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INDUSTRY REPORT

Microelectronics Forges Substantial Change, says EIA Microcomputers and microelectronics in

general are forging large and significant changes on American business, Americans in general, and the economy as a whole.

According to a report in the Electronic Industries Association's 1979 Market Data Book, recent advances in hardware now permit microcomputers to handle the higher level language software packages until recently used only in conjunction with large computers.

The EIA report said:

"Microcomputers are introducing many changes in the prevailing structures in business and in the economy as a whole. Beyond the effects within the electronic industries, the adoption of microcomputers is initiating extensive changes in other important manufacturing industries. Employment patterns in manufacturing as well as service industries are also being significantly affected ...

"The effect of microelectronics developments on consumers has social implications that extend beyond economics. One significant consequence is that highly sophisticated products that have previously been available only to institutional buyers are becoming available to, and perhaps indispensible to, the individual, private consumer. Information and communication tools, previously restricted to use by government and large corporation, are becoming more and more accessible to the individual citizen.'

Industrial Electronics Market Surges

Although the (factory) sales of all electronic equipment and systems totaled some \$65 billion last year for a 14.9 per cent growth rate compared to 1977, only the industrial market segment exceeded that average.

According to statistics compiled by the Electronic Industries Association, of the four components comprising the electronics marketplace, three of the industry groups-consumer, components, and communications, all showed negative growth rates in 1978 compared to their growth rates a year earlier.

The consumer segment, which comprised 14.4 per cent of the total market in 1977, last year dropped to 14.3 per cent. Similarly the components segment dropped from 17.7 per cent to 17.5 per cent; and communication receded from 31.3 per cent to 30.5 per cent.

Only industrial, with factory sales of some \$25.5 billion (an 18 per cent increase over 1977), showed an increase advancing from 36.6 per cent of the total market to 37.7 per cent.

One significant milestone was reached in the television marketplace, according to EIA. The number of color sets in use surpassed the number of black and white for the first time in history.

Moreover, EIA adds, the "modern color set is becoming more than a broadcast receiver" as it is now being used in conjunction with video games, home computers, pay and cable TV, and video discs and tape cassettes. The name "television" itself may be obsolete, EIA said, since it means viewing at a distance.

NESDA Transported to Texas

In an unexpected action, the executive council of the National Electronic Service Dealers Association (NESDA) has moved the administrative headquarters from Indianapolis to Ft. Worth, Tex.

In the latest episode in the continuing saga, begun early this year with the resignation of Charles Porter as executive director, it was announced that Texas Electronics Association (TEA) executive director J.W. Williams will take over as chief administrator of NESDA and IS-CET.

According to a NESDA statement, the action was taken with the concurrance of NESDA President Bob Villont and **ISCET Acting Chairman Forest Belt.**

W. S. (Bob) Harrison, editor of ServiceShop magazine has been retained as publications editor, it was announced, and the magazine will immediately begin publishing on a six, instead of 12, times a year basis. Marti McPherson, interim NESDA administrator following the resignation of Porter, will continue as editor of the association's annual yearbook in Indianapolis, the statement said.

William said the physical relocation of the office began June 3 and was completed by the 30th of the month. All association functions were continued without interruption, he said, including the organization's annual convention in Tucson, Az.

Williams said he considered his main priority to "improve upon NESDA's ability to communicate and respond to the membership."

The organization's new address is 2708 W. Berry St., Fort Worth, Tex., 76109. NESDA's phone number is 921-9061 and ISCET's is 921-9101. Both area codes are 817.

Philips to Make Scopes in U.S.

Dominick Protomastro, president of Philips Electronic Instruments, Inc., has announced that Philips plans to manufacture oscilloscopes in the U.S.

"We expect to have the American-



ELECTRONIC TECHNICIAN/DEALER LEADING THE CONSUMER AND INDUSTRIAL SERVICE MARKETS

AUGUST 1979, VOL. 101, NO. 8

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Coilless IF strips Data converters Pulses vs sign waves CES highlights

On the cover: The Surface Acoustic Wave filter could well replace IF bandpass tuning in TV receivers very soon. This month's cover background's repeating pattern emphasises its potential importance.

FEATURES
New consumer products
ET/D visits the Summer Consumer Electronics Show

Coilless IF strips SWIFs gain in popularity among manufacturers

Data converters

A look at digital to analog and analog to digital

Pulses Pulse waveforms are the basics of digital ______30

Digital part IV We continue our series with a look at flip-flops _____

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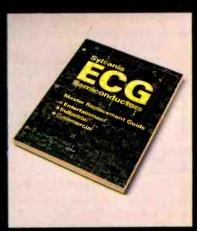
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made Philips oscilloscopes ready for delivery in this country by the last quarter of this year."

Protomastro said the manufacturing facility will be located at the present U.S. headquarters site at Mahwah, N.J. Burgeoning demand for scopes in the U.S. has necessitated the action, he added.

While scopes will comprise the U.S. manufacturing capability for Philips for the next year or so, eventually plans call for Philips to make in the U.S."a very significant portion" of all equipment sold by Philips Test and Measuring Instruments.

VLSI Technology Advancing Rapidly

The 1979 Electronic Industries Market Data Book, published by the Electronic Industries Association (EIA), reports that very large scale integration (VLSI) is among the most notable technological achievements currently impacting electronics.

"The development of large scale integration (LSI) has made it possible to combine tens of thousands of transistors into a tiny, quarter-inch chip of silicon. With the more recent advent of very large-scale integration, it is widely estimated that by 1980 it will be possible to concentrate more than a million transistors onto a single chip," EIA said.

tors onto a single chip," EIA said. In efforts to fit more information onto a chip, researchers are looking to new methods for etching smaller circuitry, including electron beam methods. An alternative to electron beams are x-rays, EIA reports, and more powerful x-ray sources are currently being sought.

Among the applications of VLSI will be large computer memories, imaging devices, and even possibly "pocket sized computers."

As the density of circuitry continues to increase, scientists are also looking for ways to develop higher speed semiconductors. One method, EIA reports, that could lead to a new generation of semiconductor devices is the use of gallium arsenide (GaAs) in place of silicon.

In describing this new method, EIA said current semiconductors are flat and their electrons flow in the positive zone, it leaves behind a positively charged spot." These positive charges, however, act as obstacles to the current and slow its flow.

"To overcome this obstruction, scientists are experimenting with ... several thin layers of GaAs. Alternate layers of the GaAs do not contain the impurities that would create separation into positive and negative regions, which enables them to absorb the obstructing positive charges left in the layers where electron current flows."

This design, at least in theory, allows electrons to flow at speeds several times previously achieved speeds, and of course, results in faster semiconductor device response times. ET/D



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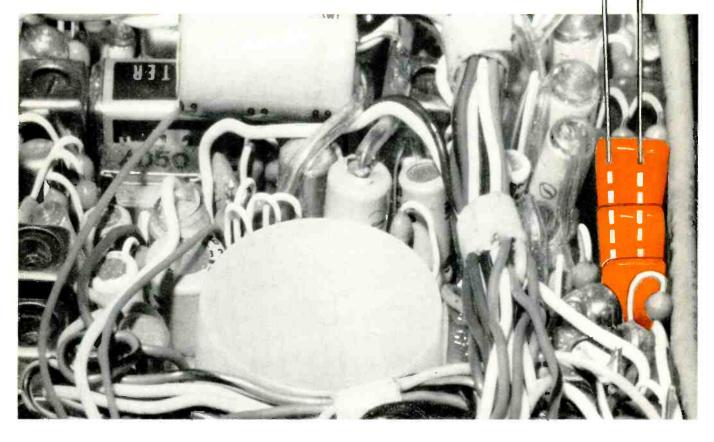
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FROM THE EDITOR'S DESK



Quite often we are able to gain new insight and perspective into our own consumer and home electronic industry by taking a moment to look at what is going on in some of the more closely allied environments around us.

Recently such an opportunity presented itself to me. I, along with a group of editors from other industrial and consumer publications, was invited to Minneapolis to investigate and learn about some of the philosophies, technologies and products which are being considered by the residential, (home, office, and apartment environmental controls) division of what is also one of America's major computer makers—Honeywell, Inc.

It was indeed an enlightening experience.

Not only were we given a glimpse of what is "really going on" in at least one high technology profit making industry, but in so doing we are able to gain glimpses of the kinds and types of utensils and systems and—even the test gear—that will make up our real world in the near future.

I can say this unequivocally. Industry already knows the microelectronics, microprocessor, computer (call it what you will) revolution is here.

The message I want to convey is that unless you, as an electronics serviceshop owner, manager, or professional technician realize this—NOW—you will not be around much longer.

Consider this. Honeywell currently designs and develops its own microelectronic chips in Minnesota. It has acquired another semiconductor manufacturing facility in Texas, and is building two new facilities for chip designs and development at, as yet, unannounced sites.

Obviously, the future of electronics design, application or repair work, lies in *understanding* the microprocessor. I underline the word understand.

For instance, by the mid 1980s, VLSI will permit (it is estimated) the placement of one million transistors on a single chip.

Yet, as one Honeywell scientists put it: "It's nothing more than a piece of sand unless you know how to use it."

Truer words were never spoken. And to think that this microelectronics revolution will escape the home entertainment and consumer electronics marketplace is—at best wishful thinking—and more practically, just plain stupidity.

One of Honeywell's purposes in inviting editors to tour its Minneapolis area facilities was to unveil a newly developed prototype of a home or office environmental control system based on microprocessor logic control. This system "senses" outdoor weather conditions, indoor load conditions, wall temperatures, etc., and compares real time conditions to user desired conditions to control the amount of heat redistribution.

Compatible with this advanced heat distribution system is Honeywell's microprocessor based W89 diagnostic device. In other words, I saw a glimpse of the test equipment of the future.

Via simple one-plug hookup to the Advanced Heat Pump Control system, this (portable) piece of gear routinely runs through its various test algorithyms, eventually displaying on a 5-inch CRT the specific malfunctioning component, such as a coil, compressor, relay, etc.

I mention this simply by way of saying that to think these systems, this type of "computerized" error detection and fault description, will escape consumer electronics is highly unrealistic.

If you haven't already pondered the larger question of what the consumer electronics service industry of the future will resemble—it is high time you did.

And, without question, the key to understanding the future of electronics service is first to understand the microprocessor, its functions and applications in modern society.

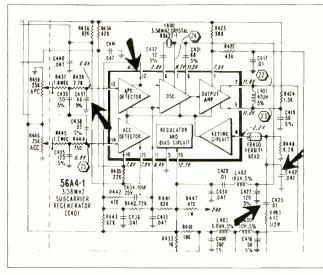
As Robert Stenstrom, Honeywell's manager of technology assessment remarked: "The semiconductor industry has a close parrallel to the cement industry ... both add value to sand."

Understanding the value is the key.

Richard M. Vay

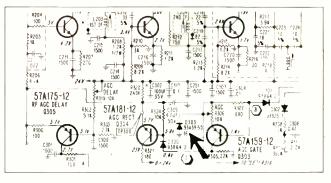
SERVICE SEMINAR

ADMIRAL



Color TV Chassis M55—Color bars across screen and possible loss of color sync. Possible Cause: Defective IC401, C423, C437, and/or C442. Note: A horz. keying pulse from the HOT should be present at pin 4 of IC401.

Touchy vert. sync. Possible Cause: Defective C801. **AGC overload with severe horz. tearing.** Ok when set warms up. Possible Cause: Defective Zener (D303).



GENERAL ELECTRIC

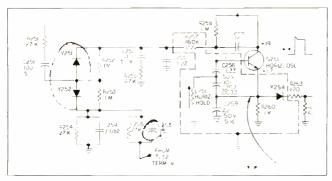
Color TV Chassis MA/MB/MB-2/MB-75, MC/MC2, YM Horizontal output transistor replacement. Failure to use the correct part will cause the following problems: When using an EP15X45 to replace an EP15X28, the device will not switch fast enough and will overheat; when using an EP15X28 to replace an EP15X45, the device does not have sufficient gain and will overheat. Use an EP15X28 in chassis numbers MA/MB/MB-2/MB-75 and an EP15X45 in chassis numbers MC/MC-2, YM. Universal replacements can cause problems. Use the authorized replacements.

Color TV Chassis XA-2, weak or no horizontal sync, arc causes failure of Y251 and Y252.

Repair: 1. Check C253. If it is bad, replace it with an ES18X69 and go to step No. 4.

2. If C253 checks good but has a tan color, replace it anyway and go to step No 4.





3. If C253 checks good and has a brown color, proceed to step No 4.

4. Now replace Y251 and Y252 (ES16X27).

5. Then check the resistance from the common connection of Y251 and Y252 to the cathode of each device. This resistance must be at least 450K measured on the board. If resistance is lower, locate the cause before going on to the next step.

6. Check the location of the green wire going to the CRT printed board. If it is connected to the W-3 hole, perform the following modification:

a. Cut green wire (W3) flush at CRT circuit board and strip 3%'' of the insulation off the end.

b. Wrap and solder the green lead to the end of R131 which is standing off the circuit board. Keep the connection about $\frac{1}{6}$ " away from resistor body.

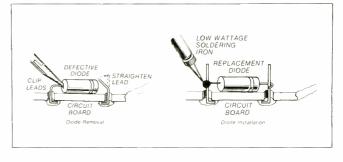
c. Cut the section of the resistor lead between the new solder connection and the board and remove it.

d. Dress R131 with green lead now attached away from board and other wires, etc.

<u>RCA</u>

Color TV Chassis CTC93. 150 Volt bridge rectifier failure. The 150 volt bridge rectifier in the CTC 93 chassis consists of CR 600, CR 601, CR 602 and CR 603. It has been determined some small percentage of these diodes suffered a degradation of reliability during the chassis assembly process. The cause was identified and corrective action taken on instruments where the first four digits of the serial number are 9031 or higher. In order to ensure continuing reliability, customer satisfaction and to prevent callbacks, when one diode failure in the 150 volt bridge is encountered, change all four diodes (Stock No. 141489, 4 required). Since the CTC 93 Components Kit (Stock No. 199060) containes three 141489 diodes, the prepared technician should carry additional quantities.

To change the diodes proceed as follows: 1. Remove each diode by clipping leads as close to body as possible, then bend remaining leads perpendicular to the printed circuit board. 2. Clip replacement diode leads to one-half length. Observing polarity, wrap each lead of the new diode around an original lead, then crimp securely and solder. Note: *This technique is recommended where applicable in this chassis.*



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NEWSLINE

WARNER ENTERS HOME VIDEO MARKET. Warner Communications has entered the consumer video tape and disc markets, a move that should significantly impact these emerging areas. According to Warner Board Chairman Steven Ross, a new division of the entertainment conglomerate will develop and market software for both VCR and video disc owners. The impact of Warner's entry into software production can be better gaged when you consider some of its subsidiaries, including Warner Brothers Records; Warner Brothers Pictures; Warner Brothers Television; Warner Cable; plus Atari, Inc., which is in electronic games and computers.

ISCET-TECH LIBRARY MOVED TO CHICAGO. Henry Golden who established this library of service data, and who has been operating it for the past half-dozen years, in Kansas City, MO, has suffered a series of strokes and a heart attack recently and has asked to be relieved of the obligation. Responsibility for the library has been assumed by George Sopocko at 5631 West Irving Park Rd., Chicago, IL 60634. (312-545-3622). George states that he is reorganizing the library and should be in operation by October. Meanwhile he will accept donations of material and can give a tax deductible receipt for fair value.

HITACHI OPENS NEW HEADQUARTERS. Hitachi has opened up its new national headquarters and eastern regional offices in New York City. According to a spokesman, the new 11,000 square foot facility is part of a seven-region system, each with its own warehouse and engineering facility. The addition was needed, Hitachi said, to accommodate "rapid expansion in the U.S. video market."

PREDICT \$22 BILLION COMPUTER MARKET. A market research firm--Frost and Sullivan -- says it conservatively estimates that \$22 billion worth of "small business computer systems" will be sold during the next 10 years. The firm stated decreasing price and software availability are the major factors influencing small business computers. A micro based system priced at \$12,000 today will cost \$9,000 in 1987, the firm predicted. "Microcomputer based systems have resulted in fundamental changes in the computer marketplace; small unsophisticated users having minimal background are now becoming involved in data processing," the firm contends.

IFH PLANS INDUSTRY POW-WOW. The institute of High Fidelity (IHF) has announced it is planning a special conference for industry leaders to evaluate major problems peculiar to them. Scheduled for October 2 at New York's Statler Hilton, the major thrust will be to examine new markets, the impact of advanced technology, changing merchandising patterns, reordering of financial priorities, and the impact of the Federal government.

INDUSTRY STATISTICS EXCHANGE ANNOUNCED. In a related action, the IHF said an industry-wide confidential sales data figure exchange has been created with the help of Price Waterhouse. A similar project attempted in the mid 1960s failed for lack of participation, according to IHF. However, modern management methods now require manufacturers to have accurate data on the size of markets and specific product categories, IHF said, and this project is intended to fill that need.

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What might this wasted time be worth to you? Well, if you get one of these calls, say, once each day per man, with a three-man crew this might be costing over \$3000 per year. If you want to figure your own cost, count the number of "not homes" in a month's time, and multiply it by the average labor income per call.

If you find that you do have a problem, there are a number of ways to go about correcting it. One of the best ways occurs at the time you are taking the service call. If the customer has no idea when during the day the technician is going to arrive, and if the customer sometime during the day has something she wants to do, she is apt to go out and do it. Inevitably, that is when the technician arrives, and you have a "not home.' If you can narrow down the time when the tech is going to arrive, the customer will be more patient. Many service firms find no difficulty in scheduling calls either AM or PM. In the General Electric Company factory operations, the day is divided into three parts . . . morning, mid-day, and afternoon. Further, GE allows the customer to choose the period when the technician is going to come. If she has selected the time herself, she is much more apt to be home at that time.

For those doing one-call-at-a-time dispatching, the procedure includes calling the customer's home. The dispatcher calls the customer. If she is at home, she is told that the technician will be there shortly. Then the tech is contacted and dispatched to the home. If the customer does not answer, that job is temporarily set aside and another customer is called instead. Note is made of the time of the phone call. Later in the day, the customer is called again, and if reached, the call is dispatched. If the customer is not reached all day, there is a written record of the attempts that are made to reach her, as she will surely say, "I was only out for a minute."

If the technician reaches the home and cannot gain entry, the tech should contact the dispatcher who will then make a phone call. This accomplishes two things. One, of course, is that the dispatcher has a written record of the fact that two attempts were made to gain entry and it is definitely established that, indeed, the customer was not home. It is also strange . . . but true . . . that many times the customer is home but just does not answer the door. But few people can resist answering the phone, at which time they are told that the technician is standing on their door step and would they please go and let him in.

There is one final technique that is used by some firms. Charge the customer for the call. Or at least, establish a charge for the call, even if it is never paid. This establishes the high cost of the missed call in the customer's mind.

Results from the computerized NARDA Service Data System program indicate that on average, service firms encounter two per cent of all calls as "not homes." With diligence, this can be lowered to less than one per cent.

"Not home" calls result in poor productivity, loss of profit, and poor customer relations. LET'S STAMP OUT "NOT HOMES."

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I have the original series of TEKFAX plus 101, 103, 104, 107, and 113. These are for sale to anyone who wishes to make an offer. M. L. Chapin 53811 Franklin Utica. MI 48087

EDITOR: By original series we assume that the TV TECH/MATICS series was

meant. These covered, in eight volumes, 1965 thru 1968 U.S. B&W and color TV production.

Having retired from business, I have for sale TEKFAX volumes 103, 105, 109, and 113. Roman Grall **Box 95** Whitelaw, WI 54247

HELP WANTED:

This is in reference to a mini-TV set Model TPS 5050, a solid state unit manufactured in 1969. Our problem is a broken neck on the CRT which is a 3 inch



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diagonal measurement. Symphonic Electronic Corp. is no longer in business. We wonder if someone might have such a tube laving around and would like to sell it. The tube number is 06407.

Delta Electronics 500 Stambaugh Ave. Farrell, PA 16121

I've been a subscriber to ET/D for over 25 years. Can you list my request in your Letters column? I need a schematic for a Bradford 9 inch b-w Model D-MAT55988 M. Ascencio, Jr. 22874 N. Brookside Dr. Dearborn Heights, MI 48125

I need a vertical output transformer for a Conar Custom 70 TV receiver (#TR47). It can be new or used. I will gladly pay a reasonable price. L. N. Canale 118 S. Main St. Spring Valley, NY 10977

Can anyone furnish a schematic of AKAI Model 8 reel-to-reel tape recorder? It is not available from AKAI. Jake Santine Jake's Repair Service 2400 NE Greenfield Place Mounds View, MN 55432

I need a schematic and operating instructions for a Heath Kit oscilloscope Model 10-12, Series 752-1012A. John Bell 195 Silleck St. Cliffton, NJ 07013

I am looking for a source of parts for the old wind-up Victrolas. Any help would be greatly appreciated. Thomas P. Falks Friendly TV Services P.O. Box 662 Hot Springs, VA 24445

Friden is out of business. I would like to contact anyone else trying to repair a Friden (Singer) Model EC1114 electronic desk calculator. I have some schematics and data and would share and exchange info. Robert Miller Rt. 1 Anadarko, OK 73005

I need information on a Bradford Model 1004B30 John Williams 35043 Altos Ct. Grisson AFB, IN 46901

I need a schematic and parts list for a bass guitar amplifier. Brand name Kay, Model K-830 by Valco. The manufacturer using the Kay name says it was manufactured prior to their purchase of the name and they cannot help me. David J. Lamb P.O. Box 104 Cairo, IL 62914

Needed: Service manual or schematic for a stereo console, Pilot 3000. Will buy or copy and return. Davila Electronics 407 Elizabeth St. Pekin. IL 61554

I need information for substituting a Sears flyback #299755. Sears says it is not made anymore. It has a Toshiba part Number AZ-9976. W.J. Crow 321 E 63rd St. Hialeah, FL 33013

I need a remote control kit for a Heath/ Kit TV, Model GR9000. Can anyone help me? Jim Nicks 10219 N. 23rd St. Tampa, FL 33612 I need a schematic or any information on a RCA CB Model M1, No. 555489. Janty Shurdon National Electronics 222 Belmont Ave. Haledon, NJ 07508

TEKFAX WANTED:

Somehow I missed out on TEKFAX 113. If any of the readers out there has a duplicate I would be glad to trade a 114 for it. E. J. Alderman RFD 2, Box 83 Madison, NC 27025

We have a copy of TEKFAX 112 and would like to purchase numbers 110, 111 and 113. Do any of your readers have copies they wish to sell? W.M. Simpson Carson Valley TV Box 1866 Gardnerville, NV 89410

I would appreciate any help in obtaining the following TEKFAX-Numbers 102, 109, 110, 111, 112, 113. W.C. Epps 1317 Hampton St. Richmond, VA 23220 **ETID**

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Consumer Electronics Show Highlights

High technology in the home

This year's summer Consumer Electronics Show in Chicago was the biggest ever from the standpoint of attendance. From a technology point of view, it proved without question that the microprocessor is king.

By Richard W. Lay

Manual is dead; all doubts have been eliminated by the high technology products shown at the 13th Annual Consumer Electronics Show (CES) this past June, in Chicago. The microprocessor has become the marketing star of "the new consumer electronics."

Replacing the old manual controls with the functional diversity permitted through the programmable microprocessor, America's consumer and home entertainment electronics' manufacturers have finally completed the circle — in effect, bringing to the consumer marketplace those innovations and technologies developed in this country during America's space research age of a decade ago.

There were micros in TVs (RCA's), micros in tape decks and stereo tuners; micros in language translators (Quasar); micros in VCRs; in home computers, of course; everywhere!!! The summer CES was a tremendously significant show because when it came right down to it, it provided an insight into the future of consumer electronics. From the technological



Fig. 1 – Thr 4¹/₂ hour Sanyo Model VCR5000



Fig. 2 – Among the host of new portables shown at CES was Akai's first video tape recording entry, ActVideo

and servicing point of view it was astounding.

Like all CE shows of recent years, this one was absolutely mind boggling from the standpoint of sheer size. There was only one difference between this and others ... this one was the biggest ever. Almost 61,000 attendees pushed through aisles jammed shoulder to shoulder in Chicago's McCormick Place and two overflow hotels for a glimpse at the 938 exhibitor's products.

Actually, the CES is a somewhat unusual show. It is run, in fact, on three different levels. One being popularity, a second from a marketing standpoint, and thirdly, from a purely technological point of view.

The winners

From the popularity standpoint, CES



Fig. 3 – Toshiba's revolutionary high speed, fixed head video tape recorder prototype model

had two clear cut winners,

Magnavox's video disc player and Texas Instruments' candidate in the home or personal computer field. From a marketing standpoint, among the products that retailers showed most interest in were, again Magnavox's disc system and third generation video cassette recorders, which are now in the portable phase. (What they've done is take the traditional recorder and chop off the tuner, leaving the record mechanism available for portable use with camera.) Thirdly, the technological prizes have to go to Toshiba's fixed head video tape recorder and Ohio Scientific's computerized home security system.

The former represents a tremendous advance in size reduction, the number of components used, and

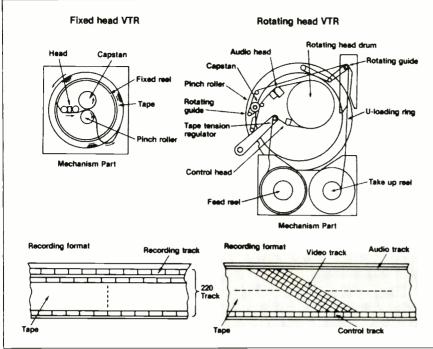


Fig. 4 – Comparison of the new fixed head and traditional rotating head VTR systems.



Fig. 5 – RCA's new programmable CTC101 chassis with comb filter.

in potential uses (if it ever gets out of the engineering lab), while the latter is an amazing state of the art advancement in home security, though admittedly with its \$5,000 price tag it is more in harmony with the commercial building and industrial marketplace.

On the stereo front, pulse code modulation continues to be the talk of the day — but that's all, just talk — because you can't buy it yet.

New VCRs

In VCR developments Matsushita Electric, through Panasonic, Quasar, and RCA, among others, showed its new 6-hour VHS system ... up from the current 4-hour playing time. Sanyo introduced its new 4-1/2 hour Beta format VCR, the Betacord III Model VCR5000 (see Figure 1).



Fig. 6 – A color portable from Panasonic featuring the "multiplexed," one-gun picture tube.

The Sanyo unit, with a suggested retail price of \$1,095, permits up to 50 per cent more playing time on a standard Beta three-hour cassette. Also, (in the extended play mode) pressing a pause button will instantly stop the tape, freezing the action on the screen for more detailed study.

ALSO showing new VCRs were Sharp, with a programmable two and six hour VHS system; Toshiba with a five-hour programmable Beta format; Akai's first VCR entry — "Activideo" — (see Figure 2). The timer can be programmed to record two programs per day for up to seven days. It also has an automatic battery recharger. Suggested retail, though, is \$1,495.

Toshiba showed its new five-hour, programmable VCR. This unit, with a suggested retail of about \$1,400 carries a "freeze frame" feature together with a fast scan capability.

Toshiba's LVR

However, without question the major attraction in VCRs this year was the display of Toshiba's prototype fixed head, endless loop, tape recorder the LVR (Longitudinal Video Recorder).

The work of Dr. Norikazu Sawazaki, the inventor of the helical scan system, the new LVR system (see Figures 3 and 4) crams an astounding 220 recording tracks on a 100-meter long endless loop tape. According to Toshiba, this model eliminates about two-thirds of the mechanical components now used, and is therefore much smaller in size and potentially cheaper.

The 220 recording tracks are accessed by the "fixed" head's ability to move up or down in relation to the width of the one-half inch tape. Tape motion is at high speed so that each track provides about 17 seconds playing time, or some 62-1/3 minutes (220 x 17) in total. A microprocessor controls positioning of the head and stepping to the next rack when the end of the current track is reached.

Toshiba says the "interesting" aspect is the random access of any selected track within a few seconds, just the time required to reposition the head. This provides virtually "instant" playback of recorded material.

Potential uses of this system when developed, Toshiba says, are data memory, video file, product explanation, surveillance and others.

Programmable TV

On the television side of things, RCA is out with its fully programmable home security system television chassis (Figure 5). While I won't go into the circuitry involved at this time (since this will be part of ET/D's annual review of new TV chassis this September), RCA is adding to some of its ColorTrak receivers a 7-day programmer. A digital clock when not displaying channel information, this AutoProgrammer controls set turn on and off and permits channel changes and schedules to be "ordered," up to seven days in advance.

Additionally, the programming instructions can be accessed and read by the set user for editing or schedule changes as desired. An AC plug on the set is included so that a lamp can be scheduled to turn on and off at various intervals while the owners are away.

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Both the DP-50 and DP-100 are well protected against overload and accidental polarity reversal. You can see the logic of it all today! Contact your B&K-PRECISION distributor for immediate delivery.



Circle No. 106 on Reader Inquiry Card 20 / ET/D - August 1979

Incidentally, RCA is the first manufacturer we've heard about to follow Magnavox's suit of adding a high picture resolution comb filter to its circuitry (see ET/D, Sept. '78).

About the only other real innovation insofar as television is concerned, was the introduction, by Panasonic, of Matsushita's new one-gun color CRT which uses only 60 per cent of the power of a comparable CRT (see ET/D, March, p. 27). Panasonic is using this tube in its new battery-operated (nine "D" cells) portable (see figure 6).

This unit, the CT-1010, has a 4.5 inch screen, weighs 10 pounds and features pushbutton channel selection.

Home computers

While most of the computer manufacturers seemed to toss in the towel on the so-called "home" or "personal" computer market — and direct their efforts toward "small"



Fig. 7–The TI-99/4 home computer system, including 13-inch color monitor, retails for about \$1,150

business applications — at least one company went in the opposite direction — Texas Instruments.

With the majority of the personal computer people opting for the National Computer Conference (run simultaneously with CES) in New York — TI came up with what in my opinion is the most user oriented personal computer on the market. From the standpoint of ease of operation and available software, TI's 99/4 home computer system (complete with 13-inch video monitor manufactured by Zenith) is really — in this writer's opinion — the first small computer system that can really be called a "home" system.

The key to TI's approach is its solid state software packages, which will range in price from \$20 to \$70. These are solid state, pre-programmed ROMs which when inserted into the console permit up to 72K bytes of RAM and ROM (combined).

Features of the TI-99/4 are 16 colors for graphics, music and sound effects generator, built in equation calculator, and 13 digit floating point BASIC. Solid state software packages include games, including football and chess, investment analysis, personal record keeping, graphics, and educational packages such as statistics, grammar, reading, etc.

Scheduled for late summer or fall introduction, the system will retail for about \$1,150.

Computerized security

Ohio Scientific, another of the high technology companies that is strung midway between the "home" and "small business" computer environments, showed its amazing \$5,000 C8P DF "home computer of *continued on page 47*



Fig. 8–Ohio Scientific's computerized home security system and personal computer combination. It carries a \$5,000 pricetag.

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3. SCANNER SYSTEMS: Timing events in video signal; how they're determined, generated and physically placed on tape. (23 min.) TAPE FORMATS:

The control, video and audio tracks; considerations, specifications, adjustments and alignments. (30 min.)

5. TAPE TRANSPORTS How tape is moved across stationary and rotating heads; transport functions; cassette machine operations. (23 min.)

6. SCANNER SERVOS:

Positioning video heads; record/ playback differences; adjustments; visible symptoms of problems shown.(30 min.)

7. LUMINANCE PROCESSING: Electronic signal processing in record/playback closely examined; theory and design of circuits; hows and whys of specific alignments. (29 min.)

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Surface acoustic wave filters

Their impact on consumer electronics grows

First Zenith, now Toshiba, and soon others are sure to follow with these special passband filters for truly "alignment free" television.

By Paul Shih

Surface-acoustic-wave (SAW) devices have been used for several decades to provide a number of specific signal processing functions in industrial and military communications. However, the use of SAW filters in television receivers has been realized for only a few years. It is anticipated that wide-spread use of SAW devices by the TV industry will follow that of dgital tuners which has gradually become commonplace.

This article attempts to describe the basic theory and operation of the SAW filter and presents a practical example in which a SAW filter is used in the IF section of a TV receiver.

Piezoelectric effect

The operation of SAW devices is primarily based on the principle of piezoelectricity. Nearly a century ago. Pierre and Jacques Curie discovered an inherent property, called piezoelectric effect, in certain natural crystals, such as rochelle salt, quartz, and sodium chlorate. The piezoelectric effect is exhibited by the deformation of piezoelectric materials through pressure, tension or shear. It is accompanied by the appearance of an electrical potential across particular surfaces, or the application of a potential difference across the surfaces is transformed into a mechanical strain or stress in the materials. Some 60 years after the first discovery of piezoelectricity, it was recognized that piezoelectricity can also occur in certain

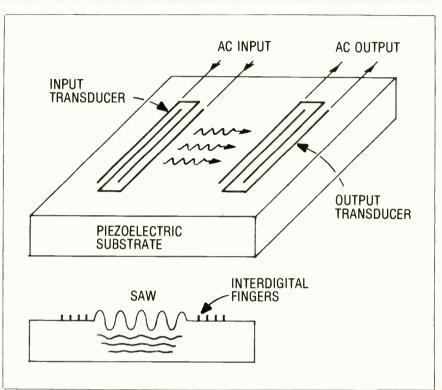


Fig. 1-The initiation and propagation of surface acoustic waves.

materials other than single natural crystals, and the effect was demonstrated in high polymers and some synthetic materials. The most widely used piezoelectric materials nowadays for SAW components are lithium niobate, bismuth silicon oxide, lithium tantalate and thin-film zinc oxide.

Surface acoustic waves

The fundamental physics of acoustic, or Rayleish, waves which propogate on the surface of solids was first described by Lord Rayleigh in 1895. Basically, the acoustic waves are launched on a solid surface by a thin metal transducer deposited on the surface of a piezoeletric substance.

Tha AC electrical signal applied to the transducer electrodes causes the substrate material between the electrodes to be distorted due to the piezoelectric effect. This periodic strain spreads on the surface for some distance, but decays expoentially into the solid within a very short distance from the surface. The mechanical deformation on the surface manifests itself as acoustic surface waves propagating from the input transducer to an output transducer. The basic setup for generating surface waves is shown in Fig. 1.

Detection of the SAWs by the output transducer transforms the surface periodic strain back to the corresponding periodic electrical signal which appears across the output terminals of the SAW device.

The SAW can also be generated and detected on the surface of a non-piezoelectric substrate. This

process can be accomplished by employing structures which are composed of zinc oxide piezoelectric film layers overlying interdigital metal electrodes (Fig. 2). Application of an electrical signal to the electrodes which are sandwiched between the oxide film and the non-piezoelectric substrate will cause the mechanical strain in the film to be transferred onto the

non-piezoelectric surface. This transfer process causes SAWs to be generated on the non-piezoelectric surface. Upon receiving the SAWs, an output transducer converts the acoustic waves back to an electrical signal by a reverse geometic structure of the transducer determines the bandwidth and the frequency characteristics of the SAW filter. High-frequency SAWs are generated or received at that part of electrode array (or comb) which has electrodes (fingers) close together; whereas low-frequency SAWs are generated or received where the fingers are further apart.

A structure with uniform fingers responds best to one frequency whose wavelength equals the periodic distance L of the fingers (Fig. 3). A uniform array with only a few fingers has broad frequency responses above and below

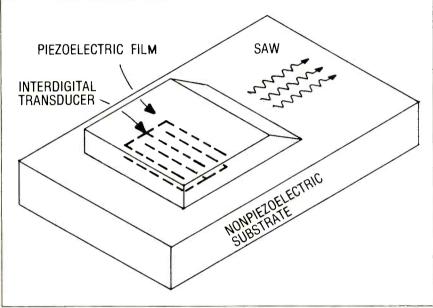


Fig. 2-A look at the physical layout of the interdigital transducer on a non-piezoelectric substrate.

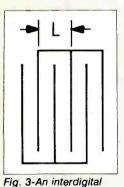


Fig.4-The weighted finger

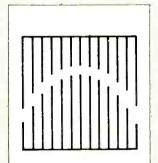


Fig. 5-This "dummy-finger" array provides better phase response.

piezoelectric process.

transducer with uniform

fingers.

Interdigital transducers

For most surface acoustic wave (SAW) filters, the interdigital transducer is the prime component. It consists mainly of a periodic structure of film-coated metal electrodes deposited on the surface of a piezoelectric substrate by a photolithographic process. The

array.

the fundamental frequency. This characteristic makes the array suitable for broad-band operation as a receiving transducer. If a large number of uniform fingers is used, the frequency response of the array is sharpened, resulting in limited bandwidth operation.

For control of specific frequency response with sharp cutoffs, the fingers are amplitude "weighted" during the design process by varying the amount of overlapping of electrodes in certain parts of the array (Fig. 4). One drawback, however, for the non-uniform finger overlapping is phase distortion caused by different propagation velocity as the SAWs travel through each pair of overlapped fingers. One geometic structure that can provide specific frequency response and has very little phase distortion is an array of dummy fingers as shown in Fig. 5. With this latter structure, the propagation velocity of the waves is not altered because the SAWs "see" the same amount of "metal" as they propagate through each pair of now-overlapped (dummy) electrodes. Other methods employed to decrease the undesirable spurious response include use of split fingers and slant electrode arrays.

Multistrap coupler

Distortion in SAW transmission can also be caused by spurious bulk-wave signal reflection. This undesirable source for distortion can be suppressed considerably by the use of a multistrap coupler (MSC). The coupler, consisting of parallel metallic straps deposited on a substrate, can transfer acoustic energy from one acoustic track to another (Fig. 6).

The bulk waves which are generated along with the SAWs by an interdigital transducer become prominent as the number of finger pairs is reduced to provide broadband operation. Most of the bulk-wave energy penetrates into the solid, but the bottom surface of the solid substrate may reflect the energy back to the top surface. The reflected bulk waves may cause interference to SAW operation. If this kind of interference is allowed to go unchecked in filtering operation, it can degrade the stop-band performance and cause spurious response. The use of MSC in an arrangement shown in Fig. 6 can keep most of the reflected bulk waves off the SAW propagation path, thereby reducing the bulk-wave interference. Due to this desirable characteristic, the MSC may be used to couple a "weighted" finger array to a uniform array with only a few fingers for wideband operation.

Another way to suppress the bulk-wave interference involves treatments of the substrate bottom surface, such as cutting oblique grooves or drilling blind holes. Certain substrate materials have a property of retarding the bulk-wave propagation; therefore, a simple treatment of the substrate bottom surface as mentioned above is adequate to control the bulk-wave interference without having to use the MSC.

Coupler design generally involves choice of the strap length and the optimum strap repeat distance. For specific bandwidth response, the repeat distance of straps is critical. With proper design, transmission and reflection response for an MSC can approach almost 100% transfer from one track to another with very little or no loss.

Transit response

Triple transit response refers to SAW reflection along the propation path between the input and output transducers. This phenomenon occurs when part of the SAWs is first reflected off the receiving or output transducer and later reflected back to the output transducer by the input transducer. These double-reflected waves take three times as long to produce an output at the receiving transducer as do the original waves after leaving the transmitting or input transducer. This kind of time delay in a video transmission can cause multiple images or "ghosts" in the reproduced picture.

Triple-transit echoes can be suppressed by using undirectional transmission in which two mismatched transducers are employed to cancel out waves traveling opposite to the forward propagating direction. One disadvantage, however, for such unidirectional transmission is high signal loss due to cancellation of energy.

Another way to reduce the triple-transit response is to use a split-finger array as a receiving transducer. Waves reflected by the split fingers are twice as high in frequency as the original waves, and therefore they are too far away from the passband to cause any further interference.

SAW IF filters

Basically, all SAW components are in one way or another bandpass structures, and bandpass filters are among the most fully developed SAW devices. Traditionally, SAW devices are used exclusively for signal processing in industrial or military communications and radar systems. However, potentially large-scale application of the SAW components in consumer electronics is possible due to research and development in manufacturing technology and cost reduction.

The greatest potential for SAW filters in consumer products is probably in television receivers. Typically, in a conventional TV IF section, a number of

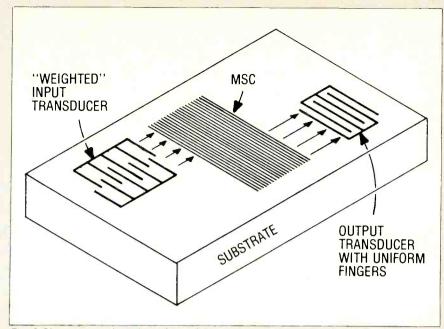


Fig. 6-Shown above is a view of the multistrap coupler used as a track changer.

LC circuits or traps need to be tuned or adjusted individually for specific frequency response during production assembly and occasionally during field servicing. Conversely, a single SAW filter in place of those LC tuned circuits needs no tuning because its specific frequency response band is established during the design and manufacturing process. In addition, the SAW filter is more stable in operation. Once it works in the circuit, one can expect it to function that way for a long time without any attention.

About 10 years ago, DeVries and his co-workers at Zenith Radio Corporation first demonstrated three cascaded SAW filters for use in the TV IF section. The filters, built on lead-zirco-nate-titanate substrate, had a low loss at 44 MHz, a bandwidth of 3.6 MHz and a 50-dB trap attenuation within 1 MHz of the IF passband. However, due to high production costs and technical problems of bulk or spurious reflection, use of the SAW components never went beyond the laboratory at that time. Subsequent research solved the technical problems and found ways to cut the production cost. The result has been the development of SAW filters as practical components and they have been used in some of Zenith's color chassis for several years.

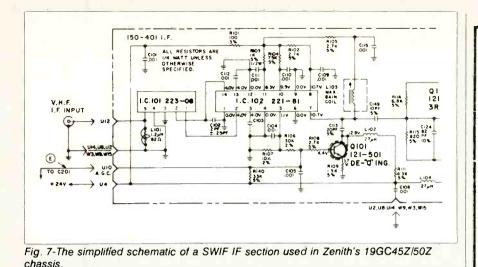
Besides Zenith's pioneer work, a number of industrial laboratories and TV manufacturers have also launched their researches in SAW devices for use in TV circuits. Mullard Research Laboratories, Redhill, England, demonstrated TV IF SAW filters which are built on bismuth silicon oxide substrate. It is claimed that

the substrate being used has better bulk-wave suppression properties than lithium niobate, the most widely used substrate material for SAW filters. As a result, a simple treatment of the substrate bottom surface is enough to check the bulk-wave interference without using a multistrap coupler. Another advantage bismuth silicon oxide has, in addition to its low material cost, is better velocity properties which permit the filter to be built smaller and results in lower production costs. Nevertheless, bismuth silicon oxide does have lower acoustic coupling efficiency which causes more wave-propagation loss than with more expensive lithium niobate.

Toshiba Electric Company of Japan has begun to use SAW devices as IF filters for their 14- and 18-inch color chassis. The filter is fabricated with three sets (input, shield, output) of interdigital aluminum electrodes on lithium tantalate crystal material. The substrate material has good temperature stability and low spurious response and the crystal can be grown in air, instead of in a protective gas environment. This results in low production costs.

Zenith's SWIF

The earlier work on the SAW filter done by Zenith, as previously mentioned, provided the foundation for the development of the current Surface Wave Integrated Filter, called SWIF. The filter is composed of input and output interdigital transducers built along with a miltistrap coupler of 100 metal lines on a 1/2 by 3/16 inch lithium-niobate substrate similar in



arrangement to the one shown in Fig. 6. The input transducer is amplitude "weighted" to provide the required frequency selectivity for the IF section. The typical responses of the input transducer include low signal loss for the 44-MHz I.F. passband, some attenuation for the sound carrier at 41.25 MHz, large attenuation of the signals outside the passband, and sharp trapping action at 39.75 MHz and 47.25 MHz for the adjacent picture and sound carriers.

The receiver or output transducer is intended for broad-band response with its fewer uniform interdigital fingers. Coupling between the two different transducers is carried out by the multistrap coupler that also helps to reduce unwanted reflection of bulk or spurious waves.

The substrate wafer is mounted with epoxy on a thin conductive coating which is deposited on the inside bottom of a ceramic package which in turn is connected to ground in the circuitry. Four terminals for the two transducers are brought out of the package with wire-bonding, and a ceramic lid is used to seal the package with epoxy.

The SWIF (IC 101) has been used in a number of Zenith's color chassis. A simplified schematic of an IF section using a SWIF as found in Chassis 19GC45Z/50Z is shown in Fig. 7.

Wideband tuner

A wideband tuner with a bandwidth of 10 MHz is used with the SWIF IF section. The input from the tuner is coupled through a 75-ohm IF cable to pins 4 and 5 on IC 101, the SWIF. L101 terminates the cable in the IF module to provide proper impedance matching to the SWIF. The output from the SWIF at pins 1 and 2 is coupled to pins 2 and 14 on IC 102, a 3-stage IF amplifier. The conductive coating on the bottom of the SWIF is connected to the ground through pin 3 on IC 101.

Several capacitors associated with IC 102 help to stabilize the operation of the amplifier; C102 at pin 14 provides neutralization, and C112 and C103 at pins 3 and 13 respectively decouple the DC feedback network which is used to establish the DC operating point for the amplifier.

An internal zener reference source of 6.3 volts at pin 11 is obtained from a 24-Volt external source at U4 on the IF module. The IF AGC control voltage from IC 401 on the AGC module is coupled through U10 to pins 10 and 5 on IC 102 and also to the base of Q101, the de-"Q"ing transistor.

The amplified IF output is taken across the Max Gain coil, L103, between pin 7 on IC102 and the ground. L103, being the load for the IC amplifier, is the only tuned component before the 3rd IF amplifier.

Transistor Q101 is connected in parallel with the gain coil L103. As the received composite video signal increases in magnitude, so does the AGC control voltage. This action causes Q101 to conduct more current, partially shorting out L103. The result is that Q of the coil is decreased and the IF output at pin 7 is reduced as well. With less signal input to the receiver; the opposite action takes place to increase the gain of the amplifier for more IF output at pin 7. The de-"Q"ing network, functioning as a variable damping resistor for the gain coil L103, helps to maintain the constant video and sound output under varving signal strength conditions.

Conclusion

The earliest applications of surface-acoustic-wave filters were continued on page 47

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Intro to data converters

The real world is analog.

Most of the new test instrumentation, as well as many of today's consumer products for the home, display information in digital readout form. For a general look at how these circuits function, read on.

By Joseph J. Carr, CET

A large portion of modern industrial, scientific, medical and military instrumentation uses *digital* circuits which may or may not involve a digital computer. Most *transducers* which are used to sense physical parameters such as position, force, pressure, temperature, etc., however, are *analog* devices. They produce an output voltage or current that is proportional to the parameter being measured.

Similarly, strip chart recorders (used to make permanent records of waveforms and other pertinent analog data), and control system components such as motors, require digital interface circuitry in order to put out an analog signal. The circuits which are used as communicators between the analog and digital worlds are called *analog-todigital converters* (ADC) and *digitalto-analog converters* (DAC).

DAC circuits

It is the usual practice to introduce the DAC first, because several of the more popular ADC circuits use a DAC in a negative feedback circuit. The DAC is a circuit that will produce an output voltage or current that is proportional to both a reference voltage (or current) and the digital binary word applied to its inputs. The most common DAC technique is the

registor ladder, of which two types exist: binary weighted and R-2R (see Fig. 1).

The binary word at the input will be made of *bits* that are represented by two voltage levels; 0 volts for logical-0 and some positive or negative voltage for logical-1. These bits, or "binary digits," are represented in Fig. 1 as switches that connect to ground to produce the logical-0 state and *E*1 for logical-1.

The binary weighted ladder circuit is shown in Fig. 1A, and is essentially a multiple-input inverting follower op-amp circuit. Binary numbers are weighted by position, similar to the more familiar decimal numbers (see ET/D, Nov. 1977).

In Fig. 1A each input resistor represents a different weight, with B1 being the most significant bit, and B_n being the least significant bit. From Ohm's law, and the basic rules governing op-amps, we know that output voltage E_o is given by

 $\underline{E}_0 = \underline{E}_1 \times \frac{B1}{R} + \frac{B2}{2R} + \frac{B3}{4R} + \dots + \frac{Bn}{nR}$ Where B1 through B_n are either "1" or "O" depending upon the actual binary

"O" depending upon the actual binary word being represented.

The problem with the binary ladder, however, is that resistor values become unreasonably large or small if more than a few bits are represented. In an ordinary eight bit system, popular in microcomputer applications, if R is 10 Kohms, then the resistor at B8 will be 1.28 megohms. In a twelve bit system, even higher values are needed.

The R-2R ladder

The solution to this problem is to use the R-2R resistor ladder (Fig. 1B). In this circuit all resistors, with the exception of load resistor R_L , have one or two possible values, R or 2R (i.e. 50 Kohm and 100 Kohm are popuar). The load resistor should have a value that is as high as possible.

It is the circuit of Fig. 1B that forms the basis for most commercial DACs. An example of a commercial DAC is shown in Fig. 2. This particular model is the DAC-08 by Precision Monolithics, Inc., and is an example of a *current* output DAC (i.e. no load resistor). The switches in Fig. 1B are now shown as transistors. The output current will be

 $l_0 = lref = \frac{B1}{2} + \frac{B2}{4} + \frac{B3}{8} + ... + \frac{B8}{256}$

Fig. 2B shows a voltage output circuit using the DAC-08 connected to an external load resistor and op-amp buffer. Also shown are the outputs expected for various input words. Note that I_{ref} is created from V_{ref} and a 5.00 Kohm resistor.

The output of a DAC rises or falls in *steps*, and this produces a staircase ramp as in Fig. 3. The value of each step is also the amount of change caused by the least significant bit (LSB), which is given by $V_{ret}/2n$ (where n is the number of bits). In our popular eight bit system, then, the minimum step is $V_{ret}/256$. If V_{ref} is 10.00 volts, as is often the case, then each step is approximately 40 mV.

If the DAC is designed to operate only with positive outputs, then zero volts (or zero mA), is represented by 0000000, but in *bipolar* DACs, 0000000 represents the maximum *negative* output. Since this is a digital system, we find that zero volts actually lies between two of the possible binary states (i.e. 10000000 and 01111111). Examine the chart in Fig. 2B. This phenomenon creates the notion of "plus and minus zero." In the eight bit system with a 10.00 volt reference potential, the nearest we can get to zero is 40 mV.

ADC circuits

Although quite a few different ADC circuits exist, we are going to consider

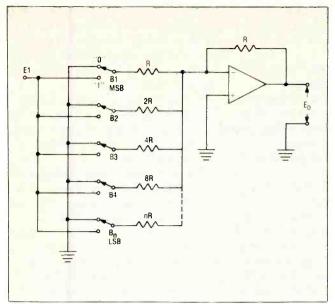
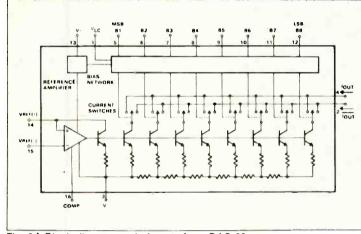


Fig. 1A-Binary weighted resistor ladder DAC circuit



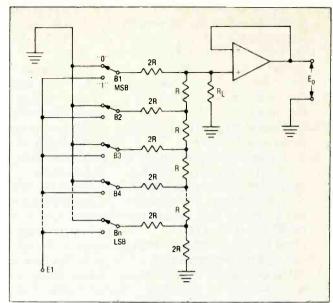


Fig. 1B-R-2R resistor ladder DAC circuit

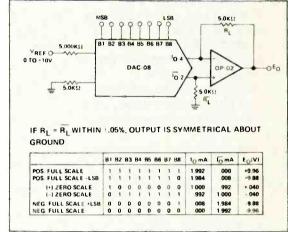


Fig. 2A-Block diagram and pin-outs for a DAC-08 eight bit IC DAC.

only the ramp, successive approximation, and dual-slope integrator. Those readers who desire more information may be interested in my book "How to Design & Build Electronic Instrumentation," TAB Books Cat. no. 1012.

The block diagram for a ramp type of ADC circuit is shown in Fig. 4. Note that this circuit is also called the binary counter ADC or the servo ADC. The principle sections of the circuit are a binary counter, a DAC, a voltage comparator, and a control logic section.

When a *start* pulse is applied, the control logic section resets the binary counter to zero, making the DAC output also zero. Since the DAC output E_o is less than E_{in} the comparator output is HIGH. This output level remains HIGH until $E_o = E_{in}$.

A clock causes the binary counter to increment once for each clock pulse, so the DAC output voltage will ramp upwards (see Fig. 4B), changing one step for each pulse. When $E_o = E_{in}$, then the comparator output drops LOW, shutting off the counter, and issues an *end-of-conversion* (EOC) pulse. The binary number on the output of the counter when the comparator stopped the action is latched, and represents the analog input voltage E_{in} . In an eight-bit, unipolar, ADC 0000000 usually represents 0 volts, and 11111111 represents fullscale, in our example 10 volts.

The ramp-type ADC is used where moderate operating speeds are needed. The conversion time for a fullscale input is 2n clock pulses, where n is the number of bits. Suppose, for example, that we have an eight bit ADC using a 100 kHz (i.e. 10 μ S period) clock. The fullscale conversion time would be (2⁸) 10 μ S), or 2560 μ S (2.56 mS).

The successive approximation ADC circuit of Fib. 5A operates at a much higher speed, and can complete a conversion in (n + 1) clock pulses. For

Fig. 2B-Voltage output, bipolar, connection, with table showing output voltage level for various input states.

our hypothetical eight bit system using a 100 kHz clock, the conversion time would be $(8 + 1)(10\mu S) = (9)(10\mu S) =$ 90 μ S, which is 28 times faster than the ramp type ADC operating at the same clock frequency. The principle components are the DAC, voltage comparator, and a special successive approximation register (SAR).

The SAR previously was constructed of discrete digital logic components in the past, but now some semiconductor manufacturers offer SAR integrated circuits. An SAR, whether discrete or integrated, consists of some control logic, output latches, and a shift register (i.e. array of cascaded flip-flops). The output latches are connected to the digital inputs of the DAC.

ADC circuit operation

When the *start* pulse is received, the control logic clears the SAR, setting all shift registers and output latches to "0." The operation is as follows (assume that

- $E_{in} = 6$ volts in this example):
 - 1. On the first clock pulse following the start pulse (i.e. t1 in Fig. 5B), B1, the MSB, is set HIGH. The word applied to the DAC, then, is 10000000. This word produces a DAC output E_0 of 5 volts dc (i.e. half-scale).
 - 2. E_o is less than E_{in}, so the SAR sets output latch B1 HIGH.
 - 3. On the next clock pulse (t2), B2 is set HIGH, producing an output word 11000000. E_0 is now 7.5 volts, so is greater than E_{in} . This situation tells the control logic section to set the B2 output latch LOW.
 - 4. At the time t3, bit B3 is set HIGH, making the new output word 10100000. E_0 , then, is 6.25 volts so is greater than E_{in} . Again, the control logic section sets the output latch LOW, leaving the w000.
 - 5. At time t4, bit B4 is set HIGH, giving an output word of 10010000. The value of E_0 is now 5.63 volts, so E_0 is less than E_{in} . In this case, then, the output latch is set HIGH, leaving the word at 10010000.
 - 6. This process continues for four more trials. At each trial the output latch is set LOW if E_0 is greater than

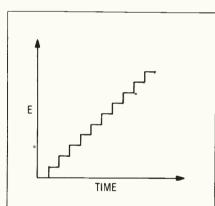
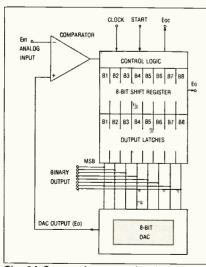
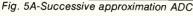


Fig. 3-Step ramp output voltage





 E_{in} , in set HIGH if E_o is less than E_{in} . An EOC pulse is issued following the ninth clock pulse, or when $E_o = E_{in}$.

The successive approximation type of ADC is used where high speed is required. Although most are designed for use with clocks between 500 Khz and 2.5 Mhz, some circuits exist using clocks as fast as 13 Mhz, resulting in conversion times of less than 700 nanoseconds.

One of the slowest ADC circuits is the dualslope integrator. But what it lacks in speed, it makes up in operation. The dual-slope integrator is more immune to noise on the signal than are the other types. The dual-slope integrator, then, is almost ideally suited for use in digital voltmeters. In fact, most DVMs use this type of ADC.

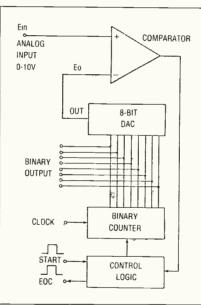


Fig. 4A-Ramp type ADC

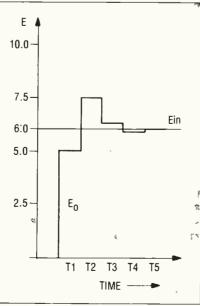
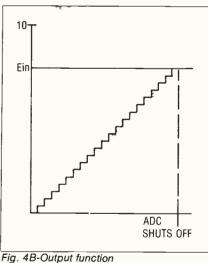
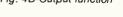


Fig. 5B-Output function

The block diagram of the dual-slope integrator is shown in Fig. 6. It consists of an operational amplifier integrator (A1), a voltage comparator (A2) a binary counter, and a control logic section. The operation is as follows:

- A start pulse at time t_ocauses the electronic switch S1 to connect the input of the integrator to the analog input signal, and to reset the counter to zero.
- 2. The integrator output signal begins to rise as capacitor C1 begins to charge under influence of E_{in} . As soon as E_A is more than a few millivolts above ground, the output of comparator A2 goes HIGH, thereby turning on the counter.
- 3. The counter increments until it overflows (t1). The counter's overflow creates a *carry* pulse that tells the control section to switch S1 to connect the integrator input to the precise stable reference source.
- At time t1 the counter is at zero, and the charge on C1 is proportional to the average value of E_{in} during the t₁-t_o interval.
- 5. Between t₁ and t₂ E_{ref} causes C1 to discharge at a constant rate. During this same period the counter is incrementing once for each clock continued on page 49





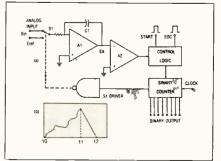
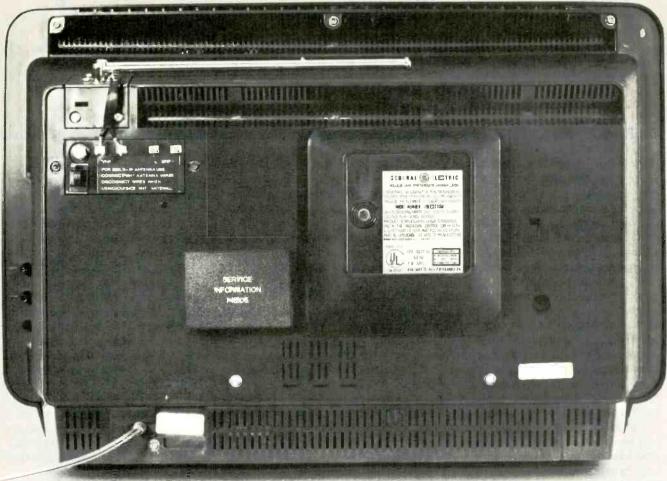


Fig. 6-Dual slope integrator ADC

28 / ET/D - August 1979

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Vs sine waves

You cannot simply depend upon the apparent frequency of a waveform to predict circuit behavior. Here's an explanation why.

By Bernard Daien

It may come as a shock to experienced technicians to learn that inductive reactance is not 2 pi f L, and capacitive reactance is not $\frac{1}{2 \text{ pi f C}}$ for most of the waveforms encountered in electronic equipment! Similarly, peak voltage is not 1.4 times rms for such waveforms.

The classic formulae apply only to a sine wave, which is a most unusual waveform because it is the only waveform that consists of a single frequency. All other waveforms consist of a fundamental and one or more harmonics. The formulae used for sine waves cannot be applied to non-sine waves, and other means must be used to deal with them.

Common examples of non-sine waveforms are the vertical and horizontal sync pulses, vertical and horizontal sweeps, video wave forms, audio waveforms, and practially all digital waveforms. Thus, it is essential that the modern technician understand non-sine waves. This article discusses, in easy style, some concepts of non-sine waves, how to deal with them, and how to use them.

Terminology

The sine wave is the only waveform which cannot be considered to be a "pulse." All other waveforms consist of more than one frequency, all harmonically related. The output of a half wave rectifier is a series of pulses, even though it is half a sine wave. When we speak of pulses, the term "repetition rate" is used, not "frequency," since the

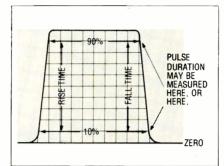


Fig. 1-Pulse rise and fall times.

pulse consists of many frequencies.

Other terms used with pulses can be defined with the aid of Fig. 1... "rise time" is the time required for the voltage or current to rise from the 10% level to the 90% level. "Fall time" is the time to fall from 90% to 10%. "Pulse duration" may be measured in any of several ways—so be careful. It can be measured at the 10% point, the 90% point, or in terms of a square wave, which contains the same amount of energy as the pulse being examined.

Each pulse shape has its own relationship between peak, average and rms. The common square wave pulse has a ratio of 1 to 1 to 1, i.e., peak, average, and rms are the same. A term commonly used is "crest factor," which is the ratio of peak to rms. As you know, a sine wave has a ratio of 1.4 between rms and peak; thus, it has a crest factor of 1.4. Some other wave forms frequently seen are the triangular wave with a crest factor of 1.73, and the previously mentioned square wave with a crest factor of 1.0.

Another variable we must deal with is "duty cycle." Fig. 2 illustrates pulses with 50% and 10% duty cycles. Pulses with a low percentage duty cycle have a small rms value. Viewed in a somewhat simplified way, duty cycle is the ratio of "on" to "off" time.

One way to determine the energy in a waveform is to reproduce it on graph paper, as shown in Fig. 3. Energy in the

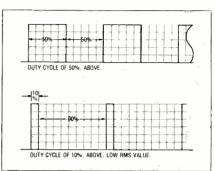


Fig. 2-Pulse Duty Cycle.

wave is proportional to the area under the curve. By counting the number of boxes, and the number of half boxes, etc., and adding them up, we can arive at the total number of boxes under the curve. We can then construct a square wave with the same total number of boxes, and the same peak amplitude. It then becomes a simple matter to determine any equivalent factor, since the rms, average, and peak of the reconstructed wave are equal.

Pulse composition

A sine wave has a single frequency and, therefore, occupies a very small bandwidth. It passes through circuitry of any bandwidth, with no change in waveform, but it may be changed in amplitude. A pulse has changes in its waveform when passing through circuitry which is not capable of passing the entire bandwidth of the pulse. Since the pulse has harmonics, the bandwidth required is considerable. Fig. 4 illustrates some common waveforms and their harmonic content.

You already know that in a color TV set, horizontal sync pulses are formed into sharp spikes by the horizontal differentiator circuit. This is an example of how a pulse can be changed in shape by the bandwidth of the circuitry, since a differentiator is an RC high pass filter, which passes the high frequencies, but attenuates the low frequencies.

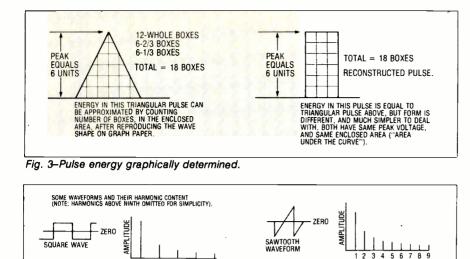


Fig. 4-Harmonic content of waveform.

HARMONIC CONTENT

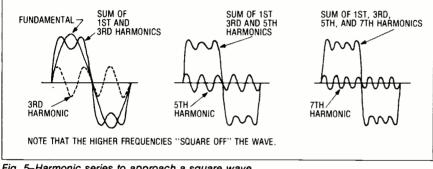


Fig. 5-Harmonic series to approach a square wave.

Look closely at Fig. 5. Notice that it is the higher frequencies which fill in the corners, and square off the sides of a square wave. If the high frequencies are suppressed, we get a sine wave (the fundamental only). If we suppress the low frequencies, we are left with only the steep sides of the wave or the spikes... which is the principle of differentiation.

A Frenchman, Jean Fourier (pronounced Foor-yay), first stated that pulses can be analyzed as a series of harmonically related sine waves. Fourier's Theorem resulted in some interesting revelations about pulses: 1. The fundamental frequency is the pulse repetition rate; 2. The waveshape depends upon which harmonics are present, their relative strengths, and phase relationships; 3. The series of pulses may contain a dc level.

Let's look at the last statement with the aid of Fig. 6, which is a series of identical square wave pulses with a 50% duty cycle. We rely upon this dc level when using "dc restoration" in a TV set.

We can sum up by stating that if the positive half of the wave is greater than the negative half, we have a net positive dc level. If the negative half is greater, we have a net negative dc level. The absolute value of the positive or

negative dc level also depends upon the cycle, as discussed earlier.

HARMONIC CONTENT

Square wave analysis

Square waves are easily generated by amplifying and clipping sine waves. The resulting square waveshape can be used to analyze the characteristics of bandpass amplifiers, such as audio amplifiers, video amplifiers, IF amplifiers, etc. By using the appropriate repetition rate, any circuitry can be quickly tested.

Fig. 7 shows some results commonly encountered in square wave testing, and the causes. Study of these waveforms reveals that tilting of the wave tops and bottoms indicates phase shift, with the direction of tilt revealing phase lead or lag. Rounding of the corners indicates loss of high frequencies. Dishing of the wave tops and bottoms indicates loss of lows. Overshooting on the square wave edges indicates excessive high frequency response. Ringing indicates poor transient response, instability, or the presence of a high Q tuned circuit which is shock excited by the fast rise and fall times of the pulse. It is guite common to have a combination of these defects, resulting, for example, in a wave which has both

loss of lows and phase shift, as indicated by the presence of tilt and dishing.

When using an "X10" high impedance probe with an oscilloscope, you will notice an adjustable trimmer capacitor built into the probe. By viewing a good square wave, and adjusting the trimmer for the best waveform, you actually set the probe for "flat response, thus, passing the fundamental and all the harmonics of the wave. Without this adjustment, pulses would appear distorted on the scope screen.

Reshaping a pulse

Since pulse shapes can be altered by passing the pulse through circuitry which does not have a flat bandpass, we can use this property to reshape a square wave by using a high pass RC filter or a low pass RC filter (RC filters don't "ring"). Look again at the waveforms shown in Fig. 7. Notice that the high pass RC filter yields a series of spikes, useful for sync purposes. This is the old familiar "differentiator" used in TV horizontal sync circuits. To achieve this, the RC time constant (R in ohms X C in farads) must be short when compared to the period of the wave. The low pass RC filter is, similarly, the "integrator" used in TV vertical sync circuits. To achieve this, the RC time constant must be long when compared to the period of the wave. For all practical purposes, we can substitute the words "duration of pulse" or "pulse width" for the term "period," in most cases.

It should be mentioned that pulses consisting of exponential curves, such as shown in Fig. 8, are not suitable for integration or differentiation. . . a not too well known fact, which has led to the frustration of many experimenters. You will recall that the waveshapes which are generated for sync and other purposes involving wave reshaping, are generally square, rectangular, triangular, sawtooth, or combinations thereof. All of these wave shapes have straight sides. Exponentially curved wave shapes are used very infrequently because of the above mentioned peculiarity. Remember, integration and differentiation is accomplished with RC filters. It is possible to change all wave forms, except sine waves with LC filters, such as narrow bandpass, band reject, etc., however. Or with other sharply tuned circuits.

Finally, it should be pointed out that since a pulse has harmonics of the repetition rate, these harmonics will be spaced throughout the frequency spectrum, often up into the UHF range.



Circle No. 123 on Reader Inquiry Card 32 / ET/D - August 1979

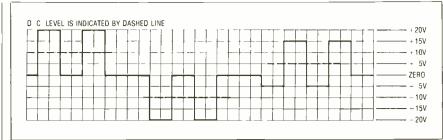


Fig. 6-Pulse DC component.

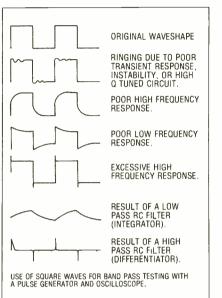


Fig. 7–Use of square waves for bandpass testing with a pulse generator and oscilloscope.

The spacing between harmonics is, of course, equal to the repetition rate. Thus, a 1kHz rep rate will have harmonics spaced every 1kHz through the audio spectrum. A 1MHz rep rate will vield harmonics every 1MHz all the way through the VHF range. This is why switching type power supplies put out so much hash over such a wide range of frequencies, since most of them run at 20kHz to 50kHz, with appreciable power levels. Anytime you are generating pulses, you must be careful about grounding, shielding, and filtering, or you will certainly have radiation problems.

Summary

It was pointed out at the beginning of this article that the usual formulae are not suitable for use with non-sine waves (pulses). Now that you understand that a pulse consists of many different frequencies, in varying proportions, you can better understand why this is true.

Since most technicians have access to an oscilloscope, this article suggested the use of graphical methods of dealing with pulse analysis and pulse testing. There are mathematical methods of great precision, but all require extensive

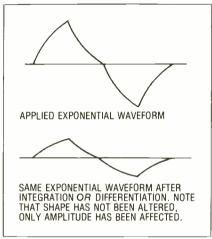


Fig. 8-Exponential wave forms.

use of higher mathematics, and precision measuring instruments, with the capability of handling waveforms with large crest factors. Unfortunately, most of the service shop type of digital voltmeters suffer from several faults which preclude their use for such measurements: A.) Frequency response is generally very limited. B.) They are only calibrated for either a sine wave, or for very low crest factors. C.) They are incapable of handling the very fast rise and fall times in pulses, even when the repetition rate is moderate.

Thus, the value of this article lies in giving the technician with service shop test equipment a practical entry into the world of pulses. Incidentally, since we are dealing with wide bandwidths, and high frequencies, don't forget to use your antenna transmission line theory. Impedances must be matched, and all interconnections become transmission lines... otherwise, you will start to see transmission line reflections, high frequency attenuation, and all the other problems usually associated with the transmission of high frequencies over wires! You cannot use high capacity audio shielded cable for your interconnects, unless they are kept very short. Remember the problems you had with wiring and grounding when you first tried to align a TV IF strip? Some modern computers are running at 100MHz and higher. That's twice the frequency of a continued on page 47

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ETD 8/79

Digital electronicspart IV

More Flip-Flops

Flip-flops are available in several configurations. This month we examine three more types

By Joseph J. Carr, CET

In Part III of this series we introduced you to the concept of the "flip-flop," a digital circuit logic element somewhat more complex than a simple gate. The flip-flop functions as a one bit storage cell, or "memory." It was noted that there were a number of different types of flip-flop circuits, and they operated according to different sets of rules. But one common point among them all was the ability to store a single bit of information, i.e., a HIGH or a LOW condition ("1" or "0").

In Part III you were introduced to four types of flip-flop: NAND logic RS, NOR logic RS, clocked RS, and the master-slave flip-flop.

In this installment, we will discuss the type-T flip-flop, the J-K flip-flop, and the Type-D flip-flop. In considering the latter type, we will also consider a so-called latch circuit, which is a special case of the type-D flip-flop that has become a class of its own in IC families.

Type-T flip flops

The Type-T flip-flop (also known as the toggle FF) is shown in Fig. 1A. This FF can be constructed by providing the feedback connections shown, around a master-slave FF. Recall that the M-S FF was constructed from a pair of RS FFs and an inverter. Note that the *Q* output is fed back to the reset input, and the not-Q output is fed back to the set input.

The type-T flip-flop functions as a binary divider, that is the output signal has a frequency that is one-half (i.e., divide by 2) of the input signal frequency (the clock frequency). The timing diagram for this circuit is shown in Fig. 1B. Note that the Q output changes state only on negative-going transitions (i.e., HIGH to LOW) of the clock pulse. At the first negative transition, the Q output will snap HIGH, and it will remain HIGH until the clock input sees another negative transition. This condition occurs at pulse No. 2, at which time the Q output goes LOW again. We, therefore, have binary division; one output pulse is produced for every two input pulses.

There are sometimes found differences in terminal designations from one text or spec sheet to another. In Fig. 1A, for example, we have called the clock input "MC for "main clock." But it is also very likely that you will see "T" for "toggle," or "Cp for "clock."

J-K flip-flops

One of the most useful, and perhaps most common, types of flip-flop is the J-K. There are several advantages to the typical J-K FF: a) there are no invalid or disallowed states in the clocked mode, b) it can cause the outputs to complement, and c) it can provide non-clocked operation (some IC versions).

Fig. 2A shows one of several popular ways to represent the J-K FF. In this case, we see that it is a type-T flip-flop with the feedback to the set and reset inputs controlled by a pair of two-input AND gates. One input from

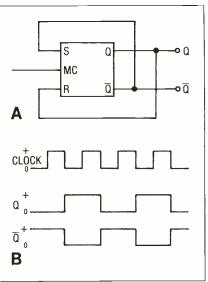


Fig. 1 - A) Master-slave FF connected as a Type-T FF B) Timing diagram.

each gate accepts the feedback lines, while the remaining inputs of the gates are used to form the "J" and "K" inputs, respectively.

Fig. 2B shows the circuit symbol for a J-K flip-flop. Not all versions of the J-K will have the direct mode (preset and preclear) inputs. These inputs do, however, make it a more useful device. The preset input may also be called a direct set, and the preclear input may be called either direct clear or direct reset.

Direct Mode Operation. The operation of the J-K FF in the direct mode is very simple. It is independent of conditions applied to the J and K inputs. The direct mode is controlled by conditions on the preset and preclear inputs, and the rules are summarized in Fig. 2C.

The direct mode inputs are active when LOW, so the only disallowed state occurs when both are LOW

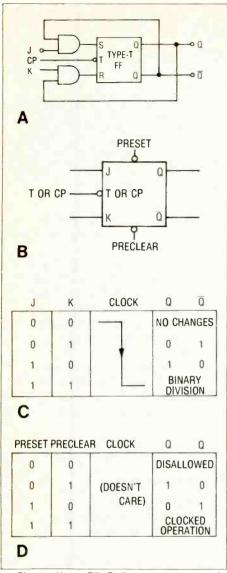


Fig. 2 - A) J-K FF, B) Schematic symbol, C) Truth table for direct mode operation, D) Truth table for clocked mode operation.

simultaneously.

If the preset input is LOW, and the preclear input is HIGH, then the outputs immediately go to a condition where *Q* is HIGH and not-*Q* is LOW.

If the preclear input is made LOW, and the preset input is made HIGH, then the outputs go directly to the state in which Q is LOW and not-Q is HIGH.

It is a general rule, when dealing with flip-flops of any type that set or preset operations make *Q* HIGH, and clear, preclear, or reset operations make *Q* LOW.)

If both preset and preclear inputs are made HIGH, then the flip-flop is ready for normal clocked operation.

Clocked Mode Operation. Whenever the preset and preclear inputs (where used) are simultaneously HIGH, the J-K FF will operate in the clocked mode. The rules for clocked operation are summarized in Fig. 2D.

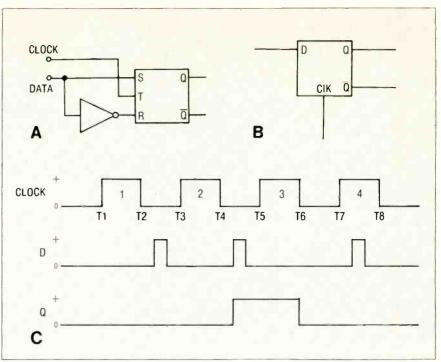


Fig. 3 - A) Type-D FF circuit, B) schematic symbol, C) Timing diagram

Like the type-T FF, the J-K FF (in clocked mode) reponds on the negative-going transitions of the clock pulse. No output changes will occur, regardless of changes at the J and K inputs, until one of these negative-going clock pulse transitions is seen. The outputs will then respond according to the J-K input conditions. The rules for clocked operation of a J-K FF are as follows:

a) If both J and K are LOW, then the FF is inert and does nothing. No changes will occur at the outputs, even though the clock is pulsed.

b) If J is LOW and K is HIGH, then the clocking makes Q LOW and not-Q HIGH.

c) If J is HIGH and K is LOW, then clock pulse transitions make Q HIGH and not-Q LOW.

d) If both J and K are HIGH, then the J-K FF behaves very much like a type-T FF; clocking complements the outputs. This means that negative-going clock transitions force the outputs to go to the opposite state. The output waveform is identical to Fig. 1B.

The type-D flip-flop is shown in Fig. 3. The equivalent circuit is shown in Fig. 3A, while the usual schematic circuit symbol is shown in Fig. 3B.

The equivalent circuit is a clocked R S FF in which the set and reset inputs are fed by the same signal, but out of phase with each other. An inverter accomplishes this neat trick.

The common line to the set-reset-inverter is called the data or

"D," input. This line is usually labeled "D" on most schematics and schematic symbols (i.e. Fig. 3B).

The rule for the operation of the type-D FF is very simple: data appearing on the D input will be transferred to the Q output only when the clock line is HIGH.

a) If the clock is HIGH, then the output follows changes in the D input (i.e., Q goes HIGH when D is HIGH and LOW when D is LOW).

b) If the clock is LOW, then the output retains the last data that existed on the D input at the instant the clock line dropped LOW.

These rules can be seen by the timing diagram in Fig. 3C. While reading the description below, keep in mind the rules of operation given above.

1. When the first clock pulse arrives (T1, T-2), the D input is LOW so the Q output will be LOW.

2. During the interval T2-T3, the D input goes HIGH, but since no clock pulse is present it cannot affect the outputs.

3. At the beginning of interval T3-T4, clock pulse No. 2 is HIGH, but the D input is LOW. The output, therefore, remains LOW.

4. About midway through clock pulse No. 2, however, the D input goes HIGH, forcing the Q output to also go HIGH.

5. The Q output stays HIGH even after clock pulse No. 2 goes LOW.

6. At the onset of clock pulse No. 3, the D input is LOW, so the Q output

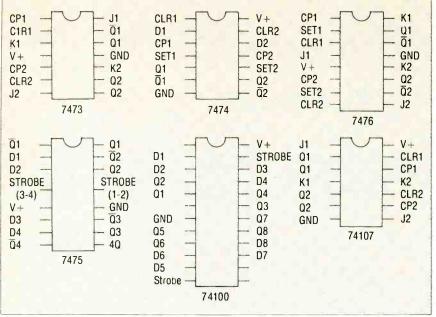


Fig. 4 - Pinouts for popular FF ICs

drops LOW also.

7. The pulse on the D-input during the interval T6-T7 cannot affect the Q output, because the clock input is LOW.

The so-called "data latch" is a special case of the type-D FF. This device is used in digital readout circuits, i.e., on a frequency counter or similar instrument, to hold current data until the new data has been updated and is ready for presentation. This gives the illusion that the data is updated instantaneously. In most cases, the clock input is called a strobe input. Data at the D input will be transferred to the outputs only when the strobe line is HIGH. The idea is to momentarily bring the strobe line HIGH when the data at the input is valid, and then let the strobe go LOW again until the new data is ready.

IC flip-flop examples

Very few designers will use the gate circuits for flip-flops presented in this article. The reason is that IC manufacturers offer IC FFs that can be used as circuit building blocks, reducing the number of interconnections needed. Below are listed some of the more popular examples. (Fig. 4 shows the pinouts of the devices discussed in this section.)

- 7473 dual J-K level-triggered FF with preclear Each section is a J-K FF, in which the clock input responds only when LOW (TTL).
- 7474 Dual Type-D, edge triggered FF. This is a type-D FF that

allows output state changes only on positive-going transitions of the clock pulse. (TTL).

- 7475 Quad latch. This IC contains four type-D FFs, arranged so that the clock lines for two are tied to one strobe pin (No. 13), and the clock lines to the remaining two are connected to another pin (4). When the strobe lines are HIGH, the outputs will follow the data applied to the inputs, but when the strobe is LOW the outputs will retain the last valid data before the strobe pulse dropped LOW. (TTL).
- 7476 Dual level-triggered J-K FF with both preset and preclear inputs
- 74100 Dual quad latch circuit. Can be used as an 8-bit latch.
- 74107 Similar to 7473 but uses standard pinouts for +5 voltd and ground (TTL).
- 4013 Dual type-D FF (CMOS)
- 4027 Dual J-K FF (CMOS)

Experiments

In the experiments to follow we will investigate the operation of the flip-flop. A type 7476 device is used because it has both preset and preclear inputs. The circuit of Fig. 5 is used. Only a Powerace 102 is needed.

Experiment No. 1

Direct mode J-K operation

- 1. Connect the circuit of Fig. 5
- 2. Set the following conditions

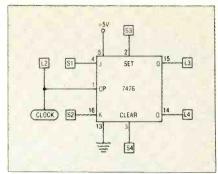


Fig. 5 - Circuit for experiments.

- a. J (S1) and K (S2); HIGH
- b. Set (S3) and clear (S4): LOW
- c. Clock: off
- 3. Observe Q (L3) and not-Q (L4). Q should be LOW (L3 off) and not-Q should be HIGH (L4 on).
- Turn on the clock. Have any changes in L3/L4 taken place? (There should not be any change.)
- Set J to HIGH. Any change? Set J to LOW, K to HIGH. Any change? Set J and K both HIGH. Any
- change?
- 6. Repeat steps 1- 5, but with set (S3) LOW and clear (S4) HIGH.

Experiment No. 2.

Clocked J-K operation.

- Connect the circuit of Fig. 5
 Set up the following conditions

 a. Set (S3), clear (S4), J
 (S1) and K (S2): HIGH
 b. Clock: off
- 3. Turn the clock on, and observe L2 (clock signal) and L3 (Q output signal). Note the binary division action.
- 4. Make J LOW and K HIGH. Observe L3/L4.
- 5. Make J HIGH and K LOW. Observe L3/L4.

Experiment No. 3.

Complementing the output on clock pulse. Connect the circuit of Fig. 5, except replace the clock with S6-Q. This will cause the clock input of the 7476 to go HIGH when S6 is pressed, and then drop back LOW when S6 is released. S6 is used to allow us to manually clock the FF, while observing the output.

- 1. Set S1 S4 HIGH
- 2. Clear the FF by momentarily bring S4 LOW. Q is now LOW (L3 off) and not-Q is HIGH (L4 on).
- 3. Set J LOW
- continued on page 47

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SK Solid State Replacement Guide, 1979 edition, has recently been announced by RCA. The new edition reportedly lists 957 replacements for over 153,000 types of domestic and foreign semiconductor devices. A notable feature of the new guide is the dual stock number system referring where applicable to the ECG (GTE/Svlvania) numbering system. As an example, the SK 3444 is now listed as a SK 3444/123A since it is a direct replacement for the ECG-123A. The guide includes a comprehensive data section and an index. Available from your RCA SK distributor or for \$1.50 from RCA Distributor and Special Products, PO Box 597, Woodbury, NJ 08096.

A new 32-page catalog "1979 CSC" features signal generators, test instruments, logic probes, frequency counters, solderless breadboards, digital troubleshooting instruments and IC test clips from *Continental Specialties Corporation*. New products in this catalog include four instrument cases and the experimentor system of complimentary breadboards, circuit boards and worksheet pads. The catalog is available from CSC distributors or Continental Specialties Corporation, 70 Fulton Terrace, New Haven, CT 06509.

Walsco, Division of GC Electronics has recently published its 1979 catalog featuring a number of new products. The catalog includes belts, idler and drive wheels and pressure rol-

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lers for recorders and phonographs and has an added section on belts for video cassette recorders. The catalog also includes a cross reference which covers hundreds of models of 247 different manufacturers. The Catalog/ Replacement Guide is available from all GC-Walsco distributors.

Digital Multimeters and other test equipment from strip chart recorders to the latest version of the ubiquitous 260 family of analog multimeters are featured in Simpson Electric Company's latest catalog. Simpson offers a wide range of digital and analog panel meters, a series of digital multimeters, frequency counters, prescaler, one of the broadest of lines of analog multimeters and other test meters, temperature meters, insulation testers, clamp type ammeters, noise level meters, illumination meters, microwave leakage meters, secondary standards, and accessories for all of these. For a free copy of catalog 4900 write to Simpson at 853 Dundee Ave., Elgin, IL 60120.

An expanded 1979 "ECG Semiconductor Master Replacement Guide and Catalog" listing 2200 solid state replacement devices has been announced by GTE Consumer Electronics. The Sylvania ECG line presented in this 354 page book is stated to be the largest and most comprehensive selection of replacement semiconductors in the industry. The 1979 guide lists 596 additions to the ECG line. Copies are available from authorized Sylvania distributors or by mailing \$2.95 to GTE Marketing Services Center, 70 Empire Drive, West Seneca, NY 14224.

Tools and terminals are the major subjects of two new catalogs issued by Vaco Products Company. Catalog SD-222 describes Vaco's "E" paks, featuring 41 bellmouthed insulated terminal styles, and 19 non-insulated styles, as well as Nylon ties, wire connectors and insulated Quick Connects. SD-222 also describes wire strippers and electrical tools. Catalog SD-233 features new product introductions including the TORX 5-in-1 magnetic screwdriver and a 5-in-1 magnetic screwdriver for mobile homes, RV's and campers.

Both catalogs are free by writing Vaco Products Co., 1510 Skokie Blvd., Northbrook, IL 60062 or call 312-564-3300.

The "Radio Amateur's License Manual," 77th edition, has recently been pub-



lished by the American Radio Relay League. The structure of amateur licensing, renewals, license modifications, upgrading, special licenses, and reciprocal and foreign operating are explained. The various configurations of call signs are covered. Then beginning with a novice checklist, (Novice license material is covered in "Tune in the World with Ham Radio,") it continues with a study guide for the Technician, General Class, Advanced Class and Amateur Extra Class Licenses. Study material, questions and answers are included. The "License Manual" also contains information on US and international amateur regulations and the FCC regulations, Part 97, covering amateur radio. The price is \$4.00 and the "License Manual" is available at many distributors or American Radio Relay League, Newington, CT 06111.

Heath/Schlumberger has recently announced publication of its latest Instruments Catalog. This catalog features Heath/Schlumberger's line of assembled computers and electronic test equipment, chart recorders, oscilloscopes, power supplies, counters, multimeters, and signal and function generators. The catalog also lists Heath/Schlumberger's Continuing Education Programs on DC and AC Electronics, Semiconductor Devices, Digital Techniques, and Microprocessors. For a free catalog write Heath/Schlumberger, Dept. 570-200, Benton Harbor, MI 49022.

A 24-page catalog of kits of interest to the two-way radio shop or radio amateur has just been announced by Hamtronics. Products features include a new VHF FM receiver kit with four selectivity options, VHF transmitting and receiving converters, UHF receiving converters, FM transmitters and power amplifiers for VHF and UHF, preamps for VHF and UHF and RF probes for VTVM's. For a copy write Hamtronics, Inc., 65F Moul Rd., Hilton, NY 14468.

A new 100 page professional antenna catalog containing complete mechanical and electrical specifications for more than 250 land mobile antennas and accessories is now available from The Antenna Specialists Company. In addition to product data, the catalog contains information on system planning, special applications and performance standards. A copy is available to qualified two-way radio specialists from the Professional Products Div., The Antenna Specialists Co., 12453 Euclid Ave., Cleveland, OH 44106. ET/D

40 / ET/D - August 1979

TEST INSTRUMENT REPORT

Desoldering has gotten to be quite an art. Getting a 40 pin IC out of platedthrough holes usually results in the destruction of the IC. Desoldering braid is expensive, not to say tedious, for a job of this size. The bulb-type solder suckers don't have enough pull, unless you are lucky, to empty plated-through holes, and the commercial desoldering sta-



For more information about this instrument, circle 150 on The Reader Service Card in this issue.

The Sylvania SS100 Solder Sucker

Effective solder removal

By Walter H. Schwartz

tions require air pressure or a vacuum pump for operation. You look around for some other type of device and find that some of the spring operated solder suckers work pretty well, except like the bulbs, they require two hands to useone for the soldering iron and one for the solder sucker. But then you find you must not use them in many of the new TV's, for they can generate as much as 20,000 volts of static charge when triggered, and you may have to replace every MOS device in the set if you do. So you, at least I usually do, clip the pins off the IC and pull each out separately. If the IC wasn't bad, it sure is now.

The Sylvania SS100 is not quite a test instrument, but its appearance and its price (about \$200) make it more than a simple tool. It is the first and only, to my knowledge, complete and selfcontained desoldering system available, not acknowledging the hand bulb types. It is a neat little package—91/2 in. wide by 81/2 in, high by 6 in, deep-which will fit nicely at the back of your bench, and which contains a small high capacity diaphragm type vacuum pump furnishing suction enough to clear most solder connections or circuit boards. Attached to the pump unit by means of a power cord and a vacuum hose is a hollow tip dual heat (20/40 watt) soldering iron. The vacuum pump is controlled by a switch on the side of the iron handle. Place the tip over the IC pin connection on the board, heat until the solder flows and suck it out of the joint. Turn off the vacuum pump when through with each connection. The air flow cools the iron tip excessively otherwise. Eight tip sizes from .031 in. to .090 in. I.D. are available for almost any size solder connection.

The unit ET/D used was very satisfactory. We were able to clean out platedthrough holes in 1/16 in. board clearly enough so that TO-3 power transistors fell out of the board. I decided to try to salvage some prototype circuit cards that I had bought at a swapfest on the chance they could be salvaged. (New cost about \$8, so for a dime each I thought I'd gamble.) The process was a bit time consuming, but I was able to push parts and leads free guite easily after going over the board with the SS100. (Now if I can just keep those kids interested long enough to salvage all of those cards.) The SS100 seems to have no trouble at all clearing solder from the single sided board, which is used in most consumer electronics, and it can be used satisfactorily to resolder most components. So instead of having that soldering iron ready to go all day on your bench, have the SS100 on 20 watt heat and use it as you would your regular iron. Which brings up the only complaint I have about it. The rack or cradle which is furnished with it does not hold the iron-unless the tip is carefully hooked in the hole. The vacuum hose and power cord are too heavy and pull it off the rack and it doesn't lie conveniently on the bench either. It needs a new holder.

Features include, in case I forgot any that are important, a compressed air outlet to help clear the tip of solder, silverplated nickel tips, eight different sizes of tips (.031 in. and .063 in. are included), and an industrial service rating, which I assume allows continuous use.

Feedback from Sylvania: They don't recommend using the solder sucker as a soldering iron, though I experienced no difficulty with it. Their point is—if you feed excessive solder to the tip, it may fill up unless it is blown clean regularly. You won't really damage anything, just have to remove and clean the tip. **ET/D**

NEW PRODUCTS



Vehicle Detector Circle No. 136 on Reader Inquiry Card

A new detecting system sets up an adjustable electro-magnetic field in a driveway, or any vehicle passage area, to detect vehicle entrance. Upon sensing, the system will activate outside lights and provide an audio alert signal. The system can be installed reportedly in less than four hours time. A low voltage probe is buried next to the driveway (pavement or roadway is not disturbed), and the electronics can be placed inside the premises, garage, house, office, or commercial area. The Cartell is suitable for residential applications, parking lots, drive-in windows, vehicle counting, traffic control, cemeteries, used car lots, service stations, etc. Vehicles and trucks leaving a protected premises will also activate it, thus increasing effectiveness for truck terminal applications. It is stated that a system can be purchased and installed for less than \$350.

"Z" Meter

Circle No. 137 on Reader Inquiry Card

Sencore has just introduced a unique digital, inductance/capacitance meter. The Model LC53 measures capacitor values from 1 pico farad to 200,000 microfarads and inductance values from 1 microHenry to 10 Henrys, checks



capacitor leakage and dielectric absorption, and checks inductor "Q" by means of Sencore's ringing test. The LC53 is stated to be accurate to 1% on capacitance and 2% on inductance (plus a resolution error of plus or minus 2 counts on the third significant digit) and is auto ranging. Special provision is made for testing yokes and flybacks. The price is \$695; a capacitor only checker, the CA55 is priced at \$495.

Shelf Boxes

Circle No. 138 on Reader Inquiry Card

A line of fiberboard shelf bins for low cost storage and inventory of small parts is now available from *Economy Carton Company*. Called Econo-Bins, the fiberboard units come in nine different size styles ranging from 2 in. wide x 12-in. deep x 4-1/2 in. high up to 12-in. wide x 12-in. deep x 4-1/2-in. high. The



Econo-Bins are designed to fit neatly and compactly into Econo-Bin steel storage racks. Up to 100 Econo-Bins can be stored in an Econo-Bin rack 36-in. wide x 12-in. deep x 75-in. high. Quantity lot prices range from 24 to 50 cents each depending on size. Prices of complete racks with 100 bins start at \$90.00.

Temperature Tester

Circle No. 139 on Reader Inquiry Card

Universal Enterprises MT012 is a general purpose indicating pyrometer for measuring temperatures from 0° F to 1200° F. Temperature is sensed by a probe with a fast response thermocouple sensor that has a welded, shielded hot junction and attachment clip. The MT012 is suitable for testing many items including baking ovens,



grills, fryers, process ovens, dryers and for measuring stack temperatures. Optional 4 foot disposable temperature probe, stock No. ATT7, is available for testing self cleaning ovens. It is housed in a compact ($10 \times 7\frac{1}{2} \times 3\frac{1}{2}$ in.), hinged polyethylene case, and is covered by a one year warranty. Other features include color coded five way binding posts and a 4 inch meter with bold easy to read numerals on the scale plate. Complete with 4 foot temperature probe and instructions, the suggested trade price of the MT012 is \$31.95. It is also available with a centrigrade scale, stock No. MT012C.

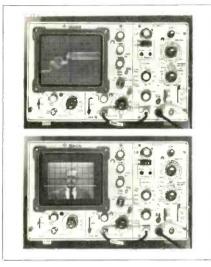
Desoldering Tool Circle No. 140 on Reader Inquiry Card



A desoldering tool that is refillable is now available from *Tech-Wick Tool*. The hand-held heat resistant plastic tool has a see-through plastic cap that snaps off for reloading. The stranded wick is available in three sizes: round .040, flat 5/64 width and flat 1/16 width. Each refill contains approximately 20 feet of pure copper stranded wick. The Tech-Wick Tool sells for \$7.50, which includes a TWT Tool, plus one refill (approximately 20 feet of wick) in any of the three sizes. The refills are \$4.50 each.

Portable Video Monitoring Scope

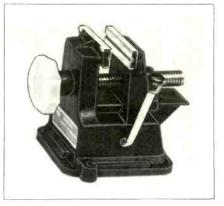
Circle No. 141 on Reader Inquiry Card A new video monitoring oscilloscope, the *Gould* OS3350, combines the functions of a TV waveform monitor and a conventional 40MHz, dual trace oscilloscope in a single portable instrument. It has been developed for use in testing and servicing commercial TV, cable TV, closed circuit TV, Telefax and video recording/playback equipment including home systems. It is stated that a special timebase generator in the new scope



provides comprehensive video triggering facilities which enable it to be used for both detailed line-by-line examination of 525-line TV waveforms and the viewing of complete pictures on its 8 x 10 cm CRT. (A 625-line version of the scope is also available.) The OS3350 accepts a standard 1-volt composite video input signal with or without "sound-in-sync" pulses and provides any of six triggering modes: vertical field 1; vertical field 2; vertical field 1 and 2 alternating: horizontal line repetitive; single horizontal line with line number indicated on a 3-digit LED display; and selection of individual line pairs specified for Telefax data. Triggering can be delayed continuously by up to 90 micro-seconds via a multiturn pot, which allows the signal to be examined in detail. When the instrument is used to display a TV picture, the line and field selected are displayed on the digital "up-down" counter. This corresponds with an electronic cursor on the picture, enabling waveforms to be closely related to their positions. In conventional operation the OS3350 functions as a general purpose 40MHz 5mV/cm dualtrace scope with single timebase control. The Gould OS3350 Video Monitoring Oscilloscope is priced at \$3500.

Light Duty Vise

Circle No. 142 on Reader Inquiry Card



The new Model VV-1 from O.K. Machine and Tool Corporation is a vacuum based light duty vise for holding small components and assemblies. Of ABS construction, it has 1½ in. wide jaws with 1¼ in. travel and an oversized knob for positioning. It also features screw lugs for permanent mounting. The price is \$3.49.





Circle No. 115 on Reader Inquiry Card

Low-Distortion Oscillator Circle No. 143 on Reader Inquiry Card

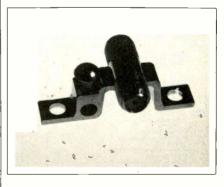


The new Krohn-Hite Model 4200A is a sine wave oscillator that can deliver a stated ½ watt of power output at less than 0.1% distortion over most of its 10Hz to 10 MHz operatig range. Its frequency response is reportedly flat within 0.025dB over most of this range. Maximum output voltage is 10V RMS open circuit, controllable in 10dB steps by a pushbutton attenuator and a separate vernier. Long term frequency stability is better than 0.02%. A fixed 1 volt output is available for synchronizing or as an auxiliary output. The price is \$550.

Grounding Block

Circle No. 144 on Reader Inquiry Card

AVA Electronics, manufacturer of cable assemblies, RF coaxial adaptors and connectors for the CATV, MATV and CB markets, announces a new Grounding Block designated No. GB 570 A. The GB 570 A is said to be the most economical of static grounding blocks for CATV and MATV usage. It is simple to install and has female "F" connectors built in to each end of the barrel. The grounding block is die-cast zinc, nickel plated, for weather resistance.



Dual Trace Miniscope

Circle No. 145 on Reader Inquiry Card

Non-Linear Systems has recently introduced its Model MS-230 30MHz, battery operated, Dual Trace Miniscope. Package size is 2.9 inches high by 6.4

The New RCA Unitized Chassis Field Service Handbook

RIGHT ON

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Color Television Field Service Handbook

Xtended Life Unitized Chassis Series

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Shop owners report in-home set servicing beats the profit squeeze by reducing time and travel expenses.

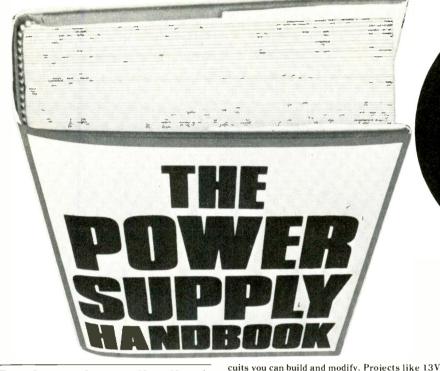
RCA's new Field Service Handbook shows you how to quickly and simply diagnose the CTC 87, 88, 93, and 97 chassis. Step-by-step troubleshooting with a volt ohm meter in the home. Symptoms are traced to their cause with easyto-read illustrations. Included are recommended component replacement procedures. Handy, loose-leaf binder (86 pages) stays open to the page you need while you work. Only \$8.50 each.

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Circle No. 112 on Reader Inquiry Card

polarity changers, 12V to 300V converters, solid-state car alternator/regulators, silver-zinc cell battery chargers, zero to 30V lab supplies, simple four-voltage bench supplies, and many more. The projects come with all the data you need to insure flawless no-hitch constructionconcise analyses of special circuits, easy-tofollow directions, detailed schematic diagrams, complete parts lists, and special discussions of construction safety precautions.

The scope of this handbook is broad-broad enough to include construction info on tested circuits that'll help you make the most of any power supply you put together-circuits that'll allow you to interface, modify, and test your own PS designs. The authors show you how to construct voltage splitters, IC protection circuits, smoke testers, two-terminal current limiters, voltage limit sensors, active voltage dividers, microfarad multipliers, capacitor rejuvenator-leakage testers, and many, many others. 420 pps., 292 illus. Hardbound, List \$12.95.

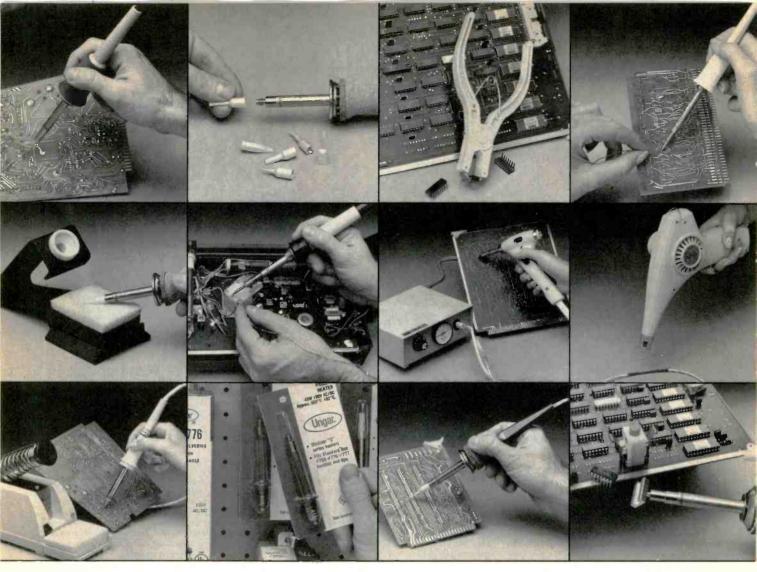
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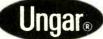


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Circle No. 130 on Reader Inquiry Card

The Only Thing We Don't Make Is The Solder.

is stated to be 3.5 lb, including batteries. The MS-230 features alternate, chopped and separate sweep modes. Internal and external trigger modes are included. There are 12 vertical gain settings for each channel's range from 0.01 to 50 volts per division. Timebase settings number 21 from 0.05msec to 0.2 seconds per division. Verniers are provided for timebase and vertical amplifier adjustment. The MS-230 Miniscope includes a horizontal input channel and an internal calibrator. The graticule consists of .25 inch divisions arranged 5 across and 4 high. The MS-230 comes complete with input cables and a battery charger permitting battery or line operation. Accessories include a 10:1, 10 megohm probe and a leather carrying case with shoulder strap and belt loop. The price is \$559.



Security Timer

Circle No. 146 on Reader Inquiry Card

A new security timer from *A. M. Corporation* can turn lamps or radios on and off automatically at random intervals of 3 to 25 minutes, to give the impression of continuous activity inside a home or business. There is no predictable off/on pattern as with some security timers. The price is \$19.95.



Shutter Multi-Test Circle No. 147 on Reader Inquiry Card

National Camera, Inc., has recently introduced a shutter speed test instrument which simultaneously displays five digital readouts of information on focalplane shutters. It shows leading and trailing contain times, and exposure at the lead edge, center and trail edge of the aperture. While it was designed for testing focal plane shutters, it also tests leaf-type shutters and flash synchronization. The Multi-Test includes a special light source and a 35mm format adapter containing three photo transistors which measure light at different points of the aperture.

ACOUSTIC WAVES

continued from page 25

commercial communications and radar systems. The time has come for large-scale uses of the SAW filters in consumer electronics, particularly in television receivers.

Use of the SAW filter in a TV IF section can eliminate all or most of the conventional IF tuned circuits. The SAW filter has good transient response, good stability and high massreproducibility. The future will see a further refinement of the device and an extension of its uses in many different circuits found in television receivers and other consumer products. ET/D

DATA CONVERTERS

continued from page 28

pulse received.

6. When E_A is zero, the comparator output drops LOW, turning off the counter. The binary output of the counter at this instant represents the average value of E_{in} during t1 t_o.

The conversion time for fullscale signals is theoretically the same as for the ramp type ADC, namely 2ⁿ clock pulses. But the typical dual slope circuit is limited to slower clock speeds by the time constant (R1C1) of the integrator.

None of the ADC circuits presented thus far is sensitive to errors in clock frequency. If the short term stability (i.e. over one conversion cycle) is good, then the count will accurately reflect the analog input value. **ET**D

SUMMER CES

continued from page 20

the future."

Highlights of this system are 2,048 upper and lower case characters, 16 colors, sound output and a digital to analog converter for voice and music generation, plus the software library of entertainment, education, and personal finance.

However, also included are two 8-inch floppy (storage) discs which allows the C8P to store pertinent information for use as a home controller "on-line." Through an AC interface the computer system can inject control signals on the AC power lines of a home which control remote switches for appliance and heat control. Also, when interfaced with a wireless home security system, such as smoke detectors, door contact switches, auto burglar alarms, etc., the computer can dial police or fire department numbers and speak to them to report an incident. ET/D

PULSES

continued from page 32

TV IF strip. . . so you may as well get used to dealing with the interconnection problem. As a matter of fact, if you examine the wiring on some high frequency digital computer printed circuit boards, you will notice that the width of the signal path pattern is much wider than the signal current requires. If you look at the underside of the board, you will see a ground plane directly under the signal path pattern. This forms a sort of coaxial transmission line, with the PC board itself the insulation. . . and the signal paths are all terminated at both ends in their characteristic impedance in order to prevent reflections and consequent pulse distortions. ET/D

DIGITAL IV

continued from page 36

- 4. Clock the FF by pressing S6 slowly several times.
- 5. Did anything change on L3/L4? It shouldn't.
- 6. Set J HIGH and K LOW
- 7. Clock the FF by pressing S6 slowly several times
- 8. Note that Q went HIGH on the first negative-going transition (releast of S6), but nothing else happened on subsequent clock pulses.
- 9. Set S1 S4 HIGH
- Set FF (S3 LOW momentarily). Q should be HIGH (L3 on) and not-Q LOW (L4 off).
- 11. Set K LOW
- 12. Clock the FF by pressing S6 slowly several times.
- 13. Set K HIGH and J LOW.
- 14. Clock the FF by pressing S6 slowly several times.
- 15. Note Q/not-Q (L3/L4) changes, and compare with step 8. Note the differences. **ET/D**



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TECH BENCH kit or plans. Designed for the TV/Radio Tech. Test instrument shelf on two power columns with 10 fused outlets. Bench has four fused outlets with C-MOS grounding, four large tool drawers and neon bench lighting. E-Z build construction. Plans and kit information \$1.98 plus 50¢ handling. Technical Workshop, Box 368, Placentia, CA 92670. 8/79

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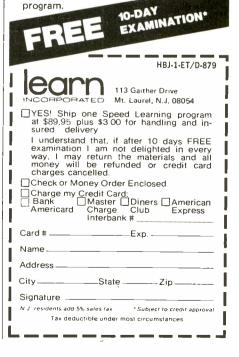
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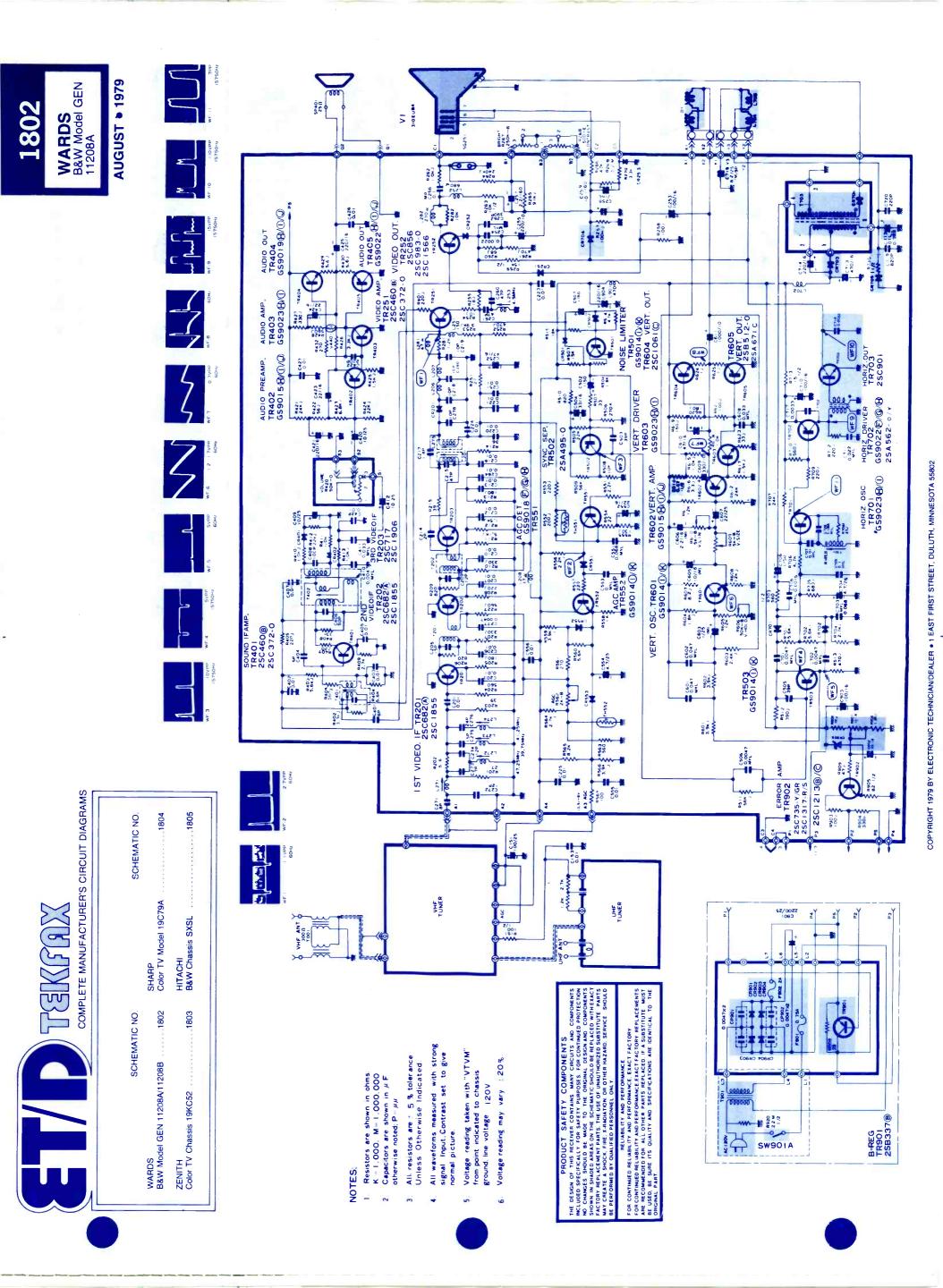
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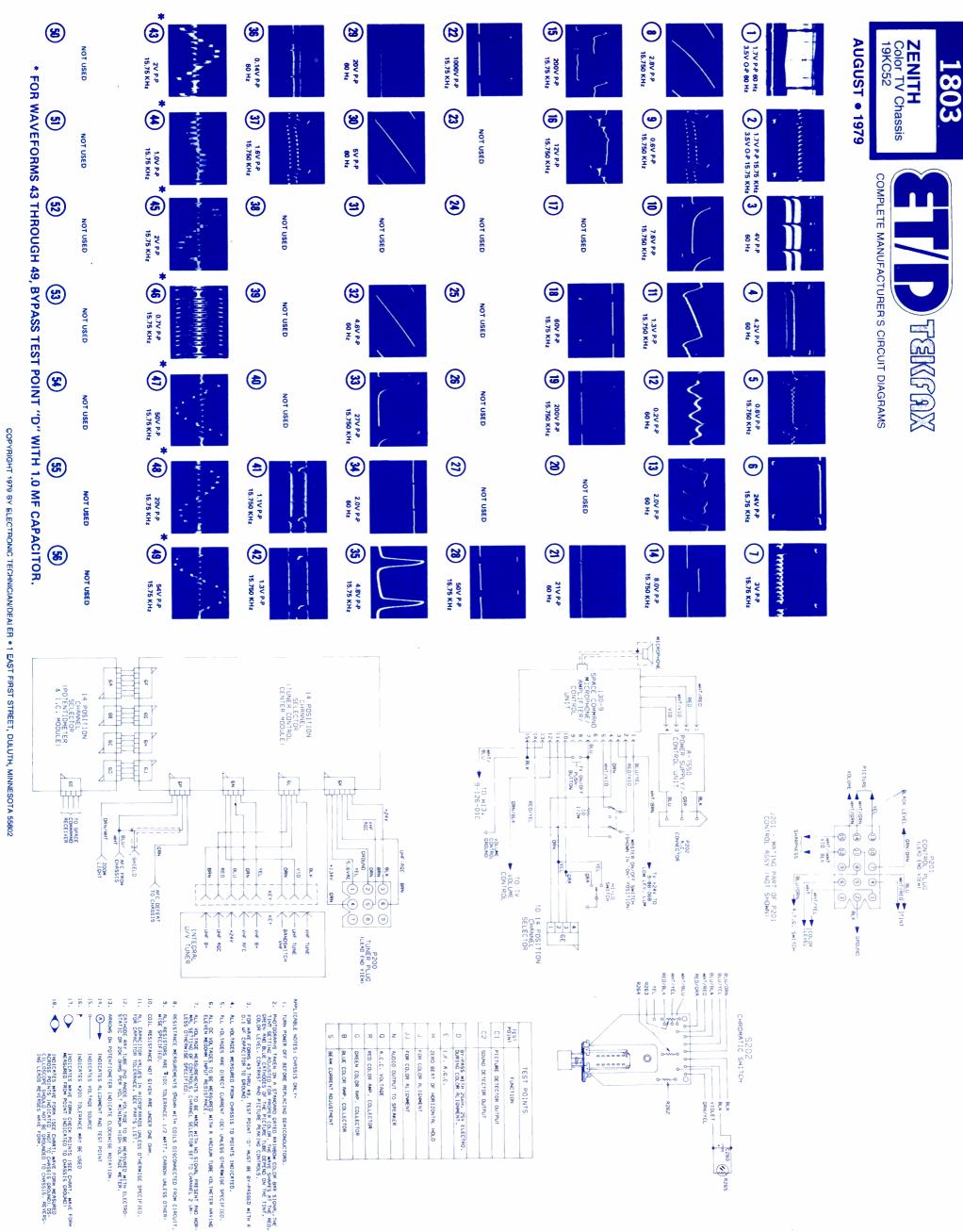
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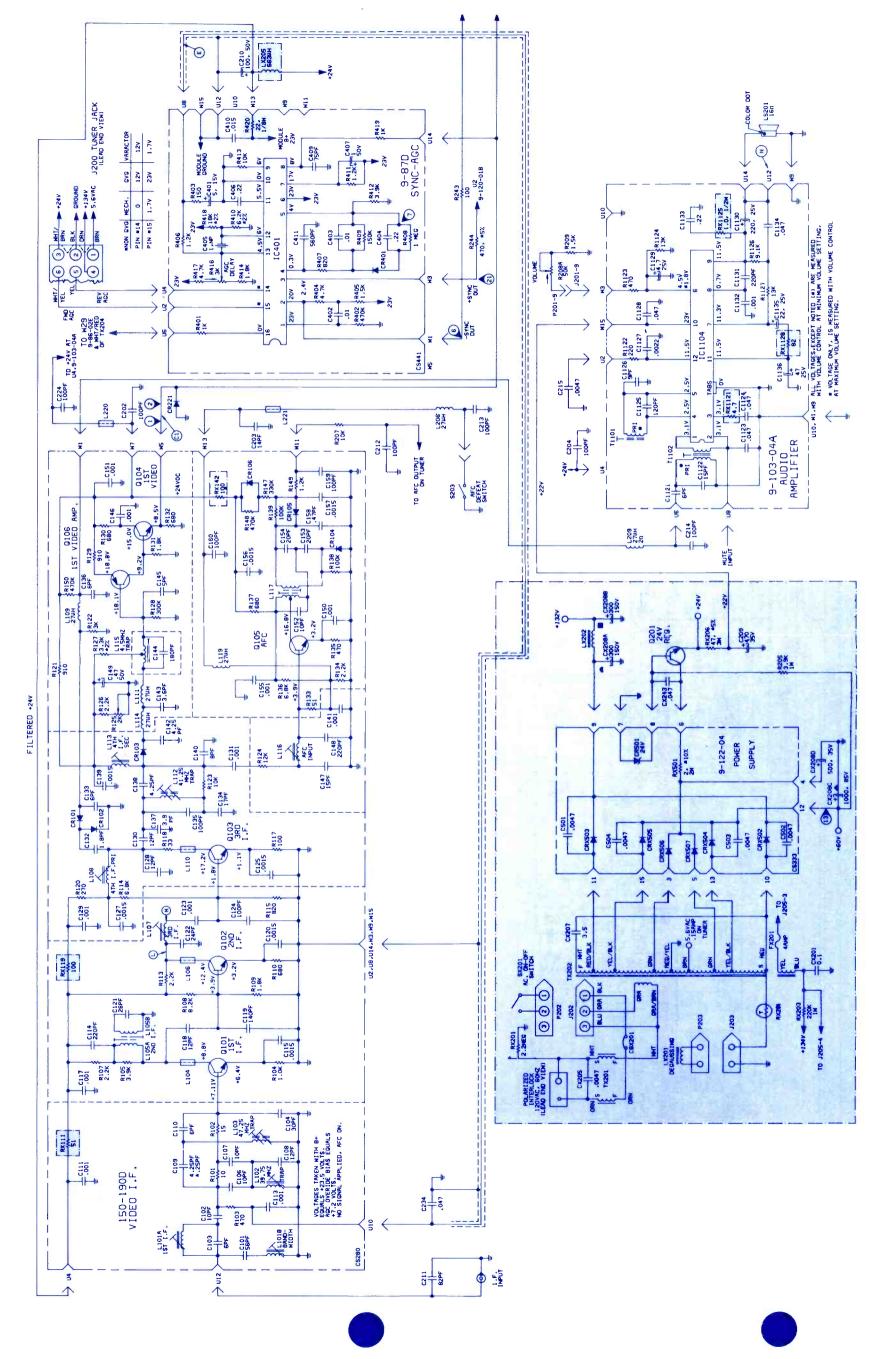


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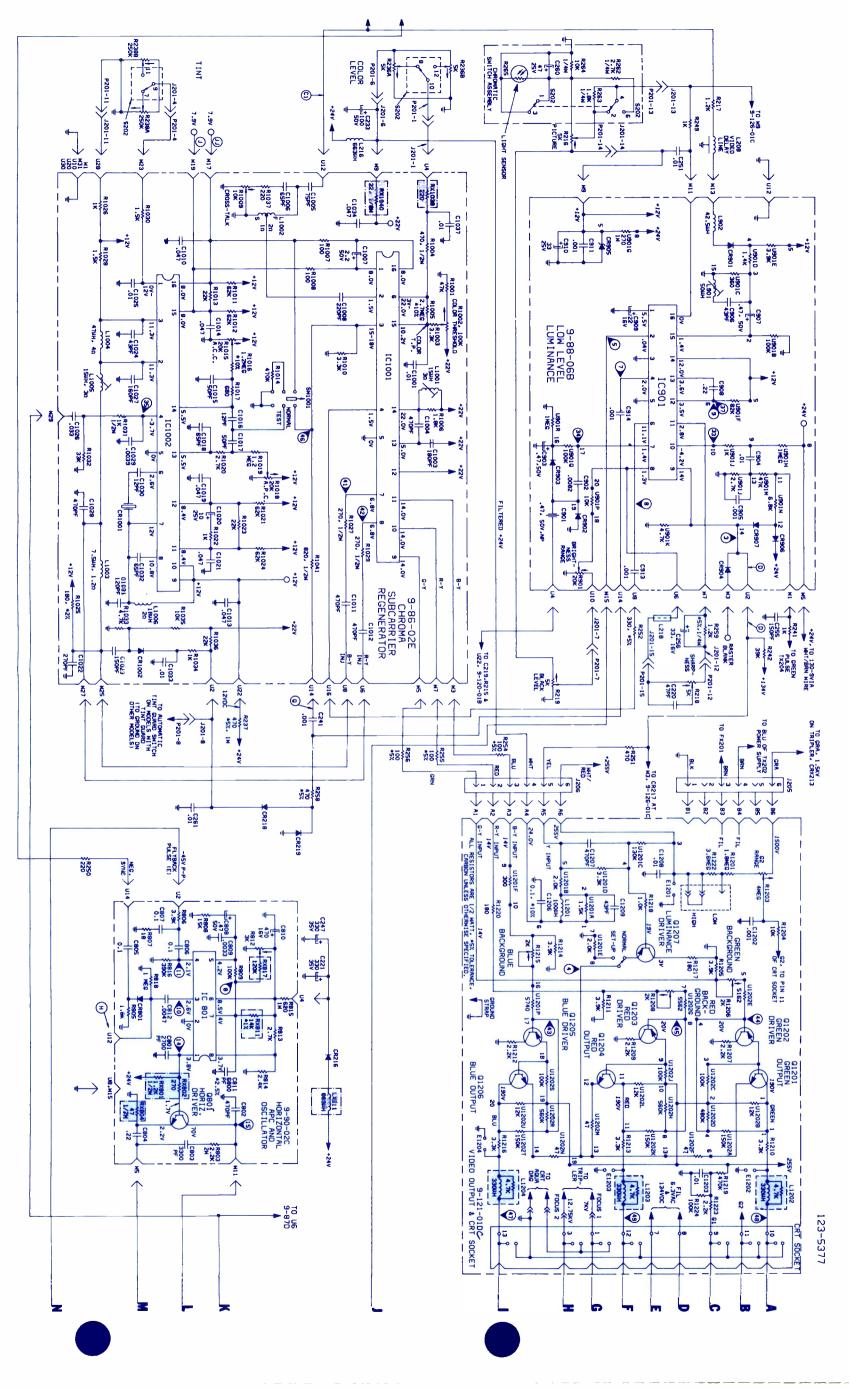
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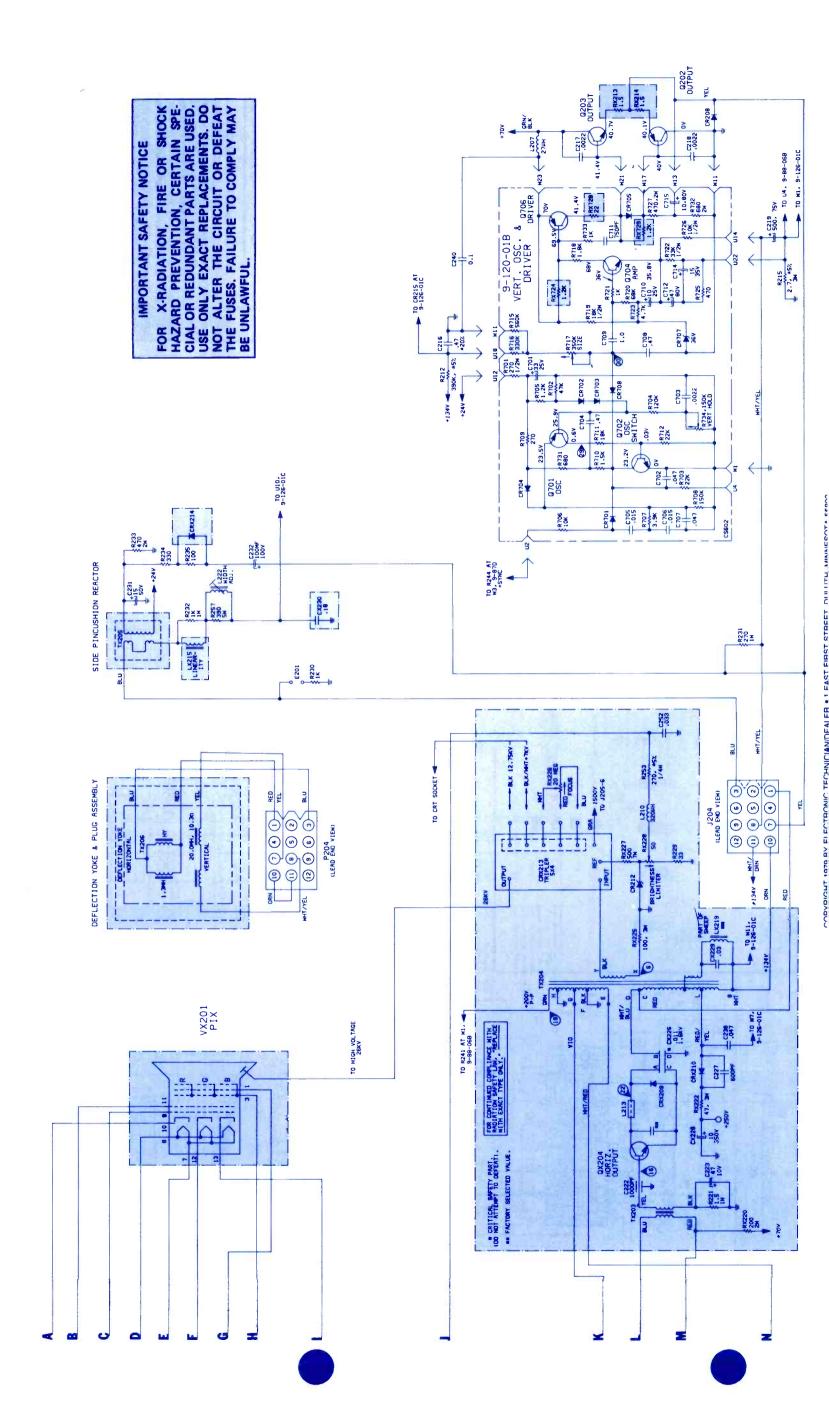
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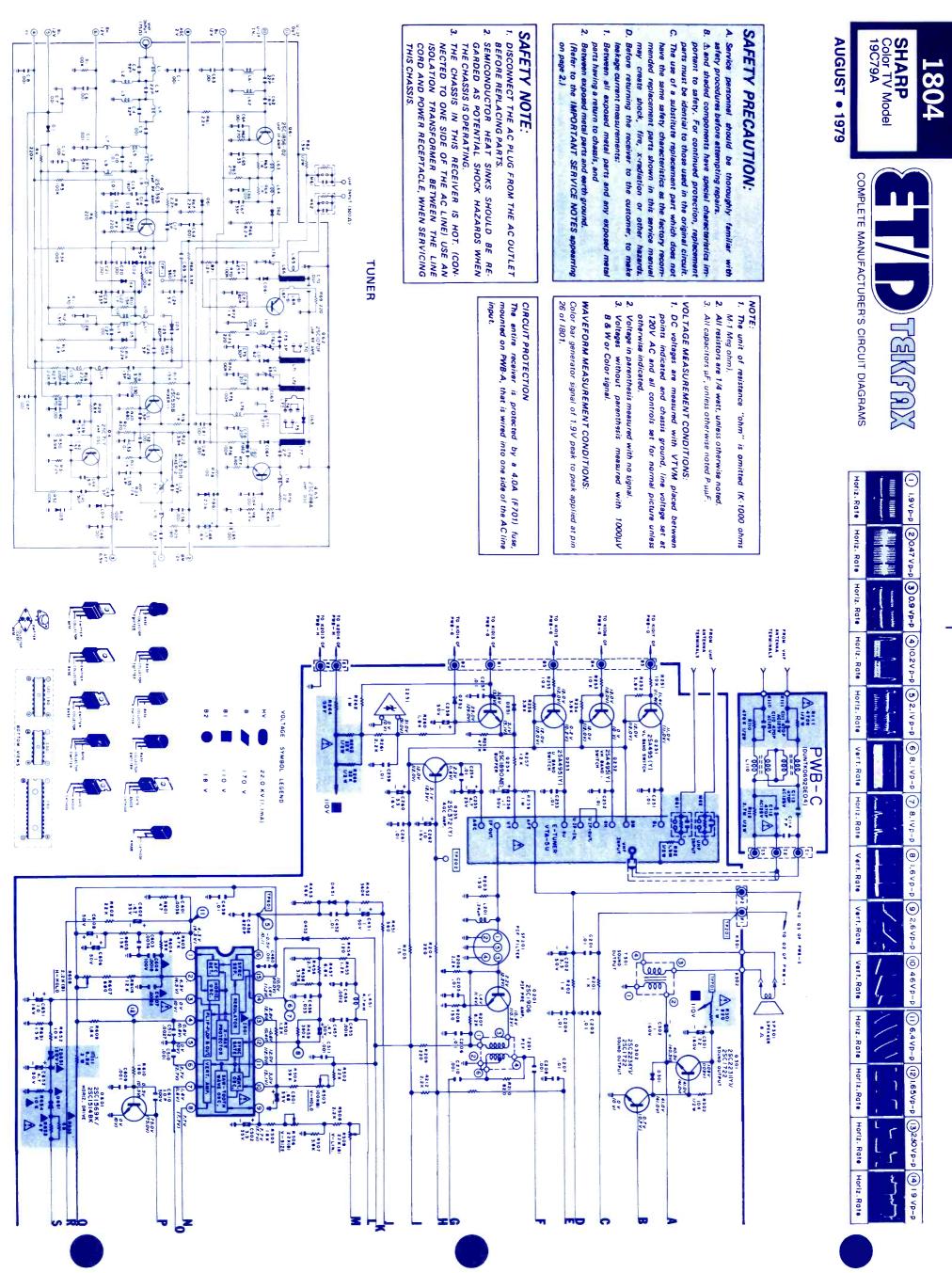


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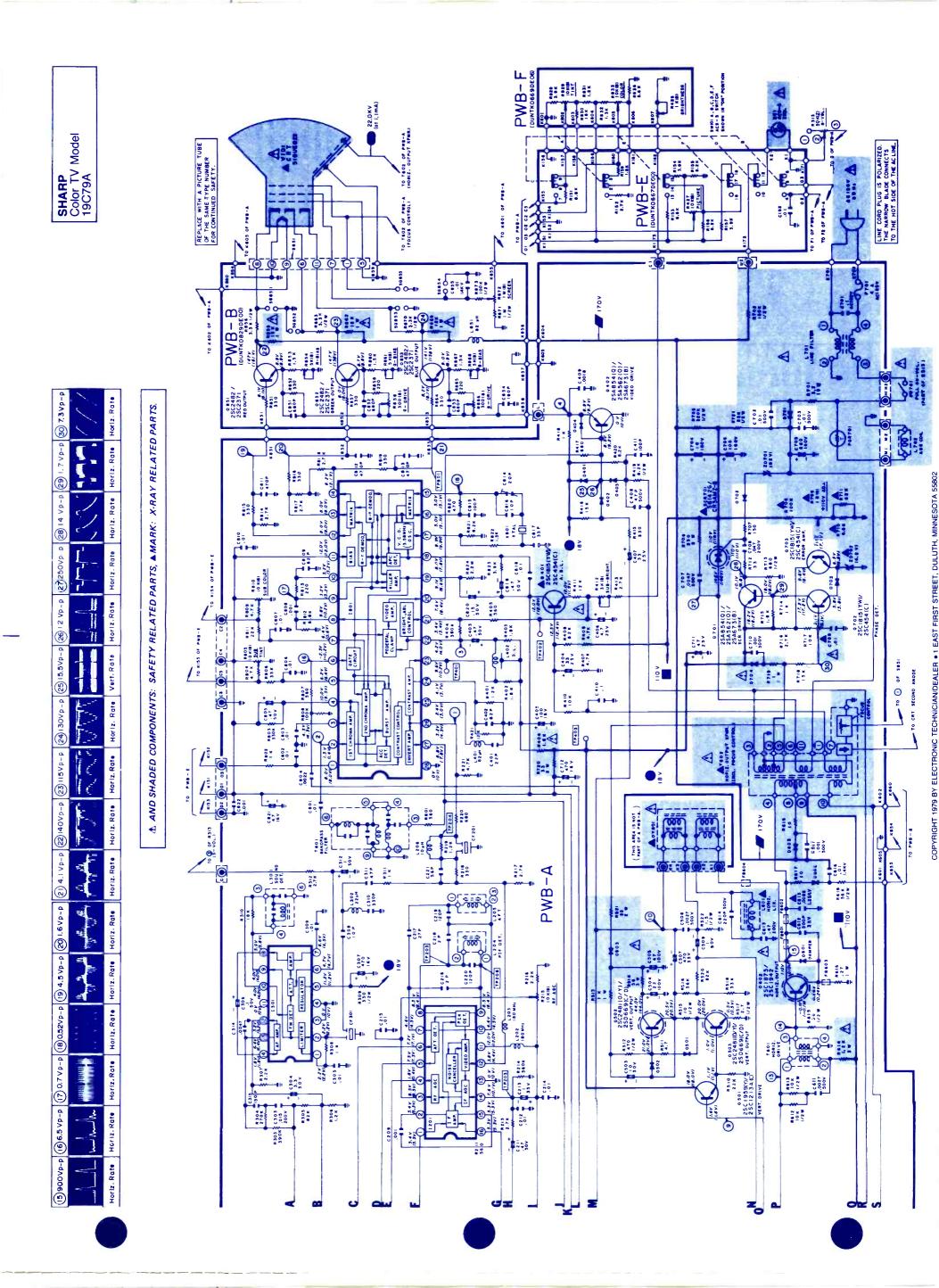
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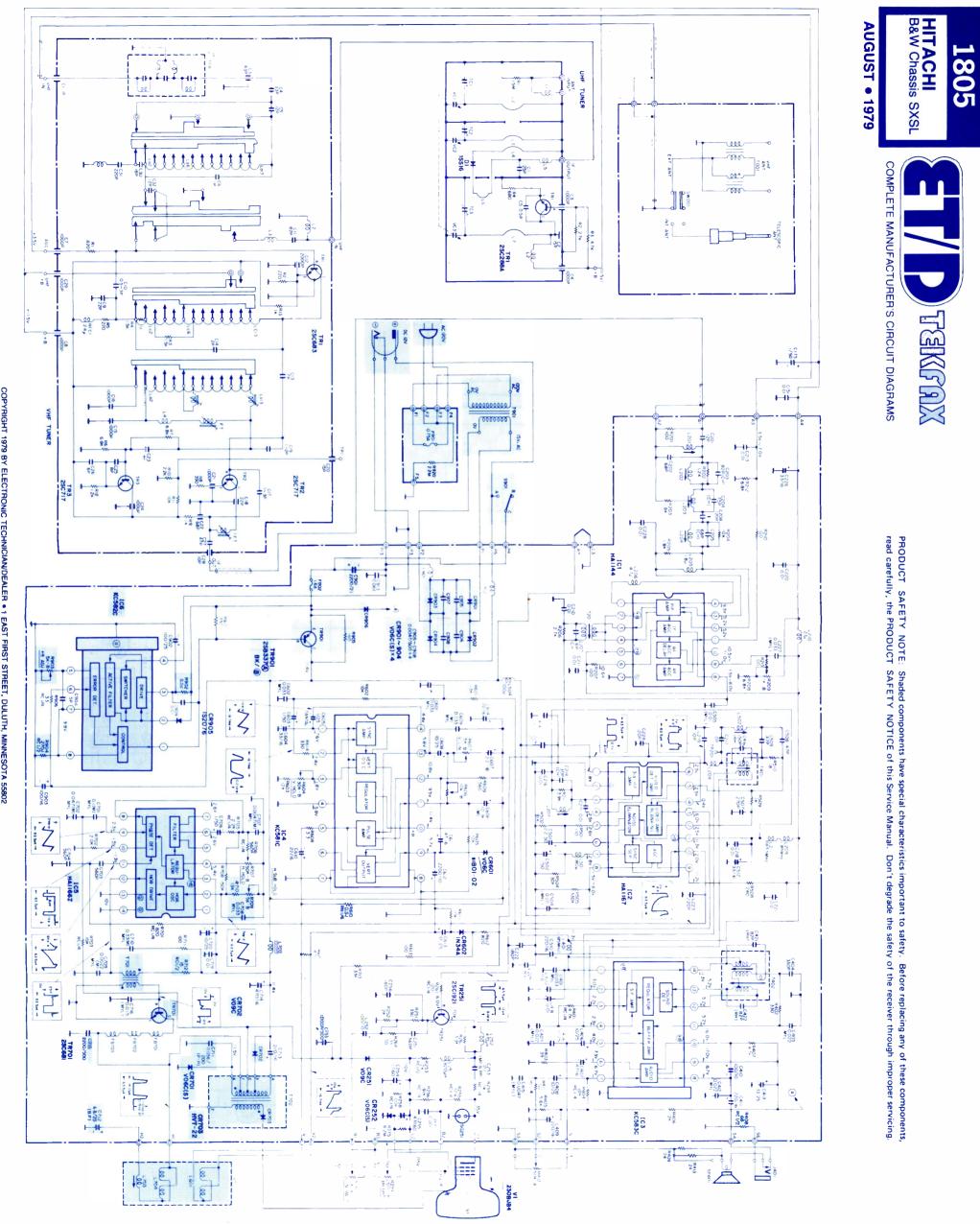




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