to match the receiver to the car antenna. This trimming is usually done on a very weak station at about 1,400 kc. A loading coil is used between the antenna transformer and grid. The oscillation transformer has a separate cathode-feedback coil and also a few turns, deadended, which act as a grid capacitor to the high side of the grid coil. Two types of shunt capacitors are used; one for trimming the high-frequency end, the other for temperature stability, minimizing frequency drift upon warming up.

The circuit shown in Fig. 8 is a permeability-tuned affair with a 6SK7 tuned r-f stage. The antenna-coupling capacitor feeds the high end of the antenna coil instead of a tap. The grid loading coil is present here, too. Coupling the r-f tube to the 6SA7 mixer is completed by a 22,000-ohm plate-load resistor, a .00001-mfd blocking and coupling capacitor, a .0003-mfd shunt and a trimmer capacitor from signal grid to ground. The permeability-tuned coil and trimmer are resonant. Thus a high r-f voltage appears across each. The voltage across

the capacitor is fed to the converter tube.

The oscillator has a separate cathode-tickler coil. The grid coil has the same length as the other permeability-tuned coils, but it has fewer turns wound at a greater pitch to obtain the required higher frequency. This is the counterpart of the cut-plate capacitor in a typical capacitor-tuned oscillator where the oscillator is made to track with the r-f tuning at a fixed-frequency difference. Shunt trimmer and fixed silver-mica capacitors are used.

Allied E-10707

The mixer shown in Fig. 9 is used in Allied's model E-10707. It features the 6K8 triode-hexode mixer tube which has a separate triode section for the oscillator. The triode grid is also grid 1 of the hexode which automatically provides electron coupling between oscillator and converter. The separate triode section has a higher transconductance than the triode part of a standard converter tube. This permits operation at much higher frequencies and also adds stability, the safe upper frequency limit being about 40 mc.

The antenna transformer consists of three primary and three secondary coils in series, all three being used on broadcast, the upper two on police band and the top coil only on short-waves. The unused coils are shorted to prevent absorption of signal energy at resonant points. Note the i-f wave-trap between the top of the primary

(Continued on page 59)

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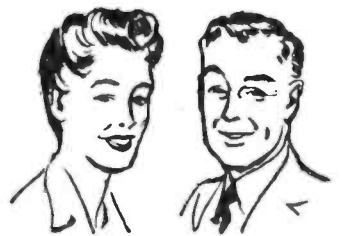
FATHER listens regularly to G-E newscasts. General Electric is a familiar name to him; he has bought G-E lamps as long as he can remember.



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Fig. 1 (below). Typical bias-type volume-control circuit.

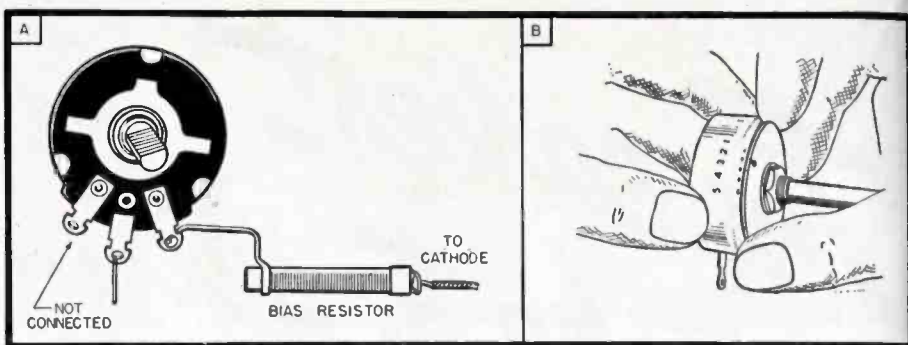
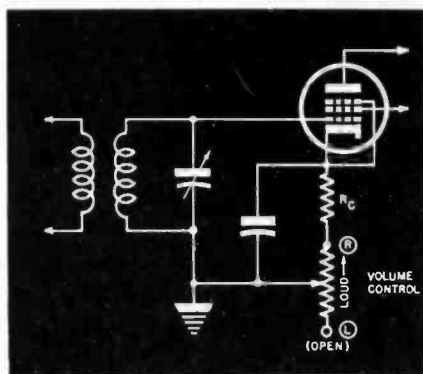


Fig. 2 (above). Volume control arrangements for bias-type control circuits, of the type illustrated in Fig. 1, that require a fixed bias resistor. In *b* appears a special type of wire-wound volume control with an adjustable stop for stopping the travel of the contact arm at any one of five marked positions. (Courtesy P. R. Mallory & Co., Inc.)

VOLUME AND TONE CONTROL RESISTORS

WHILE the electrical constructional features and characteristics of volume and tone controls, previously discussed, are of vital importance to the Service Man, there are many additional details concerning their mechanical design and construction, accessories to be attached, methods of installation, etc., that require careful consideration.

Tapped Controls

Let us, for instance, analyze tapped controls; controls having one or more taps brought out from points on the resistance element. In some makes of such controls the taps are fixed, but in others their position on the resistive element is internally adjustable at suitable intervals from 25% to 75% of the total rotation.

The common use of tapped controls is a relatively recent practice, although a few old receivers did feature them. In recent receivers they have been widely employed in the *diode-bias* method of controlling volume, where the resistance unit is used as a diode-load resistor. The additional tap is used to provide an extra *avc* voltage of a lower value than the main *avc* source.

With rare exceptions there are only three basic types of control circuits that use a tapped control: (1)—Where the control is tapped in order to provide different values of voltage, such as in an *avc* circuit; (2)—where the tap is brought out so that automatic tone compensation may be accomplished;

Part Eight of a Series on Receiver Components

by ALFREDA. GHIRARDI
Advisory Editor

and (3)—where it is desired to use one control to act upon two circuits (to provide either radio or phonograph control or to act as fader controls from one phonograph pickup unit to another, one microphone to another, and similar applications). These types of circuits will be discussed in a subsequent article of this series.

Adjustable Fixed-Bias Resistor Controls

When replacing a carbon-element volume control in which the original control included a built-in minimum-bias resistor, R_c , for the type of circuit shown in Fig. 1, one of the small 500-ohm adjustable wire-wound bias resistors available for this purpose may be connected in series with the replacement volume control. This is illustrated at (a) of Fig. 2. The adjustable clip on the bias resistor may be clamped securely to the resistance element at the proper place by means of a pair of gas pliers to obtain the correct bias resistance required (which is usually less than 500 ohms).

When replacing a wire-wound volume control having a value between 2,000 and 20,000 ohms in antenna cathode and bias circuits of this kind, one of the special types of wire-wound volume controls made with the most

suitable taper for this type of control circuit, illustrated at (b), may be used. This is provided with an adjustable stop for stopping the travel of the contact arm at any one of five marked positions near the right-hand terminal of the resistance element, permitting the control to retain a definite fixed resistance section at this end. The position of this stop may be easily adjusted to provide any of the following five values of fixed bias resistance: 100, 200, 300, 400 or 500 ohms—all with the usual commercial tolerance of $\pm 10\%$. After being adjusted for whatever value of fixed bias resistance is required by the receiver, the stop plate is locked in position by a holding nut. Whenever bias resistance values other than those specified above are required, the indicating bump may be filed off the plate and the required resistance adjustment made with the aid of an ohmmeter.

This adjustable grid-bias feature eliminates the need for an external bias resistance and also eliminates the necessity of having special controls of the same resistance value but requiring different fixed-bias resistors.

Volume and Tone Control Attachable Switches

Some receivers employ *off-on* switches (in the line, battery circuits, etc.), that are separate from all other controls. However, now most employ switches that are mounted directly on the volume control and are operated by the shaft of this control during ap-

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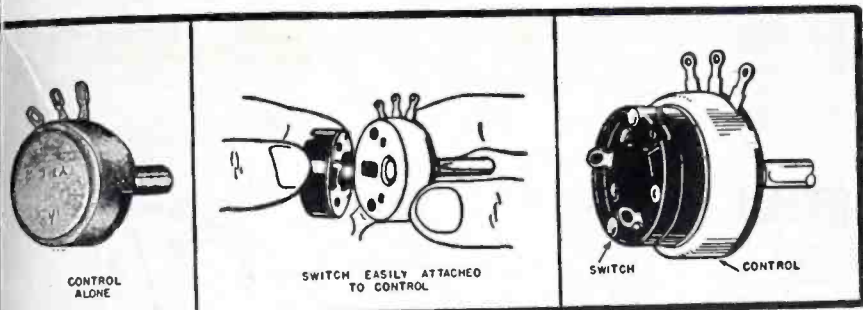


Fig. 3. How on-off-rotary-snap switches are attached to volume and tone controls. These rotary-snap switches are available with various contact arrangements shown in Fig. 4 below.

approximately the first 10° or 15° of rotation from the *off* (extreme counter-clockwise) position. To supply a line of replacement controls, all equipped with switches, obviously would increase the cost of the controls in the cases where switches are not required. Consequently the problem has been met by designing most composition-element wire-wound replacement controls so that a specially designed rotary snap switch may be easily attached to the back. The controls are provided with a switch-actuating pin and

the contact arm of the control set at the proper extreme position), so that the switch is actuated by the insulated shaft of the control—usually during the first 10° or 15° of its rotation from the *off* position.

Attachable rotary-snap switches are available with various contact arrangements to perform any desired switching function. Those most commonly used in receivers are listed herewith, together with their most customary applications. The contact arrangement of each one is illustrated in Fig. 4.

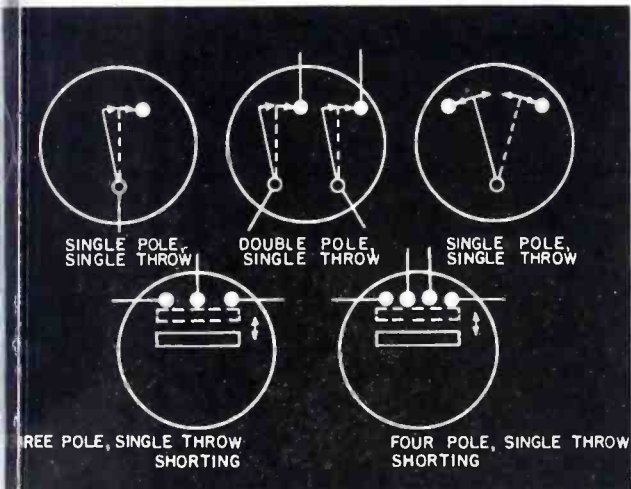


Fig. 4. Contact arrangements of the five most-used types of rotary-snap switches.

switch-mounting holes in their covers. These holes are normally covered with a blank back plate when no switch is being used. When a switch is required, the plate is removed and the switch is attached to the cover of the control by properly meshing the actuating parts, as shown in the center illustration of Fig. 3. The actuating pin meshes with the switch cam (with

(1)—*Single pole, single throw*: For general *on-off* switching of either battery or power type receivers.

(2)—*Double pole, single throw*: For use on battery receivers where it is necessary to break both the *A* and *B*, or the *A* and *C* battery circuits. This may also

be used as a three pole, single throw shorting type of switch.

(3)—*Single pole, double throw*: For use where it is desired to close one circuit during operation of the control, yet open this circuit and close another when the control is turned to the *off* position. This is usually found on radio-phonograph combinations.

(4)—*Three pole, single throw, shorting*: For use on battery-operated receivers where it is necessary to open the *A*, *B*, and *C* battery lines to prevent useless discharge of the batteries.

(5)—*Four pole, single throw, shorting*: Like the foregoing type, this switch is for use on battery-operated receivers. It allows one additional circuit to be opened. Although there are only three battery circuits (*A*, *B* and *C*), the wiring of many late model battery receivers is such that it is necessary to open four circuits.

Controls in Tandem

Volume and tone controls often are mounted in tandem. The most commonly used tandem arrangement is that of two units used as a *dual* control.

The expression *dual-control circuits* is applied to all circuits using two controls driven simultaneously by the same shaft. The two controls may be of the same, or different, resistance values and tapers, and both wire-wound and composition-element type controls

(Continued on page 46)

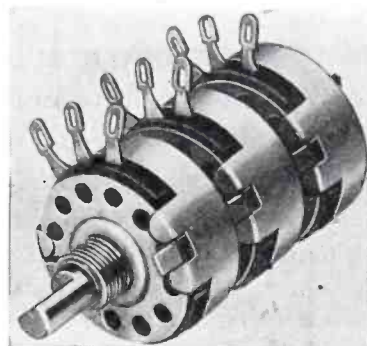
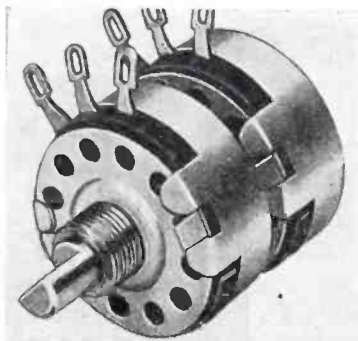
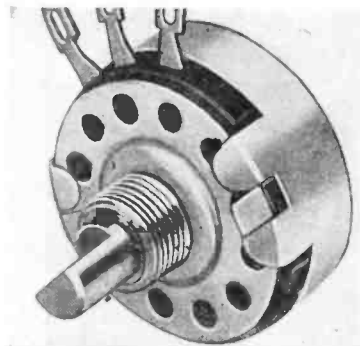


Fig. 5. Single, dual and triple control assemblies, with the same type of controls used to build up multiple units. (Courtesy Allen-Bradley Company)

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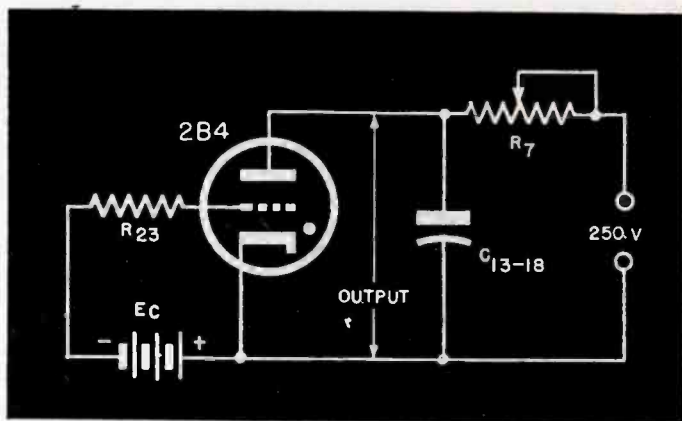


Fig. 1. Elementary linear time-base oscillator circuit. Here, the plate potential, at which the thyatron 2B4 begins to conduct, is determined by the negative grid-to-cathode potential. The timing capacitor C_{13-18} charges in series with the limiting resistance R_7 , the charge eventually reaching such proportions that the thyatron tube *breaks down*, relaxing the charge and initiating a renewed charging of the timing capacitor.

C-R OSCILLOGRAPHS SERVICING... APPLICATIONS...

UNDER certain conditions, it is necessary to utilize the cathode-ray tube deflection plates directly, without deflection plate-voltage amplification, for voltage measurement or wave observation, such as we often encounter in the study of commercial power-line voltage surges. It may be also necessary to use the c-r tube unit as a receiving device for testing of experimental television equipment. Hence, in the Du Mont oscillograph, the deflection plates are brought out to terminals on a suitable terminal board, which are located on the rear of the unit cabinet, and which are directly accessible without necessitating the removal of the cabinet, and consequent exposure of the high voltage wiring within the device. In this terminal-board system, two removable connecting links disconnect the free deflection plates from the vertical and horizontal amplifier coupling systems, respectively. An extra terminal is also brought out on the terminal board, connected to the unit chassis, thus providing a terminal potential level equal to that present between the fixed deflection plates and the tube cathode.

Where the wave from a power line surge is under observation, it may be desirable to utilize the direct connection to only the vertical deflection plate, leaving the horizontal plate connection to the horizontal amplifier output system intact to permit the utilization of the linear time-base-oscillator amplifier voltage output.

As has been stated, the output voltage of the linear-time-base sweep oscillator is amplified by the horizontal amplifier. This procedure is necessary to preserve the linear form of the time-base oscillator-voltage output waveform.

[Part Four of a Series]

by S. J. MURCEK

The operation of the linear time-base oscillator is based on the principle of controlled, recurrent relaxation of the electrostatic charge on a capacitor, under the condition that the capacitor be charged at a constant current rate in the period existing between the relaxations. In such a system, the charge on the capacitor is conveniently relaxed by conduction through a thyatron tube, this form of relaxation providing an approximately complete discharge of the charge on the capacitor in the smallest practical discharge time period. Further, the duration of the discharge is directly dependent on the thyatron characteristics.

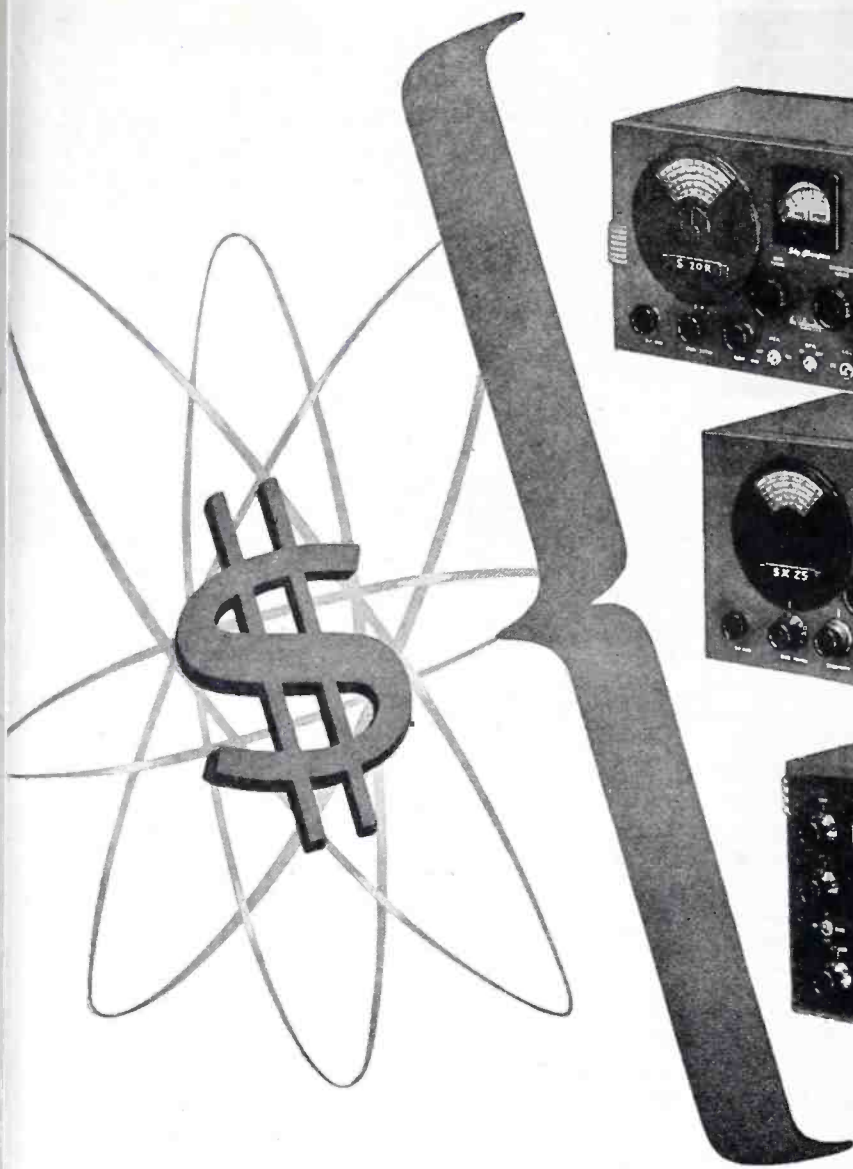
Unlike the conventional vacuum tube, the thyatron tube conducts, regardless of the control-grid potential, continuously, once the control is driven positive with respect to the cathode. The only way in which the conduction may be stopped, once it is initiated by the positive swing of the control grid, lies in the reduction of the tube plate potential to a value less than the tube arc or conduction voltage drop, or in complete interruption of the thyatron-plate circuit. In commercial thyatrons, the anode-cathode arc-drop potential lies between 8 and 18 volts, and is dependent on the nature of the tube gas or vapor filling; whether it is one of the noble gases, such as neon, or mercury.

The function of the 2B4 thyatron in the linear time-base oscillator is

well illustrated in the elementary linear time-base or relaxation-oscillation circuit of Fig. 1. Here, the thyatron is shown to be directly connected across the terminals of the timing capacitor, C_{13-18} . Since the control grid of the tube is maintained somewhat negative, the tube is not immediately conductive. Further, the plate voltage at which the tube begins to conduct is directly dependent on the negative grid voltage, and this, in turn, is so adjusted that the tube is conductive when the plate voltage rises to approximately 50 volts. If, however, the capacitor charge attains this latter potential, the tube breaks down and conducts, the conduction effecting a discharge of the charge on the capacitor until the capacitor voltage is less than the thyatron arc drop. Under this condition the tube ceases to conduct, since this final potential is insufficient to maintain ionization of the tube atmospheric gas, and therefore conduction of the discharge current.

The timing capacitor C_{13-18} , in Fig. 1, is continuously charged by the charging current available through the positive and negative terminals of the d-c low-voltage supply source. The charging current is limited by the timing control potentiometer, R_7 , resistance. When the voltage of the capacitor being charged is small in comparison with the source voltage, the current flow through the capacitor and the series limiting, or timing, potentiometer, R_7 , is relatively constant, and the capacitor charges at a relatively constant charge current rate. Hence, the rise in the capacitor terminal potential with respect to time is relatively linear, as is shown in the graph of Fig. 2. Further, the rate at which the

(Continued on page 36)



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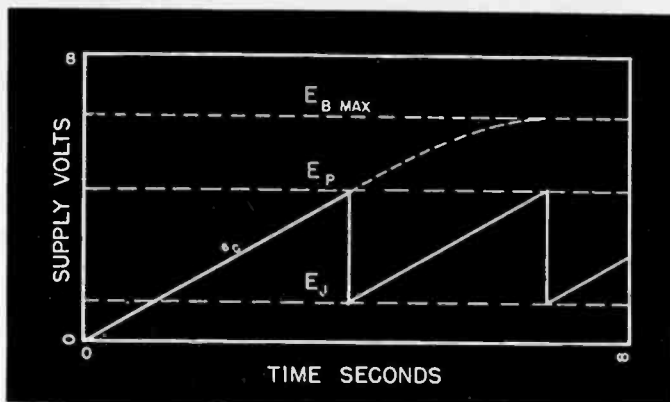


Fig. 2. Typical sawtooth deflection voltage wave produced by the linear time base oscillator shown in Fig. 1. The maximum voltage level attained by the wave occurs just before the relaxation of the capacitor charge at the point e_c and the minimum level is determined by the thyatron tube plate-cathode conduction characteristic, shown as E_J . Note that the voltage output of the oscillator is the voltage difference between the thyatron breakdown level and the conduction or arc-drop level.

timing capacitor is charged is directly dependent on the amount of series resistance interposed between the capacitor and the charge current source, e.g.,

$$t = RC \quad (1)$$

where: t is the charging time in seconds, R is the limiting resistance in ohms, and C is capacitance, in farads. From equation 1, we may determine that the capacitor charging time t may be readily varied by manipulation of the series resistance, R , since the timing capacitance, C , is fixed, or constant.

In Fig. 1 the timing capacitor C_{13-18} is constantly charged in series with the resistance of the timing control potentiometer, R_7 . Therefore the potential across the capacitor eventually attains the potential at which the thyatron tube breaks down and begins to conduct; the time required to charge the capacitor is dependent on the resistance to which the timing control potentiometer slider arm is adjusted. Further, once the capacitor is discharged, and the thyatron tube ceases to conduct, the capacitor again begins to absorb a charge. Evidently, the charging and the subsequent relaxation of the capacitor, continuing as an unlimited series of operations, give rise to a fundamental waveform in which the frequency is dependent on the total time required to charge, then subsequently discharge, the timing capacitor, inasmuch as the frequency of the oscillations is, in reality, taken as the number of capacitor relaxations occurring within a given period of time. Thus, the frequency of the oscillations, in cycles per second, is

$$f = 1/t \quad (2)$$

where: f is the oscillation frequency in cycles per second, and t is the total time elapsing for a single charging and relaxation of the timing capacitor charge in seconds.

In the linear time-base oscillation circuits presented, the timing capacitor is effectively short-circuited by the thyatron tube when the latter is con-

ductive, no series limiting resistance being interposed between the tube and the capacitor. Further, it is known that the arc-drop potential present across the plate and cathode of the thyatron during conduction remains comparatively constant, regardless of the current conducted by the tube. The latter characteristic of the thyatron tube suggests that the volume of the gas or vapor contained in the envelope of the tube, which is ionized by the current conducted through the tube, is dependent on the intensity of the plate current flow. Inasmuch as this condition is actually present within the tube when the latter is conductive, it is evident that, neglecting the tube characteristic arc drop, the tube acts as a constant low resistance, or short-circuit, during the conduction period.

The timing period required for the complete discharge of the timing capacitor is extremely short, actually being of the order of a few microseconds, and is, therefore, negligible in the determination of the oscillation frequency. Hence, in equation 2, the time may be taken as the required charging time of the timing capacitor, as given in equation 1. For ease in the determination of the oscillator frequency, the two fundamental equations may be combined as a single statement, wherein the frequency is directly proportional to the reciprocal of resistance-capacitance product, or

$$f = 1/RC \quad (3)$$

where: the frequency f is given in cycles per second, resistance R in megohms, and capacitance C in microfarads.

From equation 3, we note that the linear time base oscillation frequency is indirectly proportional to the resistance at which the timing control potentiometer is adjusted, the capacity, in any instance, being fixed or constant. Briefly, the increase in the capacitor-charging rate through decrease of the timing potentiometer resistance results in an increase in the number of capacitor relaxations oc-

curing within a given space of time.

The nature of the linear time-base oscillator-voltage output waveform may be seen from the graphical illustration of Fig. 2. Here the waveform is of *sawtooth form*; thus we have use of the common term, *sawtooth wave oscillator*, for the conventional relaxation oscillator. In Fig. 2, the initial slope of the output waveform is due to the rise in the timing-capacitor terminal voltage in the period between the relaxations of the capacitor charge. Once the capacitor charge potential e_c attains the thyatron tube breakdown voltage limit the thyatron conducts and relaxes the capacitor charge, the relaxation continuing until the voltage across the capacitor falls to, or below, the thyatron arc drop potential E_J . When this condition occurs, the capacitor again begins to absorb a charge, continuing the output voltage waveform.

In Fig. 1, it is shown that the voltage output from the linear time-base oscillator circuit is that existing between the plate of the thyatron and chassis, or the negative terminal of the low voltage d-c power supply source. We also note that this potential is always proportional to the capacitor potential, since the cathode bypass capacitor C_{20} , in Fig. 2,¹ serves to maintain the cathode resistor potential relatively constant at all times. Hence, in Fig. 2 of this paper we see that the oscillator-voltage output obtainable from the oscillator is the difference between the maximum charge potential and the thyatron tube arc drop potential E_J . The maximum capacitor potential is maintained at a low value to preserve the linear form of the oscillator output waveform. Accordingly the oscillator output voltage ranges between the maximum and minimum values of 30 to 15 volts. This condition is usual in the average commercial cathode-ray oscillograph.

Inasmuch as the linear time-base oscillator output potential is insuffi-

(Continued on page 54)

¹SERVICE; September, 1945.

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INPUT CIRCUITS

[Part Two]

by L. E. EDWARDS

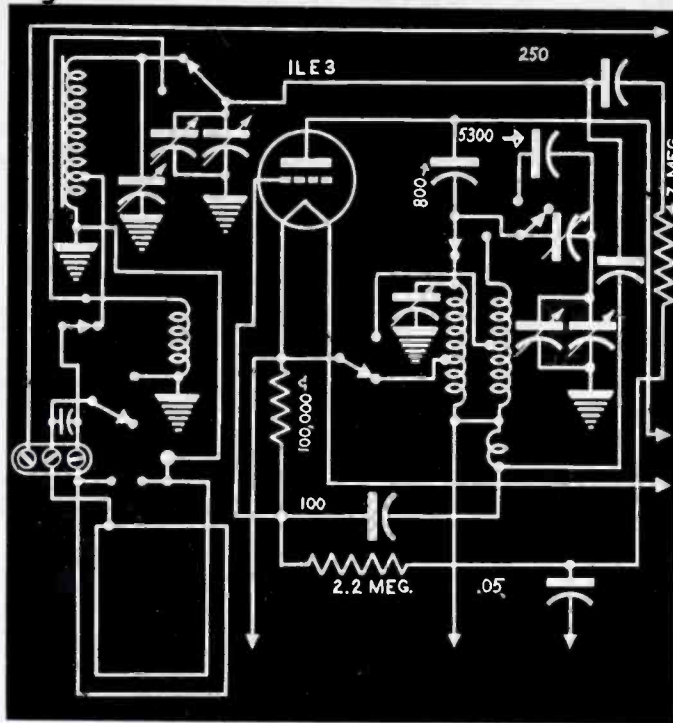


Fig. 1. Input circuit of the Philco 42-853. The tapped loop permits the use of an external antenna coupled at the tap. In addition, the tapped portion is used for short-wave pickup. (See page 51, September SERVICE for complete circuit analysis.)

AUTOMOBILE receivers require special treatment in the antenna circuit to obtain a maximum signal strength and a minimum amount of vibrator and ignition pickup. Loop antennas are unsatisfactory unless operated remotely in the clear. Such operation is too complicated and too expensive. Thus vertical rods are universally used as antennas. Because the antenna is very short, considering the wavelengths being received, the coupling must be very

close and the antenna transformer must be very efficient. A gain of 10 to 30 is usual in the antenna coil.

In Fig. 3 we see a typical auto set input. In this circuit, Lafayette model BB9, an iron-core antenna transformer

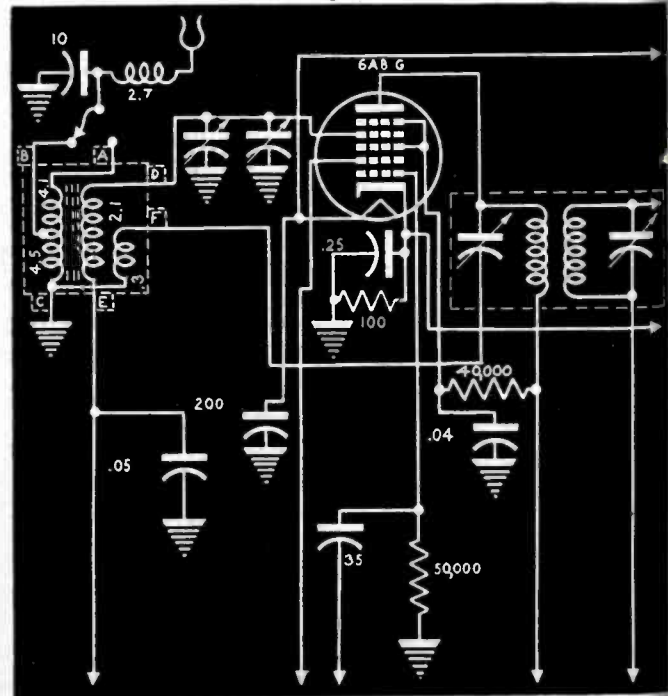
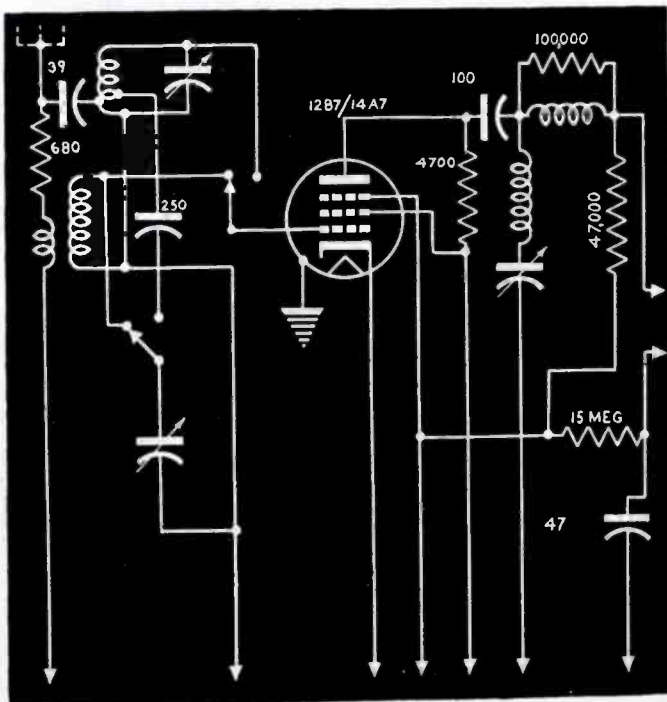
Figs. 2 (below left) and 3 (below right). In Fig. 2 appears the dual-loop system used in the G.E. L-642. A d-p-d-t switch is used for band-switching. (A complete analysis of this circuit appears on page 52, September SERVICE.) Fig. 3 A typical auto set input; Lafayette BB9. An iron-core transformer is used in the antenna circuit.

with separate taps for matching a low- or high-capacity antenna is used.

A small loading coil in series with the antenna acts as an r-f choke for high-frequency interference, particularly for the ignition system which has a maximum output of between 40 and 60 mc. A Faraday screen is sometimes used for the same purpose. This is a shield without closed loops which is placed between primary and secondary of the antenna transformer. This is very effective in preventing capacity coupling which is responsible for most of the ignition pickup. The transformer is shielded, quite important in limiting vibrator interference. A 10-mmfd bypass capacitor also helps to eliminate high-frequency interference at the low side of the antenna choke. The transformer contains a tertiary winding which is connected to a 6A8 plate through a small capacitor for feedback.

Another departure from conventional loop antennas is necessary in some permeability-tuned receivers because it is impractical to use iron in the field of a loop. In Fig. 4 we see one version

(Continued on page 40)





Our Hat Is Off...

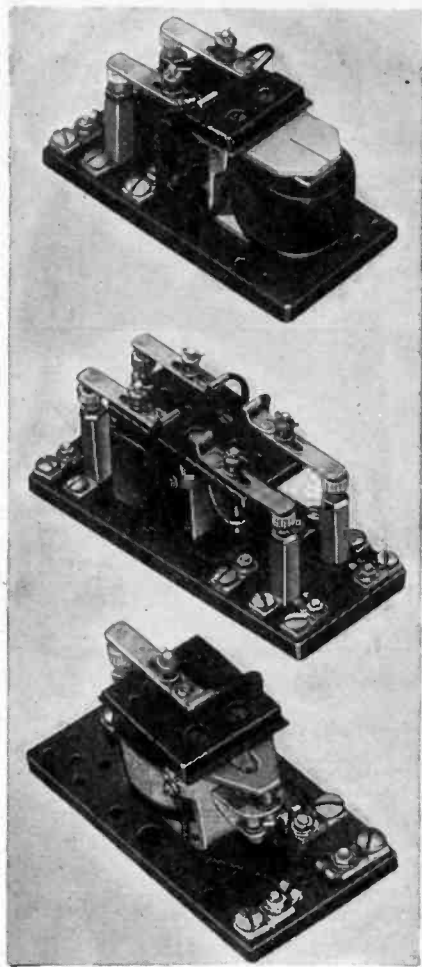
Our hat is off to those radio men, both military and civilian, who contributed so much to the successful completion of the war. Too, our hat is off to those radio servicemen and jobbers who were patient and understanding of the shortage of Rider Books caused by wartime restrictions, now removed.

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INPUT CIRCUITS

(Continued from page 38)

of this type input, Detrola model 421. A plate antenna is used with high-impedance external-antenna capacity coupling. The plate consists of a large piece of foil placed in the rear of the cabinet while the coupling capacitor has a small electrode having an effective capacity of 2 to 5 mmfd. This coupling system is critical, a little excess introducing annoying interference, hum modulation, etc.

It is possible to use a type of low-

impedance loop in a permeability-tuned system by simply putting the loop in series with the tuned coil, but the pick-up is poor. To permit a normal tuning range, the loop inductance must be held to a very low value which limits either the loop size or the number of turns, which in turn limits the pick-up. Also the permeability tuned coil must be of better quality with less distributed capacity than a standard coil. The circuit of Figure 5, Belmont model 533,

is similar to the Detrola, having permeability tuning and an antenna plate. Here, however, the plate is isolated from the input grid by a 300-mm blocking capacitor. The external antenna is capacity coupled at a low impedance point at the low side of the antenna coil and across an 800-mmfd capacitor. The 100-mmfd series capacitor which favors the high frequency compensates for the loss in high frequency due to the shunting effect of the 800-mmfd capacitor. A 200,000 ohm grid leak also shunts the antenna.

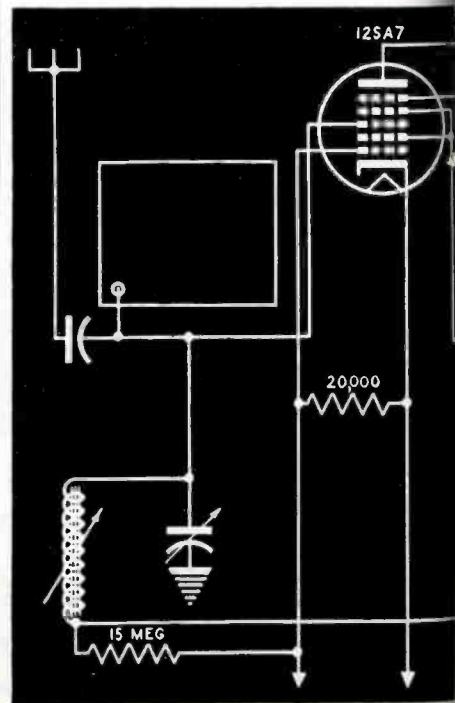
Permeability tuning will be featured in many postwar receivers, for it offers higher- Q tuned circuits with more gain and increased selectivity, space economy, simplicity of construction, simple alignment procedure and the elimination of microphonics and contact difficulties.

Notes

Electrostatically shielded loops found in some of the better type receivers, develop a signal voltage from the electromagnetic field only. Hence its directional effect will be very marked, the directional pattern being a figure 8 with two sharp minima when the loop is placed well away from other objects. Some unshielded loops also have sharp minima, particularly those mounted away from the chassis. Chassis absorption tends to destroy the directional effect.

Low-impedance loops tend to be

Fig. 4. A plate-antenna input system; Detrola model 421. The coupling capacitor has an effective capacity of 2 to 5 mmfd. The plate is usually made up of a large piece of foil placed in the rear of the cabinet.



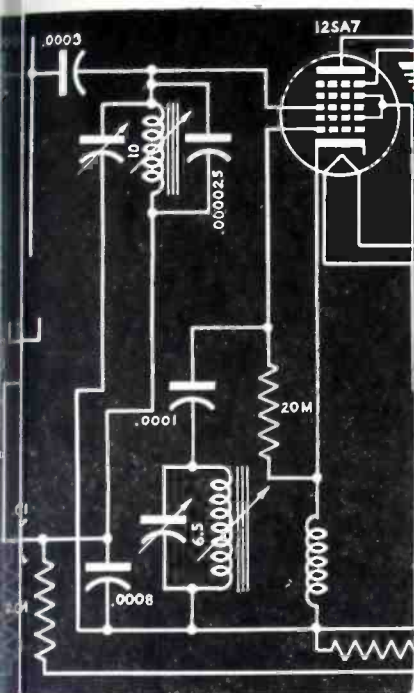


Fig. 5. Antenna-plate and permeability tuning system of Belmont 533. In this circuit the plate is isolated from the input grid by a 300- μ f blocking capacitor. The external antenna capacity coupled at a low-impedance point at the low side of the antenna coil and across an 800-mmfd capacitor.

are more directional than high-impedance antennas because they have less capacity pickup which would minimize the directional effects. Marked directional effects may be both obnoxious and useful; the former when the receiver must be tuned frequently when changing stations; the latter when some sort of man-made interference can be eliminated by setting the loop minimum toward the source of interference.

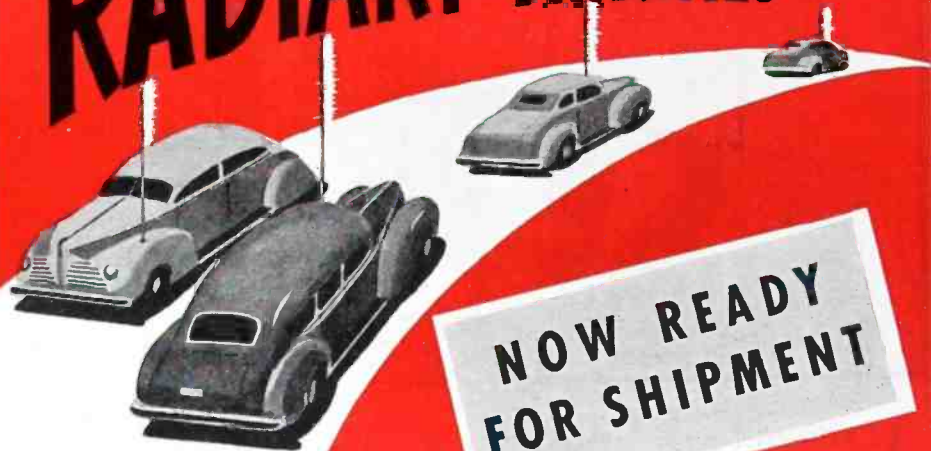
POSTWAR RECEIVERS



Above, RCA Victor's latest personal receiver. Weighs 3½ pounds complete with batteries. Below, new Garod 5P1 phono-receiver. See page 47 for views of other postwar receivers)



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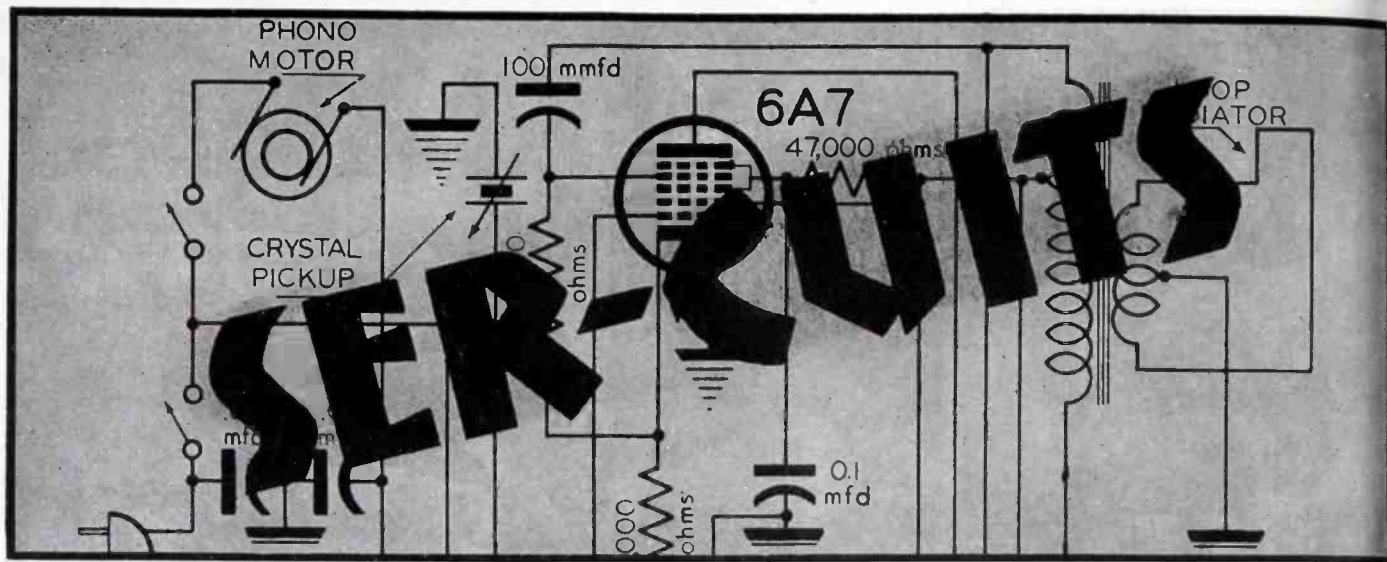
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ALTHOUGH many prewar portables were quite basic in pattern, several types did include many unique features. The 3-tube Motorola shown in Fig. 1, is an example of this special design format. Tubes used, for instance, included a 1A7GT with permeability tuning, a 3A8GT diode-triode-pentode i-f, detector and a-f, and a 1Q5GT power amplifier.

The sensitivity at 600 kc is about 15 microvolts. A rod antenna having a capacity range of 10 to 200 mmfd can be accommodated by an antenna trimmer.

The oscillator circuit is a shunt-fed

by HENRY HOWARD

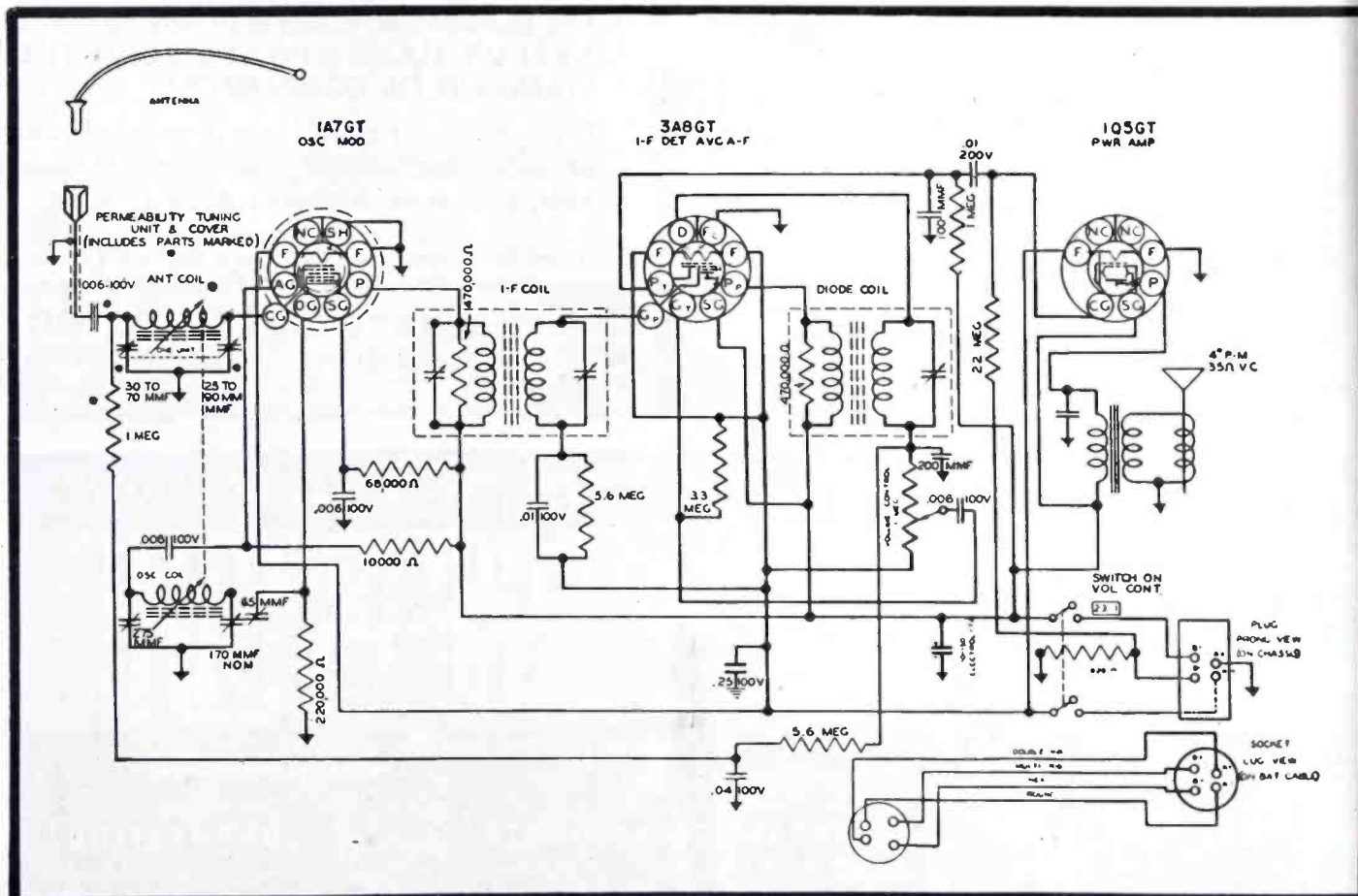
Colpitts with the plate at one end of the coil and the grid at the other. No tap is used but a capacity voltage divider consisting of a 170-mmfd capacitor at the grid end and a 275-mmfd capacitor at the plate end, places the grounded filament somewhere near the center of the coil (from a potential

standpoint). These capacity values are nominal since they are variable trimmers. A 65-mmfd trimmer-type grid capacitor is combined with the grid trimmer. The grid leak has a value of 220,000 ohms.

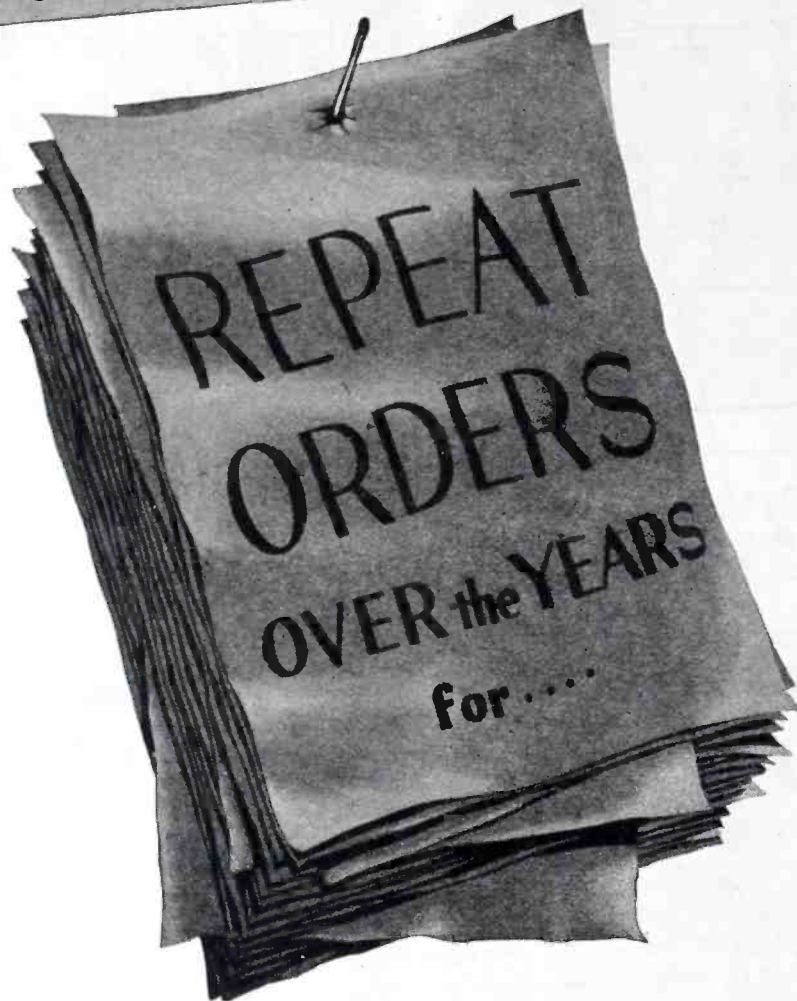
The pentode section of the 3A8GT serves as the i-f amplifier and is supplied with grid-leak bias via a 5.6-megohm resistor in series with the secondary of the i-f transformer at the low end, and bypassed by a .01-mfd capacitor. A 470,000-ohm resistor is shunted across the i-f primary. The transformer coupling the pentode to the diode detector has a similar re-

Fig. 1. Three-tube Motorola B-150, featuring a 3A8GT diode-triode-pentode as an i-f-detector-avc and audio amplifier.

(Continued on page 44)



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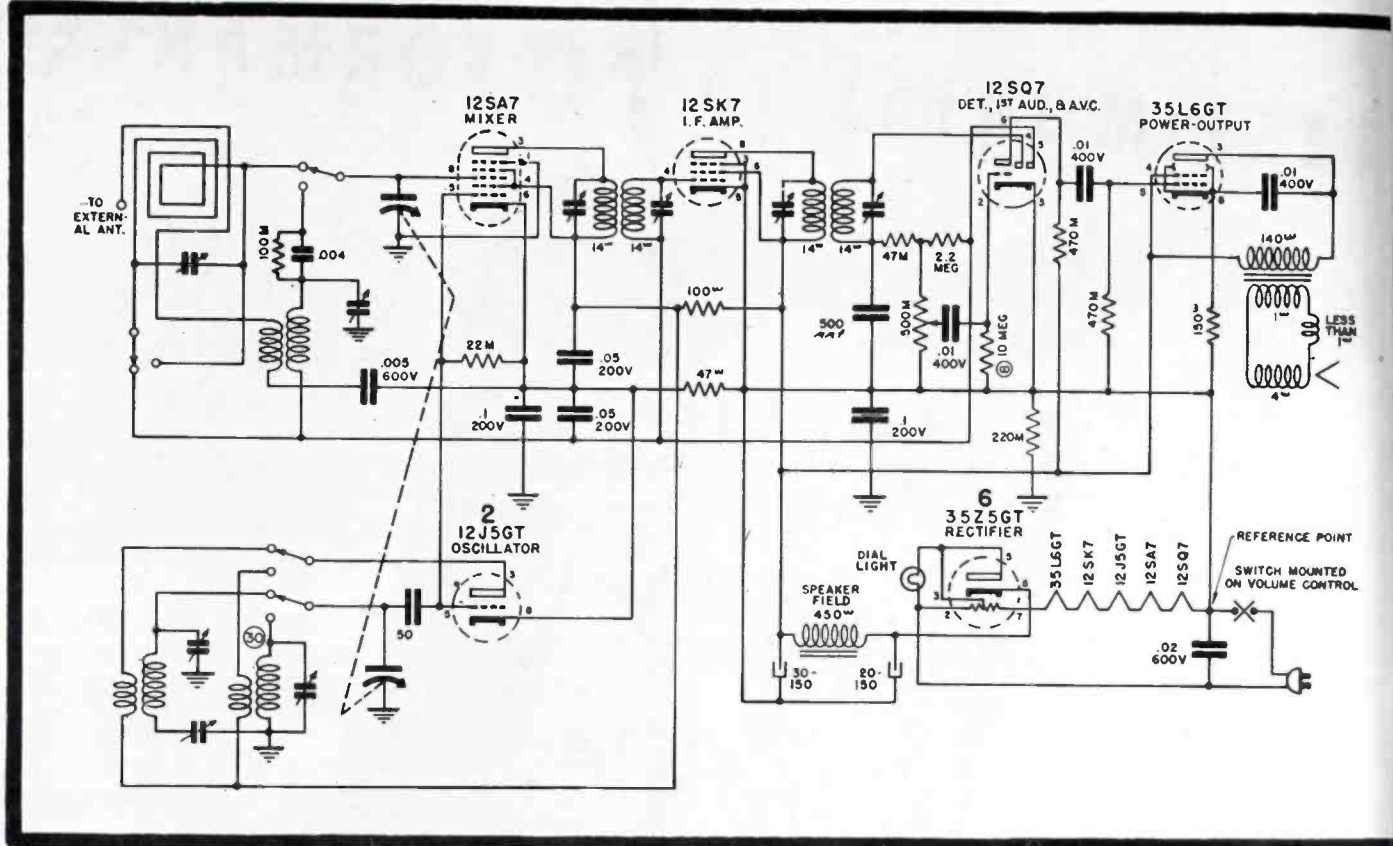


Fig. 2. Farnsworth BT-22 two-band receiver with a separate 12J5GT oscillator for grid-to-grid coupling to a converter.

SER-CUITS

(Continued from page 42)

istor load, but the primary is untuned. Avc bias is fed to the 1A7 modulator only. The 3A8GT filaments are run in parallel to accommodate a 1.5-volt *A* battery.

The audio amplifier consists of the triode section of the 3A8GT with a 3.3-megohm grid-leak bias feeding a 1Q5GT beam tetrode which derives its bias from a 820-ohm resistor in the *B*- leg of a 90-volt *B* battery. A 10-

mfd 150-volt electrolytic from *B*+ to ground serves as an audio bypass around the *B* battery and 820 ohms.

Farnsworth BT-22

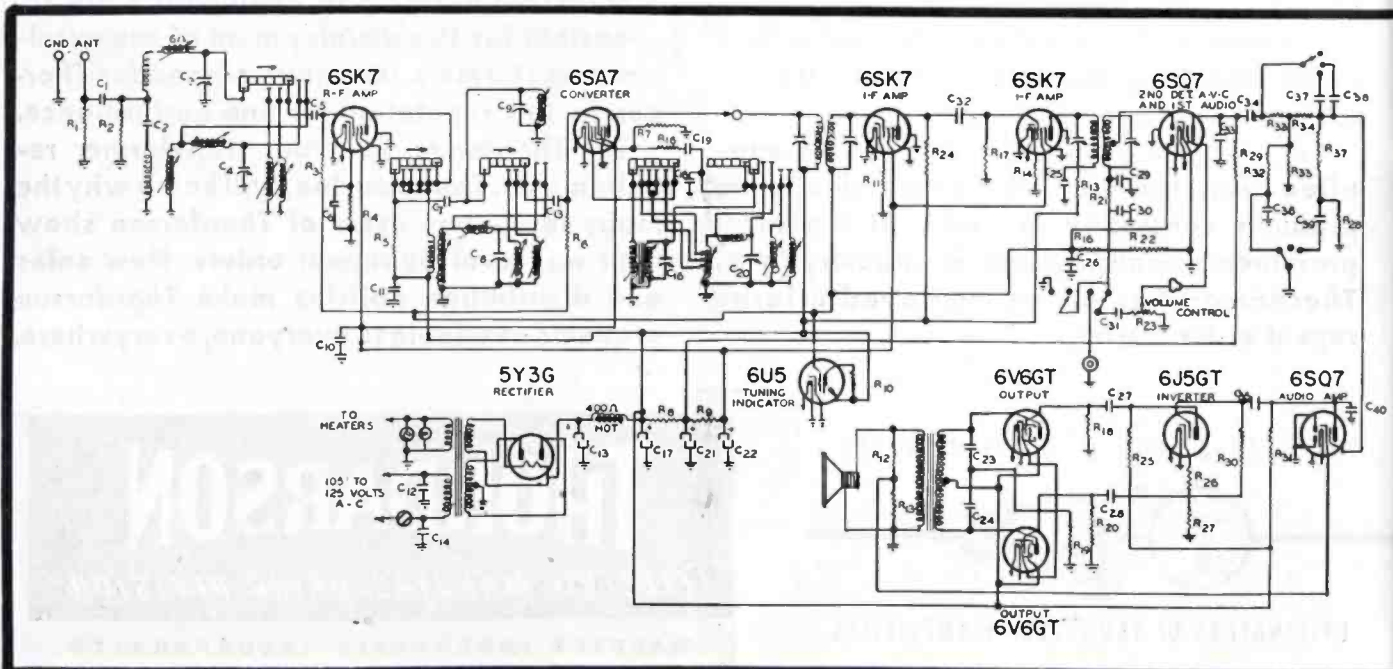
In Fig. 2 we have a 2-band receiver with several interesting features. This model, uses a separate 12J5GT oscillator with grid-to-grid

Fig. 3. Coronado C 1100 eleven-tube five-band model using permeability tuning and shunt coils for bandspread tuning. See page 53 for parts list.

coupling to a converter.

The bandswitching system is quite unique. The signal grid (grid 3) of the 12SA7 is switched from the broadcast loop to a short-wave antenna transformer through a 100,000 ohm resistor bypassed by a .004-mfd capacitor. The external antenna is connected to a single-turn loop primary which returns to chassis through the short-wave primary, a .005-mfd capacitor and the avc bus. Another arm of the bandswitch removes the loop from the avc bus and shorts it to prevent absorption in the short-wave

(Continued on page 52)



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Harry Kalber
Sales Manager

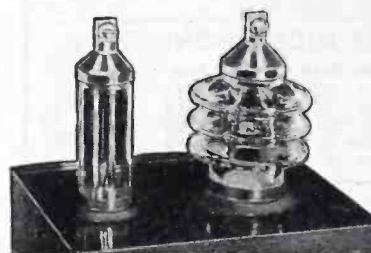
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North Adams, Mass.

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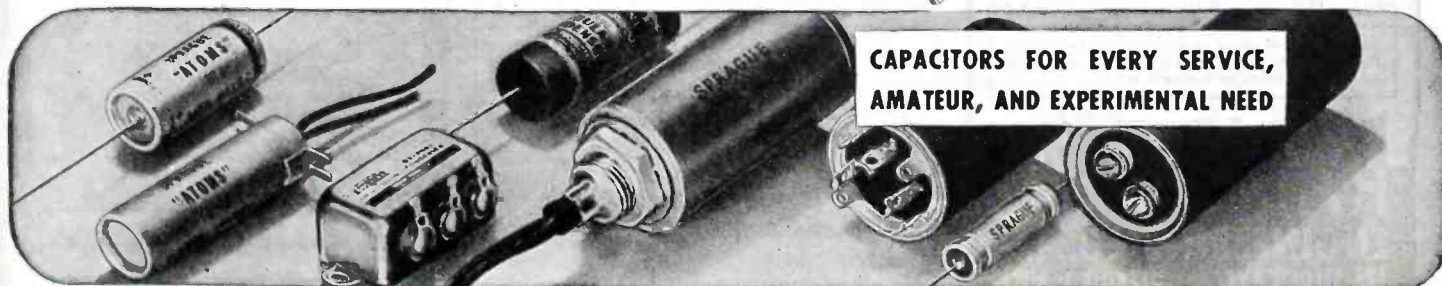
3 *CEROC 200

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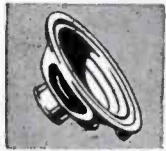
17 Watt	30.30
25 Watt	42.60
35 Watt	54.60
50 Watt	70.50
17 Watt with Phono-top.....	42.30
25 Watt with Phono-top.....	52.20
35 Watt with Record-changer.....	89.10

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Model	Type	Cord	Level	Each
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22X	Crystal	7'	-52	10.88
83X	Crystal	20'	-52	13.23
BD	Dynamic	7'	-52	8.53
83D	Dynamic	20'	-54	14.70



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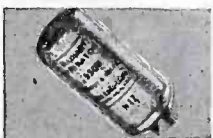
4' PM square.....	\$1.35
4' 450 ohm, square.....	1.40
5' PM 2 watt.....	1.25
5' 450 ohm.....	1.50
10' PM 11 watt.....	7.20
12' PM 16 watt.....	10.14
12' PM 17 watt.....	14.25

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VOLUME-TONE CONTROLS

(Continued from page 31)

may be used, depending on the required resistance values and taper. The reason for using a dual volume control is that due to the particular type of control circuit employed, dual control of two different circuits simultaneously is necessary in order to obtain smooth, even and complete attenuation of all signals.

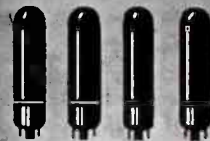
Control Applications

During the transition period of tube and receiver circuit development, some receiver manufacturers used dual or twin controls, usually to control antenna and bias voltage, antenna and screen voltage, antenna and audio, cathode and audio, etc., simultaneously, by operation of a single control shaft. The most popular use was for antenna control by one section and screen-grid control by the other section, the customary values of maximum resistance employed in this case being 10,000 ohms and 100,000 ohms respectively.

Dual control units are commonly employed where the following combinations of control circuits are used:

- (1)—Antenna shunt and bias voltage (volume control).
- (2)—Antenna shunt and screen voltage (volume control).
- (3)—Grid shunt and cathode control (volume control).
- (4)—Audio shunt in push-pull audio (volume control).
- (5)—R-f shunt, screen voltage or audio shunt (volume control), and tone.
- (6)—Audio shunt (volume control), and tone compensation.

Most makes of replacement controls are constructed so that they can either be used separately or assembled in tandem with a common shaft to form dual or triple units to fit any particular need for the simultaneous control of two or more separate circuits. Some makes of controls are so designed that it is possible to even combine wire-wound and composition-element controls together in tandem, where this is necessary to fit a particular control need. Standard switches may also be attached to the outer end of the tandem assembly where needed. The manufacturers of those makes of single controls that are not adaptable for dual mounting usually provide dual- and triple-type controls already made up in combinations of resistance size



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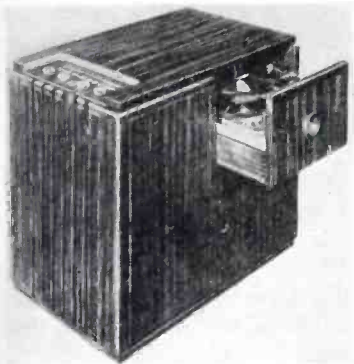
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and tapers to meet most of the popular requirements.

Fig. 5 illustrates a single control, dual-control unit and a triple unit, all made up from the same make and type of control.

(To Be Continued)

POSTWAR RECEIVERS



Above, ECA model 121, 7-tube radio-phonograph combination for 10- and 12-record operation; 8" speaker provided. Below, ECA model 106, 5-tube radio-phonograph for 10- and 12-record use; has built-in lop.



Below, Garod 6A1 a-c/dc super with untuned r-f stage.



Below, John Meck (left) and Henry Hutchins (right) with Meck 5-tube supers, demonstrated at recent press conference in New York City, that are sold through parts distributors.



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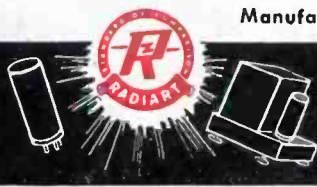
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COMMUNICATIONS RECEIVERS

(Continued from page 13)

form, with no transmitted audio modulation. The tone of the received signal is controlled by varying the frequency of the b-f-o so that the beat note lies within the audio range.

A typical b-f-o circuit is shown in Fig. 1, Hallicrafters SX 28. This circuit uses a 6J5 in a Hartley oscillator. The 25-mmfd tuning capacitor is brought out to the panel for control of the beat note. The output of the oscillator is coupled to the detector,

where it mixes with the i-f signal. In this particular receiver, coupling is accomplished by means of a pair of twisted wires, about 2 or 3 twists, which accounts for the 2 mmfd of coupling capacitance. Any greater coupling would load the detector so that weak i-f signals would not be heard. The b-f-o on-off switch is used to cut off the plate supply to the b-f-o when it is not in use.

Fig. 2 shows the b-f-o used in the

National NHU. Here, a pentode is used in a Hartley oscillator, with the output coupled to the second detector through a special 2-mmfd capacitor; note that the b-f-o on-off switch shorts out the oscillator coil. The rest of the circuit is essentially the same as that in Fig. 1.

Fig. 3 shows the b-f-o used in the R.M.E. 41-43. A 7B6 is used as a combination second detector and b-f-o, with the oscillator signal fed to the low side of the grid input of the second i-f, through a 100-mmfd capacitor. This large value of coupling capacitance is permissible, since the LC circuit of the i-f stage acts as an effective blocking system for the b-f-o signal. Thus, only a small portion of the b-f-o signal reaches the grid of the tube. The grid return of the 7B7 second i-f is unbypassed so as not to short out the b-f-o signal. The b-f-o on-off switch is in the B supply to the oscillator.

All b-f-o circuits are characterized by low-plate and screen-grid voltages. This is done to prevent any of the oscillations from entering the front end of the receiver, or any other place where it can create trouble by causing unwanted beat notes. The circuit must be well shielded for the same reason. Alignment is similar to that followed for i-f systems. Frequency stability of the b-f-o is usually good, since air capacitors are used for tuning. The dial which controls the b-f-o is usually marked 0-10. In aligning, the zero mark is taken as the point of zero beat. An i-f signal is fed into the receiver, and the b-f-o trimmer is adjusted for zero beat at zero on the dial. Advancing the b-f-o control will then produce an audio signal in the output of the receiver.

Coupling may be adjusted by using both a weak and a strong unmodulated i-f signal, to check if beat notes can be produced with both types of signal.

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Control room of the Caserta AFS radio station in Italy through which transcriptions, records and live programs are piped for troops in the Mediterranean Theatre of Operations.

(Courtesy U. S. Signal Corps)

PHOTOELECTRIC CELLS

(Continued from page 15)

sources, and are used with low-value resistances.

Electron-Multiplier Photocells

The electron-multiplier cell is not widely used at all. Essentially, this is a multi-electrode photoemissive cell with the principle of secondary emission. In a typical cell we have seven electrodes, a cathode, nine special plates called dynodes, and the final plate. The dynodes are curved metal plates coated on one side with a mixture of chemicals. This coating is able to emit electrons when a fast moving electron strikes it. The effect is termed secondary emission.

The RCA 931-A is a typical electron-multiplier cell. The dynodes have higher potentials as the steps are increased. Differences of 100 volts between dynodes may be used. As the electrons leave the cathode and move to a dynode, secondary electrons are emitted and may go to another dynode where still other electrons due to secondary emission are released. The effect continues as the electrons move from dynode to dynode. In this way the effect of a small original electron movement is greatly amplified. Current amplification of as much as 200,000 times may be obtained using suitable construction. Cells of this type, however, require inconveniently high, somewhat dangerous, operating voltages. A circuit showing the connections for a typical setup appears in Fig. 4.

FM TUNING INDICATORS

(Continued from page 18)

available voltage for the 6U5G grid.

Espey 2170

Fig. 7 shows the indicator circuit used in Espey model 2170. This system uses a combination of the limiter and discriminator systems, and is an improvement on either the limiter or discriminator systems, since it permits sharper tuning.

Initially, the eye is open. Upon tuning in a signal, two actions occur. The limiter portion acts in conventional manner; as the signal is tuned the voltage between points A and B increases, with point B positive with relation to point A. The discriminator portion of indicator system acts as a form of feedback, in that it supplies cancelling voltage, developed in opposite polarity to the limiter voltage

(Continued on page 50)

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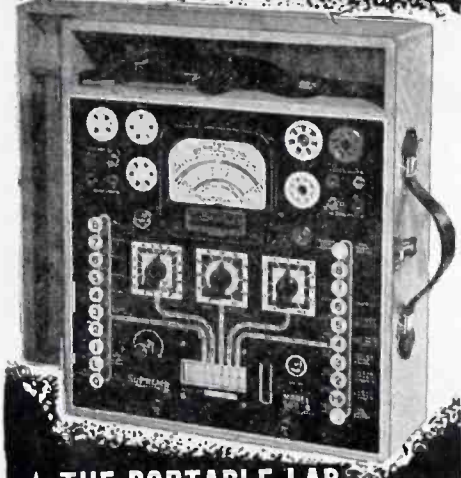
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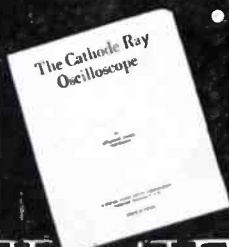


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DC AMPERES: 0-1-10
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0-5-25-100-250-500-1000-2500
AC VOLTS: 0-5-10-50-250-1000
OUTPUT VOLTS: 0-5-10-50-250-1000
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(Continued from page 49)

across R_1 between A and C . The eye-control tube plays an important role in this action. As the desired signal is approached, point E assumes a positive voltage relationship to point D . D_2 of the control diode therefore conducts, and creates a positive voltage across R_1 , which cancels part of the voltage across R_2 , and tends to keep the eye open. As the center frequency is reached, the voltage between points D and E becomes zero, and neither diode conducts. Since no bucking voltage is created across R_1 , the full effect of the voltage across R_2 is imposed on the grid of the 6U5G, and the eye closes. As the receiver is tuned away from the signal, point D becomes more positive than point E . Control diode D_2 then starts to conduct, creating a canceling voltage across R_1 , and opening the eye. Note that in this system we have the same voltage effect when coming into the signal or going away from it, since both create positive voltages.

Another variation of this system combines the biased indicator of Fig. 4 with the eye control system of Fig. 7 to produce a closed eye version without overlapping. The limiter voltage is omitted.

The action of the eye may be used as a guide in the servicing of f-m receivers. The width of swing of the eye is indicative of the strength of the signal being received. Where the eye is used in a balanced system such that it swings twice through the tuning cycle, the alignment of the receiver is indicated by the uniformity of the two swings. Where the two swings are not uniform, an unbalanced i-f or discriminator is indicated.

A hazy edge on the two sections of the fluorescent target is due to a-c in the grid voltage. The usual cause is an open filter capacitor in the indicator's grid supply. If the a-c is being picked up in the lead to the indicator tube, a .1-mfd capacitor from the indicator grid to ground will usually cure the trouble. The addition of a small decoupling resistor in series with the grid lead will often help, if the capacitor alone is not effective. Aging of the tube is indicated by a fading of the fluorescent image in which case the tube should be replaced. An adjustment, usually found in the rear of the receiver, controls the cathode bias of the indicator tube. This control is used to set the two halves of the indicator eye so that they meet. Some idea of receiver sensitivity may be gained by feeding a signal generator into the antenna input and noting at what input voltage the eye closes.

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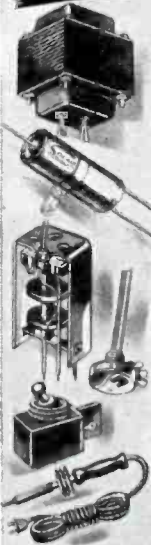
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UNLABELED AMPLIFIER TERMINAL CHART

(See Page 20 for Chart)

THERE are many models of popular commercial p-a amplifiers with unlabeled terminals on input and output speaker plugs, and sockets and terminal strips. In most cases the work of testing or repairing such amplifiers cannot proceed until many hours have been spent tracing out the wiring to such terminals or hunting through the service literature covering the amplifiers.

To solve this problem the unique chart shown in Fig. 1 was recently prepared by the Van Sickle Radio Supply Company. The chart shows unmarked amplifier connections and other necessary data for several of the most popular makes and models of p-a amplifiers.

Alfred A. Ghirardi

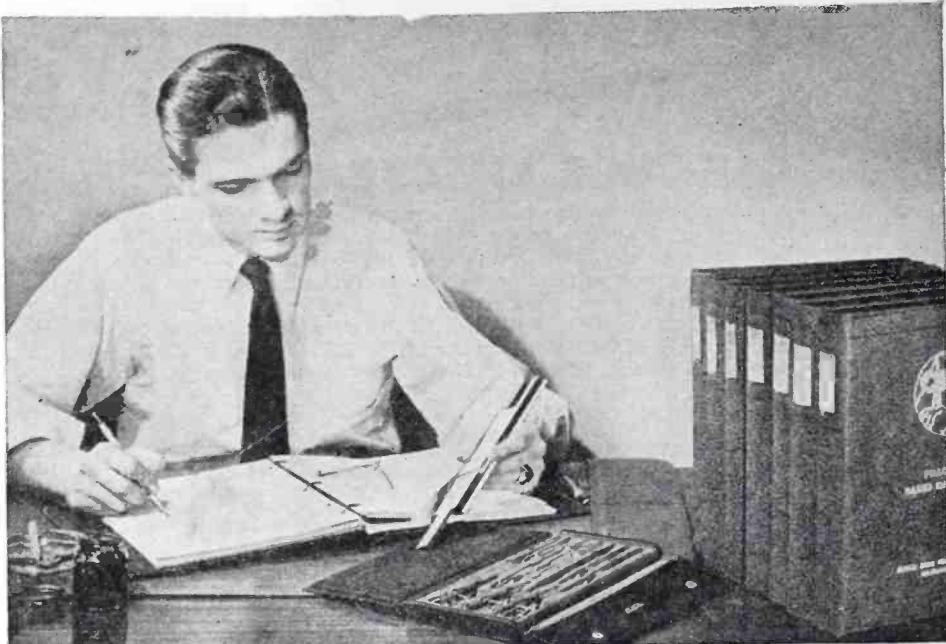
TWO-STAGE RECORD PLAYER

(See Front Cover)

A 2-STAGE record player, Emerson GL-457, featuring a rumble attenuator, is shown on this month's cover. The rumble attenuator in the form of a low-pass filter inserted in a degenerative link. Tracing the circuit from the pickup, which is a crystal type, we come to a series equalizer consisting of a 2.2-megohm resistor shunted by a 220-mmfd capacitor which is connected to the high side of the volume control. A degenerative voltage originating in the speaker voice coil circuit is also fed to the volume control. This voltage is modified by a T-type filter (47,000 ohms, .02-mfd and 1-megohm shunt) so that only the bass notes of the program pass through to the volume control and then to the amplifier. This reduces the net bass amplification which practically eliminates rumble.

In the amplifier we have a grid leak biased 6SQ7 feeding a 25L6 with a tone control across the output. A 100-mmfd capacitor shunts the output of the 6SQ7. Current degeneration is provided for in the power stage through the absence of a bypass capacitor across a 150-ohm bias resistor. The tone control consists of a .05-mfd capacitor in series with 2200 ohms, with a switch across the resistor.

The power supply consists of a 25Z6 with paralleled elements and a 2-stage resistance filter. The speaker field is a shunt type connected directly to the rectifier output; the 25L6 plate is connected to the first filter section and the output screen grid and first audio to the second filter section. The heaters are series connected with ballast resistor tube.



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SER-CUITS

(Continued from page 44)

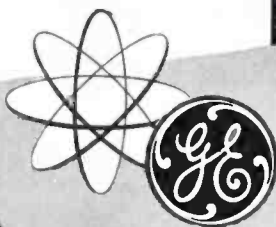
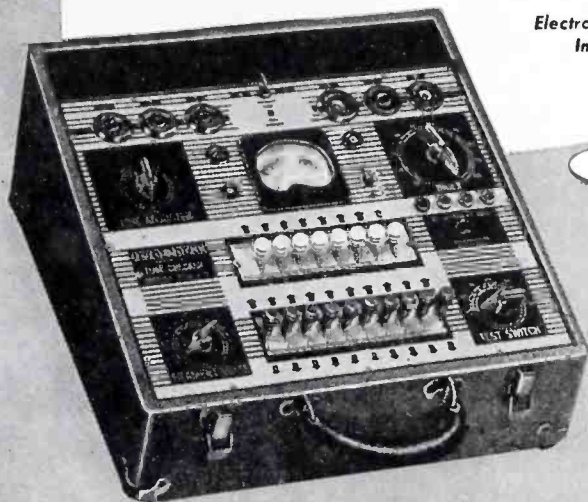
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band. This also permits the loop to aid short-wave pickup through the loop primary turn when no external antenna is employed. The oscillator grid and plate are switched to two oscillation transformers in a conventional manner.

Coronado C1100

An 11-tube, 5-band receiver, Coronado C1100, featuring permeability tuning and shunt coils for bandspread tuning is shown in Fig. 3. The loop circuit contains an iron-core adjustable loading coil, a .002-mfd series capacitor and the low-impedance primary of the short-wave transformer. The external antenna is connected in an unusual manner; fed to the low side of the loop through a high-pass filter consisting of a .0005-mfd capacitor and two 25000-ohm resistors. This is primarily a low-impedance capacity coupling. On the four bandspread short-wave bands, the antenna is connected to the antenna transformer through a .002-mfd series capacitor. The permeability tuned coils are connected in series or parallel with the secondary of the transformer. Thus, one primary serves to couple the various coils for all bands.

Coil Connections

For the 6-mc band, a coil is connected in series with the secondary; the 9-mc band uses the secondary only; the 12-mc band uses one shunt coil across the secondary and the 15-mc band uses another. In the latter three positions, the series coil is shorted to prevent absorption. These various tuned circuits are all coupled to the r-f amplifier grid through a .0005-mfd capacitor. A similar arrangement for bandswitching is used to couple the r-f amplifier to the converter with a single primary serving all short-wave bands. On broadcast, a 5,000-ohm plate resistor is used in combination with a 10-mmfd coupling capacitor to the converter grid and permeability tuned circuit.

Oscillator Frequency Control

In switching the oscillator frequency, similar series and shunt coils are employed but it is necessary to increase the feedback as the frequency is increased to obtain sufficient output. This is accomplished by a selection of three taps on the main oscillator coil. Two 6SK7 i-f amplifiers are used with resistance coupling between the stages.

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The detector i-f transformer has a tap for connecting the diode to decrease the loading, or increase the Q of the transformer.

The audio amplifier consists of a 6SQ7, a second stage 6SQ7, 6J5 inverter and push-pull 6V6s. The first stage uses a 1.25-volt bias cell, the second resistance bias from a potentiometer in the voice coil circuit which feeds a degenerative voltage to the second stage cathode. Separate treble and bass-tone controls are located at the output of the first audio, the treble hunting series resistors with small capacitors to emphasize highs. (.0003 mfd and .000125 mfd) while the bass control connects shunting resistors or combinations of shunt resistors and capacitors.

List of parts for the Coronado 1100 diagrammed on page 44.

RESISTORS

R1	25M ohm— $\frac{1}{2}$ w.
R2	25M ohm— $\frac{1}{2}$ w.
R3	1 megohm— $\frac{1}{2}$ w.
R4	250 ohm— $\frac{1}{2}$ w.
R5	5M ohm— $\frac{1}{2}$ w.
R6	1 megohm— $\frac{1}{2}$ w.
R7	25M ohm— $\frac{1}{2}$ w.
R8	6M ohm—2 watt
R9	10M—2 watt
R10	1 megohm in tuning indicator cable
R11	700 ohm— $\frac{1}{2}$ w.
R12	10M ohm— $\frac{1}{2}$ w.
R13	1500 ohm— $\frac{1}{2}$ w.
R14	1500 ohm— $\frac{1}{2}$ w.
R15	2M ohm— $\frac{1}{2}$ w.
R16	1 megohm— $\frac{1}{2}$ w.
R17	100M ohm— $\frac{1}{2}$ w.
R18	500M ohm— $\frac{1}{2}$ w.
R19	250 ohm—2 watt
R20	500M ohm— $\frac{1}{2}$ w.
R21	100M ohm— $\frac{1}{2}$ w.
R22	400M ohm— $\frac{1}{2}$ w.
R23	500M ohm volume control and line switch (S4)
R24	15M ohm— $\frac{1}{2}$ w.
R25	50M ohm— $\frac{1}{2}$ w.
R26	5M ohm— $\frac{1}{2}$ w.
R27	50M ohm— $\frac{1}{2}$ w.
R28	500M ohm— $\frac{1}{2}$ w.
R29	250M ohm— $\frac{1}{2}$ w.
R30	500M ohm— $\frac{1}{2}$ w.
R31	250M ohm— $\frac{1}{2}$ w.
R32	40M ohm— $\frac{1}{2}$ w.
R33	150M ohm— $\frac{1}{2}$ w.
R34	350M ohm— $\frac{1}{2}$ w.
R35	250M ohm— $\frac{1}{2}$ w.
R36	50 ohm— $\frac{1}{2}$ w.
R37	150M ohm— $\frac{1}{2}$ w.

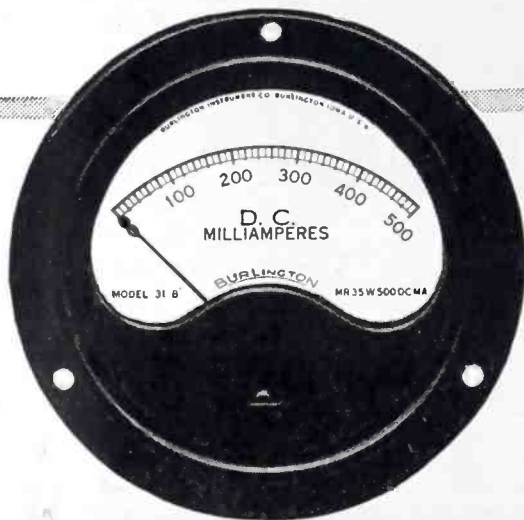
CONDENSERS

C1	.0005 mica
C2	.002 x 600 v.
C3	B.C. Antenna Trimmer
C4	9 mc. Antenna Trimmer
C5	.0005 mica
C6	.1 x 200 v. Tubular
C7	.00001 mica
C8	9 mc. R.F. Trimmer
C9	B.C. R.F. Trimmer
C10	.1 x 400 v.
C11	.1 x 400 v.
C12	.02 x 600 v.
C13	.0005 mica
C14	.02 x 600 v.
C15	30.0 mfd. lytic
C16	B.C. Oscillator Trimmer
C17	30.0 mfd. lytic x 450 v.w.
C18	.0002 silver mica
C19	.00005 mica
C20	9 mc. Oscillator Trimmer
C21	10.0 mfd. lytic
C22	16 mfd. x 350 v.w.
C23	.015 x 600 v.
C24	.015 x 600 v.
C25	.1 x 400 v.
C26	.05 x 200 v.
C27	.05 x 400 v.
C28	.05 x 200 v.
C29	.0001 mica
C30	.0001 mica
C31	.1 x 200 v.
C32	.0005 mica
C33	.00025 mica
C34	.1 x 400 v.
C35	.05 x 400 v.
C36	.008 x 600 v.
C37	.0003 mica
C38	.000125 mica
C39	.003 x 600 v.
C40	.00025 mica

C3 and C4 in same unit
C15, C17 and C21 in same unit
C29 and C30 in same unit

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- A.C. voltmeter: 0-10-100-500-1000 volts.
- Output voltmeter: 0-10-100-500-1000 volts.
- D.C. milliammeter: 0-1-10-100-1000 milliamperes.
- D.C. ammeter: 0-10 amperes.
- Ohmmeter: 0-500-100,000 ohm, 1 megohm.
- Decibel meter: minus 8 to plus 55 decibels.

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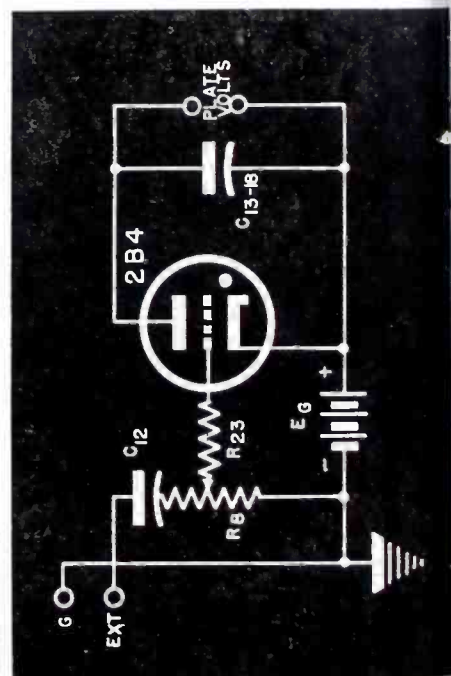
C-R OSCILLOGRAPH!

(Continued from page 36)

cient to provide full deflection of the fluorescent spot, it is necessary that the output voltage of the oscillator be amplified before application to the horizontal plate system. Consequently, in the oscillograph circuit diagram of Fig. 2,¹ the control switch S_2 is provided to introduce the voltage output of the linear time-base oscillator into the grid circuit of the horizontal voltage amplifier, providing amplification of the linear time-base voltage. Further, the linear time-base control switch S_2 is so arranged that the horizontal amplifier may be directly connected to the external signal input system comprising the input terminals I and G , and the circuit or capacitor discharge resistor R_s , the switching circuit providing utilization of the horizontal gain-control potentiometer in either instance.

In the practical oscillograph, the linear time-base oscillator output voltage effects a constant deflection of the luminous spot on the screen during the capacitor charging period. If simultaneously with the charging of the linear time-base oscillation output voltage rise, the vertical amplification circuit causes the luminous spot to vary with respect to the vertical deflection axis, the luminous spot writes an image of the resulting waveform on the screen. This action is recurrent since the beam returns to the initial position when the charge on the capacitor is relaxed. Further, because of the extremely short duration of the

Fig. 3. The Du Mont linear time base synchronizing system. A portion of the signal voltage or the variation under analysis is utilized to modulate the thyratron negative d-c grid-to-cathode biasing voltage.



duration period, the return trace written on the screen is all but invisible. However, particularly where the near time base oscillates at a very low frequency, the return trace is sufficiently pronounced to effect distortion of the wave image written on the screen, being plainly visible as a phantom base line to the waveform under observation. Again, where the frequency of the vertical amplifier voltage output is a few kc, a spurious wave image is perceptible in the completely written wave image, inasmuch as a complete wave of a voltage of this order may often be written in the time period required for the return of the cathode-ray beam to the original deflection position.

In the Du Mont oscillograph a return trace blanking circuit is provided. This suppresses the cathode-ray beam during the period the charge on the linear time-base timing capacitor is reaxed. This blanking circuit is shown in elementary form in Fig. 3. We note here that the linear time-base voltage output is dynamically coupled to the control grid of the c-r tube through application of a resistance-capacitance coupling system.

In the return-trace blanking circuit shown in Fig. 3, the dynamic coupling capacitor and the resistor are so selected that the coupling system forms a conventional *hi-pass* filtering stage. This serves to transmit to the grid circuit only those voltage variations which occur within a few microseconds, i.e.; the circuit is so arranged that the impedance of the capacitor to low frequencies is comparatively high. Thus, during the timing-capacitor C_{2-3} charging period, in which the beam of the oscillograph provides a linear base for the waveform under observation, the coupling capacitor C_{11} charges very slowly, and the resultant charge current through this capacitor develops little voltage across the series-grid resistor R_6 . Further, since the potential across the series-grid resistor is small, the effect of the grid control on the intensity of the beam current is also negligible, and the luminous intensity of the writing spot is not visibly affected.

With the relaxation of the timing capacitor charge, the plate potential of the thyatron 2B4 falls to the characteristic arc-drop limit, and the coupling capacitor C_{11} , in Fig. 3, discharges rapidly through the atmosphere of the tube and the c-r tube series-grid resistor. The resulting discharge current develops a considerable negative potential across the series grid resistor R_6 , which drives the control grid considerably negative. Here, the

(Continued on page 61)

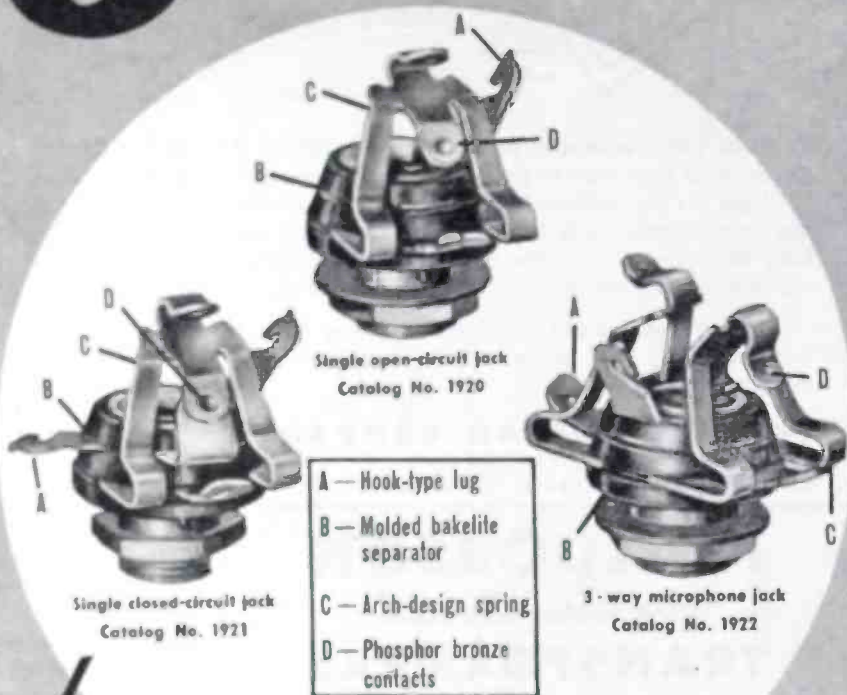


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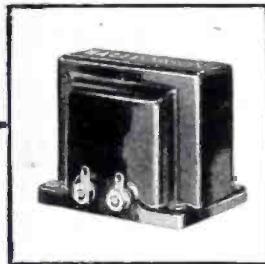
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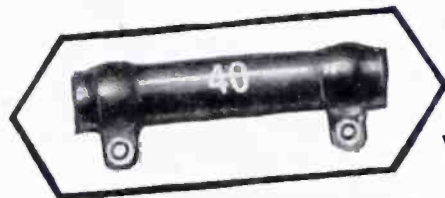
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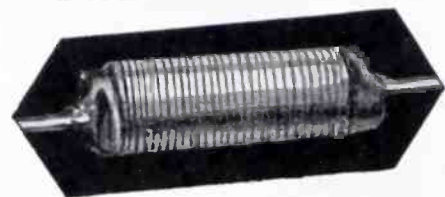
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OLD TIMER'
CORNER

by **SERVICER**

THEY used to tell me that it was the early bird that got the worm and for a long time I used to see birds getting worms at all hours of the day, and hence got to thinking that perhaps there was not much to that old adage. But when I heard about what Tommy had done I found that the store had a ring of truth to it after all.

While I don't visit Tommy's store very often, it's way over to the north end of town, I had been bumping into that young man every now and then in the odder places. Once I saw him in the poorer section of town. He was carrying two broken-down midgets—one under each arm—and yet he shouted a cheery greeting. We stopped and talked, and I told him that he had just bought two midgets for \$2 each. Both looked quite awful. The cases were half gone and parts were spilling out. I said nothing except that I couldn't imagine how he could salvage anything from those ancient sets. Tommy just smiled, and said that he had an *Idea*, with a capital I.

Then later in that week I ran into Tommy coming out of our bank president's home. Again he had a couple of midgets under his arm. They were not the ones he had bought in the other part of town, either. They were just as bad as the others. He told me he had paid \$1 each for them. But he had also repaired the president's fine parlor console. Net result for the call, said Tommy, was a profit of about \$12 even after paying for the midgets. But, whispered Tommy that still wasn't the *idea* he mentioned earlier. So I was more puzzled than ever.

A little later I met Tommy coming out of our best restaurant. This time he had or was trying to juggle, about 5 midgets. And their condition was bad, very bad. I asked him how he found all these museum pieces in the restaurant. He told me that the owner had been telling his customers, especially those who came in regularly, that they should leave their midgets with him and that Tommy would pick them up and pay for them at a maximum rate of \$2 each if they had all their parts and tubes, even if they would not play and even if they had broken cases.

My curiosity was so aroused that I finally had to ask just what this *idea* was all about. He asked me to hop into his car and he would take me over to his shop where we could talk.

Well, you should have seen the midgets he had collected. They were all over the place. Guess there must have been at least a hundred. They were of all kinds. And it seemed that there wasn't one there that could play at all.

Tommy also had a large assortment of the oldest timers you have ever seen.

These, too, were in a sad state of disrepair.

"Now, Tommy, what does all this mean?"

"Gonna sell 'em," he replied.

"How in the world do you expect to sell all that junk?" I countered.

"Well," Tommy went on, "I can do quite a bit with these sets. They may not sound so good, but that won't matter, for the use for these sets is such that the sound doesn't have to be too good. And the appearance isn't important either, because the listeners won't care one way or another. Guess I'll get rid of at least 50 of them tomorrow. Want to help me fix them a bit, and I'll declare you in for some of the profits?"

"I guess so," I said. Frankly it was all quite a mystery—tone unimportant, appearance secondary.

We worked the rest of the day fixing up the sets. They just had to be able to receive the local station only, said Tommy. We did everything for that. Regardless of how the set worked on other stations, we concentrated on the local station and peaked the sets so that it came in loud, even if not too clearly.

After 10 P.M. we took some time out for a bite, and then back to work again. Soon we had about 50 of the midgets fixed so that they received the local station very well.

Then Tommy came over and told me to take of the tuning knob and saw the tuning shaft off flush with the cabinet (if there was one) or flush with the edge of the chassis (if there was no cabinet). That got me; how were they to be tuned?

Nor was that all; Tommy then flattened each shaft on one side with a file and we loaded the sets into his car.

"Meet me at 4 A. M. tomorrow," Tommy said, "and I'll show you how to get \$10.00 for each one of these, and pick up some extra work, too. Bring your tools and portable testers!"

Well rising at that early hour wasn't the easiest thing to do, but I managed to make it by the skin of my teeth. Tommy was already sitting in the car waiting with the motor idling when I dashed up.

"How about some food?" was my first question.

"Show you where you'll get the finest breakfast you ever tasted. But you'll have to be patient. It may take quite awhile," Tommy said.

"OK," I grumbled.

We turned out into the country and soon we were riding along nicely through the crisp morning air. It was really good to see the sun rise over the low hills, and I must admit that it had been a long time since I had seen that.

Soon Tommy turned off onto a dirt road and we drove, smoking our cigarettes in silence. Suddenly around a bend we came upon old O'Reilly's farm and Tommy drew up in front. Mr. O'Reilly was standing there looking at his hired man fetching some kerosene out of the tank in the yard.

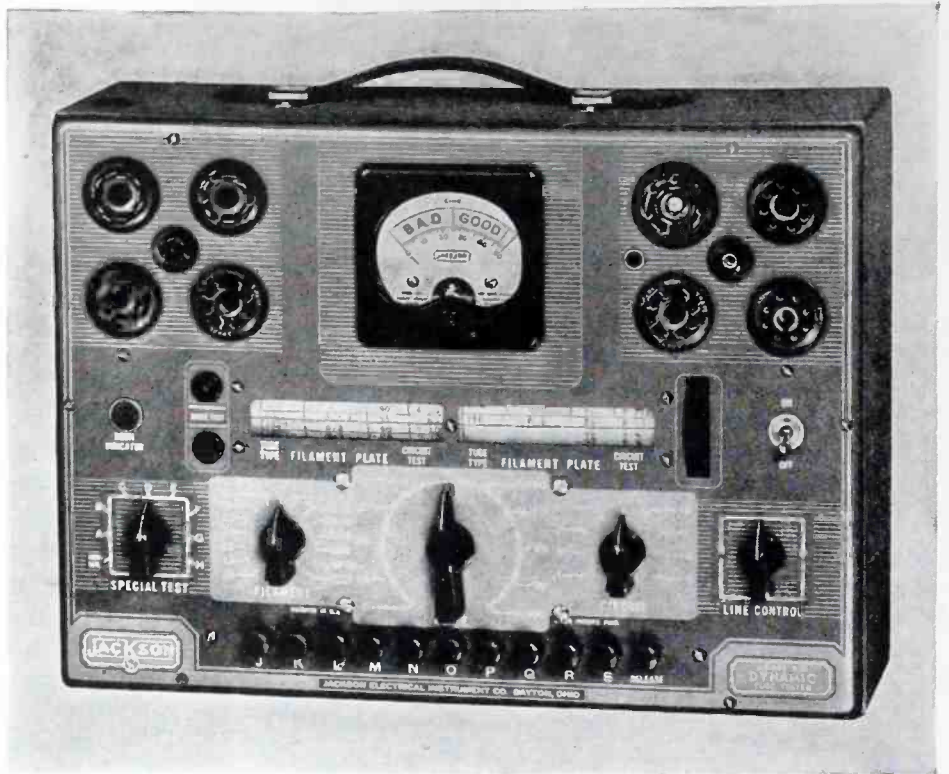
"Morning, Mr. O'Reilly," said Tommy.

"Morning, Tom. Well, I see that you got here just in time for breakfast. Who is that with you, your helper?"

"Sort-of," Tommy rejoined, "and we're both hungry as bears."

Well we went into the kitchen where we had the best breakfast I had tasted

(Continued on page 60)



Model 636 Dynamic* Tube Tester

With Built In Rotary Tube Chart

Tops in design and performance including the latest Jackson patented switching circuits.

Modern in every feature of construction, appearance and operation.

Complete with every valuable feature. Up to date for all newest tube types.

SPECIFICATIONS

"Dynamic" Method of Test—Makes a better test on every tube. The "Dynamic" method is more accurate, frequently finding "poor" tubes which might pass for "good" in ordinary testers.

Tests All Tubes—All of the popular receiving types and television amplifiers, including *Bamtuams—Loctals—Single Ended—High Voltage Filament Types and Miniatuvs*. Provision for many more. The tester

is protected against obsolescence in every possible feature.

Roll Chart tube index—simplifies correct settings.

Full Range Filament Selection—marked directly in volts.

• • •

Bench Model 636-B (illustrated) is installed in welded steel cabinet. This instrument is also furnished (portable model 636) in a French grey leatherette case with removable lid—matched in dimensions and finish to other testing instruments in the Jackson line. It can be assembled with them in the Jackson Service Lab. Buy now with an eye ahead—on a *matched* Jackson testing set.

*TRADE MARK REG.

BUY WAR BONDS AND STAMPS TODAY

JACKSON

Fine Electrical Testing Instruments

JACKSON ELECTRICAL INSTRUMENT COMPANY, DAYTON, OHIO

SERVICE, OCTOBER, 1945 • 57

SUPERHETERODYNE MIXERS

(Continued from page 26)

and ground. The oscillator has a similar bandswitch with only two plate oscillator coils used. An oscillator decoupling filter is also used. This con-

sists of a 10,000-ohm and .05-mfd combination. It bypasses the oscillator voltage so that none of this voltage appears in the *B* supply circuit.

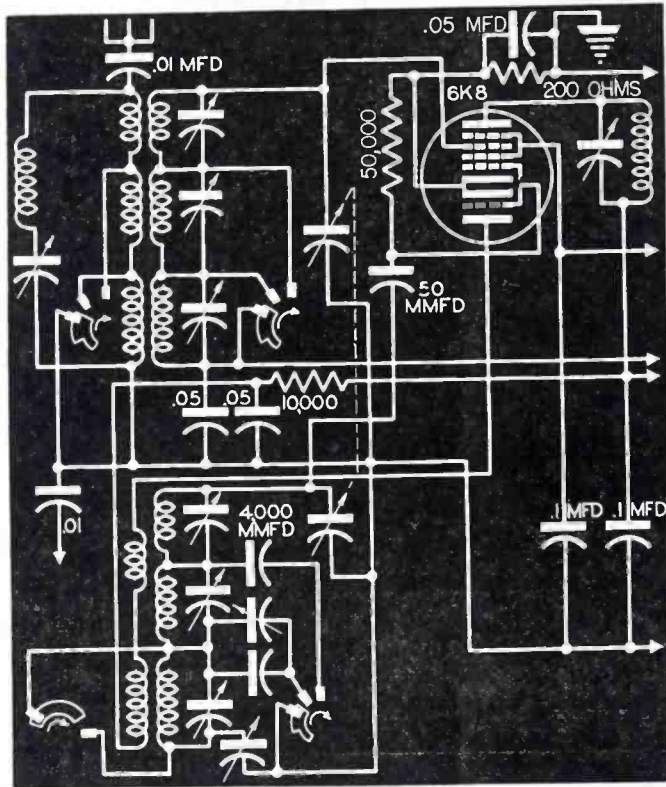
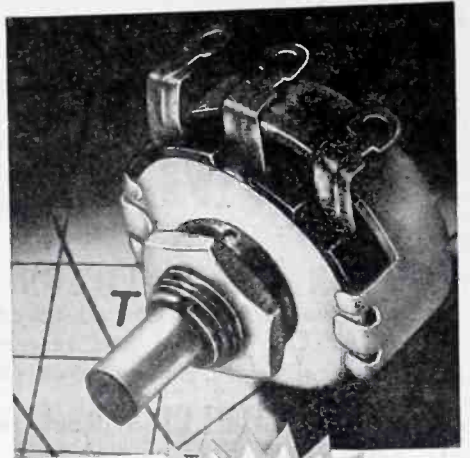


Fig. 9. Allied E-0707. The use of a diode-hexode for mixing permits receiver operation at frequencies up to 40 mc. The oscillator decoupling filter consisting of a .05-mfd capacitor and a 10,000-ohm resistor prevents the r-f developed by the oscillator from entering the *B* supply.



It's a
CLAROSTAT!

★ And that tells the story. For Clarostat is the name and guarantee of a better composition-element control such as is now found in the finest radio-electronic assemblies where trouble and failure just can't be tolerated.

The *stabilized* element, exclusive in Clarostat controls, sets new performance standards. Extreme immunity to humidity, temperature and other severe climatic conditions. Rated at 1 watt. Resistance values of 500 ohms to 5 megohms. With or without power switch.

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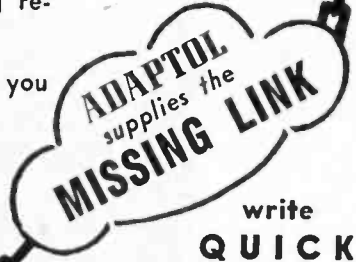
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RADIO

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QUICK
for the
WHOLE STORY

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Bad modulation hum: Found the trouble in the .05-mfd bypass capacitor in the avc circuit at the low end of the antenna-grid coil. This capacitor offers considerable reactance to the 60-cycle hum and builds up sufficient voltage to modulate the signal in the first tube.

Inserting any resistor, 50,000 ohms or higher, from the antenna to chassis removes this hum modulation with less than 5% signal attenuation.

On the underwriters approved models of this circuit it may be necessary to return the resistor to the common side of the a-c line.—R. G. Chrouch.

OLD TIMER'S CORNER (Continued from page 57)

in many a year. I was still curious as to what Tommy had up his sleeve about the midgets, when Mr. O'Reilly suddenly asked, "Bring the sets with you, Tom?"

"Sure thing."
"Well let's get out into the barn and set them up."

So that was it! Seems like Tommy
(Continued on page 61)

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0-1.25-5-25-125-500-2500 Volts, at 20,000 ohms per volt for greater accuracy on Television and other high resistance D.C. circuits.

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0-2.5-10-50-250-1000-5000 Volts, at 10,000 ohms per volt.

OHM—MEGOHMS

0-400 ohms (60 ohms center scale)
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DIRECT READING OUTPUT LEVEL DECIBEL RANGES

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TEMPERATURE COMPENSATED CIRCUIT FOR ALL CURRENT RANGES D.C. MICRO-AMPERES

0-50 Microamperes, at 250 M.V.

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For greater reading accuracy on the Triplet RED DOT Lifetime Guaranteed meter.

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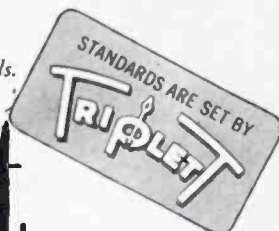
Greater Ease in changing ranges.

Write for descriptive folder giving full technical details.

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RADIO EQUIPMENT CO. 1415 W. FRANKLIN AVE.
MINNEAPOLIS 5, MINN.

OLD TIMER'S CORNER

(Continued from page 60)

ad found out that the cows liked music and might give a bit more milk or something like that. Tommy had gone to the trouble to write the State College of Agriculture to verify and they had written him that while they couldn't be sure it would work, it was well-known that animals were more docile under the tones of music than without, and it certainly would not do any harm.

So Tommy had canvassed the farms around the town and had sold the farmers these old sets for a flat \$10 each installed. Since there was no reason to blame them, and since the cows were not so particular about the set's appearance as was only necessary to find a set that would received a station. With the flat-

tened shaft they could be adjusted just enough to be tuned right on the nose.

The taking off of the tuning knobs prevented the farmers from tuning the sets to other stations which might not come in as well, and at the same time Tommy made it clear that the sets were supposed to be used with only one station.

We left Mr. O'Reilly's with \$70.00 in our pockets, and seven sets sold and installed. Also Tommy stopped to fix their console which netted him another \$7.50.

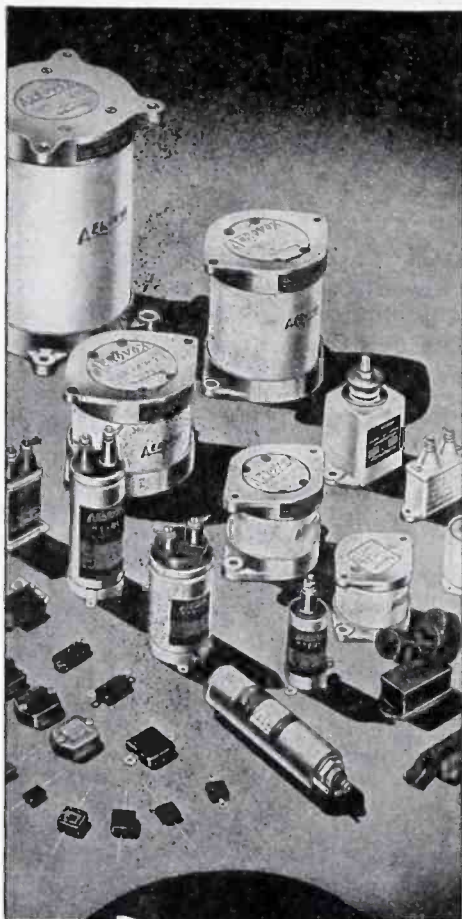
It was dark when we returned to the store. Every set had been sold. Tommy got out a sheet of paper and figured. We had taken in \$500.00 for the sets, and a little over \$97 in service work. Solemnly he handed me \$100 for my day's efforts.

Nice work if you can get it!

C-R OSCILLOGRAPHS

(Continued from page 55)

high negative grid bias potential present across the terminals of the series grid resistor effectively suppresses the electron beam, and the luminous spot which writes the wave pattern on the tube screen disappears for the duration of the existence of this voltage. The electron beam is suppressed in *synchronism* with the relaxations of the linear time-base timing capacitor charge, and the visible trace written by the beam ceases during the period in which each relaxation occurs; it is not visible in the complete wave pattern which the beam writes on the screen.



Post-war Parade

● Hats off to these veterans! They have served with rare distinction on many battle fronts — on land, on sea, and in the air. And now that the needs of our fighting men have been fully met and the victory clinched, these heavy-duty mica, oil-filled, paper and electrolytic capacitors are once more becoming generally available. Because of their outstanding wartime service, they will be still better prepared to meet those heavy-duty service requirements of post-war radio and electronics. ● Consult our local jobber. Or write us.



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 In Canada: AEROVOX CANADA LTO., HAMILTON, ONT.
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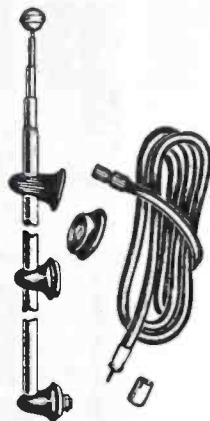
NEW PRODUCTS

RADIART ANTENNAS

Antennas, DeLuxe CF, featuring two short, one long and one wedge type, adapter insulators to fit curved or straight cowls and fenders, with a 50" lead, have been announced by The Radiart Corp., Cleveland, Ohio. The rod assembly has a top rod of stainless steel. Tubular sections are of antimonial admiralty brass which is said to resist salt air and spray corrosion.

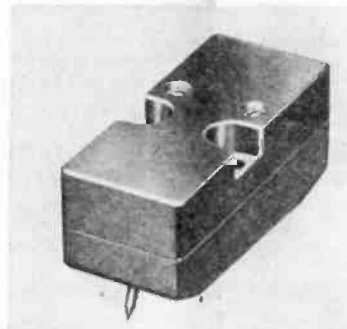
Leads are of Plasti-Loom, which is said to be impervious to moisture. The inner conductor is covered by polyethelene tubing which is then tape wrapped and covered with a closely woven copper shield, and the whole loom is then coated with an extrusion of abrasion resistant vinlyte.

Mounting insulators are of Durez. Other features are: static muffler ball, phosphor bronze anti-rattler and single-pin connector with bayonet adapter.



CALTRON MAGNETIC PHONO PICKUPS

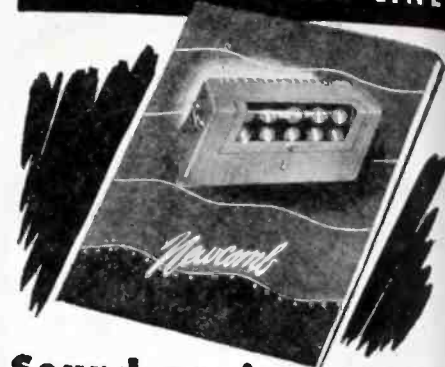
A high-fidelity magnetic phonograph pickup with no bearings, pivots or needle chuck has been produced by the Caltron Company, 11746 West Pico Boulevard, Los Angeles 34, California. It is stated the unit will track fully modulated pressings with 15 grams needle pressure.



TRIPLETT TUBE TESTER

A tube tester, model 2143, featuring a flexible test circuit for tube-values, short and open-element tests, and a trans-

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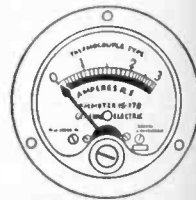


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VACO DRIVER**

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TO

HELP YOU

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VACO TYPES

Yes. Vaco has created more than just a variety of screw drivers. Vaco has built the exact type of screw driver to do the particular job that can be tedious and troublesome when an ordinary driver is used. No wonder mechanics who do precision work say Vacos are "tops" among all drivers. Vacos, with gleaming Amberyl handles, are shock-proof and break-proof. Write for catalog.

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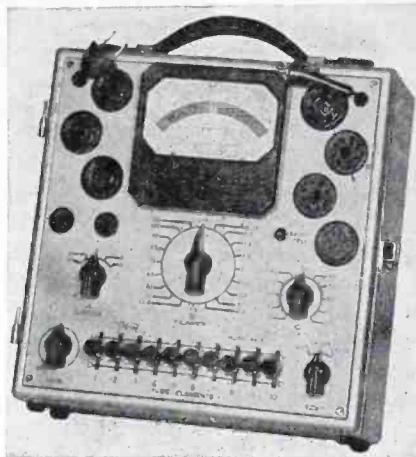
SHEFFIELD RADIO CO.

917 Belmont Ave., Chicago 14, Ill.

conductance comparison check for matching tubes, has been produced by The Triplett Electrical Instrument Co., Bluffton, Ohio.

Has three-position lever switching and multi-color scale to determine tube condition.

Size, 10" x 10" x 5 3/4".



**GENERAL TRANSFORMER PORTABLE
POWER SUPPLY**

A portable power supply for 4-, 5-, or 6-tube, 1 1/2-volt battery farm or portable radios, operating off 105-125 volt, 50-60 cycle lines has been announced by General Transformer Corporation, 1250 West Van Buren St., Chicago 7, Ill.

Provides A; 1.5 v at 200 ma, 1.35 v at 250 ma, 1.55 v at 300 ma, 1.35 v at 350 ma; B; 90 v at 13 ma, and 101 v at 8.5 ma.

Two section A filter is composed of three high-capacity capacitors, and two oversized iron core chokes; B has two high-capacity capacitors and oversized choke.

Universal sockets for battery plugs. Weighs 4 1/2 pounds. Size, 2 1/8" x 4 1/2" x 6 3/4".



INSULINE AUTO ANTENNAS

Several new auto antenna models have been announced by Insuline Corporation of America, Long Island City, N. Y.

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Portable Phonograph Case of sturdy durable plywood, in handsome brown leatherette finish. Inside dimensions 16 1/2" long, 14" wide, 9 1/2" high. Has blank motor board. As illustrated above, specially priced at **\$6.95**



Portable Phonograph Case in brown leatherette covering. Inside dimensions 17 1/2" long, 13" wide, 7 1/2" high. Has blank motor board and opening for speaker. As illustrated at left, specially priced at **\$7.95**

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#8	17"	L x 9"	H x 9 1/2"	D \$4.50
#9	21"	L x 9 1/2"	H x 10 1/2"	D \$5.50

*Speaker Opening in center of front side. Cabinets available in ivory color and Swedish Modern. Write for prices.

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4, 5, or 6 Tube—6.3 V at 2 amp	\$2.45
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70 Mill Power Transformer.....	\$2.65

All types of radio cabinets, equipment and parts are available at Lake's lower prices. A large stock is listed in our catalog.



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Handles AC and DC Voltmeter, DC Milliammeter, High and Low range Ohmmeter. Size 5 1/4 x 8 x 3 3/4" meter with sturdy D'Aronval movement.

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\$18.75 Less Leads

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Sincerely,
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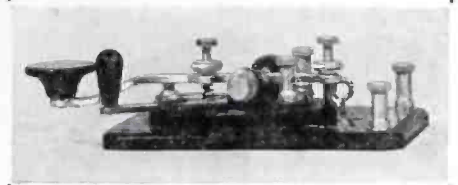


Wholesale RADIO LABORATORIES

JOTS AND FLASHES

THE Muter Company, 1255 South Michigan Avenue, Chicago, has purchased the Rola Company, Inc., Cleveland. Larry King, formerly with Operadio, has been named president and general manager of Rola. Ben Engholm, former president of Rola, will act as a consultant for Rola. . . . Simplex Radio Corporation, Sandusky, Ohio, will hereafter be known as the Philco Corporation of Ohio. . . . H. B. Fisher has become president of a new distributing unit, the Northwest Distributing Company of Minneapolis, 1012 LaSalle Avenue. Mr. Fisher was formerly with the O'Donnell Motor Co. L. G. Miner will be sales manager. . . . Jack T. Dalton has been named manager of distribution of Bendix home radios. W. H. Autenreith succeeds Mr. Dalton as district manager for the metropolitan New York area, including Newark and Newburgh. . . . Chambers Radio Supply Company, 1104 Broadway, Cincinnati, will distribute Lear home receivers in the Cincinnati area. E. L. Chambers is owner of the supply company. . . . An "E" has been awarded to the Eastern Amplifier Corporation.

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Genuine U. S. Signal Corps key with switch to close contacts, polished durable enameled metal base mounted on a bakelite base, key lever is nickel-plated brass-silver contacts; packed in new, original boxes. Shipping, weight, **\$1.29** 1 lb. 10 for \$11.00 ea.

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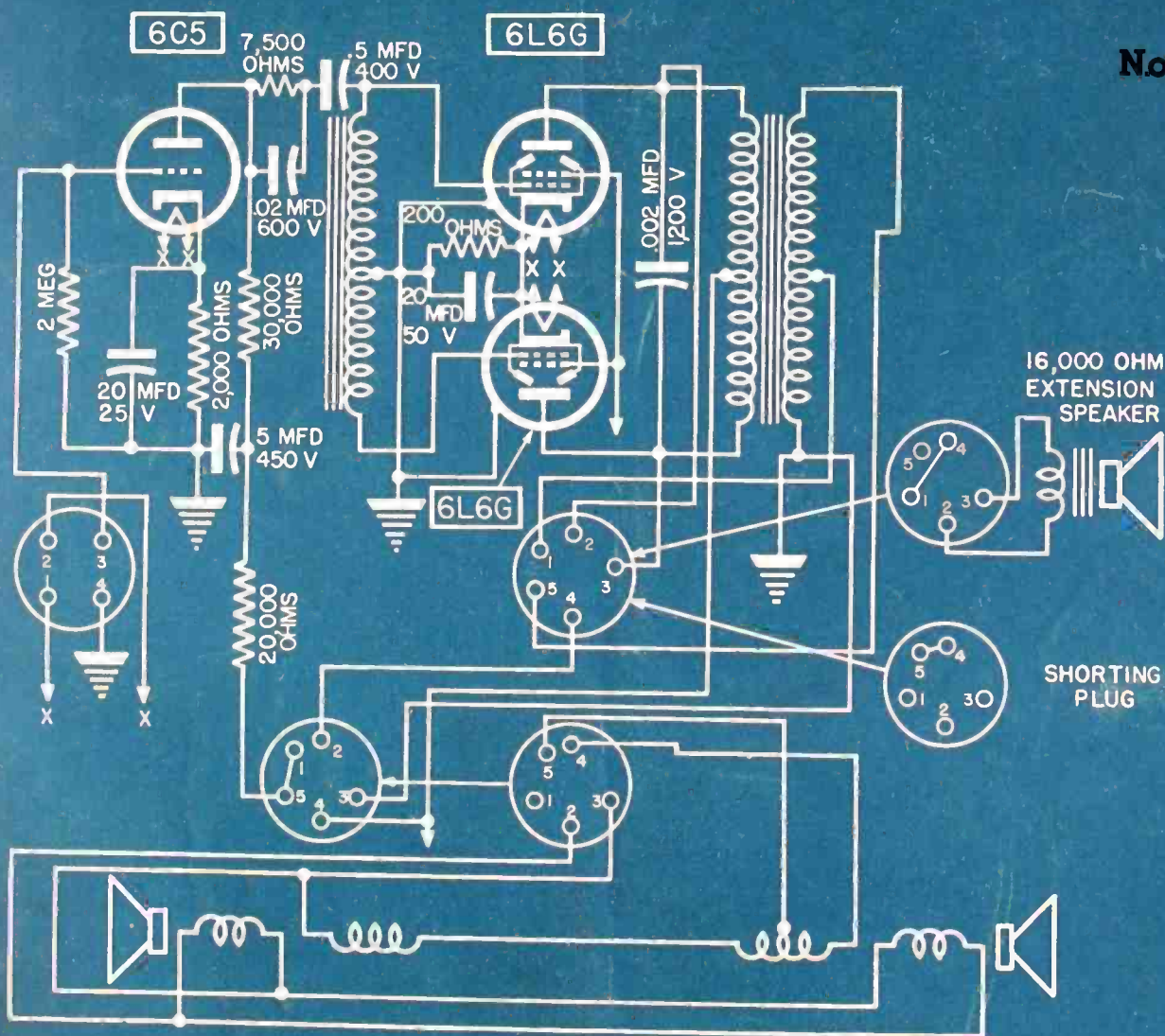


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SERVICE

November
1945



High-fidelity 25-watt amplifier featuring bass-reducing control and provision for dual speaker operation. (See pages 46 and 47.)

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He's not a stunt man. Just a regular radio guy like you and all the others. The reason he rides so easy is that he gets a good head start . . . keeps his nose to the ground, but has his eyes wide open. Every month he pinches a couple of minutes off his working time to read the C-D Capacitor and get the tip-off on short cuts in servicing.

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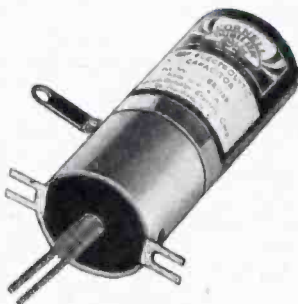
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THE intensive postwar expansion plans of the aircraft industry, indicating a production of around 50,000 planes for civilian travel, projects many unusual opportunities for the Service Man. For this large program will require wide-scale installation, servicing, and maintenance facilities for the planes' receivers and transmitters . . . a program that will tax the present facilities.

Servicing of this equipment will, of course, demand not only a specialized knowledge of aircraft units, but the acquiring of either of two licenses; a first-class commercial license for transmitter tests and a CAA license to permit testing of equipment, as well as installation, or any necessary plane alteration to accommodate equipment changes. While these license examinations will require schooling and hours of study, the results should prove quite profitable.

The hundreds of airports scheduled for construction will demand one or more shops on the field for radio equipment servicing. Such servicing will call for quite a profitable rate structure, commensurate with the specialized training needed for the aircraft activities. In most instances, it will be possible to arrange for a weekly maintenance and service fee, since some equipment will require checkups quite often.

Components, accessories and battery sales will also be a profitable feature of aircraft service shops. Battery sales alone will be substantial, since all planes will use battery-operated units, dry and wet. The wet-cell batteries will require charging, another medium of income.

The CAA has published a list of current airports and will soon publish a list of those airports to be constructed. You can secure such listings from the CAA department of information.

Aircraft radio servicing offers many advantages. Study its possibilities in your community now.

THE postwar f-m receivers covering the new bands are scheduled to feature an unusual tuning-dial numbering system. The first frequency (88.1 mc) will be designated as 201. The second assignment (88.3 mc) will be known as 202. This will continue up to 300. It had been planned to begin with 1 for the first channel, but the FCC said that the bands may be extended up or below the new assignments and thus provision should be made for such extensions.

This is a standard that will undoubtedly be adopted by all manufacturers to simplify f-m tuning. A wise move!

LEWIS WINNER

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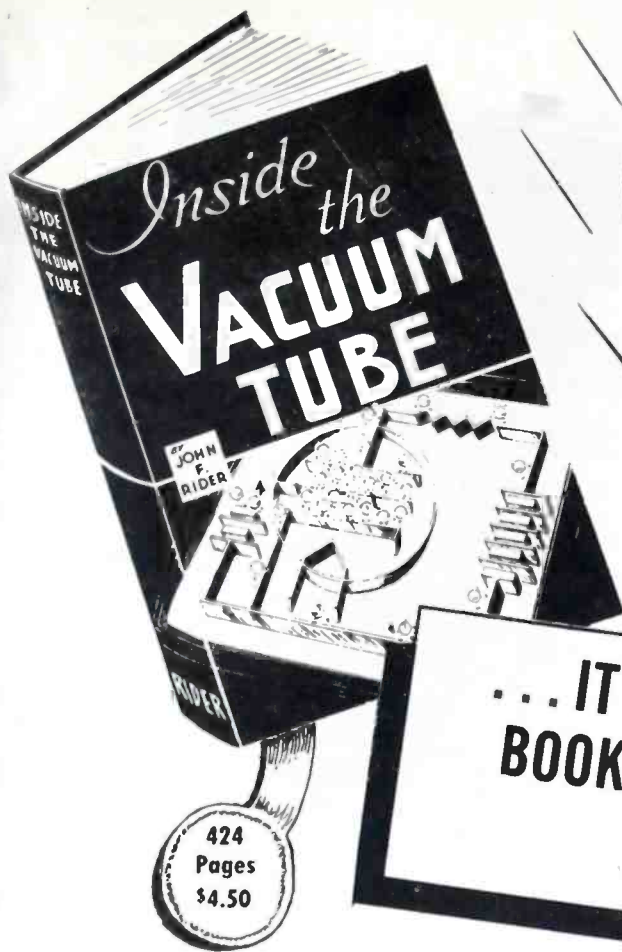


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This is not just another book on the vacuum tube, but a typical Rider Book, offering a new approach to the subject—presented with a technique that makes its message clear and easy to understand. Here is a solid, elementary concept of the theory and operation of the basic types of vacuum tubes upon which can be built more advanced knowledge.

After explaining the electron theory, the text presents a discussion on electrostatic fields, on the theory that the reader's understanding of the distribution and behavior of the fields within a tube will give him a better picture of why amplification is accomplished within a tube and how the grids and plates are interrelated.

To give a clear physical picture of its subject, the book

employs novel physical devices. For example, certain diagrams and graphs are repeated, to reduce to a minimum the bother of turning pages back and forth to read text and drawings. Another innovation is the use of anaglyphs, "three-dimensional" pictures of phenomena heretofore seen only in two dimensions. Viewed through glasses supplied with the book, they are invaluable aids toward the rapid understanding of the text.

Although this is an elementary book on a fundamental subject, therefore a goldmine for the student; developments in radio and the new fields of television and microwaves make it a must for the libraries of servicemen, amateurs and engineers. Place your order today.

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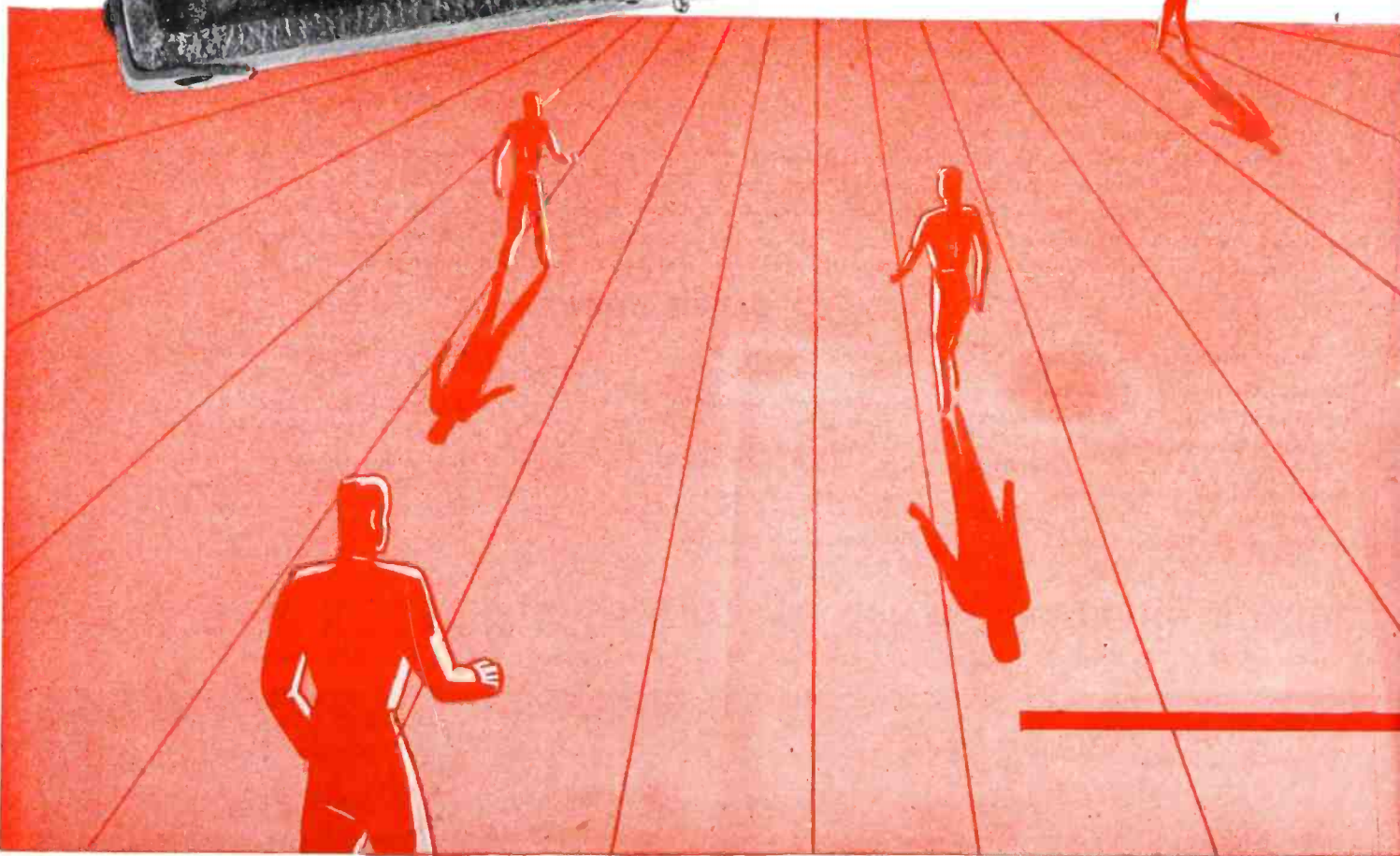
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As you read below the many other features of this pioneering instrument, remember this: It is a Simpson instrument, with all that implies in creative engineering research, in controlled testing and manufacture. Simpson products are not "assembled", they are engineered and built in the Simpson plant. Practically every component part, from the dial and movement to the beautifully designed panels and the bakelite cases and panels, is made by Simpson. It is this that makes Simpson's the "instruments that stay accurate" with ideas that stay ahead.

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1. Size—15½" x 9½" x 6½"
2. Case—Sturdy plywood construction, with heavy fabricoid covering, corners trimmed in leather, rustproof hardware—removable cover with slip type hinges.
3. Panel—Heavy molded bakelite, beautiful satin grained finish. All characters, numerals, and dial divisions are engraved and filled in white, insuring long wearing qualities.
4. Meter—4½" rectangular of modern design with artistic four-colored dial indicating good, fair, doubtful, and bad—also "Percentage of Mutual Conductance" scale.
5. Sockets provided for all types of tubes with two spare socket positions.
6. Neon glow tube incorporated to indicate shorted tubes.
7. New simplified revolutionary switching arrangement (see description above).
8. The tube chart provided is arranged for quickly identifying the tube and setting the controls.
9. Tests tubes with voltage applied automatically over the entire operating range and under conditions approximating actual operation in a radio set.

Ask Your Jobber

The New Simpson Mutual Conductance Tube Tester Brings To Radio Servicemen and Dealers An Entirely New Method of Testing Tubes And A Revolutionary New Switching Arrangement!

Tube manufacturers consider that a radio tube has reached the end of its usable life when it falls to 70% of its rated value. Until now there has never been an instrument to test tubes in percentage terms.

But now here is such an instrument. The new Simpson Model 330 tests tubes in terms of percentage of rated dynamic mutual conductance—a comparison of the tube under test against the standard rated micromho value of that tube. The colored zones on the dial coincide with the micromho rating or the percent of mutual conductance, indicating that the tube is good, fair, doubtful or definitely bad. Thus, at a glance, you can check the tube against manufacturers' ratings. If, for any reason, it becomes desirable to know the actual value in micromhos, the percentage reading may be easily converted.

This is the way tubes should be tested—the way testers always should have worked—but Simpson is first again in bringing this needed development. It tests tubes with voltage applied automatically over the entire operating range, reproducing more completely than ever before the actual conditions under which a tube functions in a radio set. No instrument, not even delicately adjusted laboratory devices, can do this 100%. But this new Simpson Mutual Conductance Tester approaches perfection as never before.

Besides this revolutionary new method, Simpson offers you an equally revolutionary switching arrangement. The circuit is so arranged that, even though there are numerous combinations possible, very few switches require moving to test any one tube. Many of the popular tubes are tested in the "normal" position without moving any of the nine tube circuit switches.

Ten push button switches and nine rotating switches of six positions each provide infinite combinations in tube element and circuit selection. Only a few settings are necessary for the most complicated tube. The tube chart provided is arranged for quickly identifying the tube and setting the controls.

When you have finished a tube test, the Automatic Reset takes over to speed and simplify the next test. Just press the reset button and instantly all switches, both push button and rotary, return to normal automatically!

Here is the test instrument you have had a right to expect from Simpson. With greater flexibility in its circuit and switching arrangement than any other tester can provide, it gives maximum provision against obsolescence. It's the tester of a new era.

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FOR SALE—Crosley car radio, single unit, with lead-in, \$12; other radios; small assortment volume controls, resistors, P.M. and dynamic speakers; earphones; condensers; coils; power and audio transformers, and some tubes. Also 28 back issues Radio Craft; 20 of Radio News, and 13 of Radio. Hal Bundy, 119 Chlp-deva Ave., Manistique, Mich.

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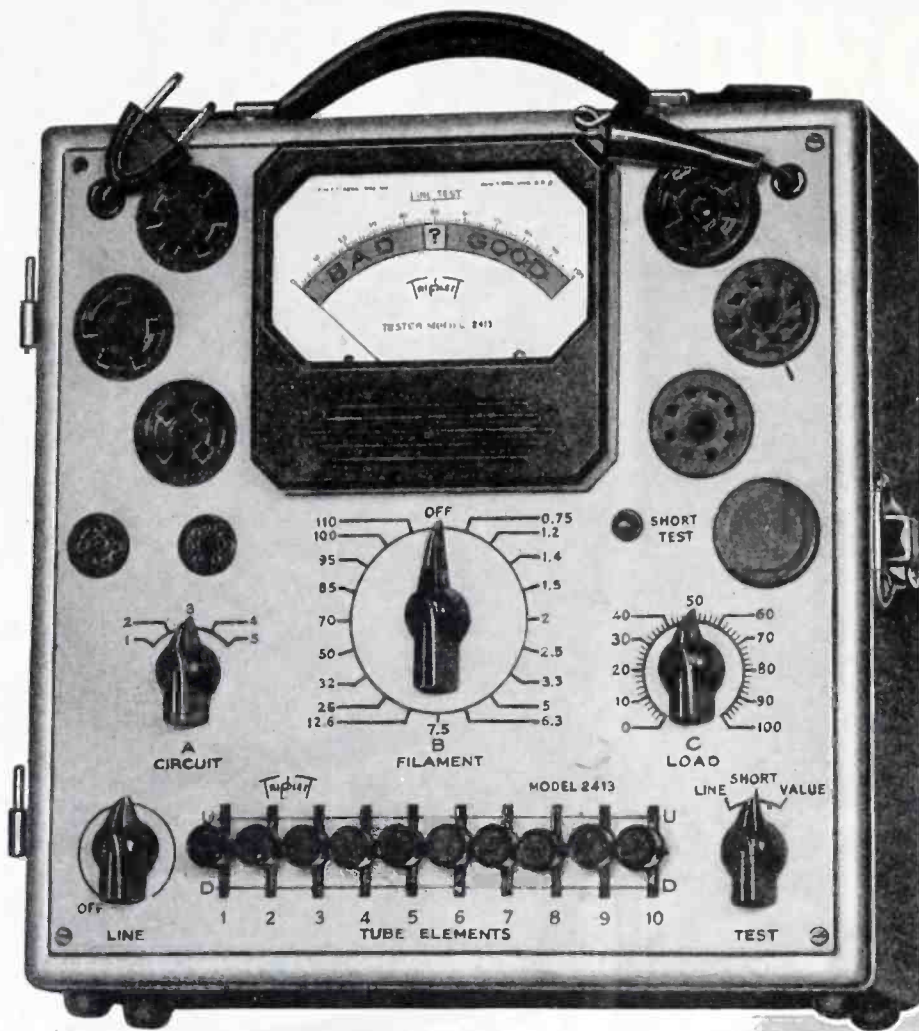
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2413**

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member of the
**NEW TRIPLETT
Square Line**

The New Speed-Chek Tube Tester

MORE FLEXIBLE • FAR FASTER • MORE ACCURATE

Three-position lever switching makes this sensational new model one of the most flexible and speediest of all tube testers. Its multi-purpose test circuit provides for standardized VALUE test; SHORT AND OPEN element test and TRANSCONDUCTANCE comparison test. Large 4" square RED • DOT life-time guaranteed meter.

Simplicity of operation provides for the fastest settings ever developed for practical tube testing. Gives individual control of each tube element.

New SQUARE LINE series metal case 10" x 10" x 5 1/2", striking two-tone hammered baked-on enamel finish. Detachable cover. Tube chart 8" x 9" with the simple settings marked in large easy to read type. Attractively priced. Write for details.

Additional Features

- Authoritative tests for tube value; shorts, open elements, and transconductance (mutual conductance) comparison for matching tubes.
- Flexible lever-switching gives individual control for each tube element; provides for roaming elements, dual cathode structures, multi-purpose tubes, etc.
- Line voltage adjustment control.
- Filament Voltages, 0.75 to 110 volts, through 19 steps.
- Sockets: One only each kind required socket plus one spare.
- Distinctive appearance with 4" meter makes impressive counter tester—also suitable for portable use.



Triplet

ELECTRICAL INSTRUMENT CO. BLUFFTON, OHIO





designs of
DISTINCTION

In medieval times discriminating knights journeyed to Toledo, Spain, to obtain hand-wrought blades of steel. Only the famed guildsmen of Toledo could produce the flawless metal from which they fashioned graceful foils and swords of sleek beauty.

For hundreds of years these proud guildsmen stamped their guild marks or signatures on their creations.

A few firms today still preserve that spirit of craftsmanship. You find it in the plants of Detrola Radio. That is why the "guild mark" of Detrola Radio on a radio receiver, record changer or other electronic instrument is a guarantee of production quality. The world's finest merchants, and their customers recognize the value of this mark.

DIVISION OF INTERNATIONAL DETROLA CORPORATION  DETROIT 9, MICHIGAN



PRECISION MACHINERY plus PRECISION-EL means QUALITY in Mt. Carmel, Ill.

Precision machinery is part of Meissner's famed "precision-el" corps, too, and the men and women who build Meissner quality electronic equipment are the first to share the credit with their bench and tool-room friends. The photographs on this page show typical precision-el "teams" at work.



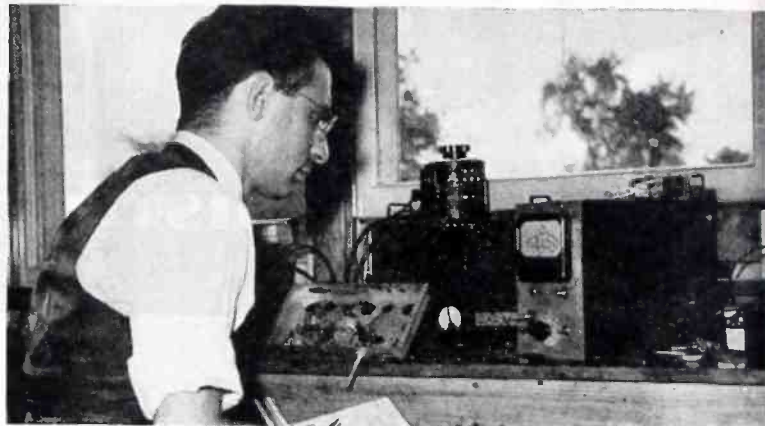
Here's a man who smiles proudly as his "helper"—a precision lathe—does a good job of holding extremely close tolerances.



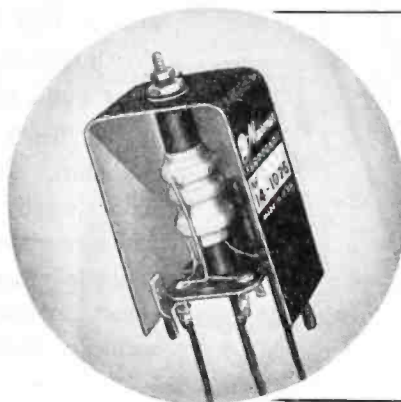
His "partner" receives a delicate adjustment with all the skill he can command. This care of equipment by Meissner *precision-el* has meant higher quality and fewer shut-downs for repairs on a big war job.



Here's another winning combination. Even the smallest parts warrant careful machining at Meissner. It's another reason for precision performance by Meissner products.



This is the proof of the pudding. "Rejects" are surprisingly few, even under the sharp eye of the sensitive testing instruments used by this member of Meissner's *precision-el*.



Replace Broadcast Band Coils Easily

These Adjustable-Inductance Ferrocart (iron core) coils will replace Antenna, RF or Oscillator coils without the trouble of locating "exact duplicates" because they are continuously variable in inductance over a wide range. The inductance of the old coil is easily matched by simple screwdriver adjustment. Ferrocart iron cores add gain and selectivity to the receiver. Available shielded or unshielded, shipped with complete instructions. Order by number. 14-1026 Univ. Ant. Coil; 14-1027 Univ. R.F. Coil; 14-1028 Univ. Osc. Coil. Price \$1.50 each.



MEISSNER

MANUFACTURING COMPANY • MT. CARMEL, ILL.

ADVANCED ELECTRONIC RESEARCH AND MANUFACTURE
Export Division: 25 Warren St., New York; Cable: Simontrico

The New Model CA-11

SIGNAL TRACER



Simple to operate
... because it has only
ONE connecting cable-
NO tuning controls!

INTRODUCED in 1939-1940 Signal Tracing, the "short-cut" method of Radio Servicing quickly became established as the accepted method of localizing the cause of trouble in defective radio receivers. Most of the pre-war testers (including ours) were bulky requiring a number of connections before the unit was "set for operation" and included a tuned amplifier which had to be "retuned" to compensate for signal shift.

The new model CA-11 affords all the advantages offered by the pre-war models and only weighs 5 lbs. and measures 5"x6"x7".

Always ready for immediate use without the necessity of connecting cables, this amazingly versatile unit has **NO TUNING CONTROLS**.

Essentially "Signal Tracing" means following the signal in a radio receiver and using the signal itself as a basis of measurement and as a means of locating the cause of trouble. In the CA-11 the Detector Probe is used to follow the signal from the antenna to the speaker—with relative signal intensity readings available on the scale of the meter which is calibrated to permit constant comparison of signal intensity as the probe is moved to follow the signal through the various stages.

Features

- ★ **SIMPLE TO OPERATE**—only 1 connecting cable — **NO TUNING CONTROLS.**
- ★ **HIGHLY SENSITIVE**—uses an improved Vacuum Tube Voltmeter circuit. Tube and resistor-capacity network are built into the Detector Probe.

- ★ **COMPLETELY PORTABLE**—weighs 5 lbs. and measures 5"x6"x7".
- ★ **Comparative Signal Intensity** readings are indicated directly on the meter as the Detector Probe is moved to follow the Signal from Antenna to Speaker.
- ★ Provision is made for insertion of phones.

Please place your order with your regular radio parts jobber. If your local jobber cannot supply you kindly write for a list of jobbers in your state who do distribute our instruments or send your order directly to us.

The Model CA-11 comes housed in a beautiful hand-rubbed wooden cabinet. Complete with Probe, test leads and instructions.

\$18.75
NET PRICE



SUPERIOR INSTRUMENTS CO.
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NEW YORK 7, N. Y.

SYLVANIA NEWS

RADIO SERVICE EDITION

NOV.

Published by SYLVANIA ELECTRIC PRODUCTS INC., Emporium, Pa.

194

SYLVANIA "LOCK-IN" ADVERTISEMENTS SEL THIS SUPERIOR TUBE TO NATION'S MILLIONS

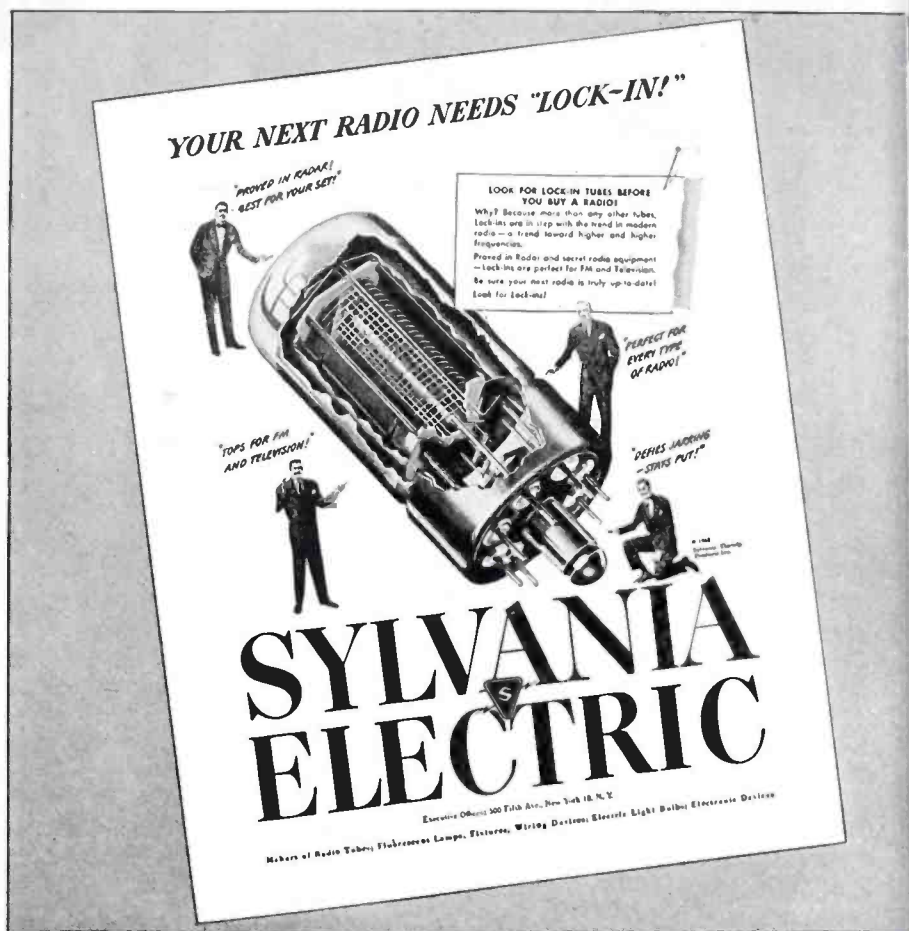


A large, attractive, three-color display banner featuring the phrase "Complete Radio Service" is now ready for distribution to servicemen by Sylvania.

The banner measures 46 by 28 inches, is printed in black, green and white on special weather-proofed "duckine" material, making it suitable for use either inside or outside of the store. It has six metal grommets to provide extra reinforcement.

This useful, durable and attractive display banner may be obtained for only \$.40—or three for a dollar—from your local Sylvania distributor, or by writing to me at Sylvania Electric Products Inc., Emporium, Pa.

This banner is only one of the items on an extensive list of Sylvania promotional material designed to help servicemen merchandise both their own service and Sylvania radio tubes.



Servicemen will find even more people asking about the war-famed Sylvania Lock-In Tube—because of big, full-page Lock-In advertisements appearing in eight national magazines. These ads are telling over ten million people that Lock-Ins have advantages possessed by no other radio tube.

Lock-Ins are noted for their electrical efficiency and rugged durability. Element leads are brought directly through a low-loss glass header to become sturdy

socket pins—effecting a much desired reduction in lead inductance and interelement capacitance. Support rods are stronger and thicker. There are few welded joints and no soldered joints.

These remarkable tubes are designed and built to handle the high and ultrahigh frequencies of FM and Television—as well as the lower frequencies. Today, set-manufacturers are looking for the Lock-In Tube as the perfect electronic unit for all new radios.

SYLVANIA ELECTRIC

Emporium, Pa.

MAKERS OF RADIO TUBES; CATHODE RAY TUBES; ELECTRONIC DEVICES; FLUORESCENT LAMPS, FIXTURES, WIRING DEVICES; ELECTRIC LIGHT BULBS

Fig. 1 (right) A crystal unit in its holder, with the cover removed. The two springs serve to hold the electrodes against the crystal surface. (Courtesy Crystal Research Laboratories)

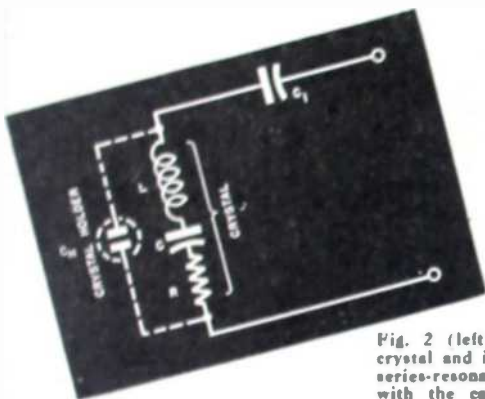


Fig. 2 (left). The electrical equivalent of the crystal and its holder. In effect, the crystal is a series-resonant circuit, consisting of L , C , and R , with the capacitance of the holder across the entire system. C_1 represents the series capacitance between the crystal proper, and the electrodes.

CRYSTAL-CONTROLLED OSCILLATORS

by J. GEORGE STEWART

series capacitance between the crystal proper, and the electrodes.

IN many types of postwar receivers crystal-controlled oscillators will be quite an important feature. The extensive use of these oscillators in Army-Navy equipment has developed crystal manufacture to the point where they are economically feasible for mass production. At the winter IRE meeting last January, we were shown a receiver which tuned the entire b-c band through the use of push-button crystal oscillators.

Most of the new f-m receivers will use crystal-controlled oscillators. Stability requirements in the newly assigned v-h-f band will create a need for double superheterodyning, in which one of the fixed oscillators will probably be crystal controlled.

In the past most Service Men have had little opportunity to work with crystal controlled oscillators, since their use has been restricted to transmitters and fixed frequency receivers.

Physical Properties of Crystals

Physically, the quartz crystal is less than an inch square and only several thousandths of an inch thick. This crystal is sandwiched between two small, flat squares of metal, called electrodes, which serve as surface con-

tacts. Spring pressure is usually applied to these metal squares to hold them firmly in place, and leads are brought out from these electrodes to external pins or contacts. The entire assembly is housed in a unit called the crystal holder. This has been the practice in the past. However, cost economy factors in receiver design may change the form of crystal holder, so that a simpler device embodying the same principles may be used.

Electrical Crystal Properties

The crystal may be likened to a two-plate condenser, with the crystal acting as the dielectric, Fig. 1.

Electrically, the crystal is equivalent to a high Q , parallel resonant-tuned circuit, whose frequency is largely determined by the physical dimensions of the quartz crystal. Its electrical equivalent is shown in Fig. 2, where L , C and R are the series electrical constants of the crystal unit, and C_H represents the capacitance between the metal electrodes, with the crystal acting as the dielectric. C_1 represents the

Crystal Operation

When an electrical current of approximately resonant frequency is applied across the crystal, sympathetic vibrations are set up in the crystal structure. This vibration, in turn, causes large voltages to appear between the electrodes. For this reason, the crystal may be used in place of an LC element in the grid circuit of an oscillator to supply the necessary grid driving voltage. Since the physical dimensions of the crystal are constant, and do not expand appreciably with heat, and since these same dimensions determine the frequency of operation, in the same way that the dimensions of a tuning fork determine its audible frequency, it can be seen that a high degree of frequency stability is thus obtained.

Grid Circuit Activity

When installed in the grid circuit of an oscillator, the value of C_H is further increased by the input capacitance of the tube, and the capacitance of the associated wiring. The result-

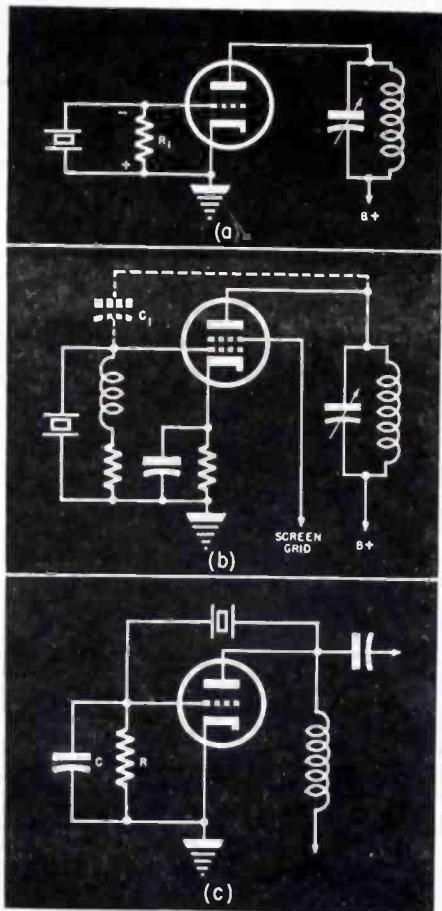


Fig. 3. Three circuits employing crystals for frequency control. In *a*, a triode circuit in its simplest form is shown. In *b*, we have a pentode circuit, while *c* shows the Pierce oscillator, which does not require a resonant circuit in the plate.

ages used, and they must be watched carefully to make sure that they are not excessive. Since power is not important in a receiver, high value grid resistors, and low grid and plate voltages may be used.

Pierce Oscillators

Fig. 3c shows a third method of crystal control for frequency stability the Pierce oscillator circuit. A triode is used, although a pentode may be used too. Here, the crystal is used as the coupling element between the plate and grid circuits. Note that the plate circuit is untuned. Its use in a circuit of this type is similar to a crystal filter, in which only resonant voltages are passed by the crystal, the crystal performing as a series resonant circuit. For all other frequencies, the crystal acts as a pure capacitor. C_1 and the crystal may be considered as a load across the output of the tube. Therefore increasing the value of C_1 increases the load across the output circuit and the resultant grid current. Because of its position in the circuit the crystal is subject to high voltage strains. Therefore the plate voltage of Pierce oscillators is usually lower than for other crystal circuits.

must be kept below the crystal rating, else the crystal may be punctured and rendered inoperative. Expressed another way, the activity of the crystal is a function of the r-f voltage across it. If this voltage exceeds the limits of the crystal, the overactivity will shatter the crystal. Therefore, decreasing the value of the grid resistor reduces the current through the crystal. In Fig. 3a the cathode has been returned to ground, so that the grid bias is a function of the grid current which creates the bias across the grid resistor.

Pentode Circuit

In Fig. 3b a pentode has been substituted for the triode. Since the gain of a pentode is higher than that of a triode, less grid excitation is needed. The feedback from the plate to the grid has been reduced by the lower g-p capacitance inherent in the pentode structure. If this capacitance is too low, an external coupling capacitor represented by C_1 is added, so that sufficient feedback is available. The size of the grid resistor for pentode crystal oscillators is usually 20,000 ohms or less. Since the lower value of resistor may shunt the crystal too effectively, and prevent oscillation, a r-f choke is usually added in series with the resistor. The choke supplies the necessary a-c impedance to reduce the shunting effect of the resistor, at the same time introducing a negligible amount of d-c resistance. Where cathode bias is used, the size of the grid resistor is reduced.

Harmonic Oscillators

Fundamental frequency operation of crystal oscillators is limited by crystal size to about 15 mc. Crystals for frequencies above 6 or 7 mc are very expensive. To overcome this condition, the crystal may be cut to operate on a mechanical harmonic of its fundamental frequency, or may be employed in a circuit where some harmonic of the fundamental frequency of the crystal is amplified. When the crystal is operated on a mechanical harmonic of its fundamental frequency, the resonant circuit in the plate of the oscillator is tuned to the desired harmonic. The crystal then behaves as though it were oscillating fundamentally at the harmonic frequency. When the crystal is used to drive the frequency multiplier,

tant influence on the crystal frequency is quite small, and insofar as related to receivers, may be considered negligible.

Crystal Outputs

Crystal units are capable of delivering large values of r-f voltage, depending on the tube used, and the circuit voltages. However, in receiver applications, the amount of power required is small, and the circuit components reflect this in their size.

Any of several standard circuits may be employed using a crystal as the frequency-controlling element. Three typical circuits are shown in Fig. 3a, b, and c.

Triode-Crystal Oscillators

In Fig. 3a is shown a triode-crystal oscillator in its simplest form. This circuit is essentially a tuned-plate tuned-grid oscillator, with the feedback supplied by the grid-plate capacitance of the tube. Since the crystal itself is a discontinuous d-c circuit, the grid of the tube is returned to ground through the resistor R_1 . This resistor serves a second purpose, since it also limits the r-f current in the grid circuit. This grid current limitation is important, since the permissible current through the crystal

Crystal Excitation

The crystal excitation is a direct function of the plate and screen volt-

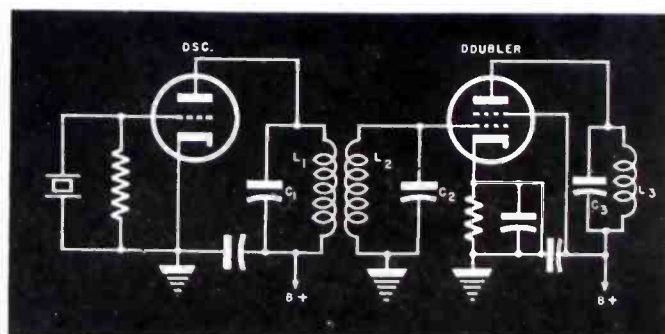


Fig. 4. A method for doubling the frequency of the crystal circuit. The first r-f transformer is tuned to the crystal frequency, while L_3C_3 is tuned to twice the crystal frequency.

he crystal first oscillates at its fundamental frequency. This fundamental frequency is then used to drive the multiplier stage. Sometimes, where the desired frequency is quite high, both methods are used concurrently.

Frequency Multiplier

Fig. 4 shows a typical crystal oscillator and frequency multiplier. In this circuit, L_1C_1 and L_2C_2 are tuned to the crystal frequency. L_2C_2 is tuned to twice the crystal frequency. Thus, the output of the doubler stage is twice the fundamental or crystal frequency.

Tri-tet Circuits

This same principle may be so used that only one tube is necessary for both operations. For example, the crystal oscillator may be one-half of a twin triode, and the doubler may be the other half. Or, a pentode may be used, as shown in Fig. 5. This circuit is known as the *tri-tet*. Here, the control grid, cathode, and screen grid perform as a triode-crystal oscillator. The screen grid serves as the plate of the triode. The plate of the tube is then used as the multiplier, with L_2C_2 tuned to the desired harmonic. This circuit is usually used where even multiples of the fundamental frequency are desired. The circuit of Fig. 6 is used where odd multiples of the fundamental frequency are desired. This circuit is known as the *grid-plate oscillator*. The essential difference between the two circuits is that in Fig. 5 the crystal is returned to ground through the resonant circuit L_1C_1 , whereas in Fig. 6 the crystal is returned to ground directly.

Resonant Circuit and Cathode Return

Actually, the circuit of Fig. 6 is a Pierce oscillator, since the screen grid, which is being used as the plate of a triode oscillator, and the crystal return, are connected together through their common ground terminals. Since the cathode of a tube may be considered as a continuation of the plate circuit, the placing of the resonant circuit in the cathode return does not change the relationship, other than placing the actual plate of the tube at -f ground.

Oscillator Tuning

All crystal oscillators are tuned in essentially the same way. Fig. 7 shows a typical plate-current characteristic

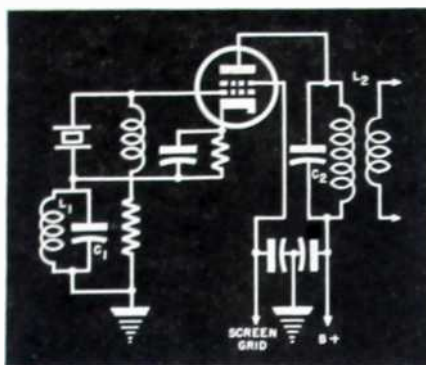


Fig. 5. A crystal frequency multiplier using one tube. L_1C_1 is tuned to the crystal frequency, while L_2C_2 is tuned to a multiple of this frequency. This circuit is used where even multiples of the crystal frequency are desired.

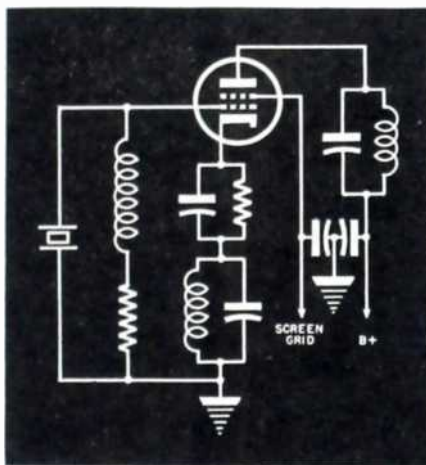


Fig. 6. This multiplier circuit is used where odd multiples of the crystal frequency are desired. The crystal portion of the circuit is essentially a Pierce oscillator, with the screen grid acting as the plate of a triode oscillator.

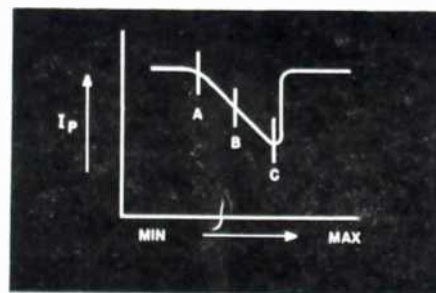


Fig. 7. Plate current characteristic of a crystal oscillator. For stability requirements, the circuit is tuned so that the current is in the vicinity of point B. This also prolongs the life of the crystal.

for a crystal oscillator. When the oscillator is in the non-oscillating stage, the plate current will be found to be at some high level. As the plate-tank tuning capacitor is tuned from minimum capacitance, the plate current will dip as shown in Fig. 7; the

current decreases slowly until it reaches some minimum value, and then rises sharply. The maximum oscillation will take place at the point of minimum plate current. However, for stability purposes, it is best to operate the crystal oscillator at some point about halfway between maximum and minimum plate current. This point of operation also limits the amount of r-f current in the crystal, and will help prolong its useful life.

Causes of Non-Oscillation

If the crystal oscillator stops oscillating, the cause may be traced to physical and electrical problems.

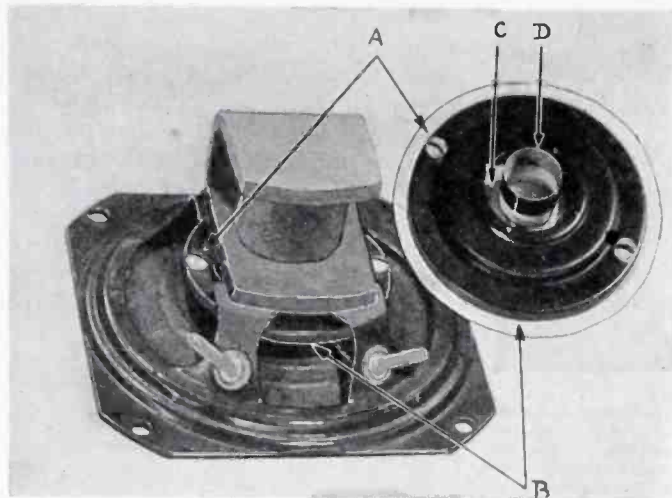
For instance, dirt on the crystal faces will interfere with oscillation. To clean crystals, carbon tetrachloride should be used. The faces of the crystal should be immersed in the liquid and then carefully dried on some lint-free cloth. The faces of the crystal should never be touched with the fingers, since a light film of grease is thus deposited on the crystal impairing its performance. The crystal should always be picked up by its edges, and care should be exercised not to chip the edges. The electrodes should receive similar care, since dirt or grease on their faces will produce the same effects as they would on the crystal.

Tight Coupling

If the crystal oscillator is coupled too tightly to the load, oscillations will cease. This condition will be rare in receivers, but is mentioned here in case some variable coupling method is used.

Other Sources of Trouble

Detuning of the plate tank circuit is another source of trouble. The cure is obvious. All bypasses and coupling capacitors should be checked if some unusual condition appears. For example, an open g-p coupling capacitor, or if a variable coupling capacitor is used, a low value of coupling capacitance will prevent oscillations from starting. An open screen-grid bypass, or a reduction in its value, may cause excessive excitation of the crystal. Another cause of excessive excitation is high bias. This should be checked with a v-t voltmeter in the grid circuit. For other troubles, the crystal-controlled oscillator may be treated in the same manner as any oscillator.



Construction of the Adjust-A-Cone assembly; the spider is kept in position with a pressure or clamping ring, which in turn is held down by two machine screws. In insert view, we have a closeup of pressure ring, which is underneath at B. At C is the spider; D shows the voice coil.

SERVICING HELPS

RECENTERING LOUDSPEAKER CONES WITH QUAM-NICHOLS ADJUST-A-CONE

THE loudspeaker is a device for the conversion of electrical energy into sound. It is composed of electrical and mechanical parts which acting in conjunction with each other make the conversion possible. Thus the electrical components control the mechanical ones, and the electrical impulses to which the loudspeaker is subjected are converted into mechanical action which creates the sound waves.

Analysis of Two Types

In this discussion we will consider only two types of loudspeakers (though there are at least three others). The most commonly used, namely, the electrodynamic and the permanent magnet type will be discussed. Both of these function exactly alike, the sole difference lying in the method employed to obtain the magnetic flux in the field in which the voice coil moves. In the former, it is created by an electromagnet and in the latter by a permanent magnet.

The electrical parts of the loudspeaker are the magnet, pot assembly, and the voice coil; while the mechanical parts are the housing and the cone or diaphragm. The voice coil assembly, known as the driver mechanism, is rigidly attached to the cone so that whatever movement is electrically caused in the driver is transmitted directly to the cone. The movement of the cone against the air in contact with it causes the radiation of air waves, or sound.¹

In order for the voice coil to func-

by FRANK C. KEENE

tion, it must be concentrically located around the end of the magnetic pole-piece of the loudspeaker with a clearance between it and the pole-piece. The clearance between the pole-piece and the pot is very close so that the air gap energy is held at a maximum. It is the action of the audio currents through the voice coil while it is in the direct-current magnetic field that causes the voice coil to move in and out.² This movement, when transmitted to the cone to which the voice coil has been rigidly attached, causes the propagation of sound waves and hence sound.³

Clearances

Clearances must be close for optimum results, but it is imperative that the voice coil ride free within the space between the pole-piece and the pot which is termed the gap. If, for instance, grit or dust gets into the gap, the efficiency and work of the voice coil is thereby impeded. Similarly, the voice coil cannot rub either against the pole-piece or against the pot and give good reproduction.

To center the voice coil within the gap, a membrane, called a spider is built

¹Terman, *Radio Engineering*, page 767.

²Terman, *Radio Engineering*, page 765.

³Olson-Massa, *Allied Acoustics*; Massa, *Electronics*, Feb. 1936; Seabert, *Electrodynamical Speaker Design Considerations*, Proc. IRE, June 1934.

into the loudspeaker assembly. This supports the voice coil at the pole-piece, while the housing (or basket, as it is termed) supports the outer edge of the cone. The spider normally permits movement of the voice coil parallel with the side of the pole-piece, but restricts all side-way movements. If the spider itself gets off center, then the voice coil is no longer concentrically located over the end of the pole-piece and a rubbing voice coil results. The same would occur if the voice coil itself were bent at its junction with the spider.

Rubbing Voice Coils

A rubbing voice coil not only causes losses in power because of the friction developed between the voice coil and the pole-piece or the pot, as the case may be, but it also introduces distortion.⁴ Such off-center operation is apparent in the reproduction in the sound by rasps and rattles and by highly distorted frequency responses. This widely divergent output response from that of a normal speaker cannot be reconciled by the human ear which, while not intolerant of small aberrations and distortions,⁵ does and can register those of this magnitude.

The result is that the user of a loudspeaker with an off-center or rubbing voice coil usually calls in the Service-Man to restore the quality which has

(Continued on page 51)

⁴Knowles, *Electronics*, Sept. 1935; Terman, *Radio Engineering*, page 774.

⁵Terman, *Radio Engineering*, page 763.

Many headlines like this
have raised the question

**RADIO RACKETEERS
ASSAILED BY COURT**

Declaring that radio repairmen were fleecing customers by charging all the traffic

Should Radio Service Dealers be *Licensed?*

RAYTHEON

HAS THE ANSWER!

and will announce it shortly . . .

Screaming headlines in the New York Times, the World Telegram, the Herald-Tribune, articles in *The Reader's Digest*—you know the unfavorable talk they have helped spread, the hardship they have worked on every *honest* radio service dealer.

DEALER LICENSES DISCUSSED

You are well aware that federal regulation, *dealer-licensing* and even finger printing, are being suggested and discussed by a lot of influential people.

What's the answer? *Raytheon will announce it shortly* for Raytheon has been working for years on a new, foolproof way to protect the public—and to help the *ethical radio service man*. A revolutionary new merchandising plan that will raise the public's opinion of the radio servicing profession and protect the reliable service dealer from outside interests.

GREAT COMPETITIVE ADVANTAGE

You can see the tremendous competitive advantage this Raytheon plan will give every dealer who can qualify! Watch for all the facts on the Raytheon program to protect the public — and help the honest service-dealer!

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RADIO RECEIVING TUBE DIVISION

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RAYTHEON

Radio Tubes

DEVOTED TO RESEARCH AND THE MANUFACTURE OF TUBES FOR THE NEW ERA OF ELECTRONICS

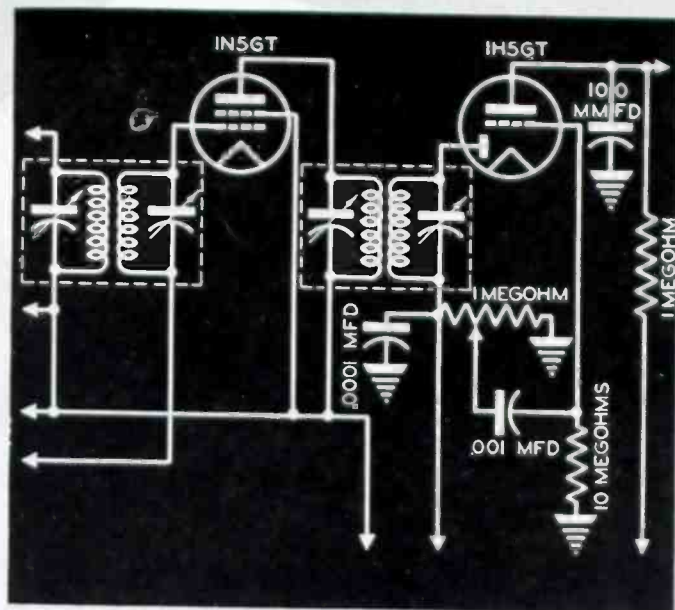


Fig. 1. The i-f system of the Westinghouse WR-678. The sensitivity of portable-receivers is about 30 μ P for an output of 50 mw. Most of this gain is supplied by the high gain i-f stage.

by L. E. EDWARDS

I - F A M P L I F I E R S

DURING the past few months we have been discussing some of the important circuit systems that constitute the modern receiver. Thus far we have covered inputs. (Martin W. Elliott's analysis of mixers appeared last month and continues in this issue on page 32.) In the i-f amplifier we have another vital element of receivers. For this section provides both sensitivity and selectivity.

High-gain remote cut-off pentodes are the most suitable amplifier tubes, allowing a wide range of avc control without detuning, and have thus been used in most i-f amplifiers.

I-F Transformers

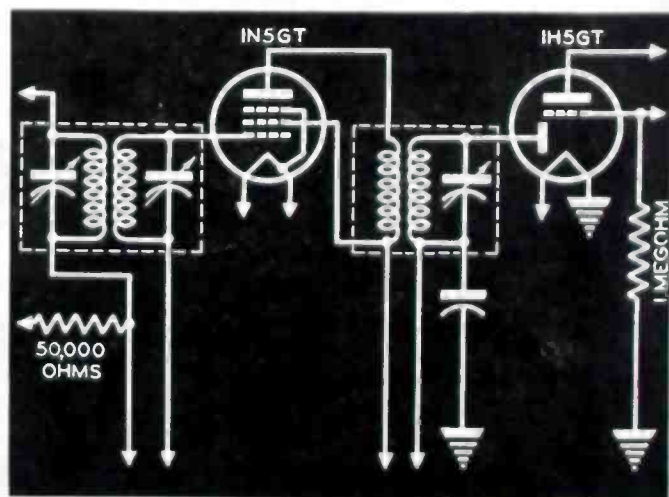
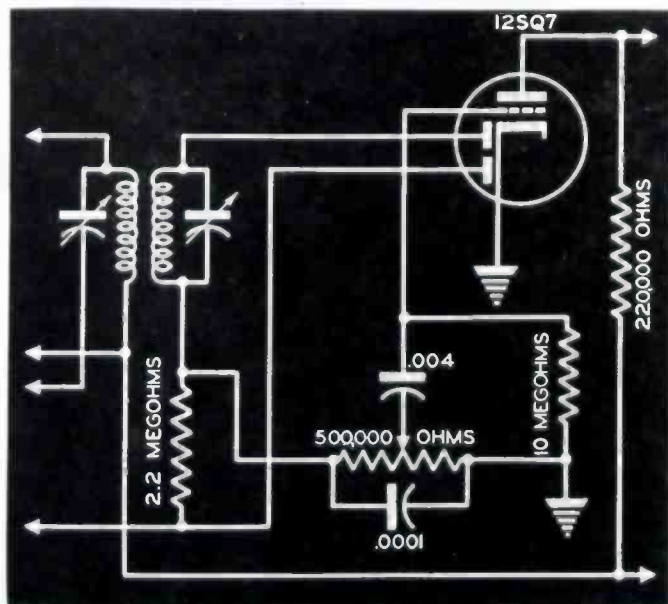
I-f transformers may be divided into

two classes based upon their inductance; high-inductance coils of 2.0 to 2.5 mh and low-inductance coils of 1.0 mh or less. The former are tuned to 455 kc by low-capacity trimmers of 50 to 100 mmfd, giving a high L/C ratio and a high anti-resonant impedance which presents a good match to the pentode plate resistance. However, this arrangement is extremely critical to adjust to resonance and still harder to keep there because the trimmer is subject to change with temperature and age. Mechanical fatigue and warping are also annoying. Therefore, the attainable gain is not usually obtained for very long. On the other hand, low L transformers can use larger tuning capacitors, 150 mmfd and up, which are less subject to mistuning or detun-

ing because they are not so critical. Small changes in capacity cause less change in resonant frequency.

Personal receivers using only 45 or 67 volts B must use very high quality, high Q transformers of the order of 80 to 100, to obtain sufficient overall gain. Some of these types are potted, forming a closed magnetic circuit like two E laminations, or shell type which greatly reduces absorption in the shield, or even eliminates the shield in some instances.

I-f coils of the low-priced a-c/d-c receivers are wound with No. 37 or 38 solid copper, while the higher-priced receiver i-f's use 3 to 5 strand Litz for the input and either solid or Litz for the output, or second detector transformer. The i-f's of the very high



Figs. 2 (left) and 3 (above). Fig. 2 shows the i-f section of the Spiegel 1-40. No i-f tube is used, the gain of the single i-f transformer being enhanced by a small amount of regeneration. Fig. 3. I-f section of the Allied D-366. Primary of the second i-f transformer is untuned. The elimination of this tuned stage reduces both the gain and the selectivity of the receiver.

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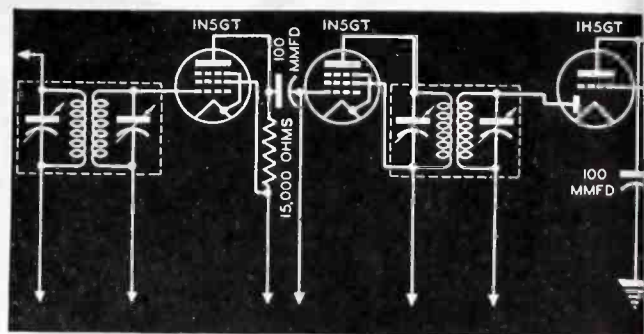
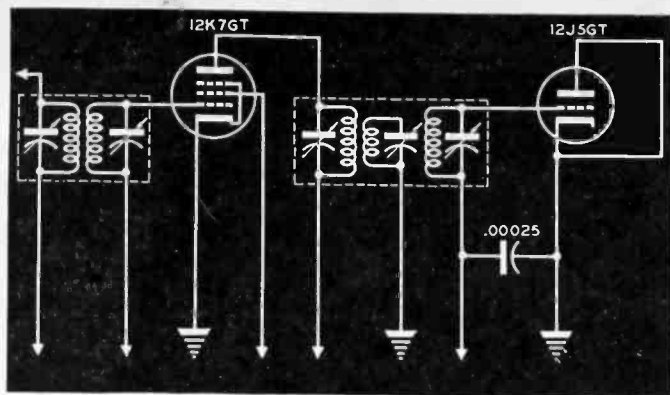
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quality receivers have been wound with 7 to 10 strand Litz on larger coils, and often are triple-tuned or iron-cored, and encased in cans. For improved stability, the tuning capacity is often divided between a fixed silver mica capacitor and a small trimmer, any variation in the latter representing only a small part of the total.

Westinghouse WR-679

In Fig. 1 we have a conventional i-f amplifier of a portable, Westinghouse WR-679, using a 1N5GT with standard dual air-core transformers. Portables of this type have a sensitivity of about 30 microvolts from converter grid to speaker for an output of 50 milliwatts, the principal part of the gain coming from the i-f. For comparison, a typical a-c/d-c job has a sensitivity of about 180 microvolts.

The detector transformer is loaded by a 1H5 diode and its load resistance, a 1-megohm volume control. It is important that the second detector be well grounded to the chassis to prevent coupling to the loop antenna. Sometimes eddy currents are formed in the chassis which act as coupling loops. This condition is worse where the loops are poorly designed, since this prompts broad tuning because the i-f frequency

Figs. 4, (above left) and 5 (above right). In Fig. 4 appears the i-f system of the Air-King 4034. Triple tuning in the second i-f transformer provides good gain. At the same time the band-pass characteristic is improved, resulting in high fidelity reception. Fig. 5. Resistance coupling in an i-f stage in the Ward O4WG-2672. This is an inexpensive way of increasing the gain of a receiver with very few parts. The increase in gain is of the order of 12-20.

of 455 kc is quite close to the 540-kc setting at the low end of the band.

Spiegel 1-40

The i-f section of a midget 3-tube and rectifier superhet without an i-f amplifier tube is shown in Fig. 2. In this receiver, Spiegel 1-40, a 12SA7 modulator feeds a 12SQ7 second detector through the single i-f transformer. Sensitivity and selectivity are both enhanced by regeneration by returning the primary tuning capacitor to an RC-feedback element in the cathode circuit. One diode is used as detector, the other as a gate on the avc system.

Allied D-367

In Fig. 3, we have another portable receiver, Allied D-367, which contains a conventional i-f input transformer but uses a single-tuned detector transformer. This transformer is a cartwheel type, wound on a single ceramic

base, with the windings very closely coupled. This type of unit hasn't much selectivity.

Air-King 4034

In Fig. 4 appears the i-f system of the Air-King model 4034. In this system we have a triple-tuned second detector transformer which provides good gain and, at the same time, band-pass characteristics for passing a wide band for high fidelity. This may be accomplished by staggering the tuning of the three circuits so they resonate at three equally separated frequencies. The added tank circuit is grounded to prevent electrostatic coupling. The detector is a 12J5 used as a diode with 1/2-megohm load resistance. The input i-f transformer is standard.

Ward O4WG-2672

A Ward portable, model O4WG-2672, with a resistance-coupled second i-f stage, is shown in Fig. 5. This method is ideal for portables, since it provides an additional gain of 12-20 with but one extra tube, two resistors and a coupling capacitor. Its use is generally limited to applications in which selectivity is not a problem. There is a further disadvantage in the reduction of the signal/noise ratio. With the additional i-f gain in this type of receiver, the circuits are pretty hot compared to the standard single i-f circuits; hence, such items of stability as bypass capacitors must be watched carefully. Replacement units must be of good quality and adequate capacity.

The first i-f plate load consists of 15,000 ohms. Some designers have used up to 75,000 ohms. The coupling capacitor is 100 mmfd.

G. E. L-643, 653, 663, 673

In Fig. 6 (G. E. L-643, 653, 663, 673), we have an iron-core i-f input system, with a large air-core unit for the second detector, the pair providing exceptionally good i-f gain without the use of high-inductance coils. In some receivers the cores are sometimes made

(Continued on page 48)

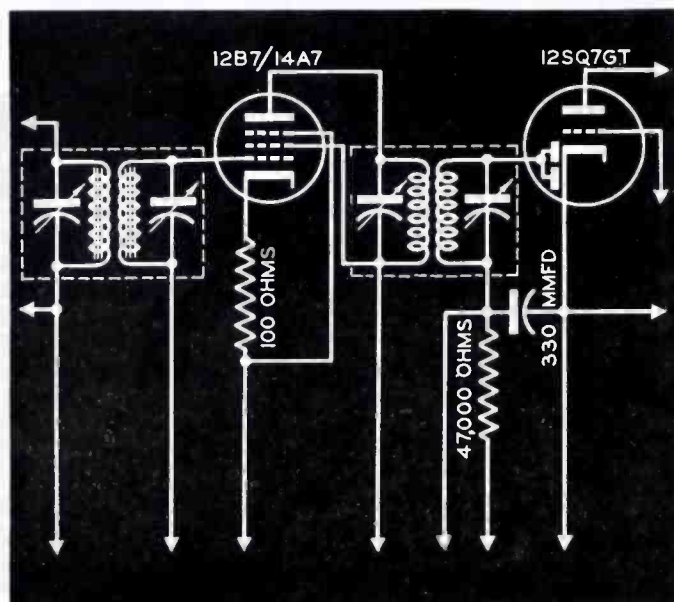
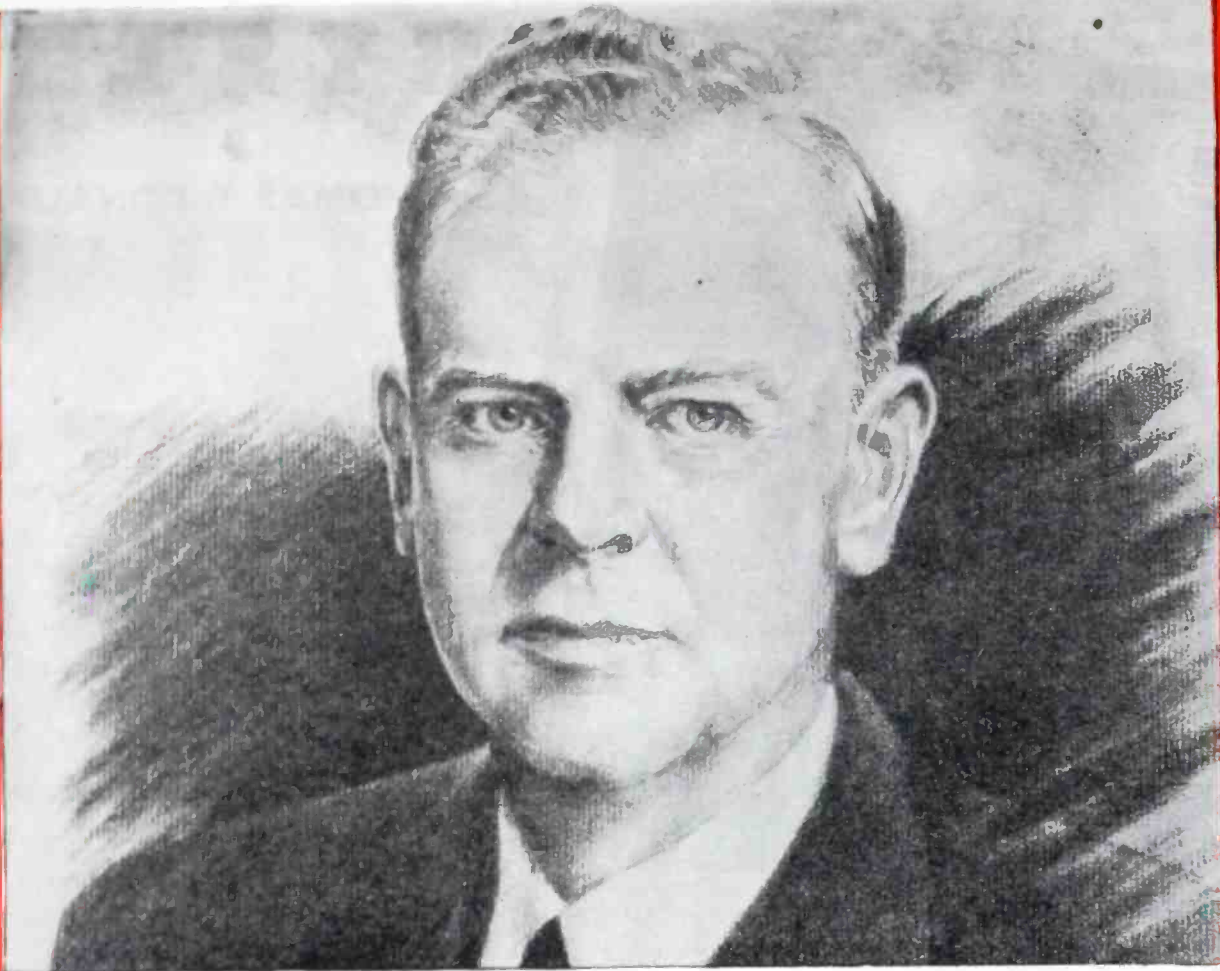


Fig. 6. The G.E. L-243 i-f system. Iron core coils are used to improve the Q of the i-f system. In some receivers, the cores are made adjustable, permitting the use of stable, fixed capacitors.



Portrait of Randolph C. Walker by John Carlton

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by THOMAS T. DONALD

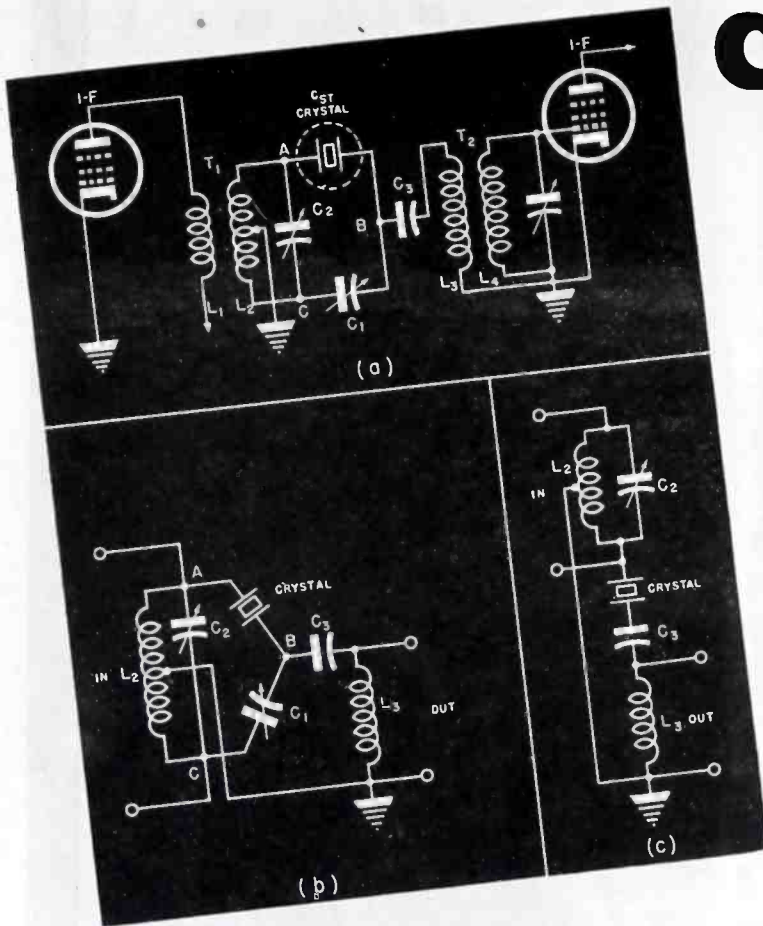


Fig. 1. A typical crystal filter i-f network. In *a*, the crystal filter circuit is shown; *b* shows its close relationship to a balanced-bridge type network; *c* shows how the series resonant characteristic of the crystal is used to provide extreme selectivity.

MANY types of communications receivers feature single-signal circuit design for c-w or code reception.

In c-w (continuous waves) we have the transmission of an r-f carrier only, with no audio modulation. The carrier is then broken up into short and long dashes, or coded. Since there is no audio modulation, the only means of detecting the signal, is through the use of a beat-frequency oscillator or b-f-o which was analyzed in last month's article. However, in the bands used for this type of communication, two adjacent signals may be no more than a few cycles apart, since the volume of air traffic is quite heavy. Therefore, the selectivity of a broadcast type receiver, and its band acceptance of ten kc required to accommodate the side band transmissions necessary for true fidelity of music and voice, would be unaccept-

able for c-w work. It therefore becomes necessary to improve the selectivity of the receiver to a point where the band acceptance is 100 cycles or less. The best method for accomplishing this is through the use of a crystal filter. In addition, a narrow band acceptance helps to reduce static as well as other types of interference. Many Service Men may have noted that when European pickups are retransmitted in this country c-w signals are heard in the background. With a sharp crystal filter, it is possible to receive the code signal, and almost completely obliterate the broadcast signal.

Crystal Filter Positions

Crystal filters are usually installed between the first detector of a superheterodyne receiver, and the following i-f stage, or between i-f stages. A typical crystal filter i-f network is shown in Fig. 1a. It is redrawn in

Fig. 1b to show its close relationship to a bridge type, or balanced network. In this figure C_1 is the phasing control. If the crystal could be installed in the circuit without the accompanying capacitance introduced by the crystal holder and associated wiring, C_1 as well as the balanced type circuit, would be unnecessary. However, due to the introduction of this stray capacitance, represented by C_{ST} in Fig. 1a, it is necessary to balance out its effect. This is accomplished with C_1 , the phasing control. If this were not done, the circuit enclosed by the dotted line in Fig. 1a, would act as a coupling capacitor, with the crystal assuming the role of a dielectric, serving to link T_1 and T_2 , and permitting the passage of all r-f signals present in T_1 . However, when C_1 is adjusted so that it is equal in value to C_{ST} , any non-crystal-resonant voltage developed between points *A* and *B*, is cancelled out by a like voltage between points *C* and *B*. A study of Fig. 2b shows how the balanced-type circuit accomplishes this. For crystal resonant voltages, the crystal acts as a series resonant circuit, thereby providing a coupling path between T_1 and T_2 .

Phasing Controls

The phasing control, C_1 , also performs another function. Since it is a

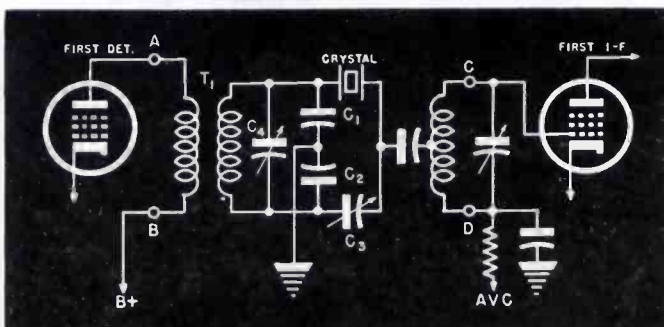


Fig. 2. The crystal filter network of the National NC 100 XAB. C_1 and C_2 split the secondary of the first i-f transformer capacitively. C_3 is the phasing control. This is a plug-in type stage, *A*, *B*, *C*, and *D* representing the four prongs of the plug.

FILTERS USED IN COMMUNICATIONS RECEIVERS

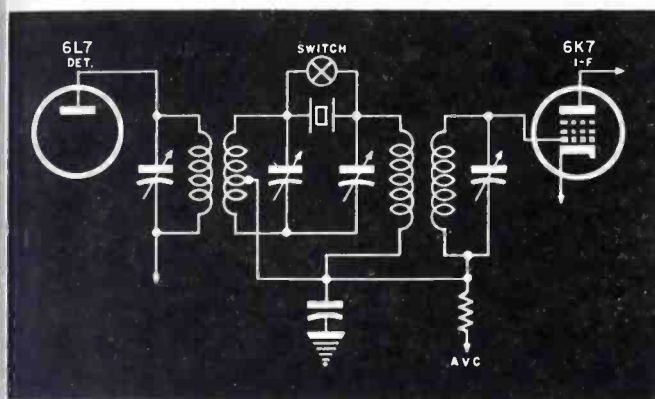


Fig. 3 (above). Crystal filter of the Hallicrafters SX 18. Here, the transformer is split inductively. A panel switch is provided to cut out the crystal for voice reception.

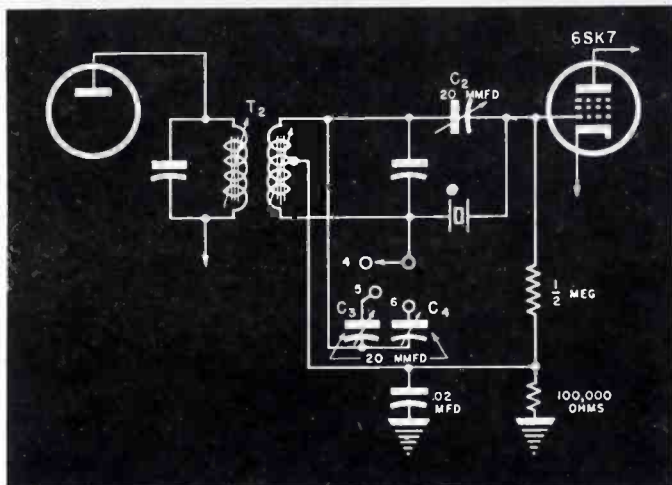


Fig. 4. The variable-selectivity system used in the Hallicrafters SX 28. Capacitors C_3 and C_4 detune the secondary of T_2 , thereby increasing the effectiveness of the crystal and improving the selectivity of the system.

ancelling agent, any partial cancellation of the distributed capacity in the crystal circuit would tend to decrease its selectivity. Therefore, the phasing control may also be used to control the selectivity of the crystal filter.

Selectivity Control

The adjustment of C_2 , which tunes T_1 , may also be used as a selectivity control. When C_2L_2 is tuned to the resonant frequency of the crystal, it places a high resistance in series with the crystal, since, at resonance, a parallel tuned circuit offers the greatest impedance, or resistance. (The circuit is shown in Fig. 1c.) Therefore the effectiveness of the crystal Q is reduced, since it only represents a small portion of the entire resistive network represented by L_2C_2 , the crystal, C_3 , and L_3 . However, if L_2C_2 is detuned, the resistance of this portion of the network is reduced to the reactance of either L_2 or C_2 , whichever is smaller, and the effectiveness of the crystal is increased. Thus, the selectivity of the circuit is increased.

Basic Designs

The three points previously discussed are important since they are not only the basis of most of the crystal-filter network communications

receiver designs, but a major factor in servicing and alignment.

National NC 100 XAB

Figs. 2 to 6 show the crystal-filter networks used in typical communications receivers.

Fig. 2 is the crystal-filter circuit of the National NC 100 XAB. C_1 and C_2 are used to split the secondary of T_1 to obtain a balanced circuit. C_3 and C_4 are the phasing and selectivity controls, respectively. This particular model is so arranged that a standard i-f transformer of the plug-in type may be used instead of the crystal-filter unit, which is also a plug-in type. The plug-in points are represented by A , B , C , and D . The selectivity of the crystal unit is preset, before insertion.

Hallicrafters SX 18

Fig. 3 shows the crystal system used in the Hallicrafters SX 18. Here, the primary of the first i-f transformer is tuned, and its secondary split inductively. A panel switch is provided to cut out the crystal when the set is used for b-c reception. Note the similarity of this circuit to Fig. 1a.

Variable Selectivity Filters

The circuits shown previously have been simple versions of crystal filters. More expensive types of communications receivers feature a variable selec-

tivity i-f system, with and without crystal filters.

All variable selectivity crystal-filter systems revolve around some method of decreasing the Q , or band acceptance, of the crystal. This is necessary, since it permits easier tuning of c-w signals when noise conditions are not restrictive. It can be appreciated that when dialing for a signal with an i-f channel that is only 100-cycles wide, the slightest movement of the dial would pass over the signal. Figures 4 to 6 show three such systems.

Hallicrafters SX 28

Fig. 4 shows the variable selectivity system used in the Hallicrafters SX 28. Three positions, 4, 5 and 6, are provided for crystal *broad*, *medium*, and *sharp*. In position 4, T_2 is tuned accurately to the crystal frequency. This causes broad-band acceptance, as explained in Figure 1c. Position 5 adds trimmer C_3 , which detunes T_2 slightly, thereby increasing the effectiveness of the crystal filter. Position 6 further

(Continued on page 50)

ELECTRONIC ALARM SYSTEMS

SYSTEMS

by WILLARD MOODY

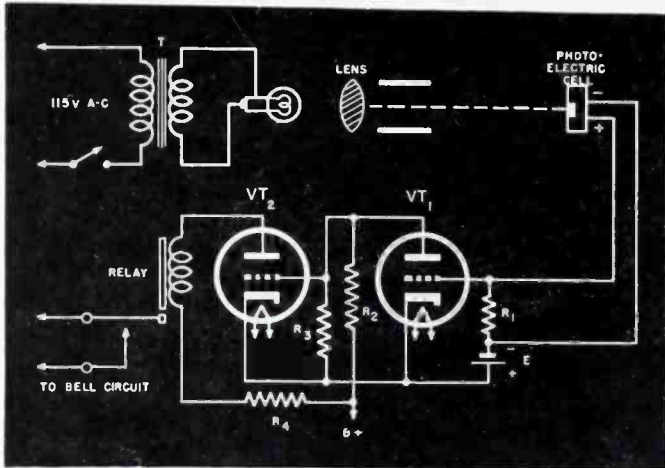


Fig. 1. An elementary photoelectric alarm system. Interruption of the light source reduces the voltage across R_1 , which is bucking the bias voltage. This reduces the plate current, and thereby actuates the bell system.

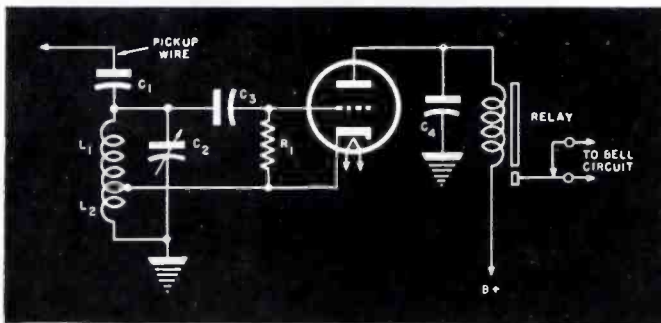


Fig. 2. A circuit typical of r-f types of alarm systems. Variation in the grid capacity across the grid circuit of the oscillator causes a decrease in plate current, which in turn closes or opens a relay.

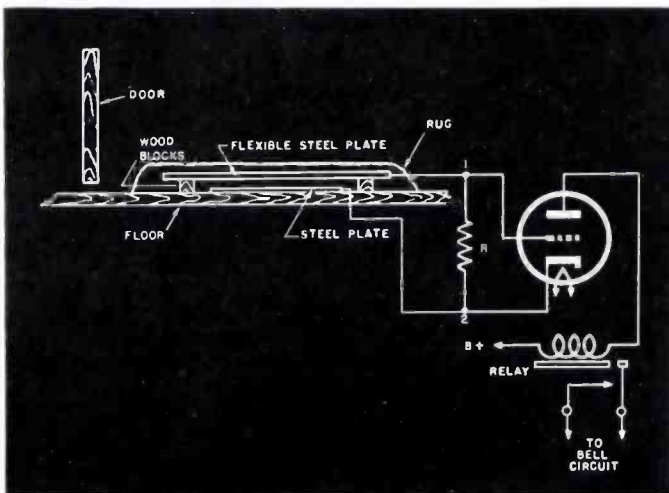


Fig. 3. A step-operated type of alarm system. Resistor R is usually of the order of 10 to 15 megohms. Shorting of the flexible steel plates by stepping on them shorts out the grid resistor, causes the plate current to rise, and actuates the relay.

ELECTRONIC circuit developments have introduced many unusual tube applications, such as the electronic alarm. During the war electronic alarms were used in a variety of installations. The postwar era will see an extensive use of these alarms in industry and the home.

Types of Alarm Systems

There are several types of electronic alarm systems. In Fig. 1 we have one where light from an auto type bulb is directed through a lens and barrel-like tube to a photoelectric cell which may be four or five feet away. In some cases a filter is used in front of the barrel for passing invisible infrared rays only. In other cases, ordinary white light is used. In operation, the light strikes the photocell which develops a potential across the cell terminals. This voltage is applied to the grid of the first tube and is bucked out by a bias voltage. When light no longer strikes the cell, the voltage is zero and the grid bias potential causes a decrease in the plate current, since the bias is more negative.

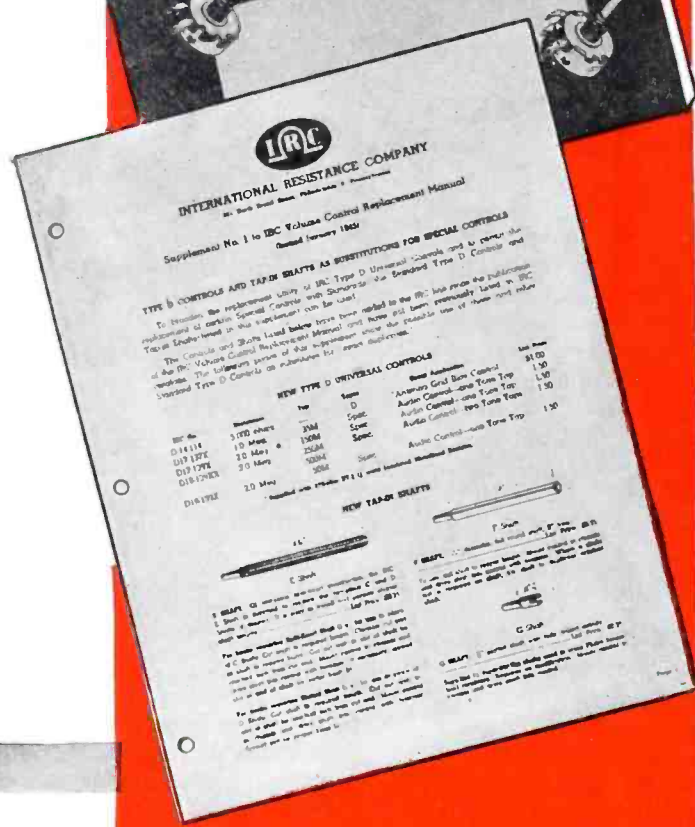
Relay Activity

The interruption of the light beam thus actuates the alarm system. That is, the drop in plate current, with an increased negative grid potential, causes less current flow in R_2 and a decreased voltage drop across R_2 . Then, the increased positive potential on the grid of the second tube causes a rise in plate current and the relay closes. A latching or lock-in arrangement may be used on the relay, so that

(Continued on page 38)

IT'S A HUNDRED TO ONE YOU'LL FIND THE RIGHT CONTROL

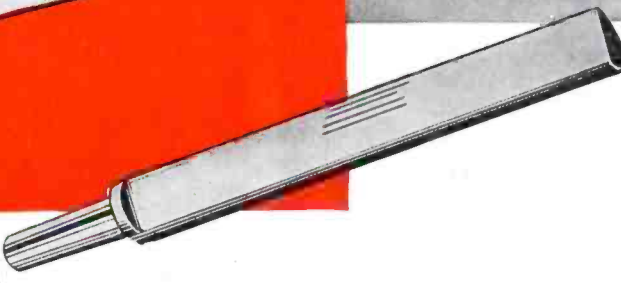
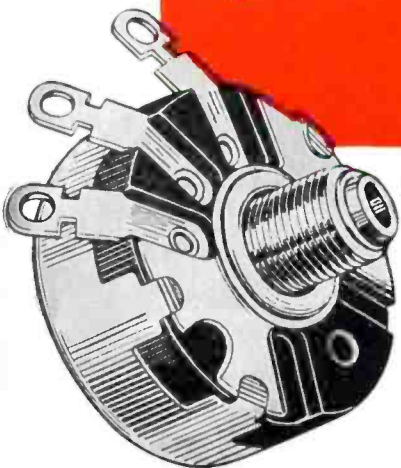
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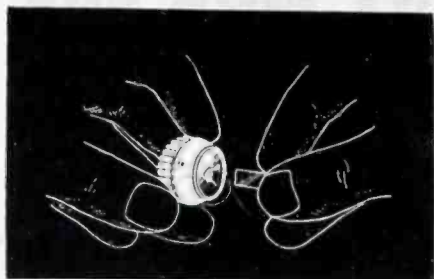
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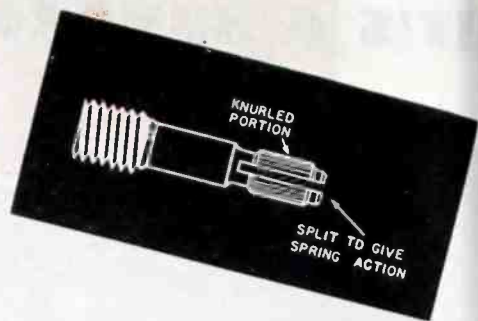


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Figs. 1 (left) and 2 (right). Fig. 1. How the metal spacer is inserted in the knob against the flat spring in push-on type knobs requiring only a $1/32$ " flat. (Courtesy P. R. Mallory & Co., Inc.)
 Fig. 2. Split-knurled type shaft that makes a set screw or spring in the control knob unnecessary.



VOLUME AND TONE CONTROL RESISTORS

VOLUME and tone controls have, in part, reached standardization of certain mechanical dimensions. In general, the tendency has been toward a reduction in overall size, particularly for automobile and midget receiver applications. Perhaps the greatest variance in the controls used as original equipment concerns the length of shaft and the method of fastening the control knob to the shaft.

Control Shafts and Knobs

The knobs used on most of the home and portable receivers have been of two general designs, the *set-screw* type and the *push-on* type knob. The shaft diameter has (practically from the start) been $1/4$ " in diameter and the bushing $3/8$ " in diameter, so from the replacement-control angle, the main problem involves the providing of a universal means which will allow the use of either the screw type or the push-on type of knob.

Provision of a *flat* on the shaft accommodates the screw type; it provides a secure mounting. The *push-on* type also utilizes a flat on the shaft, but in the design of such knobs two sizes have been developed, one which uses a shaft milled down $3/32$ " and one which uses a $1/32$ " milling. The former was extensively used in earlier receivers. The problem of making a universal line of home receiver controls has been met by one manufacturer by milling all shafts to $3/32$ ". This covers the majority of *push-on* type knobs and also accommodates the *screw* type. Then, for those cases which require a $1/32$ " milling, a small $1/16$ " metal insert or spacer is used on the deeper milling to bring it up to $1/32$ ". This spacer is inserted in the

Part Nine of a Series on Receiver Components

by **ALFREDA. GHIRARDI**

Advisory Editor

knob, resting it on the flat spring member (as illustrated in Fig. 1) before assembling the knob to the shaft. When this assembly is pushed on the shaft, it provides a secure and simple method of application. The milled side of the shaft is turned to the downward position allowing the insert to remain in the proper location in the knob during assembly.

Split-knurled shafts and correspondingly knurled knobs also have become popular, especially in auto-radio receivers, because the split gives a spring action and no additional set-screw or spring insert is needed in the knob. Furthermore, the knob can be pushed on the shaft in any relation to the sliding contact arm of the control. A split-knurled shaft is illustrated in Fig. 2. The knobs for split-knurled shafts will not fit the conventional flattened shaft.

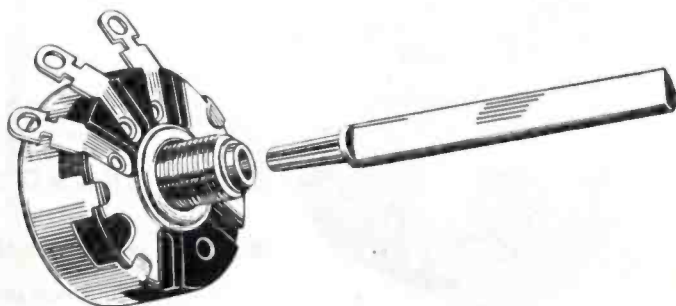
Plug-in Shafts

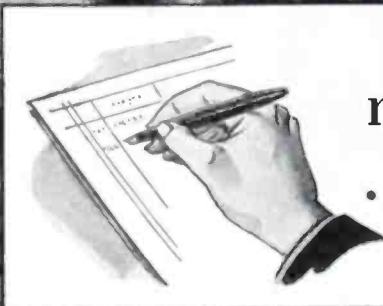
The *plug-in* type shaft is a recent

innovation in universal shaft design. Such shafts are made in plug-in form to fit a special line of controls made by the particular manufacturer. The shaft is easily attached or detached to a special fitting in the bushing, and is held rigid. A recent shaft design employing a tapered plug-in portion is illustrated in Fig. 3; a complete line of plug-in shafts is illustrated in Fig. 4. With this entire set, the Service Man is sure of always having the right replacement control shaft at hand for nearly every job. For household receivers a kit comprising eight shafts (SS1, 2, 5, 16, 18, 22, 25 and 26) answers most needs. For automobile radios, a kit comprising twenty-two shafts (SS1, 2, 3, 4, 6, 10, 11, 12, 14, 15, 17, 19, 20, 21, 23, 24, 27, 28, 29, 30, 31 and 32) will meet all requirements.

Plug-in type shafts are becoming increasingly popular for the following reasons: (1)—They result in a tremendous increase in the flexibility of control applications, for only a few types of controls are required to service the large majority of receivers. Hence they reduce the stocking and inventory problem. (2)—They either replace the original shaft exactly, or they can be made into exact replicas by simply cutting to the required length.

Fig. 3. A recent design of tap-in (plug-in) shaft. (Courtesy IRC)





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SERVICE, NOVEMBER, 1945 • 27

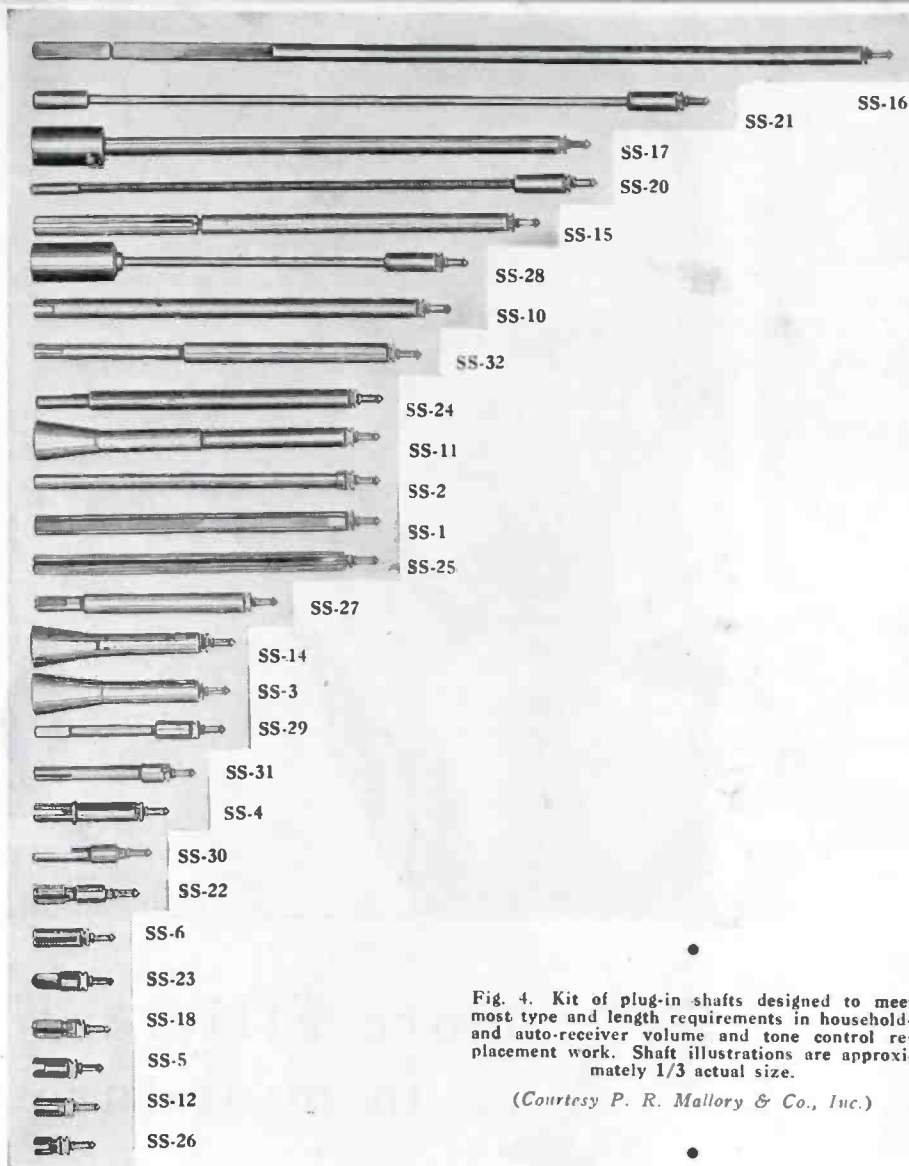


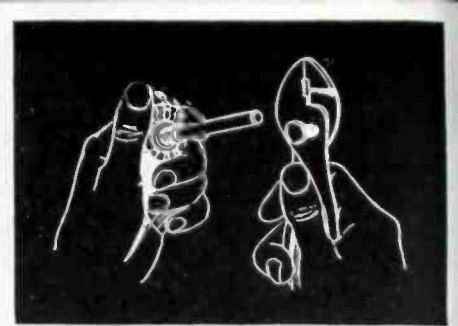
Fig. 4. Kit of plug-in shafts designed to meet most type and length requirements in household and auto-receiver volume and tone control replacement work. Shaft illustrations are approximately 1/3 actual size.

(Courtesy P. R. Mallory & Co., Inc.)

(3)—They speed up volume and tone control replacement in the many receivers in which other components are crowded against the back of the control. In such cases, the replacement control may be inserted in place *before* attaching the shaft, thus eliminating the necessity of first having to disconnect and remove nearby components from behind the control to

provide sufficient space in which to work. (In such cases, if the defective control that is to be replaced is constructed so its shaft is not removable, it may be slipped out from a crowded place by first cutting off its shaft as close to the panel as possible by means of a hacksaw.)

The length of shaft used on controls in receivers is a variable. It de-



A sharp tap is all that is necessary to drive the shaft into the control.

pends on the chassis mounting, thickness of the receiver panel, etc. This dimension varies from 1/2" to 6" or more, with the majority of controls having shaft lengths of 1" to 1 1/2". To adapt a line of fixed-shaft replacement controls to all receivers, the shaft usually is made 3" or 4" in length. For the few receivers having longer shaft controls, extension shafts are obtainable. For shorter shaft controls the ordinary shaft (which usually is made from a special grade of aluminum or other fairly soft alloy) can be notched at the required length by means of a file or knife, as shown in Fig. 5, after which it can be easily broken, as shown.

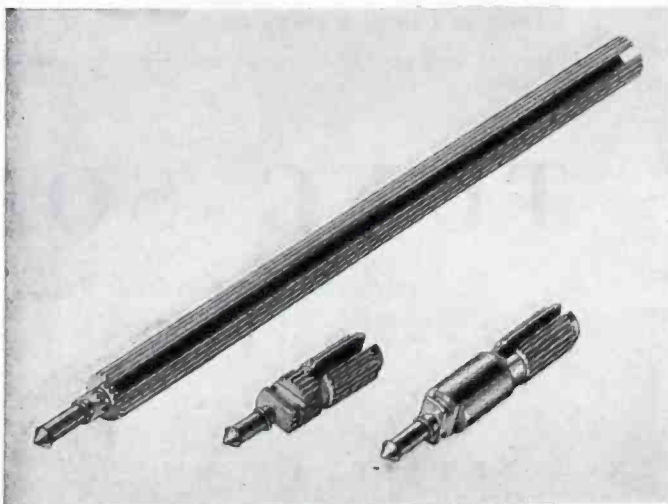
A set of knurled, plug-in shafts of three different lengths up to 4", illustrated in Fig. 6, provide a flexible kit for plug-in shaft type replacement controls where a simple type of shaft is required. These may be cut to the required dimensions to make plug-in shafts of any desired shorter lengths.

Clutch Type Controls

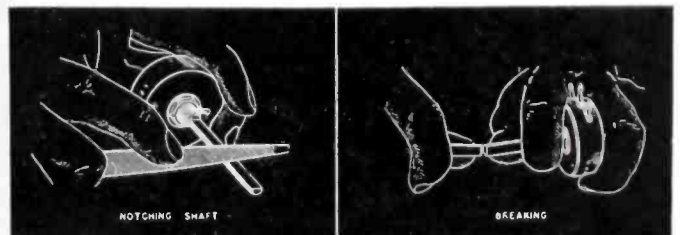
A large number of auto-radio receivers have been constructed with the *on-off* switch that is in or upon the control head located on the car instrument panel, instead of being attached to the volume control in the receiver, Fig. 7.

This arrangement requires a special type of control known as the friction *clutch type* because it contains a friction clutch which permits the shaft to

(Continued on page 30)



Figs. 5 (below) and 6 (left). Fig. 5 Shortening a long shaft to the correct length. Fig. 6. Knurled plug-in shafts in three sizes up to 4". (Courtesy P. R. Mallory & Co., Inc.)



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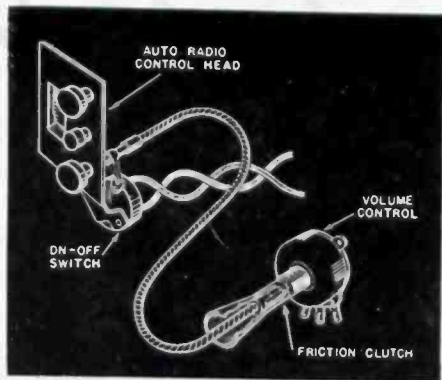
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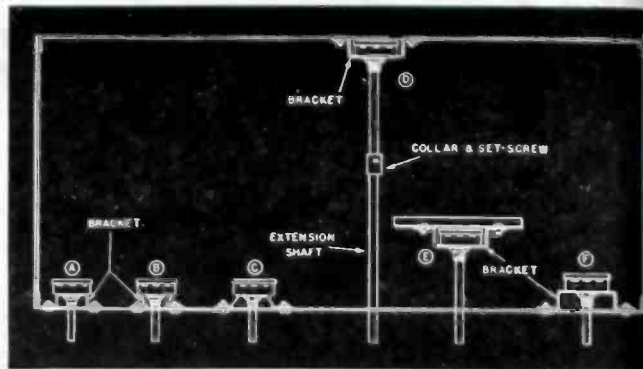
RADIO CORPORATION OF AMERICA

TUBE DIVISION • HARRISON, N. J.

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Phonographs . . . Records . . . Electronics



Figs. 7 (left) and 8 (right).
 Fig. 7. Application of special type controls having a friction clutch-drive arm which permits the shaft to slip. Used in auto sets. Fig. 8 illustrates the use of brackets for mounting volume and tone controls to front panel and sub panels; also the use of an extension shaft where an extra long shaft is required.
 (P. R. Mallory & Co., Inc.)



slip in order to allow alignment of the contact arm of the control with the knob indicator on the tuning head so that the on-off switch operates at the correct position. When installing a repaired or replacement control of this type, we must first install the control and insert the driving shaft; then the control knob is turned through its full rotation in both directions. The result is the proper alignment of the contact arm of the control with the driving knob so that the switch operates at the correct position.

Controls having this clutch feature are usually provided with a plain cover, but with a proper portion of the resistance shorted out, so the volume control does not begin to function until the switch has been operated.

Several clutch-type control shaft assemblies of the plug-in type and in different lengths for various models of auto-radio receivers are illustrated at SS-3, SS-14 and SS-11 in Fig. 4.

Mounting Brackets, Extension Shafts and Bushings

Metal mounting brackets with slotted mounting holes are available to enable the Service Man to accommodate available replacement controls to most of the special methods of control mounting which are found in some radio chassis, or for attaching the controls to special mounting brackets provided on the receiver chassis. Fig. 8 illustrates several ways of using such brackets.

A narrow bracket may be used, as

shown at *A*, *B*, and *C*, where the control is to be fastened to the panel by means of two screws instead of by its bushing. In arrangements *B* and *C* the bracket is simply bent so that the spacing between the centers of its mounting-screw holes will be the same as that of the holes already in the receiver panel.

Illustration *D* shows the use of a longer mounting bracket, and an extension shaft with its collar and set-screw, when the control is to be mounted to a panel behind the front panel of the receiver. Notice the inverted position of this longer bracket.

In *E* we see the same type of mounting where however the shaft of the control is long enough to make the use of an extension shaft unnecessary. The mounting bracket can be used in the same way as in illustration *F*, if more convenient.

In some types of receivers, particularly auto-radio and communications-type receivers, many parts are mounted by means of such brackets, so some should be included in the Service Man's kit as a matter of convenience and to promote rapid replacement work.

Most controls employed as original equipment on receivers use a standard bushing $\frac{3}{8}$ " long. This has been adopted as standard by the RMA standards committee. Accordingly, a standard $\frac{3}{8}$ -32 bushing, $\frac{3}{8}$ " long is supplied on most commercial replacement controls.

In a few cases it is necessary to

mount replacement controls on extra thick panels. To accomplish this at minimum cost, hex-type shoulder nuts are available as accessories to the control and are sold separately. In using these hex-type shoulder nuts, it is necessary to enlarge the hole in the panel slightly by reaming it. These nuts are screwed on over the standard bushing; the regular flat nut supplied with all controls is not used.

Wire-Wound/Composition-Element Control Applications

Two broad types of volume controls are in general use . . . the composition-element or so-called carbon type and the wire-wound type¹. The former is popular applications of volume controls in cathode and voltage-supply circuits required controls having fair low resistance but a definite current-carrying capacity. Thus wire-wound controls were mostly employed in such circuits. However, the increasing popular practice of using a volume control that controls the audio circuit in AVC receivers, calls for a high-resistance type control which is not required to dissipate much power.

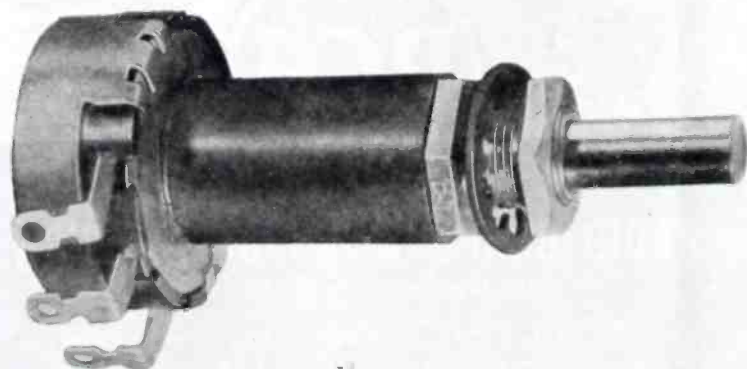
Because it is possible to manufacture the carbon-type control in a greater resistance range and flexibility in the matter of resistance taper², it is the type most used for such control circuits today, especially when intricate resistance tapers are required.

It is obvious that both types have a definite receiver application. It cannot be said that either one type or another is best for all purposes, for each has distinct advantages and disadvantages. Consequently, each type of control is limited in its application to the circuits or conditions requiring the particular advantages of its type.

Substituting Controls

Although volume- and tone-control manufacturers offer both types of controls

(Continued on page 61)



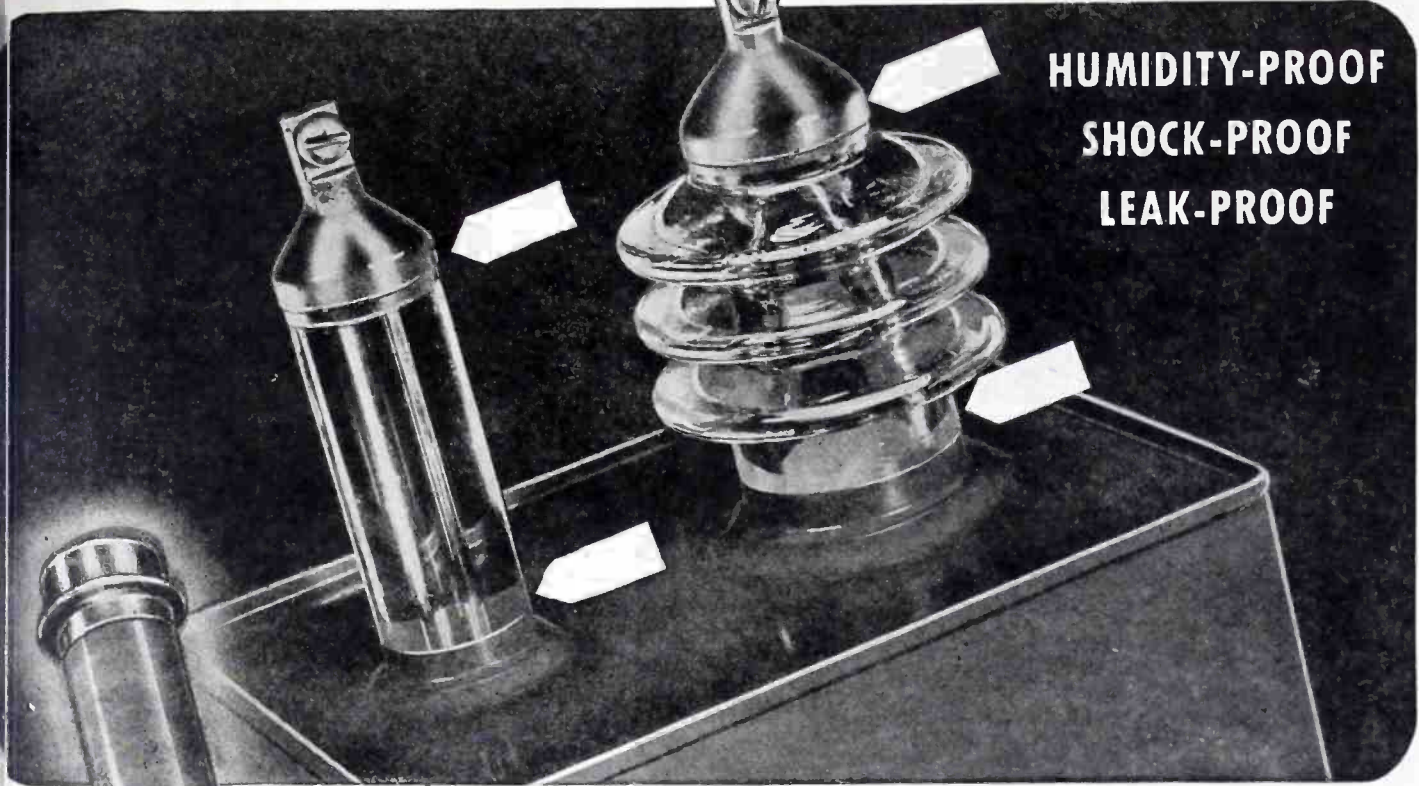
High-voltage insulating coupler applied to control that must be used in high-voltage circuits such as in television, c-r oscillographs, etc.

(Courtesy Clorostat Mfg. Co., Inc.) [Additional data on these couplers will appear in next month's installment.]

¹See Part 6 of this series, August 1944 SERVICE.

²See Part 7 of this series, September 1944 SERVICE.

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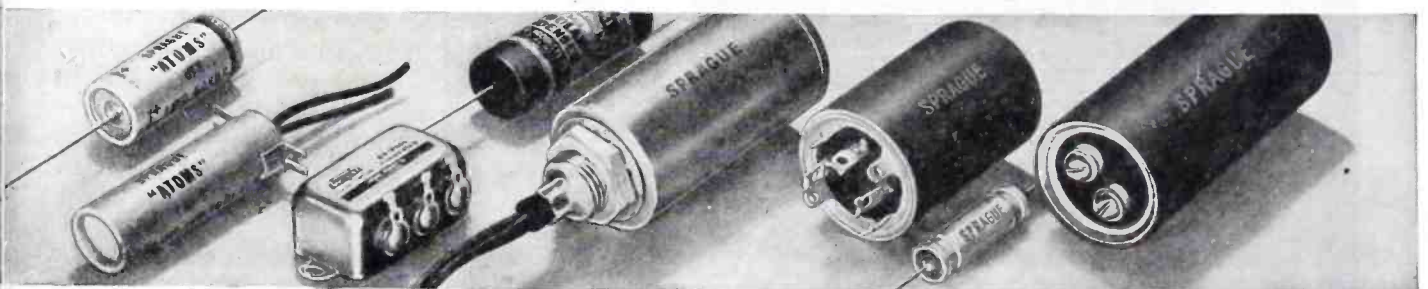
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[Part Two]

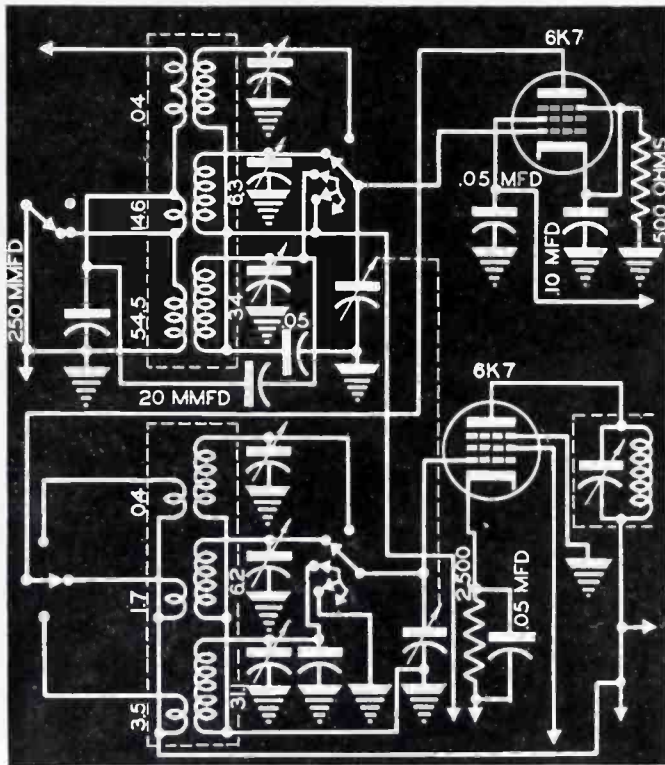
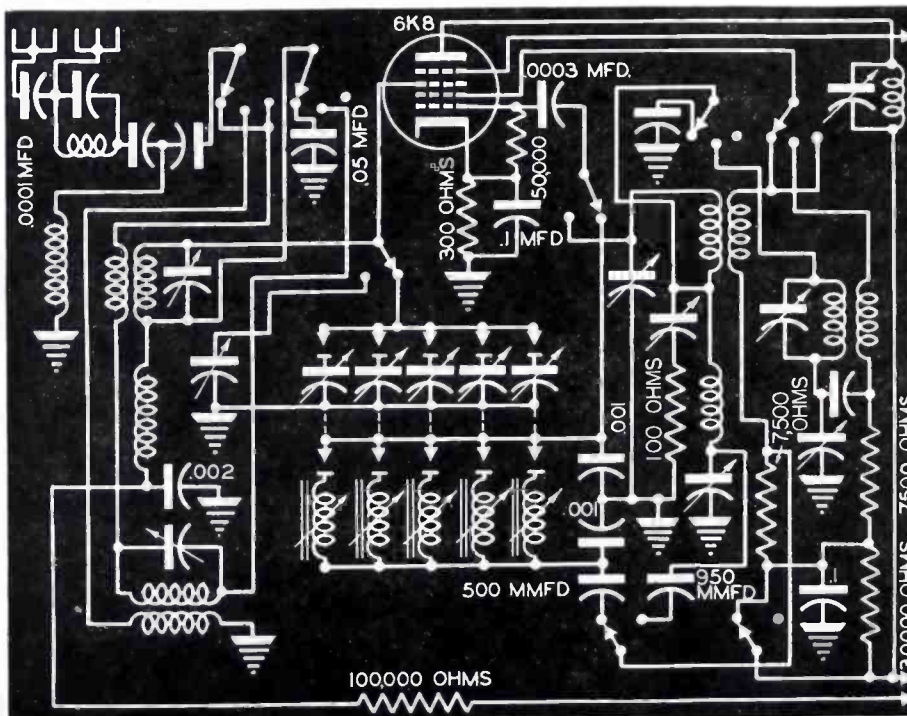


Fig. 11. Mixer circuit of the Ward 62-262. Here, a separate oscillator, not shown, is used. Coupling to the mixer tube is accomplished by tying the oscillator plate to the mixer screen grid.

Fig. 10 (below). Mixer circuit of the Lafayette C-37. A Colpitts-type oscillator is used to simplify the wiring, since only two terminals are required. Note the d-p-d-t switch used to change from manual to automatic tuning.



THE mixer of a 3-band receive Lafayette C-37, using a 6K8, shown in Fig. 10. Provision made for long and short antennas, 456-kc i-f wavetrap, a shunt r-f choke isolated by two capacitors and push button automatic tuning with capacitor tuning for the signal frequency, a permeability tuning for the oscillator frequency. A 300-ohm cathode resistor and 50,000-ohm grid leak provide tube biasing. A Colpitts oscillator circuit with the grid at one end of the coil and the plate at the other end, and the cathode at the potential of the center of the coil by virtue of two .001-mfd capacitors affords a convenient tuning circuit because only two coil terminals are required. The grid is connected through a large .0003-mfd grid capacitor, while the plate is connected through a .0005-mfd capacitor. This is called a shunt-feed system. A 50,000-ohm leak is connected between the grid and cathode. Manual to automatic tuning is controlled by a d-p-d-t switch.

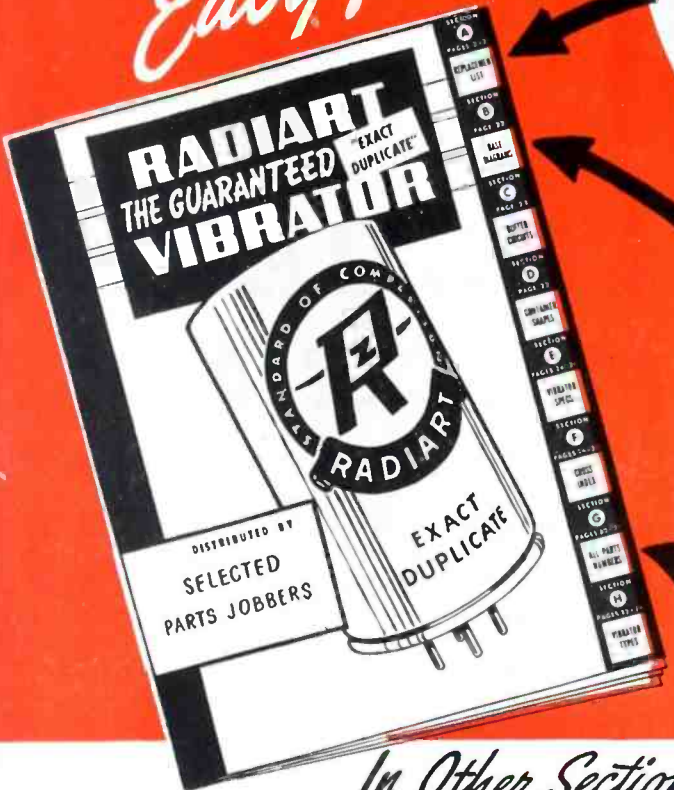
Capacitor-Tuned Oscillator Control

The capacitor-tuned oscillator used in the manual position is also unconventional. On the s-w position shown the grid is connected to the top of the oscillator-tuned circuit. The plate is connected through a tickler coil and .00075-mfd capacitor to the opposite end of the tuned circuit. The junction of the two coils in the tuned circuit is connected to ground through a trimmer and 100 ohms, also through a switch to ground through a .0065-mfd capacitor, virtually shorting the low coil. On the police band the low coil is shunted by a grid coil of second-oscillation transformer. The

(Continued on page 39)

RADIART VIBRATOR GUIDE (Most Complete Published)

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Section A...Vibrator

MFRS. PART NO. RADIART NO. BASE DIA.
SERIES NO. SET MFR. YEAR MADE LIST PRICE BUFFER COND.

CAR MAKER

Name, Model No.	Mfrs. Part Number	Radiart Number	List Price	Base Dia.	Buffer Condenser
CHRYSLER					
C1808 (Elec. P. B.) (Philco—1941)....	83-0027	5326P	3.00	A	.005
25C6 (Wells-Gardner—1938)...	19A32	5437	5.95	AB	.018
600 (Mech. P. B.) (Colonial—1941)...	43697	5301	3.55	A	.004
601 (Colonial—1942)...	911545	5301	3.55	A	.004
800 (Philco—1941)....	83-0027	5326P	3.00	A	.005

Every model listed includes all available data. The correct Radiart Replacement number and other essential information is determined instantly.

SECTION "B"—Cross

Diagram Number	Shape	Voltage	Diam.	Ht.	Freq.	Identifying Characteristics	Max. Load Amps
B 3417	2	6	1 1/4	4 1/2	105	6
3815	9	6	1 1/8	4 1/2	105 Spec. Cup	6
C 5309	1	6	1 1/2	2 3/4	105	6
5331	1	6	1 1/2	3 1/4	105	6
D 4256	1	6	1 1/2	3 3/4	105	10
4256-12	1	12	1 1/2	3 3/4	105	6

In addition to conventional base diagram drawings this section is unique in that it groups all similar base types together indicating readily the differences between vibrators with the same base wiring. All characteristics are shown, including frequency and maximum load limit of each type.

In Other Sections..

- Section "C"—Buffer Condenser Values and Circuits.
- Section "D"—Container Shapes permitting an easy method of "visual" identification.
- Section "E"—Complete Vibrator Specifications arranged numerically by number. Contains necessary data not published in any other replacement guide.

- Section "F"—Long a favorite with users of this guide. The only cross-index of all other manufacturers or merchandisers of vibrators, converting their type numbers to the Correct Radiart Replacement.
- Section "H"—Numerical Listing of Radiart Vibrators. Furnishes complete information as to all models serviced by each unit. Also advises year each type was originated.

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SECTION "G"—Radiart and Original Equipment

Original Equipment Part No.	Radiart Part No.	Original Equipment Part No.	Radiart Part No.	Original Equipment Part No.
75	3283	1974	5301	8539
80-161	5421	2080	3417	8540
82B	5341M	2110	3417	8541
83-0017	5326P	2269	5413	8542
83-0025	5326P	2404	5340M	8601
83-0026	5326P	2501	5411	8602

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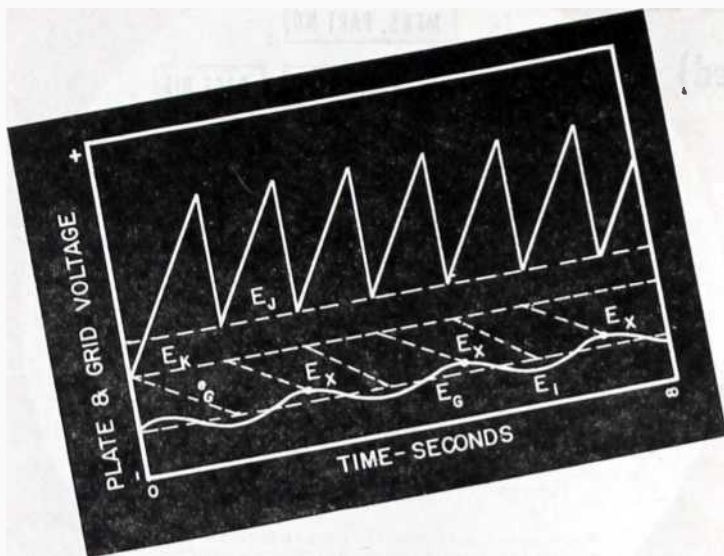


Fig. 1. Graphical synchronization of the linear time-base oscillator system. The critical grid voltage E_c , at which the thyatron conducts, is proportional to the plate-to-cathode voltage E_p . Thus when the timing capacitor voltage, which is the thyatron plate voltage, is near a maximum value, the signal voltage component E_i exceeds the critical grid-to-cathode voltage level. This condition occurs at the critical grid voltage level E_x , and the thyatron relaxes the capacitor charge synchronously with the arrival of the maximum positive potential level of the signal voltage.

C-R OSCILLOGRAPHS SERVICING... APPLICATIONS...

WHERE the oscillograph is utilized to provide a visual analysis of voltage variations, under the condition that the linear time-base oscillation system is not synchronized to oscillate in phase with the frequency of the variation under observation, the image appearing on the screen appears to be in continuous motion. This condition results from the existence of the heterodyne or beat frequency which is developed between the frequency of the voltage under analysis and that of the linear time-base system output.

In order that the waveform appearing on the screen be stationary, it is imperative that the frequencies of the incoming signal voltage and of the linear time-base oscillator synchronize perfectly. Thus, if the image or waveform which is written on the screen varies in exactly the same pattern with each positive motion or sweep of the electron beam, the image of the waveform is written on the screen in exactly the same manner with each succeeding sweep. If, however, the subject waveform occurs earlier in each of the succeeding sweeps of the electron beam, the waveform written on the screen is altered in position with each sweep. Moreover, since the waveform is recurrent earlier in each charging of the linear time-base timing capacitor, the resulting image of the waveform on the electron screen appears to *move to the left*. Again, if the waveform should occur later in each positive motion of the electron beam, a similar alteration of the wave

[Part Five of a Series]

by S. J. MURCEK

image position obtains, and the image appears to move to the *right*.

As a direct consequence of the definite motion which is imparted to the wave image written on the screen by the beat which is present between the two frequencies, it becomes possible to determine accurately the frequency of the voltage variation which is under visual analysis. This, if the motion of the written image is in a left hand direction, the frequency of the signal voltage is greater than that of the linear time-base oscillator. Conversely, if the image motion is in a right hand direction the signal voltage frequency is less than that of the linear time-base oscillator. Zero beat, or synchronization of the two frequencies, occurs when the image is stationary.

For wave- or voltage-variation analysis, it is essential that the image remain stationary. This, in turn, requires that the oscillation of the linear time-base oscillator occur in exact synchronism with the voltage variation which is under analysis. Commercial oscillographs are, therefore, provided with suitable means for the necessary synchronization of the linear time-base system and the signal voltage frequencies. In all of these oscillographs, the

synchronization is usually effected through the modulation of the linear time-base relaxation tube grid bias potential by a portion of the voltage variation.

The synchronizing system utilized in the du Mont 164E oscillograph is shown in the circuit diagram, Fig. 2. Here, the voltage which is under observation is impressed across the synchronization system input terminals H and G . Since the capacitance of the dynamic coupling capacitor C_{12} is large, and the resistance of the synchronization potentiometer R_s is high, the voltage variation impressed across the input terminals EXT and G appears, in the greatest part, across the resistance element of the synchronization control potentiometer. Further, since a portion of this potential appears between the slider arm and the grounded terminal of the synchronization control potentiometer, and is thus directly in series with the control grid of the $2B4$ thyatron, together with the grid current limiting resistor R_{g1} , a part of the signal voltage variation is effectively in series with the thyatron control grid-to-cathode bias potential, the latter maintaining the thyatron control-grid negative. Hence, each positive alternation of the signal voltage effects a reduction of the negative grid-bias voltage present between these electrodes.

The effects of the signal-voltage modulation of the $2B4$ grid-to-cathode potential are evident from the graphical illustration of Fig. 1. Here the

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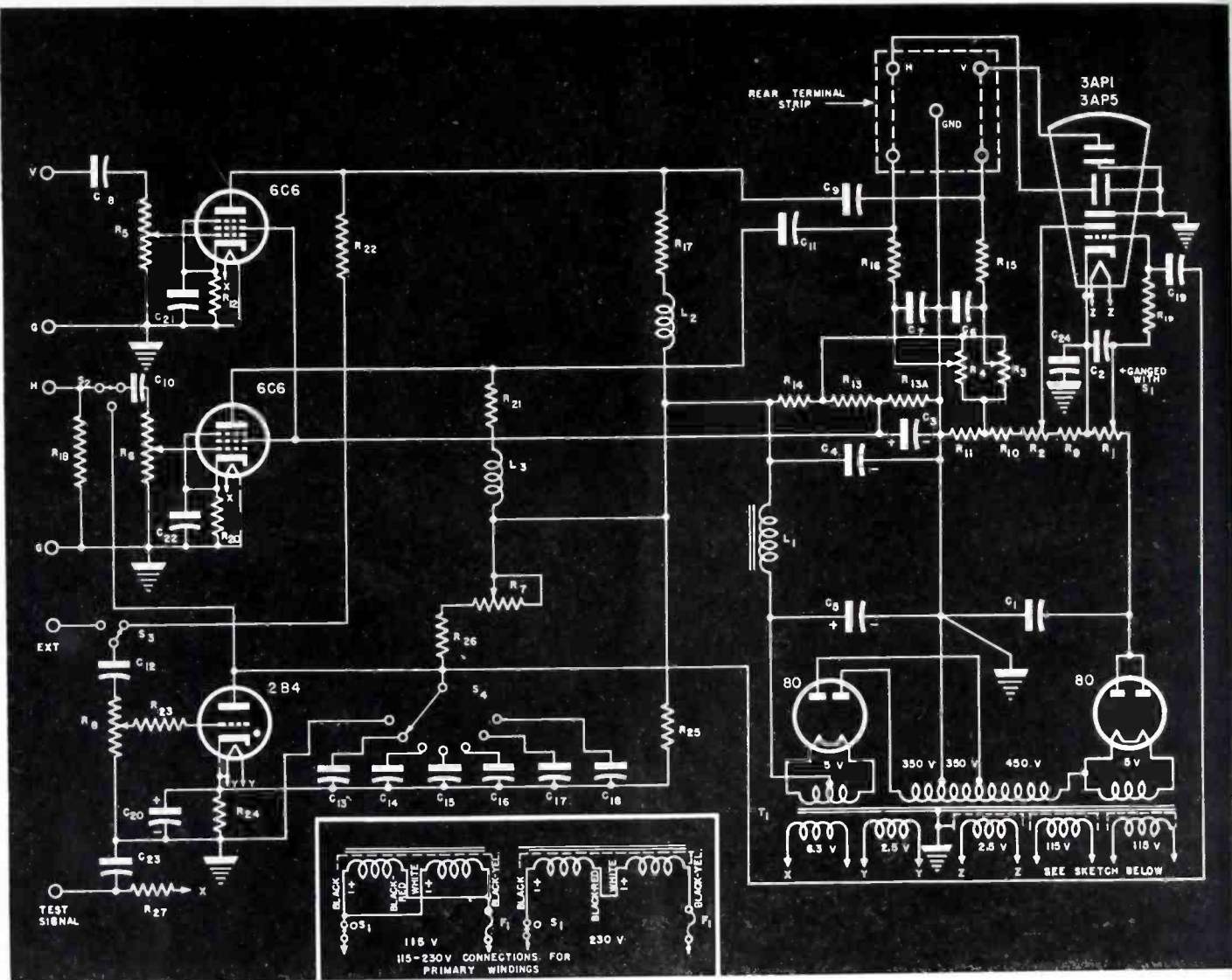


Fig. 2. Circuit of Du Mont 164 E oscillograph.

relations of the various voltage variations occurring in the synchronized linear time-base oscillator operation are plotted with respect to the 2B4 cathode potential level E_k . The d-c component of E_c , which is negative, is shown to be modulated by a portion of the signal voltage variation E_s . Since the critical grid potential E_r is increasingly negative with each increase of the plate-to-cathode potential, E_p , and the latter increases directly in proportion with the charge on the timing capacitor, the positive variations of the grid-to-cathode control voltage eventually exceed the critical voltage E_r . Thus the control grid of the thyratron is effectively positive and becomes conductive, at which instant the tube relaxes the charge on the timing capacitor. Therefore, when the linear time-base oscillation circuit is so adjusted that the frequency of the relaxations is near that of the signal voltage, as we see in Fig. 1, each relaxation must occur in synchronism with each positive alternation or peak of the signal voltage.

Further study of Fig. 1 indicates that thyratron breakdown and the relaxation of the charge on the timing

capacitor occur when the signal voltage attains its maximum positive crest, under the condition that the signal voltage wave is of sine wave form. Since the maximum positive voltage level in any sine wave alternation occurs 90° after the inception of the cycle, the relaxations of the linear time-base capacitor charge occur 90° out of phase with the signal voltage variation. The wave image written on the screen is consequently initiated at the maximum positive potential level in its pattern.

Studying the circuit of Fig. 2, we note that the signal voltage variation required for the synchronization of the linear time-base oscillations is obtained either from the plate circuit of the vertical amplifier, or from the external signal synchronizing voltage source, available through the input terminals *EXT* and *G*. A convenient switch, S_3 , is provided to connect the ungrounded terminal of the synchronization control potentiometer, R_8 , to either voltage source. The series resistor, R_{22} , connected between the *INT* contact of the

switch S_3 and the plate of the vertical amplifier pentode prevents excessive loading of the vertical amplifier plate circuit by the linear time-base synchronizing input circuit. Only a very small portion of the vertical amplifier output voltage is necessary to effect satisfactory synchronization of the two frequencies.

In general, modern electronic apparatus is designed for synchronous operation from low-frequency commercial power sources. Hence, synchronization of the horizontal sweep frequency in the oscillograph with that of the voltage variations usually encountered in industrial electronic apparatus, is most effectively accomplished through a linear time-base synchronization circuit connected directly to a voltage source of the same frequency. This type of operation is especially important where the phase relation of the voltage variation under observation to that of the source voltage wave must be ascertained, inasmuch as such phase relationships are not evident when the synchronizing system is activated by the plate circuit of the vertical amplifier.

Where the synchronization of the

linear time-base frequency to that of the voltage under study is accomplished by exciting the plate circuit of the vertical-amplifier pentode, relaxation of the timing capacitor charge must always occur at the maximum positive voltage level attained by the amplified signal voltage.

Thus, if the maximum positive voltage crest occurs when the vertical-amplifier output voltage is completely out of phase with that of the voltage source wave, the linear time-base capacitor relaxations occur at the maximum positive peak of the amplifier output voltage and are, therefore, completely out of phase with relation to the source voltage wave. Further, if the phase position of the amplifier positive peak voltage swing varies with relation to its initial position, the linear-time base capacitor relaxations must also vary in phase position, and the wave image written on the screen shows no resultant motion. This factor is of great importance where the signal voltage is, for example, the a-c component of a phase-controlled rectifier grid-to-cathode control potential, where the phase position of the a-c component must be shown to vary directly with the operation of the phase-control potentiometer.

When it is necessary to synchronize the oscillograph horizontal sweep voltage with that of the line frequency, or that of the source, it is only necessary to connect the terminal, *test signal*, to that marked *EXT*, and to operate the switch, S_8 , to the *EXT* position. Then the horizontal sweep voltage will be synchronized with the a-c or source voltage frequency, at a 90° phase lead angle. When the oscillograph is operated with this form of horizontal frequency synchronization, application of the input voltage results in the development of a wave image which is initiated at the *positive* zero voltage inflection of the sine voltage wave. The maximum positive crest of the signal potential is shown clearly as a positive peak or cusp in the screen image. Moreover, if the phase position of the signal voltage wave with relation to that of the source voltage wave is varied, the extent of the variation is clearly visible in the motion of the screen image.

Where the oscillograph is operated from a stable voltage source, the voltage present across the phase-shifting capacitor, C_{20} , may be readily utilized to calibrate the vertical deflection system. The calibration is accomplished through connection of the capacitor terminal, *test signal*, to the vertical amplifier input terminal, V , and the subsequent adjustment of the vertical gain control to such a position that the height of the vertical motion of

the luminous spot on screen is twice the division number.

The horizontal voltage sweep-frequency range is arranged for operation over a frequency range extending from a low frequency limit of approximately 12 cps to a high-frequency limit approaching 50 kc. Since this extended range cannot be practicably arranged in a circuit comprising a single capacitor and a single variable resistor or potentiometer, a multiplicity of capacitors, $C_{13-14-15-16-17-18}$, of various capacities are used, together with a *vernier frequency* control potentiometer, R_{20} , and range selector switch, S_4 . Each of these capacitors is so selected that the frequency ranges covered appreciably overlaps the ranges covered by the capacitors adjacent to the former. It should be observed here that the shield terminal of each capacitor is common with the cathode of the relaxation thyatron, and that the maximum potential which is developed across these capacitors is relatively low in level. Further, because of the low-capacitor operational potential, the charge stored is correspondingly low, necessitating the application of high capacitances in the lower-frequency ranges.

It is the horizontal deflection system, together with the linear time-base oscillator, which must be generally depended upon to effect the writing of recognizable waveforms on the screen. Where the signal input or dynamic voltage variation applied to the input terminals of the vertical deflection amplifier is subject to sporadic disturbances or interruptions, the continuous horizontal motion of the beam, effected by the linear time-base oscillator and the horizontal deflection amplifier, prevents accidental damage to the screen which would result with a stationary luminous spot. Hence, before any cathode-ray oscillograph is placed into actual operation, it is prudent to be sure that the beam will be in motion when the cathode of the tube reaches operating temperature.

In the du Mont unit of Fig. 2 the *intensity* or beam control is ganged with the primary or power input control switch, S_1 . Thus, when the unit is placed into operation, it is only necessary to partially turn the intensity control to the a-c line control switch, S_1 to the *on* position. The slider arm is then placed so that the grid is maintained quite negative. This prevents further development of an electron beam during the period in which the tube heaters rise to operating temperature. Then, it is necessary to see that the horizontal amplifier input control switch, S_2 , which is usually ganged with the linear time-base *coarse-frequency* control switch, S_4 , is in the

linear sweep position, if no other form of horizontal deflection potential input is to be used. In this way we can be sure that the beam will be in motion when the beam is permitted to strike the screen.

Since the first plate, or accelerating electrode, is effective in the development of the beam, it is necessary to turn the *focus* control potentiometer knob a complete half-turn in a clockwise direction. The *vertical* and *horizontal* positioning controls determine the normal or *idle* position of the electron screen pattern.

The length of the horizontal sweep pattern is governed by the amplification level at which the horizontal amplifier operates. Inasmuch as no actual deflection of the electron beam occurs if this control is left in the minimum or zero position, it is advisable to advance the horizontal or *X* axis amplifier gain control, in a clockwise direction, at least to the 50% dial position. At this time, the intensity control may be advanced in a clockwise direction until a visible green trace is written on the screen. The intensity of the luminous trace is then carefully adjusted to the desired level or brightness, and focussed to the desired clarity, by manipulation of both the intensity and the focus control potentiometers. Here, it may be found that the horizontal sweep voltage causes the written trace to extend beyond the edges of the electron screen area, causing a visible parasitic glow at either of its extremities. This condition is corrected by appropriate reduction of the horizontal amplifier gain. The final position of the trace may be brought to the geometric center of the screen by the proper manipulation of the vertical and horizontal positioning controls. In the instance of the vertical control, the screen pattern moves *upward* when the vertical control is turned in a clockwise direction, and, in the instance of the horizontal control potentiometer, the pattern moves to the *right* when the control is turned in a clockwise direction.

Under the condition that the controls are in the position just described, the pattern written on the screen will be a short, straight line. If, at this time, an a-c potential is applied to the input terminals V and G of the vertical amplifier, and the vertical gain control is advanced slightly, the beam will be subjected to deflection voltages which operate at a right angle with respect to each other. Briefly, the vertical deflection is perpendicular to the horizontal deflection. The pattern written on the screen is reformed into rectangular coordinates, the actual

(Continued on page 52)

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RADIO CITY PRODUCTS COMPANY, INC.

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ELECTRONIC ALARMS

(Continued from page 24)

once it is tripped it remains closed until opened manually. R_1 limits the plate voltage on tube 2, so that the plate current will not be too high for the positive grid condition of operation.

Although circuits of this kind can be developed experimentally, it usually is better to purchase commercially manufactured products which have had the kinks removed.

Another type of alarm control is

shown in Fig. 2.* The operation is very simple. The oscillator may be tuned to a fairly high frequency, perhaps 7000 kc. If a small change in capacity occurs in the grid circuit, the oscillator plate current will change. Adding capacity to the grid circuit causes a decrease in the operating frequency, which, in turn, causes the oscillator plate current to rise. This increase in current may be sufficient to

cause the closing of a sensitive relay in the plate circuit of the oscillator tube. When the relay contacts close, an external bell system circuit is set in operation, giving the alarm.

In this circuit, C_1 is a small capacitance to limit the detuning effect. L_1 and L_2 represent the oscillator coil, the lower section L_2 serving to provide inductive coupling between grid and plate circuits and develop oscillations. C_2 the tuning capacitor to set the frequency of operation. C_3 and R_1 are the usual gridleak and capacitor, and C_4 is a plate circuit r-f bypass capacitor which keeps the plate-circuit impedance low in value, and aids oscillation.

In a typical installation the pickup wire would be connected to the object to be protected. If the object were a safe, it would be insulated from the ground by rubber pads and serve as the pickup wire. Anyone coming near the safe would upset the capacity of the circuit and detune the oscillator, setting off the alarm. Anyone approaching a door or window where the pickup would be located would also cause the alarm to be set off.

Another type of alarm is shown in Fig. 3. Two metal plate electrodes are used. Normally, they are separated, but when anyone exerts pressure on them the plates touch and the alarm is set off. Once the alarm is set, the relay stays closed, due to a locking arrangement, until turned off manually. Normally, with the plates not touching, the grid circuit of the tube is open, since R may have a value of 10 or 15 megohms. Closing the grid circuit causes the plate current of the tube to rise and the relay swings into operation, causing the alarm to go off.

Thin steel plates are probably the best to use, for they are quite tough and flexible.

Electrically, the steel is not very conductive, but since the resistance can be fairly high and still permit efficient operation of the tube this is no particular disadvantage.

Alarm circuits may also be devised to actuate cameras. The cameras may be concealed in the walls. The relay contacts are simply connected in series with a flashbulb circuit using a couple of dry cells to set off the bulb. The shutter on the camera can be left open. The speed of the flash explosion is sufficient to catch the action without using intricate timing arrangements.

*Some of these circuits are covered by patents and cannot be duplicated for sale to others.

MIXERS

(Continued from page 32)

plate is switched to the tickler of the second transformer. On b-c both the coils of the first transformer are used in series. The plate voltage is increased for automatic tuning by shorting a 30,000-ohm series resistor in the B supply.

Ward 62-262

A complex mixer system with a tuned r-f stage, 3-gang capacitor and a separate 6C5 triode oscillator, Ward 62-262, is shown in Fig. 11. This model uses 6K7s for both r-f amplifier and mixer. Three bands are covered; 148 to 380 kc, b-c and s-w. The antenna transformer has three primary coils in series with a shorting switch for the l-f and b-c primaries, as well as a .00025-mfd capacitor across them. A 20-mmfd coupling capacitor links the b-c primary and the l-f secondary for additional l-f coupling. A separate secondary is used for each band with a combination selector and shorting switch for wavechanging. The interstage transformer is similar except that the r-f amplifier plate is switched to individual primaries.

The oscillator transformer uses separate cathode ticklers for l-f and b-c and a combination of cathode-tapped Hartley and plate tickler for s-w. The mixer tube is excited by cathode-to-cathode coupling through a bias resistor of 2500 ohms and its .05-mfd bypass. The oscillator plate is also directly connected to the mixer screen. The plate is at ground potential at l-f and b-c but is hot on the short-wave band because of the plate tickler. Therefore, this tie to the screen constitutes an additional source of excitation. In some receivers with a separate oscillator, supplementary short-wave coupling is supplied to the signal grid. Still other sets use magnetic coupling between oscillator and converter by winding the coils on the same coil form.

VIDEO WINDOW DISPLAY



One of a series of five window displays used by Gimbel's-Philadelphia to promote the RCA in-store television demonstration being staged by Gimbel's.

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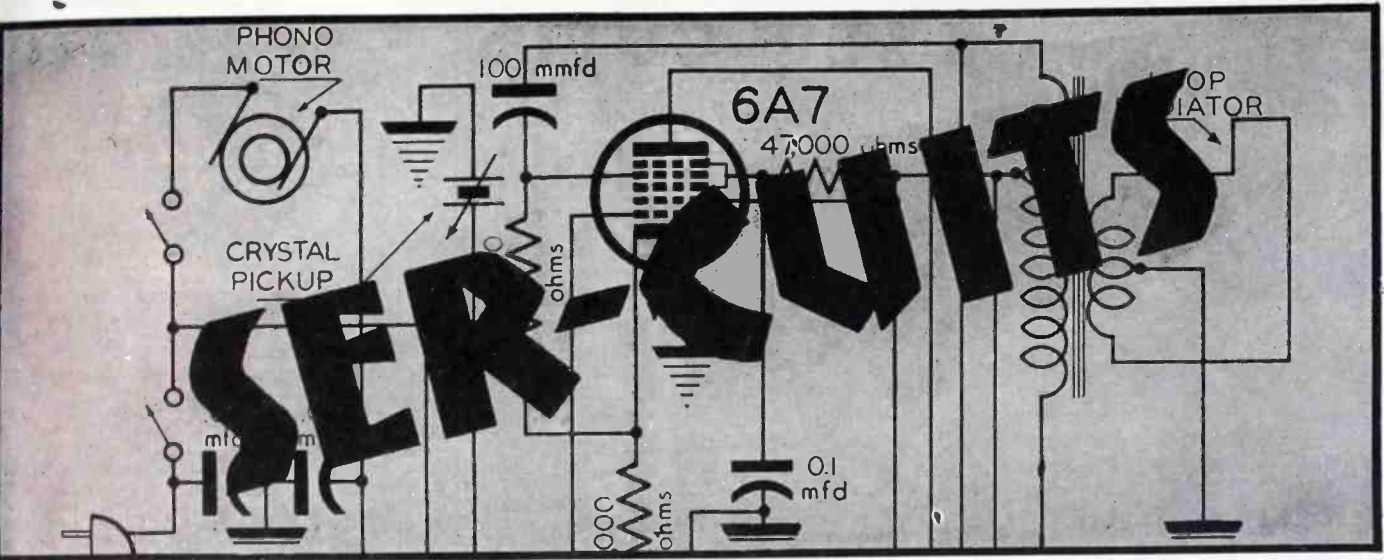
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THE postwar receivers, long anticipated, have now begun to come off the production line. From the circuits of several of the models, just received, we find that quite a few interesting features have been included.

by HENRY HOWARD

a-c/d-c 4-tube and rectifier unit, model 571. One of the features of this model is a fixed bias for the avc bus. This may be considered delayed avc and is ob-

tained from the rectified grid voltage developed by a 12SA7 oscillator across a 22,000-ohm grid leak. Since this voltage is usually of the order of 5 volts, it is necessary to reduce it considerably. This is done by a 15-megohm resistor. This resistor also serves as a filter in cooperation with a .05-mfd bypass capacitor. The filter is required to keep oscillator r-f out of the avc system.

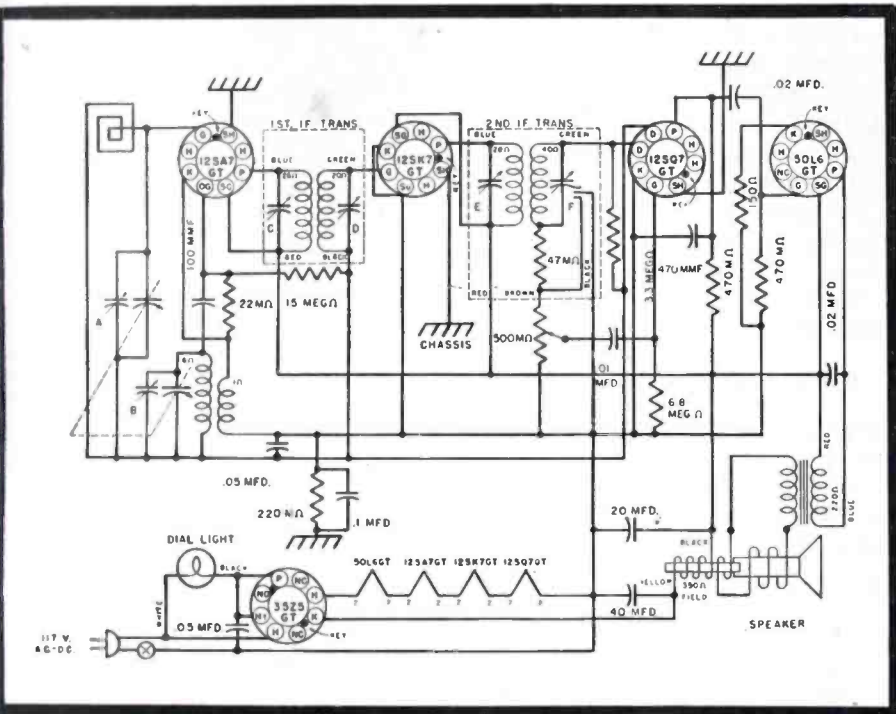
The oscillator uses a cathode-type tickler circuit. Chassis is connected to the B-supply through a 0.1-mfd capacitor and 0.22-megohm resistor in parallel. A 350-ohm series field speaker supplies the only series filter element; no resistors are used in the power supply.

Meck RC-5C5

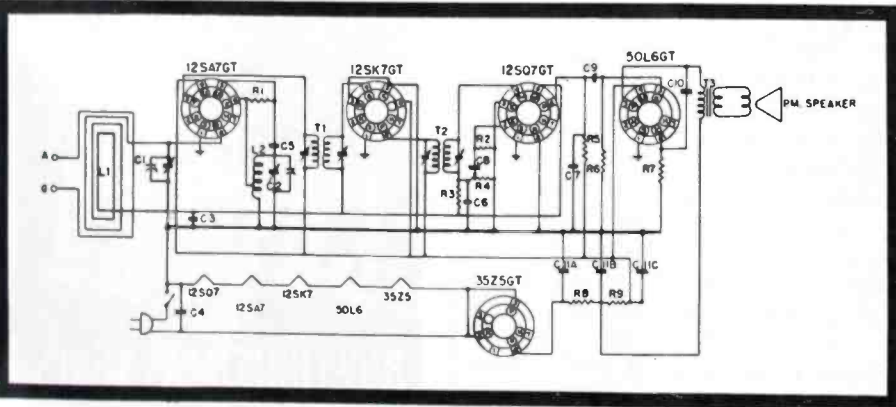
In Fig. 2 appears a Meck Industries postwar loop receiver, model RC-5C5. Provision for an external antenna is also provided in this model. The oscillator is a grounded-plate hot-cathode type Hartley. To afford a negative bias one of the 12SQ7 diodes is directly connected to the avc bus. The 150-ohm bias resistor of the 50L6 power tube is not bypassed.

A p-m speaker is used, necessitating a two-section resistance filter consisting of 200 ohms and 1,000 ohms, the

(Continued on page 42)



Figs. 1 (above) and 2 (below). Fig. 1. Detrola 571. Fig. 2. Meck Industries RC-5C5. List of parts at right.

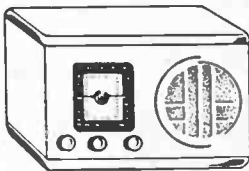


Circuit Symbol	Description	Model
C1, C2	Condenser-Variable, with pulley	RC-5C5
C1, C2	Condenser-Variable, with pulley	RC-5C5-A
C1, C2	Condenser-Variable, with pulley	RC-5C5-B
C1, C2	Condenser-Variable, with pulley	RC-5C5-C
C3, C4, C10	Condenser-Paper, 0.05mfd, 400V	All
C5	Condenser-Mica, 0.00025mfd.	All
C6, C7	Condenser-Mica, 0.00025mfd.	All
C8, C9	Condenser-Paper, 0.01mfd, 400V	All
C11, C11B, C11C	Condenser-Electrolytic 20/20/20 mfd 150V	All
R1	Resistor-Carbon, 20,000 ohms	All
R2	Resistor-Carbon, 10 megohms	All
R3	Resistor-Carbon, 2 megohms	All
R4	Control-Volume, with switch, 1 megohm	All
R5	Resistor-Carbon, 250,000 ohms	All
R6	Resistor-Carbon, 500,000 ohms	All
R7	Resistor-Carbon, 150 ohms	All
R8	Resistor-Carbon, 200 ohms	All
R9	Resistor-Carbon, 1000 ohms	All
L1	Antenna-Loop	RC-5C5, A, B, C
L2	Coil-Oscillator	RC-5C5, A, B, C
T1	Transformer-1st I.F.	RC-5C5-C
T2	Transformer-2nd I.F.	All
T3	Transformer-Output	All
SPKR	Speaker-P.M. 4" round, less T3	All
SPKR	Speaker-P.M. 4" round, with T3	All

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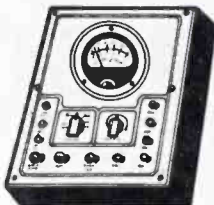
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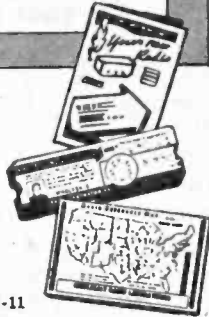
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SER-CUITS

(Continued from page 41)

electrolytic being a triple 20-mfd capacitor.

Detrola 568

A postwar a-c/dc 2-band receiver, Detrola, model 568, is shown in Fig. 3 (page 44). This model has an unusual bandswitch system. The signal grid of a 12SA7 is switched to either the short-wave or broadcast transformer. A supplementary 2.2-mmfd capacitor acts as a capacity coupling from antenna to grid, boosting the high-frequency end. In the circuit diagram the switch is shown in short-wave position. Here the antenna is connected to the short-wave primary through a .002-mfd capacitor, the primary circuit being completed through the bandswitch to B-. The same switch member also shorts the unused broadcast oscillator coil, completing the short-wave oscillator circuit to B-. A third section of the switch connects the 12SA7 cathode to a tap on the short-wave oscillator coil, or to the cathode tickler of the broadcast coil.

A 150-ohm resistor is connected in series with a 100-mmfd grid capacitor. A 5100-mmfd padder is in series with the oscillator coils. Bias for the 50L6 is supplied by an unbypassed 150-ohm resistor. The chassis is connected to B- through a 0.1-mfd capacitor and 220,000 ohms, in parallel.

Garod High-Fidelity Receiver

A prewar high-fidelity a-m receiver with several interesting design features is shown in Fig. 4 (page 44). This model has a variable bandwidth and separate low and high-frequency p-m speakers. The tuner and power amplifier are built on separate chassis, each with its own power supply. A 2-section 10-kc low-pass filter has been included. This may be switched into the audio amplifier between the tuner and power amplifier to minimize interference in the high-frequency audio range, including the 10-kc beat between adjacent channel carriers.

In the input is an iron-core antenna transformer, designed for a short antenna or a long antenna, in series with a .0001-mfd capacitor. A .006-mfd blocking capacitor prevents grounding the antenna. In the tuned secondary circuit is a 150-ohm series resistor. There is a similar 50-ohm unit in the tuned first detector circuit to broaden the response of these circuits for acceptance of an extended treble range.

A 6SA7 converter employs a 300-



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OF SERVICE, published monthly at New York, N. Y., for October 1, 1945.
State of New York } ss.:
County of New York }

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The r-f, converter and two i-f screens are tied to a common supply. The first three stages are supplied with avc bias. The r-f detection components are filtered out by a low-pass filter consisting of 50 mmfd, 100,000 ohms and another 50 mmfd. A ¼-megohm resistor is connected in series with the volume control to prevent overloading of the detector with the consequent distortion. The treble tone control is connected in parallel with the volume control. When the grounded arm is at the lower end of the control, a .001-mfd capacitor is connected in shunt with the volume control, cutting the highs. When the arm is at the top, the .001-mfd unit is in series with a ½-megohm resistor making the shunting ineffective. However a .05-mfd capacitor is connected across a 2,000-ohm cathode bias resistor which causes an increase in highs. This action may be called selective degeneration because the bypassing action of the .05-mfd unit is confined to the treble only, increasing the gain in proportion to the frequency. Low frequencies are not bypassed, so the full amount of degeneration is present.

The 6J5 first audio has a grid leak of only 150,000 ohms. A 6C8G is used for the second and third a-f stages, the gain being limited by interposed feedback from the second audio plate to the first audio cathode and by a 1,000-ohm second a-f bias resistor without bypass. There is also some attenuation in the bass tone control and the associated 15,000-ohm grid leak in the third a-f stage. This control consists of a 2-megohm potentiometer which acts as a variable shunt to a .001-mfd audio-coupling capacitor. The capacitor is so small

(Continued on page 44)



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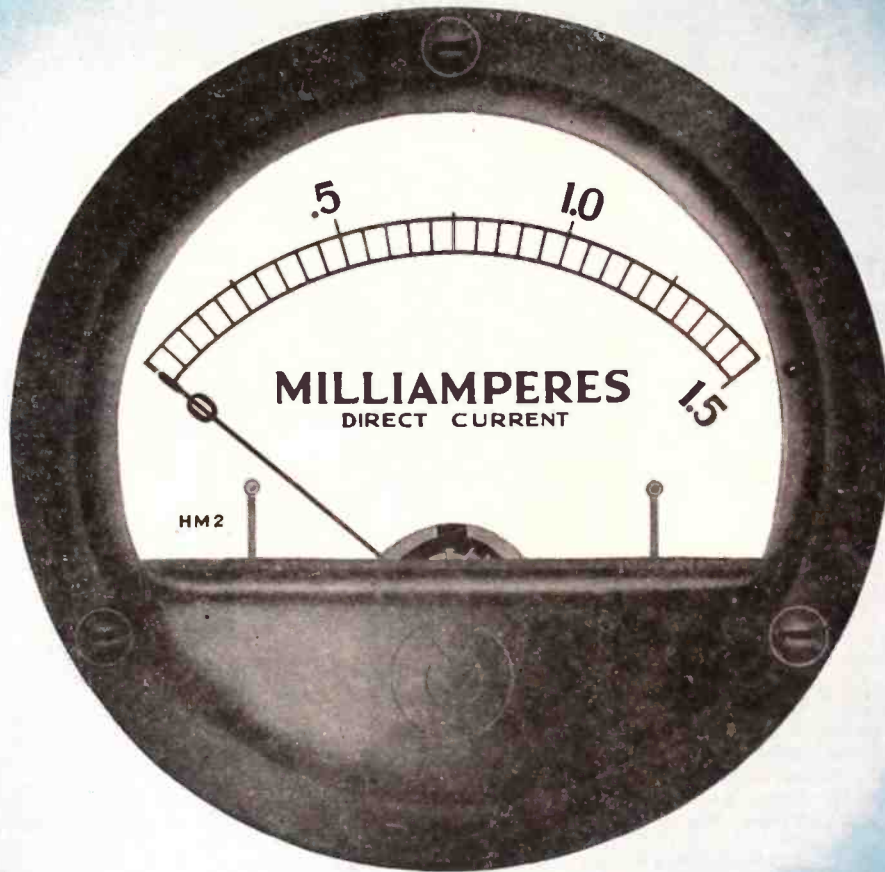
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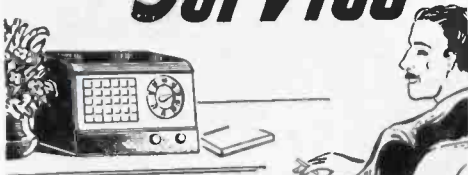
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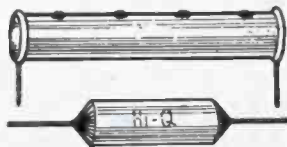
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HIGH FIDELITY AMPLIFIER

(See Front Cover)

A 25-WATT high-fidelity phono amplifier system, Magnavox A-3001C, has been diagrammed on this month's cover.

Pickup-to-Input Circuit

To effect a complete trace of the circuit, the pickup to the first-audio

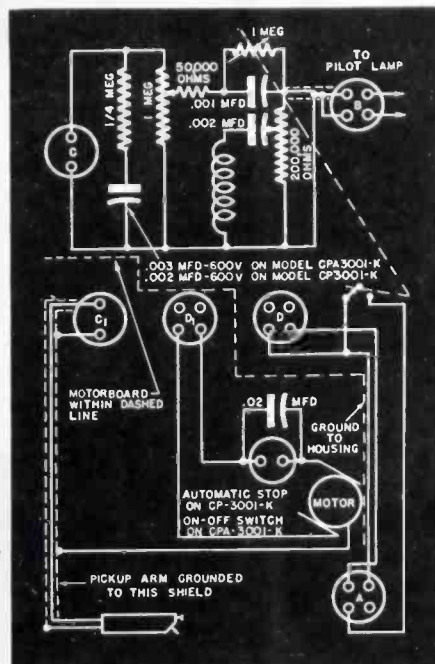


Fig. 1. Input plug system of amplifier, showing pickup and equalizer circuit.

input plug part of the system appears in a separate diagram, Fig. 1. A high-impedance pickup terminates in a 2-pin plug for easy servicing. An equalizer consisting of a .003-mfd capacitor in series with a 1/4-megohm resistor is connected directly across the pickup and a 1-megohm volume control. A 50,000-ohm resistor and bass tone control are located between the control arm and the plug feeding the input grid.

Tone Control Use

This tone control, which is attached to the on-off switch operates a .001-mfd audio coupling capacitor which favors the high frequencies. This is shunted by a 1-megohm control which brings up the bass notes as the resistance is decreased.

Reactance Ratios

Analyzing the actual capacitor-reactance ratios and their effect on bass control we find that a 1-mfd capacitor has a reactance of about 2,600 ohms at 60 cycles and 1,300 ohms at about 120 cycles, which is usually in the vicinity of the lowest bass note reproduced. So a .001-mfd capacitor has a reactance of about 1.3 megohms at 120 cycles and about 32,000 ohms at 4,800

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cles which is around the highest
 te normally reproduced, a difference
 40 to 1. The 1-megohm shunt helps
 e bass along but it has little effect on
 e treble. As the resistance is de-
 ceased, we note that the bass is in-
 creased considerably while the treble
 increased only slightly.

Treble Booster

A treble-boosting tone control is
 so included. More correctly, per-
 aps, this control should be termed a
 ss-reducing control as it shunts a
 oke coil across the line which by-
 asses the low frequencies but allows
 ost of the highs to go by unmolested.
 .002-mfd capacitor in series with
 e choke makes the control non-
 near, particularly near the resonant
 equency of the choke and capacitor.

Hum and Decoupling Filter

A 2-megohm grid leak establishes
 e input impedance of the amplifier
 2 megohms for bass frequencies and
 bit less than 2 megohms for the
 reble. The 6C5 first audio is biased by
 000 ohms and a 20-mfd capacitor.
 ere we also have a separate R-C
 um and decoupling filter. Coupling
 p the power stage is completed by a
 0,000-ohm plate resistor and a center-
 apped grid choke. An equalizer, .02-
 pfd and 7,500 ohms, is in series with
 he blocking capacitor.

External Speakers

Two output impedance taps, 1.12
 nd 2.25 ohms, and an extra plug is
 rovided for an external speaker. The
 oice coils are arranged in parallel
 with the fields in series, excitation be-
 ng provided by the current in the
 5L6 screens and 6C5 plate. A .002-
 nfd 1,200-volt bypass capacitor is
 onnected from plate to plate in the
 output stage. The entire record player
 draws an average of 134 watts from
 he power line.

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I-F AMPLIFIERS

(Continued from page 20)

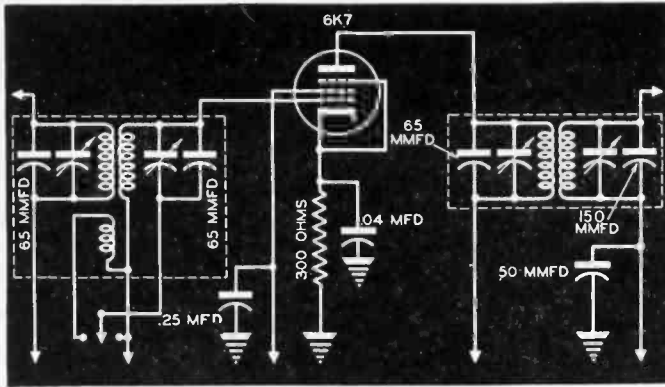


Fig. 7. The Wells-Gardner A-7 variable-width i-f transformer system. The tertiary winding provides tight coupling between primary and secondary, broadening the i-f response. The tertiary winding is shorted out for greater selectivity.

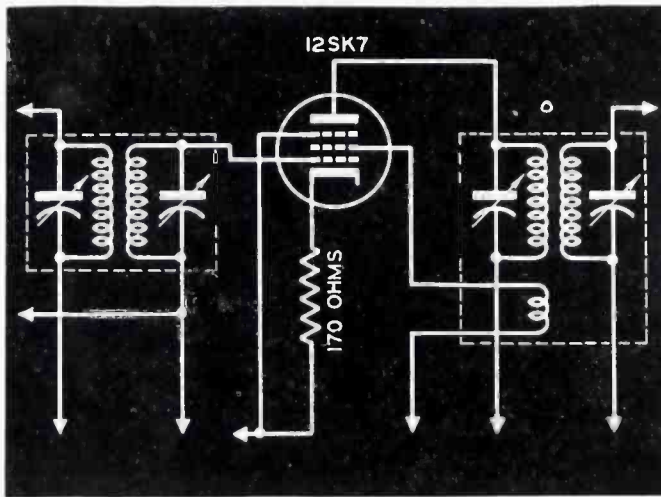


Fig. 8. I-f system of the Westinghouse M-104. The gain of this i-f system is increased by feedback, introduced into the circuit by coupling the screen grid of the i-f tube back into the detector transformer.

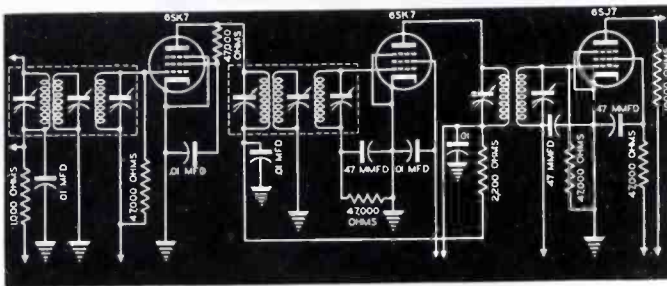


Fig. 9. The f-m i-f of the G.E. 60. Because of the high i-f frequency, and the broadband response, the gain of the i-f stage is reduced considerably. For this reason two i-f stages are usually necessary.

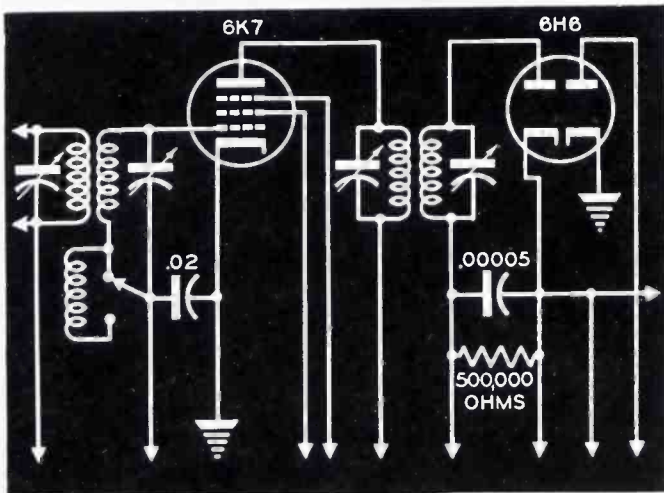


Fig. 10. The sharp-broad i-f system of the Ward 62-319. This circuit is similar to that shown in Fig. 7. A switch across a tertiary winding broadens or increases the frequency admittance of the i-f system.

adjustable, eliminating the need for trimmers. Silver mica fixed capacitors are used instead.

Wells-Gardner A-7

Fig. 7, from a Wells-Gardner model A7, introduces another type of i-f with variable selectivity transformers. The input transformer from a 6J7 first detector has a tertiary winding which is connected in series with the secondary for wide-band reception. It is cut out of the circuit for sharp tuning, the trimmers being adjusted for the sharp position. The band is widened by virtue of the tight coupling provided by the tertiary.

Other methods of selectivity control in i-f amplifiers have included the insertion of resistance in the tank circuit, shunting of the primary or secondary with resistance, moving the coils mechanically and coupling variation by means of a variometer. Combinations of these systems have also been used.

In this model fixed silver-mica tuning capacitors are used in both primary and secondary circuits of both i-f transformers, the first three having a value of 65 mmfd, the detector capacitor, 50 mmfd.

Westinghouse M-104, 204

It is often desirable to introduce regeneration into the i-f amplifier to increase gain or selectivity, or both. Westinghouse uses a method of screen-grid feedback in the detector transformer in models M-104 and 204, shown in Fig. 8. Improved performance is obtained without expensive transformers, but at the expense of critical tuning.

Other means of adding regeneration include removing the bypass from the screen grid and placing a small r-f choke in series with the screen. A 2 to 1 improvement in gain is often possible by such devices, enabling the Service Man to pep up a deficient receiver. If the amplifier tends to oscillate with the series choke, wire should be removed until stability returns.

G. E. 60, 80

The broad band i-f channels of f-m sets preclude the possibility of obtaining high gain per stage, hence at least two stages are required. Also, the gain is not as high at 4.3 mc as at 455 kc, all other factors being equal. The high i-f is necessary, of course, to obtain a wide band simply. In Fig. 9 we have an f-m model of G. E., type 60/80, with a dual 6SK7 amplifier, the first two transformers being triple-tuned. The

(Continued on page 52)

New!

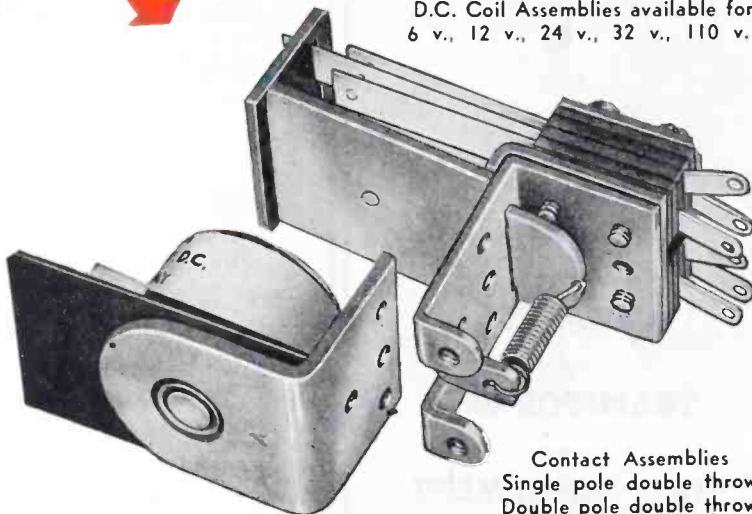
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(Continued from page 23)

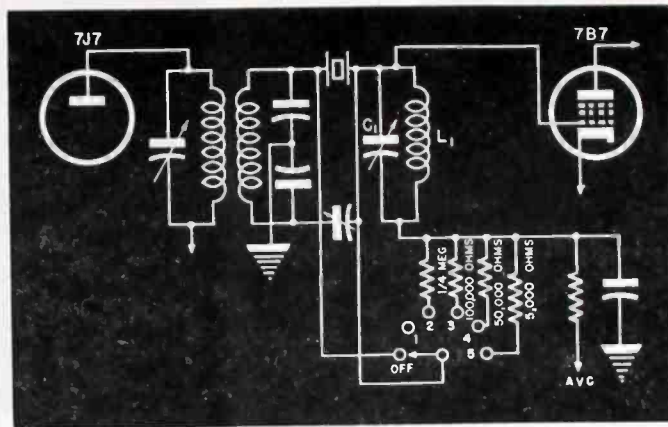
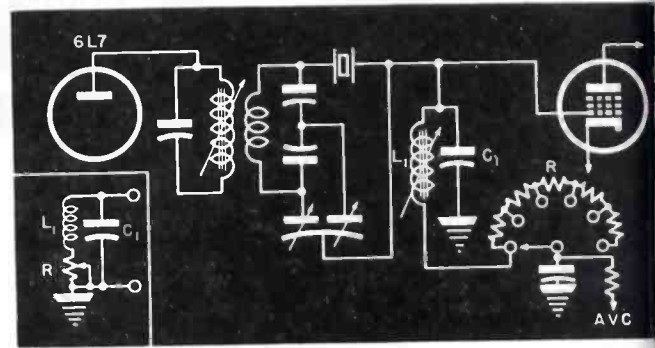


Fig. 5. The variable selectivity system of the RME 41-43. Variable selectivity is accomplished by varying the size of the resistor across L_1C_1 , the larger the value of resistor the greater the selectivity.

Fig. 6. Hammarlund Super-Pro variable selectivity system. Here, the selectivity is varied by inserting resistance in series with L_1C_1 . Increasing the value of resistance improves the selectivity by increasing the effectiveness of the crystal.



detunes the circuit, and permits the crystal to exert its greatest influence on circuit Q , or sharpness of resonance.

RME 41-43

Fig. 5 shows the variable-selective circuit used in the RME model 41-43. The tuned circuit here is on the crystal output side instead of the input. The effective resistance of the tuned circuit represented by C_1 and L_1 in series with the crystal is varied by shunting it with various size resistors, in very much the same manner as is used to broaden the response of i-f transformers used in f-m receivers. The lower the value of the shunting resistor, the greater will be the effectiveness of the

crystal and the resultant selectivity.

Hammarlund Super-Pro

In Fig. 6 we have the method applied in the Hammarlund Super-Pro. Here again, resistance is used to increase the effectiveness of a tuned circuit in series with a crystal filter. However, the resistance is used differently than for the circuit shown in Fig. 5. The Q of a coil is a function of its reactance over its resistance, $Q = X/R$. Since the resistance is introduced into the tuned circuit so that it is in series with L_1 , and C_1 is across both the resistance and the inductor, the effective resistance of the circuit as represented by L_1C_1R is reduced and C_1 then acts as a bypass capacitor. Thus the effectiveness of the crystal is increased.

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CENTERING CONES

(Continued from page 16)

lost. Every effort is made by the manufacturer to build his loudspeaker so it will stand up not only for normal operation, but that it has a safety factor which will permit some limited amount of abuse or abnormal operation without affecting the performance.

When confronted with a rubbing voice, the Service-Man can do one of two things.

First, he can replace the whole speaker with a new one and second, he can try to repair the one that is damaged.

In these days when production is so high and the demand so much, there is little time in trying to replace the unit when the chances of getting a new speaker are slim, if indeed. Therefore, the Service-Man usually tries to repair it.

A new development, the *Adjust-A-Voice* unit, developed by Quam-Nichols, is an effective solution to the rubbing voice-coil problem. In this unit, the voice coil, instead of being permanently attached or fastened to the housing, is kept in position with a pressure or clamping ring which is in turn held down by two clamping screws. This construction is illustrated at A in Figure 1, the inset showing a closeup of the pressure ring, which is underneath, at B, and the spider, which is designated at D.

Loosening the screws holding the pressure ring (A in the illustration) will permit a small amount of movement of the spider in a lateral manner which will allow the voice-coil to be centered around the pole-piece and within the gap.

It is to be noted that the screws holding the clamping ring are so positioned that it will be often unnecessary for the Service-Man to remove the loudspeaker cabinet to re-center the voice coil.

In conditions of severe rubbing voice coils, a better job can be done by moving the speaker from the cabinet; when in either instance, no audio signal generator is necessary, and only the radio (or public address system) or voice signals are required for testing and maintenance.

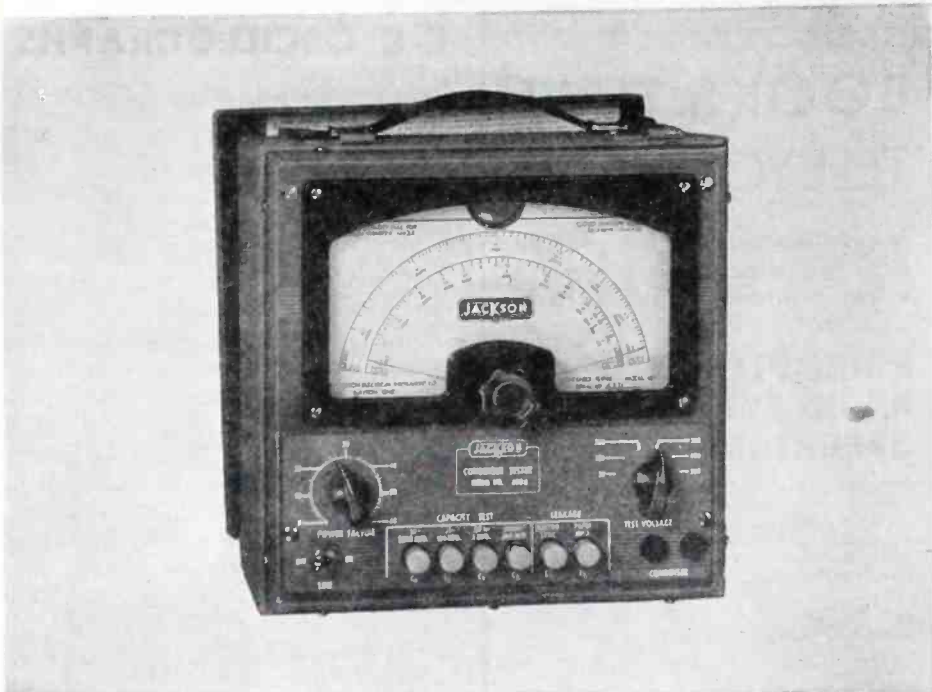
The repair of a speaker with this new unit is quite simple. Before attempting to re-center the voice coil, one first determines on which side the voice coil is rubbing by pushing it up and down in the gap. Then it is necessary to loosen the clamping ring screw nearest the point of the rubbing is found. Using the screwdriver, the voice coil is gently pulled toward the loosened clamping screw. The screw is then tightened and a check made to see if the voice coil now rides freely.

Caution should be used at this time not to be too violent with the screwdriver because of the possibility of breaking the juncture of the voice coil and the cone neck.

If this operation does not correct the rubbing voice coil, another method will have to be employed. One must first remove the felt dust cap over the voice coil by saturating it with lacquer or thinner, allowing it to soak a few minutes before picking it off. Then strips of ordinary wrapping paper approximately 5/16" wide by 1 1/2" long should be cut.

The clamping ring screws should be loosened until the clamping ring is free, then the wrapping paper shims are inserted.

(Continued on page 52)



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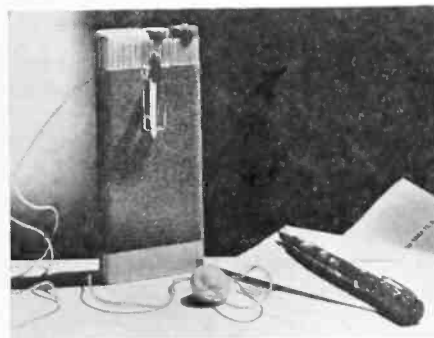
C-R OSCILLOGRAPHS

(Continued from page 37)

form depending on the settings of the linear time-base oscillator controls. In any event, the characteristic sine wave form of the a-c supply frequency waveform is evident in the pattern.

Manipulation of the linear time base coarse and vernier sweep frequency controls permits the reduction of the pattern written on the screen to either a single a-c wave pattern, or to a pattern containing a number of similar a-c cycle forms, whichever may be desired. In either case, the pattern will appear to be in motion, and complete synchronization of the sweep frequency with that of the a-c supply source will be found difficult. If, however, the test signal terminal is connected to the linear time-base synchronizing voltage input terminal *EXT*, synchronization control selector switch, *S_s*, turned to the *EXT* position, and the synchronization control potentiometer advanced slightly, the written wave pattern will stabilize completely. The wave pattern being written from the positive zero voltage inflection due to the phase-shift will be effected by the positioning capacitor *C₂₃*.

MINIATURE POCKET SETS



Five-tube pocket receivers produced by Belmont, using Raytheon sub-miniature tubes. Case is 3" wide, 1/4" thick and 6 1/4" high. Weighs 10 ounces, including batteries. Circuit is super-heterodyne. Cases will be supplied in solid gold, sterling silver, morocco, suede, etc.



RECENTERING CONES

(Continued from page 51)

serted between the voice coil and pole-piece (the inside of the voice coil). The three strips are not used one on top of the other, but merely to assure that at least one thickness of the strip circumscribes the pole-piece entirely. The final step the clamping ring screw should be tightened a little at a time, tightening first one, then the other, gradually and alternately so as to bring clamping action to bear on the ring evenly all around.

This should result in a perfectly centered voice coil. The wrapping papers can then be removed, and the dust cap glued back on with lacquer cement.

I-F AMPLIFIERS

(Continued from page 48)

third transformer which feeds the limiter stage is a conventional detuned job.

Ward 62-319, 329, 409, 419

Another receiver using sharp-tuning (i-f of 465 kc) is shown in Fig. 10, Ward 62-319, 329, 409, 419. The input transformer has a switchable tertiary winding similar to that shown in Fig. 7. The output transformer feeding the 6H6 detector is standard.

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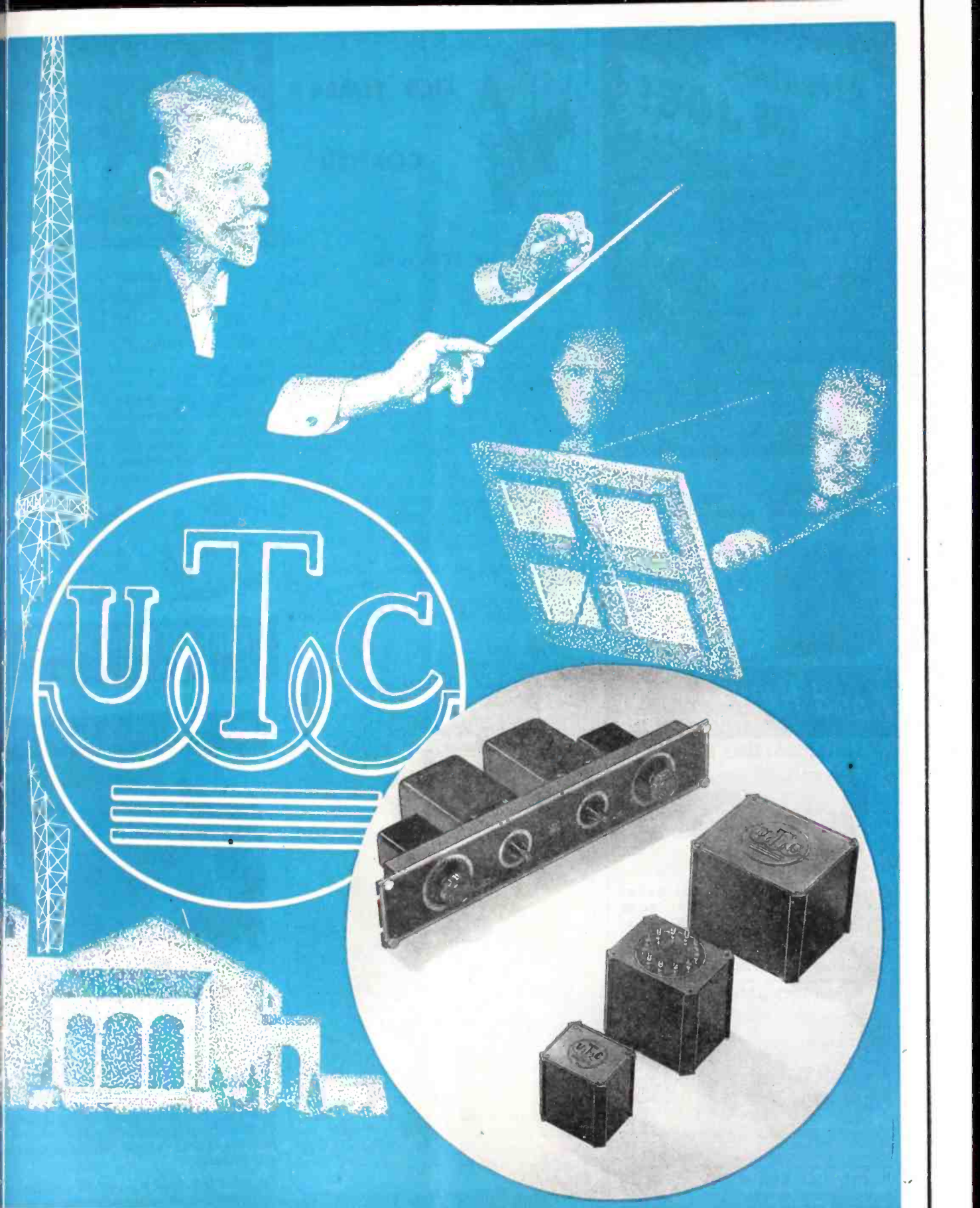
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OLD TIMER'S CORNER

by **SERVICER**

WE had quite an unusual session at an end-of-the-day get-together some weeks ago, a session that provided many unusually interesting and useful facts.

It all began when Roy walked in quite pleased with himself.

"What's with you, Roy?" I asked. "You sure look spirited."

"Well, fellows," said Roy with a grin, "I have just made a swell contact."

"What kind?" we asked.

"With a manufacturer of capacitors," answered Roy. "With my plans I will be able to cut out everybody except the manufacturer. No more distributor, and no more company representative for me. I'll deal right with the capacitor maker, direct."

"What will that mean in dollars and cents?" we asked him.

"Well, I should be able to buy at better prices. Then deliveries will be faster, and also I'll have a wider choice than any of you have been able to get from John's Radio Company, the distributor up here. That in itself is worth the deal to me. But best of all I will be buying at rock-bottom, manufacturer's prices!"

"I think you're dead wrong, Roy," said Bill.

Bill's Opinion

We picked up our ears. Bill was one of the older crowd who usually did not have anything much to say. He and his type just went ahead year in and year out, not making a very big splash in the waters of radio servicing business, but at the same time syphoning off a fair share of profits and keeping themselves high in the opinions of the community. Bill was not only conservative, but he was also highly respected for his ethics, business acumen and community pride. He was no world-winner, but his hard-headedness and carefully thought out plans often wrung a lot of silent (and sometimes not so silent) acclaim from our gang.

So when Bill fired his opinion at Roy, we were quite surprised.

"You see, boys, Roy thinks that he has made a world-winning deal by cutting out the distributor! Well, instead he has just done himself a great disservice! Sure, this particular manufacturer probably now has almost everything in stock that Roy could want. And he's anxious to get it out. So he'll do almost anything to see that Roy gets what he wants. But wait until this man-

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60 Watts — 1/4 in. Tip
Only 9 in. long. Wt. only 8 oz.

This mighty mite is backed by DRAKE's 25 years of soldering iron manufacturing experience. The high quality and long-service of DRAKE Soldering Irons have made them outstanding favorites with all types of radio men everywhere. The DRAKE No. 400 is an outstanding value at



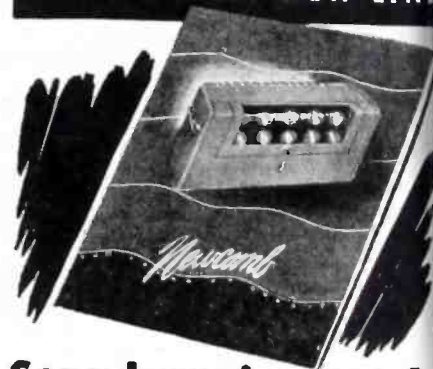
Only **\$4.50**
List

Drake Has an Iron
for Every Purpose.
Ask Your Radio
Parts Jobber

DRAKE ELECTRIC WORKS, INC.

3656 LINCOLN AVE. CHICAGO 13, ILL.

AN ENTIRELY NEW LINE



Sound equipment by NEWCOMB

Our newest amplifiers offer greater excellence in sound reproduction than ever before available to the public address field. Designed by an organization devoted exclusively for seven years to the perfection of sound equipment, they embody all the benefits of today's most advanced electronic achievements.

Send for the catalog . . . you'll find no other amplifier has so many advantages.

THE SOUND OF QUALITY

Newcomb

AUDIO PRODUCTS CO.
MANUFACTURERS

DEPT. E. 2815 S. HILL STREET
LOS ANGELES 7, CALIFORNIA

er—and I'm sure that he is not the old line men—gets going. He gave a big business some day. And he will recognize that it doesn't have Roy's orders lying for, say, ten 25-mfd 25-volt electro's, and two dozen .05 mfd's and a couple ten half mikes at 450 volts. He is to tell his production men to set aside until he gets into those runs for a set manufacturer. Thus of the capacitors Roy wants, will be only run through with the manufacturer. Now the .05 mfd's that are made for the set manufacturer are very different in size than the type ordered before, and so Roy gets the size which may or may not fit. Also price may be different each time, due to change in specifications.

Replacement Problems

and that isn't all. Suppose that Roy ordered some faulty capacitors. Can he get immediate replacements? No, not, for at that very time the type he ordered is out of stock, and another size is being run through, a size of no use to him.

So poor Roy will have to wait until the manufacturer runs through the kind Roy wants before he can get his replacements. Now since Roy has been dealing with the manufacturer directly, he not only has lost contact with the local distributor, but he has also encouraged that worthy to discontinue him. As a result, Roy can't get his capacitors from the distributor.

So he must go out and buy them himself, or hope that one of you—or me—will help him out for the time being. Normally, we would be more than willing to help out a fellow Service Man—especially Roy, because we all like to help. But business is business, and we don't like to have the returned capacitors be similar to those we gave Roy. We are not interested in the few cents that the capacitors cost. What we are interested in is some of Roy's units when his next shipment gets in. But Roy isn't going to receive the same standard parts we have been using, even when his shipment arrives. And we are not sure of exactly he is going to get. So don't let him have any of ours, and he will find himself in quite a spot!

Virtues of Distributors

Now, if Roy trades with the local distributor he'll get what he needs right from the distributor's stock. The distributor pools all of his orders and sends them in to his standard manufacturers as they make, taking in all the Service Men accounts of the distributor, and order and quite a run. If something goes bad with the units, the manufacturer cannot afford to ignore the distributor, and so he makes it good. The distributor knows that and will replace defective units for Roy on sight. Then, the distributor is a local man. Every time Roy buys from him and pays his bill promptly, he establishes a better relationship. That may come in handy when time rolls around and Roy needs a reference. Some of the boys just think much of references from an out-of-the-state place where people don't know each other except via the postage stamp route.

33 well overlapped ranges . . .

plus long-life dependability!



WESTON

(Model 665 Type 1)

VOLT-OHM-MILLIAMMETER

Its compactness, versatility and rugged dependability make Model 665 the ideal instrument for use in the field, or in the shop . . . whether servicing communications equipment, testing electrical components in production, or research or maintenance work. Provides 33 AC and DC voltage, DC current, and resistance ranges . . . with simplified switching arrangement for rapid operation. Built to WESTON standards to assure dependable measurement accuracy throughout the years. Full details on request. Weston Electrical Instrument Corporation, 605 Frelinghuysen Avenue, Newark 5, N. J.

WESTON Instruments

"So if you want some sound advice, play ball with your local distributor. The prices may seem a bit higher than those a manufacturer selling direct may offer. But when the smoke clears away, you are getting so very much more for your dollar in the form of reputation, good will and fine service, that in reality the costs are cheaper."

No Sale

"I think you have something there, Bill," said Roy. And from the way he spoke, I guess that a certain manufacturer, who sells capacitors directly to the radio Service Man, had just lost a fairly nice account.

POSTWAR RECEIVER



Receiver of the future shown at a recent postwar display by the Hallicrafters, Chicago.



Plug in METAL TUBE RESISTORS

★ To facilitate the servicing of AC-DC sets equipped with plug-in metal-tube resistors, Clarostat offers 10 Universal Types which replace 90% or better of the original numbers.

The Clarostat Universal Type operates within voltage ranges specified on tube, regardless of what pilot current is drawn or of any pilot light combination. Operates regardless of burnt-out pilot lights, and well within the .3 ampere range required for tube filaments. Operates efficiently regardless of line-voltage variation.

★ Ask Your Jobber . . .

Ask for these Clarostat plug-in metal tube resistors. Type MT. Ask for other servicing aids—controls, resistors, attenuators, etc. Ask for latest catalog—or write us direct.



CLAROSTAT MFG. CO., Inc. • 285-7 N. 6th St., Brooklyn, N. Y.



RAYTHEON BONDED SERVICE MAN PROGRAM

A Bonded Electronic Technician Program to improve standards of practice among Service Men and provide work guarantees, has been announced by the Raytheon Manufacturing Company. The program provides for the bonding of Service Men through the facilities of Raytheon distributors, Raytheon and a bonding group.

According to Arthur E. Akeroyd, distributor sales manager, the program will assist the Service Man in building a solid foundation for postwar activities.

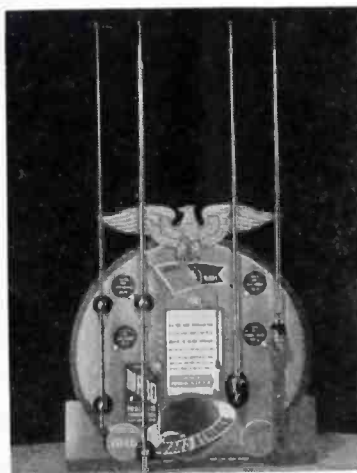
It will offer deserving newcomers such as returning veterans, the opportunity to establish themselves in business, without being handicapped by the questionable practices of some widely publicized repairmen.

Mr. Akeroyd said that it was felt that the plan should be based on guarantees to the much maligned Service Man as well as the customer. Every radio shop is entitled to a legitimate profit, he said. Thus with widely divergent costs under different conditions and in different locations, any bonding program must not interfere with the established business policies of the ethical shop. By the same token, the program must also recognize the fact that the majority of Service Men are honest. The bond provided by this program will assure the public of the Service Man's honesty and integrity, said Mr. Akeroyd.

To qualify as a Raytheon Bonded Electronic Technician, a Service Man will have to meet certain qualifications of experience, reputation and ability, and also state that he has and will use adequate equipment to do skilled service work efficiently.

The Service Man's application will have to be approved by his Raytheon distributor, Raytheon and the bonding company. When accepted by all parties, he will become bonded for the period of one year by the Western National Indemnity Company of the Firemen's Fund Group. The bond states that the Service Man agrees to guarantee complete satisfaction

POSTWAR ANTENNAS



Ward store display featuring four postwar antennas. Highlights of the antennas are said to be H-Q low-loss detachable polyethylene lead with silver-to-silver contact; one man installation and fluid type anti-rattle construction.

MUELLER



CLIPS

For Quick Temporary Connections

- Made in 10 sizes—from the tiny wee-pee-wee to the 300 ampere Big Brute.
- Offered in both steel and solid copper.
- Red and black rubber insulators to fit each size.
- A complete line with

A CLIP FOR EVERY PURPOSE

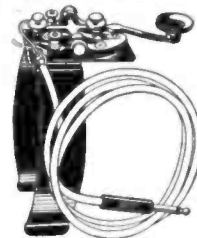
Send for free samples and catalog 810

Mueller Electric Co.

1565 E. 31st St. - Cleveland, Ohio

MONEY-SAVING SPECIALS

Immediate Delivery. Orders filled same day received.



AIRPLANE
CODE KEY
\$2.25

Knee type. Strong spring holds securely. Black enamel and brass finish. Complete with plug and cord. Limited supply. Order now. Only—\$2.25

DESK TYPE KEY—\$1.69

Cadmium plated. A good practice key for amateurs.



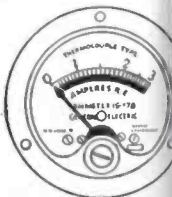
PL-55 PLUG—34¢

A high grade, dependable plug.

G. E. AMMETER

General Electric Thermocouple R.F. type—only \$4.95.

NEW ITEMS DAILY
Tubes . . . test equipment
. . . meters . . . cords and
cables . . . condensers . . .
resistors . . . switches . . .
speakers.



Write for bulletin listing hundreds of items

Lifetime

SOUND EQUIP. CO., Dept. 65

911-913 JEFFERSON AVE., TOLEDO 2, OHIO

every radio repair job for 90 days, outlines a code of ethics that he expects to observe in the conduct of his business. Mr. Akeroyd said that the requirements for certification have been drawn up so that they parallel the now generally accepted practices and standards of the competent qualified Service Man. The requirements do not represent the ideas of any single group, but rather the suggestions and opinions of hundreds of Service Men. Adequate provision is said to be provided to prevent the exclusion of any Service Men from this program, without prejudice, in the event that they feel rejection is not justified.



A. E. Akeroyd

GRENBY BUYS CARDWELL
 Grenby Mfg. Co., Plainville, Conn., has acquired full control of The Allen Cardwell Mfg. Corp., Brooklyn, N. Y. W. L. Gray, president of Grenby, has become chairman of the Cardwell board. Plans for the sales and development engineering departments of Cardwell will continue to operate from their present location at 81 Prospect St. The manufacturing division has been moved to Plainville, Conn. Mr. H. Soby, vice president and director of Grenby, has been elected president of Cardwell, following the retirement of Mr. Cardwell. Joseph K. Fabel will continue to serve as vice president and sales manager of the Cardwell development and engineering division. Ray Breckhouse will also continue as Cardwell sales manager.



C. A. Gray

CAPACITOR COLOR CODE CARDS
 Color code charts and cards for small capacitors with RMA six-dot color code and three-dot color code as well as Army-Navy standards, have been prepared. (Continued on page 58)

N. U. DISTRIBUTOR ON RANCH



Olsen, National Union distributor in Antonio, with Jack Clune, N.U. sales manager, on the Olsen ranch.

Wait for these new

HICKOK

Radio Service Instruments



Model 532
Tube Tester

If It Isn't A Hickok Indicating
 Micromhos It's Not
 Dynamic Mutual Conductance

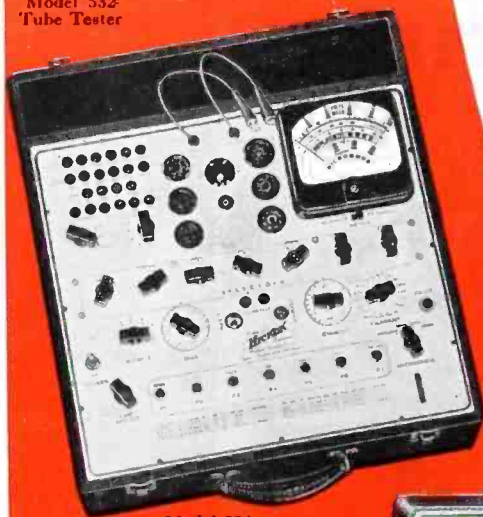
Your patience in waiting for these new 1946 HICKOK models will be richly rewarded for these new HICKOK tube and set testers make still closer tests, with finer accuracy, rejecting tubes that might get by with an ordinary tester.

Now you have 7 selector switches instead of 2. That aims to prevent obsolescence. Isn't that worth waiting for?

What's more, Dynamic Mutual Conductance, indicated in Micromhos, is a duplicate of the manufacturer's method of checking when he makes the tubes. Remember, if it isn't a HICKOK Indicating Micromhos, it isn't Dynamic Mutual Conductance.

The new Electronic Volt-Ohm-Capacity Milliammeter Model 203 reads as low as 1.0 mmf and up. It will measure at frequencies to over 10 mc with no frequency error and the ohm meter will measure up to 10,000 megohms.

Keep patiently in touch with your jobber and you will soon get the instruments that are held in highest esteem.



Model 534
All Purpose Tube and Set Tester

**THE HICKOK
 ELECTRICAL
 INSTRUMENT CO.**

10521 Dupont Avenue
 Cleveland 8, Ohio



Model 203
Electronic Volt-Ohm-Capacity Milliammeter

NEW SOLDERING GUN

THE SPEED IRON*



Soldering Heat in 5 Seconds

Wherever you have a soldered joint in radio, electrical or electronic repair and service work, the Speed Iron will do the job faster and better.

The transformer principle gives high heat—in 5 seconds—after you press the trigger switch. Convenient to hold with a pistol grip handle, the compact dimensions of this new soldering tool permit you to get close to the

*T.M. Reg. U. S. Pat. Off.

joint. The copper loop soldering tip permits working in tight spots. The heat is produced by the high current flowing through the soldering tip—permitting direct and fast transfer to the soldered connection.

If you want to save time on soldering jobs with a tool that is ready to use in 5 seconds, get a Speed Iron today. See your radio parts distributor or write direct.

WELLER MFG. CO.
DEPT. S-1 • EASTON, PA.



UNIMETER

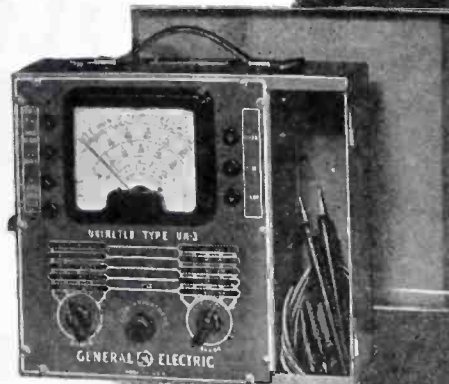
This unit fulfills an extremely important need for general utility portable service equipment. It has wide range coverage for both a-c and d-c measurements of voltage, current measurements on d-c and the popular ranges on resistance.

The UM-3 is designed to clearly indicate all the functions which aid in the prevention of application of high voltages when preparing for current or resistance measurements.

Other G-E units for better servicing include: Tube Checker TC-3, Unimeter UM-4, and Oscilloscope CRO-3A.

For details write: *Electronics Department, Specialty Division, General Electric, Syracuse, New York.*

Electronic Measuring Instruments



GENERAL ELECTRIC **UM-3**

NEWS

(Continued from page 57)

pared by Cornell-Dubilier Electric Corporation, New Bedford, Mass.

The basis of the code is the use of distinct color for every number from zero to nine inclusive.

TECHNICAL APPLIANCE CONSOLIDATES PLANTS

Technical Appliance Corporation consolidated its wartime New York City and Flushing plants and will hereafter be located at 41-06 DeLong Street, Flushing, N. Y.

The postwar Taco line will include antenna systems and kits for broadcast reception and also for f-m and television purposes.

RADIONIC EQUIPMENT CATALOG

A 32-page catalog listing components, test instruments, sound equipment and accessories, and technical books, has been released by the Radionic Equipment Company, 170 Nassau Street, New York, N. Y.

NEWS OF THE REPRESENTATIVE

John B. Tubergen, 1406 S. Grand Ave., Los Angeles 15, and Joe W. Marsh, 1100 West Pica Blvd., Los Angeles 15, have become members of the Los Angeles chapter. Jerry W. Miller, 5917 S. Normandie St., Los Angeles 3, Cal., has become an associate member of the Los Angeles chapter.

T. M. Graner, 600 Camelia St., Berkeley, is now a California chapter member.

O. N. Jones, 1085 The Arcade, Cleveland 14, O., is now a member of the Buckeye chapter.

At a recent meeting of the Wolverine chapter, H. E. Walton was elected president; J. C. P. Davenport, vice president; and Robert Milsk, secretary-treasurer.

The Hoosier chapter elected Leslie DeVoe president; Chuck Southern, president; Bruce McPherson, treasurer; and Bud M. W. Fisch, secretary.

Martin Friedman, a member of the Mid-Lantic chapter has moved to the Real Estate Trust Bldg., Philadelphia, Pa.

H. E. HARRIS PROMOTED BY BELL SOUND

Harry E. Harris, formerly sales manager of the Bell Sound Systems, Columbus, Ohio, has been appointed general sales manager of the manufacturing and jobbers sales division.

CANNON CONNECTOR BULLETIN

A revised 64-page edition of the Cannon Electric K bulletin on electric connectors has been released by Cannon Electric.

AT EASTERN AMPLIFIER "E" CEREMONIES



Left to right, Lt. Col. Harold L. Lister, Comdr. William J. Warburton, Harry Friedman and Leonard Meyerson of Eastern Amp Corp., and Major Meredith J. Roberts.

Development Company, 3209
 1st St., Los Angeles 31, California.
 This publication contains data on receptacles,
 taps, junction shells, stowage re-
 ceptacles for instruments, radio, motors,
 and general electrical applications.

TRANSFORMER BROCHURE

A 18-page brochure, *Engineering a Transformer*, covering lamination size, degage and magnetic performance; size, type and gage; winding details; transformer-reactor physical and electrical aspects; electrical-mechanical considerations of core laminations; im-
 mersion, assembling and casing; and
 testing and sealing, has been released by
 the Transformer Corporation, Chi-
 cago, Ill.



LABORATORY REPLACEMENT VIBRATOR GUIDE

A 16-page replacement vibrator guide
 provides replacement listings for auto radio
 battery-operated household receive-
 r-circuit diagrams, installation
 cross references of vibrators and
 capacitor listings, buffer capacitor reference
 data, and notes on an assortment of

FREE TO YOU

**COLOR CODE
 OHMS LAW CALCULATOR**

Great Time Saver
 Burstein-Applebee of Kansas
 City offers you this great con-
 venience FREE. Easy to work.
 Solves many problems in a jiffy.
 FREE to Radio men, electronic
 engineers and others in the
 business. Attach coupon to
 your letterhead.

MAIL COUPON NOW

BURSTEIN-APPLEBEE CO.
 222 McGEE ST.
 KANSAS CITY 6, MO.

Send me FREE Color Code and Ohms Law Cal-
 culator along with latest catalog.

NAME _____
 ADDRESS _____
 CITY _____ STATE _____

vibrators, has been published by P. R.
 Mallory & Co., Inc., Indianapolis 6, Indi-
 ana.

**CAMBURN TO PRODUCE AUTO/FM/
 TELEVISION ANTENNAS**

A variety of antennas for auto sets,
 and f-m, television and marine receivers
 will be included in the postwar line of
 the Camburn Products Company, 490
 Broome Street, New York 13, N. Y.

A new plant will be built on Long
 Island to produce the new postwar items.
 M. B. Bernstein is president of Camburn
 Products Co.

BROWNING JOINS NORMAN B. NEELY

Robert Browning has been appointed
 special field engineer for Norman B.
 Neely Enterprises, Hollywood, California.
 Mr. Browning was formerly with
 Western Electric as a radar field engi-
 neer.

PLYTUBE F-M MAST KIT

A plytube antenna kit for f-m and
 television has been announced by the
 Plymold Corporation, Lawrence, Massa-
 chusetts.

The mast is supplied with fittings for
 attachment atop a roof or side of a build-
 ing. Mast, antenna system, and all fit-
 tings are offered as a unit.

JACK BEEBE JOINS SWAIN NELSON

Jack Beebe has joined the transformer
 division of the Swain Nelson Company,
 Glenview, Illinois, and will be in charge
 of manufacturing and distributing of
 S-N-C transformers. Mr. Beebe was
 formerly general sales manager of the
 Thordarson Electric Manufacturing Com-
 pany.



**MUELLER INCREASES PLANT
 FACILITIES**

A postwar plant expansion program
 has been announced by the Mueller Elec-
 tric Co., Cleveland.

The first step in this program pro-
 vides for the installation of new plating
 and finishing facilities.

**BURGESS BATTERY REPLACEMENT
 GUIDE**

A guide listing replacement batteries
 for approximately 1,000 models of port-
 ables and farm type receivers has been
 prepared by the Burgess Battery Com-
 pany, Freeport, Ill. Included also are
 a list of private brand portables. Also

(Continued on page 60)

AEROVOX PATENTED
 ELECTROLYTIC CAPACITORS
 MADE IN U.S.A.

ARMED BY V-J DAY

**HEAVY-DUTY
 Electrolytics**

• Now that V-J Day has come and
 gone, those heavy-duty metal-can
 electrolytics are once again be-
 coming available for civilian use.
 Once again the Aerovox electro-
 lytic line is providing that outstand-
 ing choice of types for the better
 jobs you are out to do, in this post-
 war radio and electronic world.

For your very best maintenance
 work where equipment must be
 kept going day in and day out;
 for those power packs that have
 to keep delivering properly filtered
 voltages hour after hour; for those
 radio sets that "must stay put" —
 you can depend on these Aerovox
 metal-can heavy-duty electrolytics.

• Ask Our Jobber...

Ask him about the Aerovox heavy-duty elec-
 trolytics that are now starting to come through
 for civilian use. Ask about the other types in
 the outstanding choice of Aerovox capacitors.
 Ask for a catalog—or write us direct.

**AEROVOX
 Capacitors**

INDIVIDUALLY TESTED

AEROVOX CORP., NEW BEDFORD, MASS., U. S. A.
 In Canada: AEROVOX CANADA LTD., HAMILTON, ONT.
 Export: 13 E, 40 St., New York 16, N. Y. Cable: 'ARLAB'



PHONO - RADIO MATCHING UNIT

BOON FOR SERVICERS! A time-saver and moneymaker that just had to come . . . fruit of ADAPTOL initiative and research, supported by technical help from your own profession.

HOW SIMPLE! Without removing anything from either housing . . . without even breaking a circuit . . . you can install this long-wanted convenience wherever there is a radio to be utilized for reproducing record entertainment!

THINK OF THE technical data you DO NOT have to wade through! And the time you can save! And the satisfaction for your customers, while you are making a nice profit and adding to your professional prestige!

ANY
RECORD
PLAYER

ADAPTOL
supplies the
MISSING LINK

write
QUICK
for the
WHOLE STORY

ANY
RADIO

ADAPTOL COMPANY
260 Utica Avenue, Brooklyn 13, New York

NEWS

(Continued from page 59)

presented is a numerical and alphabetic listing of all Burgess Battery products. Free copies of the guide are available from department RG.

* * *

JENKINS JOINS FORSHAY

Victor E. Jenkins, formerly test equipment sales manager for the Weston Electrical Instrument Corp., has joined J. M. Forshay, 27 Park Place, N. Y., N. Y., factory representative in New York City and New Jersey for Simple Electric Company and Industrial Condenser Corporation.

* * *

COLEMAN NOW ASST. DIRECTOR RCA VICTOR ENGINEERING DIV.

J. B. Coleman has been named assistant director of engineering for the RCA Victor division. M. C. Batsel has been named chief engineer of engineering products. Mr. Coleman will make his headquarters at the company's home office in Camden, N. J.

Previous to his new assignment, Batsel was chief engineer at the RCA Victor plant in Indianapolis, Ind.

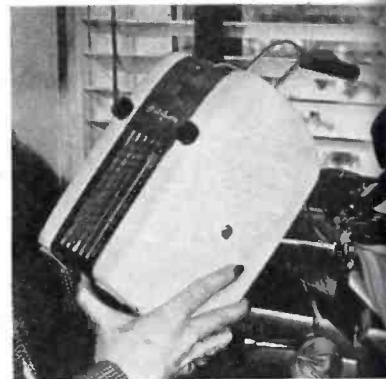
* * *

COMMUNICATIONS PARTS MOVES NEW PLANT

Communication Parts has moved to 1101 North Paulina Street, Chicago.

•

POSTWAR RECEIVERS



Portable and phono-table postwar models Westinghouse. Unit, above, can be mounted on wall or set up on flat surface. Combination unit, below, can be operated as a phono-receiver or with separate units, it being possible to remove receiver and using as a straight table model.



WARD

Antennas

**FIRST CHOICE . . .
OF AMERICA'S RADIO DEALERS**

Radio dealers, too, recognize the factors that long ago made Ward Antennas most popular with auto manufacturers and dealers. They see the top quality, precision workmanship, and now the new war-created designs that make Ward better than ever! The world's finest antennas for car and home were made, are made, and will continue to be made by Ward. Place your order for Ward Antennas now!



BUY VICTORY BONDS

THE WARD PRODUCTS CORPORATION
1523 EAST 45th STREET - CLEVELAND 3, OHIO

VOLUME AND TONE CONTROLS

(Continued from page 30)

in practically all the necessary resistance values and tapers in the wide range of resistance wherein the type may be used, the Service Man should make it a policy, when confronted with the replacing of controls of either type, to replace an original wire-wound control with a wire-wound control, and an original carbon type control with a carbon type control whenever possible to do so. By adhering to this policy, customer dissatisfaction will be avoided in most cases.

The circuit design of many receivers recently includes special considerations which make it necessary for the operator to replace the volume control with one of the same type. There are many receivers (especially older models) in which the use of a wire-wound control is definitely indicated, and where the carbon type will not give satisfactory service. Wire-wound units are frequently used in control circuits which require a comparatively high circuit-carrying capacity. Compact, low-resistance controls of this type can be made to handle greater currents than a carbon control. They are also used in critical circuits where it is necessary to have a higher degree of resistance permanence, or much closer resistance tolerance, than is possible with the carbon type.

There are certain conditions where

it might be desirable or even necessary to change the type of control; i. e., use a carbon control having the proper resistance value, taper and wattage rating to replace an original wire-wound control or vice versa. This is a matter of discretion for the Service Man. Unless it cannot be avoided, the exchange should not be made unless the advantages to be gained are not offset by the disadvantages of the particular type control. Quite often this can be correctly ascertained only by trial and error.

Midget Versus Large Size Controls

In some receivers, particularly in off brand or a few trade name receivers in which small midget-type volume controls are used in current-carrying circuits of the antenna-bias type, repeated volume-control trouble due to the overheating may be experienced. If the original midget control is damaged or burned out and a check reveals that the failure is due to excessive current in the control, the defective unit should be replaced with one of the larger type controls if there is space available.

On the other hand, a midget type may be used to replace a large type control in an audio type of control circuit whenever this procedure tends to simplify a crowded installation.

(To Be Continued)

NEW PRODUCTS

NE-O-LITE TESTER

Best unit, Ne-O-Lite Test-Lite, for testing a-c lines, checking polarity of a-c or d-c, and tracing ground lines, has been announced by the Ne-O-Lite Mfg. Co., Rockford, Illinois. Tests voltage from 60 volts a-c to 550 volts a-c or d-c by variable light intensity. Has a neon lamp. Has a clear plastic shell and insulated test points.

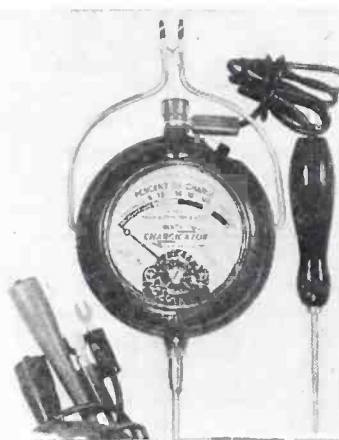


HICKOK CHARGICATOR

Chargicator to indicate electrically equivalent gravity of any lead-acid battery, regardless of size or voltage has been developed by the Hickok Electrical Instrument Company, 10521 East Avenue, Cleveland 8, Ohio.

Probe type, illustrated, gives instantaneous measurement of battery condition. It shows what charging rate to use, either for trickle charging or for an efficient, safe, high-rate charge. It indicates the percentage of charge and charging danger and warns of destructive overcharging.

Has a four-color scale dial. All models are sealed in molded acid-proof bakelite cases.



RADIART MIDGET VIBRATORS

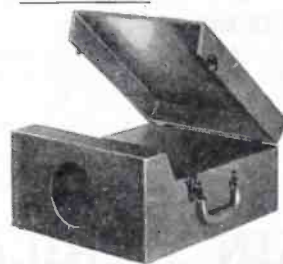
Midget vibrators, type VR-2, 2 1/8" high x 1 1/8" in diameter, have been announced (Continued on page 62)

LAKE

has a better selection of **RADIO Parts, Cabinets and Equipment!**



Portable Phonograph Case of sturdy durable plywood, in handsome brown leatherette finish. Inside dimensions 16 1/2" long, 14" wide, 9 1/2" high. Has blank motor board. As illustrated above, specially priced at **\$6.95**



Portable Phonograph Case in brown leatherette covering. Inside dimensions 17 1/2" long, 13" wide, 7 1/2" high. Has blank motor board and opening for speaker. As illustrated at left, specially priced at

\$7.95

SOUND EQUIPMENT

Complete line of amplifiers, microphones, speakers and sound accessories. WRITE TODAY!

Also blank table cabinets of walnut veneer in the following sizes, with speaker opening on left front side:

(Note: *7 has center speaker grill.)			
#1	8 1/4"	L x 5 1/2"	H x 4" D \$1.95
#2	10 1/4"	L x 6 3/8"	H x 5" D \$2.75
#3	13 1/2"	L x 7 7/8"	H x 6 1/4" D \$3.25
#7*	10 3/4"	L x 7"	H x 5 1/2" D \$2.50
#8	17 1/4"	L x 9"	H x 9 1/2" D \$4.50
#9	21"	L x 9 1/4"	H x 10 1/2" D \$5.50

*Speaker Opening in center of front side. Cabinets available in ivory color and Swedish Modern. Write for prices.

POWER TRANSFORMERS

4, 5, or 6 Tube—6.3 V at 2 amp	\$1.49
50 Mill Power Transformer.....	
7, 8 or 9 Tube—6.3 V at 3 an	\$1.89
70 Mill Power Transformer.....	



All types of radio cabinets, equipment and parts are available at Lake's lower prices. A large stock is listed in our catalog.

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by the Radiart Corporation, 3571 W. 62nd St., Cleveland 2, Ohio. Designed for operation from a small 6-volt storage battery.

Vibrator frequency, 185 cps $\pm 10\%$; input voltage (nominal), 6.0; input voltage range, 4.5 to 7.5; input current, 1.5 amperes maximum at 6.0 v; output voltage, 200 d-c maximum; and potential difference between primary reed and secondary reed, 25 v maximum.



INSULINE MIDGET JACKS

A series of midget-sized jacks has been developed by the Insuline Corporation of America, Long Island City, N. Y. Models include single closed-circuit,

NEW PRODUCTS

(Continued from page 61)

single open-circuit, and three-way microphone types. Jacks have a tooled-brass body with phosphor-bronze spring members, nickel plated.

SHALLCROSS AXIAL LEAD RESISTORS

Fixed wirewound axial lead 1-megohm, 1-watt resistors have been announced by the Shallcross Manufacturing Co., Jackson & Pusey Avenues, Collingdale, Pa. Known as Akra-Ohm type 188, the resistors are 1 3/16" long x 3/8" diameter. Axial leads, 3" long, of No. 20 tinned copper wire. Standard tolerance is said to be $\pm 1\%$.



WESTON DIRECT-READING INSULATION TESTER

A direct-reading insulation measuring device, model 799, providing a single range for .1 to 10,000 megohms with the 10,000 mark at 8% of the scale length, has been announced by Weston Electrical Instrument Corporation, 617 Frelinghuys-

sen Avenue, Newark 5, New Jersey.

The circuit is said to have a test potential of less than 50 volts d-c. Its use includes checking leakage between windings in transformers, leakage of low-voltage paper and mica condensers, etc. Size 5 3/8" x 3 1/4" x 4 7/8".



REINER VACUUM-TUBE VOLTMETER

A vacuum-tube voltmeter, 451, amplifier, 101, featuring 25 millivolts on the lowest range, 1,000 volts on the highest range, 10 cps to 700 mc frequency range, and 7 mmfd input capacity has been announced by Reiner Electronic Co., Inc., 152 West 25th Street, New York 1, N. Y.

Model 451 ranges are: a-c volts, 0-.02-.1-25. (with amplifier)-2.5-10-25-100-250-1,000; d-c volts, 0-2.5-10-25-100-250-1,000; d-c current, 0-2.5-10-25-100-250-1,000; ohms; 1 ohm to 1,000 megohms.

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SERVICE, 52 Vanderbilt Ave., New York 17, N.Y.

frequency range, 10 to 5,000 cps, amplifier) 50 cps to 700 mc. D-c ohm and current accuracy is said to be 2% on full scale. A-c volt accuracy to be 2%, 50 cps to 50 mc; entire frequency range 5% accuracy. Weight, 20 lbs. Size, 10 3/4" x 9" x 8".

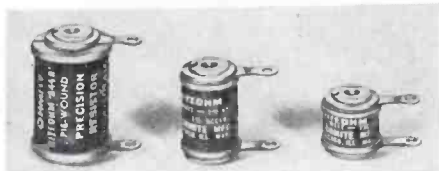


OHMITE PIE-WOUND RESISTORS

A series of pie-wound resistors, Rite-types 844A/844B/842A, that can be mounted by means of a through-bolt, has been announced by the Ohmite Manufacturing Company, 4835 Flournoy St., Chicago 44, Ill. Available in 3 sizes: 9/16" diameter x 1/2" long, 9/16" diameter by 7/8" long,

and 3/4" diameter x 1 3/16" long. The smallest is a 2 pie while the other two are 4-pie units. The minimum resistance is 1 ohm for the 2-pie unit and small 4-pie unit, and .10 ohm for the large 4-pie unit. The maximum resistance is 200,000 ohms for the 2-pie, 400,000 ohms for the small 4-pie, and 1.5 megohms for the large 4-pie unit.

Uses enameled alloy resistance wire non-inductively pie-wound on a non-hydroscopic ceramic bobbin.



CARTER MOTOR FREQUENCY-CONTROLLED D-C TO A-C CONVERTER

A frequency-controlled d-c to a-c rotary converter has been announced by Carter Motor Company, 1608 Milwaukee Avenue, Chicago, Illinois.

Designed with the frequency control in the base, including a vibration reed-type meter to visually indicate the frequency of the output.

In the 110-120 volt d-c to 117-volt a-c models, the output control is said to be within ± 10 volts at 60 cycles, over a ± 10-volt d-c fluctuation.

Models can be supplied with input voltages ranging from 6 through 64 volts for battery conversion and also 110-120 volts d-c for line conversion. Wattage ranges are from 40 through 250, continuous duty.



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JOYS AND FLASHES

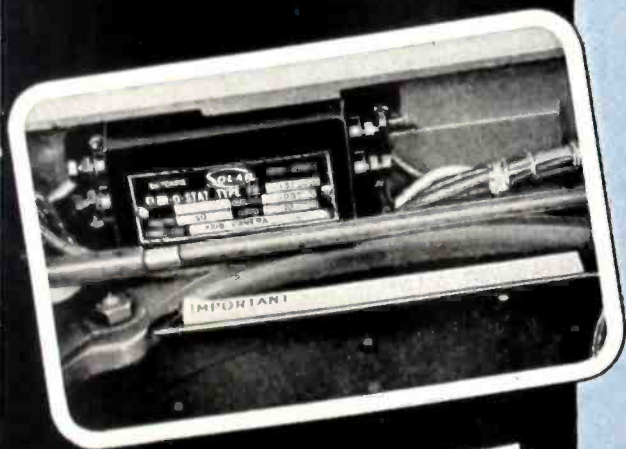
OVER 10,000,000 f-m sets will be sold during the next two or three years, according to Frank Mansfield, director of sales research of Sylvania, who based his data on a survey recently completed. . . . Irving P. Wolfe has become a distributor and opened a store at 224 Main Street, Poughkeepsie, New York. His company will be known as Chief Electronics. . . . Olson Radio Warehouse, 73 E. Mill Street, Akron, Ohio, have been appointed distributors for Philco. . . . John Meck Industries now have a Cessna T 50 plane for transportation of company personnel and special equipment. . . . Jack Kaufman, former president of Heintz and Kaufman, Ltd., has been named vice president of Aireon Manufacturing Corporation and manager of the San Francisco office of Aireon. . . . A one-story plant on a 7½-acre tract on Skokie Highway near Waukegan, Illinois, has been purchased by Belmont Radio. This will supplement the Belmont plant on Dickens Avenue, Chicago for receiver production. . . . Ray T. Schottenberg, jobber sales manager of Astatic Corporation, visited jobbers in the New England states recently. H. A. Chamberlin, Astatic New England rep., accompanied Mr. Schottenberg. . . . George Balsam has been named ad manager and director of sales promotion of Aerovox Corporation, New Bedford, Mass. . . . Westchester Electronic Supply Company, 333 Mamaroneck Avenue, White Plains, N. Y., was recently appointed distributor for RCA, IRC and Cornell-Dubilier. . . . T. R. McElroy, president of the McElroy Manufacturing Corporation, 62 Brookline Avenue, Boston, Mass., has rejoined the Merchant Marine as a radio operator, Lt. Senior Grade, and is now making the regular run between Europe and U. S. . . . Amphinol Phenolic Corporation, 1830 South 54th Avenue, Chicago, Ill., are expanding their plastics manufacturing facilities and building a three-story building next to their present plant. . . . V. Hutto has been named Georgia factory representative for Universal Microphone Company, Inglewood, Calif. . . . Radiart Industries, Cleveland, Ohio, has been bought by Maguire Industries, Inc., Leslie K. Wildberg and William H. Lamar of Radiart have sold all their common and preferred stock to Maguire. . . . James H. Hickey has been appointed general manager of the Zenith Radio Distributing Corporation.

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