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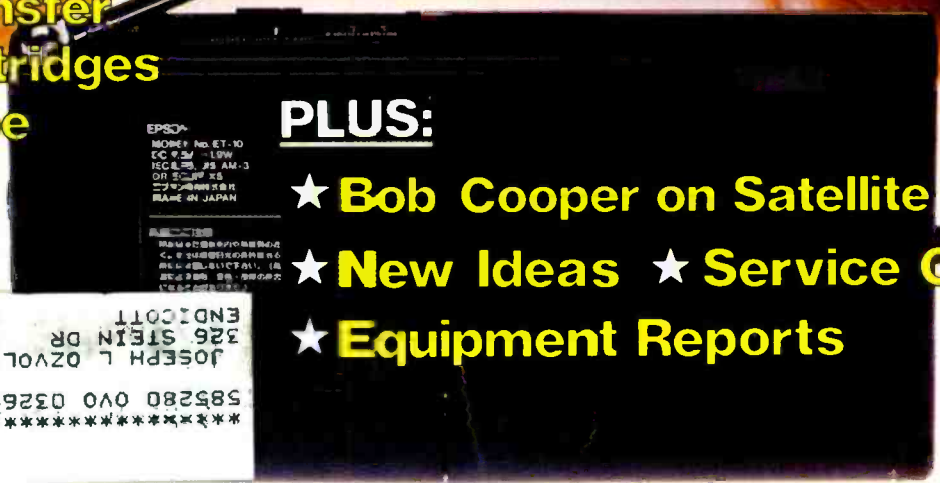
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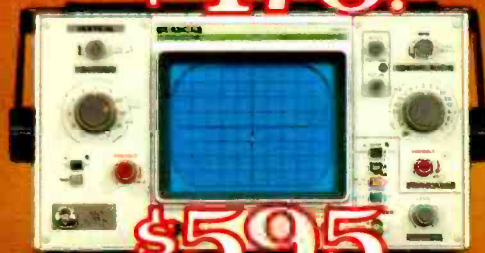
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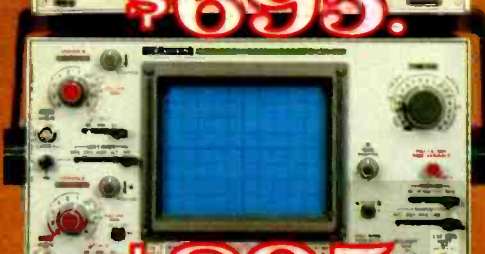
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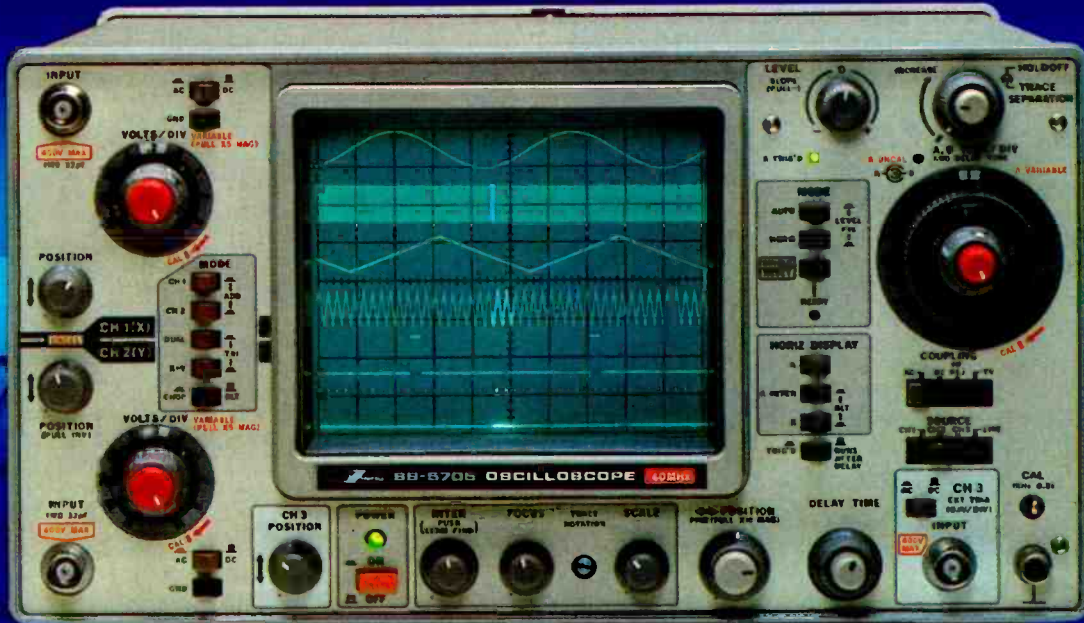
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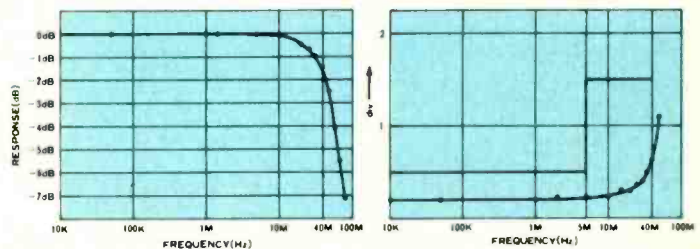
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NEW!

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Bearcat®

Products

Communications Electronics,™ the world's largest distributor of radio scanners, is pleased to announce that Bearcat brand scanner radios have been acquired by Uniden Corporation of America. Because of this acquisition, Communications Electronics will now carry the complete line of Uniden Bearcat scanners, CB radios and Uniden Bandit™ radar detectors. To celebrate this acquisition, we have special pricing on the Uniden line of electronic products.

Bearcat® 300-E

List price \$549.95/CE price \$339.00
7-Band, 50 Channel • Service Search • No-crystal scanner • AM Aircraft and Public Service bands • Priority Channel • AC/DC Bands: 32-50, 118-136 AM, 144-174, 421-512 MHz.
 The Bearcat 300 is the most advanced automatic scanning radio that has ever been offered to the public. The Bearcat 300 uses a bright green fluorescent digital display, so it's ideal for mobile applications. The Bearcat 300 now has these added features: Service Search, Display Intensity Control, Hold Search and Resume Search keys, Separate Band keys to permit lock-in/lock-out of any band for more efficient service search.

Bearcat® 20/20-E

List price \$449.95/CE price \$269.00
7-Band, 40 Channel • Crystalless • Searches AM Aircraft and Public Service bands • AC/DC Priority Channel • Direct Channel Access • Delay Frequency range 32-50, 118-136 AM, 144-174, 420-512 MHz.
 Find an easy chair. Turn on your Bearcat 20/20 and you're in an airplane cockpit. Listening to all the air-to-ground conversations. Maybe you'll pick up an exciting search and rescue mission on the Coast Guard channel. In a flash, you're back on the ground listening as news crews report a fast breaking story. Or hearing police and fire calls in your own neighborhood, in plenty of time so you can take precautions. You can even hear ham radio transmission, business phone calls and government intelligence agencies. Without leaving your easy chair. Because you've got a Bearcat 20/20 right beside it.

The Bearcat 20/20 monitors 40 frequencies from 7 bands, including aircraft. A two-position switch, located on the front panel, allows monitoring of 20 channels at a time.

Bearcat® 210XL-E

List price \$349.95/CE price \$209.00
6-Band, 18 Channel • Crystalless • AC/DC Frequency range 32-50, 144-174, 421-512 MHz.
 The Bearcat 210XL scanning radio is the second generation scanner that replaces the popular Bearcat 210 and 211. It has almost twice the scanning capacity of the Bearcat 210 with 18 channels plus dual scanning speeds and a bright green fluorescent display. Automatic search finds new frequencies. Features scan delay, single antenna, patented track tuning and more.

Bearcat® 260-E

List price \$399.95/CE price \$249.00
8-Band, 16 Channel • Priority • AC/DC Frequency range 30-50, 138-174, 406-512 MHz.
 Keep up with police and fire calls, ham radio operators and other transmission while you're on the road with a Bearcat 260 scanner. Designed with police and fire department cooperation, its unique, practical shape and special two-position mounting bracket makes hump mounted or under dash installation possible in any vehicle. The Bearcat 260 is so ruggedly built for mobile use that it meets military standard 810c, curve y for vibration rating. Incorporated in its rugged, all metal case is a specially positioned speaker delivering 3 watts of crisp, clear audio.

NEW! Bearcat® 201-E

List price \$279.95/CE price \$179.00
9-Band, 16 Channel • Crystalless • AC only Priority • Scan Delay • One Key Weather Frequency range 30-50, 118-136 AM, 146-174, 420-512 MHz.
 The Bearcat 201 performs any scanning function you could possibly want. With push button ease, you can program up to 16 channels for automatic monitoring. Push another button and search for new frequencies. There are no crystals to limit what you want to hear.

NEW! Bearcat® 180-E

List price \$249.95/CE price \$149.00
8-Band, 16 Channel • Priority • AC only Frequency range: 30-50, 138-174, 406-512 MHz.
 Police and fire calls, Ham radio transmissions, Business and government undercover operations. You can hear it all on a Bearcat 180 scanner radio. Imagine the thrill of hearing a major news event unfold even before the news organizations can report it. And the security of knowing what's happening in your neighborhood by hearing police and fire calls in time to take precautions. There's nothing like scanning to keep you in-the-know, and no better way to get scanner radio performance at a value price than with the Bearcat 180.

Bearcat® 100-E

The first no-crystal programmable handheld scanner.
 List price \$449.95/CE price \$234.00/SPECIAL!
8-Band, 16 Channel • Liquid Crystal Display Search • Limit • Hold • Lockout • AC/DC Frequency range: 30-50, 138-174, 406-512 MHz.
 The world's first no-crystal handheld scanner has compressed into a 3" x 7" x 1 1/4" case more scanning power than is found in many base or mobile scanners. The Bearcat 100 has a full 16 channels with frequency coverage that includes all public service bands (Low, High, UHF and "T" bands), the 2-Meter and 70 cm. Amateur bands, plus Military and Federal Government frequencies. It has chrome-plated keys for functions that are user controlled, such as lockout, manual and automatic scan. Even search is provided, both manual and automatic. Wow...what a scanner!

The Bearcat 100 produces audio power output of 300 milliwatts, is track-tuned and has selectivity of better than 50 dB and sensitivity of 0.6 microvolts on VHF and 1.0 microvolts on UHF. Power consumption is kept extremely low by using a liquid crystal display and exclusive low power integrated circuits.

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Bearcat® DX1000-E

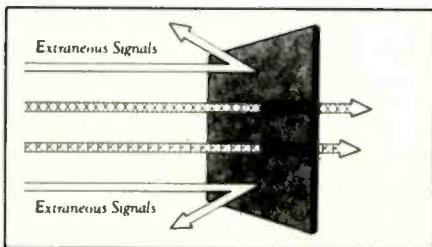
List price \$649.95/CE price \$489.00
Frequency range 10 kHz to 30 MHz.
 The Bearcat DX1000 shortwave radio makes tuning in London as easy as dialing a phone. It features PLL synthesized accuracy, two time zone 24-hour digital quartz clock and a built-in timer to wake you to your favorite shortwave station. It can be programmed to activate peripheral equipment like a tape recorder to record up to five different broadcasts, any frequency, any mode, while you are asleep or at work. It will receive AM, LSB, USB, CW and FM broadcasts.
 There's never been an easier way to hear what the world has to say. With the Bearcat DX1000 shortwave receiver, you now have direct access to the world.

Uniden® PC22-E

List price \$159.95/CE price \$99.00
 The Uniden PC22 is a 40 channel AM remote mobile CB radio. It's the answer for today's smaller cars which don't always provide adequate space for mounting. Since all the controls are on the microphone, you can stash the "guts" in the trunk. The microphone has up/down channel selector, digital display, TX/RX Indicator and external speaker jack. Dimensions: 5 3/4" W x 7 7/8" D x 1 1/2" H. 13.8 VDC, positive or negative ground.

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Both Bandit™ radar detectors feature E.D.I.T.™ the Electronic Data Interference Terminator that edits-out false alarm signals.

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Uniden® PC33-E

List price \$59.95/CE price \$44.00
 The Uniden PC33 boasts a super-compact case and front-panel mike connector to fit comfortably in today's smaller cars. Controls: Power & Volume, Squelch, Switches: ANL. Other features of the PC33 include Graduated LED "S"/RF Meter, Digital channel indicator. Dimensions: 6" W x 6" D x 1 1/4" H. ±13.8 VDC.

Uniden® PC55-E

List price \$89.95/CE price \$59.00
 The full featured Uniden PC55 front-panel mike connector makes installation easier when space is a factor. It has ANL, PA-CB, Channel 9 and RF Gain switches. LED "S"/RF Meter, TX lite, PA & external speaker jacks. Dimensions: 6" W x 6" D x 1 1/4" H. ±13.8 VDC.

Bandit™ Radar Detectors

Now that everyone else has taken their best shot at radar detection, the Uniden Bandit™ has done them one better...with E.D.I.T.™, the Electronic Data Interference Terminator that actually edits-out false alarm signals.

The Bandit 55, features a convenient brightness/dimmer control for comfortable day or night driving, plus a handy highway/city control for maximum flexibility wherever you drive. The Bandit 95 Remote, is a two-piece modular unit that lets you mount the long-range radar antenna behind the grill, out of view. The ultra-compact control unit can then be inconspicuously tucked under the dash or clipped to the visor. Order Bandit 55-E for \$119.00 each or the Bandit 95-E Remote for \$139.00 each.

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DECEMBER 84

**Radio-
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Vol. 55 No. 12

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*The editors and staff
of Radio-Electronics
join in sending
holiday greetings and
our best wishes for
a happy new year*

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COVER 1



Flat-panel color TV's have been promised for many years, but before an appropriate display for those sets could be produced, major technical problems needed to be resolved. Epson has resolved many of those problems, and the results of its efforts—a tiny pocket-sized TV—should be available soon. This month we'll look at that tiny TV, the flat-panel LCD display that it uses, and the technology that makes both possible. The story, which is part of our special video-entertainment section, begins on page 57.

NEXT MONTH

ON SALE DECEMBER 20

VERSATILE VIDEO SWITCHER

Build this project and end your video-switching problems forever.

ALL ABOUT THERMISTORS

A look at those valuable components and how to use them.

ALL ABOUT VOLTAGE COMPARATORS

Learn about voltage comparators, including window comparators, and their applications.

ATARI GAME RECORDER

More on a device that lets you store your library of games for the 2600 on cassette tape!

AND LOTS MORE!

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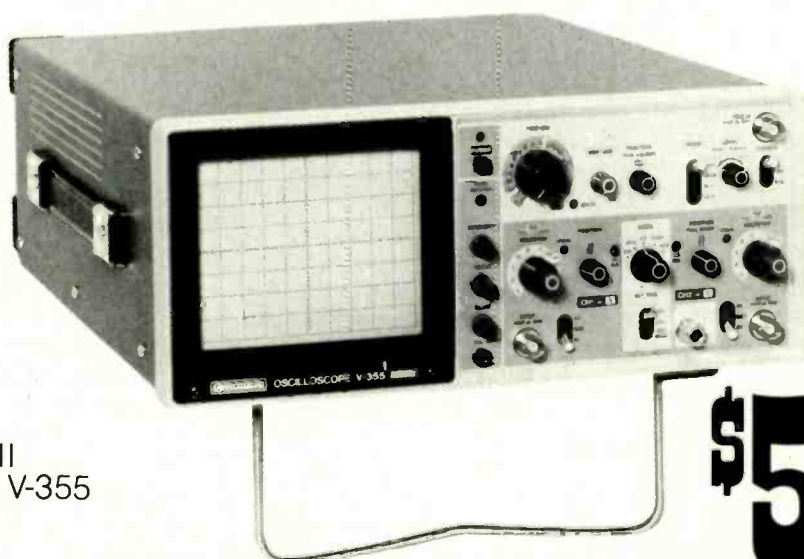
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Advertising Sales Offices listed on page 30.

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WHAT'S NEWS

New "computerized home" uses TV, house wiring

General Electric has developed what may be an important step toward the fully automated home—a new electronic home-control system that uses the family television set and the electric wiring of the house to achieve its results.

The *HomeMinder* can virtually run the modern household: adjust temperatures, dim lights, turn appliances on at specific times, store messages, and display important dates and appointments. It provides in-home remote control, control away from home, and a memory that remembers things the user might forget.

The new "home controller" works through the house wiring, and TV screen visuals guide the user step by step. It will come in

two versions—a unit that connects to the back of any TV set, or as a feature built into a 25-inch GE component television set.

The TV screen acts as a display, showing each room of the house, with numbered "menus" of lights and appliances, selectable by the remote control. The screen also displays simple instructions, as well as questions when the user seems unsure of the next step. Special modules tie appliances, overhead and outside lights, and the thermostat into the system via the existing house wiring.

The *HomeMinder* is expected to retail for about \$500, depending on the number of modules required. Modules range from \$20 to \$40 each.

Radar detector makers organize against ban

Three of the country's leading radar detector manufacturers have formed RADAR (Radio Association Defending Airwave Rights) dedicated to keeping the sale and use of radar detectors legal in all 50 states. They invite other manufacturers to join them.

Since 1962, at least 40 states have tried (unsuccessfully) to pass legislation to make radar detectors illegal. In its short existence (it was founded in February 1984), RADAR has been instrumental in squelching at least twelve such attempts.

RADAR's defense is based on the fact that any state legislation prohibiting radar detectors is already preempted by Congressional mandate; the fact that police radar's capricious fallibility has been established, and the claim that a radar-detector ban would violate citizens' rights.

National Semiconductor breaks ground for lab

Construction has begun on a new \$75 million National Semiconductor Corp. research and development center, in Santa Clara, CA. It will employ more than 500 people, and will be completed in the spring of 1985.

The research portion of the center will be devoted primarily to two advanced technology thrusts: CMOS and high-density bipolar processes. CMOS provides high speeds while consuming low power at a high level of reliability. High-density bipolar technology is being applied to classical logic applications and to VLSI products. Among those are microprocessor peripherals, hard-disk circuits, and local-area networks.

continued on page 8



MODULES THAT MAKE THE *HOMEMINDER* WORK. The ApplianceMinder (left top) and LampMinder (next right) connect any lamp or appliance to the system. The Light Switch module (right) installs like a dimmer switch and connects indoor or outdoor lights to the *HomeMinder*. The Temperature Minder module (second from right) is attached under the existing thermostat and regulates heating and air conditioning. It connects to the power supply module beneath it. The MiniMinder remote control (lower left) can operate up to eight lights and appliances from any electric outlet in the home.

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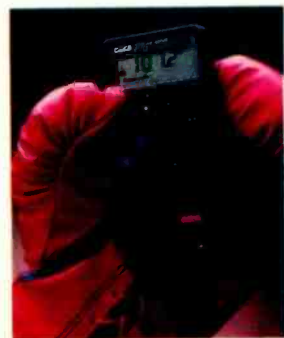
You also get the extra resolution of a 3200-count LCD display, plus a responsive analog bar graph for quick visual checks of continuity, peaking, nulling and trends.

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2000+ hour battery life
3-year warranty

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Audible continuity
Autorange/range hold
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\$129*
Analog/digital display
Volts, ohms, 10A, mA, diode test
Audible continuity
"Touch Hold" function
Autorange/range hold
0.3% basic dc accuracy
2000+ hour battery life
3-year warranty
Multipurpose holster

* Suggested U.S. list price, effective July 1, 1984.

** Patent pending.



WHAT'S NEWS

continued from page 6

Joint effort to end illegal phone use

An ITT Corp. task force, the Federal Bureau of Investigation (FBI), and other law enforcement agencies are engaged in a major crackdown on illegal users of the ITT Longer Distance telephone service. That service is provided to residential and business customers in 113 major metropolitan areas. To place a call on the system, customers dial a special access code, then the telephone number, and finally a confidential authorization code, which bills the call to the customer's account.

The perpetrators have been placing phone calls illegally by using authorization codes assigned to ITT customers. In one such case, an FBI investigation led to the indictment of a former ITT employee, Oliver Benner, who was charged with selling ITT's confidential authorization codes.

The indictment charges that Benner supplied the codes to a New Jersey company, which used them in a nationwide campaign to sell its products through its large telephone sales force. If convicted on all charges, Mr. Benner could be sentenced to 40 years in prison and fined up to \$17,000.

Solid-state TV camera makes better pictures

A color camera using three charge-coupled devices (CCD's) instead of camera tubes has been introduced by RCA. The new camera, intended especially for news and sports coverage, can see much greater detail in rapidly moving objects and performs over a wider range of lighting conditions than tube-type cameras.

The new camera eliminates red streaks or "comet tails" behind

rapidly moving lights, or "streaking" behind a fast-moving baseball. It can produce clear images in dark shadows while simultaneously handling bright lights in the same scene.

The CCD's in the new camera have 403 horizontal and 512 vertical picture elements. Under well-lit conditions, with little or no motion, resolution of the CCD and the $\frac{2}{3}$ -inch tube camera is about the same. In low light or rapid action, the CCD is markedly better.

The camera is immune to magnetic fields and acoustic interference, and is exceptionally capable of handling bright highlights.

New message service to minimize costs

A new communications service, which is expected to make it possible for small businesses to send and receive international messages for a small fraction of the cost of Telex or similar services, has been initiated by Service Systems Technology (SST) of Marina del Rey, CA and Milan, Italy.

Known as TINA International Message Service, the new system has one limitation as compared with Telex or similar services: Communication is between subscribers in U.S. or foreign "gateway cities," or more specifically, from the computer of a subscriber to the computer at his other "electronic mailbox." (There are 13 gateway cities in California, 9 in New Jersey.)

A subscriber dials a local number to get on an international network, then sends his message through a modem attached to his telephone. The network is that of INFONET, which has offices worldwide.

Cost of the service, which includes two "electronic mailboxes" and two hours of computer time, is \$99.60 per month. That charge, says SST, gives subscribers the amount of service that would cost about \$2200 by conventional services. Extra computer connect time is obtainable at \$58.60 per hour. Extra electronic mailboxes and user I.D.'s are \$10 per month.

New company to operate Landsat satellites?

The new Earth Observation Satellite Co. (EOSAT) has submitted to the Department of Commerce a proposal to operate the network of satellites now being managed by the Department's Oceanic and Atmospheric Administration (NOAA). It would also be responsible for designing, fabricating, and launching additional Landsat satellites. The new corporation is a joint venture of Hughes Aircraft Co. and RCA Corp.

The proposal calls for a 12-year program to operate the existing facilities at NASA's Goddard Space Flight Center, and to build and launch four satellites, each with advanced instrumentation and a five-year design life.

The satellites view the world with high-resolution sensors that distinguish an area only 30 meters square. They circle the earth in a polar orbit at an altitude of 438 miles, passing over practically every spot on the globe every 16 days.

They have provided governments and private industry with information about the earth's vegetation, mineral resources, and marine and atmospheric conditions. The satellites have helped predict crop and forest yields and have monitored pollution. R-E

OK's Hot Tip for Desoldering Problems

SA-6 DESOLDER IRON

Revolutionary new electric desoldering iron combines the ease and portability of a hand-held, manual, desolder pump, with performance of an industrial desolder station. This unique AC powered compact tool features portable, one-hand desoldering eliminating the need for separate soldering iron and desolder pump. No shop air required. Essential for all tool kits, field service technicians, and repairmen, as well as production applications. Vacuum chamber is easily removed for cleaning or replacement. Replacement tips available. Tool is supplied with SAT-6-059 tip; diameter .059 inch (1.5mm).

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- Replacement nozzles available.

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SA-6-230	230V AC 50/60Hz	
NOZZLE	NOZZLE HOLE DIAMETER	
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SAT-6-070	.070	1.7



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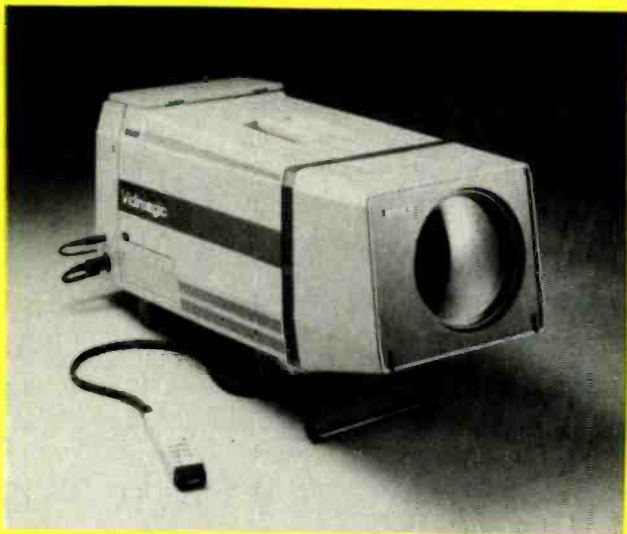


VIDEO NEWS



DAVID LACHENBRUCH
CONTRIBUTING EDITOR

• **New tube.** Sony's unique *Vidimagic*, which has a list price of \$2,995, is an all-in-one combination of projection TV, *Betamax* VCR, 181-channel TV tuner, and PA system. Designed for the industrial-TV market and looking like a large cannister vacuum cleaner, it weighs 34 pounds. One end is a fast *f1* projection lens assembly, the other end a videocassette receptacle.



What is truly unique about *Vidimagic* is its picture tube—Sony's first *Indextron* color tube, which uses the principles of beam indexing—almost as old as shadow-mask technology but never fully developed because of the problems of circuit design, which Sony presumably has solved with IC technology. The *Indextron* uses a single gun and no shadow mask, the electron beam being directed to the proper phosphor stripe electronically. Thus, Sony says, nearly 70% of the electrons land on the screen and activate phosphors, as opposed to about 20% in a shadow-mask-type tube. *Vidimagic* is brighter than previous single-tube projection systems, requires no convergence, and can project a picture from 30 to 200 inches in diagonal measurement.

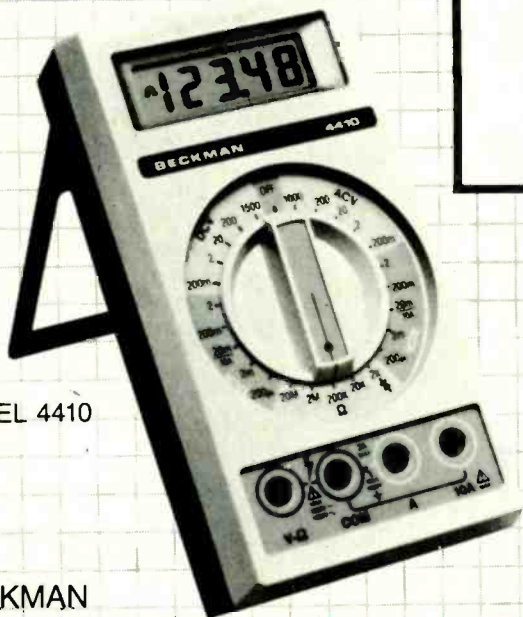
• **Toward a \$995 camcorder.** The one-piece video camera-recorder combination, or

camcorder, seems to be coming into its own, and manufacturers are tracking its progress very carefully. So far, all approaches appear to have some drawbacks. The *Betamovie* is a record-only machine and the tape can be played back only on a separate Beta deck. The *VHS VideoMovie* uses the small VHS-C cassette, which permits only 20 minutes of recording. The new 8mm format is non-standard and incompatible with 1/2-inch tapes. And all camcorders so far have one thing in common—they're expensive. Most manufacturers believe that, in order to become a true mass-market product, the camcorder must use a full-sized standard 1/2-inch cassette, be capable of recording and playing back, and retail for less than \$1,000. As a result, Japanese VCR manufacturers are developing such units in both Beta and VHS formats. When they come—probably in about two years—those units will be relatively stripped-down, simple-to-use machines. They will weigh somewhat more than the 5-1/2 to 6-1/2 pounds of current camcorders, and probably will record at a single speed, Beta II or VHS SP, for two hours per cassette.

• **Picture-tube chaos.** The unexpectedly high sales of color-TV sets and the proliferation of tube types have both contributed to a shortage of picture tubes throughout 1984, as the tube and glass industries work at capacity to keep up with demand. Manufacturers of glass for tube bulbs and funnels, and of metal shadow masks, are undergoing major expansions to try to keep up with demand. One of the biggest problems is the vast increase in the number of picture-tube sizes and types. There are still tubes being made in the traditional 13, 15, 19, 21, and 25-inch sizes. In addition, there are the new square-cornered versions in 14, 20, and 26 inches, with a 27-incher coming up. Then in those new sizes, there are both the rounded and the flattened faceplates. To make matters worse, there are at least three different transparencies of glass—the high-brightness 85% light transmission glass and the high-contrast 52% glass, plus the new blue-tinted glass.

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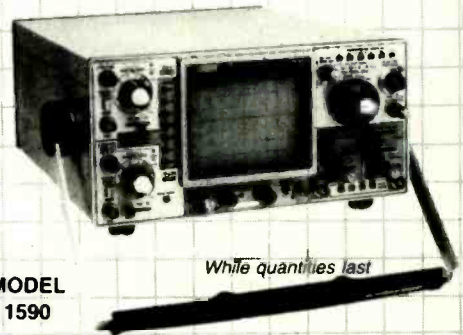
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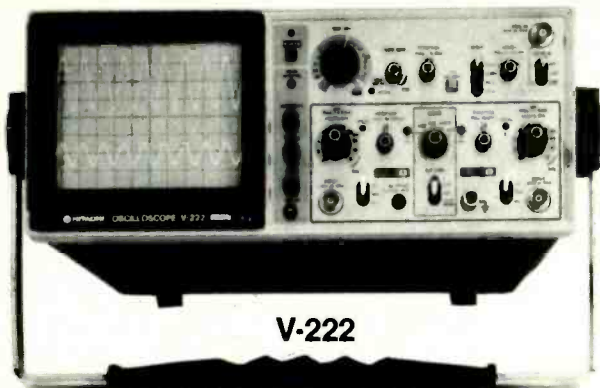
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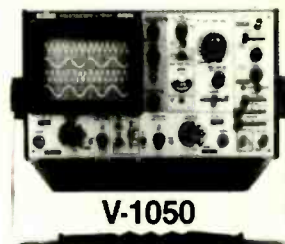
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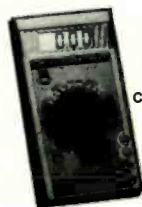
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SATELLITE TV

TVRO Evolution

LAST TIME, WE LOOKED AT SOME OF THE basic elements of a TVRO. This month, we'll look at how those elements have evolved over the years.

Feed changes

Although the reflector and its mount are the first earthbound portions that the satellite signals "see," we'll start with the feed because it is positioned in front of the dish proper. The feed is a small antenna, designed (on purpose) to "see" just the surface of the dish, from which it intercepts and collects energy. The 1979/80 feed was typically built from brass, had a semi-rectangular shape, and presented little real mystery to the user. That was before "automatic feeds."

Feeds in 1979/80 had to be mechanically moved from one stationary position to another station position (turned or rotated on their own axis) when the user wished to change from one set of channels with *horizontal polarization* to another set with *vertical polarization*. To do that, without running outside to move something by hand, required that a small motor attached to the feed physically rotate the feed and the LNA it was attached to. As often as not, that small motor was a standard television antenna rotor pressed into service for that unusual function.

The 1984 feed is quite a sophisticated device. First of all, it is no longer rectangular; it is round. That round shape is supposed to match the reception abilities of the



FIG. 1

feed to the round surface of the dish. That's not hokum; it really helps.

More important than the shape is the gadget inside: a tiny sensor that either moves a probe from one position (horizontal) to another position (vertical), or a non-moving ferrite material that twists the signals themselves as they pass by the ferrite.

The end result is that the user no longer has a small motor turning or twisting the LNA plus feed; he has an automatic switching system that matches the polarization of the antenna's feed system to the channel the user has tuned in.

In 1979/80, the user had to first determine what channel he wanted to tune in; then he had to decide whether that channel used horizontal or vertical polarization. Once he/she knew that, the next job was to decide which position the feed was already in and whether it needed to be rotated. If

BOB COOPER, JR.*
SATELLITE TV EDITOR

rotation was required, a cumbersome knob was turned and after 15 seconds had passed, the feed was now properly polarized. Finally, the channel/transponder could be changed!

In 1984, the viewer simply changes the transponder. Everything else is automatic. All of the control circuits are built into the receiver and the polarizer is controlled by those. Pretty neat, and exceedingly reliable.

Dish changes

It was not until early 1980 that the first firm (ADM/Antenna Development and Manufacturing) introduced a home-style dish that was designed from the ground up to be used by home TVRO's. Earlier dishes were either found in surplus-sale yards or they were the heavy-duty dishes created for commercial service. There was one interim stage in between. The very first dishes were actually fiberglass copies, struck off other fiberglass or metal dishes (as molds). ADM started from scratch with a petalized all-metal dish (like the one shown in Fig. 1) that was capable of being shipped coast to coast at reasonable shipping costs. Those that followed shortly thereafter were either copies of the original ADM or copies of older commercial-style dishes. Here's what the installer had to work with:

1) Surface accuracy or its trueness to the desired parabolic curve, was marginal. Piece antennas, such as the first ADM's, fitted together with some difficulty—primarily because of a lack of machin-

continued on page 20

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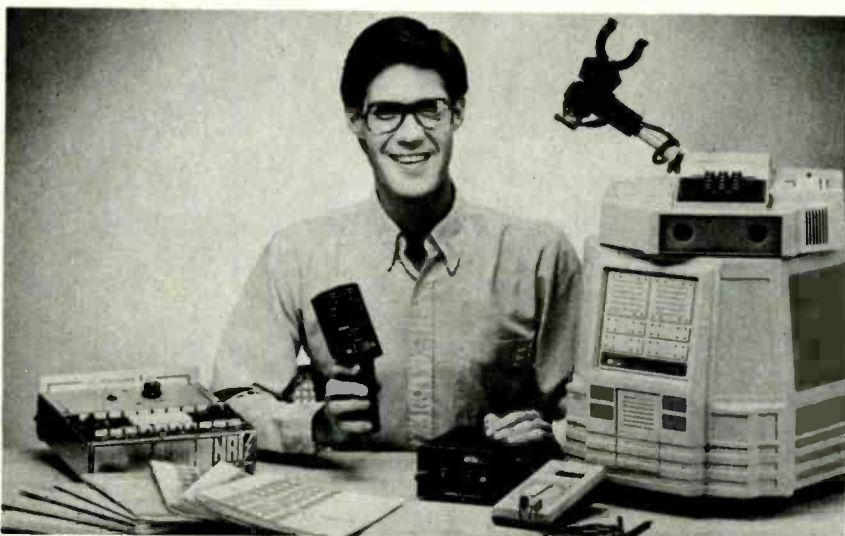
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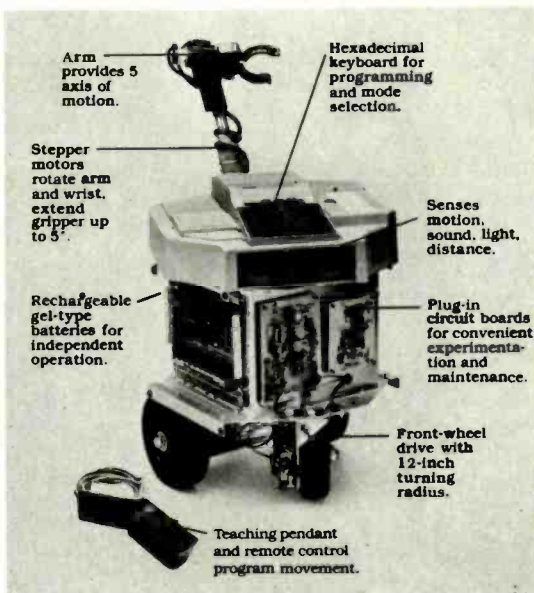
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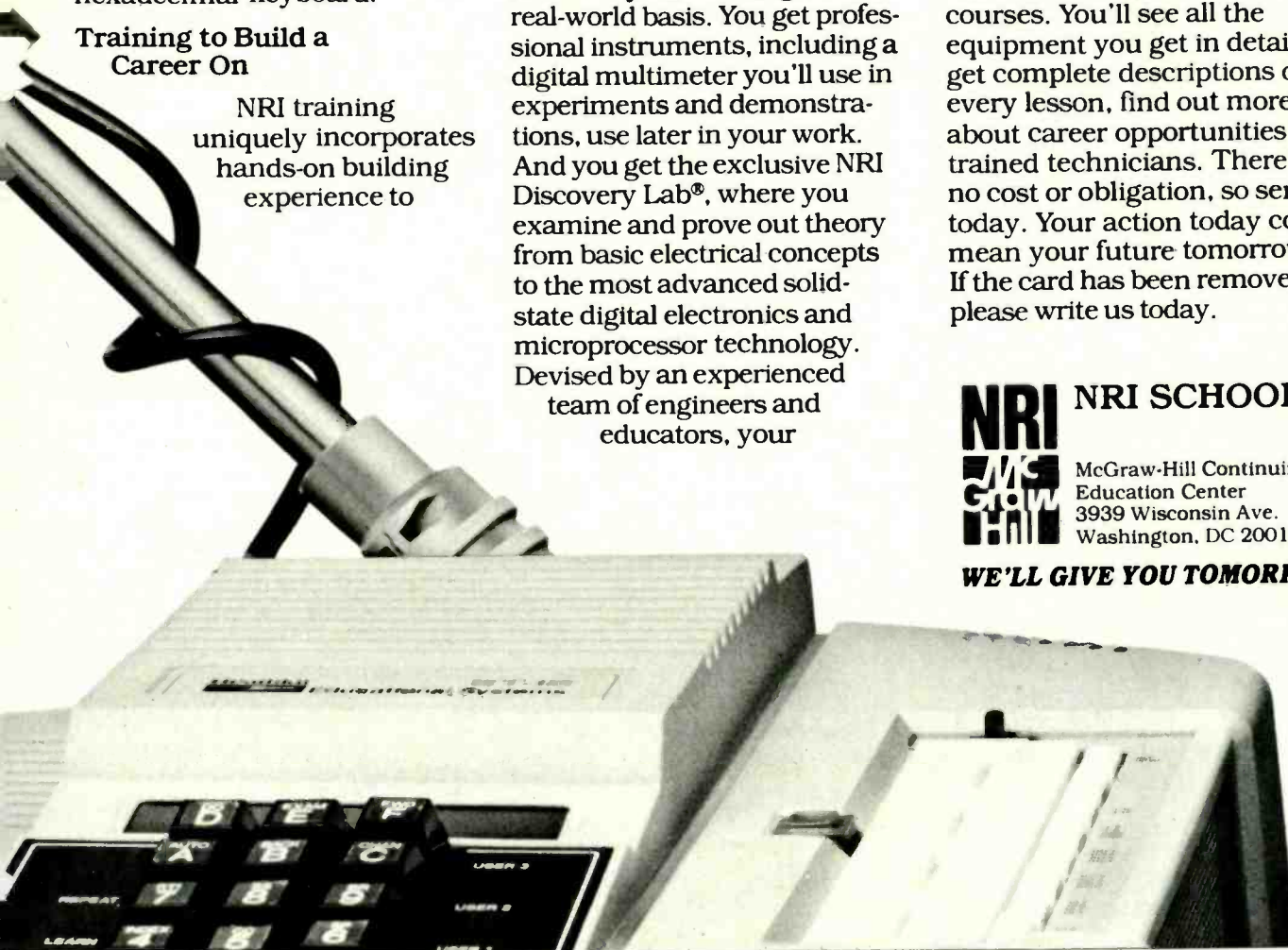
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SATELLITE TV

continued from page 14

ing tolerances at the manufacturer. The field installer made the pieces fit by pushing and shoving, drilling new holes and, in exasperation, rebending metal or torquing the fiberglass. In all of that, the parabolic surface, so necessary for high performance, was lost.

2) Antennas were sold without

a feed; that was an add-on item and the dealer was left on his own to locate a source for feeds. When he found a feed source, his next problem was ensuring that the feed was designed to work properly with a dish that had particular focal length-to-diameter ratios. Often that did not happen, and once again, the system performance suffered.

3) Mounting systems were especially poor. The object was to have a mount that supported the

dish in a rigid, stationary position, pointing at the desired satellite. Most mounts initially were designed to adjust the dish first in one direction (such as azimuth or side to side) and then in elevation (up and down): two separate steps.

That made it impossible for an antenna system to "track" from one satellite to another easily, since any change required two separate adjustments. The answer would be *polar* mounts, but it was later in 1980 before the first began to appear and work well.

4) The overall efficiency, a measurement of the accuracy of the parabolic surface, the design, and positioning of the feed, was seldom (if ever) over 55%. That wasn't bad; virtually all of the commercial antennas made claims no higher than that. But much better performance was coming.

5) Finally, there was the price. The early ADM established a pricing plateau, to dealer, in the \$2000/\$2500 region. The volume was small, and start-up costs were high. Even fiberglass knock-off antennas were almost as expensive. That was a function of many ruined-piece-parts tossed out in the process of getting those that were acceptable.

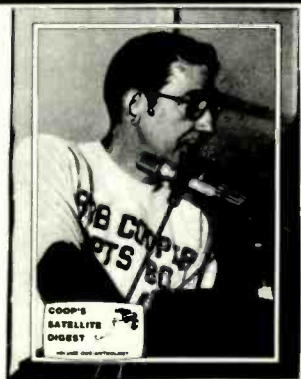
It was not a unique scenario; everything and everybody was new. Most of those designing and selling equipment were brand new to microwave; many were brand new to anything electronic. A giant learning curve was ahead.

The 1984 dish scene is much brighter. Surface accuracy is far better because computer-aided machining techniques have been applied. Feeds are generally sold with the antenna (although not always) and they are the same sophisticated devices we detailed earlier. The dealer is no longer chasing bits and parts. The antenna mounts are now mostly polar and they have evolved from large, cumbersome devices to lightweight (and usually strong) supports that allow the antennas to zip through the sky with a minimum of tracking error. Antenna range tests, done on professional test ranges, are now common and antenna (including feed) efficiencies

continued on page 90

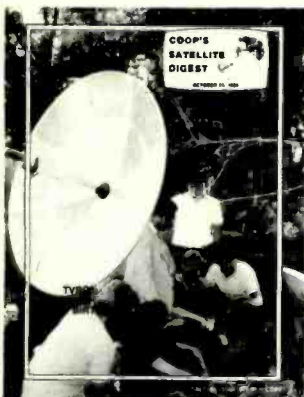
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LETTERS

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ANOTHER TYPE OF SATELLITE DISH

I want to thank you for the fine articles by Martin Clifford, "All About Satellite TV" and "The Dish," which appeared in the June, 1984 issue.

Although I already have my dish, I enjoyed his article with one exception. The statement on page 51, ("The Dish"), which says, "All dishes are made of stainless steel or aluminum..." There are a lot of fiberglass dishes, in fact, mine is a ten-foot four-section fiberglass type, and gives perfect reception of all channels and all birds. But, if



I had it to do again, I would purchase the spun aluminum, one-section aluminum as it would be much lighter in weight.

WILBUR T. GOLSON
 Baton Rouge, LA

COMPLEXITY AND ELECTRONICS

As a recent subscriber to Radio-Electronics I thought that my comments might be of interest. First let me say that I am not exactly the kind of subscriber you perhaps would expect to lay down \$15.00 a year for your magazine. I am a non-electronics person. The reason I buy Radio-Electronics is that I'm interested in where we are in the "State of the Art" and what we as consumers can expect from various producers and our government, which seems to get its fingers into everything.

The article that prompted this

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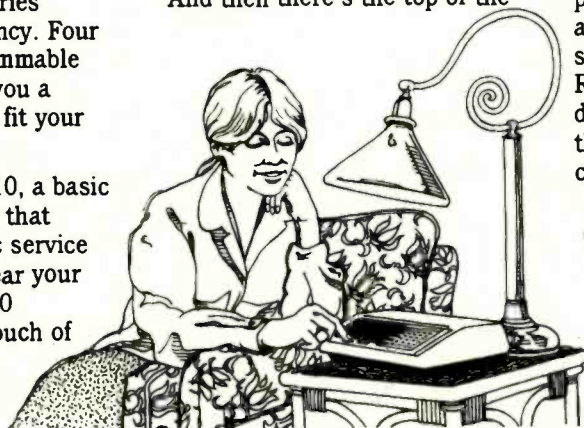
And then there's the top of the

line Z 60. It covers all the public service bands plus aircraft and FM radio broadcasts with sixty total channels.

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Regency

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letter is "Build this Auto Exhaust Analyzer" (*Radio-Electronics*, May 1984). I currently repair and rebuild automobile fuel-systems and can attest to the complexity of modern auto emission-devices and the government's role in fostering this expansion of electronic components in automobiles, a point I'm sure hasn't escaped your detection. The fact of the matter is that no current magazines (including yours) spend any amount of time on that increasingly complex area

of electronics. For example, the General Motors Computer Command Control (CCC) has its own PROM's and I've recently wondered about the possibility of re-programming those to modify them for performance use.

Then there's the problem area of increasingly expensive test equipment in the marketplace (i.e. \$10,000-\$30,000). It would be gratifying if somebody with the proper electronics experience could cover the area of electronic auto-

motive-test-equipment. Both articles that evaluated those units, and ones that covered their repair and testing would be appreciated.
PETE KISSA
Dayville, CT

I certainly would not expect a non-electronics person to read even one issue of Radio-Electronics. However, you do make your reason for being a subscriber quite clear.

The points you raise are interesting, and certainly from my point of view, well worth exploring, but first I must touch on the reasons why very few publications other than those interested in automobile engineering would touch on the subject matters you mention. While it is fascinating to learn about the many electronic devices in the modern automobile, unless you are personally involved in the manufacturing of these devices, such knowledge has little value to slake your own curiosity. All of these elements are made and constructed to be modular replacement items, so that repairing the system does not entail very much more than unplugging one module and plugging in another.

As you must know, this also applies to European vehicles. For quite some time Volkswagen has used a fuel-injection module made by Bosch. When the 25-cent SCR in the unit breaks down, the entire module is replaced.

While I personally deplore the idea of replacing a \$500.00 module for the sake of a 25-cent part, the need for a relatively unskilled mechanic to get a customer's automobile back on the road operating properly, once again makes that procedure necessary.

Incidentally, that problem exists in many other areas as well. For example, in a General Electric clothes dryer that I recently looked at, there is a simple little module that turns off the machine when the clothes are dry. It is a simple SCR that is fed a signal by a moisture sensor. The module costs \$48.00. If you had the equipment and skill to service that module the chances are your parts cost would be under \$3.00, and allowing 30 minutes for repair, about \$22.00 in labor. Again, the repair-

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man for just a few dollars more, can immediately restore operation of that machine in the customer's home by the simple replacing of the entire module.

The real question that your letter has addressed (and it's a question that many have addressed) has two reaching effects in the editorial coverage of our publication: "Even if the repair is a module replacement, does the Radio-Electronics reader want to know how the module functions and how he might troubleshoot it and repair it—even though he realizes it may not be cost-effective to do so?"

So that we may get a better feeling for our readers sentiments on those subjects, we invite our readers to write us and express their feelings on them.—Larry Steckler, Publisher

VOLTAGE ERROR

Your article, "Designing With Linear IC's," by Joseph Carr in the July 1984 issue has an error on page 55, column 3 line 2. The gain is 20 not 100. That is found from: $A_v = (R_2/R_1 + 1)(N_s/N_p) = (2)(10) = 20$. The voltage mentioned later should also be 20 not 100.

WILLIAM LEFLER
Forks, WA

INTERFACE ERROR

I built the interface for the TS1000/ZX81 described in the article "Interfacing the ZX81" that appeared in the July 1984 issue of Radio-Electronics. I found two errors that I would like to bring to your attention.

First of all, in the schematic shown in Fig. 2, the A2 output of IC8 is at pin 6, not pin 5 as shown. Secondly, in the card-edge pinout shown in Fig. 1, there are two A1 lines. The one at the bottom of the illustration (above ROMCS) should be A4.

BOB MIX
Seattle, WA

CONVENTIONAL FLOW CONFLICT

As an electronics student, I strive to find several ways to justify a point of an accepted theory. Occasionally in my reading I encounter strongly conflicting views. One case that puzzles me is the continuing use of the terms "electron

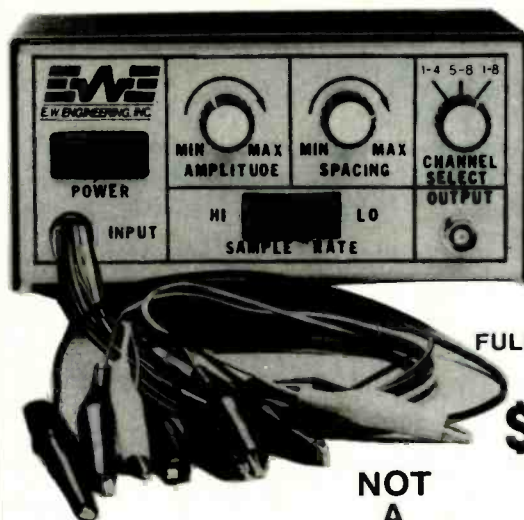
flow" and "conventional flow."

I have read coverage of that topic by Jack Darr, ("Service Clinic," Radio-Electronics, January 1983) and other reputable writers who have attempted to explain why there are two ways to describe electrical current; however, none that I have found propose a reason why reference is still made to "conventional flow." If Benjamin Franklin's theory backing "conventional flow" is a long past proven fallacy, then why is it still

referred to, and accepted by some technical writers as the proper approach to describe current flow?
CHRISTINE MOORE
O'Fallon, Missouri

There is really no conflict in theory—everyone agrees that electrons flow from negative to positive. Conventional current is just that—a convention. It is internationally agreed upon, however, and you should become comfortable with it.—Editor

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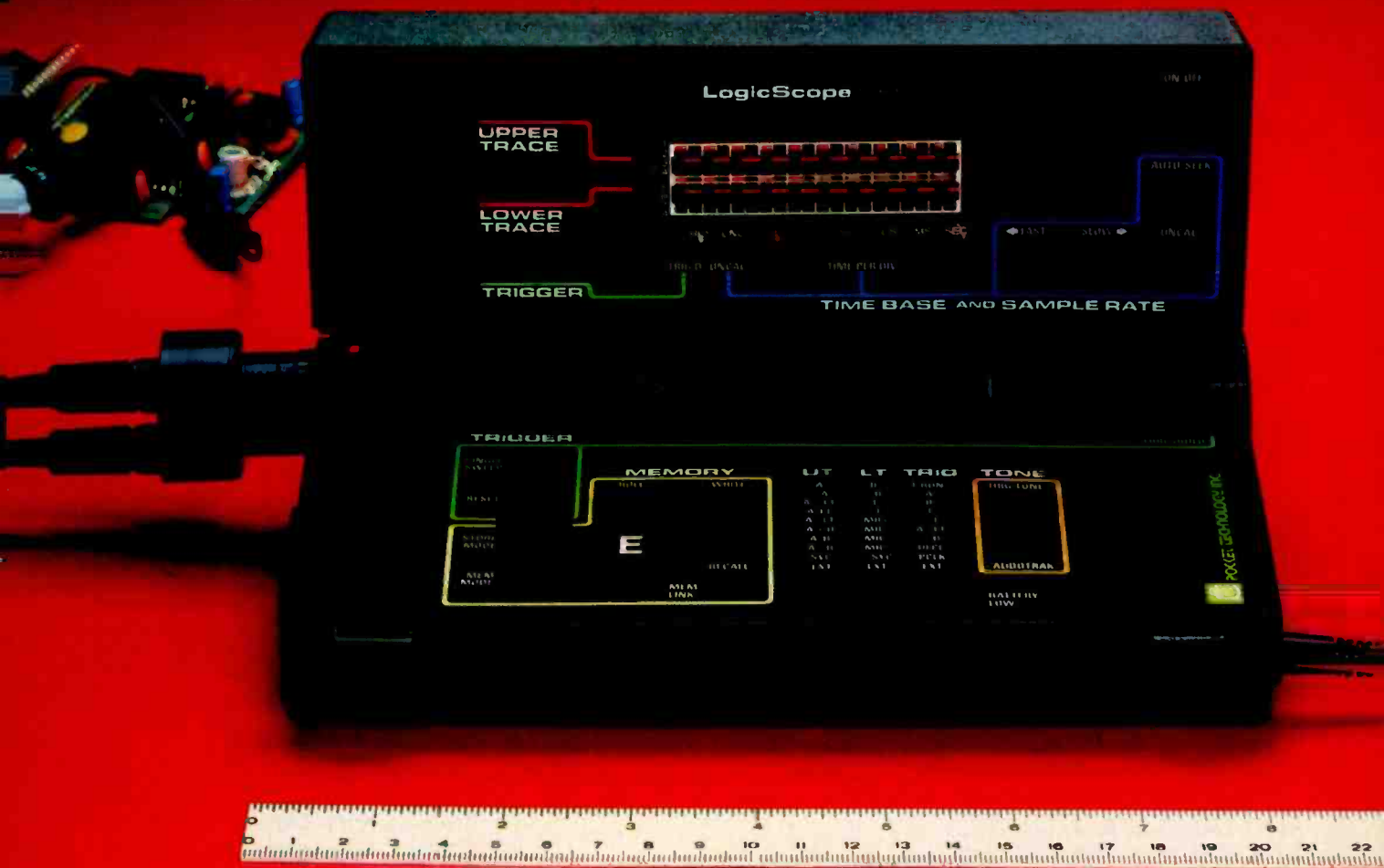
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and—most important—also portable.

A tool that combines those features is the *Solder Scooter* from Paladin (3543 Old Conejo Road, #102, Newbury Park, CA 91320). OK Industries, Inc. (3455 Conner Street, Bronx, NY 10475) offers a practically identical tool. Apparently, both are made by the same company. The only differences that we saw were the color and the imprinted model number (SA-6-115 for OK's).

The main advantage of the *Solder Scooter* over those other hand desoldering tools we mentioned is that it does the work of two tools—it both melts the solder and vacuums it up. A 30-watt heating element heats up quickly; the tool is ready for use typically in about 1½–3 minutes. Recovery time after desoldering a large joint is also fast.

Operating the *Solder Scooter* requires only one hand. That's a big advantage over vacuum-bulb-

type methods. You can use your free hand to hold the circuit board you're working on, or to gently pull a component off the board from the other side (or loosen up a connection). The unit is 10¼ inches long, but it's lightweight (about 4 ounces) so it's easy to handle. It fits well into a standard soldering-iron holder. The vacuum-pump part of the *Solder Scooter* is similar to desoldering pumps that you can buy separately. To "load" the pump, you push a plunger down with your thumb. A side-mounted "trigger" releases the plunger, and solder is pulled into the reservoir. The difference between the *Solder Scooter* and other hand pumps is that the solder is pulled in right through the heated tip.

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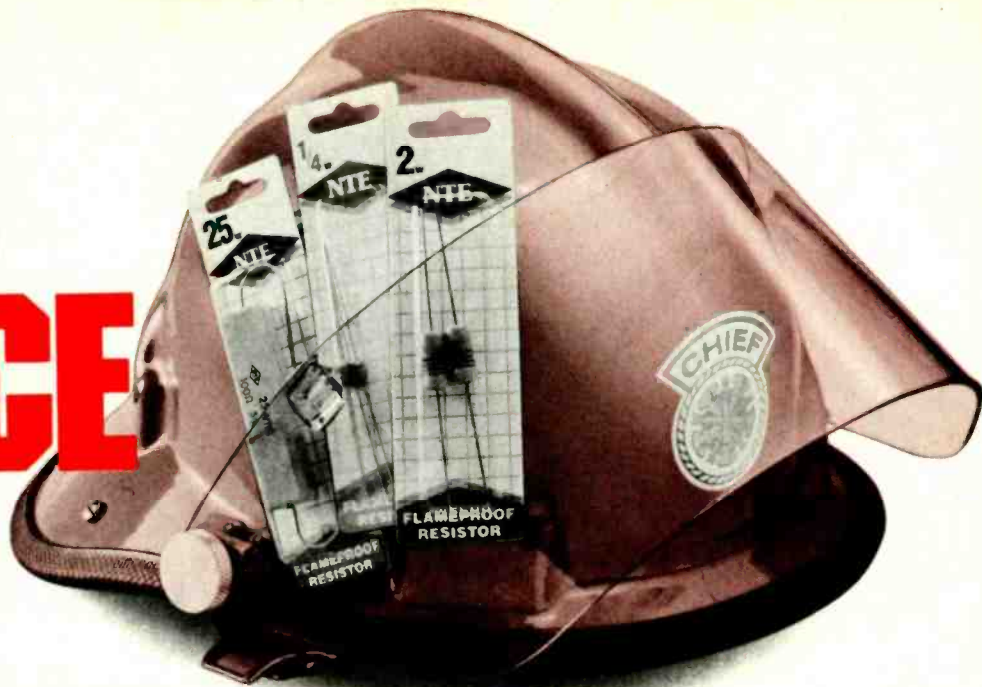
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	Poor			Fair			Good			Excellent

The pump, along with the reservoir, can simply be unsnapped from the tool. Once removed, the cover of the reservoir can be opened and the solder simply dumped out.

Replacing the tip is as easy as cleaning the reservoir—it simply unscrews. The tip that comes with the unit has a 1.2-millimeter opening. A 1-millimeter tip is also available, and a 1.5-millimeter tip is available for larger jobs. (Paladin also sells other replacement parts for the desoldering tool, including the heater, the heat-conductor tube, O-rings, and pump assembly.) Paladin sells two versions of the *Solder Scooter*: Model PA 1707 comes with a two-wire cord and PA 1706 has a three-wire cord.

The *Solder Scooter* sells for \$22.95 (\$24.95 for the three-cord model.) It is well suited for low-volume applications, such as for hobbyists or field-service technicians. We should point out one more thing—in a pinch, it makes a good soldering iron, too. R-E
continued on page 30

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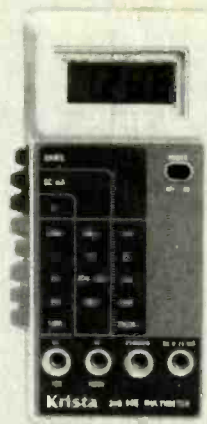
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and DC voltage, DC current, and resistance; there is also provision for performing a diode test. All range and function switches are located along the side of the case for easy, one-handed operation; the POWER switch is located on the front panel.

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IN THIS SPACE WE OFTEN REPORT ON devices that represent the state-of-the-art in test-equipment technology. Those units are sophisticated, highly accurate, and, more often than not, very expensive. That's fine if you are a professional who needs the best for his work, or a dedicated hobbyist who constantly has one project or another on the bench. But what about those for whom electronics is just an occasional diversion, or those

who can not afford the latest in microprocessor-controlled gear? Well, they are not out of luck. There's quite a bit out there in the way of low-cost, but quite serviceable, test equipment.

One such instrument recently came to our attention. It is the Krista (PO Box 3423, Torrance, CA 90510) model 30B-140 multimeter. That unit is a hand-held digital multimeter with a $\frac{1}{2}$ -inch, $3\frac{1}{2}$ -digit LCD readout. It can measure AC

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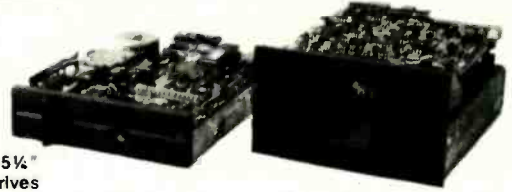
A. TM50-1	SS/DD	\$ 99.50
B. TM55-2	DS/DD	179.00
C. TM55D-2	DS/DD	199.00

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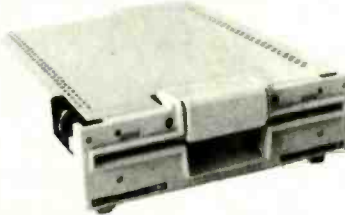
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E. TM100-2	DS/DD	159.00
F. TM100-1	w/o controller boards (mechanics only)	\$45.00

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N. IDC 25S	4.03	3.69
O. IDC 37S	6.14	5.57

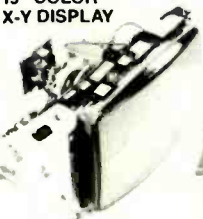


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U. IDP-20	\$1.01	\$.90
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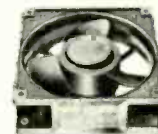
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AC voltage is measured only on two ranges—200 and 1000, full scale. The claimed accuracy is $\pm 1.2\%$ and input signals with frequencies from 40 to 500 Hz can be handled. Overload protection is 500-volts DC and 350-volts RMS AC for the 200-volt range. For the 1000-volt range it is 1100-volts AC and DC.

DC current is measured over five ranges. Those are 200- μ A, 2-mA, 20-mA, 200-mA, and 10-amps full scale. The accuracy for all current ranges is $\pm 1.2\%$. Overload protection is provided via an internal 0.5-amp fuse. Maximum voltage input is 200 mV.

Finally, resistance is measured over 4 ranges. Those are 2, 20, and 200 kilohms, and 2 megohms. The claimed accuracy is $\pm 1\%$ on all ranges. Overload protection is provided to 250-volts DC and RMS AC. The nominal test-current produced by the meter varies from 100 μ A for the 2K range to 0.3 μ A for the 2-megohm range.

The unit is powered by a transistor-radio type 9-volt battery. Ex-

pected battery life is specified as up to 200 hours of continuous use. An annunciator on the LCD readout gives warning of a low-battery condition.

Krista		30B-140												
OVERALL PRICE														
EASE OF USE														
INSTRUCTION MANUAL														
PRICE/VALUE														
		1	2	3	4	5	6	7	8	9	10			
		Poor		Fair		Good		Excellent						

The accessories supplied with the unit are a set of test probes, battery, spare fuse, and the operator's manual. The six-page manual is, in all honesty, not very good. It is poorly written, most likely owing to the fact that the manual is a translation (the unit is made in Hong Kong), and provides only the barest details concerning the unit.

The unit is fairly convenient to

use, and operates as claimed. We did feel that it was a bit slow. The meter takes readings at a rate of about 2.5-per-second, and it usually took several seconds for the meter to "zero-in" on a reading. It should be noted, however, that that is a characteristic common to most other digital meters.

On the plus side, the meter has a tilt stand built into the case, and the large display is easy to read under most circumstances.

The model 30B-140 is covered under a one-year warranty. Complete details concerning the warranty, including the address of the U.S. service station, are supplied on a separate card that is included with the unit.

Now we come to what has to be the best thing about the unit—the price. It sells for just \$41.95, certainly an excellent price for a meter of this type.

The model 30B-140 is available from your local distributor; it is also available by mail order from Fuji-Svea (PO Box 3375, Torrance, CA 90510). R-E

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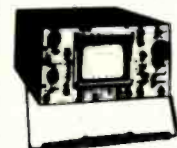


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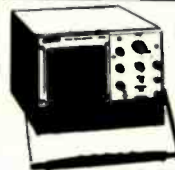


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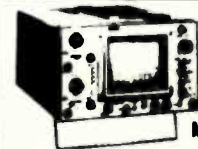


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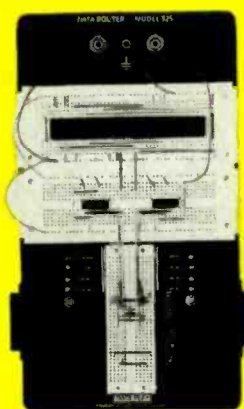
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HAVE YOU EVER HAD TROUBLE INTERFACING a modem or printer to your computer even though the connections followed the RS-232 "standard?" Have you ever wired a custom RS-232 cable only to find that you goofed? If you use a lot of peripherals and/or several different computers, you've undoubtedly come up against those problems many times. The quickest and easiest way to find out just what the problem is—and how to go about solving it—is to use a breakout box such as the *Data Router 325* from Global-Data (70 Fulton Terrace, New Haven, CT 06509)

Global Data	Data Router										
OVERALL PRICE											
EASE OF USE											
INSTRUCTION MANUAL											
PRICE/VALUE											
	1	2	3	4	5	6	7	8	9	10	
	Poor			Fair				Good			Excellent

The *Data Router 325* consists basically of two 25-pin D-type connectors (one male and one female), eight LED's, and three solderless breadboards. One connector and 4 LED's (along with current-limiting resistors) are wired to either side of a solderless breadboard. Thus, by simply inserting jumper wires from one side to the other, you can feed through, cross-patch, or leave open, any of the RS-232 lines (except pin 1, which is permanently connected as a ground.)

The LED's can be used to monitor the signals on any of the control lines. Because one side of each LED is grounded, and the other side is connected through a current-limiting resistor to the solderless breadboard, simply inserting a jumper wire (between the LED and the line that you monitor) completes the connection. The RS-232 standard pin assignments are printed on one side of the breadboard—that is most certainly a convenience.

Along with the breadboard that is used to make the RS-232 and LED patches, there are two additional breadboards. Those extra breadboards are what set the *Data Router 325* apart from other breakout boxes we've seen. One breadboard (with 0.3-inch center-channel spacing) can be used for standard DIP IC's, and other components, while the other breadboard, (with 0.6-inch center-channel spacing) can be used for larger (even 40-pin!) IC's! So the *Data Router* can be a very convenient way to test out your data buffer or serial-to-parallel converter. Three color-coded binding posts are located above the two extra breadboards so you can conveniently bring outside power to your breadboarded circuits.

The *Data Router 325* sells for about \$107. While that may seem expensive for a breakout box, remember that you're getting both a breakout box and ample solderless-breadboard space. If you believe that time is money—and if you've ever spent hours discovering that a manufacturer decided to include some non-standard features in his RS-232 configuration—you can begin to see its value. R-E



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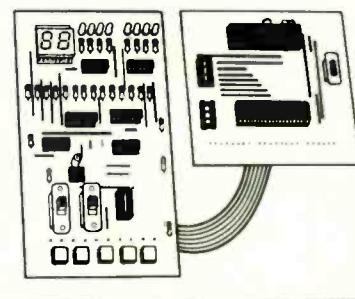
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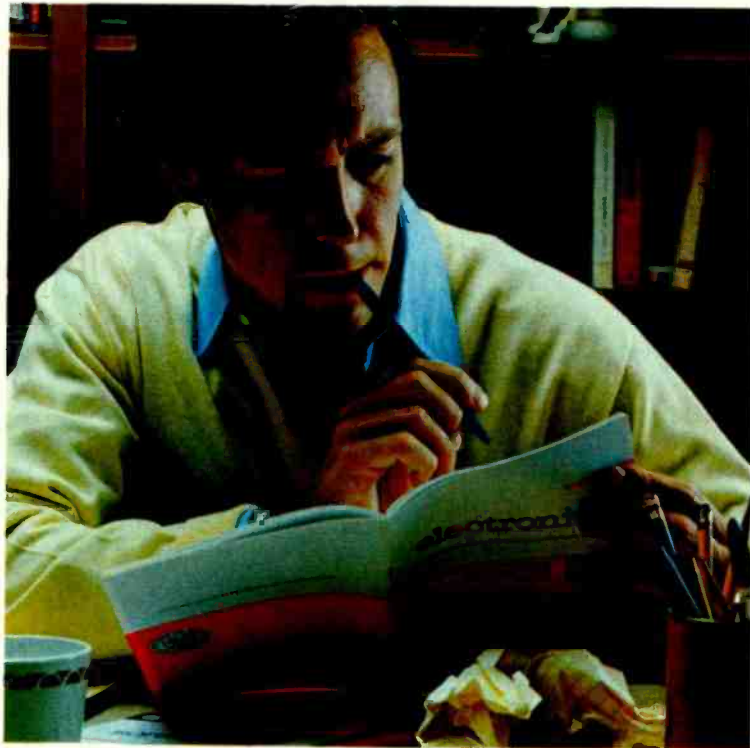
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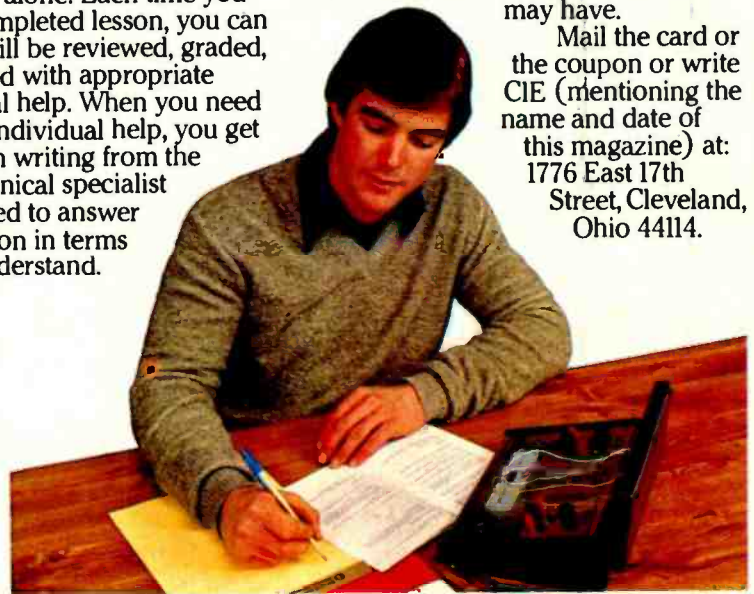
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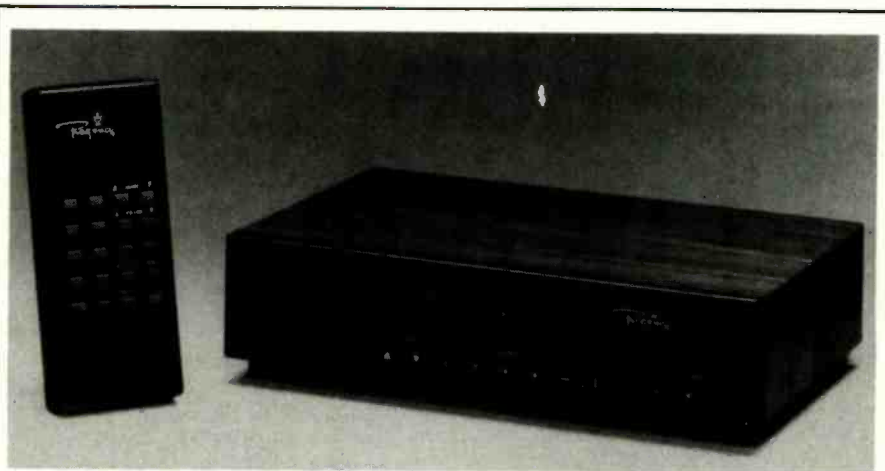
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SATELLITE RECEIVER, model SR5000, has infrared remote control and dual-microprocessor circuitry that allows the user to preset satellite positions, polarity, and skew, audio-subcarrier frequencies, and tuning voltages into memory. The programmed information can then be selected from the unit's front panel or the full-function remote-control unit. Additional remote-control functions include volume control with mute,

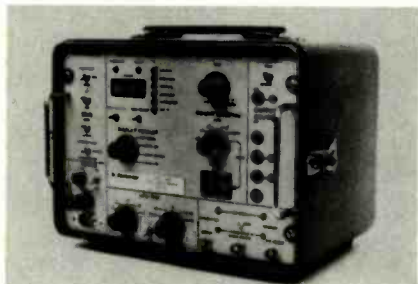
direct or scan channel-selection, and video fine tuning.

A special feature of the model SR5000 is that it uses a block down-converter instead of the single-conversion type. One of the chief advantages of using a block converter is that it allows the user to install a multiple receiver system.

The model SR5000 is priced at \$699.95.— **Regency Electronics**, 7707 Records St., Indianapolis, IN 46226.

TEST SET, model 273A, is a light-weight, rugged portable error-rate test set. It has a self-contained receiver and transmitter, permitting complete testing for digital-transmission systems or other components such as T1 and T1C carrier, T1 Outstate, Lenkurt Duobinary Carrier, Multiplexed T Carrier and digital-radio systems.

The model 273A features a checkout with an output bit rate of 1.544 megabits/second \pm 50 bits/second in the T1 mode and 3.152 MB/s \pm 50 bits/second in the T1C mode. It operates over a temperature range of 0°C to +50°C.



CIRCLE 9 ON FREE INFORMATION CARD

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R-11

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reach out and bring in those distant stations from all over the world.

Simplicity of operation is enhanced by a band-spread type tuning control. Electronic band switching, with LED band indicator, along with a tuning meter to indicate received signal strength, combine to provide you with superior listening capability. Safety Hold-Release switch prevents accidental station loss. Large front mounted speaker provides excellent sound quality. Tone switch adjusts for high, low and voice transmission.

Optional HS-7 micro-head phones allow for private listening pleasure.

All this along with a record output jack, external antenna terminal and a rugged and attractive carrying case make the R-11 portable receiver the perfect travel companion!

More information on the Kenwood receivers is available from authorized dealers of Trio-Kenwood Communications 1111 West Walnut Street, Compton, CA 90220.



R-2000 Top-of-the-line general coverage receiver • 150 kHz to 30 MHz • Ten memories • Dual 24-hr clock with timer • Scanning • 100-240 VAC (Opt. 13.8 VDC) • Opt. VHF (118-174 MHz converter).

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by Bell Systems J98710R T1 quasi-random signal source. The receiver operates independent of the transmitter. It performs bipolar-violation-detection on any signal and bit-error-detection while working in conjunction with its own quasi-random transmitter or equivalent source.

The model 273A, with a one-year warranty, is priced at \$2750.00. — MR Associates, Inc., 162 Great Road, Acton, MA 01720.

MICROCASSETTE CLEANER, model 79000, is non-abrasive and represents an adaptation of the Allsop "wet" cleaning system to the requirements of the tiny components of the microcassette recorder. As in the standard-size version, cleaning felts and solution work together to remove oxides and other impurities from not only the



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head, but the capstan and pinch roller as well. The cleaning cassette is simply inserted in the recorder and activated like an ordinary microcassette. The package includes two cleaning cassettes and a 1/2-oz. bottle of cleaning solution. The suggested retail price of the model 79000 is \$9.95.—Allsop, Inc., PO Box 23, Bellingham, WA 98227.

MINIATURE SOLDER IRONS, model C and model G, feature non-charring thermoplastic handles and long-lasting pretinned iron-plated slide-on tips. Safe for

even the most delicate electronics components, they are grounded directly from the tip through a flexible, 6-foot cord and a 3-prong molded plug.



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To change or replace tips on either model, the user simply removes the old tip and slides on one of the more than 40 styles presently available. The model C is priced at \$15.95; the model G costs \$17.95, including a pretinned iron-plated number 2 chisel tip.—M.M. Newman Corporation, 148 Linden Street, Suite 105, Wellesley, MA 02181.

RF DOPPLER SENSOR model PD-245 is a UHF device that can be used in a variety of security and home-convenience applications.

The device emits a beam angle of 120° and will sense objects or personnel moving in this field at a range adjustable from 5 to 25 feet



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or more, depending upon the specific application. The field is not restricted by non-metallic surfaces and the unit can thus "see" through wooden doors, glass windows, etc. Upon detection, an internal triac will energize a 120-volt AC load (up to 250 watts) for an adjustable duration of from 3 to 90 seconds.

The model PD-245 can be used as a "hands-off" switch to turn on

lamps; in alarm applications to energize a siren or bell, as well as many other applications. It comes with a six-month warranty and is priced at \$69.96. — **Sentrynet Company**, PO Box 1208, Evanston, IL 60204.

COMMUNICATIONS RECEIVER, Bearcat model *DX1000*, is micro-processor-controlled and features direct-access keyboard tuning. Frequency coverage is continuous from 10 kHz to 30 MHz, including all shortwave bands, longwave, standard broadcast band (AM), amateur-radio broadcasts, and even the marine band.



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A ten-station memory makes it possible to store favorite frequencies for instant recall—or for faster “band scanning” during important openings. The digital display measures frequencies to 1 kHz, or at the touch of a button, doubles as a two time-zone, 24-hour digital quartz clock. A built-in timer can wake the user to a favorite station, or can be programmed to activate a tape recorder to record up to 10 broadcasts, in any frequency or mode, while the user is asleep or at work.

The model *DX1000* has a suggested retail price of \$599.95. — **Electra Company**, 300 East County Line Road, Cumberland, IN 46229.

METER, the Tenma Combination DMM/DCM meter, has transistor DC current-gain tester. Users can easily read voltage, current, resistance, capacitance, and h_{FE} on the clear ½-inch 3½-inch digit LCD display. The color-coded panel allows user to easily identify the function and range settings.

Safety features include overload protection, single fusing (with



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spare fuse inside), and stress-relief test leads. The Tenma Combination DMM/DCM meter comes in a convenient carrying case, with alligator clip h_{FE} leads, and has a one-year warranty. It is battery operated, and the LCD readout indicates low-battery condition. It is priced at \$74.95. — **MCM Electronics**, Centerville, OH.

RADIO/CASSETTE PLAYER, model 5770, features both Dolby “B” and DNR noise reduction for an improvement in signal-to-noise ratio on tape of up to 20 dB. The DNR noise reduction also functions on AM and FM for an improvement of up to 10 dB S/N. Other features include a dual-function fader (for 4-speaker control on the internal amplifier or for controlling 2 external amplifiers on the line-level



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outputs), program search on tape, auto-reverse with precision motorized tape-load and key-eject, electronic-governed DC servo tape motor, SDC ceramic tape head, 6-station memory, and up and down frequency seek. There is also signal-actuated stereo blend, an interference-absorption circuit on FM, automatic FM sensitivity control with local/distant range switch, separate bass and treble slide controls, and front-panel illumination.

The model 5770 is priced at \$399.95. — **Autotek**, 1447 Carolan Ave., Burlingame, CA 94010 R-E

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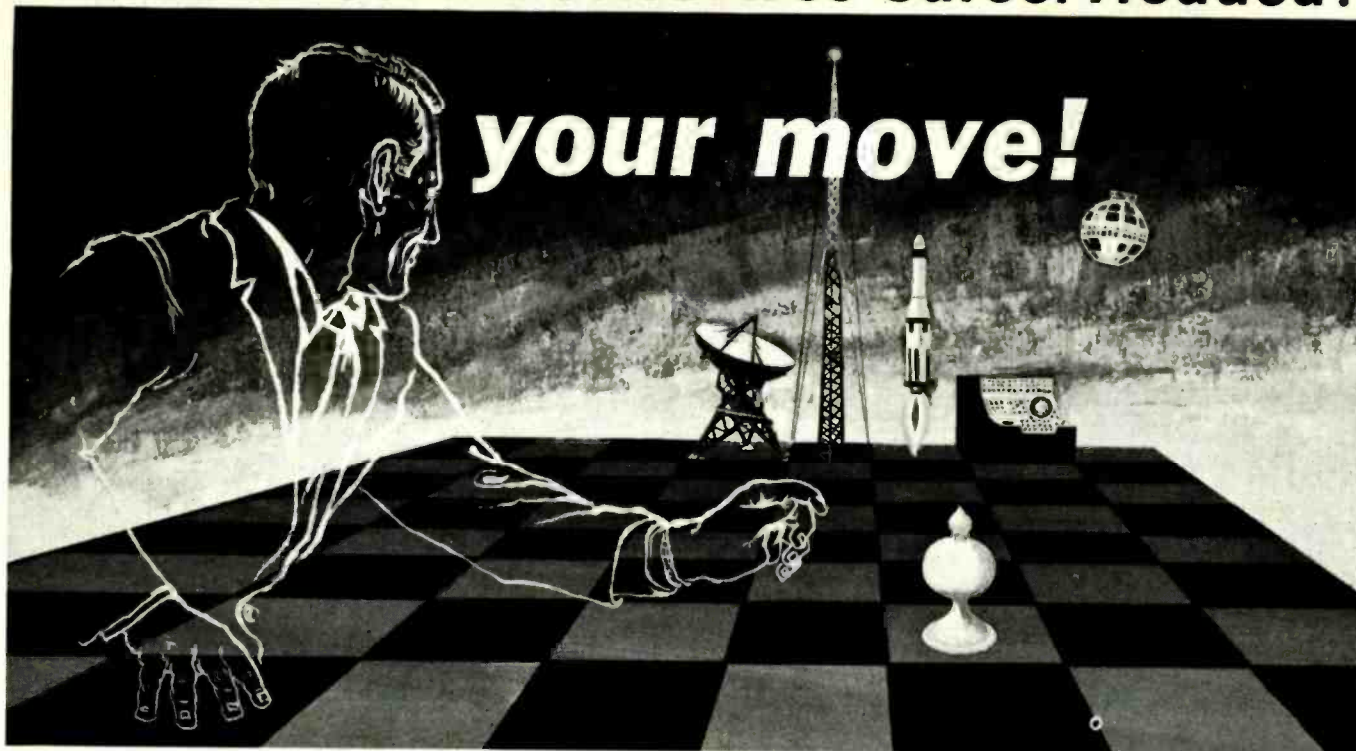
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YOU'VE PROBABLY ALWAYS WANTED TO own a high-performance, high-power stereo amplifier. If you don't have one, there are two likely reasons why: You are not sure you need that much power and you are deterred by the cost. But these days, with the increasing popularity of digital audio disc players, there is a new motivation for owning a high-power amplifier that can faithfully reproduce a wide dynamic range without distortion. And while the cost of commercial high-power amplifiers is still high, we'll describe a very high-performance design that you can build at a reasonable cost. Just what do we mean by "high performance?" Table 1 summarizes the characteristics of our design.

One of the most important features of the design is the use of power MOSFET output transistors in a complementary configuration. Those transistors, by themselves, eliminate a number of the problems usually associated with their bipolar counterparts.

The highly desirable characteristics of power MOSFET's for audio amplifiers have been recognized for a few years.

However, for many years only N-channel devices were available—only recently have their P-channel counterparts appeared at reasonable prices, making it possible to design amplifiers with remarkable performance but little complexity.

As we'll see shortly, MOSFET's aren't the only transistors used in the amplifier. Ahead of the output stage, a fully complementary bipolar design combines simplicity with high performance.

Why MOSFET's?

Although the evolution of power MOSFET's has primarily been (and still is) fueled by power-supply applications, there are a couple of reasons why MOSFET's make ideal devices for audio-amplifier output stages. First, they allow the design of amplifiers with very wide bandwidths, high slew rates, low distortion,

and straightforward simplicity. Also, MOSFET's lack a secondary-breakdown mechanism. (Secondary breakdown in bipolar devices is a localized heating effect in which "hot spots" develop under high-current conditions. A hot spot then conducts even more current, creating more heat, which, in a positive-feedback manner, may lead to a catastrophic destruction of the device.)

Because of secondary breakdown, bipolar devices must be operated within a "safe" area that often falls far short of the device's stated static current and power-dissipation characteristics. Safe-operation-area limiter circuits (whose misoperation has often been notorious) must be used in bipolar circuits. Because MOSFET's do not exhibit secondary breakdown, simpler and more reliable designs can be used.

Get high performance and high fidelity from this FET stereo amplifier. It feels equally at home in your living room or in a disco!

TABLE 1—SPECIFICATIONS

- Power output:**
250 watts/channel into
a 4- or 8-ohm load
- Frequency response (-3dB):**
5 Hz to 1.1 MHz @ 1 watt
5 Hz to 330 kHz @ 250 watts
- Distortion:**
< 0.05% IM to 250 watts
< 0.05% THD 20 Hz-20 kHz
- Signal-to-noise ratio:**
> 100 dB
- Damping factor:**
> 500 to 1 kHz with 8-ohm load
- Risetime:**
< 0.5 μ s @ 80 volts P-P
- Slew rate:**
> 160 volts/ μ s

The characteristics of the MOSFET's used in this amplifier are shown in Fig. 1. They are, of course, voltage-controlled devices. When the gate-to-source voltage, V_{GS} , drops below about 3.5 volts, the drain-to-source current, I_D , quickly drops to zero. That is called the *gate threshold voltage*, V_T . Above V_T , the *transconductance* (or transfer admittance) builds up to

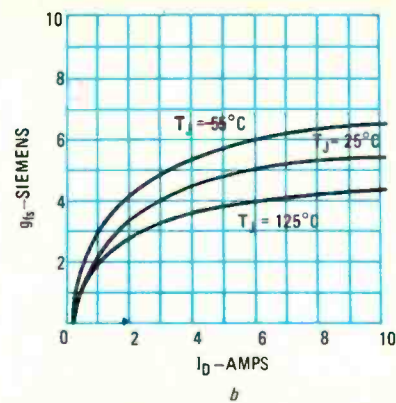
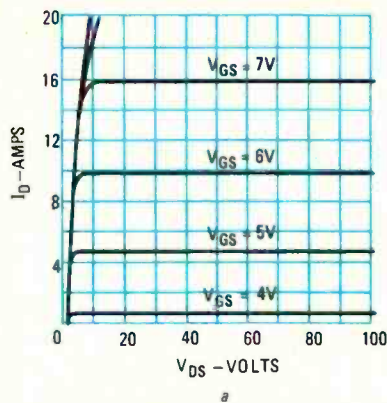


FIG. 1—MOSFET CHARACTERISTICS. Shown in *a* are the typical output characteristics of the IRF630. Shown in *b* is the typical transconductance as a function of drain current for the same device.

an asymptotic value, averaging about 3 amps of drain current per volt increase in gate-to-source voltage, V_{GS} . (Measured with V_{DS} constant, $\Delta I_D / \Delta V_{GS} = 3$ siemens)

A look at the circuit

The stereo power amplifier consists of four main stages: input, voltage-amplifier, inverter/driver, and output. Since the MOSFET outputs are the center of attraction, we'll begin there and work our way backward. The amplifier schematic (for one amplifier channel) is shown in Fig. 2.

Transistors Q21 through Q28 are the N- and P-channel MOSFET power output transistors. Each one is capable of con-

tributing a minimum of 6 amps of the output current for peak current requirements. Since the output transistors are in a common-source configuration, the output stage can have voltage gain, and the transistors must be biased with respect to the supply rails. The major advantage of that approach is that the bipolar driver-stage does not have to swing very much voltage, but the outputs may swing from rail to rail. (A common-drain output stage would require the driver to swing the entire output-voltage range which, with bias, would mean that either a pair of separate higher-voltage supplies would be required for the drivers, or that the output would not swing from rail to rail. That

PARTS LIST

All resistors 1/4-watt, 1% unless otherwise indicated. (5% types—values shown in parenthesis—can be substituted)

- R1—10,000 ohms, audio-taper potentiometer
- R2—2050 (2000) ohms
- R3, R4, R13, R14—10,500 (10,000) ohms
- R5, R6, R11, R12, R22—100 ohms
- R7—2490 (2400) ohms
- R8—500 ohms, potentiometer
- R9—2470 (2700) ohms
- R10, R29—100,000 ohms
- R15, R16—1000 ohms, 2 watts
- R17, R18—1000 ohms
- R19—5000 ohms, 10-turn potentiometer
- R20—8660 (8200) ohms
- R21—1500 ohms, 2 watts
- R23—R26—511 (510) ohms
- R27, R28—2000 ohms, 5 watts
- R30—50 (47) ohms
- R31—R38—24.9 (24) ohms
- R39—162 (160) ohms
- R40—5110 (5100) ohms, 1/2 watt
- R41—4.64 (4.7) ohms
- R42—4.64 (4.7 or 5) ohms, 10 watts

Capacitors

- C1—10 μ F, Mylar film
- C2—220 pF, ceramic disc
- C3, C4, C11—150 pF, ceramic disc
- C5—220 μ F, 63 volts, electrolytic

- C6—8 pF, ceramic disc
- C7—0.1 μ F, 50 volts ceramic disc
- C8, C9—0.1 μ F, 100 volts, ceramic disc
- C10—1500 pF, 50 volts, ceramic disc
- C12—C15—100 μ F, 100 volts, electrolytic
- C16, C17—25,000 μ F, 75 volts, electrolytic (Sprague 253G075CF2A or similar)

Semiconductors

- Q1—Q4—2N5210
- Q5—Q8—2N5087
- Q9—ECG289A
- Q10—ECG290A
- Q11, Q12, Q17, Q18—ECG129
- Q13—Q16—ECG128
- Q19—ECG373
- Q20—ECG374
- Q21—Q24—IRF9630
- Q25—Q28—IRF630
- Q29—ECG123AP
- BR1—25 amps, 400 PIV bridge rectifier
- D1, D2—1N4148
- D3—D5—1N4002
- D6, D7, D21—1N4735A 6.2 volts, 1 watt, Zener
- D8—D11, D23—1N4750A 27 volts, 1 watt, Zener
- D12, D13—1N4737A, 7.5 volts, 1 watt Zener
- D14, D15—1N4738A 8.2 volts, 1 watt Zener

- D16—1N4728A 3.3 volts, 1 watt Zener

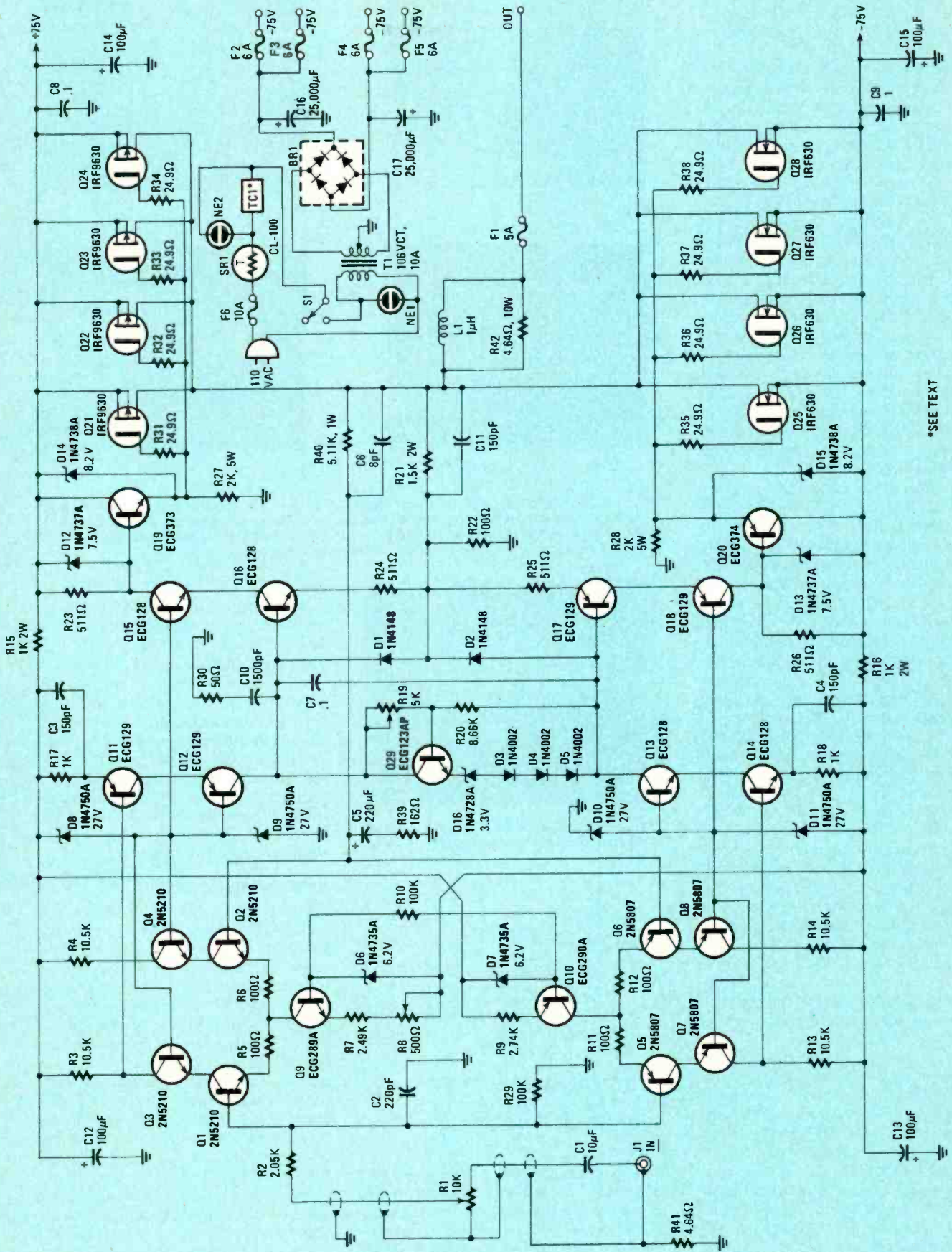
Other components

- L1—1 μ H (15 turns of No. 16 wire wound on R42—see text)
- NE1, NE2—Neon bulbs, 110 volts
- F1—5 amps, fast-blow fuse
- F2—F5—6 amps, fast-blow fuse
- F6—10 amps, fast-blow fuse
- T1—106 volts, center-tapped power transformer
- S1—SPST power switch
- J1—Phono jack for input

Miscellaneous

Heat Sinks, Wakefield 512 series, 2x7 inches or equivalent; TO-5 heat sinks for Q12, Q13, Q15, and Q18; chassis; handles; fuse holders; capacitor clamps; power cord; input jacks; binding posts; wire; hardware; insulators, etc.

The following items are available from A&T Labs, Box 552, Warrenville, Illinois, 60555: Etched, drilled, plated-through PC boards, \$22 each; Power transformer, \$69 each; Set of 8 matched power FET's, \$66; Drilled heatsink (type 512), \$27. Add 5% shipping and handling, 12% for transformer. Illinois residents include 5 1/4% sales tax.



*SEE TEXT

FIG. 2—AMPLIFIER SCHEMATIC for one channel. The power supply shown is sufficient for two channels. While not necessary for home use, the optional thermal cut-out device and inrush limiter shown should be used, for example, in a disco.

would make the stage operate far less efficiently.) The relatively high gate-capacitance of the power MOSFET's is also somewhat easier to drive in the common-source configuration.

Resistors R31 through R38 help to suppress the parasitic oscillations that might otherwise occur with the extremely fast transistors used. Zener diodes D14 and D15 limit the amount of drive available to the output. Finally, L1 and R42 serve to isolate the amplifier output from capacitive loads at very high frequencies.

The inverter/driver stage consists of Q15 through Q20. Its purpose is to deliver bias and drive signals to the FET output stage. Their basic requirement is to sit at about 3.5 volts with respect to the source, increasing about .3 volt per ampere of output current. Transistor Q29 forms a conventional voltage multiplier, which, in this case, multiplies the voltage across D3, D4, and D5 and D16 to about 7 volts. The 7-volt bias is presented to the bases of Q16 and Q17, which form the bottom transistors of a pair of complementary cascode amplifiers.

An output-stage gain of 10 is set by R21, R22, R25, and R26. Therefore, the voltage generated by Q29 is split in half and reflected up against the two supply rails as a pair of bias voltages across R23 and R26. Those voltages, along with the AC drive-signals from the previous stage, are passed along to emitter followers Q19 and Q20, which have the high-current drive capacity required by the gate capacitance of the output devices. Using cascode stages here, as well as in the input and voltage-gain sections, serves the dual purpose of splitting the emitter-collector voltage and power drops among two transistors per rail, while increasing the open-loop frequency response of the amplifier.

The voltage-gain stage consists of transistors Q11 through Q14, again configured as complementary cascode amplifiers. The collector loads for Q12 and Q13 are essentially the input impedance of Q16 and Q17. That is in the neighborhood of 50K, leading to a stage gain of about 50 (the quotient of 50K and R17 or R18). Capacitors C3 and C4 increase the frequency response of the stage. Zener diodes D8, D9, D10 and D11 set the base voltages for the upper transistors in the cascodes.

Now we'll look at the input stage, which consists of Q1 through Q8. Those transistors are connected as complementary-cascode differential amplifiers, supplied by current-sources Q9 and Q10. The gain is set at about 100 by the ratios of R3 to R5 and R13 to R11.

Resistor R8 is used to zero the output voltage by varying the collector currents of Q1-Q4, compensating for any V_{BE} offsets that may exist in Q1, Q2, Q5, and Q6. That is important, because with an extremely low output-impedance such as

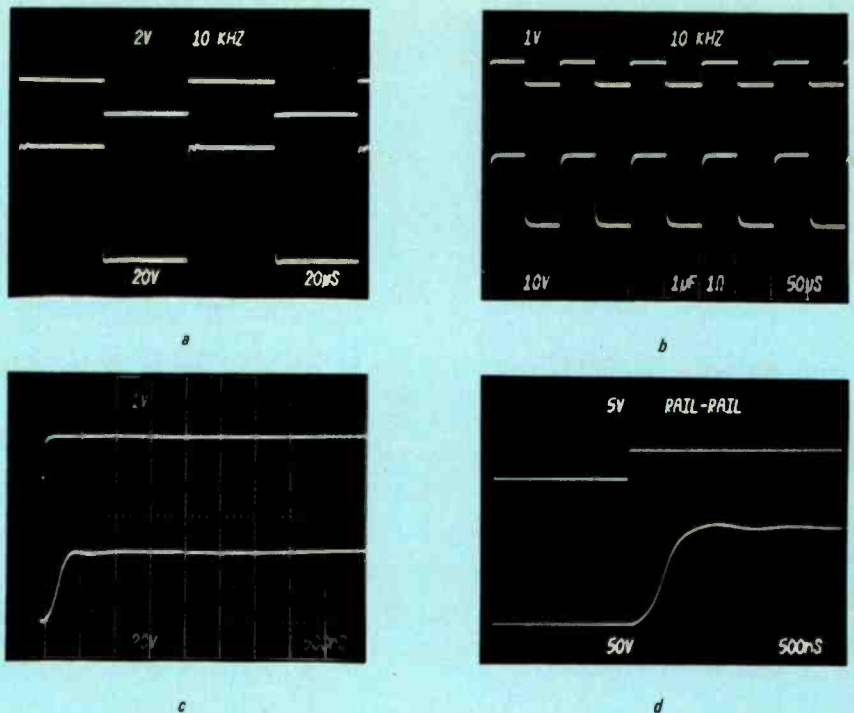


FIG. 3—AMPLIFIER RESPONSE CHARACTERISTICS. A shows the response to a 10-kHz squarewave input at 150 watts into an 8-ohm load, while b shows the response into a 1-ohm, 1- μ F load. Shown in c and d are the step responses at 50 watts and full output, respectively (both with input filter C2 removed). Note the excellent slew-rate and risetime capabilities.

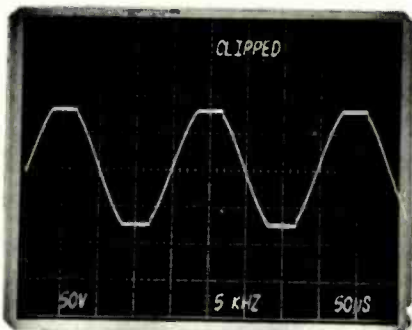


FIG. 4—FULL-POWER OUTPUT with a 5-kHz sinewave input. Note the clipping level is about ± 75 volts.

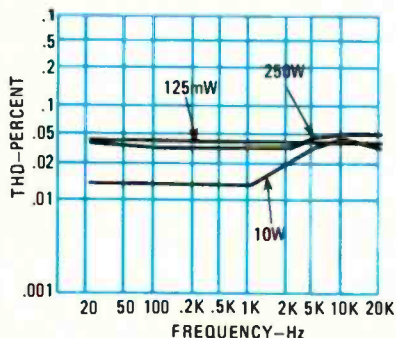


FIG. 5—TOTAL HARMONIC DISTORTION (THD) at 1 kHz.

this amplifier has, even very low output offsets (in the tens of millivolts) can deliver many amps into a short.

The overall voltage-gain of the amplifier is set at about 30 by the ratio of R40 to R39. A 3-dB rolloff is set at about 3 Hz by C5. High-frequency compensation is

provided by C10, R30, C6, and C11.

Some optional components are shown in the schematic, notably in the power-supply section. First, there is TC1, the thermal cutout made by Elmwood sensors (1655 Elmwood Ave., Cranston, RI 02907). It is normally closed, and opens at 70°C. Another optional component is SR1, an inrush limiter made by Keystone (Thermistor Div., St Marys, PA 15857). For home applications, those shouldn't be necessary. However, if you plan to run the amplifier continuously at high power (in a disco, for example), you should include all the protection you can.

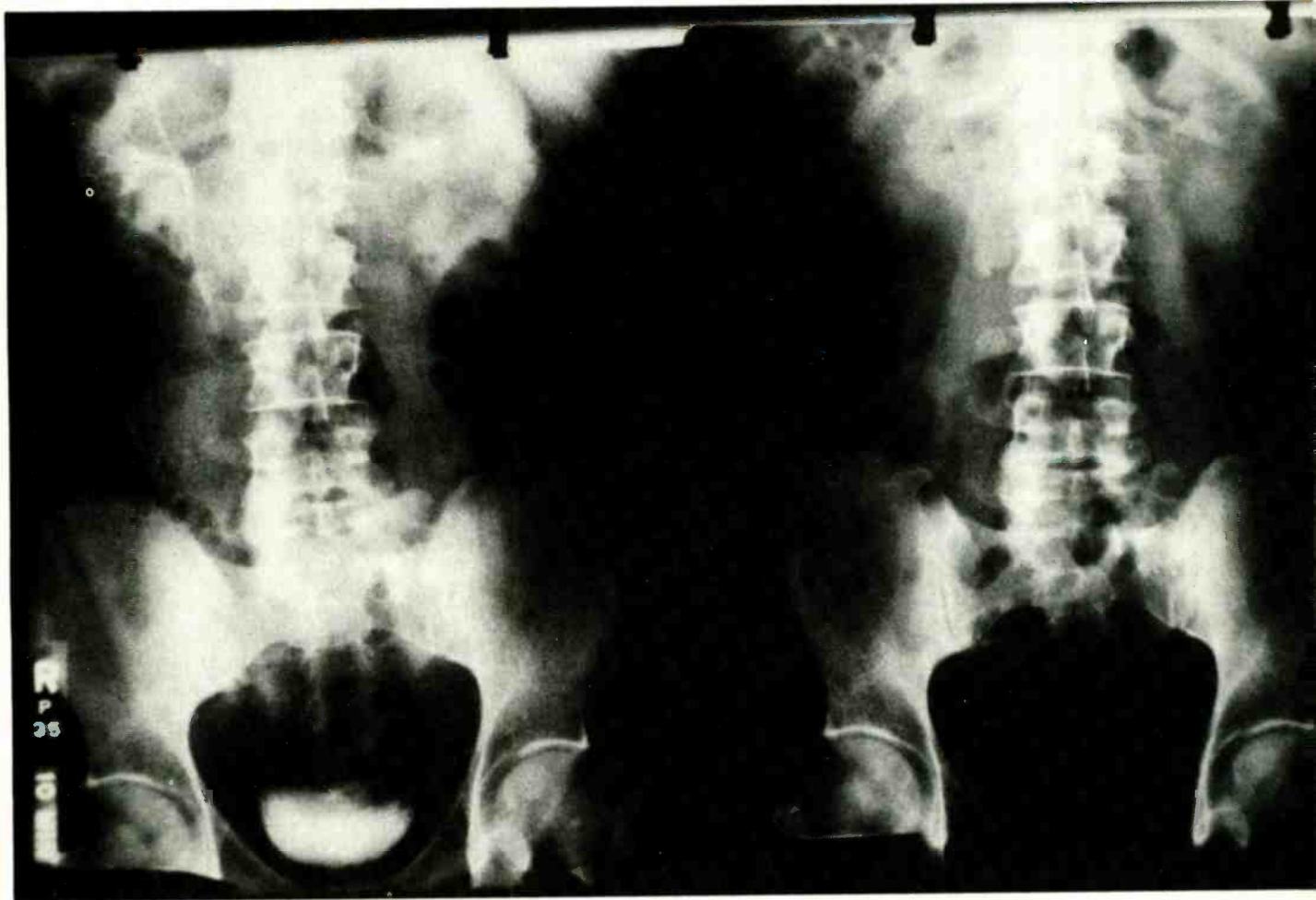
Amplifier performance

Some of the response characteristics of the amplifier are shown in the oscilloscope photographs in Fig. 3. For example, in Fig. 3-a we see the response to a 10-kHz squarewave at 150 watts into 8 ohms. Figure 3-b shows the response with a 1-ohm, 1- μ F load. Figures 3-c and 3-d show the step response at 50 watts and full output, respectively. (Those two risetime tests were made with input-filter capacitor C2 removed.) Figure 4 shows the full-power output with a 5-kHz sinewave input. Figure 5 shows the total harmonic distortion from less than 1 watt to 250 watts at 1 kHz.

Unfortunately, that's all we have room for this time. When we continue, we'll show you how to build the amplifier and provide the foil patterns that are essential for the successful completion of the project.

R-E

Electronics In Medical Imaging



A look at three advanced medical-imaging techniques and the role that electronics plays in them.

RAYMOND M. FISH, Ph.D., M.D.

Part 2 IN OCTOBER'S ISSUE, we explained the principles of X-ray, conventional, and computerized tomography, fluoroscopy, digital subtraction angiography, and ultrasound. This month we'll turn our attention to three other valuable medical-imaging techniques—those are nuclear medicine, nuclear magnetic resonance, and positron emission tomography.

Nuclear medicine has been in clinical use for several decades, in contrast to nuclear magnetic resonance (NMR) and positron emission tomography (PET). NMR and PET are not in general use in all parts of the country, but they do hold out the promise of improved medical care in the future.

Nuclear medicine

In nuclear medicine, a radioactive substance is put in the body. Which particular substance is used depends upon which part of the body is being examined; that's because different parts of the body absorb different radioactive materials differently. The resulting radiation can then be measured and imaged electronically. Arrays of sensitive radiation detectors are used so that the patient is exposed to as little radiation as possible. If the radiation is to be taken up by a tumor, larger amounts of radioactive material may be given in an attempt to selectively destroy the cancer.

The radioactive materials are called radioisotopes or radionuclides. Those substances are radioactive varieties of

normally stable elements. The radioactive form of the element is unstable and emits radiation such as alpha, beta, or gamma rays. Most radioisotopes used in medical imaging emit gamma rays.

The radioactive substance may be given to a patient by mouth, intravenously, or by inhalation (breathing), depending on the test being done. The material travels to a site in the body that selectively absorbs it. A scan is then performed to image the organ or tissue that has absorbed the radioactive substance.

A nuclear medicine scan can be performed by one or more radiation detectors that move across the body over a period of several minutes or by a stationary array of detectors. The radiation detected at each

point near the patient is measured and stored in a computer memory. When the entire area of interest has been scanned, a composite picture of radiation intensity is produced electronically. Today most nuclear medicine imaging is done with gamma or scintillation (light-producing) detectors using a fixed array of detectors. When scintillation detectors are used, the light from the detectors can produce a photographic image directly, eliminating the need for a computer.

In the body, different tissues and organs selectively absorb and concentrate different radioactive materials. For example, in the thyroid, iodine is normally selectively absorbed and concentrated. Radioactive I-131 is similarly concentrated in the thyroid. Tumors and other abnormal areas in the thyroid will absorb more or less of the radioactive material, depending on the function of the abnormal tissue. When scanned and imaged, valuable diagnostic information about the abnormal thyroid tissue can be obtained. A thyroid scan is shown in Fig. 1.

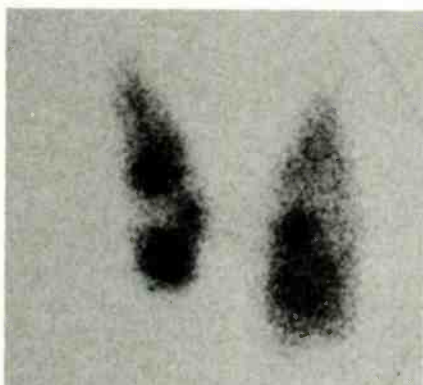


FIG. 1—A THYROID SCAN. Note the areas of increased and decreased radioactive iodine concentration.

Some isotopes are substituted for another element of similar chemical properties. For example, strontium 85 is taken up in sites of active bone formation in place of calcium. There are several reasons why one would want to be able to image new bone formation. For instance, some tumors cause the breakdown and reformation of bone and some fractures cannot be seen with usual X-rays, but new bone formation occurs at the fracture site. Figure 2 shows a bone scan made with technetium-99m pyrophosphate, a substance that has replaced strontium in clinical use.

Certain cells in the liver and spleen are responsible for clearing waste substances from the blood; those cells form the reticuloendothelial system. Those cells will selectively ingest radioactive substances such as technetium labeled colloid. As the reticuloendothelial cells are fairly well distributed throughout the liver and spleen, imaging the liver and spleen will detect areas that are being replaced by abnormal material such as tumors, infec-

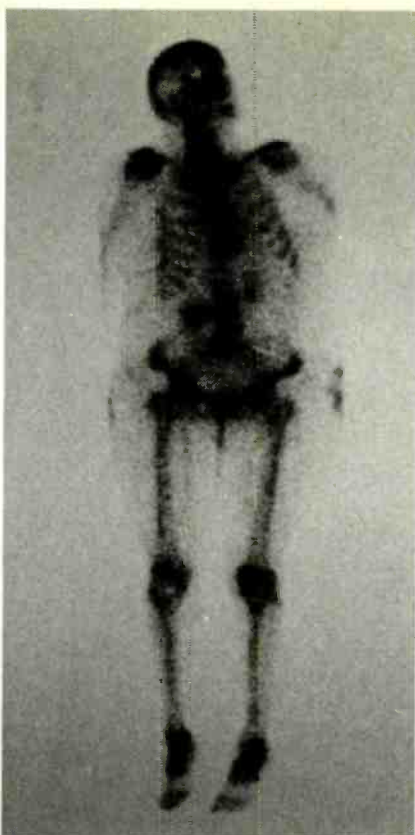


FIG. 2—A BONE SCAN. Such a scan can sometimes show information that is missed on standard X-rays.

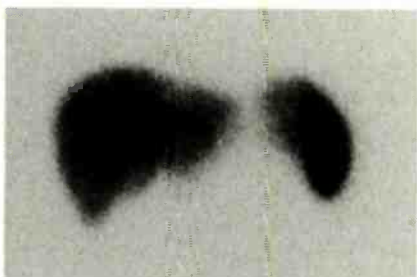


FIG. 3—A LIVER-SPLEEN SCAN. If the proper radioactive substance is used, it is easy to spot any areas that are abnormal. This scan shows a normal liver and spleen.

tions, or blood clots following injury. Figure 3 shows a normal liver-spleen scan.

About 10% of the technetium-99m sulfur colloid particles used for imaging the liver and spleen go to the bone marrow. A scan showing a decrease in the normal uptake of radioactivity in the bone marrow would indicate a tumor or other abnormality in the area.

The lungs can be imaged by having the person inhale radioactive material or by injecting radioactive material into the bloodstream. In the first case, the inhalation scan, radioactivity is evenly distributed throughout the lung unless the airway is blocked. In the second method, the perfusion scan, radioactivity is distributed throughout the lung everywhere except where circulation of blood is blocked. There are many diseases,

however, where either or neither method will work because the airway, the circulatory system, or both, are blocked. For example, swallowing a foreign body may just block the airway. A blood clot to the lungs would interrupt just circulation. Pneumonia or a slowly growing tumor would tend to block both.

Technetium 99-m derivatives can be used to scan the brain. They are injected into a vein and travel to areas of the brain where blood circulation is normal. That is helpful in detecting tumors, lack of circulation, collections of blood, and infection. That technique has limitations, however, because tumors normally would have to be at least one centimeter in diameter if they are to be seen. Thus, brain scans are used relatively infrequently these days.

To image the living heart, two radioactive substances are commonly used: thallium-201 and technetium-99m. Thallium is picked up by muscle in which circulation is normal. Technetium-99m, when bound to albumin, remains in the blood and permits the movement of larger amounts of blood to be observed. Thus, thallium will show blood flow in the heart muscle itself, something that is often disturbed by coronary artery disease or a myocardial infarction (heart attack). Any decrease in heart-muscle blood supply (coronary artery perfusion), whether to the entire heart or just to a localized area, can be observed. The scan can be performed during or after exercise to show partial coronary artery blockages.

Nuclear magnetic resonance

Nuclear magnetic resonance (NMR) was discovered in 1946 and has been used since then in chemistry and physics to identify and determine the structure of molecules. The first two-dimensional NMR images were made in the early 1970's.

For medical applications, the molecular structure of tissues determines the NMR image that is formed. Blood flow in the area also plays a part in determining the image seen in an NMR scan. The primary advantage of the technique is that structures and phenomenon that would not show well on X-ray or computerized tomography will often be seen by an NMR scan. Such structures include certain tumors, inflamed tissue, and changes caused by the amount of metabolism (energy usage) of tissue.

Another advantage of NMR is that it uses no ionizing radiation. Instead, NMR imaging depends on the behavior of molecules in mixed magnetic and RF fields. Atomic nuclei with an odd number of protons or neutrons possess spin. Because of that, those nuclei have a small magnetic field. Thus, the nuclei can be thought of as spinning electrical charges that generate magnetic fields.

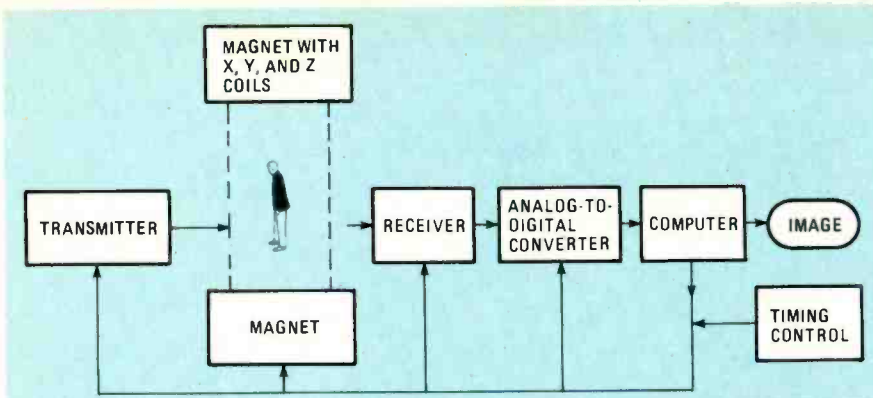


FIG. 4—IMAGING SYSTEM used to perform a nuclear magnetic resonance (NMR) scan. To obtain a three-dimensional image, the scanning is done by varying a magnetic field and analyzing the received RF signals that result.

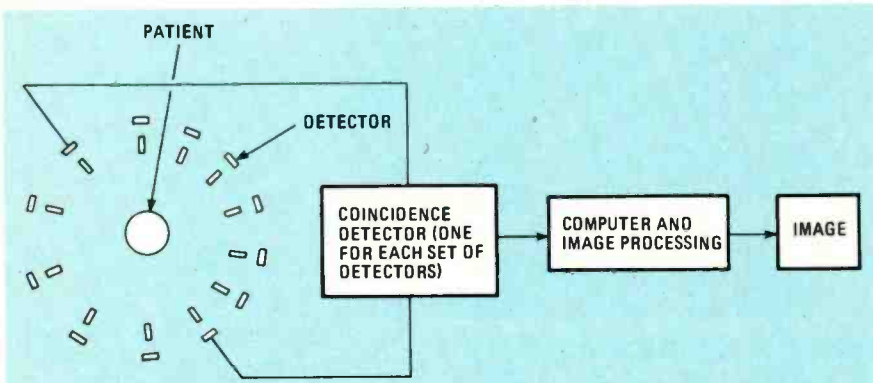


FIG. 5—POSITRON emission tomography (PET) scanning. Coincidence detectors, spaced 180° apart, detect when a positron and electron collide, creating two gamma rays that are emitted in opposite directions (180° apart). From those emissions, using computer techniques, an image of a positron-emitting region can be produced.

When placed in an externally applied static magnetic field, a force is exerted on the nuclei because of the interaction of the two magnetic fields. That force tends to align the nuclei with the applied field. The nuclei will rotate about the field direction (precess) at a frequency that depends on the strength of the applied magnetic field. That frequency is called the precession frequency. If an alternating radio-frequency field at the precession frequency is superimposed on the magnetic field, the nuclei will absorb energy from the RF field.

The nuclei in the magnetic field absorb energy only if the RF field is at a discrete resonant frequency. At that resonant frequency, the magnetic moments of the nuclei become aligned against the applied static magnetic field. The resonant frequency is determined by the chemical composition of the tissue that is being examined.

When the RF field is removed, the nuclei in the excited state revert to the more stable state and emit RF energy. The amount of time it takes for the nuclei to return to their stable state (relaxation time), varies depending on the chemical composition of the tissue. For instance, some cancer cells have longer relaxation times than normal cells. Using computer

techniques, those relaxation times can be used to generate an image (see Fig. 4).

To obtain an image, spatial information must be obtained. That is accomplished by several methods. One involves varying the magnetic field with position. That, in turn, causes the resonant frequency to vary with position. To obtain images in three dimensions, sequences of different magnetic field pulses are used, usually applied along x, y, and z axes. To image a thin cross section of tissue, an RF field perpendicular to the plane of the slice is used.

It is difficult to produce the required

magnetic fields because they must be several thousand times stronger than the earth's magnetic field (the stronger the field the better the image) and large enough to enclose a human body. Thus, NMR machines are sure to be expensive.

Even so, the technique is promising and useful. For instance, NMR is capable in some cases of detecting brain tumors and changes due to multiple sclerosis that were not seen by a CAT scan.

Positron emission tomography

Positron emission tomography (PET) involves the use of isotopes that decay by emitting positrons. The isotopes include fluorine-18, oxygen-15, nitrogen-13, and carbon-11. Those isotopes are attached to metabolically active compounds. The compounds are taken up at certain areas in the body, depending on the functioning of the body.

When an isotope emits a positron, the positron collides with a nearby electron, destroying both but causing two gamma rays to be emitted; those rays travel in opposite (180° apart) directions.

An array of detectors around the person is used to detect those gamma-ray emissions (see Fig. 5). Typically 50 such detectors are used; those are rotated about the patient. Computer techniques are then used to reconstruct images of the radiation-emitting areas.

One of the first metabolically active compounds used in PET scanning was 2 deoxy-D-glucose (2 DG). That chemical is transported through the blood/brain barrier and is used as a source of energy by the brain. By bonding a positron-emitting isotope to that chemical, various areas of the brain can be imaged and the effects of drugs, disease, or mental disorder can be observed. Similarly, other metabolically active compounds are used to study other organs and tissues in the body.

The advantages of PET and NMR is that those techniques can produce images based in part upon the chemical makeup and functioning of the body. In contrast, most X-rays show only the structure of the body. New uses for PET and NMR are still being developed.

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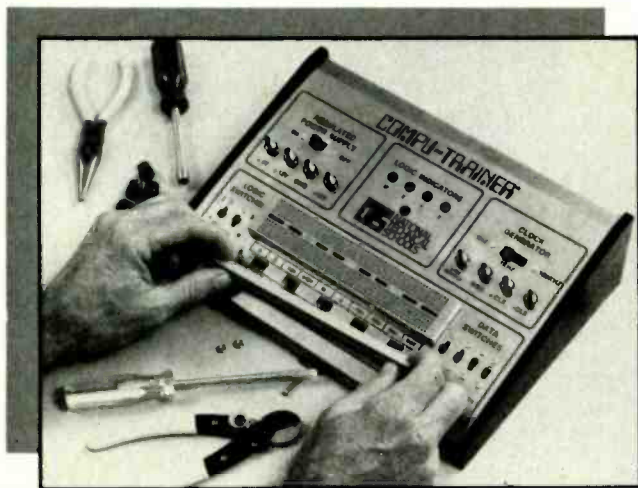
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Bob Lucas calls the SK Guide's Cross Reference Directory "a very important reference." He points out that even without a schematic diagram, a technician can find a suitable replacement for a defective part just by cross-referencing a part number. (2,300 RCA SK devices replace over 193,000 industry types.)

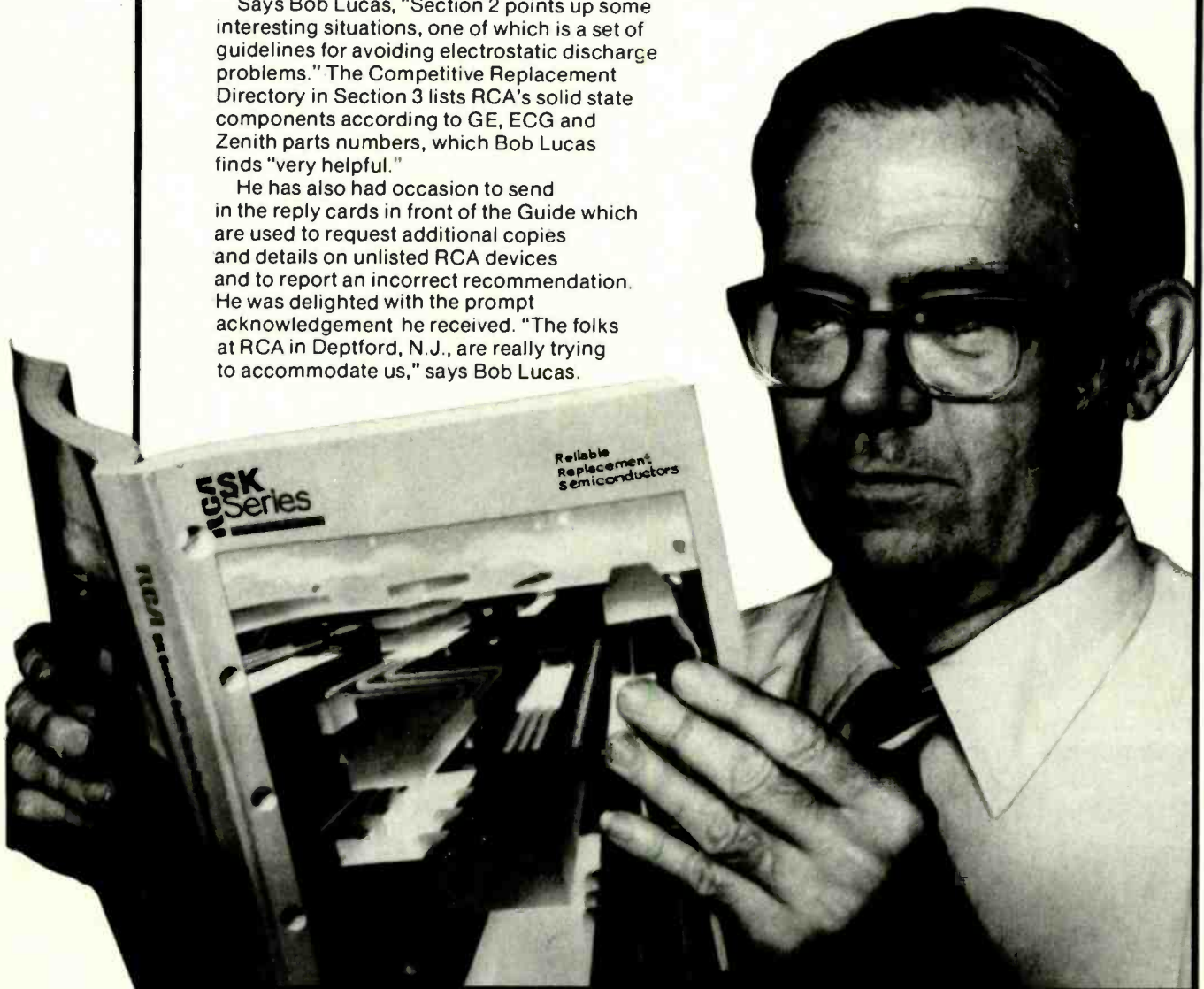
Says Bob Lucas, "Section 2 points up some interesting situations, one of which is a set of guidelines for avoiding electrostatic discharge problems." The Competitive Replacement Directory in Section 3 lists RCA's solid state components according to GE, ECG and Zenith parts numbers, which Bob Lucas finds "very helpful."

He has also had occasion to send in the reply cards in front of the Guide which are used to request additional copies and details on unlisted RCA devices and to report an incorrect recommendation. He was delighted with the prompt acknowledgement he received. "The folks at RCA in Deptford, N.J., are really trying to accommodate us," says Bob Lucas.

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Video
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Flat Panel Color TV

A practical flat-panel color display has long been a dream. Now, thanks to a recent breakthrough, that dream has come true. Here's a look at that breakthrough, and the revolutionary TV that makes use of it.

CARL LARON, ASSOCIATE EDITOR

MOST READERS OF RADIO-ELECTRONICS are familiar with the first generation of flat-panel LCD-TV's that began appearing during the past year. While they represented a significant step forward in technology, they left a bit to be desired in terms of performance. Among other things, those displays suffered from blurring; images seemed to flow across the screen, leaving comet-like trails behind. Also, up to now, the displays were available in black-and-white versions only.

Those drawbacks have been eliminated, however, in a new development recently announced by Epson (23530 Hawthorne Blvd., Suite 100; Torrance, CA 90505). That development is a flat-panel, color, liquid-crystal display with a very fast response time. In fact, despite its lower resolution, the quality of the picture that can be produced by the Epson display is comparable to that of a CRT.

A flat-panel display

In the CRT that we are all familiar with, the picture is created by sweeping an electron beam across a phosphor-coated screen in response to a video signal. In the

display developed by Epson, on the other hand, the picture is generated by rows of pixels (picture elements). Each pixel is switched on and off by a microscopic thin-film transistor. The pixels in the Epson display are not phosphors, however, but are liquid crystals.

Liquid crystals are long organic molecules with the optical properties of both liquids and solids. In the display, the liquid-crystal material is sandwiched between two polarizers whose transmission axes are orthogonal (separated by 90 degrees) to each other. When no electric field is present, the condition shown in Fig. 1-a, the liquid crystal molecules are arranged so that the one nearest the front polarizer is parallel to that polarizer's transmission axis, and the one nearest the rear polarizer is parallel to that polarizer's transmission axis. The successive layers of molecules twist gradually through the 90 degrees between the front and rear polarizers. Light that enters through the rear polarizer is twisted 90 degrees by the liquid crystal molecules and passes out the front polarizer.

But when an electric field is present, as

shown in Fig. 1-b, the molecules stand on end, parallel to the electric field. Since then the light is no longer twisted, light that passes through the rear polarizer is absorbed by the front polarizer.

Before a successful liquid-crystal display could be created, some relatively difficult technical problems needed to be solved. For one thing, conventional liquid crystals, the kind used in watch and calculator displays, switch relatively slowly. (By switch, we mean change from their twisted to their untwisted orientation when an electric field is applied, and back again when it is removed.) That problem was solved through the development of a liquid-crystal that reacted faster to the presence or absence of an electric field.

Incidentally, the blurring that is a common problem of earlier LCD-TV displays is caused by slow switching times; Epson's display switches fast enough to totally eliminate such blurring.

Other significant problems were the low contrast of liquid-crystal displays and the fact that most were capable of only producing dark images on a light background or light images on a dark back-

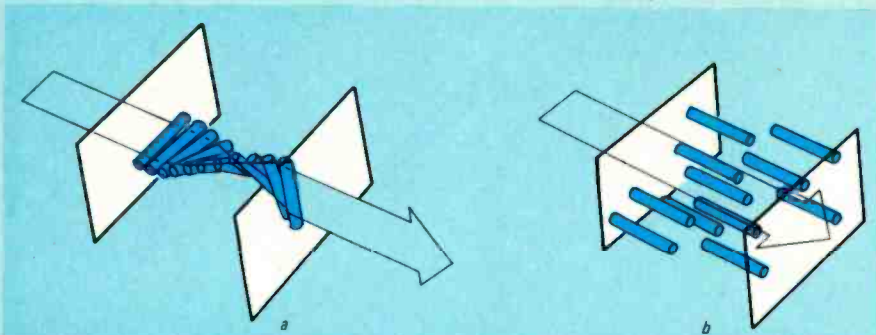


FIG. 1—WHEN NO ELECTRIC FIELD is present, the liquid-crystal molecules twist the light 90 degrees, thus allowing it to pass through the front polarizer as shown in a. When an electric field is applied, the molecules no longer twist the light so that the light is absorbed by the front polarizer as shown in b.

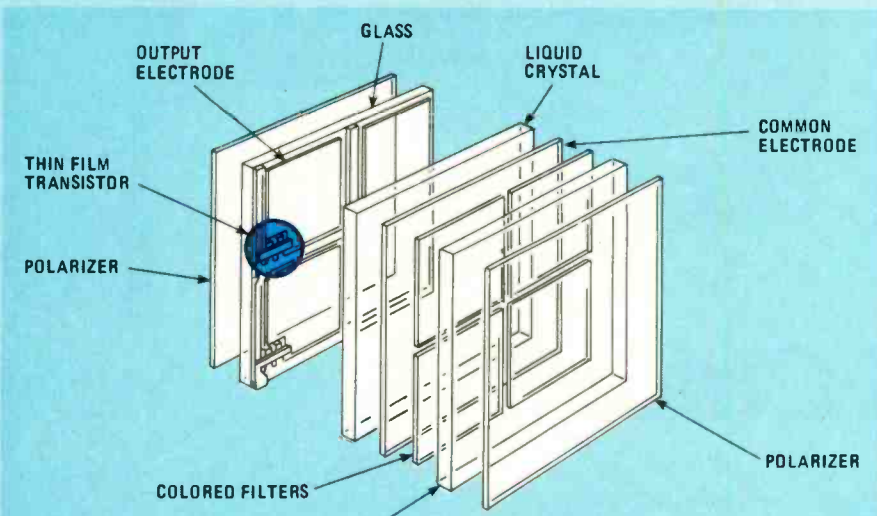


FIG. 2—THE EPSON DISPLAY consists of a rear horizontal polarizer, liquid-crystal cell, and front vertical polarizer. The electric field is applied using a unique system consisting of thin-film transistors and a common electrode.

ground.

The solutions

Prior to the development of Epson's display, multiplexing was used in liquid-crystal display devices to control the thousands of pixels needed to generate an image. In multiplexing, rows of electrodes are placed on one side of the liquid crystal, while columns of electrodes are placed on the other; the junctions where the rows and columns crossed would correspond to a pixel.

To turn on a pixel, control pulses would be fed in rapid succession to each row. Those pulses would turn on selected electrodes in that row. Meanwhile, all of the column electrodes would be pulsed simultaneously. While the voltage generated by the column electrodes would be insufficient to affect the liquid crystal molecules, when the column and selected-row electrodes are both pulsed, the voltage level is sufficient to effect the liquid crystal molecules and they respond.

That technique has a serious drawback—poor contrast. The reason for it is that the time-weighted average on-off voltage ratio is very low, which means that

the difference between the black and white levels is not very great.

Epson's solution to that problem is a technique called "active-matrix addressing." In it, the 240 row and 220 column electrodes are all placed on a single glass substrate. On the opposite side of the display is a common electrode.

At each row and column junction, a Thin Film Transistor (TFT) is located. Those transistors, made from polycrystalline silicon, turn on whenever a pixel is to be activated. Which pixels are to be turned on is controlled by the driver circuitry of the device. Through the use of TFT's, each pixel receives the full voltage required for turn-on. As that voltage is no longer a time-weighted average, the on-off ratio is much higher than in multiplexed devices, resulting in good contrast levels. A diagram of Epson's LCD system is shown in Fig. 2.

Adding color

Once the problem of devising a suitable monochrome display was solved, the next step was the addition of color. The approach taken was not unlike that used in conventional color CRT's. In those, the

color image is created by selectively exciting red, blue, and/or green phosphors arranged in a tight matrix.

In the Epson system, color is created through the use of color filters. Tiny red, blue, and green filters are placed in a tight matrix pattern, and the entire arrangement is placed in front of the LCD. The matrix is arranged so that one of the colored filters is placed in front of each TFT (pixel).

Let's see how the system works. If, for instance, a red area is to be created, the TFT's at the blue and green filters are turned on, preventing light from passing through them. In the meantime, light continues to pass freely through the red filter. Conversely, if blue is desired, the TFT's at the red and green filters are turned on; if green is desired, the TFT's at the blue and red filters are turned on.

Colors can, of course, be combined to produce others. White is created by turning off all of the pixels in an area, thus allowing all of the colors through. Black is created by turning on all of the pixels, thus blocking all light. A full gamut of other colors and shades (see Fig. 3) can be created by selectively turning on or off the various pixels in a region.

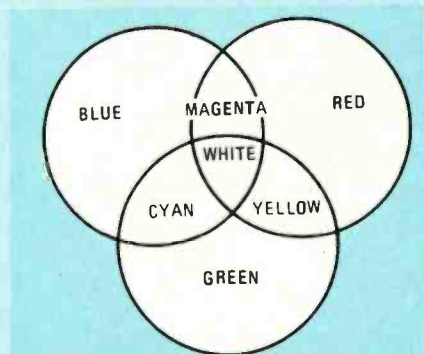


FIG. 3—A WIDE VARIETY OF COLORS and shades can be created using various combinations of red, green, and blue.

The Elf

Epson's first application of its new technology is its *Elf* flat-screen TV (see Fig. 4). According to the manufacturer, that tiny color TV should be on store shelves by the time you read this.

The Epson *Elf* is almost transistor-radio sized, measuring 3.15 x 6.3 x 1.22 inches, and weighs just 1.1 pounds. The set features a 2-inch, diagonal-measured screen. The heart of the device is the new flat-panel LCD unit, which is shown in Fig 5 and described above.

The tiny TV can be powered from any one of three power sources. Those are either standard or rechargeable "AAA"-sized cells, an AC power adaptor, or a car-battery adaptor.

Among the user controls are TINT, COLOR, and BRIGHTNESS. All VHF and UHF TV channels can be received, and

Video Entertainment



FIG. 4—THE EPSON ELF is as small as a paperback book, weighs just over one pound, and can operate indoors or out. It makes use of Epson's flat-screen color liquid-crystal display.

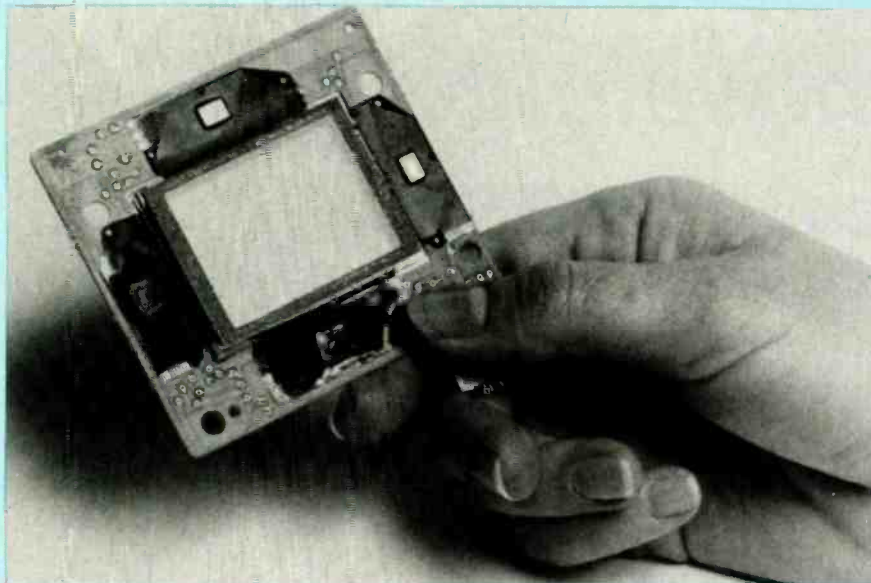


FIG. 5—THIS FLAT-SCREEN color liquid-crystal display is the heart of Epson's new *Elf* pocket-sized TV.

channel selection is done via a slide-rule type tuner. There is also an earphone jack that allows the use of a standard earphone or mono headset for private viewing.

When used outdoors, conventional TV's are faced with the problem of poor contrast due to the high ambient light levels. But because the *Elf* uses a backlit display, a unique feature turns the tables on that troublesome problem. The rear of the unit can be opened, allowing the sun's rays to be used as the light source for the backlit LCD. That greatly improves viewing in outdoor settings. When the back is opened, a switch allows you to turn off the set's internal light source (it's no longer needed) to conserve batteries.

The *Elf* comes with a number of standard accessories. Those include an AC

adaptor, mini-earphone, handstrap, soft carrying case, and a 27-inch telescopic antenna. Optional accessories include car-battery adaptor and a rechargeable battery pack. There is also a fold-out tilt stand in the rear.

After spending some time with the unit, our overall impressions of it are very favorable. This set has advanced the state-of-the-art of LCD imaging manifold. The picture produced is far better than those produced by previous LCD devices. The addition of color is also a major step forward.

In fairness, however, we must point out that the image is nowhere near as sharp as that produced by a comparable-sized CRT display. That reduced resolution is, of course, caused by the fact that far fewer

pixels are used to create the image in the LCD. Even so, the image was extremely watchable. The color reproduction was true and the contrast level was acceptable for viewing even in a brightly lit office.

Other aspects of the set are pretty much what you would expect in a set of this type. Sound quality is definitely not "hi-fi," but it is adequate. The level of the audio is quite sufficient for personal listening in all but the noisiest environments. For those, you would want to use an earphone or a headset anyway. Although we tried the unit out in the "concrete canyons" of Manhattan, with all of the reception problems that that entails, the overall quality of the picture and sound was good on all receiveable VHF and UHF channels. There were a few "birdies" (spurious signals) generated by the unit when tuning between the high and low VHF bands, but those were inconsequential.

Whenever a product makes use of a technological breakthrough, you would expect the initial price to be high. The Epson *Elf* is no exception. The suggested list price of the unit at the time of this writing was \$500. As with any other new technology, however, expect prices to fall as more units are sold and the costs of production go down.

The size of the display used in the *Elf* was not selected primarily because of the current popularity of small-screen personal TV's. The cost of the display is directly related to its size. Thus, although a set with a somewhat larger display (up to about 5-inches) is within the current technology, the cost of such a display would make the set too expensive to market practically at the present time.

Eventually, of course, those costs, too, will come down. Once they do, the applications for the Epson display are almost limitless. Indeed, company researchers are looking at a number of future products, including a flat-panel liquid-crystal TV that could be hung on a wall like a picture. While such a set is still many years away, the development of products like the *Elf* have brought it a little closer to realization.

R-E



Lightweight Video Cameras

Confused about the new lightweight cameras? Here's a guide that will help you sort things out.

CARL LARON, ASSOCIATE EDITOR

A GREAT DEAL OF ATTENTION HAS BEEN focused of late on the coming of the camcorder. While those one-piece video-camera/videocassette-recorder combinations offer the consumer a great deal of convenience, they force a trade-off in terms of versatility. Some require a separate deck for playback, others require the use of limited-length tapes. As for the 8mm camcorders, the future of the standard they use is very much in doubt.

There is another choice for those seeking a lightweight alternative. That is a combination consisting of a lightweight (typically 5 to 8 pounds without battery) portable VCR and one of the new generation of ultra-lightweight cameras. In this article we are going to take a close look at that new generation of cameras.

Miniaturizing video camera

Manufacturers have taken many different routes to arrive at today's downsized portable video camera, but the key technological difference between cameras is the type of pickup they use—either tube or solid-state.

Most cameras still use tube-type pickups such as the Saticon, Newvicon, etc. The difference in the new cameras is the

size of the pickups. Earlier cameras used 1- and $\frac{3}{8}$ -inch tubes; the new generation of cameras use $\frac{1}{2}$ -inch and even $\frac{1}{4}$ -inch tubes. That reduction in size translates into a considerable reduction in overall camera size and weight as the pickup is the largest and heaviest component in a tube-pickup camera.

One possible drawback to using a smaller pickup is that the smaller the tube the poorer the horizontal resolution. Horizontal resolution is a specification that refers to the number of horizontal lines that the camera uses to create its image. The fewer the lines, the poorer the resolution (or sharpness) of the picture. It is important to note that even the best videocassette recorders are capable of horizontal resolutions of only 250 lines or so. However, most video cameras, even those with the smallest pickups, offer resolutions that are that high or better. That means that, at least as far as home video is concerned, the limiting factor on resolution is the recorder, not the camera.

Figure 1 shows a block diagram of the signal-processing circuitry of a popular tube-pickup video camera, JVC's GX-N7. As is shown, the signal from the pickup is filtered and separated into luminance

(Y) and chrominance (R - Y) and (B - Y) signals. Those signals are then combined to form an NTSC-compatible output.

Also shown in Fig. 1 is a block diagram of JVC's *Auto Color Tracking System*; that is an automatic white-balance system. Just to backtrack a little for those who may not be familiar with the purpose of such a system, a camera's ability to reproduce colors is strongly affected by the type of light it is used in (indoor vs. outdoor, etc.). Video cameras use a variety of schemes to compensate for that. Some use switch-selectable presets to choose between indoor/outdoor and/or cloudy/sunny conditions. Often when presets are used, a variable WHITE-BALANCE control is provided for "fine tuning." In more advanced cameras, white balance is adjusted automatically. In some, all you need do is point the camera at a white surface, press an automatic white balance switch, and the camera takes care of the rest. It is important in those systems to be sure to go through that procedure any time the ambient light changes.

In the newest of cameras, such as the JVC unit, depressing a switch is not nec-

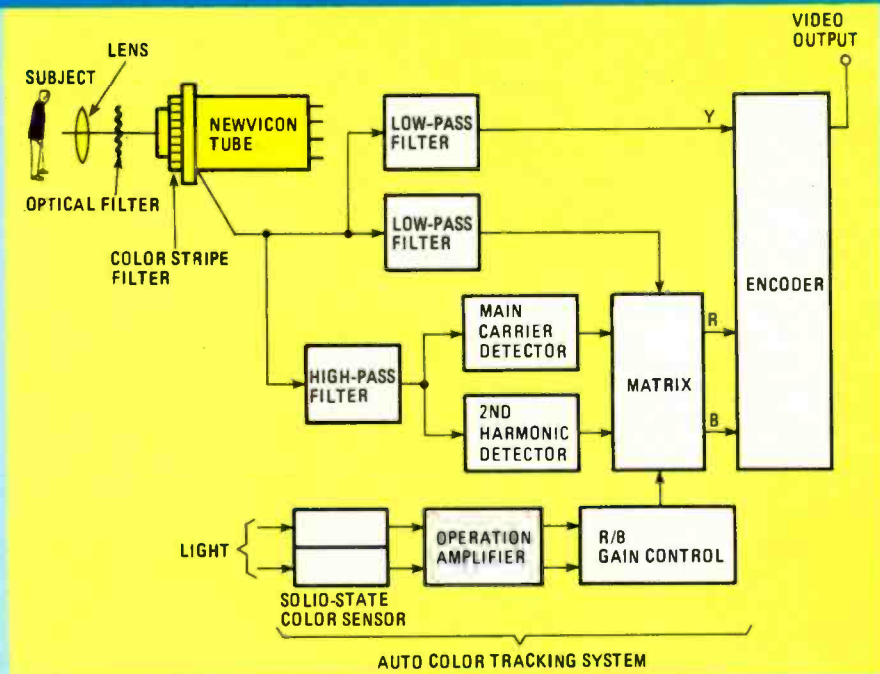


FIG. 1—THE JVC GX-N7. Analog signal processing is used to derive the luminance (Y) and chrominance (R - Y and B - Y) signals.

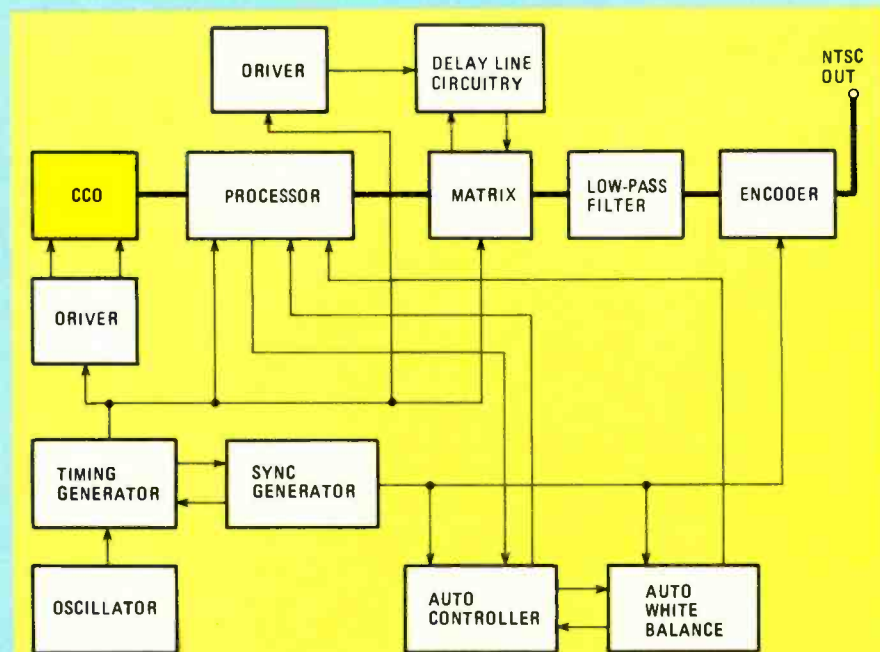


FIG. 2—BLOCK DIAGRAM of the signal-processing circuitry in the Sony CCD-G5. The video signal path, from pickup to camera output, is indicated by the bold line.

essary. Instead, a sensor on the camera detects any changes in light. In Fig. 1, the sensor is a pair of color-sensitive photodiodes. Those are used to analyze the red and blue components of the light. Information from the photodiodes is amplified and then fed to the color-processing circuitry, which in turn biases the color signals for accurate color-reproduction under the prevailing ambient-light conditions. Those systems are given a variety of names by their manufacturers—for instance, auto color tracking (as above) or

continuous automatic white balance. Of course, the biggest breakthrough in small-size pickup devices is the solid-state CCD (Charge Coupled Device) or MOS (Metal Oxide Semiconductor) pickup. The cost of those devices has now dropped to the point where it is practical to use them in consumer products. As a result, those pickups are beginning to appear in home video cameras. One such video camera is the Sony CCD-G5. The pickup used in that camera is a CCD with a mosaic color filter. The

size of the CCD used in the Sony unit is 10.7×9.3 mm, and the imaging area is 8.8×6.6 mm, which yields a 2×3 picture format. The picture itself is made up of 384 horizontal and 491 vertical picture elements (pixels). While that number of pixels is relatively low (the CCD used in the Sony *Mavica* camera is 570×488 pixels), the camera's circuitry still allows for a horizontal resolution of greater than 250 lines.

Another fundamental difference in the Sony camera (or any camera with a solid-state pickup) is that the signal processing is digital (not analog as it is in tube-pickup cameras) in nature. A block diagram of the camera is shown in Fig. 2. Let's follow the main signal path though the camera, as indicated by the bold line in Fig. 2, to see how the camera handles the required signal processing. Light that reaches the CCD is converted into an electrical signal and fed to the processor circuitry. In the processor, sample-and-hold circuits are used to separate out the component color signals. Those are passed to the matrix circuitry. In the matrix, switched sample-and-hold circuits and 1H (1 horizontal line) delay lines are used to synthesize the chrominance and luminance signals from the color signals. Finally, the chrominance and luminance signals are fed to a low-pass filter and then to the encoder circuitry, which mixes them with a sync signal to form an NTSC (or PAL) compatible output.

What of the relative merits of tube versus solid-state pickups? Tubes offer better performance in low-light situations and, at least until now, were less expensive. Solid-state pickups, on the other hand, are small, allowing for smaller camera sizes, and have lower power requirements. They are also sturdier than tubes, less susceptible to streaking, and require no warm-up time.

Of course, smaller pickups don't tell the entire story behind the miniaturization of home video cameras. Manufacturers are continuously finding ways of compressing more and more circuitry into smaller and smaller areas. In addition, creative packaging has played a major role in reducing the size of video cameras.

Consider, for instance, the Konica CV-301 shown in Fig. 3. Despite its amazingly stubby profile (2.6-inches wide \times 8.9-inches high \times 4.8-inches deep), it uses a 1/2-inch tube pickup. The secret is the position of the tube. It is mounted vertically and located in the handle of the camera. Light from the lens is directed to the front of the pickup by a mirror.



FIG. 3—KONICA'S CV-301 sports a stubby profile despite using a tube pickup. That is possible because of the location of the pickup—it is mounted vertically in the handle.

Features

Later on, we are going to look at some of the lightweight cameras that are currently available, their specifications, and the features that they offer. We've already touched upon some of those features (automatic white balance, for instance), but it would be helpful if we took a look at what the other relevant features and specifications are, and which ones are most important.

The camera's lens is the unit's "window to the world." The terms used to describe a video camera's lens are identical to those used to describe a still camera's lens. The width of the camera's aperture, which is adjustable, is measured in *f*-stops; the wider the aperture the smaller the *f* number. The maximum aperture is an important parameter of lens performance as it is an indication of the maximum amount of light that can be admitted and is provided for all lenses.

Of course, the proper aperture opening depends on the amount of ambient light. Almost all video cameras have autoexposure, which means that the camera sets the proper aperture automatically. That feature is often referred to as auto iris. For flexibility, a manual override of that feature, though not provided on all cameras, is desirable. In place of a manual override, some manufacturers provide a "backlight compensation" switch. That switch acts to open the aperture an additional 1/2 *f*-stops.

Almost all cameras come with zoom lenses. Zoom lenses are lenses in which the focal length (amount of magnification) can be varied. The range of the zoom

can be specified in one of several ways—a power of magnification (i.e. 6 \times), the ratio of highest-to-lowest focal lengths (i.e. 6:1), or the range of focal lengths (i.e. 8.5 mm–51 mm). Zooms can be power or manual. Power zooms are desirable because they allow for a smoother transition between focal lengths during taping. Manual zooms, on the other hand, add less weight to the camera.

Lenses can be either permanently mounted or detachable. Most cameras with detachable lenses use a C-type lens mount, one of the most popular of the photographic lens mounts. Because of that, in cameras with detachable lenses, any photographic lens that uses a C-mount can be used in place of the lens supplied by the manufacturer.

If you plan to do any close-up work, be sure that your lens has a "macro" setting. You will find that most do.

Viewfinders come in two types—electronic and optical. Electronic viewfinders are, in essence, small TV monitors. They allow the taper to see exactly what is being recorded by the camera. Due to the cost and weight that a color viewfinder would entail, nearly all are black-and-white. Optical viewfinders use the TTL (Through The Lens) system used by modern SLR still cameras. The major drawback of that system is that the image seen is not precisely the same as the one recorded; often the image area recorded is significantly smaller. If the taper does not account for that, the result is cut-off heads or left-out friends. On the other hand, optical viewfinders are much less expensive and add much less weight to the camera. All viewfinders, be they electronic or optical, provide information, usually via LED's, on the camera's operating parameters. Those parameters most often include such things as whether or not the recorder is operating, low light, and low power.

Optical viewfinders do have one other major advantage over electronic ones—they are easier to focus. That's why one of the most popular of the video camera "bells and whistles" is auto focus. The autofocus system can be fooled, however, if, for instance, there are several objects in the camera's field of view. Some cameras also offer a "focus-free" setting. In that setting the video camera works much like an *Instamatic* or similar fixed-lens camera. That is, a large "depth of field" is selected so focusing is not needed. Be warned, however, that while most objects will appear to be reasonably in focus, they won't necessarily be razor sharp.

Almost all cameras provide some means of controlling a VCR. Those controls most often consist of record/pause and review switches. The review switch allows you to replay in the viewfinder a scene that already has been recorded. Of course, that would only be available on a camera with an electronic viewfinder.

When talking video camera specifications, the two most often mentioned are minimum illumination and horizontal resolution. Minimum illumination refers to the lowest usable ambient light-level for satisfactory recording; it is measured in lux. Horizontal resolution refers to the number of horizontal scanning lines in the picture. When comparing horizontal resolution, it would bear to remember, as stated previously, that the maximum resolution for a VCR is about 250 lines. Thus cameras with higher horizontal resolutions would not necessarily provide more detailed pictures.

Now, let's take a look at some of today's tiny video cameras.

General Electric

General Electric (Video Products Division, Portsmouth, VA 23705) offers its lightweight (2 pounds) *Mini-Cam* (model number *ICVC5032E*). Among its features are auto focus, fade-in/fade-out, 6:1 power zoom, permanently mounted *f*1.4 lens with a macro focusing (to one inch), auto iris with backlight switch, automatic white balance, and an electronic viewfinder. The camera uses a 1/2-inch Newvicon pickup and has a minimum illumination requirement of 30 lux.

Hitachi

Hitachi (401 West Artesia Blvd., Compton, CA 90220) offers the *VK-C1500* MOS color-video camera. As indicated, rather than a tube, this camera uses a MOS pickup. The permanently mounted *f*1.2 lens has a 6 \times zoom and a macro setting. The automatic iris has a manual override. Among the camera's other features are a continuously automatic white-balance control and an electronic viewfinder with in-the-viewfinder LED's to indicate low-light and low-power conditions, and the mode of the recorder (record, stand-by, etc.). Minimum illumination required is 35 lux and the horizontal resolution is 300 lines. The unit weighs 2.16 pounds.

JVC



JVC GX-N7.

JVC (41 Slater Drive, Elmwood Park, NJ 07407) offers two lightweight models. The lightest of those is the 2.2-pound *GX-N4*. That camera uses a 1/2-inch Newvicon pickup and features an electronic viewfinder with in-the-viewfinder LED indicators. Color balance is handled via two (indoor/outdoor) switch-selectable presets. The automatic iris offers backlight compensation. The standard lens is *f*1.2, has a 6:1 zoom ratio (manual), and offers a macro setting. The lens is removable, but the mount used is a non-standard one. To use 35-mm SLR lenses, a special optional adaptor must be purchased. Minimum illumination is 10 lux and horizontal resolution is more than 270 lines.

The *GX-N7* is a similar unit but adds many "bells and whistles." Among those are auto focus (an infrared method is used), fade-in/fade-out, and continuously automatic white-balance (called "Auto Color Tracking" by JVC). The *GX-N7* weighs 2.4 pounds.

Among the options available from JVC is a character generator for titling. That device can be used with either camera.

Konica

Konica (440 Sylvan Ave., Englewood Cliffs, NJ 07632) is one of the many highly-regarded SLR camera manufacturers entering the home-video market. Their offering is the 1.6-pound *CV-301*. That camera uses a TTL optical viewfinder (an electronic viewfinder is an optional accessory) with in-the-viewfinder LED indicators and a 1/2-inch Cosvision pickup tube. The *f*1.5 lens is permanently mounted and offers a 3:1 (10 mm–30 mm) zoom. Color balance is handled via four switch-selectable presets. The minimum illumination is 35 lux and the horizontal resolution is more than 270 lines.

Magnavox

Magnavox (a division of NAP Consumer Electronics, Interstate 40 and Straw Plains Pike, PO Box 6950, Knoxville, TN 37914) offers two models. The *VR8275BK* weighs 2.2 pounds. The pickup is a 1/2-inch Newvicon tube. The lens is *f*1.2 and features a 6× manual zoom. Standard 35-mm lenses can also be used via a bayonet mount. Features include automatic iris, electronic viewfinder, and continuous automatic white-balance. Minimum illumination is 10 lux and horizontal resolution is 270 lines.

The *VR8276BK* weighs 2.4 pounds and adds auto focus and fade-in/fade-out.

Among the options offered by Magnavox is a character generator for titling.

Minolta

Minolta (101 Williams Drive, Ramsey, NJ 07446) is another long-established SLR manufacturer. Their entry into the home-video market is the *K-500S*. The pickup used is a 1/2-inch Saticon tube. The



MINOLTA K-500.

viewfinder is of the optical TTL variety. The permanently mounted *f*1.2 lens has a 4× zoom, macro setting, and "free focus" setting. The automatic iris has a backlight-compensation control. The white-balance is continuously automatic. Minimum illumination is 10 lux. The unit weighs less than two pounds.

Panasonic

Panasonic (One Panasonic Way, Secaucus, NJ 07094) offers two models. The *PK450* weighs 2.5 pounds. It features auto focus, 6× power zoom, automatic iris with backlight compensation, electronic viewfinder, and automatic white-balance. The pickup is a 1/2-inch Newvicon tube. The *f*1.2 lens has a macro setting. Minimum illumination is 20 lux.

The *PK410* weighs in at approximately 2 pounds. It has a 6:1 power zoom, *f*1.4 lens, electronic viewfinder, 1/2-inch Newvicon pickup, automatic color balance, fade, and an automatic iris with backlight compensation. Minimum illumination is 30 lux.

Quasar

Two models are available from Quasar (9401 W. Grand Ave., Franklin Park, IL 60131). The *VK704XE* weighs just two pounds. It uses a 1/2-inch Newvicon pickup. The *f*1.4 lens is permanently mounted and features a macro setting. Among the features are a 6:1 power zoom, automatic white-balance control, fade-in/fade-out, electronic viewfinder with in-the-viewfinder LED's, and automatic iris with backlight compensation control. The minimum illumination is 30 lux and the horizontal resolution is 260 lines.

The *VK714XE*, which weighs 2.4 pounds, adds infrared autofocus and a time and date display, and upgrades the lens to *f*1.2.

RCA

RCA's (30 Rockefeller Plaza, New York, NY 10020) *Small Wonder* (model *CCK020*) uses a solid-state MOS pickup. The *f*1.2 lens is permanently mounted and has a macro setting for focusing as close as 3/8-inch. The power zoom has a 6:1 ratio. The electronic viewfinder has LED indicators to alert the operator to low-light, low-battery, and record mode. The automatic iris has a manual override. Both constant automatic white-balance and

four switch-selectable white-balance presets are provided. The camera weighs 2.2 pounds and requires a minimum illumination level of 35 lux.

Sanyo

Sanyo (1200 Artesia Blvd., Compton, CA 90220) offers a pair of interesting cameras. Their models *VSC700/VSC800* (the only difference between the two is that the *VSC800* adds auto focus to the basic model) are styled to resemble 35mm still cameras. The units weigh 2 3/4 pounds. The pickup used is an MOS semiconductor. The C-mount, *f*1.2 lens has a 15mm–75mm power zoom and a macro setting. The electronic viewfinder can be positioned for ease of use. The cameras' horizontal resolution is greater than 260 lines and the minimum required illumination is 28 lux.

Sony

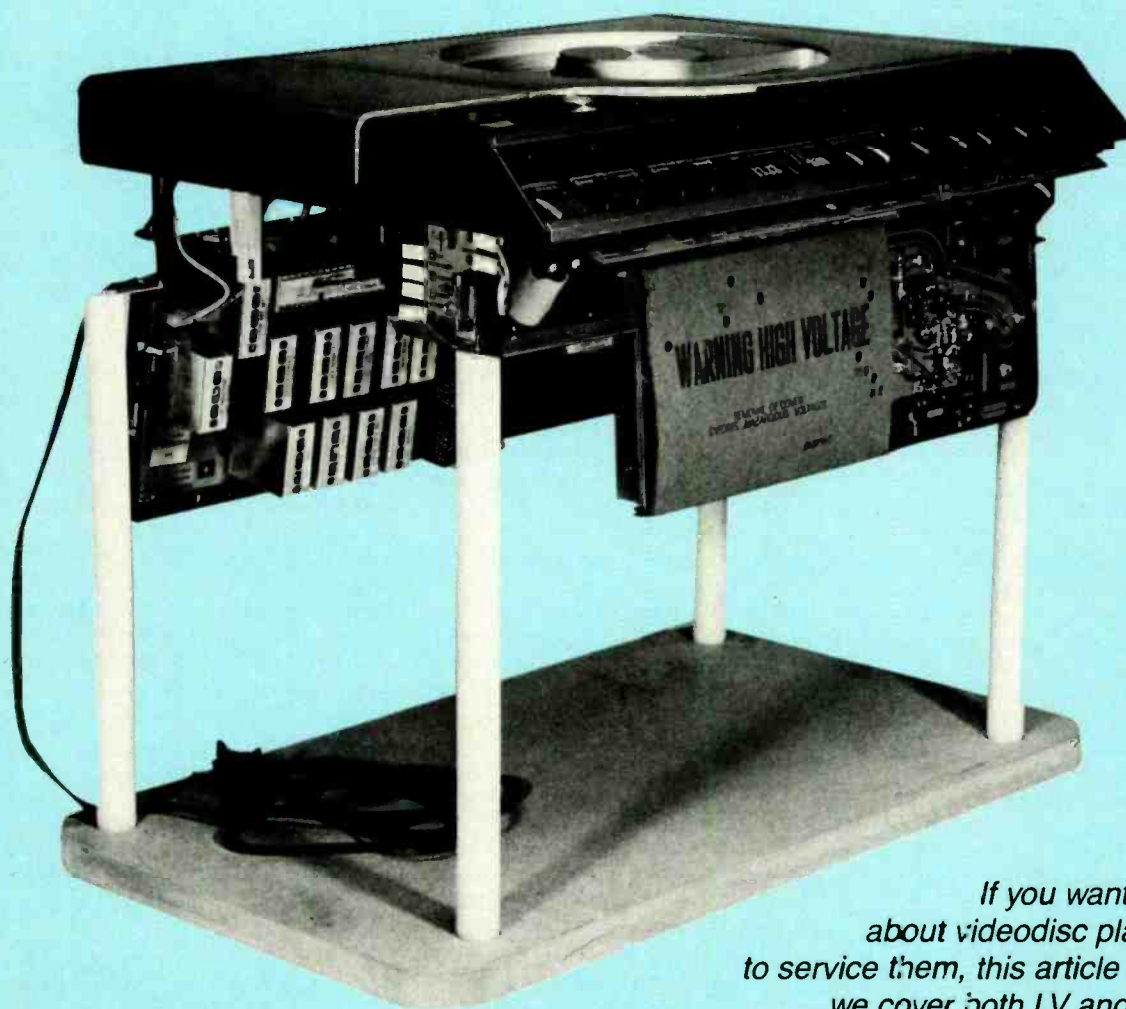
Sony's (Sony Drive, Park Ridge, NJ 07656) CCD-G5 video camera weighs 2.25 pounds. It features a solid-state CCD



SONY CCD-G5.

pickup. The unit is equipped with a permanently mounted *f*1.4 lens with a macro setting. The power zoom has a 6:1 ratio. The electronic viewfinder includes in-the-viewfinder white-balance and low-light indicators. Other features include automatic white balance with indoor/outdoor presets and fade-in/fade-out. The minimum illumination is 30 lux and the horizontal resolution is 250 lines. R-E

Servicing Videodisc Players



JOHN LENK

If you want to learn more about videodisc players and how to service them, this article is for you. In it we cover both LV and CED players.

NOW THAT WE'VE SHOWN YOU HOW TO service VCR's (**Radio-Electronics**, Dec. 1983, Jan. and Feb. 1984), it's time to try our hand at videodisc player service. As in the case of VCR's, servicing videodisc players takes all the expertise required to service a TV set and/or record player, and then some. Actually, videodisc-player electronic circuits are relatively simple compared to VCR's and most TV's. However, the mechanical functions of a typical videodisc player are substantially more complex than those of a record player or phonograph. An improper mechanical adjustment can not only put a videodisc player out of operation, but can result in permanent damage to the player and/or disc.

Don't let that frighten you away from videodisc player service. If you follow the procedures in the service manuals you should have no trouble. However, it helps if you understand the "what" and "why" of the procedures. That is one area where the manufacturer's service literature is often somewhat fuzzy. Many service-manual writers simply assume that you know all about how videodisc players operate, just as you do TV sets and record players. Hopefully that will be the case when you have read this article from beginning to end.

Let us start by reviewing how videodisc players, both LV and CED, operate. Note that LV (also called LaserVision or laser video) and CED (capacitance electronic

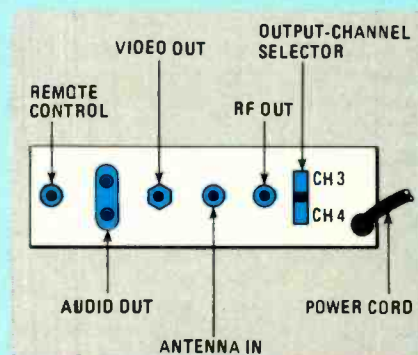


FIG. 1—REAR PANEL of a typical videodisc player showing the input/output connectors.

disc) are the two most common types of home-entertainment videodisc players.

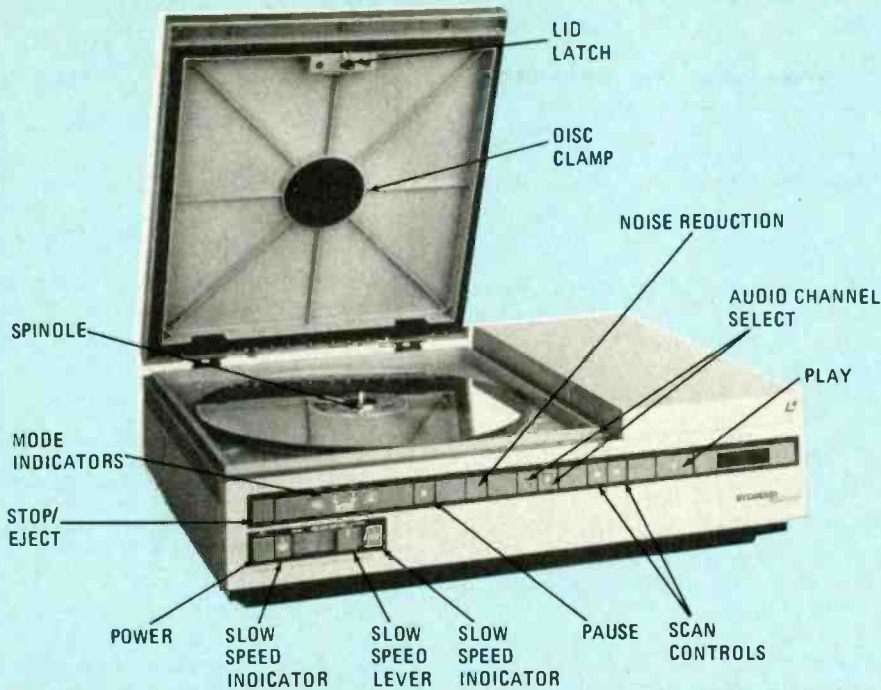


FIG. 2—CONTROLS AND FEATURES of a typical LV videodisc player. While details will vary from machine to machine, the controls and features shown here will be found on most LV videodisc players.

There is a third system, VHD (video high density), with its companion AHD (audio high density) that has not quite gotten off the ground, so we will not cover it here. Also, we will not go into full circuit descriptions or mechanical details for any videodisc player here. (To do so would require a book of at least 350 pages.) But we will go through videodisc player functions so you can understand the theory-of-operation sections found in some service literature.

The videodisc player

Videodisc players are very specialized forms of phonographs or record players that play pre-recorded discs carrying both picture and sound through any standard TV set. The picture can be either black-and-white or color. The sound can be monaural on all players, and stereo on some players (and even two-channel independent or bilingual on some players).

The LV player uses a *reflective optical pickup system*, developed by NV Philips in the Netherlands and MVA Inc. The LV system was called "video long play" at one time, and was introduced in the United States in 1978.

The CED player uses a *capacitance pickup system* developed by RCA Laboratories, and was introduced in 1981.

With either system, the player circuits function to convert picture/sound information recorded on the disc into electrical signals used to modulate an RF unit (also known as a VHF modulator). In the simplest of terms, the RF unit is a miniature TV-broadcast station operating on an unused TV channel (typically Channel 3 or

4). The output of the RF unit in the player is fed to a TV set. The videodisc spins at a high rate of speed compared to a conventional audio record, and uses either a *light beam (LV)* or *capacitance (CED)* pickup.

CED versus LV

There are similarities between CED and LV. For example, both systems use a plastic disc rotating on a turntable. In both systems, the player picks up information represented by changes in the disc surface, and converts the information into signals for playback on the TV set. The two systems use FM for both the video and audio signals. Each disc also has a spiral track to carry the information, rather than a series of circular tracks.

Plastic discs for the LV system are coated with metal on one side (the recorded surface), and then bonded with the metal inside for protection. Carbon is added to a CED disc to make the disc conductive. A lubricant is also added to the CED disc because the CED system has grooves for stylus tracking. That makes the CED system simpler (no servo tracking is required for CED) but does cause disc wear.

Quality standards for both systems require that the discs be relatively defect-free, flat, and stable with time and temperature changes, and have an acceptable signal-to-noise ratio. All players must be mechanically balanced, and must also accommodate imperfect mass-produced discs. All three systems can step the pickup backward and forward one or more track widths, for repeat play or rapid

search. In addition, every disc includes a code in the signal recorded so that features not included in every type of player, such as automatic search, can be added.

In spite of the basic similarities, the systems differ not only in the pickup technique (optical versus capacitive) but also in the format in which the information is encoded, and in the method by which information is tracked on the disc. Other differences include disc size, material, rotation speed, and signal-protection schemes. We will talk about those differences as we go along. For now, let us consider the connections between a videodisc player and the TV set.

Connecting the player

All connections to the player are usually made via the rear panel. Figure 1 shows how a rear panel of a typical videodisc player might appear.

The ANTENNA IN connector (generally a 75Ω coax type) is connected to the antenna or cable nut. The CHANNEL 3/4 VHF OUT connector (also 75Ω) is connected to the antenna input of the TV set. That permits the TV set to be connected to either the antenna (for off-the-air TV program reception), or to the player (for videodisc program play) depending on the setting of a front-panel switch.

In addition to the Channel 3/4 modulated-RF output, most videodisc players also provide audio outputs (for use with stereo systems) and a baseband video output. The baseband video output is for connection to a video monitor or a TV set equipped with a video input.

Some videodisc players also have a CONTROL connector that allows for the connection of an external device (such as a remote-control unit) for wired electronic control of the player. In other players, an infrared (IR) control is used. As in the case of a conventional TV set, no cable or other direct physical connection is required when an IR remote-control is used.

The LV system

Now that we have reviewed the operation of videodisc players in general, let us go into a bit more detail on the LV system. We start with a description of the user

controls and major features found on a typical LV player, such as the one shown in Fig. 2. Keep in mind that while we'll be discussing the controls for a particular player, the same or similar controls are found on all LV players.

In use, you place the videodisc over the turntable and spindle as you do a phonograph record. The turntable is coupled directly to a motor that rotates the disc at the proper speed.

When you close the lid, a magnetic *disc clamp* holds the disc on the spindle automatically to ensure stable rotation.

The disc is placed over the *objective lens*, which is the key part of the player that reads the signal recorded on the disc. Note that the objective lens surface must be kept clean in order to maintain optimum performance. Generally, the player is shipped from the factory with a lens cap over the lens. (Note that the objective lens can not be seen in Fig. 2 due to the presence of a disc on the turntable.)

The *playback mode indicator* lights are located above individual control buttons, and turn on when the corresponding mode is selected.

You press the STOP/EJECT button to cut off operation and to open the lid.

You press the POWER button to turn the power on and off. The red indicator above that control turns on when power is on.

The *slow indicators* are used to indicate slow motion play.

You use the SLOW SPEED lever to adjust the speed of slow motion play. At its normal speed, the videodisc is played at a rate of 30 frames-per-second. At its slowest speed, the videodisc is played at a rate of 1 frame-per-second. The SLOW SPEED control is used to vary the playing speed between those extremes.

You press the PAUSE button to temporarily halt disc operation. Operation stops on the last frame played when that button is pressed, and no video image is reproduced on the TV screen. The PAUSE mode is released by pressing the PAUSE button again.

Some videodiscs are recorded using CBS's CX noise-reduction system. The NOISE REDUCTION button is pressed to activate the player's noise-reduction system for those discs.

The two AUDIO CHANNEL SELECT buttons are on/off controls for the two audio channels.

The SCAN controls are used to quickly locate a specific part of the program.

The PLAY button is pressed to begin playing a videodisc, or to resume playing after another playback mode is selected.

Although LV players are not difficult to operate, the basic operating procedures are different from those of a typical audio record player or phonograph (and from those of a CED player, which we'll discuss in next month's article). The following is a quick run-through for operation of

a "typical" LV player. Keep in mind that you must study the literature for the particular player you are servicing.

To install and remove an LV videodisc on a typical player, press the POWER switch to turn on the player. Press the STOP/EJECT button to release the lid latch. Open the lid, *being careful not to force the lid beyond the normal fully-open position*. With the label of the side you want to play facing up, place the disc on the turntable. (When that is done, the "recorded" side is facing down so that it can be scanned by the objective lens.) Be sure that the center hole of the disc stays in the convex spindle. Shut the lid firmly. The disc clamp on the underside of the lid holds down the disc magnetically. The videodisc is now ready to play.

To remove the disc, press the STOP/EJECT button, open the lid carefully, hold the disc by *both edges*, and lift the disc from the turntable. Replace the disc in its jacket after use.

To start a typical LV player, turn on the power to the player, TV set, and stereo system (if you are reproducing the audio signal through a stereo, which happens to be one of the big selling features of the better videodisc players). Next, install a disc and close the lid. Most LV players cannot operate unless the lid is closed completely. Tune the TV to the channel (3 or 4) chosen via the player's rear-panel CHANNEL SELECTOR switch (see Fig. 1). Now (if all is well) the STAND BY indicator will begin flashing when the PLAY button is pressed. After a few seconds, the turntable reaches the proper rotation speed, the laser beam begins picking up the signal from the disc, and the video picture appears on the TV screen.

Although the following notes apply specifically to the player of Fig. 2, they also apply generally to all LV players.

When an extended play disc (CLV) is being played, special functions such as still/step, slow play, fast play, frame number search, etc., do not operate on most players.

If you try to operate an LV player without a disc, or if the unrecorded side of a disc is facing down, turntable rotation stops automatically.

When the player is used for the first time, adjust the FINE TUNING control of the TV set for the best picture quality. (This is also a good starting point if you are faced with a "poor picture quality" symptom.)

If the player fails to respond to a command, or continues to show some unusual characteristics, turn off the unit via the POWER switch, and then start the operating sequence again.

Moisture condensation may impair operation of a videodisc player. Watch for any sudden changes in temperature, particularly when you move the player from one location to another.

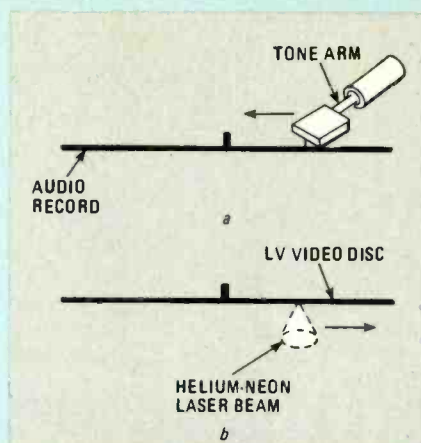


FIG. 3—A PHONOGRAPH RECORD, as shown in a is played from the outside in, with the pick-up, consisting of a tone arm and needle, resting on the top of the disc. As shown in b, a videodisc is played from the inside out, with the pickup being a laser focused on the underside of the disc.

Most LV players have such operating functions as pause, scan, slow, still/step, frame-number display, chapter-number display, and fast operation. We will not go into those here since the functions are unique to each player model. But you should be aware of the functions, *before* you start to service any player. You could spend hours trying to troubleshoot a function that does not exist.

LV videodiscs versus audio records

Figure 3 compares the familiar audio record playing technique with the LV videodisc. Audio records are played with a phonograph needle on top of the record. The beginning of the record is at the outside edge, and the needle moves inward as the music is played. The LV videodisc is played from the bottom with a light beam. The beginning of the LV disc is near the center, and the light beam moves outward toward the edge as the program plays. The light beam is generated by a helium-neon laser inside the player.

The light beam is focused up on the bottom of the disc through an objective lens. That lens is located in the player under the disc. As the disc is played from beginning to end, the lens moves from near the center to the outside edge of the disc. The light beam actually reflects off microscopic *pits* beneath the bottom surface of the disc. Those pits are coded with the picture and sound information.

Each disc side contains thousands of separate pictures. The rapid playback of those pictures creates the program on the TV screen. Each picture is numbered, and a 5-digit "picture number" can be displayed in the upper left portion of the TV screen. That feature allows any given portion of the program to be located easily. Also, some videodisc programs have two or more segments. Each segment is called a chapter, and a 1- or 2-digit-chapter number can be displayed on the screen

instead of the picture number.

In addition to the picture, two channels of high-fidelity sound are recorded on most LV videodiscs. Either one or the sum of both channels may be played through the TV set. Those sound channels are also available at the rear panel (Fig. 1).

LV is called the non-contact, pick-up system since LV uses a laser beam, and there is no physical contact between the pickup and disc. (That is in contrast to CED where there is some physical contact). When the laser beam strikes a series of pits, the light is reflected back into the system, and the variations of the reflected light are converted into the reproduced signal.

CAV versus CLV

The *standard play* LV videodisc, also known as the CAV or *constant angular velocity* disc, spins at the same constant speed of 1800 rpm from the inner circumference to the outer circumference, and provides a maximum of 30 minutes playing time per side. On a CAV disc, one video-picture frame is recorded for each revolution. That makes possible several features (stop or still picture, stable visual pictures during scan or search, true slow motion, etc.) when CAV discs are played.

Although the extended play LV disc, also known as the CLV or *constant linear velocity* disc, does not offer the additional operating features, CLV does provide a maximum playing time of one hour per side. With CLV, the rotation speed varies from 1800 rpm at the inner circumference to 600 rpm at the outer circumference.

Most LV players will play either CAV or CLV discs, and automatically detect which type of disc is being played, without resetting of controls by the user.

LV microprocessor control

Most LV videodisc players have some form of microcomputer or microprocessor control. That provides a number of push-button-selected operating features, such as still picture, slow motion, etc. On many LV players, there is also a feature called the *frame number random access* that finds a specific frame automatically by frame number within 15 seconds. The LV videodisc has a maximum of 54,000 "tracks" in a continuous spiral from the inner to the outer circumference. On a CAV disc, the signal for one video-picture frame is recorded on one track covering one full revolution. Beginning at the inside circumference, each frame is recorded along with the frame number.

Audio

Audio is recorded on the videodisc in the form of two separate FM signals. That makes either stereo or two-channel independent (such as bilingual) sound possible. Typical AF response is 40 Hz to 20 kHz, with an S/N ratio of 60 dB, and a

total harmonic distortion of 0.5% or less. The S/N ratio can be increased to about 70 dB when a special noise-reduction system, CX, is used. Not all LV discs are recorded with CX and, on most LV players, you must operate a control to select CX operation. As a point of reference, the quality of stereo reproduction from an LV player is generally comparable to conventional phonograph records or FM broadcasts (but not to digital audio discs).

LV characteristics

An LV videodisc is composed of thousands of circular tracks making up a continuous spiral from the inside of the disc to the outside. Each track is a series of pits. Light reflected from inside a pit is less bright than light from the spaces between the pits. Thus, the intensity of the light is modulated as the videodisc rotates.

The intelligence encoded on the disc results in three FM signals: 8.1-MHz FM, modulated with the composite video (including the chroma or color signal); 2.3-MHz FM, modulated with the audio from one of the audio channels (channel I), and 2.8-MHz FM, modulated with the audio from the other audio channel (channel II). Each of the sound carriers has a maximum deviation of ± 100 kHz. The 8.1-MHz video FM carrier has a deviation of 1.7 MHz (7.6 MHz at the sync tips to 9.3 MHz at the white peaks). However, the bandpass of the 8.1-MHz video carrier extends from below 4 MHz up to above 12 MHz in order to include all necessary sidebands.

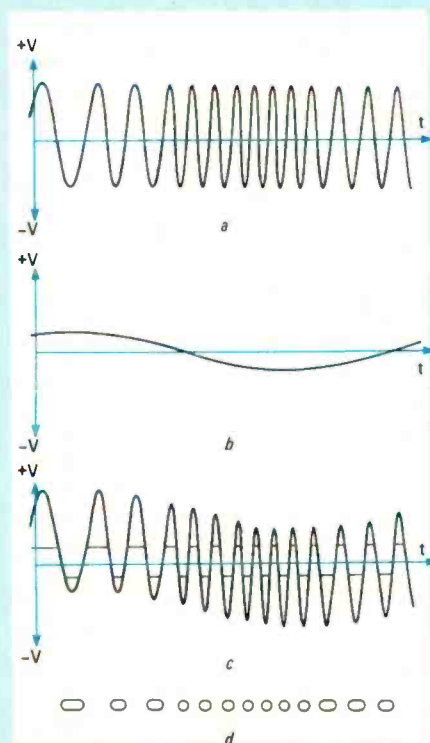


FIG. 4—AN 8-MHz video signal (a) is pulse-width modulated by an FM sound carrier (b), and the resultant signal is clipped (c) and used to create the pits (d).

Video Entertainment

Figure 4 shows how the 8-MHz FM video signal is pulse-width modulated by one of the sound carriers. Each of the sound FM carriers pulse-width modulate the 8.1-MHz carrier to create the actual resultant signal that becomes encoded on the disc. The resultant signal in Fig. 4 is clipped and used to create the pits in the disc. Note that waveform can cause the length of the pits, and the spacing between the pits, to vary.

In addition to the play tracks, special tracks called *lead-in* and *lead-out* tracks (at the inner and outer diameters of the disc) are coded so that the focused laser beam does not move beyond them. When the lead-out tracks are reached, the laser automatically moves back to the lead-in tracks and stops.

Tracking

Tracking of the laser over the disc is a very important part of LV-player operation. It also is probably the cause of most service problems. Two types of tracking are involved: radial and tangential. Both are shown in Fig. 5. Radial tracking refers to keeping the light beam centered on the LV videodisc tracks. Without some form of radial tracking, the light beam can drift between the tracks, resulting in a lost picture. Radial movement of the beam is always perpendicular to the tracks. Tangential tracking refers to keeping the beam in line with the track. That direction of movement is necessary to compensate for momentary speed errors of the track passing over the beam.

In the LV system, both radial and tangential tracking is done by means of two moveable mirrors, as described next.

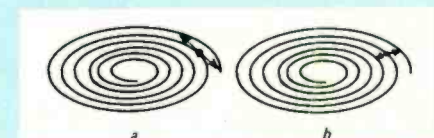


FIG. 5—TANGENTIAL TRACKING (a) and radial tracking (b) of the laser on an LV videodisc. Note the spiral tracking pattern.

LV player functions

The heart of the LV system is the *slide assembly*, also known as the *sled*; the sled

contains the laser and the optical system. A slide drive-motor moves the entire slide assembly beneath the disc as the program is played. The laser generates a red light beam that passes through an optical divider. The beam is then deflected by the automatic tracking mirror up into the objective lens. The objective lens focuses the beam into a tiny point on the bottom of the disc. The beam is reflected by the disc surface.

The reflected beam follows the same path back through the objective lens and automatic tracking mirrors to the optical divider. The reflected beam is then separated from the original beam and sent to the light-sensitive diodes (photodiodes). The diodes conduct a current that varies according to the amount of light falling on the diode surface. Since the reflected beam is intensity modulated by the pits on the disc surface, the diodes recreate the FM signal that was recorded on the disc.

The diodes also create a focus error-voltage if the disc gets too close or too far from the objective lens (which can move up or down to follow movements of the disc, and thus maintain correct focus). That keeps the light beam focused if the disc is warped or otherwise distorted. The focus error-voltage is applied to the focus servo that controls the objective lens movement.

The diodes also generate a radial error-voltage if the beam tends to drift off the track. That radial error-voltage is applied to the radial tracking mirror servo that moves the radial tracking mirror to bring the beam back to the track center.

The FM signal generated by the diodes (as the beam passes over the pits) is applied to the signal processing electronics where the FM signal is demodulated. The demodulated FM is a composite video and audio signal (similar to that shown in Fig. 4) that is applied to the RF-modulator unit. The RF modulator places the composite video and audio on an RF carrier of the correct frequency for either TV Channel 3 or 4. The resultant TV RF signal passes through an automatic antenna switch to the VHF antenna terminals of the TV set. When the player is off, the regular external antenna is automatically connected to the TV set.

In addition to the single audio signal that is applied to the FM modulator, two separate audio signals are supplied to the left and right audio jacks on the rear panel of the player.

The signal-processing circuitry also generates an rpm error-voltage, which is derived from the horizontal scan rate, and is proportional to errors in the turntable motor speed. The rpm error-voltage is applied to a PLL motor-control servo that, in turn, controls the speed of the turntable motor.

The signal-processing circuitry also generates the tangential error-voltage, which is proportional to the momentary

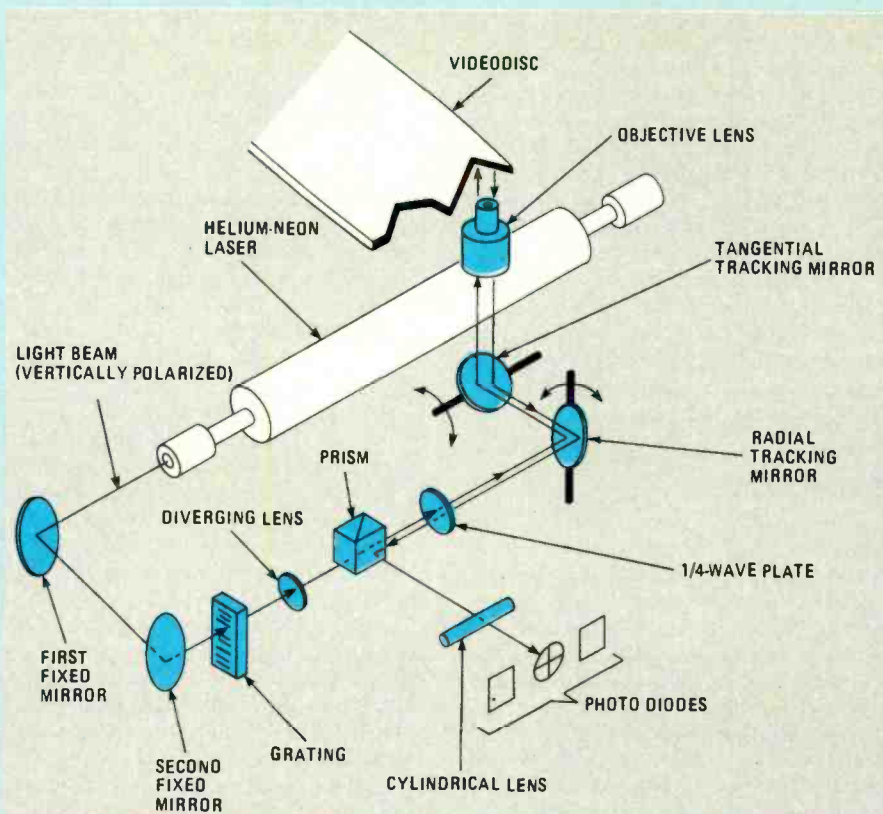


FIG. 6—PRIMARY COMPONENTS of a LV videodisc player's optical system.

speed errors in the tracking. Such errors are caused by slightly elliptical tracks, or an offset center hole in the disc. The tangential error-voltage is applied to the tangential-tracking-servo that moves the tangential-tracking mirror.

There are two tracking mirrors, one for radial tracking and one for tangential tracking. Those mirrors are part of the optical system, which we will discuss next.

The optical system

Figure 6 shows the basic components of the LV player optical system. All of those components are mounted on the slide assembly below the videodisc. The optical system uses components that are affected by the polarity of light. The laser beam is vertically polarized. The first optical component encountered by the vertically polarized light beam is the first fixed mirror, which reflects the beam around a corner to the second fixed mirror. In turn, the second fixed mirror reflects the beam around another corner, and onto the grating, which is a piece of optical glass with several fine etched horizontal lines. The grating divides the beam into three beams: a center or main beam and two secondary beams (above and below the main beam). The secondary beams are less bright than the main beam.

The center or main beam is used to read the tracks on the disc, while the secondary beams are used for tracking. The three beams, or light bundle, from the grating is applied to a prism through a diverging

lens that focuses the beam to the correct size to completely fill the aperture of the objective lens. As the beam exits the end of the prism, the beam passes through a quarter-wave plate that changes the beam into a circularly-polarized beam that is reflected off the tracking mirrors into the objective lens.

The objective lens is similar to a microscope and focuses the beam into an extremely fine spot on the disc surface. The reflected beam from the disc is intensity modulated by the pits, which have a depth equal to one-quarter wavelength of the laser beam. Since the lightwave consumes one-quarter of a wavelength going into the pit, and another one-quarter wavelength coming out, the beam reflected by the pits is one-half wavelength out-of-phase with the light at the surface. A cancellation effect takes place and reduces the beam intensity as the beam passes over a pit.

The reflected beam follows the identical path as the beam from laser to disc (incident beam) all the way back to the prism. However, on the return trip, the reflected beam is polarized opposite to the incident beam (the reflected beam is horizontally-polarized as the beam passes through the quarter-wave plate).

Unfortunately, that's all we have room for this time. When we continue next month, we'll finish our discussion of the LV system by examining more carefully the system used to focus the laser precisely on the videodisc. Following that, we'll take a detailed look at how the CED system works.

R-E

BUILD THIS

DID YOU EVER WISH THAT YOU COULD make copies of game cartridges for your Atari 2600? Well, with the circuit we'll describe, you can! We'll show you how to record the contents of your cartridges on cassette tape—and how to load the game back into the 2600. Before we get into the

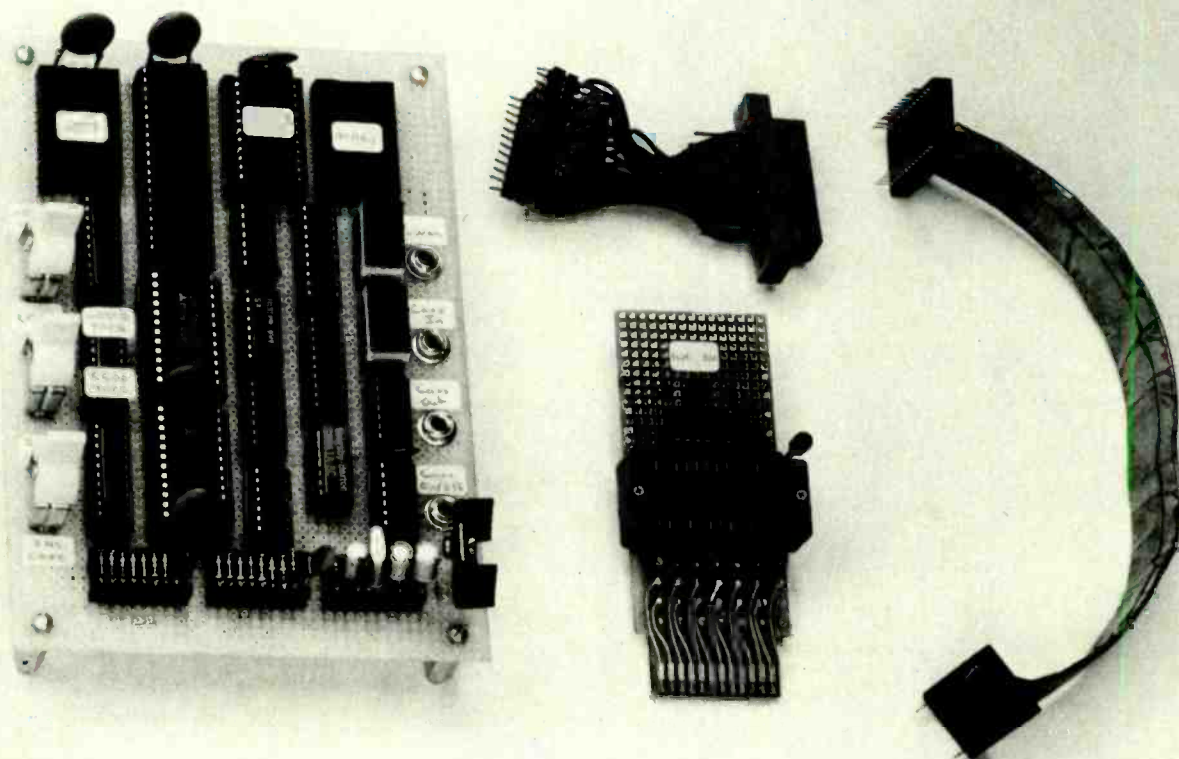
of ROM—that type of memory can be read but not written to.

If a videogame is just a simple home computer, as we stated earlier, you might wonder why the programs stored in the ROM cartridges cannot be stored on magnetic tape or floppy disks like programs

game cartridge (ROM), a cassette player, RAM, and a control device, which allows us to correctly direct the flow of data. For example, the first step in copying a game cartridge is to load the contents into RAM. Then the contents of RAM is transferred to cassette tape much in the same

ATARI Game Recorder

GUY VACHON and DAVID A. CHAN



Store your library of Atari videogame cartridges on cassette tapes!

details of the circuit, let's review some basics.

As you probably know, a videogame is just a simplified home computer—one that has been dedicated to the specific task of playing games. Keep in mind, though, that the videogame operates much the same as any computer—the electronic circuits that make up the machine (the hardware) execute instructions that make up the game (the software).

The software is stored, of course, in the game cartridge, which consists simply of ROM (Read-Only Memory). As its name implies, you cannot change the contents

for other home computers. Well, they can! But videogames like the Atari 2600 lack the necessary hardware to record them. And that's what this article is all about.

The basic approach

Our approach will be to copy the contents of the ROM cartridge into RAM. (That's Random-Access Memory, also known as read/write memory.) Once we have the game program in RAM, we can then copy it to cassette tape.

Figure 1 shows a very basic block diagram of what we need: the videogame, a

way that many home computers save programs on cassette. (The Timex Sinclair 1000, is one example.) When we want to play the game, we reload it from cassette to RAM. We get the 2600 to think that the RAM is just a game-cartridge ROM by setting the READ/WRITE input of the RAM to READ and connecting its other inputs and outputs to the 2600 just as if it were ROM.

We can also make tape-to-tape copies easily using that scheme. Once we load the program from cassette into RAM, we can simply dump the RAM contents to another tape.

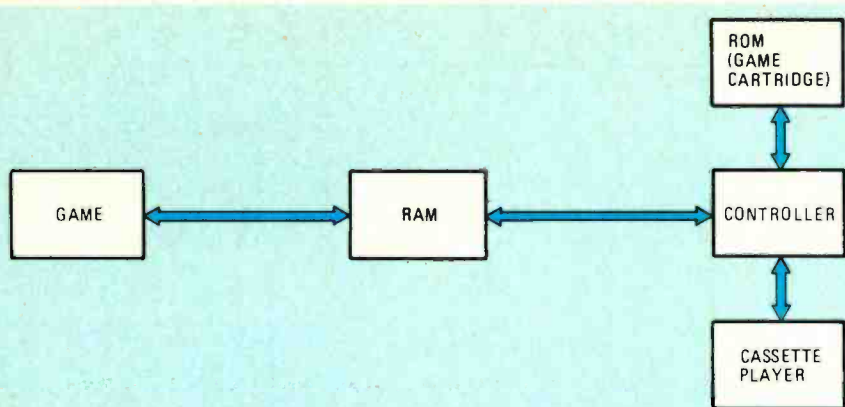


FIG. 1—A CONTROLLER IS NEEDED to properly direct the flow of data from the game cartridge ROM to the computer's RAM, from the cassette player to the RAM, etc.

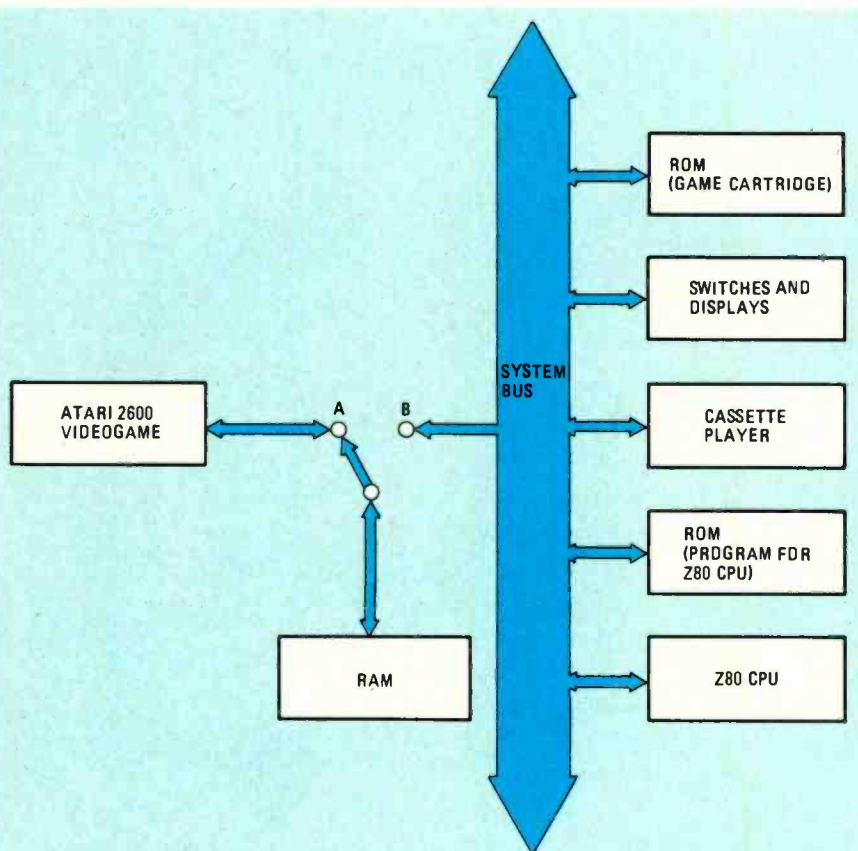


FIG. 2—A DEDICATED, SIMPLIFIED COMPUTER. This block diagram gives a basic idea of what we need to record the contents of Atari 2600 videogame cartridges.

A dedicated computer

If you're familiar with home computers—even the cheapest models that you can buy for under \$50—you know that they have all the capabilities we need. We could approach the problem by modifying a computer to do exactly what we want. But that is not the way we will go. Instead, we will build our own dedicated, simplified computer.

A block diagram of the computer that we need is shown in Fig. 2. When the switch is in position "B," the 2600 is out of the picture and we're left with only our dedicated computer. It sees the game cartridge and RAM as part of its memory. It

can transfer data from the ROM cartridge to the RAM, and it can store and retrieve programs from tape. The game cartridge is not the only ROM: Another block of ROM holds what can be thought of as the operating system of our computer. It contains the instructions that tell the Z80 CPU how to perform the appropriate data-transfer tasks.

Note that also "hanging from the bus" of our computer are switches and displays that are used for I/O. By setting the switches, we can give the computer certain commands. The displays let the computer tell us what it is doing.

When the switch shown in Fig. 2 is

moved to position "A," the Atari 2600 videogame uses the RAM simply as if it were ROM. So, for example, after you loaded the RAM with a program contained from cassette, you would flip the switch to position "A" so that the 2600 could see it.

Game-recorder computer hardware

Let's look at the hardware that we'll use to help us record game cartridges. Figure 3 shows the schematic of the computer/recorder. As you can see, the computer is structured around the Z80 bus. Connected to the bus, directly or through buffers, are all the computer's components: the Z80 microprocessor (IC3), the RAM (IC11-IC13), and the I/O devices (S1-S5, DISP1, DISP2, cassette output, game cartridge connector, etc.). We can also see IC10, the ROM that contains the program for our computer.

Most of the components of our computer are used in the usual fashion. In other words, the ROM and RAM is used just as it is in any given home computer. The cartridge connects directly to the bus and, as far as our computer is concerned, seems to be another several kilobytes of addressable memory. That same technique of memory-mapped I/O is used to drive the seven-segment displays and to interface with the tape recorder.

Note that we do not use BCD-to-seven-segment decoders to drive our LED displays. Instead, the Z80 CPU has control over the segments and turns them on or off as needed to represent hexadecimal digits 0-F and an error message of three horizontal bars. But we're getting a little ahead of ourselves. What is important here is that, as far as the Z80 is concerned, the displays are "write only" memory locations. Information encoded in the common seven-segment display format is sent to the display at their locations. The information is latched with the WRITE signal from the Z80 just like any other memory location. The same method is used for the tape-recorder interface. A 1 is latched to send a high-level voltage to the tape and a 0 is latched to send a low-level voltage.

The last major component of the computer is the interface to the Atari 2600. That interface is essentially made up of IC4, IC5, and IC6—three 74LS244 octal buffers with three-state outputs. By looking at the direction of the buffers, you can see that the dedicated computer accepts addresses from the Atari game and outputs data to it. (Remember: That's just what ROM does!) The buffers are enabled by the BUS ACKNOWLEDGE signal (pin 23) from the Z80 (IC3).

When we want the 2600 to play a game, we simply close the SETUP/PLAY switch, S6, which brings the Z80's BUS REQUEST line (pin 25) low. Thus, the 2600 actually does DMA (Direct Memory Access) on the computer when requested by you through the SETUP/PLAY switch.

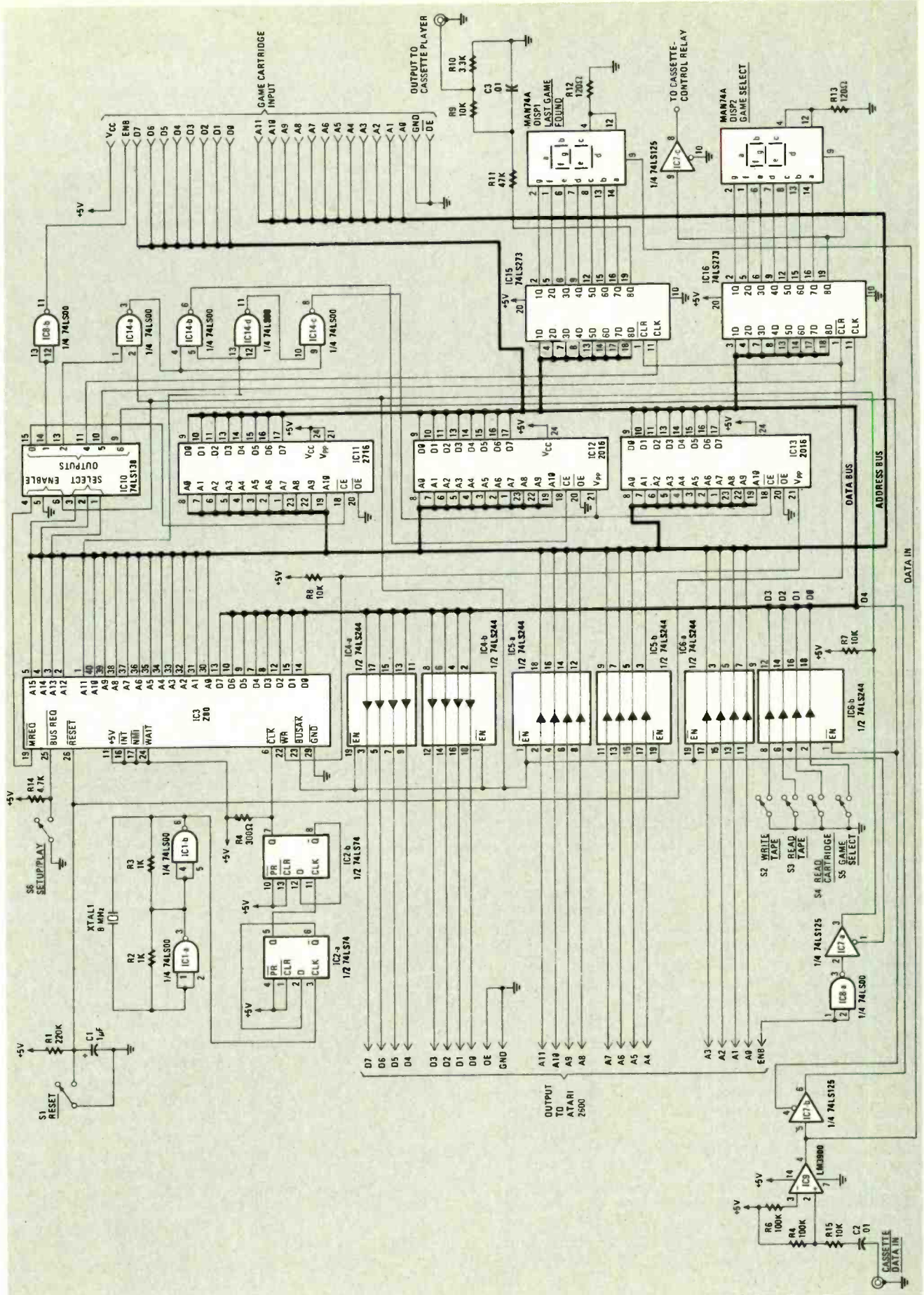


FIG. 3—A Z80 MICROPROCESSOR, along with the ROM-held operating system make up the heart of our computer/recorder. The game-cartridge ROM, LED displays, and cassette input/output are memory mapped.

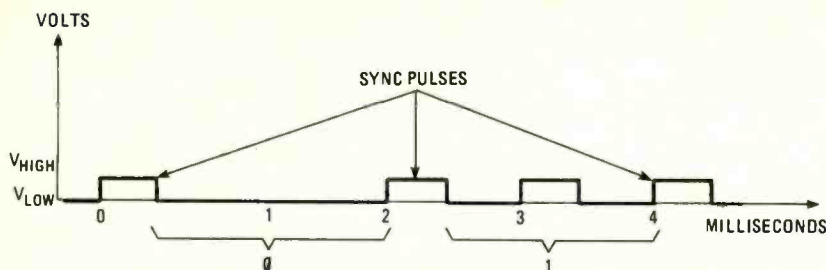


FIG. 4—SYNC PULSES, 2 milliseconds apart, are used to make sure that—even with slight changes in tape speed—the computer will be able to correctly read a tape. Data pulses are sent between the sync pulses: the sequence “01” is shown above.

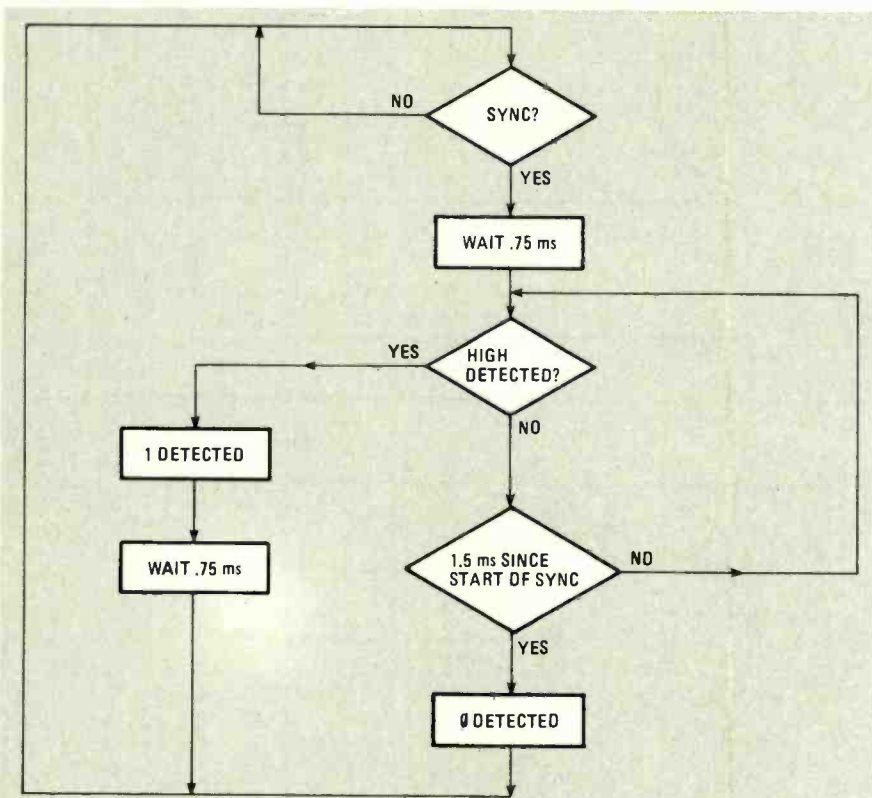


FIG. 5—THE CASSETTE-READ ALGORITHM. Rather than using hardware, software is used for timing operations.

Cassette input/output

Reading the ROM, of course, isn't the only job of our computer/recorder—we must write the contents of the ROM into tape. We'll do that by outputting one bit at a time by sending different voltage waveforms to the microphone input of the tape recorder. The bit to be output is put on data line D8, which is stored in IC16 (a 74LS273 D-type flip-flop), which is clocked by the \overline{MREQ} line of the Z80. (Note that the output of IC7-c can be used to switch a relay to control your cassette player through its REMOTE input. That is, of course, optional.)

We will not only send pulses to represent zero bits and one bits—we'll also send out synchronization pulses. Those pulses are 0.25 milliseconds wide and are sent every 2 milliseconds, regardless of whether a 1 or 0 is being written. Those sync pulses are used to ensure that if the

tape recorder speed varies slightly, our computer will be able to keep track. A data bit will be represented by a pulse—or the lack of a pulse—between the sync pulses. Figure 4 shows what the sequence “01” would look like. As we can see there, a “0” is represented by no pulse between sync pulses, and a “1” is represented by a pulse.

Each instruction for the 2600 consists of 8 bits. We will add a parity bit to be able to detect if a program has been mis-recorded or when a recording has degraded and has errors. Therefore, the contents of a game-cartridge ROM are stored as follows:

- Header (2000 zeros)
- End of header (4 ones)
- Name tag (4 bits)
- Contents of location 1 (8 bits)
- Parity for location 1 (1 bit)
- Contents of location 2 (8 bits)
- Parity for location 2 (1 bit)

PARTS LIST

All resistors are ¼-watt, 5%, unless otherwise specified.

- R1—220,000 ohms
- R2, R3—1000 ohms
- R4—330 ohms
- R5, R7—R9—10,000 ohms
- R6, R15—100,000 ohms
- R10—3300 ohms
- R11—47,000 ohms
- R12, R13—120 ohms
- R14—4700 ohms

Capacitors

- C1—1 μ F, 10 volts, electrolytic
- C2, C3—.01 μ F, ceramic disc

Semiconductors

- IC1, IC8, IC14—74LS00 quad 2-input NAND gate
- IC2—74LS74 dual D-type flip-flop
- IC3—Z80 microprocessor
- IC4—IC6—74LS244 octal buffer
- IC7—74LS125 quad bus buffer
- IC9—LM3900 quad op-amp
- IC10—74LS138 3-to-8 line decoder
- IC11—2716 EPROM containing the computer's operating system
- IC12, IC13—2016 2K \times 8 static RAM
- IC15, IC16—74LS273 octal D-type flip-flop
- DISP1, DISP2—MAN74A
- S1—S6—SPST switches
- XTAL—8 MHz

That continues until all the ROM's contents are stored.

The header serves two purposes: It separates programs and provides an audible tone to detect where the program begins. (If you listen to the tape, you will hear a high pitch tone for the header. The program itself sounds like high- and low-noise.) The name tag allows you to save several programs on one cassette, and to search for those programs.

Reading the ROM contents from tape is also done one bit at a time. The computer/recorder constantly monitors what is coming out of the tape and can tell whenever the output is high or low. The sync (and data) pulses are detected by waiting for the level to go from low to high.

Detecting those pulses doesn't require much hardware. The proper timing can be implemented by counting machine cycles in a loop that does nothing. The algorithm is illustrated by the flowchart in Fig. 5.

As you can see from the flowchart, the algorithm for cassette operation is very simple: Wait for the sync pulse to appear then wait .75 millisecond and start looking for the data pulse. If the data pulse isn't seen within 1.5 milliseconds, assume that a 0 was recorded, and wait for the next sync pulse. If a data pulse is found, assume a 1 was recorded. Then wait 0.75 milliseconds and start looking for the next sync bit.

When we continue next time, we'll take a closer look at the software. Then we'll give you some construction hints. R-E

DESIGNING WITH LINEAR IC'S

This month, we'll learn about voltage-controlled amplifiers, integrators, and differentiators.

JOSEPH J. CARR

Part 7 IN THIS INSTALLMENT of "Designing with Linear IC's we will examine three circuits that we've previously overlooked but are nonetheless very important. Those are the voltage-controlled amplifier (VCA), integrator, and differentiator. As for the latter two circuits, interestingly most of the designs that are usually published do not work. We'll show you why, then provide a design that *does* work.

Voltage-controlled amplifier

A voltage-controlled amplifier (VCA) allows you to set the amplifier's gain via a control voltage. In a way, the VCA is much like the automatic gain-control (AGC) amplifiers found in receivers and certain electronic instruments. One of the most common AGC and/or VCA circuits is shown in Fig. 1. The circuit can be built either from discrete components as shown, or be obtained in IC form (the RCA CA3028, for example).

In the circuit shown, Q1 and Q2 form a differential pair. The output of the circuit can be taken from either collector, or differentially between the collectors. The input designations assume single-ended output from the collector of Q2.

The collector-emitter currents for Q1 and Q2 (I1 and I2, respectively) are derived from I3. We can thus control the gain of the circuit by controlling the collector current of Q3. Of course, that current is determined by the voltage at the base of Q3, which is applied via terminal V_C and divided down by the voltage divider consisting of R1 and R2.

Fig. 2 shows a VCA built from an operational transconductance amplifier (OTA), the RCA CA3080. Recall from

our earlier discussion that an OTA has a transfer function that relates an output current to an input voltage. The gain is expressed in units of transconductance (G_M). The voltage gain (A_V) is determined by the product of G_M and the load resistance R_L. The value of G_M, on the other hand, is set by a bias current I_{ABC}, where G_M = 19.2I_{ABC}.

The bias current is set by control voltage V_C and resistor R6. The current is maximum (i.e. 0.5 mA) when V_C = 0, and minimum when V_C = -15 volts. The maximum transconductance, then, will be (19.2)(0.5 mA) = 9.6 millisiemens = 0.0096 siemens. The voltage gain, therefore is G_MR1 = (0.0096 siemens)(10⁴ ohms) = 96. The voltage gain will therefore change from 0 to almost 100 as V_C varies from -15 volts up to 0 volts.

Integrators

An integrator is a circuit that will produce an output that is proportional to the time average of the input signal. In other words, the circuit performs the mathematical operation known as integration.

The simplest form of integrator is the R-C network shown in Fig. 3. That circuit may be more familiar to you as a low-pass filter. While it does perform that function, it also does, as we'll soon see, a bit more.

In the circuit of Fig. 3, when voltage V_{IN} is applied, a current flows in the resistor to charge the capacitor. Assuming that any load resistors connected across the capacitor are extremely large compared with R1, output voltage V_O reflects the accumulated capacitor charge, and is proportional to the integral of V_{IN}.

There are a number of problems with the simple circuit of Fig. 3, but most of

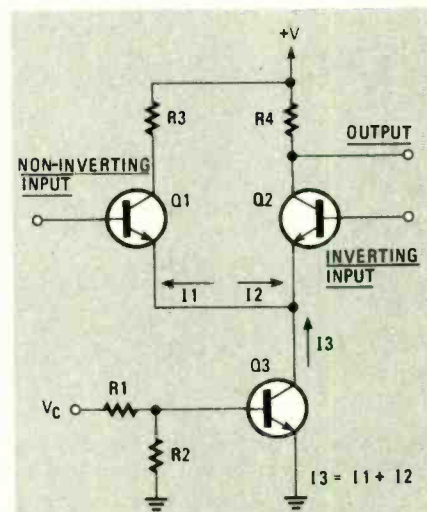


FIG. 1—ONE OF THE MOST COMMON VCA circuits. The differential amplifier can be formed from discrete components as shown, or obtained in IC form.

those are solved by the Miller integrator of Fig. 4.

The Miller integrator consists of a resistor in series with the inverting input of an op-amp, and a capacitor in the feedback loop of the IC. The capacitor charges under the influence of output voltage V_O. The transfer function for the circuit is given by:

$$V_O = \frac{-1}{RC} \int V_{IN} dt$$

where V_O is the output voltage, V_{IN} is the input voltage, R is the resistance in ohms, C is the capacitance in farads, and dt denotes integration over time.

The "gain" of the integrator is controlled by the product RC, which is called the time-constant of the integrator. The general rule is to make RC much larger than the period of the waveform applied to V_{IN}.

There is a problem associated with the time-constant, however. Notice that the R-C (time constant) term is in the denominator. Since that product can be very low, gain can be very high. Consider, for example, the case where R = 100,000 ohms and C = .001 μF (i.e. 10⁻⁹ farads). There the time constant is equal to (10⁵

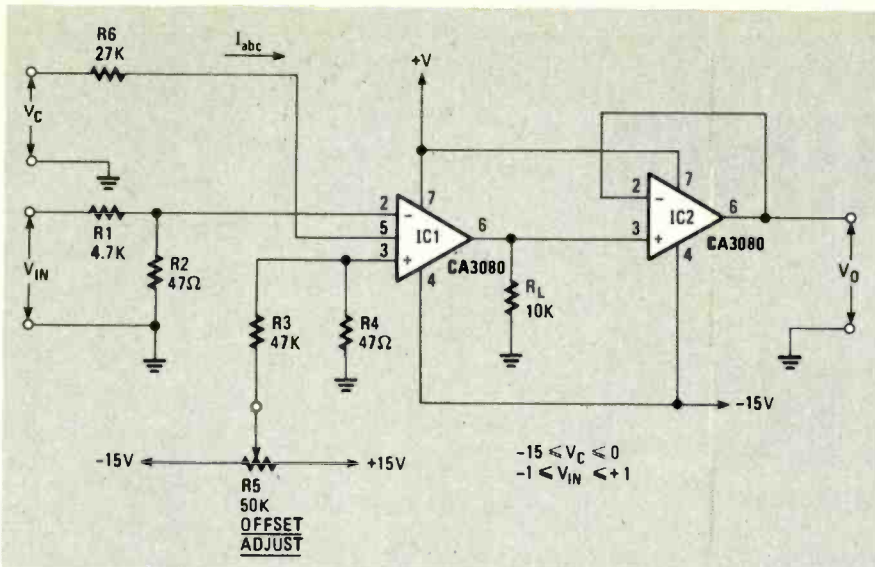


FIG. 2—THIS VOLTAGE-CONTROLLED AMPLIFIER is built using operational transconductance amplifiers. By varying V_c , the gain of the circuit can be made to vary from 0 to 96.

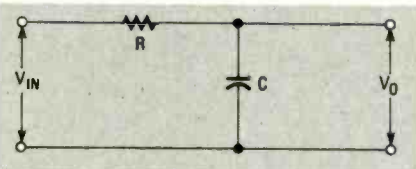


FIG. 3—SIMPLE INTEGRATOR CIRCUIT. It may be more familiar to you as a low-pass filter.

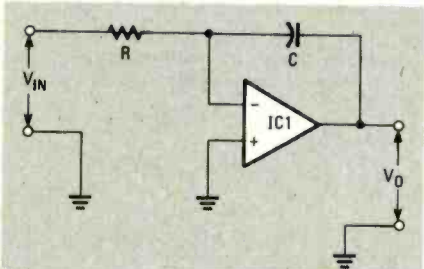


FIG. 4—MANY OF THE DEFICIENCIES of the simple integrator are solved by the Miller integrator shown here.

ohms)(10^{-9} farads) = 10^{-4} seconds. That also results in a gain of 10,000 ($1/10^{-4}$ = 10,000).

What does such a high gain mean in practical terms? It means that very small values of V_{IN} can saturate the integrator in short order! The maximum output permitted, assuming positive and negative supply voltages of 12, will be about 10 volts. If we applied a 10-millivolt DC signal to V_{IN} , therefore, the output voltage rising at a rate of $V_{IN}/RC = 0.01/10^{-4} = 100$ V/S will hit the 10 volt saturation limit in 0.1 second! If there is an input offset potential on the op-amp, or if the signal erroneously contains a DC offset (e.g. from the offset voltage of a previous stage), then the integrator output will rapidly rise to the saturation limit. Of course, shorter time constants than 10^{-4} seconds (0.1 milliseconds) will make the integrator saturate even more quickly.

There seems to be several rules for de-

signing op-amp integrators. Those are to use an op-amp with low input-offset voltages, remove (where possible) erroneous DC offset potentials in V_{IN} , provide offset nulling for the integrator, and use the longest R-C time constant practical in designing the integrator.

The integrator in Fig. 4 is the circuit usually published in texts, and it does not work nicely for the reasons given above. With a typical 741 op-amp for example, typical input offsets cause V_O to rise to $V_O(\text{max})$ so rapidly that you might think the op-amp was shorted! With judicious selection of an op-amp, the modified cir-

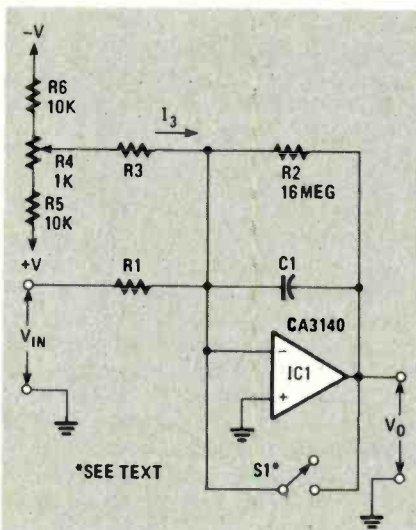


FIG. 5—A PRACTICAL INTEGRATOR. With careful op-amp selection, the circuit shown here will perform well.

cuit shown in Fig. 5 works a lot better.

The selection of an op-amp can be critical, and not all is as it appears in the data sheets. While working on another project,

the author ran a series of tests on op-amps to find those best suited for use in integrator circuits. A test circuit was built that allowed different op-amps to be plugged-in for the test. The integrator used a time constant of 0.1 second, and an input voltage, V_{IN} , of 0. In an ideal integrator, V_O should remain zero. It was found that 741 devices saturated in an average of 2 seconds. The so-called "premium" 725 devices saturated in an average of 5 seconds (still too fast). Other high-priced premium-grade devices saturated in 2-8 seconds. Those rates, it was found, were too fast to easily counteract with the usual null circuit (R3-R6 in Fig. 5). Devices with MOSFET or JFET input transistors behaved themselves much better. Saturation times with those tended to be 20-30 seconds, or more. In the end, we selected the non-premium, low-cost, CA3140 BiMOS op-amp (RCA) as the best device for the integrator design.

The "integration" components in Fig. 5 are R1 and C1; everything else in the circuit is there to "fix problems." The electronic CMOS switch, S1, for example, allows us to dump charge from C1. That charge comes from two sources: previous integrations and output offsets. Switch S1 must be momentarily closed immediately prior to each operation. That switch may be electronic CMOS, mechanical, or a relay. If C1 is very large, however, beware of exceeding the current rating of CMOS switches.

Resistor R2 shunts the integrator capacitor. The purpose of R2 is to keep C1 from being charged by certain offset voltages. Without R2, the output signal zero-baseline will rise to saturation. In one test, we applied a 1-Hz sinewave to V_{IN} and watched the output sinewave climb off the oscilloscope screen. Normally, a symmetrical sinewave will not show any DC component at all at the output of an ideal integrator.

The value of R2 is found by experimentation. If it is too high, then the circuit won't work; if it is too low, then the integrator will act like an ordinary inverting follower with a frequency compensating capacitor across R2! The value 16 megohms was found reasonable with CA3140 op-amps.

What output drift exists is easily counteracted using the null circuit (R3-R6). The input voltage V_{IN} should be zero when that circuit is adjusted. Each time R4 is adjusted, close S1 momentarily to discharge C1. Use either an oscilloscope or sensitive analog DC voltmeter to monitor V_O ; select ever more sensitive ranges as you adjust R4 in order to maximize the change in V_O .

In some cases, R4 may have to have a lower value (100-1000 ohms) in order to obtain better control resolution. In all cases, R3-R6 should have a low temperature coefficient.

Integrator calibration

There are cases where we need some means of scaling or calibrating the output of the integrator. That is done by inputting a function whose integral has a uniform slope over time and then calculating that slope. Two functions have integrals that are appropriate for that purpose: a square-wave and a constant voltage.

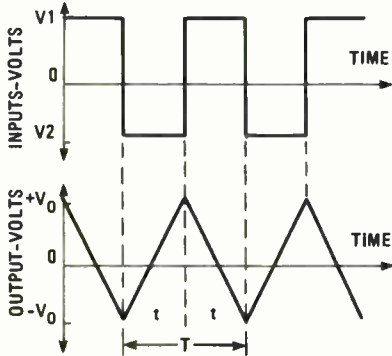


FIG. 6—IF A SQUAREWAVE is input to an integrator, the output will be a triangular wave.

When a squarewave (see Fig. 6-a) is input to an integrator, the resulting output is a triangular wave (see Fig. 6-b). (Note that for a positive input, the output is the negative integral, as is indicated by the circuit's transfer function.) Assuming a symmetrical input, that is $|V1| = |V2|$, the slopes of the ramps that make up the triangular wave are equal to $2V_0/t$, where t is equal to $1/2$ the period (T) of the input squarewave. It is then a simple matter to measure V_0 and calculate that slope.

Figure 7 shows a calibrating circuit for

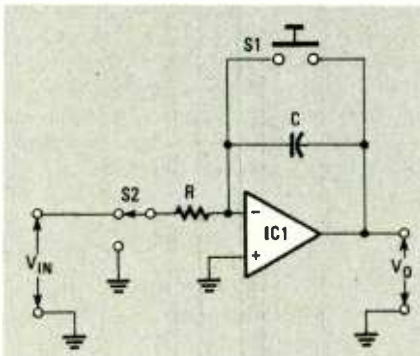


FIG. 7—WITH THIS CIRCUIT, a constant voltage can be used to calibrate an integrator.

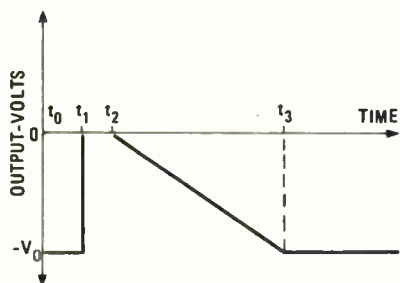


FIG. 8—WHEN A CONSTANT VOLTAGE is input to the calibration circuit of Fig. 7 in the manner described in the text, this output will result.

use when the input is a constant voltage; the resulting output is then a ramp. Initially, the inverting input of the op-amp is grounded via S2. Before starting the test, close S1 to discharge C1; that is done at time $t1$ (see Fig. 8), but don't allow a lot of time to pass before starting the test. A voltage is then applied to the inverting input via S2 for a fixed period of time ($t2$ to $t3$). That will cause the output to decrease uniformly (ramp) from zero down to $-V_0$, which is the output voltage at $t3$. The input is then grounded via S2 and V_0 is measured. The slope of the ramp can then be found from $V_0/(t3 - t2)$.

Differentiators

A differentiator is a circuit whose output is a derivative of the input. In other words, the output voltage is proportional to the rate-of-change of the input signal.

Differentiation and integration are inverse functions of each other. If we apply a time-varying signal, $V_{IN}(t)$, to the input of an integrator, and then apply the integrator output signal to the input of an equivalent differentiator, we should find the differentiator output to be the same as $V_{IN}(t)$ —with a little propagation-delay phase-shift.

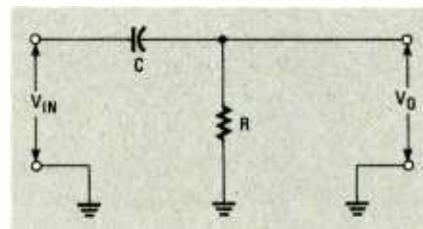


FIG. 9—A SIMPLE DIFFERENTIATOR. The circuit may be more familiar to you as a high-pass filter.

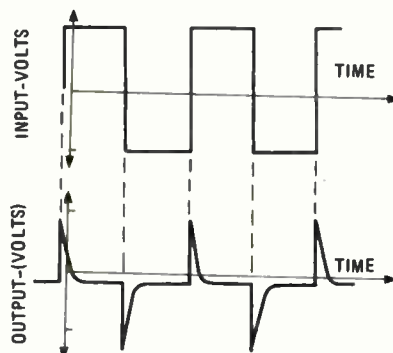


FIG. 10—WHEN A SQUAREWAVE is input to a differentiator, the output is a series of voltage spikes.

The simplest form of differentiator is the R-C network shown in Fig. 9. Note that that circuit may be more familiar to you as a high-pass filter.

The operation of the differentiator on squarewaves is shown in Figure 10. The squarewave is characterized by areas of constant amplitude (zero rate-of-change) sandwiched between edges with extremely rapid rates of change. The result

is a spike-like output wave that is positive for positive-going edges, and negative for negative-going edges. Those spikes will be very broad for long time constants (compared with signal periods), and very thin for very short time constants. A differentiator time constant should be short compared with signal periods.

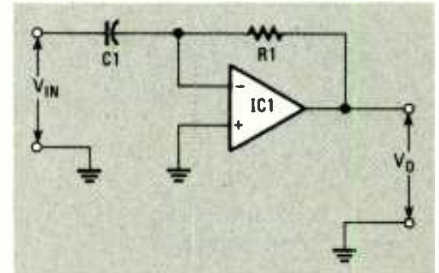


FIG. 11—ALTHOUGH THIS IS a classic differentiator, the circuit tends to be unstable under some circumstances.

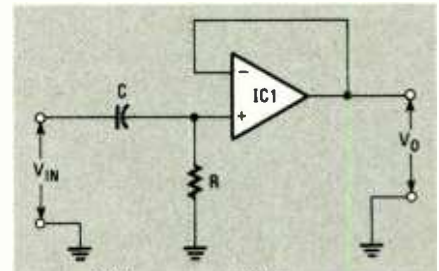


FIG. 12—WHILE THIS CIRCUIT performs much better than the one shown in Fig. 11, it is used only in limited applications.

Two forms of active operational amplifier differentiators are shown in Figs. 11 and 12. The inverting version shown in Fig. 11 is the classic differentiator, and will produce an output potential of:

$$V_0 = -R1C1 \frac{dV_{IN}}{dt}$$

Unfortunately, the circuit of Fig. 11 tends to be a little unstable (i.e. it will "ring") under some circumstances. In a moment, we will see how to "fix" that problem.

The circuit of Fig. 12 merely uses a noninverting operational amplifier (unity gain) to buffer the R-C differentiator output. That circuit is simple, produces a low output impedance for the R-C differentiator, and is generally well-behaved.

Even so, the circuit is not frequently used. More common is a "fixed" version of the circuit in Fig. 11; that circuit is shown in Fig. 13. Two extra components are used to stabilize the circuit: R2 and C2.

A frequency-response plot of that circuit is shown in Figure 14. As is shown, the frequency response of the amplifier (A_{VOL}) is flat from DC to some frequency, at which the gain begins to roll off at a rate of -6 dB/octave. In order to achieve stability, we will want the curve $1/\beta$ to

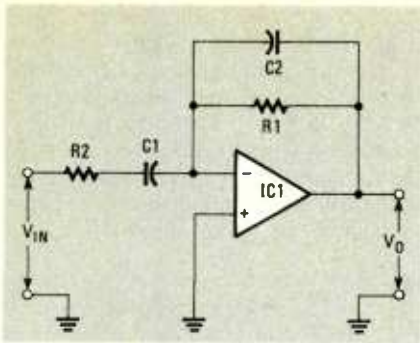


FIG. 13—AN IMPROVED VERSION of the differentiator shown in Fig. 11.

differentiators is that the high-pass filter nature of the R-C networks means that gain increases with frequency. Hence, high frequency noise in active differentiators can be vicious. Capacitor C2 is used to prevent that problem, which creates curve $1/\beta^3$. The value of that capacitor should be found using the following formula:

$$C_2 = \frac{1}{2\pi f_4 R_1}$$

Capacitor C2 will provide integrator action at frequencies above f_4 , and differentiator action at frequencies below f_4 .

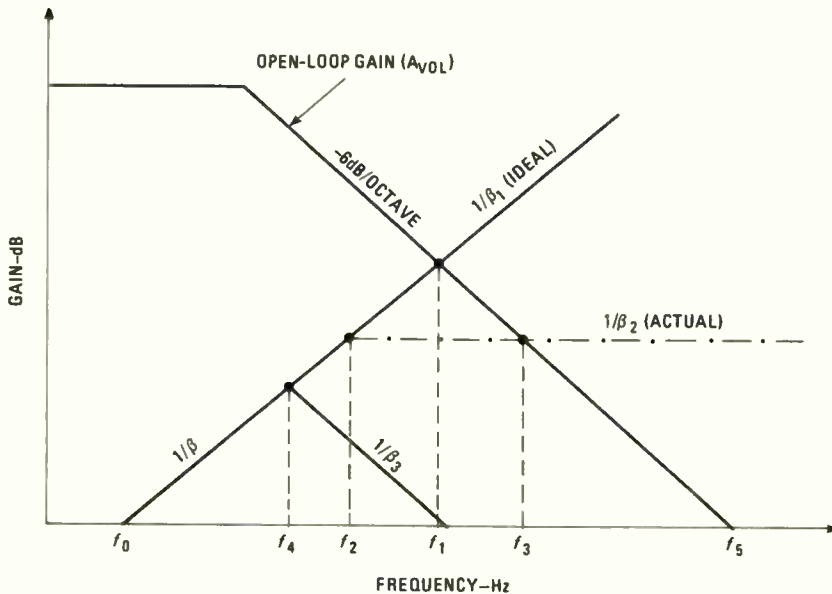


FIG. 14—FREQUENCY RESPONSE plot of the differentiator shown in Fig. 13. Note that the frequency response of the circuit is flat from DC to some frequency, at which point it rolls off at a rate of -60dB/octave .

intersect A_{VOL} with a net slope between them of less than -12dB/octave . (Note: β is the feedback attenuation factor introduced by R_1 and C_1). Since the net slope between A_{VOL} and $1/\beta$ is high, the circuit may tend to oscillate. We must modify the feedback frequency response to make the feedback curve like $1/\beta_2$; that is the function of resistor R_2 , which is in series with C_2 . We want R_2 to introduce a frequency response breakpoint at f_3 . If f_1 is the frequency at which the ideal curve $1/\beta$, intersects A_{VOL} , then f_2 must be 3.16 times lower than f_1 (i.e. $f_2 = f_1/3.16$). The minimum value of R_2 that will accomplish that trick is given by:

$$R_2 = \frac{3.16}{2\pi f_1 C_1}$$

Combining constants yields:

$$R_2 = \frac{0.503}{f_1 C_1}$$

In general, minimum values for R_2 fall in the range of 40 ohms to 500 ohms (although that is not absolute).

Another problem often seen in active

Differentiator calibration

The output signal from the differentiator is proportional to the rate of change of the input signal in volts per second. We can calibrate the differentiator using a function with constant-slope ramps.

One such function is a triangular wave. A triangular waveform has two constant-slope edges, one positive and the other negative. Since the usual op-amp differentiator is an inverting circuit, the output will be a positive voltage for a negative-going ramp, and a negative voltage for positive-going ramps. Thus, a triangle input signal will produce a squarewave output. If the amplitude of the input signal is V_1 , and the period T , then the rate-of-change of each slope is $V_1/(\frac{1}{2}T)$, assuming a symmetrical triangle wave. The amplitude of the output squarewave is 0 to $+V_O$ for the negative ramp, and 0 to $-V_O$ for the positive ramp.

A linear ramp can also be used for differentiator calibration. Such a ramp could be generated by inputting a known constant voltage to a Miller integrator. The differentiator output will be a constant

voltage that is proportional to the ramp slope.

If we want the output signal quantified, then we will have to provide some means to vary V_O for calibration purposes; a variable-gain inverting follower will do the trick nicely and will also flip the polarity so that positive outputs are obtained for positive inputs and negative outputs are obtained for negative inputs.

Let's look at a practical example. Differentiators are used in a wide variety of biomedical applications. One of those is as an arterial pressure amplifier. Assume that the leading edge of a human arterial blood-pressure waveform, $P(t)$, has a rate of change (dP/dt) that's on the order of 5×10^3 mmHg/second (mmHg is millimeters of mercury). A typical arterial pressure amplifier has an output voltage scale factor of 10mV/mmHg , so it will have a rate-of-change output, dV_O/dt , that's equal to:

$$\begin{aligned} \frac{dv_o}{dt} &= \frac{5 \times 10^3 \text{ mmHg}}{\text{second}} \times \frac{10\text{mV}}{\text{mmHg}} \times \frac{1\text{V}}{10^3\text{mV}} \\ &= \frac{5 \times 10^3 \times 10 \times 1}{10^3} = 50 \text{ volts/second} \end{aligned}$$

The differentiator output voltage is:

$$V_O = -RC \frac{dV_o}{dt}$$

$$V_O = -RC (50 \text{ volts/second})$$

We can vary the value of R and C (those are the components used to determine the time constant of the circuit, such as R_1 and C_1 in the differentiator of Fig. 13), and the gain of any following amplifiers, to produce a value of V_O that is easily displayed on, say, a strip-chart recorder. Suppose our strip-chart recorder has a plus-or-minus 1-volt input range, and we want one volt to represent 5×10^3 mmHg/second. The R-C time constant should be:

$$RC = V_O / (50 \text{ volts/second})$$

$$= \frac{(1 \text{ second})(1 \text{ volt})}{(50 \text{ volts})} = \frac{1}{50}$$

$$= 0.02 \text{ seconds}$$

Once we have a value for our R-C time constant, we need to find a combination of R and C that is appropriate. Let $C = 0.1 \mu\text{F}$ (a tentative guess) and calculate R :

$$R = \frac{.02}{C}$$

$$= \frac{.02}{1 \times 10^{-7}} = 200,000 \text{ ohms}$$

We can, therefore, build our differentiator using a 200,000-ohm resistor and a $0.1 \mu\text{F}$ capacitor.

R-E

NEW IDEAS

Contrast meter for photography buffs

IF YOU'RE AN AMATEUR PHOTOGRAPHER who enjoys developing his own pictures, you have probably found it necessary to choose the right paper to fill certain requirements. If you're among the fortunate few who can afford a densitometer, then you have nothing to worry about. But if you're like most of us and cannot afford that piece of equipment, then perhaps this easy-to-build substitute is for you.

Contrast meter

Figure 1 is a schematic of a contrast meter that can be used to help you choose the right grade of paper for your photographic needs. The circuit, built from readily available parts, will work well with almost any photocell and 1-mA panel meter you choose.

The circuit is powered by a dual 15-volt power supply. If you have trouble in getting the parts to build the power supply, then the design can be modified to use a dual 12-volt supply by changing the values of resistors R1, R6, and

R7 to 8200 ohms, 180 ohms, and 560 ohms respectively. The only critical components are resistors R3 and R4, which should be tested to ensure a good 1:3 ratio.

How it works

One leg of the photocell (R1) is tied to the +15-volt supply and the other end is connected to ground through resistor R2, forming a voltage-divider network. The non-inverting input of the 741 op-amp, IC1, is tied to the junction formed by R1 and R2, while its inverting input is grounded through resistor R3. When switch S1 is pressed, another divider network is formed, reducing the the voltage applied to the inverting input of the op-amp (more on that later).

When light hits the photocell, its resistance begins to decrease causing a greater voltage drop across R2 and a higher voltage to be presented to the non-inverting input of IC1. That causes IC1 to output a voltage proportional to the

The circuit gives a meter reading that depends on the intensity of light hitting photocell R1; therefore, R1 should be mounted in a bottle cap so that the light must pass through a $\frac{3}{16}$ -inch hole. Potentiometer R5 is used to adjust the circuit for the negative you're working with.

The diode chain, D1-D3, is used to protect the meter in case direct room light hits the photocell. If the dark resistance of the cell is less than about 1 megohm, it may be necessary to use four diodes, in-
continued on page 88

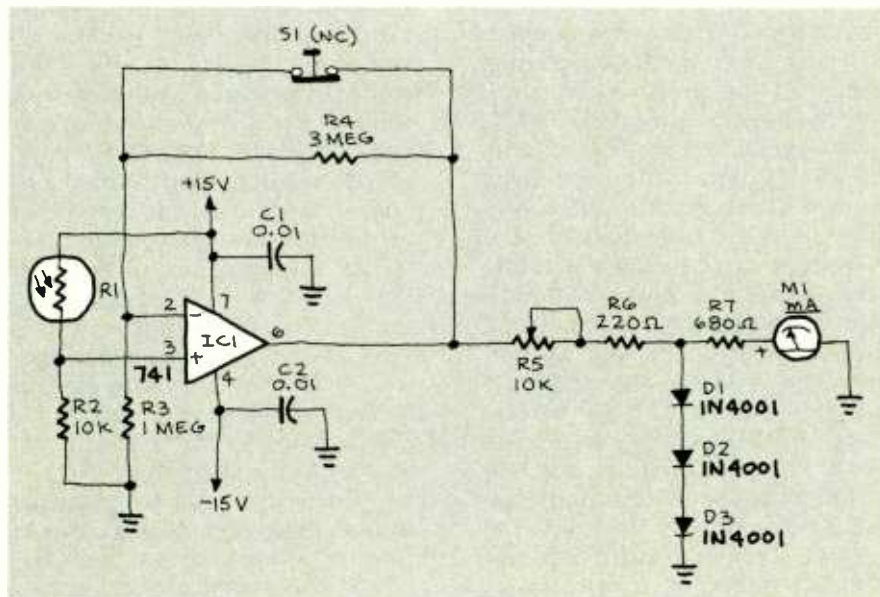


FIG. 1

NEW IDEAS

This column is devoted to new ideas, circuits, device applications, construction techniques, helpful hints, etc.

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HOBBY CORNER

How target games work

THERE ARE A NUMBER TARGET GAMES on the market that use light beams instead of physical projectiles to test one's aim. One of our readers, I. Barditch (MO), wants to know how they work.

Well, Mr. Barditch, rather than just giving you the actual schematic of a commercial product, I'll outline the principles behind those devices to give you some insight on how to go about building your own.

The "gun" (of whatever type) sends a pulse of light when it is fired. The light source can be a regular flashlight bulb, which—if the pulse is extremely short—can be overloaded beyond its normal supply voltage without destroying the bulb. A lens is used to focus the light from the source into a relatively narrow beam.

On the receiving end, you may also find a lens. That lens does two things: It helps prevent stray light from hitting the sensor and triggering a false "hit," and it also focuses the incoming beam on a photodetector.

Figure 1 shows a basic photodetector circuit. The detector itself can be any one of three devices. A cadmium-sulfide photocell will do the job, but that device has a slow response time. You could also use a photodiode or phototransistor. (They work well in this application.) Each device passes current when struck by light.

If the current requirements of the load aren't too great, you could simply connect the load in series with the detector. In the light, the detector would pass current and allow the load (whatever it might be) to operate. Most ap-

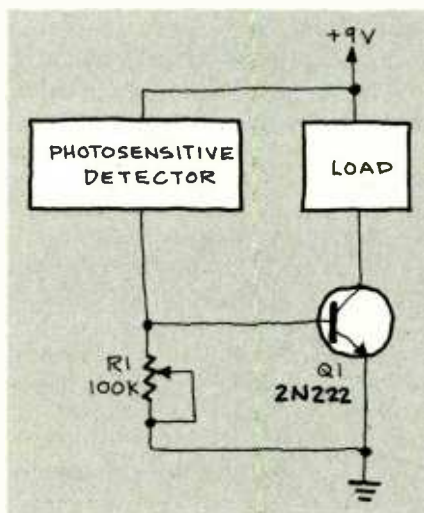


FIG. 1

plications, however, require some type of switching arrangement.

In Fig. 1, transistor Q1 acts as a switch to energize the load. When the base is at or near ground potential, the transistor is turned off and therefore passes no current. However, when the base potential swings in the positive direction, the transistor is turned on and allows current to flow. Potentiometer R1 regulates the switching point of the transistor and therefore acts as a sensitivity control.

The load can be almost anything from a lamp, to a row of LED's, to a sound generator. If the actual load requires a higher voltage or current than available, transistor Q1 may be used to turn on a relay (about 500 ohms at 6-8 volts). The relay, in turn, would control motors, lamps, TV, a sound system, and so on.

If you want to control a device that has heavy current requirements (like a large motor), the little relay could be used to turn on a



EARL "DOC" SAVAGE,
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larger relay, which would then handle the heavy load.

One more point regarding Fig. 1: If you want the circuit to turn on in the absence of light, all you have to do is reverse the positions of the detector and the potentiometer in the circuit.

Well, Mr. Barditch, you should be able to take it from there and build a game or almost any other light-controlled device. Good luck!

Current flow

Back in April's "Hobby Corner" we talked about testing transistors. One reader took me to task for talking about "electron flow." And several others admitted to some confusion about the positive-to-negative and negative-to-positive action used to describe current flow. So, let's see if we can straighten things out. (This effort to simplify and clarify may be repetitious to those who are well versed in this area. If so, just read along and realize that the following is not meant for you!)

First, a bit of pertinent background: Back in the old days (read that as pre-transistor), we in electronics always spoke of electron flow as going from negative to positive. From the action of tubes, especially, it was more than obvious that electricity consisted of the flow of electrons.

Electricians, on the other hand, were equally sure that current flowed from positive to negative. Many an argument took place over the question of who was right. Finally, a compromise of sorts was reached: It was decided that electrons flowed from negative to

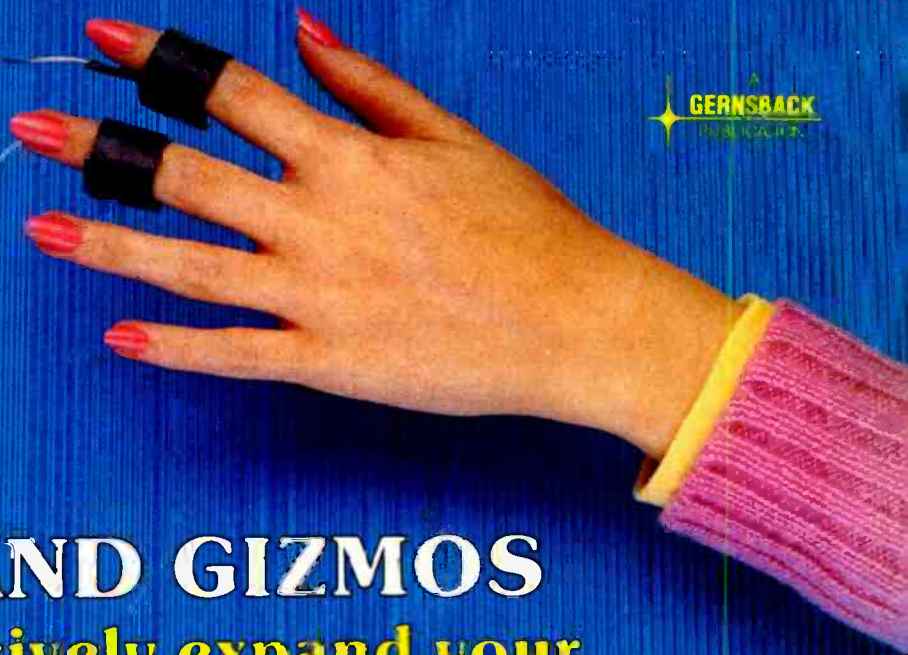
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REBSON	00	
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ON THE COVER

While we're not making any medical claims, biofeedback monitoring seems to help lots of people attain calm. By computerizing the results, you can keep a constant check on how well you're doing. **See page 11.**



EDITORIAL

Platonic dialectic and the computer

■The next generation of computers will have the ability to reason.

Don't expect anything particularly massive at first, for principals have to be explored and tried. But if you tell tomorrow's computer that "All fish live in the water," and that "The trout is a fish," the computer will be able to answer the question "Where do trout live?" by saying "in the water."

This is done by inference. The new generation of computers will indeed be able to draw an inference from information it is supplied, and if you carry this out to extremes, massive changes can be expected.

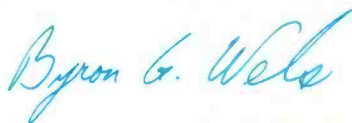
For one thing, today's modern, up-to-the-minute computer will be archaic by comparison. Just as we now compare masses of memory from one computer to another, we will, in the future, be comparing levels of inference. There isn't the least doubt that tomorrow's computers will have the ability to solve, by inference, more and more complex equations. And the more-complex the equation, the better the computer. Another parameter—inference level—will be added to the vast store of requirements that we compare when purchasing a new computer system.

If you stop and think about it for a moment, the applications for inference are legion. In business, in science, why there's hardly an area where sound, logical reasoning can't make a viable, important contribution. Give such a computer the basic elements of a story plot and let it go to work, and it can spit out a 50,000 word novel in the twinkling of an eye! A physician can feed in a series of symptoms, and the computer can make one or more possible diagnoses. "What if" considerations take on a whole new meaning.

According to a recent news story in the New York Times, the reality of this is almost upon us, and is the goal of the 1990's.

With all of this, I am reminded of a class in Basic Philosophy that I took in college, and the proposition was posed as follows: "All fish swim. Some men swim."

What was the logical conclusion? Of course (incorrectly) it's... "Some men are fish."



Byron G. Wels
Editor

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LETTERS

More and better

I wanted to cast a positive vote for your magazine, which I enjoy very much. I'd like to see more space devoted to it each month. How soon will ComputerDigest become a "stand-alone" magazine?—Mark Matson, San Bernardino, CA.

We're really trying Mark, but unless we get sufficient advertising support to warrant standing alone, it might be some time! The reader response has been absolutely wonderful however.

Same authors?

I've noticed that—for the most part—you use the same authors much of the time. I don't quibble about it, for the articles are superlative. I was just wondering.—Frank Sutton, Wilmington, Del.

If you start recognising some of

the names, rest assured that it's only because they're good—and prolific.

Reads editorials

I don't know how other people read your magazine, I suppose that they always begin with articles that catch their fancy first, then go on to others. Me? I read editorials. Your last one, about the future being here today, really struck home. I'm now hard at work on that project, and will have a submission for you shortly. I'm anxious to see what others come up with, too.—Martin Friedkin, Kalamazoo, MI.

Thanks Martin, we're anxious to see what you come up with!

More info

I'm relatively new to computing and saw your magazine at a friend's home. I don't actually own

a computer myself as yet, and was wondering if you could provide me with some information on what to buy?—Charles Horst, Bloomfield, NJ

Charley, that's a tough one. But you're doing the right thing. Read ComputerDigest and ask around. You can't fill yourself with too much information!

Loaded question

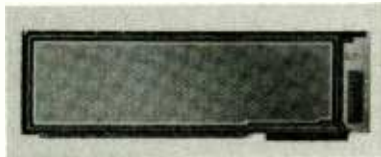
Here's a loaded question for you. My young son is getting deeply involved with computers at school, and I assume that this is good. But how do I keep up with him? He asks questions now that I just can't answer!—Fred Steen, Detroit, MI.

Fred, try an adult education course in computers. You'll catch up, and who knows? Might even develop a brand-new interest for yourself!

COMPUTER PRODUCTS

For more details use the free information card inside the back cover

PROTOTYPING CIRCUIT BOARD, model 4613-3, allows use of both wire-wrap and solder interconnections to speed interface design for IBM PC or XT microcomputers. The model 4613-3 has power and ground buses surrounding the component area on both sides of the board. Plated-through holes, on 0.1-inch centers, mount up to 91 16-pin DIP'S.



CIRCLE 21 ON FREE INFORMATION CARD

Form and plug-compatible with IBM cards, the board may be installed in any expansion slot in the IBM PC or XT. A 31/62-contact card-edge connector with nickel-gold-plated fingers mates

with the IBM system bus. The contacts are chamfered at 45 degrees for easy insertion. The board also has a dedicated area, predrilled to mount 9-, 15-, 25-, or 37-pin miniature connectors for external input/output. A connector-mounting bracket, with cutouts for all four connector sizes, relieves strain on the connector pins.

The model 4613-3 is priced at \$40.28. It comes with complete instructions, including IBM bus signal conventions.—**Vector Electronic Company**, 12460 Gladstone Avenue, Sylmar, CA 91342.

MICROCOMPUTERS, Morrow Inc.'s model MD1E and model MD3E are economy-model business/personal computers aimed at users whose primary application needs are for word-processing software.

The model MD1E features one double-sided, double density 5.25-inch

disk drive and NewWord word-processing software. The model MD3E features two double-sided, double-



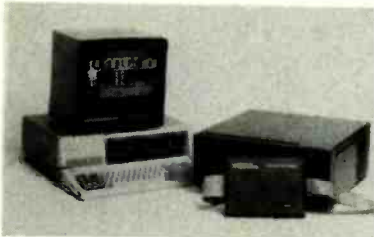
CIRCLE 22 ON FREE INFORMATION CARD

density 5.25-inch disk drives, NewWord word-processing software, and the Correct-It spelling checker. Both systems come with a full-featured terminal and detachable keyboard.

The model MD1E is priced at \$999.00; the model MD3E costs

\$1499.00.—**Morrow, Inc.**, 600 McCormick Street, San Leandro, CA 94577.

EMULATOR PORT, the Kontron PC Interface *KPCI*, turns the IBM *PC/XT* into a universal development system for the design, test, debugging, and im-



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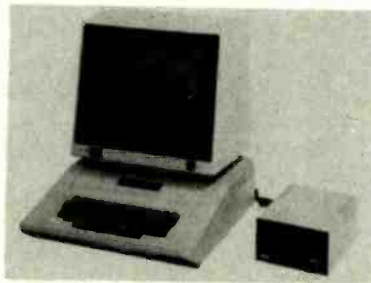
plementation of hardware and software for most microprocessor devices. The *KPCI* package consists of hardware and a set of software tools, including a cross-assembler, linker, emulator software, and additional CP/M utilities. For operation, the *KPCI* requires an IBM *PC/XT* with monitor and DOS. A Kontron emulator subsystem

and Pascal compiler are optional.

The *KPCI* is priced at \$1500.00.—**Kontron Electronics**, 630 Price Avenue, Redwood City, CA 94063.

COLOR-DISPLAY MONITOR, model *SC-100*, is a 13-inch CRT monitor with 90° inline, 0.65-mm dot pitch, and an audio speaker with earphone jack. The model *SC-100* is compatible with Apple II, Apple IIe, Atari 800, Commodore 64, VIC20, IBM, PCjr, T199, and many others.

The model *SC-100* has a resolution of 280 lines horizontal and 300 lines



CIRCLE 24 ON FREE INFORMATION CARD

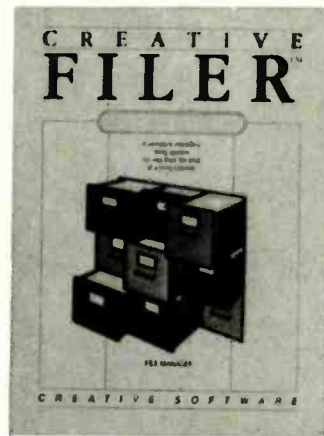
vertical; display format of 1000 characters (5 x 7 dots, 40 x 25), and many other features. It generates 16 different colors. The sound is from a one-watt amplifier coupled to an internal mini speaker.

The model *SC-100* is \$329.00.—**Sakata USA Corporation**, 651 Bonnie Lane, Elk Grove Village, IL 60007.

SOFTWARE SERIES, *Creative Writer*, *Creative Filer*, and *Creative Calc* are designed for use with IBM, Apple, and Commodore 64 home computers.

Creative Writer has all the standard word-processing functions. Documents can be composed, edited, saved, retrieved, and printed. The program is especially slanted for composing memos, letters, and reports that can be detailed by using data obtained from *Creative Filer* and *Creative Calc*.

Creative Filer is an electronic filing system that simplifies data management. Consumers can create computerized index cards on the screen in any format and then add, modify, delete, or browse through alpha-numerically stored data. An added feature allows report formats to be created, to which any stored data can be applied.



CIRCLE 25 ON FREE INFORMATION CARD

Creative Calc is a spreadsheet that simplifies any mathematical process. Numbers are entered and results automatically calculated and displayed on the screen. If a number is changed, *Creative Calc* changes all other related figures to fit the new format. It can be used to summarize and analyze household expenses, plan investments, and play "what-if" with various tax options.

The three programs are priced at \$49.95 each.—**Creative Software**, 230 East Caribbean Drive, Sunnyvale, CA 94089. ◀▶

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CIRCLE 56 ON FREE INFORMATION CARD

GIZMOS

Here's a look at cheap gizmos and expensive gadgets for extra computer power.

HERB FRIEDMAN

■With few exceptions, most of the low-cost personal computers are designed to marry the user to the manufacturer through unusual interfacing, or by providing odd-ball features that can be secured only by using the manufacturer's own peripherals and accessories. While the computer might be jam-packed with programming features such as extended BASIC, graphics, color and sound, getting the end product out of the computer is often difficult if you don't use the manufacturer's own peripherals—which are usually overpriced for what you get.

An IBM PC, on the other hand, is possibly the most expensive personal computer system. The basic package consists of the keyboard, 64K of RAM and a cassette I/O—you must add expensive plug-in interfaces and a monitor just to get a visual display. The price of an IBM soars from about \$1350 (for the basic package) to well over \$3000 if you include disk drives.

But regardless what kind of computer you have, if it's a popular brand such as the Atari, Commodore, Radio Shack or IBM, or almost any IBM-compatible, you can usually do things at much less expense by using the gizmos and gadgets available from what are called *aftermarket* or *third party* vendors. Keep in mind, however, that accessories from aftermarket vendors might not provide all or similar features to those of the manufacturer's own hardware.

Adapters

One of the best-known Commodore serial-to-parallel adapters is the *The Connection* (Micro Ware, 1342 Rt.



THE CONNECTION, FROM MICROWORLD, connects the RS-232 serial output of the Commodore 64 or the VIC-20 to standard Centronics parallel so you can print standard ASCII on any Centronics-input printer.

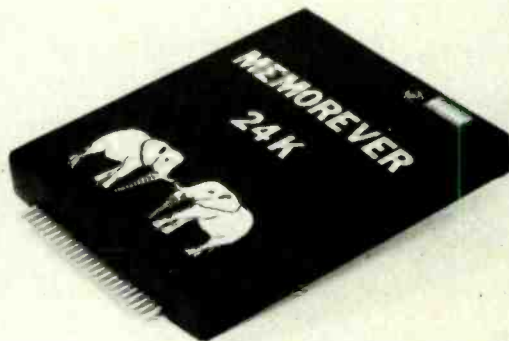
23, Butler, NJ 07405). It is priced well under \$100. Connected between the computer and the printer, it converts the non-RS-232 serial output of the Commodore 64 and VIC-20 computers to standard Centronics parallel, which permits you to print the ASCII character set on any daisy, matrix, or ink-jet printer that has a Centronics-type input. If the special graphics are important to you, check with the manufacturer of the adapter because they often have specific models for emulating the Commodore graphics.

A similar adapter called the *Ape Face*, (Digital Devices Corp., Suite 127, 151 Sixth St., Atlanta, GA 30313) is available for Atari computers. Again, it converts the non-standard Atari printer output to standard Centronics.

It's a different story if you plan on using one of the



APE FACE from Digital Devices Corp., converts a non-standard Atari printer output to standard Centronics.



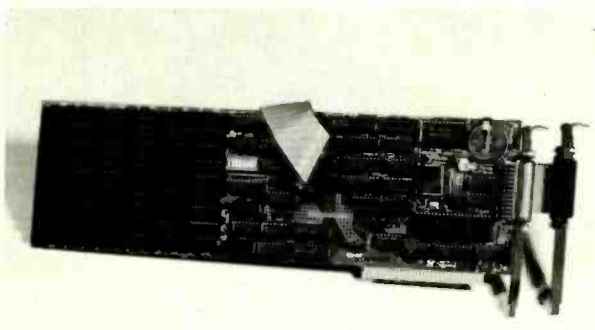
24K MEMORY EXPANSION for the VIC-20 with a built-in lithium battery to keep the memory non-volatile is available from Memotron.



TIGERTRONICS MODEL 770 plugs into the Color Computer's serial input/output and converts serial data to a Centronics-type output.

low-cost parallel printers with a CoCo: They won't work together without some form of accessory RS-232-to-parallel conversion interface. Again, several well-under-\$100 RS-232 serial-to-parallel adapters such as the *Tigertronics Model 770* (Tigertronics, Inc., 1501 Pine St., Oxnard, CA 93030) are available. They plug into the CoCo's serial I/O—which is also the printer port—and convert the serial data to a Centronics-type output for parallel printers. None of the Color Computer printing adapters we know of will make the necessary conversions for emulating the Radio Shack printer graphics. If you need Color-Computer graphics you must use the appropriate Radio Shack printer. Connecting a printer to an IBM-compatible computer is normally expensive because a plug-in board with a serial or parallel printer output is required: A printer output port is not part of the basic computer configuration. However, several multi-function plug-in boards are available which include both parallel and serial I/O.

For example, if you're upgrading the memory in an IBM-compatible you might want to consider using a board such as the Tecmar *CAPTAIN* (Tecmar, Inc., 6225 Cochran Rd., Solon, OH 44139-3377), which provides both a memory upgrade and both serial and parallel



THE CAPTAIN from Tecmar provides a memory upgrade and both serial and parallel ports.

ports. If you start adding up the cost of the memory expansion and I/O of an aftermarket board you'll probably find the total is several hundred dollars less than if you purchased the individual IBM modules, even though the cost of the multi-function board is somewhere in the range of \$225-\$350.

Modems

In order to access a database through the dial-up telephone system you need a modem between the computer and the telephone system. Unfortunately, most of the home/family/small-business computers don't have a standard RS-232 I/O, so it's extremely difficult to connect a standard modem. While most manufacturers sell a proprietary modem for their computer, if you want to enjoy the convenience features of the more common high-performance models—such as the auto-dialing and auto-answer of the Hayes Smartmodem—it can't usually be done unless you connect some kind of interface that provides an RS-232 I/O for the computer. It doesn't make any difference whether the interface matches the TTL logic of the user port (where the game cartridges are plugged in) or the special disk-drive serial port as long as the end product is a standard RS-232 I/O that supports all the "bells and whistles" of RS-232 accessories. Just such a device is the *VIC20/C64 RS-232 Interface* (Omnitronix, Box 12309, Seattle, WA 98111), which plugs into a VIC-20 or Commodore 64's TTL user port and provides an RS-232 I/O that supports pins 2 through 8, 20 and 22...all independent of the others.

If you're interested in writing your own applications programs on a Color Computer, consider using a *mouse* to control the screen functions. Formerly available only for the most expensive personal computers such as Apple's Lisa and the IBM-compatibles, a *mouse* can now be used with a CoCo by simply plugging it in and loading a control program.

While we normally tend to associate memory upgrades with the expensive IBM-compatible computers, they are also available for the least-expensive computers, in particular, the Commodore VIC-20 and the Commodore 64.

The basic VIC-20 comes with only 5K of RAM, which can't do very much unless you're experienced at



THE VIC20/C64 RS-232 interface from Omnitronix plugs into a TTL user port and provides true RS-232 I/O.

writing very tight code. Commodore's own memory upgrades are expensive; aftermarket memory enhancements are often a better value, or, sometimes, something special. For example, Memotron (Box 714, McPherson, KS 67460) sells a *non-volatile* 24K memory expansion for the VIC-20. A built-in lithium battery keeps your program or data "live" after the computer's power is turned off. If you have already partially upgraded your VIC-20's RAM, say with an additional 8K, you can utilize a RAMAX Jr. (Apropos Technology, 1071 Avenida Acaso, Camarillo, CA 93010) plug-in memory expansion board that brings the total memory up to 32K. One of the best accessories for low-cost computers is often nothing more than a cooling fan, usually mounted on the outside of the cabinet. Almost without exception, even on the hottest of summer days, the openings in a computer's cabinet provide a sufficient air flow to keep the internal ambient temperature within safe limits. But the internal temperature can increase sharply when the computer is upgraded with extra internal memory, printer drivers and other accessories not originally provided in the basic purchase, and the "extra" heat can be no end of problems: intermittent memory failures and disk errors, blown fuses, etc. Accessory cooling fans and blowers are available for just about all computers which lend themselves to user-installed upgrades. For example, there is no end to the number and kinds of cooling fans for the Apple II computers. Most are similar to the unit from Jameco Electronics (1355 Shoreway Rd., Belmont, Ca 94002), which fits on the outside of the Apple's cabinet.

Regardless of what kind of computer you have, if it didn't come with an integral fan, an add-on might prove to be the best investment you can make. If nothing else, on a muggy, soggy day it moves the air around inside the cabinet and keeps moisture from settling out on the components and on the sockets.

Higher prices

Moving along to the very high-priced gadgets brings us to accessories designed for IBM-compatible computers. Just about any accessory you can think of is

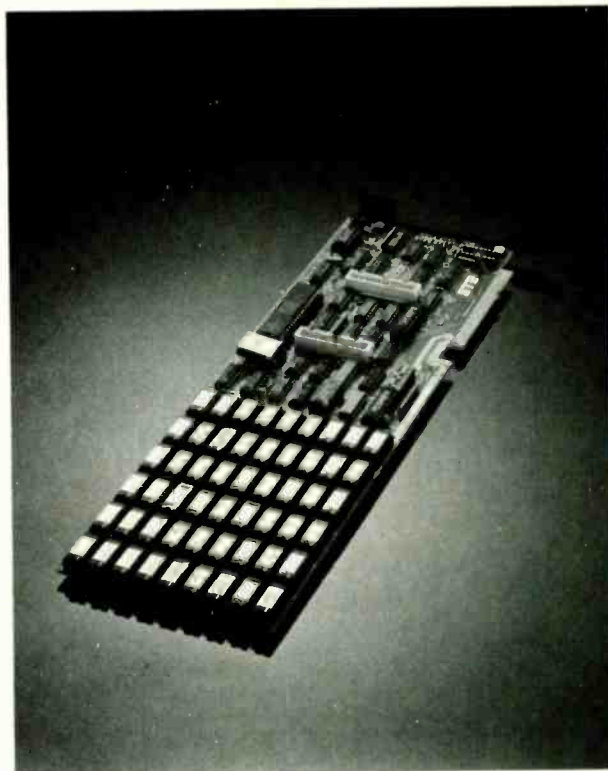


IF YOU UPGRADED your VIC-20's RAM with an additional 8K, add a Ramax Jr. from Apropos Technology, and up it to 32K.

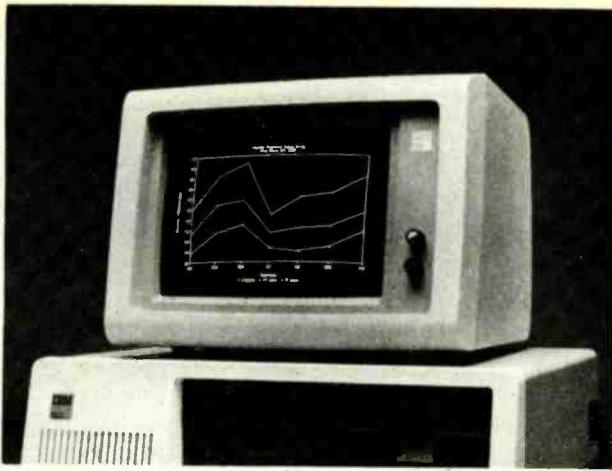


FITTING OUTSIDE the Apple's cabinet, this fan unit from Jameco helps keep things nice and cool.

made available by aftermarket vendors; and if what you want isn't available today, wait until tomorrow. Leading the list of IBM-compatible accessories are the *memory upgrades*, which are often combined with some other necessary features generally sold as a separate plug-in module. For example, the *RIO PLUS* board (STB Systems, Inc., 601 North Glenville, Suite 125, Richardson, TX 75081) can be loaded with 64K to 348K RAM, has a serial port for a printer or modem, a parallel port, a game port, and a battery operated clock/calendar that remembers the date and time even when the computer is turned off. And if the *RIO PLUS* doesn't have enough RAM for your needs, you can add a 512K *piggyback* board for a total upgrade of 768K RAM. Or maybe you're into graphics but aren't ready for the



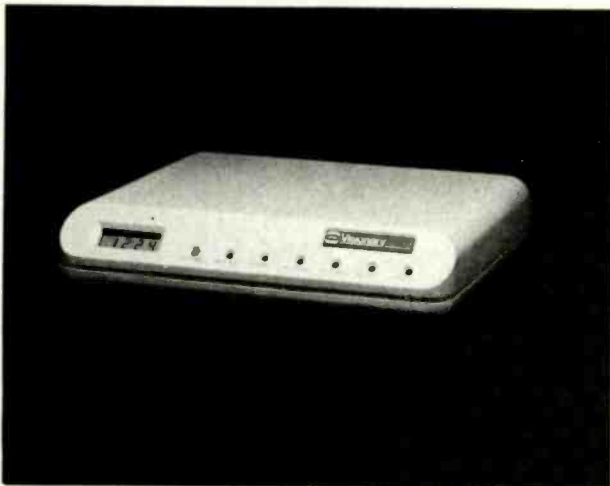
The **R10 PLUS** from **STB SYSTEMS** can be loaded with 64K to 348K RAM, boasts a serial port for a printer, a parallel port, a game port, and a battery-operated clock/calendar.



THE HERCULES GRAPHIC CARD from Hercules Computer Technology delivers high-resolution graphics on both monochrome and color monitors.

extra expense of an RGB color monitor: monochrome would be just fine for your Lotus 1-2-3 graphics. Then look into something called a HERCULES graphic card (Hercules Computer Technology, 2550 Ninth St., Berkely, CA 94710). It delivers high-resolution graphics on both monochrome and color monitors. Many of the RAM upgrade plug-ins can have their memory partitioned to serve as an independent printer spooler, or as a RAMdisk. For those of you unfamiliar with the term, a *RAMdisk* is a block of volatile RAM that emulates a floppy or hard disk, but unlike the mechanically-delayed access of a disk's files, the RAMdisk response is almost instantaneous. As a general rule, the user creates a mirror image of the desired disk data or program in the RAMdisk, which is assigned a drive identifier, such as "M:," "C:," etc. As far as the computer is concerned the RAMdisk is a conventional disk drive that is accessed the same as a mechanical drive, except the response is instantaneous. Most RAM upgrades require a software routine to partition the memory for use as a spooler or RAMdisk.

While we're on the subject of theory, how about a modem such as the *Visionary 1200* (Visionary



THIS MODEM FROM VISIONARY ELECTRONICS has 48K of non-volatile RAM, its own microprocessor, an internal clock, auto-answer, auto-dial, redial, lots of other goodies.



COMPUTER ACCESS CONTROL from Anchor Pad International uses encoded magnetic cards to restrict access to a computer, display, drive or printer.

Electronics, 141 Parker Ave., San Francisco, CA 94118), which has 48K of non-volatile CMOS RAM, its own microprocessor, an internal clock, auto-answer, auto-dial, redial, auto-log on, and data capture. It operates completely independent of the computer. On-board software allows the unit to send and receive messages (data) automatically, even when the host computer is switched off. You can load its memory with data and program the modem to transmit at a specific time, or have the modem turn itself on and receive and store data—which you later load into the computer at your leisure. But whether your computer is a budget special or an IBM-compatible with every imaginable accessory, when you come down to the nitty-gritty, it's the software and data that has the real value.

Protecting the computer

One of the ways to protect individual data and/or restrict general access to a computer is with a device called a Computer Access Control (\$100-\$300 from Anchor Pad International, Inc., 3224 Thatcher Ave., Marina Del Rey, CA 90291.) It uses either a key or a system of encoded magnetic cards (resembling a credit card) to allow only authorized persons access to a computer, display, disk drive, or printer.

The list of gizmos and gadgets for personal computers is almost endless. We have just touched on a few unusual ones. Between the low-cost accessories for the home and family computers and the *budget-busters* for the IBM-compatibles is just about anything you can imagine. The major difficulty is usually finding where to purchase what you need because the computer stores stock just a fraction of the available accessories—and they are primarily for the most popular computers. But dogged determination will usually uncover exactly the accessory or peripheral you're looking for—though in some instances be prepared to mortgage the old homestead. Except for the gizmos intended for home and family computers, upgrading accessories don't come cheap.

BUILD THE BIO-BOX

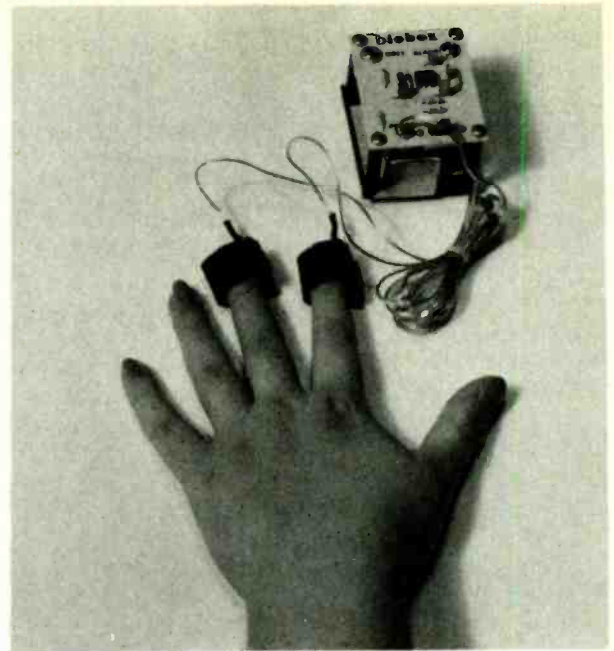
You can build this biofeedback monitor for your TRS Model I or Model III.

JIM BARBARELLO

■ Biofeedback uses an electric device to monitor certain bodily functions and relays how those functions are changing. As you consciously vary your behaviour (thoughts, mood, etc.) you can immediately see how your efforts are affecting your level of tenseness. With practice, you can learn which variations help you to reduce stress. Knowing this, you can practice conscious control of those emotions.

We're not claiming any medical benefits, but it is accepted that biofeedback can help control everyday minor stress. Practice, and it may be able to help you too.

What we're offering here is a hardware biofeedback interface for your Model I or Model III with associated software that allows you to use the interface and



document the results of your trials in a tabular format. The interface (called the BioBox) is simple and inexpensive to build. It monitors the changes in galvanic skin resistance (GSR) between two adjacent fingers on one hand. GSR is a measure of your level of excitation or tenseness. The BioBox is battery powered for safety, requires no modification of the Model I and can be used on the Model III as well. (See the section on "Model III differences.")

The hardware

We'll call the GSR R_{BIO} and measure it with two probes connected to the BioBox. Look at the schematic

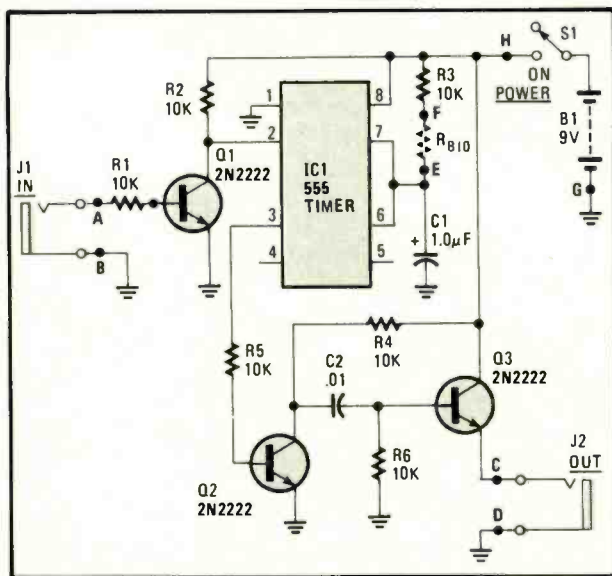


FIG.1—SCHEMATIC DIAGRAM FOR THE BIOBOX shows the relative simplicity of the circuit. The entire unit is built on a printed circuit board.

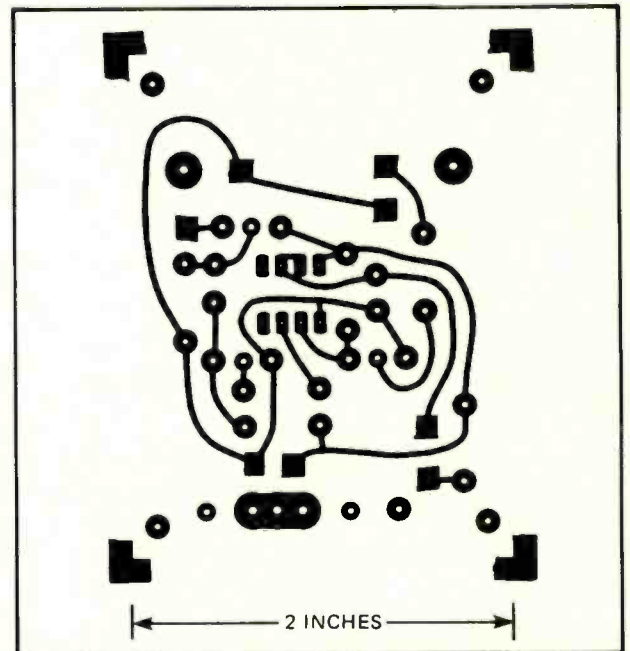


FIG.2—LAYOUT OF THE PRINTED CIRCUIT BOARD is shown full-size for those who want to construct their own.

diagram, Figure 1. The BioBox receives its input from the AUX (large grey) connector on the cassette cable, and provides its output to the cable's EAR (black) connector. Under software control, a short, positive-going pulse is provided to J1. This pulse is inverted by Q1 to trigger IC1 (a 555 timer IC). In the configuration shown, pin 3 of IC1 immediately rises to 9 volts. It stays there for roughly $C1 \times (R3 + R_{BIO})$ seconds (where R3 and R_{BIO} are in megohms, and C1 is in microfarads). After this time, pin 3 returns to zero volt.

At the junction of R4 and Q2's collector, the voltages appear exactly opposite of those at IC1, pin 3. Thus, when the timing cycle starts, C2 sees zero volts. When the timing cycle ends, C2 sees a positive transition to 9 volts. C2 and R6 form a differentiator which converts the positive transition (step) into a positive, short duration pulse. Note that the emitter of Q3 has a 100-ohm resistor connected to it. This resistor is actually in the Model I but forms an electrical part of the BioBox. Q3 acts as an emitter follower, providing sufficient current to the low impedance (100 ohm) load. This positive pulse provided through J2 signals the computer that the timing cycle is complete.

The time between the positive pulse to the BioBox and the positive pulse back to the computer is directly proportional to the values of R3, C1 and R_{BIO} . Since R3 and C1 are constant, any change in duration is a direct result of a change in R_{BIO} . When R_{BIO} decreases, (with increased sweating caused by tension), the duration between pulses is shorter. When R_{BIO} increases (with increased calm), the duration is longer. So the duration is a measure of level of calmness. All we need is a software controller to send out the pulse to the AUX connector and count until it senses a pulse at the EAR connector. The resultant count can then be used in a BASIC program to determine the current level of tension.

Building the BioBox

The BioBox circuit can be constructed on a perfboard, project board or using the printed circuit board of Figure 2. The PCB is recommended, since it produces the best results. Once the PCB has been fabricated, install all components as shown in Figure 3 being sure to observe the orientations of C1, IC1, Q1, Q2 and Q3. Next attach J1, J2, S1 and B1 as shown in Figure 4. The unit may be housed in any suitable case,

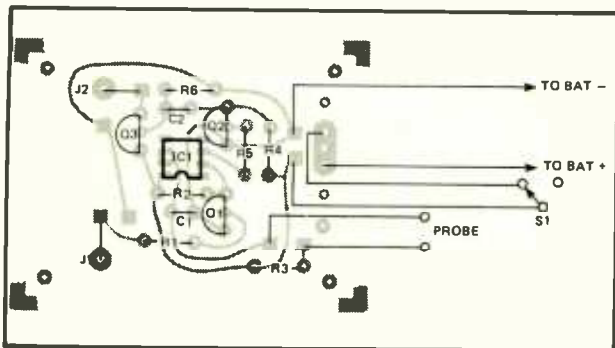


FIG.3—THE COMPONENT SIDE of the printed circuit board is also the panel for the BioBox. Parts placement and locations are shown here.

with the jacks and switch available for use.

The last item to be constructed (and perhaps the most important) is the bioprobe set. It consists of two identical bioprobes which are attached to the index and middle fingers of one hand. Its purpose is to make electrical contact with the skin surface. You will require one package of self-sticking hook-and-loop fasteners, five feet of #24 AWG stranded speaker wire (two-conductor zip cord), two #4-40 \times $\frac{1}{4}$ -inch machine screws, two #4-40 nuts, four #6 washers, a small piece of ordinary aluminum foil and an X-Acto knife. The Velcro comes with two sets of hook-and-loop (Velcro) fasteners, each three inches by one inch. To begin, "unzip" about seven inches of the wire and tie a knot at the end of the separation. Now cut a 1- $\frac{1}{4}$ -in. \times $\frac{3}{4}$ in. piece of the Velcro loop material. Cut one of the "hook" pieces to 3-in. \times $\frac{3}{4}$ in. Using the knife, cut a $\frac{1}{8}$ -in. square in one of the short ends of each of the pieces just formed (See Figure 5.)

Take a 3-inch \times 2-inch piece of aluminum foil and fold it in half, then in half again to form a piece 1- $\frac{1}{2}$ -in. \times 1-inch. Fold each side over $\frac{1}{8}$ -inch to a final size of $\frac{3}{4}$ -inch \times 1- $\frac{1}{4}$ -inch. Remove the backing paper from the loop piece of Velcro and place the aluminum foil on the sticky surface so the $\frac{1}{8}$ -inch folds contact the surface.

On the end of the hook piece where you cut out the square, measure back $\frac{1}{2}$ -inch and make a cut in the backing paper only, so that the half-inch piece of backing paper can be removed. Leave the rest of the backing paper intact. Now place the loop piece on the exposed self-stick surface of the hook piece so the $\frac{1}{8}$ -inch squares align and the aluminum foil is in the middle. (See Figure 6).

Puncture the aluminum foil within the square, but do not remove the aluminum. We only want a hole that will pass a screw. Insert a screw through the square so that the screw head rests against the hook piece. Place a single washer over the end of the screw. Strip $\frac{3}{4}$ -inch of insulation from the end of one of the separated wires, and wrap the exposed wire around the screw. Place another washer over the screw so that the

PARTS LIST (All resistors $\frac{1}{4}$ -watt 10%)

R1—R6—10,000 ohms

Capacitors

C1—1 μ F, 10 volts electrolytic

C2—0.01 μ F, 10 volts, ceramic disc

Semiconductors

IC1—555 Timer

Q1—Q3—2N2222 or PN2222A NPN Silicon Transistor

Other Components

S1—SPST Slide Switch (Radio Shack 275-406)

B1—9-volt battery

J1, J2—miniature phone jacks

Miscellaneous: 5 feet #24AWG Stranded

speaker wire, hook-and-loop fasteners,

aluminum foil, two #4-40 \times $\frac{1}{4}$ -inch machine

screws, #4-40 hex nuts, 4 #6 flat washers, PC-board, cabinet, etc.

insulation comes right up to the washer. Secure this assembly with one nut, but do not rotate the screw while tightening the nut. The foil makes contact with the screw and we do not want to break this contact.

Remove the remaining backing paper from the hook piece. Continually touch the sticky surface so the oils from your hand render it "unsticky." For a faster removal of the stickiness, simply apply a bit of ordinary talcum powder and rub it in.

Repeat these steps to make another bioprobe exactly like the first. Strip 1/4-inch of insulation from the free end of the zip cord. Pass this end through an opening in your case and attach either conductor to either of the two remaining holes in the PCB. Snap a nine-volt battery into place at B1, place S1 to the OFF position and reinstall the circuit in your case.

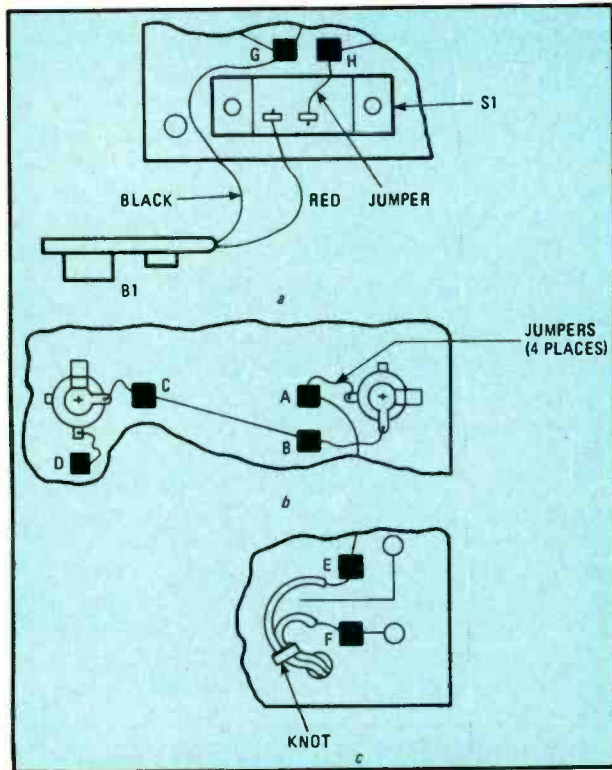


FIG.4—JUMPER REQUIREMENTS are shown in Figures 4A, B, and C. Refer to text for full details and explanations.

The BioBox software

There are two separate elements of software. The first is the machine language subroutine utility. The second is a BASIC program that uses the information provided by the machine language subroutine to perform the biofeedback monitor/human interface.

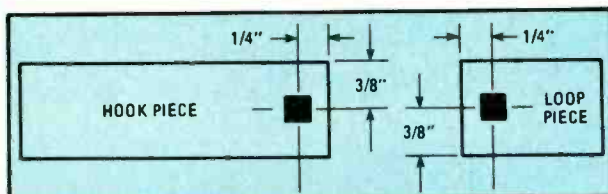


FIG.5—FINGER PROBE dimensions are provided in this drawing. Refer to the text for additional details.

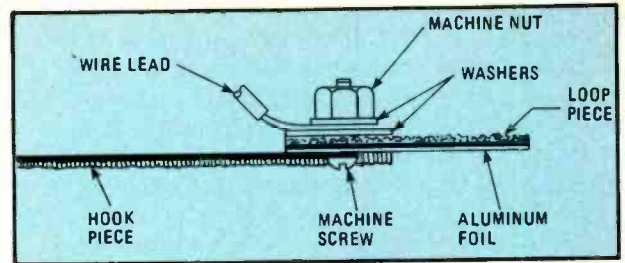


FIG.6.—TO FASTEN, tighten the nut without turning the screw head. Do not tear the foil.

Program Listing shows the machine language subroutine for the Model 1. This subroutine is also contained in DATA values of our BASIC program where, during operation, it will be POKEd into protected memory and called upon via the BASIC USR function. If you're not interested in how it works, you can skip the next section.

Program Listing Table 1 has been ORGed (originated) at 0, since it contains relocatable code and can be placed anywhere in memory. Line 110 disables any interrupt, such as the disk system 25-millisecond real time clock. Lines 120 through 170 send out a positive pulse of sufficient duration to trigger the BioBox.

Next, we initialize our variables. Line 180 sets the DE register pair to 1. This is our counting increment, which will be added to the HL register pair (initialized to zero in line 190). We loop through line 200-240. Each time through, we check to see if a pulse has been sensed from the BioBox. If not, we increment HL and then check to see if it has incremented past FFFF to 0 (causing a carry). This would occur if the timing cycle took too long, or a fault had occurred. If there has been no carry, we loop back to J1 and continue monitoring.

If a pulse has been sensed, or a carry produced, we proceed to J2 where any interrupts are re-enabled (line 250). Finally, we call the ROM routine at OA9AH to transfer our count to the BASIC program.

Let's review

Chances are that if you're like most people who build projects from magazines such as this, you like to work carefully and slowly, and you should. In this issue, you have been given all of the construction details and some of the rationale behind the BioBox. What you will be getting in the next (January) issue, will be Program Listing II and detailed information on how best to use the BioBox.

Working slowly and carefully, you should be well-able to complete the construction by the time you receive the next issue of this magazine. However, we suggest that you assemble the parts, put the unit together, and look it over carefully for such things as solder bridges, excess rosin, and other problem-causing trivia. Stranded wires, such as those that connect the probes to the circuit board, have a way of escaping, and an almost-invisible strand can cause trouble later on.

An interesting point

You might find it interesting to note that since the BioBox operates on galvanic change in skin resistance, it

also makes an excellent lie detector, which can be a lot of fun at parties. While we certainly do not recommend its use as a professional polygraph, the principles are identical and if you establish a line of questions that are designed to elicit humorous information, the BioBox can indeed be an amusing diversion for your guests.

Toward that end, we recommend that you do not simply "breadboard" the unit, but assemble it as carefully and as professionally as you can. Making it look more professional will enable it to command more respect and more credibility.

Other applications

As you work with the unit, other applications are bound to occur to you, and are worth consideration. As an example, since the probes measure skin resistance, it is conceivable that a pair of metal prods could be attached to these, the prods implanted in the potting soil of a plant, and you should be able to thereby indicate when the plant needed additional water.

The important value of the BioBox is that it enables you not only to record, but to store the results of any input information, for recall at any time in the future.

It's a computer accessory that is truly limited only by your own imagination, and one that you will put to excellent use many, many times.

Model III differences

In Program Listing 1, line 140 checks the cassette "ear"

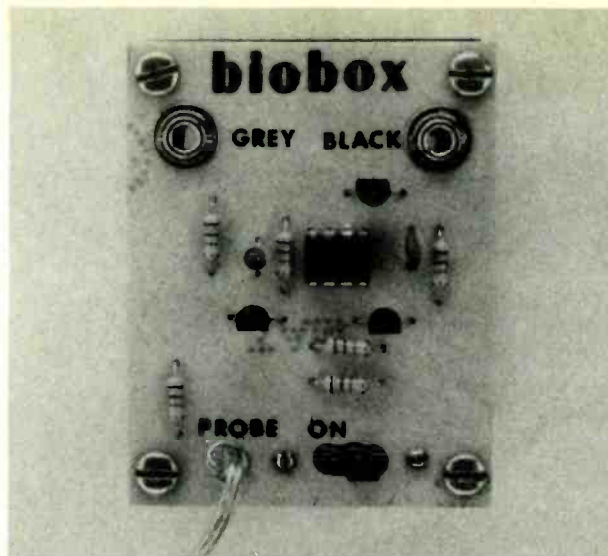


FIG. 7—LOOKING HEAD-ON at the completed BIOBOX, you get a clear idea of where the parts are located, and what the finished project should look like.

input and looks for the number 255. On the Model III, the number we are looking for is 233. So, in line 80 of the Basic program (Program Listing 2, which we'll show you next month), change the second "255" to "233" (i.e.- 80 DATA 0, 0, 219, 255, 254, 233...). This, of course will decrease the checksum, so modify line 50 by changing the number "3647" to "3625." (i.e IF K <> 3625 THEN...). Finally, the Model III will display a right bracket instead of an up arrow. So change the declaration of T\$ in line 140 to T\$ = CHR\$(94) + "TENSE." With these changes made, the BioBox is compatible with the Model III.

Well, it looks as though we've run out of space for this issue, but don't be concerned. In our next issue (January, 1985) we'll finish the article with the necessary program listings and software plus more information on how to use the unit.

That's going to give you a full month to work on your BioBox, assemble all of the parts and put it all together. We'll be talking about it some more. ◀▶

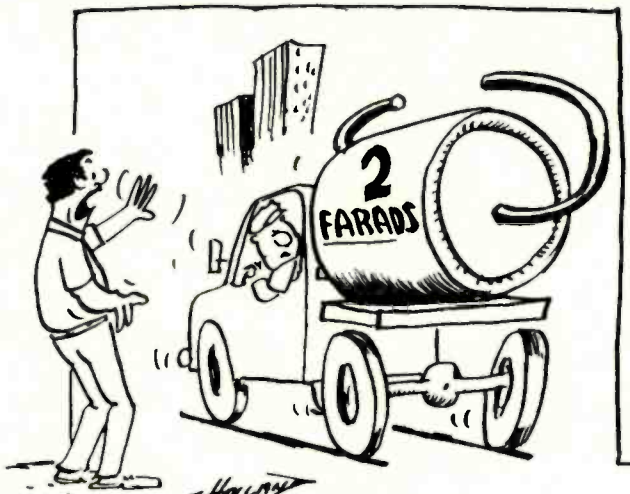
PROGRAM LISTING 1

```

00010 ;BIOBOX MACHINE
00020 ;(REQUIRES BIOBOX
;VERSION 1.0 - 19 FEB 1983
BF04 00030 ;ORG 48900 ;FOR 32K
BF04 F3 00040 DI ;DISABLE 25 MS
;INTERRUPT
BF05 3E01 00060 LD A, 1 ;"AUX" OUT TO
BF07 D3FF 00070 OUT (255),A ;0.8 V D.C.
BF09 0640 00080 LD B,64 ;KEEP IT THERE
BF0B 10FE 00090 JMP DJNZ JMP ;FOR AWHILE.
BF0D 3E00 00100 LD A,0 ;RETURN "AUX"
;OUT
BF0F D3FF 00110 OUT (255),A ;TO 0.4 V D.C.
BF11 110100 00120 LD DE,1 ;INCREMENTOR
BF14 210000 0130 LD HL,0 ;COUNT
;STORER
BF17 DBFF 00140 J1 IN A, (255);CHECK "EAR"
;IN.
BF19 FEFF 00150 CP 255 ;TRIGGER
;SENSED?
BF1B 2803 00160 JR Z, J2 ;IF SO, DONE.
BF1D 19 00170 ADD HL,DE ;OTHERWISE,
;HL=HL+1
BF1E 30F7 00180 JR NC, J1 ;COUNT<65536
BF20 FB 00190 J2 EI ;RE-ENABLE
;INTERRUPTS
BF21 C39A0A 00200 JP 0A9AH ;RETURN HL TO
;USR VAR.

0000 00210 END
00000 TOTAL ERRORS
J1 BF17 00140 00180
J2 BF20 00190 00160
JMP BF0B 00090 00090

```



"Hold it! I said two MICRO farads!"

PATCHING WORDSTAR

You can use the *INSTALL* program to modify or "patch" *Wordstar* for use with your Epson MX-80 printer.

KIRK VISTAIN

I bought the Epson *MX-80* printer because it offered such features as superscripts, subscripts, italic and double-width, features that I really wanted. But these were not even listed as options in the *WordStar* program. Despite all my efforts, the printer kept ignoring my requests for these.

Now, after a few keystrokes and some concentrated effort, I'm getting what I paid for, and all it took was a little "patching."

An applications program, such as *WordStar*, is made up of many lines of numbers and mnemonics (English-like names for variables, such as DEL1 for Delay 1), called code. When we use a special program to change some of this code, we are said to be "patching."

Fortunately, *WordStar* comes with an *INSTALL* program. This allows us to easily customize a system. Unfortunately, trying to figure out how to do this from reading the "documentation" is frustrating unless you have a degree in computer science.

Desired modifications

I basically wanted to access five special Epson *MX-80* functions from within *WordStar*. According to the printer manual I could enable them with the following ASCII (American Standard Code for Information Interchange) characters (See Table 1).

To make things more interesting, we'll find that the ASCII codes used to control the printer must be converted to their hexadecimal (base 16) values before being entered into the patch areas. Don't let this intimidate you. I'll list both ASCII and hex values for all the functions.

Of course, any text fed to the printer is also in ASCII. So how does it know when to interpret the code as text, and when as a command? Well, some ASCII characters are specifically reserved for control. But there aren't enough of those to cover all Epson options.

FUNCTION	ON	OFF
1. Compressed type	S1	DC2
2. Double Width type	ESC W 1	ESC W 0
3. Italics	ESC 4	ESC 5
4. Superscript	ESC 2 0	ESC H
5. Subscript	ESC S 1	ESC H

So we have to use the escape (ESC) code. Its hexadecimal value is 1B. By prefixing this number at the head of an ASCII command string, we tell the printer to interpret the next character as a command. How does the Epson know when to exit the command mode? We include this information as the first number in the patch. Let's begin.

Making the changes

To begin with, we'll assume that you have a properly installed *WordStar* program for your machine. Make a copy of it using the facilities of your operating system. Never make changes to the distribution disk! You should be running an installed copy, and the original should be filed away. We are now going to alter one of those copies.

Load the *WordStar* *INSTALL* program. It will ask you whether you want a normal, first-time installation. You answer "NO" and are given four choices. B or C will be the correct answer. You will then be prompted to give the file name of the pre-installed *WordStar* to be modified. This is usually *WS.COM*. You will then be asked to name the new version.

Something like *WSA.COM* would do nicely.

You will then see several menus in succession and be asked to designate your terminal type, etc. Since you are modifying an otherwise working program, you should answer "U" which indicates "no change." Continue until you reach the query "Are modifications to *WordStar* now complete?" Answer "No."

This enables the patcher routine. Individual patch locations are identified by a mnemonic followed by a colon. For example, *PALT:* is the entry point for the alternate type patch. If you don't use a colon, you'll get an error message.

An actual patch consists of a string of numbers. The first one usually designates how many others are to follow. The rest are ASCII or other special codes. Remember that all the numbers are entered in hexadecimal, or base 16 format. Decimal numbers will not be recognized by *WordStar*. See Table 2.

MNEMONIC	HEX VALUE	ASCII
RIBBON:	03	
RIBBON: +1	1B	ESC
RIBBON: +2	57	W
RIBBON: +3	01	
RIBOFF:	03	
RIBOFF: +1	1B	ESC
RIBOFF: +2	57	W
RIBOFF: +3	00	

We used the ribbon-change area for double-width type. We won't be needing that function on a dot-matrix printer. The Epson manual, Appendix B, incorrectly lists 61H as the code; 57H is the correct one.

Use of double-width type requires you to adjust line lengths to account for half as many characters horizontally. Also, the double-width command is a toggle, which means that the first invocation turns it on,

**TABLE 3
ITALIC TYPE**

MNEMONIC	HEX	ASCII
USR1:	02	
USR1:+1	1B	ESC
USR1:+2	34	4
ROLUP:	02	
ROLUP:+1	1B	ESC
ROLUP:+2	35	5
ROLDOW:	02	
ROLDOW:+1	1B	ESC
ROLDOW:+2	35	5

the second off. This is unlike some other features which require different commands for on and off. (Table 3.)

Now a \wedge PQ will turn on italics and either a \wedge PT or \wedge PV will turn it off. Although you might have thought we would use the ROLUP and ROLDOW patches for scripting, since they correspond to *WordStar* commands for these functions, it doesn't work.

Subscripts and superscripts

Scripting on the Epson is done with a special type font. This font is enabled with an "ESC S n" string where "n" determines whether a "sub" or "super" is printed. If "n" is "0" printing occurs at the top of the line. If non-

TABLE 4

MNEMONIC	HEX	ASCII
USR2:	03	
USR2:+1	1B	ESC
USR2:+2	53	S
USR2:+3	01	
USR3:	03	
USR3:+1	1B	ESC
USR3:+2	53	S
USR3:+3	00	
USR4:	02	
USR4:+1	1B	ESC
USR4:+2	48	H

zero, printing occurs at the bottom. An "ESC H" turns either off. See Table 4.

Compressed type

Our next change will be to the alternate type patch area, called PALT, where we'll install the compressed type option. On the Epson MX-80, an ASCII SI (Shift In) enables compression and DC2 (Device Control 2) shuts

TABLE 5

MNEMONIC	HEX	ASCII
PALT:	01	
PALT:+1	0F	SI
PSTD:	01	
PSTD:+1	12	DC2

it off. The patch in Table 5 will accomplish this.

Also, this is the only patch for which we don't use the escape code. When the MX-80 gets the Shift In (SI) command, it starts to print in italics. The Device Control 2 (DC2) code shuts italics off.

I forgot to initialize the printer before each test run. Functions set in one test would remain in the printer's memory and interfere with the next printing run in unpredictable ways. I needed to turn the printer off and back on again, which would have reset all functions.

Fortunately, there is a way to do this automatically. We patch the printer initialization area, which sends out a code to reset all special functions and TOF (Top Of Form), at the beginning of any printing run. It also sets the printhead to the left margin of the paper. It's just as if you'd turned the printer power off and then on again, but it's done in the software. Refer to Table 6.

TABLE 6

MNEMONIC	HEX	ASCII
PSINIT:	05	
PSINIT:+1	1B	ESC
PSINIT:+2	40	
PSINIT:+3	1B	ESC
PSINIT:+4	4F	O
PSINIT:+5	0D	CR

New *WordStar* printer commands

Now that we've modified *WordStar*, we need to use the following codes, some of which are different from those for which *WordStar* is initially set. All of the commands in Table 7 are accessed from the *WordStar* printing menu, so must be preceded by \wedge P.

TABLE 7

COMPRESSED TYPE	A
STANDARD TYPE	N
DOUBLE-WIDTH TOGGLE	Y
ITALIC ON	Q
ITALIC OFF	T or V
SUPERSCRIP ON	E
SUBSCRIP ON	W
SUB/SUP/DOUBLE OFF	R

THIS IS DOUBLE WIDTH TYPE.
THIS IS ITALIC TYPE. THIS IS COMPRESSED TYPE.
THIS IS A SUPERSCRIP THIS IS A SUBSCRIP.

FIG.1—WHEN YOU COMPLETE the patching job, you'll find that your Epson MX-80 printer and the *WordStar* program can provide even more printing versatility.

See Figure 1 for samples of the results.

These modifications to *WordStar* ought to help you get the most from its partnership with the versatile Epson MX-80 printer. There are even more patches which can help you customize *WordStar* to match your own needs. But that's another story. \blacktriangleleft \blacktriangleright

positive (called *electron flow*), and current flowed from positive to negative (known as *conventional current flow*). The electricians were happy because we stopped giving them a hard time. We were also happy because they made similar accommodations.

These days, most textbooks covering the subject usually refer to the direction of current flow as going from positive to negative, and that's convention most widely accepted in electronics. However, my own point of view is that it doesn't matter which current convention you use. If it works for you, why worry about it? But when you talk to other people, try to stick to conventions. *Current* flows from positive to negative (even though *electrons* flow from negative to positive).

Tracking the sun

Last year, (June, 1983) "Hobby Corner" carried some suggestions for a control circuit for tracking the sun with a solar collector. Now one of our readers has volunteered to communicate directly with others interested in that subject about his own system. If you would like information on the system, write: Jim Huskey, Box 26 Gate Circle, Lexington, NC 27292. Thanks, Jim, for the offer.

Radio

One of the more popular fields in your inquiries is radio—CB, ham, etc. Tim Martin (NY) and George Boone (VA) sent in the most recent letters about radio. Perhaps my answer to them will help others of you who are radio hobbyists.

Tim is having difficulty adjusting his antenna with an SWR/watt meter. The process does seem straightforward but it can get tricky, especially on a mobile installation. A grid-dip meter can do the job, but using that instrument can be even trickier. My own preference is a simple field-strength meter: You can hardly go wrong with that little beauty.

George, on the other hand, is looking for schematics and instructions on constructing simple CW (Morse code) transmitters and receivers for use on the ham

bands. He would also like to know where to purchase used equipment. One source of used equipment is any "hamfest;" you'll find plenty of stuff there, but be sure it functions to your satisfaction before parting with your hard-earned money!

I don't want to sound like a broken record but Tim and George should check the publications of the ARRL (American Radio Relay League, Newington, CT 06111). That is the best single source I know for information useful to radio hobbyists. Their books range from the general to the specific, and from the highly technical down to good solid information for the electronics beginner.

Your local library should have some of the ARRL publications. If they don't, or their selection is too limited, be advised that you don't have to be a member of the ARRL to ask them to send you a list. (Donald Mitchell and Victor Ducot, have you guys been paying attention there in California and Puerto Rico?)

By the way, that local library (or the larger one in a nearby city) is an excellent place to go when you are looking for construction information on some specific device. Until you can build up your own library of back issues of magazines, look through theirs. You may be surprised at what you'll find. Oh yes, check out past issues of **Radio-Electronics** first! **R-E**

STATEMENT OF OWNERSHIP, MANAGEMENT AND CIRCULATION	
FOR THE YEAR ENDING 1983	
1. TITLE OF PUBLICATION RADIO-ELECTRONICS	DATE OF FILING 7/21/83
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DESIGNER'S NOTEBOOK



ROBERT GROSSBLATT

A simple solution to switch debouncing

SOME OF THE BIGGEST HEADACHES that show up in circuit design have absolutely nothing to do with electronics. That is, after you've spent all kinds of energy in taming electrons, the time comes when you have to connect the circuit to the outside world, and that's when the real trouble begins! Mechanical switching of electronic circuits is always an "iffy" business; and any designer who doesn't know that couldn't possibly recognize the symptoms, much less, solve the problem.

The most common causes of circuit "insanity" is what the data books refer to as *input-signal conditioning* or what the rest of the world calls debouncing. No mechanical switch is perfect, no matter how well it's made. As a result, pushing down on that little red button is going to generate more than one pulse. Any circuitry that's being triggered by that pulse is going to do exactly what it was designed to do—respond to each pulse it "sees."

There are all sorts of schemes to handle the problem. For one, you can use more expensive non-mechanical switches, or simply redesign the front-end of your circuit to respond to only one pulse. But the easiest way is to debounce the switch. There are dedicated IC's that can be used for that purpose but, as with most other things, there's an easier way.

Debouncing circuits

The basic idea behind all switch debouncers is to put some type of isolating circuit between the switch and the circuit being triggered. The job of the extra circuit

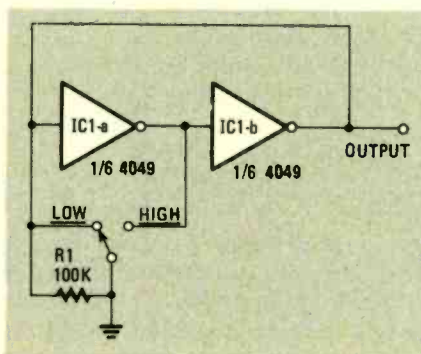


FIG. 1

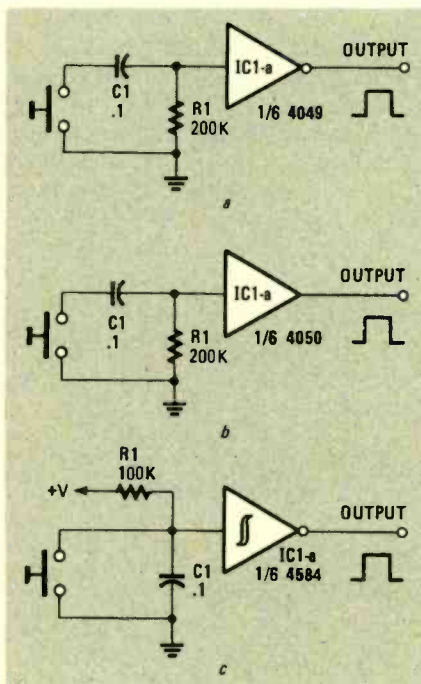


FIG. 2

is to output one (and only one) pulse no matter how many bounces it "sees" from the switch. You can use anything from a flip-flop to a 555 timer (set up as a one-shot), but the problem can be handled a lot easier with inverters.

The most straightforward approach is to build a simple latch

like the one in Fig. 1. Throwing switch S1 one way or the other will change the state of the output. Since there's always some period of time during which no connection is made, resistor R1 is added to keep the circuit from glitching when the switch is thrown. That circuit is ideal for applications where you want to switch from one state to another. Even the noisiest single-pole, double-throw switch can be used because the resistor acts as a temporary storage device while the switch is being thrown.

The real problem appears when you want to use momentary (push-button) switches. That's because those switches are notoriously noisy, and if you don't take several precautions, they can screw up the operation of any circuit—no matter how well it's designed. Fortunately, there are two simple circuits that can take care of the problem.

The circuits in Fig. 2 are *half monostables* or edge detectors made from a single gate. The only difference between Figs. 2-a and 2-b are the gates: One is inverting and the other non-inverting. (We'll get to Fig. 2-c in a moment.)

As you can see, the way the circuit responds depends on which end of the supply rail is tied to the resistor. The capacitor integrates the incoming switch bounces and causes the gate to change states. The capacitor then starts to discharge through resistor R1, and the gate (IC1) doesn't change back until its threshold voltage has been reached.

If you're still in the design stage of your circuit, you can add an ex-



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Radio-Electronics mini-ADS

tra IC to the board and get six (pushbutton) switch debouncers or three double-pole, double-throw debouncers. Doing the same thing with circuitry that's already in the circuit-board stage is a bit more difficult; you'll have to make a small "outrigger" board for the inverters. Remember that almost any inverting logic will do the job, so hunt around your design to see if you have any unused gates.

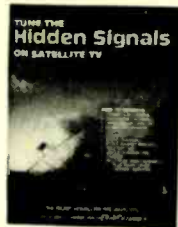
The values for the passive components depend on the type of switches you're using. In general, you should make sure that the output pulse is much longer than the switch bouncing. A good rule of thumb is to aim for at least a ten-to-one ratio. An output pulse width of 10 milliseconds should handle most bounce problems quite nicely. The values given in Figs. 2-a and 2-b should work for most applications. Just remember that the inverting gate will change the polarity of the input pulse, and the non-inverting one will preserve the polarity.

Although you can use any high-gain inverter to make a half monostable, the best all around choice is the Schmitt trigger. Not only do they have enough "zip" to respond properly, but its built-in hysteresis means you can get longer output pulses.

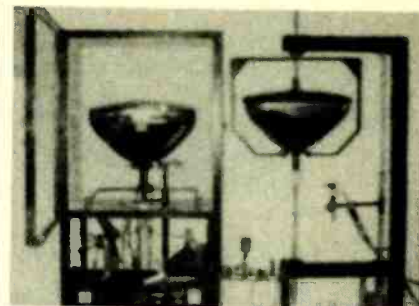
Half monostables use the capacitor as an integrator, but you can also use it as a "sponge" to absorb extra pulses from the switch, as shown in Fig. 2-c. When the switch is open, the input to the gate is held high, forcing the output of the IC low. If there's bouncing when the switch is closed, the R-C time constant keeps the glitching from affecting the output state of the gate. Just as we saw earlier, though, make sure that the time constant is going to be at least ten times the bounce time.

A lot of bench time has been wasted because pulses from a "bouncing" switch were masquerading as some other, more serious problem.

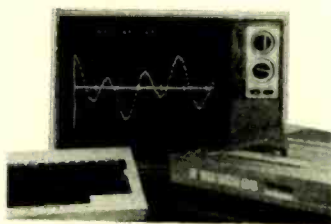
One more thing: It's been a couple of months since I started the one-gate design contest in August, and so far the number of entries has been disappointing. So, let's get with it you guys! R-E



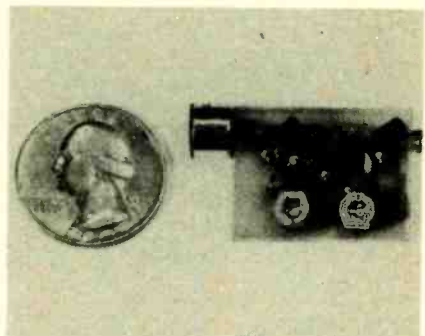
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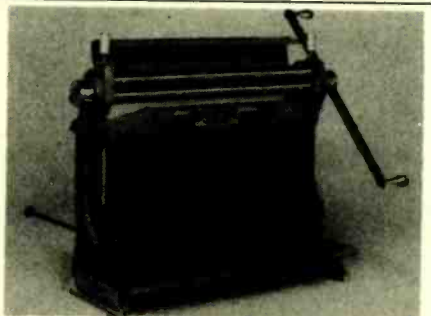
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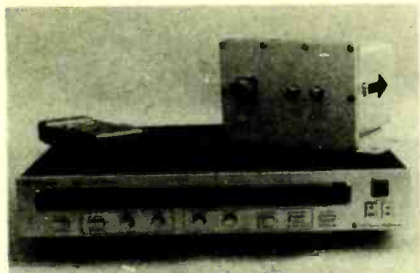


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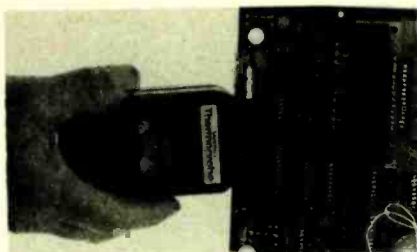
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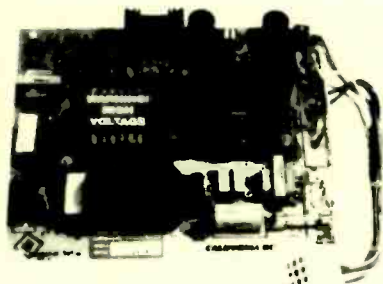
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ROBERT F. SCOTT,
SEMICONDUCTOR EDITOR

Power op-amp IC's

POWER OP-AMPS ARE RELATIVELY NEW arrivals on the semiconductor scene, and they've brought with them several interesting applications. One such device is the L272 dual, power op-amp from SGS. A pinout of that device is shown in Fig. 1-a, and a schematic of one op-amp contained in the package is shown in Fig. 1-b.

Housed in a 16-pin, power-DIP package, the IC is intended for various applications including servo amplifiers and power supplies. The L272 can operate from either single or split power-supplies ranging from 4- to 28-volts DC. Its output current can range up to 1 ampere. Other pertinent electrical characteristics are given in the table in Fig. 2.

The wide voltage range of the L272, along with its current-handling capabilities, make the unit ideal for controlling low-voltage DC motors. Therefore, it should find many uses in the fields of remote control and robotics. The data sheet includes such applications as a motor current control and a bidirectional DC-motor control (with or without micro-processor-compatible inputs).

Figure 3 shows a circuit using the L272 that's designed as a position control for automobile headlights. However, it may be used along with a surplus gear-motor for positioning heavy ham or CB beam antennas. And if you're interested in building satellite TVRO equipment, the circuit might be used in a motor-drive system to aim the antenna dish at various satellites.

The circuit is a bridge arrange-

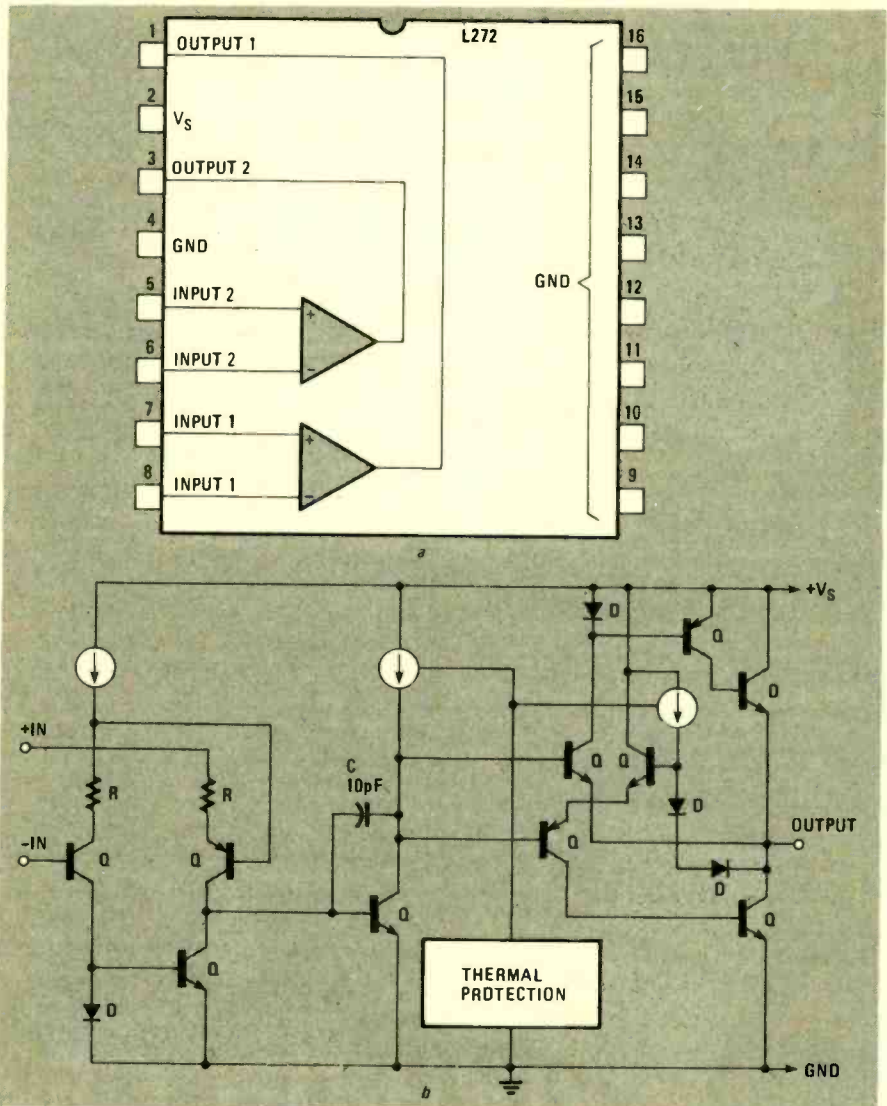


FIG. 1

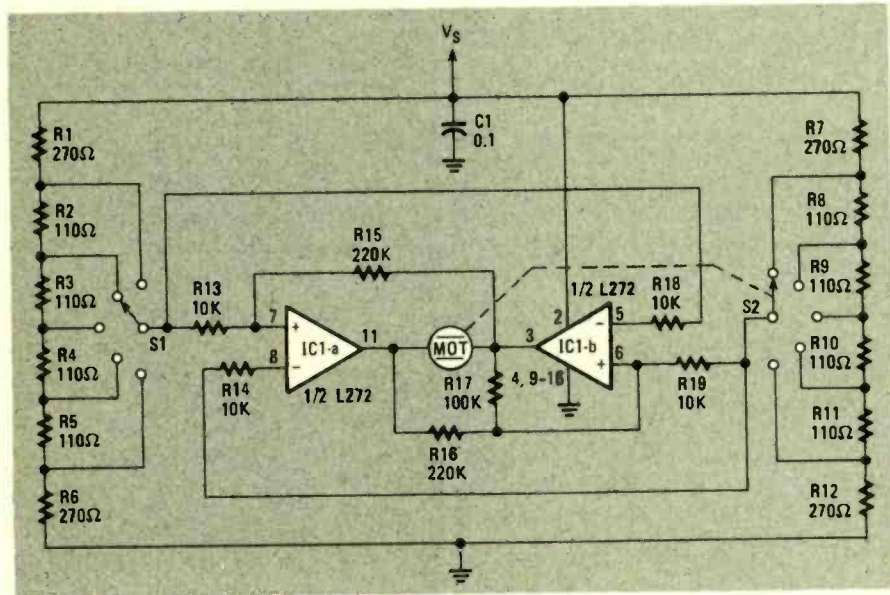
ment with two voltage-divider networks. The non-inverting input (pin 7) of IC 1-a is connected to one divider network through switch S1 (the position-selector switch). The non-inverting input of IC1-b at pin 6 is connected to a second resistor

string through switch S2 (which is driven by the positioning motor).

When identical voltages are applied to the two non-inverting inputs of the op-amps, the bridge is balanced and the motor is at rest. When the bridge balance is upset

L272					
PARAMETER	TEST CONDITIONS	MIN.	TYP.	MAX.	UNIT
V _S	SUPPLY VOLTAGE	4		28	V
I _Q	QUIESCENT DRAIN CURRENT		5.5	12	mA
I _b	INPUT BIAS CURRENT		0.5	25	μA
V _{OS}	INPUT OFFSET VOLTAGE		15		mV
I _{OS}	INPUT OFFSET CURRENT		50	250	nA
SR	SLEW-RATE	G _v = 1	1		V/μs
B	GAIN-BANDWIDTH PRODUCT		350		kHz
V _O	OUTPUT VOLTAGE SWING	f = 1 kHz I _b = 0.1A I _p = 0.5A	23	22.5	V P-P
R _i	INPUT RESISTANCE	500,000			Ω
G _v	VOLTAGE GAIN (OPEN LOOP)		70		dB
S _N	INPUT NOISE VOLTAGE	B = 10 TO 10,000 Hz	5		μV
I _N	INPUT NOISE CURRENT	B = 10 TO 10,000 Hz	200		pA
CMR	COMMON MODE REJECTION		70		dB
SVR	SUPPLY VOLTAGE REJECTION	f _{ripple} = 100 Hz SINGLE SUPPLY SPLIT SUPPLY	70	62	dB
T _{SD}	THERMAL SHUTDOWN JUNCTION TEMPERATURE		160		°C

*V_S = 24V, T_{AMB} = 25°C UNLESS OTHERWISE SPECIFIED



(by changing the position of S1), the motor turns in the direction that brings the bridge back into balance and moves the controlled device into the position selected by S1. For more information and/or data sheets write: **SGS-ATES Semiconductor Corp.**, 1000 East Bell Rd., Phoenix, AZ 85022.

Four-channel analog switches

Dual four-channel analog switches, the LM1037 and 1038, for source selection in stereo-audio equipment and for use in a wide range of industrial, automotive, multiplexing, and sampling applications have recently been announced by National Semiconductor Corp.

The LM1037 units have four con-

trol inputs to select any one of four possible stereo-input signals. All channels are muted internally when no input is selected. Electronic controls simplify the routing of audio signals, and allow DC selection with low noise and low distortion. The high-input and low-output impedances make the LM1037 advantageous when compared to CMOS types.

The LM1038 is similar to the LM1037, except that it is designed to be controlled by a micro-processor.

Available in 18-pin plastic DIP's, the LM1037 sells for \$2.00 in 100 piece lots, while the LM1038 sells for \$2.30.—**National Semiconductor Corp.**, 2900 Semiconductor Drive, Santa Clara, CA 95051. R-E

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JACK DARR
SERVICE EDITOR

Helpful flyback tests

YOU'VE OFTEN HEARD ME SAY, "I GET BY with a little help from my friends." Never was that statement more true than now! I've received a letter from a (very smart) reader, John P. Chalupski (MD), who has worked out a handy procedure for testing flyback transformers—the heart of the horizontal deflection circuit. (See Fig. 1.)

His letter said he wished he had a *flybacker*—a 16-kHz oscillator with a meter to read grid current—like the one described in October 1974's "Service Clinic." Not having a flybacker, he devised his own test procedure to use with the test equipment he had on hand (scope and function generator).

Flyback test procedure

What John did was to substitute an audio function-generator and scope for the flybacker. He hooked the function generator across the output tube plate and high-voltage rectifier—evidently he had a generator with either a built-in sweep, or one that could be swept by applying a low AC-voltage across the VCO. The scope was hooked across the generator output.

While sweeping through 10 kHz to about 100 kHz, he noted that the resonant points (as seen on the scope) showed that the bad flyback, or the one he suspected of being bad, had fairly sharp resonant peaks at around 71 kHz. The good flyback that he had tested prior to that showed a much broader peak at the same frequency. When he took out the damper tubes, both flybacks showed the same thing: You guessed it—a shorted damper tube!

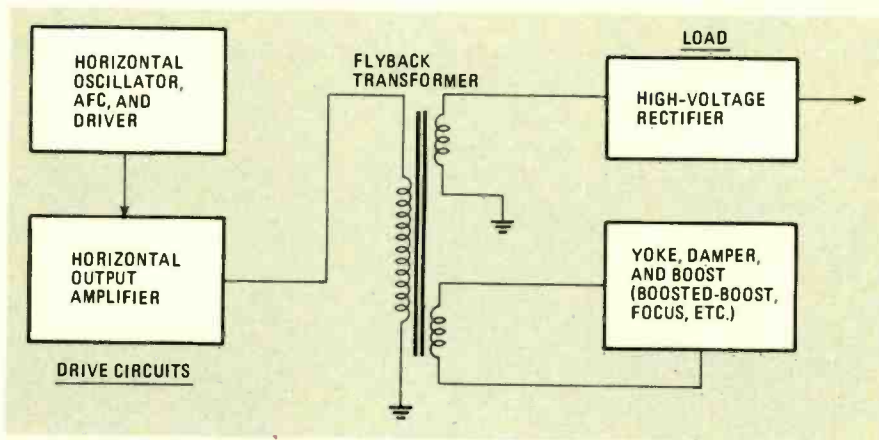


FIG. 1

It should also be possible to make a similar test without using a swept signal by simply sweeping manually with an AC voltage. To do so, turn the function generator's dial through the same range (10 to 100 kHz) with the scope connected at the same place (across the terminal). You'll see a bar pattern on the screen, but you will not need to synchronize the sweep of the scope with it. Simply note the amplitude of the signal and find the resonant points (where the pattern increases in height; sometimes it will become more square).

He mentioned that this test can be made with only a scope and an audio-signal source that's variable over the necessary range. Also, if you don't have a scope, any good AC voltmeter will show the peaks, and that's all you need. He also said that this couldn't be used to check for a shorted winding.

This is a good example of one of those faithful readers who are smarter than I am (I'd say that includes roughly, 93% of them)! So keep those cards and letters com-

ing folks! They are really appreciated.

Checking shorted windings

While John's procedure cannot be used to test for shorted windings in a flyback transformer, there is, however, a simple way to do so. (I found this one in the book that discussed the operation of the flybacker.) Simply hook your function generator up to the flyback and observe the scope trace, or reading (on the flybacker). Now, pick up that little coil of solder that you have on the bench and unwind about 3–4 inches. Now slip it around the core of the suspected bad flyback, then pull the ends together and pinch.

That makes a closed loop (one shorted turn) around the core. The reading on the flybacker should drop to zero, and the curve on the scope should vanish. If it does, that's a normal reaction with this test. It shows that you have no shorted windings. But if there is little or no change in your reading, then you've got a problem.

What's happening here is that the solder coil is placing an AC short across the transformer, which lowers the Q of the circuit and causes a bad reading. But if the transformer is already shorted, the solder-coil will have little or no effect on the circuit. That's a difficult problem to detect with ordinary test instruments such as ohmmeters and voltmeters because the DC continuity of the circuit will check out OK, but it won't work with the normal AC drive.

You can, however, measure the small resistance of the little windings, provided you have an extremely accurate digital VOM. I would recommend that you use needle-point test prods to ensure that you're able to get through any flux or whatever else might be on the terminal. Sharp tips allow you to get right down to the bare solder so you can get an accurate reading.

By using the test procedure worked out by John, and then doing the shorted-turns test (with a loop of solder) while observing changes in the scope pattern to see if it goes to a straight line, you can tell if the flyback or some other component is causing the problem. If when doing the shorted-turns test, the scope shows a very narrow range of movement of the tuning dial, the transformer is OK. The broad peak can be identified in the same way.

Since we're talking about flybacks anyway, this seems to be as good a time as any to tell you about a letter I received long ago from a man who had this complaint about a TV set he was working on.

The letter said that with the set's horizontal oscillator plugged in, the fuse would blow right away, but if oscillator was pulled out, the fuse wouldn't blow. From the symptom, I speculated that the cause of the problem was an AC short (and told him so).

Not long after that, I received another letter from that person saying that I was absolutely right. He had found that one winding of the flyback was shorted to the other. Again I wrote saying that, to me, it sounded as though the short were in the leads out of the winding! He wrote back again and

said, "Darned if you weren't right again!"

The key to locating the trouble was the almost normal current without any drive, and the overload of current with drive. The DC path was alright, but when an AC drive signal was put on it, the AC saw a dead short. So, remember that it's possible to have an AC short in circuits of that type without showing any indication using regular ohmmeter tests.

Finally, I'd like to thank all the good people who sent get-well cards. You can be sure that they were much appreciated. R-E

SERVICE QUESTIONS

THE EASY SOLUTION

On a Systems 3 Zenith, I found several components shorted, including the output transistor. I replaced them, plugged the set in, and bang! The output transistor blew, taking out a fast recovery diode. Any help will be appreciated.—O.R., Virginia Beach, VA

I hate to rain on your parade, but replacing the 9-160 module in its entirety will save you time, money, and also your sanity.

MOMENTARY SYNC-PROBLEM

This MGW Magnavox chassis B5-O4, will drop out of sync momentarily, causing a flash in the picture, and then go back in sync. That happens every 10 minutes. Any suggestions?—W. K., Columbus, OH

Of all the information you sent with your letter, the bit that deserves the most attention is the slowly rising voltage you get at R504 and C505. That's the point of AFC correction, and any changes in its potential will affect the horizontal frequency. As you describe it, I suspect something is causing a slow buildup and then a sudden discharge. Check all the components between the oscillator base back to, and including, the dual-diodes. Measure those resistors out of circuit! Don't ignore the R-C network returning the pulse from the flyback! R-E

cable TV

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NEW IDEAS

continued from page 77

stead of the three shown, to get a full scale reading. If the internal resistance of the meter is less than 90 ohms, you may only need two diodes.

The density range of the negative can be expressed as the logarithm (log) of the light intensity (I) through the clearest (shadow) area minus the log of I through the densest (highlight) area. In the form of an equation: density range = $\log(I_s/I_h)$.

TABLE 1

DENSITY RANGE (I_s)	(I_h)	Paper Grade
>1.4	<4	0
1.2-1.4	4-6	1
1.0-1.2	6-10	2
0.8-1.0	10-16	3
0.6-0.8	16-25	4
<0.6	>25	5

By using a simple table of anti-logs, you can avoid the need of a log amplifier to determine the correct paper grades corresponding to the specific density ranges.

To use the contrast meter, focus the negative in the enlarger with the lens diaphragm wide open. Then place the photocell under the lightest portion of the negative. Using potentiometer R5, adjust the meter for full-scale deflection. Now, without changing the setting, place the photocell beneath the darkest portion of the negative and read the meter. If the meter now shows less than ten percent of the full-scale reading, it may prove to be very difficult to read accurately.

When that happens, it will be necessary to push switch S1. Pressing S1 removes the short across resistor R4. Because R4 is three times the value of R3, only 1/4 the voltage applied to that leg of the circuit will appear at the inverting input of the op-amp, resulting in a reading four times as great. Now simply divide that reading by 4 and compute the ratio of the first and second measurements. And then refer to Table 1 to find the right paper grade for that negative.

—Phillip W. Albro

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SATELLITE TV

continued from page 20

in the 65 to 70% region are common; that means more gain from the antenna by a dB or two than their 1979/80 counterparts. Finally, the price per antenna has dropped dramatically with our equivalent 10 footer in 1984 selling for one quarter or so of its 1979/80 price. All of that has happened for all of the obvious reasons:

- 1) Volume has gone way up (as many as 500,000 new terminals this year, no less than 20% of which should be of the 10-foot size);
- 2) Those people who started out building antennas years ago have caught up with the learning curve and every part of the antenna system is now approaching state-of-the-art capabilities.

Satellite changes

There is one more factor, perhaps the most important factor of all, to consider. Virtually all of the satellites that were providing our primary TVRO services in 1979/80 have been retired, and replaced by newer satellites. That has had a

UHF Descramblers. Gated, sinewave, Zenith. Low prices! Free information. Catalog \$1.00. Dealers wanted! Visa/MasterCard. AIS SATELITE, Box 1226-S, Dublin, PA 18917, (215) 249-9411.

NOTCH filter for Cable-TV. Channels 2-6, 14-22, A-1. Send \$20.00 for sample and quantity price list. Specify channel. Money back guarantee. CATV, PO Box 17621, Plantation, FL 33318.

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WALKMAN style headphones \$7.00. Piezo super tweeter, 40,000 Hz \$8.00. JAMES FIGIELSKI, PO Box 42, Florham Park, NJ 07932. No checks.

SINEWAVE descrambler model MC-3. Non-working-new units, supplied with schematic, \$29.95 each 2 \$49.95. HUDSON CABLE COMPANY, Box 9179 Niskayuna, NY 12309. (518) 382-5349.

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CABLE-TV products. Jerrold, Hamlin, and Oak converters. Send \$3.00 for information. ADDITIONAL OUTLET CORP., 1041 W. Commercial Blvd., Ft. Lauderdale, Fla. 33309.

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dramatic effect on TVRO performance.

Newer satellites are more powerful (as much as 9 watts versus the older 5-watt maximum) and because they are newer, they are "run harder." As satellites grow older, their operators (RCA, Hughes, Western Union, etc.) become more conservative in the operations; 5-watt "capable" transponders are backed off so their actual operating power may be closer to 4 or even 3 watts. That is done without fanfare or announcement and the unaffiliated TVRO system owner simply sees weaker pictures and naturally blames his own terminal.

The higher-power satellites have led to the use of smaller and smaller dishes with success. Recent TVRO industry trade shows have seen a proliferation of dishes in the 4- to 6-foot region; some of

which deliver excellent pictures on as many as 30 to 40 channels (a function, as always, of where the user is located since satellite signals continue to be strongest in the center of the boresight; that's the central midwest in the U.S.).

Law changes

Finally, there is the law. TVRO users have been called "pirates" from the very beginning. That there might be close to 900,000 pirates as 1985 dawns does not change the label.

Something else will; *legislation*. Several influential Senators (i.e. Goldwater from Arizona) and Congressmen have introduced a pair of bills in both houses of Congress; bills that establish *Satellite Viewing Rights*. Those bills made excellent progress during 1984, an election year when such new bills seldom do anything but get a number assigned. When the bills are passed (and their eventual passage seems assured because of the excellent efforts of the trade association SPACE) home TVRO viewers (and equipment sellers) will find the "illegal" aspect of their operations a thing of the past. R-E


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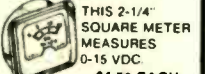


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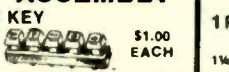
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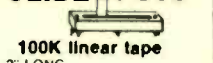
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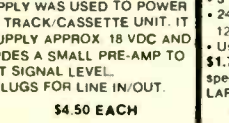
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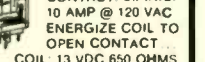
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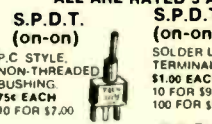


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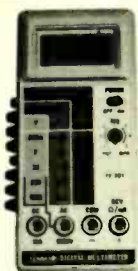
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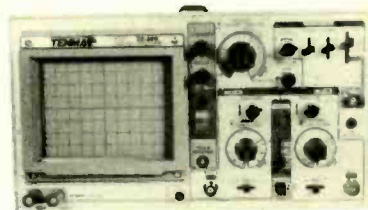
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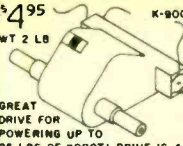
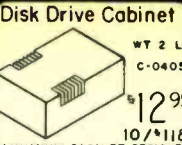
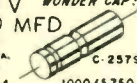
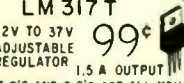

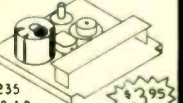

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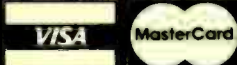
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74LS20	24	74LS155	88	74LS352	1.25
74LS21	26	74LS156	88	74LS353	1.25
74LS22	24	74LS157	64	74LS363	1.30
74LS26	28	74LS158	58	74LS364	1.90
74LS27	28	74LS160	88	74LS366	.48
74LS28	34	74LS161	64	74LS368	.48
74LS30	24	74LS162	88	74LS367	.44
74LS32	28	74LS163	84	74LS368	.44
74LS33	54	74LS164	88	74LS373	1.35
74LS37	34	74LS165	94	74LS374	1.35
74LS38	34	74LS166	1.90	74LS377	1.35
74LS40	24	74LS188	1.70	74LS378	1.13
74LS42	48	74LS189	1.70	74LS378	1.13
74LS47	74	74LS170	1.45	74LS385	1.85
74LS48	74	74LS173	88	74LS386	.44
74LS49	74	74LS174	54	74LS390	1.18
74LS51	24	74LS175	54	74LS393	1.18
74LS54	28	74LS181	2.18	74LS395	1.15
74LS55	28	74LS188	8.80	74LS399	1.45
74LS63	120	74LS190	88	74LS424	2.90
74LS73	38	74LS191	88	74LS447	.38
74LS74	34	74LS192	78	74LS490	1.90
74LS75	38	74LS193	78	74LS624	3.95
74LS76	38	74LS194	88	74LS640	2.15
74LS78	48	74LS195	88	74LS645	2.15
74LS83	58	74LS198	78	74LS668	1.85
74LS85	88	74LS197	78	74LS669	1.85
74LS86	88	74LS221	88	74LS670	1.45
74LS90	54	74LS240	94	74LS674	9.80
74LS91	88	74LS241	98	74LS682	3.18
74LS92	54	74LS242	98	74LS683	3.15
74LS93	54	74LS243	98	74LS684	3.15
74LS95	74	74LS244	125	74LS685	3.15
74LS98	88	74LS245	145	74LS688	2.35
74LS107	38	74LS247	74	74LS888	3.18
74LS109	38	74LS248	88	74LS783	23.85
74LS112	38	74LS249	88	81LS85	1.48
74LS113	38	74LS251	58	81LS86	1.45
74LS114	38	74LS253	58	81LS87	1.45
74LS122	44	74LS257	58	81LS88	1.45
74LS123	78	74LS258	58	25LS2521	2.75
74LS124	2.85	74LS259	2.70	25LS2568	4.20

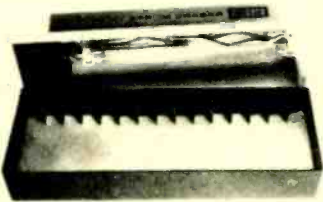
CRT CONTROLLERS

1771	14.95	2797	84.85
1791	23.95	6843	33.95
1793	25.95	6272	38.95
1795	28.95	UP0765	38.95
1797	48.95	MM8876	23.95
1799	79.95	MM8877	25.95
2793	79.95	1691	18.95
2795	84.95	2143	17.95

DISC CONTROLLERS

1771	14.95	2797	84.95
1791	23.95	6843	33.95
1793	25.95	6272	38.95
1795	48.95	UP0765	38.95
1797	48.95	MM8876	28.95
1799	79.95	MM8877	33.85
2793	79.95	1691	16.95
2795	84.95	2143	17.95

QUV-T8/1 EPROM Eraser



QUV-T8/1 Economy Model:

Low cost EPROM eraser in plastic enclosure. The UV element is in the lid and you place the EPROMs in the bottom half. No timer or switch option.

- Erases up to 8 EPROMs in 15 - 20 minutes.
- 12,000 uWatts at 1" distance.
- 90-Day Warranty

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6500

1 MHZ		2 MHZ	
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6504	6.90	6522A	10.95
6505	8.90	6532A	10.95
6507	8.90	6545A	28.95
6520	4.30	6551A	10.95
6522	6.90		
6532	8.90		
6545	21.50	6502B	9.90
6551	10.85		

6800

68000	58.95	6860	9.90
6800	3.90	6862	10.95
6802	7.90	6875	6.90
6808	12.90	6880	2.20
6809E	18.95	6883	21.95
6809	10.95	68047	23.95
6810	2.80	68488	18.95
6820	4.30		
6821	3.20		
6826	13.95	68800	9.95
6840	11.95	68802	21.25
6843	33.95	68809E	28.95
6844	24.95	68808	28.95
6845	13.95	68810	6.90
6847	10.95	68821	6.90
6850	3.20	68845	18.95
6852	15.70	68850	5.90

8000

8035	5.90	8088	88.95
8038	6.90	8155	6.90
IMS-8090	18.95	8155-2	7.90
IMS-8073	48.95	8156	8.90
8080	3.90	8185	28.95
8085	5.90	8185-2	38.95
8085A-2	10.95	8185-2	38.95
8086	28.95	8741	38.95
8087	198.00	8748	48.95
8088	38.95	8755	23.95

8200

8202	23.95	8255-5	5.20
8203	38.95	8257	7.90
8205	3.45	8257-5	8.90
8212	1.75	8259	6.85
8214	3.90	8259-5	7.45
8216	1.70	8271	75.00
8224	2.20	8272	38.95
8226	1.75	8275	28.95
8228	3.45	8279	8.90
8237	18.95	8279-5	9.00
8237-5	20.95	8282	8.45
8238	4.45	8283	6.45
8243	10.95	8284	14.95
8250	16.95	8285	6.45
8251	4.45	8287	6.45
8253	6.80	8288	24.00
8253-5	7.90	8289	48.95
8255	4.45	8292	18.95

Z-80

2.5 MHZ		4.0 MHZ	
Z80-CPU	3.90	Z80A-CPU	4.29
Z80-CTC	3.85	Z80A-CTC	4.90
Z80-DART	18.95	Z80A-DART	9.95
Z80-OMA	13.85	Z80A-OMA	12.85
Z80-PIO	3.85	Z80A-PIO	4.29
Z80-810/0	11.95	Z80A-810/0	11.95
Z80-810/1	11.95	Z80A-810/1	12.95
Z80-810/2	11.85	Z80A-810/2	12.85
Z80-810/9	11.85	Z80A-810/9	12.85

8.0 MHZ

Z808-CPU	9.85	ZILOG	
Z808-CTC	12.85	Z8132	33.95
Z808-PIO	12.95	Z8671	38.95
Z808-DART	12.95		

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4 POSITION	.84
5 POSITION	.89
6 POSITION	.89
7 POSITION	.94
8 POSITION	.94

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88728	1.84	DM8131	2.90
8795	.88	OP8304	2.24
8798	.88	OS8835	1.94
8797	.88	OS8836	.88

CRYSTALS

1.0000 MHz	3.89	8.0000 MHz	2.89
1.8432 MHz	3.88	10.0000 MHz	2.89
2.0000 MHz	2.88	10.7388 MHz	2.89
2.0972 MHz	2.89	12.0000 MHz	2.89
2.4576 MHz	2.89	14.3182 MHz	2.89
3.2768 MHz	2.89	15.0000 MHz	2.89

IC SOCKETS (1 to 99)

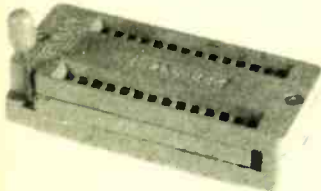
8 pin ST.....	.12	8 pin WW.....	.50
14 pin ST.....	.14	14 pin WW.....	.50
16 pin ST.....	.16	16 pin WW.....	.50
18 pin ST.....	.18	18 pin WW.....	.50
20 pin ST.....	.20	20 pin WW.....	1.04
22 pin ST.....	.22	22 pin WW.....	1.34
24 pin ST.....	.24	24 pin WW.....	1.44
28 pin ST.....	.30	28 pin WW.....	1.84
40 pin ST.....	.40	40 pin WW.....	1.94

ST = Soldertail WW = Wirewrap

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16 pin ZIF.....	5.90
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ZIF = TEXTTOOL (Zero Insertion Force)



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SOFT SECTOR with HUB RING

BULK 5 1/4" DISKETTES (NO LABEL)

SS/DD ... 10 for	14.90
100 up.....	139.00

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9 for \$45.00**

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- Serial Port
- Clock Calendar
- Software Included
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MEMORY CARD



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- Fully compatible w/IBM diagnostic utilities
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Cooling Fan	...	38.95
Power Supply	...	74.95
Joystick	...	29.95
RF Modulator	...	13.95
Disk Drive	...	199.00
Controller Card	...	59.95
Paddles	...	7.95

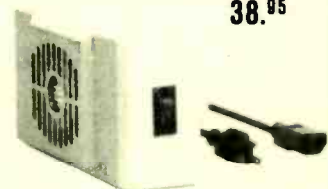
APPLE COMPATIBLE JOYSTICK

29.⁹⁵



COOLING FAN

38.⁹⁵



APPLE COMPATIBLE POWER SUPPLY

74.⁹⁵



- Powers Apple type systems
- +5V @ 5A +12V @ 3A
- -5V @ .5A -12V @ .5A
- Includes instructions

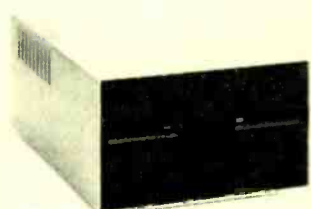
16K RAM Card - Apple II+

- 2-Year Warranty



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APPLE COMPATIBLE DISK DRIVE



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- Shugart mechanism, made in U.S.A.
- Directly replaces Apple Disk II
- Fully compatible with Apple Controller or other Apple compatible controllers.
- One Year Warranty

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VIEWMAX-80 149.⁹⁵

- 80 Col. card for Apple II+
- Video Soft Switch
- Inverse Video
- 2 Year Warranty



VIEWMAX-80e 129.⁹⁵

- 80 Col. card for Apple IIE
- 64K RAM Expandable to 128K

64K RAM Upgrade 40.00



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-5V @ .2A Highly Filtered

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AMD2901	8.95 8238 3.95		
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6800	2.50 8251 8.00		
6803L	12.95 8253 8.00	A76-1013A 3.75	
6809	8.95 8255-A 8.00	A73-1015D 3.75	
6810	4.00 8257 8.00	1488 .90	
6821	4.50 8259 8.00	1489 .90	
6845	13.95 8275 24.50	TR1802B 2.95	
6850	3.50 8279-S 5.95	BR1944L 8.95	
6875	4.50 8288 17.00	3341A 3.95	
8035	8.95 8355 12.95	A75-3600PRO 9.95	
8085A	10.00 TMS9927N L 8.95	CR75037 18.95	
8088	72.50 68000L B 39.50	MM5037 7.95	
8155	8.00 280A CPU 4.75	MM5569 2.50	
8202	19.95 280B CPU 9.00	8130 2.50	
8205	6.50 280C CTC 4.80	8830 2.50	
8212	3.00 280A DART 9.00	8833 2.50	
8214	4.50 280A P10 4.50	8834 2.00	
8216	3.00 280A S10 10.95	8837 2.00	
8226	3.50		

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MM1402	1.75	1771	16.50 1795
MM1403	1.75	1791	25.00 1797
MM1404	1.75	1793	35.00 D765C
MM5013	2.50		
MM5055	2.50		
MM5056	2.50		
MM5057	2.50		
MM5058	2.50		
MM5060	2.50		

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2121-3	2.50		
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745474	3.95	AK40273	1.75
2708	3.75	TMS4050NL	2.95
2712B	22.50	NK4096-11	1.25
2716 + 5V	3.75	4108-3	1.50
2725	6.25	4116-15	1.25
TMS232	6.95	4118-4	1.00
2764	2.50	4164-18	6.00
3628A-3	3.00	NK4802	5.95
6331	1.95	51104-4	6.75
7645-3	3.95	6116-3	6.75
8256-6	1.25	8118-12	4.95
AM9214C	2.96		3.00 ea.

CRYSTALS	
1.843	8.000
2.000	6.144
3.000	8.000
3.679	10.000
4.000	18.000
5.000	18.432
	20.000
	3.00 ea.

LINEAR CIRCUITS	
DA0080C	3.75 LM380 1.20 LM1310 1.40
TLO62CP	.96 LM384 1.60 LM1391 1.00
TLO64N	1.50 LM386 1.00 1456 80
TLO72	1.25 LM387 1.28 1488 .90
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LM307	.45 LM556 90 CA3018 1.95
LM308	.66 568 1.75 CA3078AT 1.50
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LM311	.75 566 125 CA309E 1.75
LM318	1.25 567 .85 CA3094 1.30
LM319	1.30 NE592 95 CA3130 1.00
LM324	.75 709C 80 CA3140 1.00
LM339	.90 LM710 50 CA3822 7.5
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LF351	.80 733 .95 4136 85
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LF355	.90 741CV 40 8700CJ 5.95
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1/16" thick with 1/10" spacing	
4 1/2" x 6 1/2" \$1.95	

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100	.35 .40 1.40	100	.35 .80 1.40
200	.40 .50 1.80	200	.50 .80 1.90
400	.80 .70 2.40	400	.70 1.00 2.60
600	.80 1.00 3.60	600	1.00 1.20 3.60

C/MOS			
74C00	50 74C921 3.50 4026 1.25 4071 30		
74C02	40 4001 30 4027 45 4072 30		
74C04	40 4007 30 4028 70 4076 80		
74C10	40 4006 .85 4029 75 4077 50		
74C14	60 4017 30 4030 40 4061 30		
74C20	40 4008 90 4034 1.75 4082 30		
74C32	40 4009 40 4038 85 4093 70		
74C42	120 4010 45 4048 1.75 4098 70		
74C76	75 4011 30 4041 75 4501 95		
74C83	120 4012 30 4042 85 4503 65		
74C86	40 4013 35 4083 85 4506 75		
74C154	3.00 4014 .75 4044 80 4510 120		
74C157	1.70 4015 40 4046 30 4511 85		
74C161	1.10 4016 40 4047 95 4514 120		
74C174	1.10 4017 .75 4049 35 4515 160		
74C175	1.10 4018 .75 4050 35 4516 150		
74C192	1.10 4019 40 4051 80 4518 85		
74C193	1.10 4020 75 4052 1.00 4520 80		
74C901	40 4021 75 4053 80 4528 110		
74C903	80 4022 75 4060 70 4529 140		
74C907	90 4023 35 4066 40 4538 150		
74C915	1.10 4024 .66 4068 40 4539 150		
		4069 35 4583 90	
		4070 40 4586 75	

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74S03	.35 74S89 2.00 74S175 .90		
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74S10	.35 74S133 45 74S189 1.60		
74S11	.35 74S135 85 74S194 1.30		
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74S16	.35 74S139 80 74S240 2.00		
74S20	.35 74S151 90 74S257 .90		
74S30	.35 74S157 90 74S260 75		
74S32	40 74S158 90 74S373 2.00		
74S42	85 74S161 1.75 74S374 2.00		
74S51	.35		

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200	.80 1.30 2.20
400	1.00 1.65 3.30
600	1.30 1.90 4.40

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400	.09 26 .85 1.50 10.00 12.00
600	.11 30 .80 2.00 13.00 15.00
800	.13 36 1.00 2.50 16.00 18.00
1000	.20 46 1.25 3.00 20.00 26.00

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LM317T	5 1.35 340T-5, 6, 8, 12, 15
320T or 24	1.5 15, 18 or 24V \$ 75
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7403	.20 7480 45 74166 100
7404	.30 7483 50 74170 150
7405	.30 7485 60 74173 75
7406	.30 7486 35 74174 90
7407	.60 7489 1.90 74175 90
7408	.75 7491 50 74176 75
7409	.25 7492 50 74180 190
7410	.20 7493 50 74181 200
7411	.25 7494 60 74182 80
7412	.25 7495 55 74190 80
7413	.35 7496 60 74191 80
7414	.50 74107 80 74192 80
7415	.20 74116 120 74193 80
7416	.30 74121 30 74194 60
7426	.30 74122 45 74195 80
7427	.30 74123 50 74196 75
7430	.20 74125 45 74199 125
7432	.30 74126 45 74221 125
7437	.60 74145 60 74273 100
7438	.30 74148 120 74279 70
7440	.20 74150 135 74365 65
7442	.50 74151 55 74367 66
7445	.60 74152 60 74390 90
7446	.50 74154 150 74395 60
7447	.70 74155 75 74592 100
7448	.70 74157 55 9601 100
7450	.20 74160 85 8726 110
7472	.35 74161 70 8728 110
7473	.35 74162 70 8738 110

74LS SERIES	
74LS00	.30 74LS109 40 74LS241 95
74LS01	.30 74LS112 40 74LS242 100
74LS02	.30 74LS113 40 74LS243 100
74LS03	.30 74LS114 40 74LS244 125
74LS04	.35 74LS123 75 74LS245 140
74LS05	.35 74LS125 60 74LS246 140
74LS06	.35 74LS126 60 74LS247 150
74LS10	.35 74LS132 60 74LS248 100
74LS11	.35 74LS136 40 74LS251 60
74LS11	.35 74LS137 90 74LS253 60
74LS12	.35 74LS138 60 74LS257 60
74LS13	.45 74LS139 60 74LS258 60
74LS14	.50 74LS147 2.20 74LS259 1.75
74LS15	.35 74LS151 55 74LS260 60
74LS20	.30 74LS153 55 74LS266 55
74LS21	.30 74LS155 70 74LS273 150
74LS22	.30 74LS156 60 74LS274 150
74LS26	.30 74LS157 65 74LS280 170
74LS27	.30 74LS158 60 74LS283 70
74LS28	.35 74LS160 70 74LS290 90
74LS30	.30 74LS161 65 74LS293 90
74LS32	.35 74LS166 60 74LS298 90
74LS37	.35 74LS163 65 74LS320 200
74LS38	.35 74LS164 70 74LS323 350
74LS40	.30 74LS168 70 74LS365 60
74LS42	.50 74LS166 1.75 74LS386 60
74LS47	.75 74LS170 130 74LS267 60
74LS51	.30 74LS173 70 74LS368 60
74LS54	.30 74LS174 55 74LS373 130
74LS73	.40 74LS175 55 74LS374 130
74LS74	.40 74LS181 2.00 74LS377 130
74LS75	.40 74LS190 50 74LS386 45
74LS76	.40 74LS191 90 74LS390 110
74LS83	.60 74LS192 80 74LS393 110
74LS85	.70 74LS193 80 74LS446 200
74LS86	.40 74LS194 65 74LS398 250
74LS92	.35 74LS195 70 74LS541 2.25
74LS92	.55 74LS196 75 74LS625 1.75
74LS95	.75 74LS197 75 74LS668 160
74LS96	.85 74LS221 90 74LS670 125
74LS107	.40 74LS240 95 81LS98 140

MULTI-TURN TRIM POTS	
50 OHM	5K
100 OHM	3/2.00 10K
1000 OHM	20K

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RAMSEY

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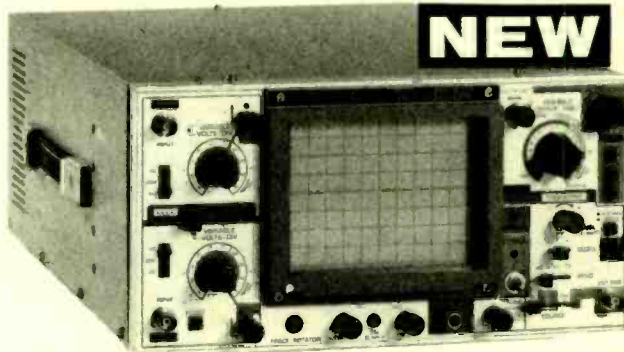
20 MHz DUAL TRACE OSCILLOSCOPE

Unsurpassed quality at an unbeatable price, the Ramsey oscilloscope compares to others costing hundreds more. Features include a component testing circuit for resistor, capacitor, digital circuit and diode testing. • TV video sync filter • wide bandwidth & high sensitivity • Internal graticule • front panel trace rotator • Z axis • high sensitivity X-Y mode • regulated power supply • built-in calibrator • rock solid triggering

*USA—Add \$10.00 per unit for postage, overseas orders add 15% of total order for insured surface mail.

\$399⁹⁵*

high quality hook on probes included



45 MHz DUAL SWEEP OSCILLOSCOPE

The Ramsey 625 is a dual time base, delayed sweep unit that includes a built-in signal delay line to permit clear viewing during very short rise times of high frequency waveforms. Other features include, variable trigger holdoff • 20 calibrated sweep time ranges from 0.5 μ s/div to 0.2 μ s/div. • fully adjustable sweep time • X5 sweep magnification • five trigger sources: CH1, CH2, LINE EXTERNAL and INTERNAL (V mode) • front panel x-y operation, Z axis input • sum difference of CH1, and CH2 waveforms displayed as single trace • sweep gate and sweep output • auto focus • single sweep

*Same as unit to left.

\$799⁹⁵*

high quality hook on probes included



RAMSEY D-1100 VOM MULTIMETER

Compact and reliable, designed to service a wide variety of equipment. Features include • mirror back scale • double-jeweled precision moving coil • double overload protection • an ideal low cost unit for the beginner or as a spare back-up unit.

\$19⁹⁵ test leads and battery included



NEW RAMSEY 1200 VOM MULTIMETER

Check transistors, diodes and LEDs with this professional quality meter. Other features include; decibel scale • 20K volt metering system • 3 1/2" mirrored scale • polarity switch • 20 measuring ranges • safety probes • high impact plastic case

\$24⁹⁵ test leads and battery included



RAMSEY D-3100 DIGITAL MULTIMETER

Reliable, accurate digital measurements at an amazingly low cost • In-line color coded push buttons, speeds range selection • abs plastic tilt stand • recessed input jacks • overload protection on all ranges • 3 1/2 digit LCD display with auto zero, auto polarity & low BAT. Indicator

\$49⁹⁵ test leads and battery included



CT-70 7 DIGIT 525 MHz COUNTER

Lab quality at a breakthrough price. Features • 3 frequency ranges each with pre amp • dual selectable gate times • gate activity indicator • 50mV @ 150 MHz typical sensitivity • wide frequency range • 1 ppm accuracy

\$119⁹⁵ wired includes AC adapter

CT-70 kit \$99.95
BP-4 nicad pack 8.95



CT-90 9 DIGIT 600 MHz COUNTER

The most versatile for less than \$300. Features 3 selectable gate times • 9 digits • gate indicator • display hold • 25mV @ 150 MHz typical sensitivity • 10 MHz timebase for WWV calibration • 1 ppm accuracy

\$149⁹⁵ wired includes AC adapter

CT-90 kit \$129.95
OV-1 0.1 PPM oven timebase 59.95
BP-4 nicad pack 8.95



CT-125 9 DIGIT 1.2 GHz COUNTER

A 9 digit counter that will outperform units costing hundreds more. • gate indicator • 24mV @ 150 MHz typical sensitivity • 9 digit display • 1 ppm accuracy • display hold • dual inputs with preamps

\$169⁹⁵ wired includes AC adapter

BP-4 nicad pack 8.95



CT-50 8 DIGIT 600 MHz COUNTER

A versatile lab bench counter with optional receive frequency adapter, which turns the CT-50 into a digital readout for most any receiver • 25 mV @ 150 MHz typical sensitivity • 8 digit display • 1 ppm accuracy

\$169⁹⁵ wired

CT-50 kit \$139.95
RA-1 receiver adapter kit 14.95



DM-700 DIGITAL MULTIMETER

Professional quality at a hobbyist price. Features include 26 different ranges and 5 functions • 3 1/2 digit, 1/2 inch LED display • automatic decimal placement • automatic polarity

\$119⁹⁵ wired includes AC adapter

DM-700 kit \$99.95
MP-1 probe set 4.95



PS-2 AUDIO MULTIPLIER

The PS-2 is handy for high resolution audio resolution measurements, multiplies UP in frequency • great for PL tone measurements • multiplies by 10 or 100 • 0.01 Hz resolution & built-in signal preamp/conditioner

\$49⁹⁵ wired

PS-2 kit \$39.95



PR-2 COUNTER PREAMP

The PR-2 is ideal for measuring weak signals from 10 to 1,000 MHz • flat 25 db gain • BNC connectors • great for shifting RF • ideal receiver/TV preamp

\$44⁹⁵ wired includes AC adapter

PR-2 kit \$34.95



PS-1B 600 MHz PRESCALER

Extends the range of your present counter to 600 MHz • 2 stage preamp • divide by 10 circuitry • sensitivity: 25mV @ 150 MHz • BNC connectors • drives any counter

\$59⁹⁵ wired includes AC adapter

PS-1B kit \$49.95

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Telescopic whip antenna—BNC plug \$ 8.95
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Direct probe, general purpose use 13.95
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The JE232CM allows connection of standard serial RS232 printers, modems, etc. to your VIC-20 and C-64. A 4-pole switch allows the inversion of the 4 control lines. Complete installation and operation instructions included.

- Plugs into User Port
- Provides Standard RS232 signal levels
- Uses 6 signals (Transmit, Receive, Clear to Send, Request to Send, Data Terminal Ready, Data Set Ready)

JE232CM \$39.95

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- Recreates a clear, natural male voice
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- Case size: 7 1/4" L x 3 1/2" W x 1-3/8" H

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- Security Warning
- Teaching
- Instrumentation
- Telecommunication
- Handicap Aid
- Games

Part No.	Description	Price
JE520CM	For Commodore 64 & VIC-20	\$114.95
JE520AP	For Apple II, II+, and IIe	\$149.95

Computer Memory Expansion Kits

IBM PC AND PC XT
Most of the popular Memory Boards (e.g. Quadram™ Expansion Boards) allow you to add an additional 64K, 128K, 192K or 256K. The IBM64K Kit will populate these boards in 64K byte increments. The Kit is simple to install - just insert the 9-64K RAM chips in the provided sockets and set the 2 groups of switches. Complete conversion documentation included.

IBM64K (Nine 200ns 64K RAMs) \$43.95

COMPAQ • COLUMBIA • EAGLE
These PC compatibles and others use the IBM64K for memory expansion.

IBM64K (Nine 200ns 64K RAMs) \$43.95

APPLE IIe
Extended 80 Column/64K RAM Card. Expands memory by 64K to give 128K when used with programs like VisiCalc™. Fully assembled and tested.

JE864 \$99.95

TRS-80 MODEL II, III
Each Kit comes complete with eight MM5290 (UPD416/4116) 16K Dynamic RAMs and documentation for conversion. Model II - 16K equipped with Expansion Interface can be expanded to 48K with 2 Kits. Model III - Can be expanded from 16K to 48K using 2 Kits. Each Kit will expand computer by 16K increments.

TRS-16K3 200ns (Model III) \$8.95
TRS-16K4 250ns (Model I) \$6.95

TRS-80 MODEL IV
Easy to install Kit comes complete with 8 ea. 4164N-20 (200ns) 64K Dynamic RAMs & conversion documentation.

TRS-64K-2 (Converts from 16K to 64K) \$38.95
TRS-64K-2PAL (8 ea. 4164 w/Special PAL Chip to expand from 64K to 128K) \$59.95

TRS-80 COLOR AND COLOR II
Easy to install Kit comes complete with 8 ea. 4164N-20 (200ns) 64K Dynamic RAMs and documentation for conversion. Converts TRS-80 Color Computers with D, E, F, and H circuit boards to 32K. Also converts TRS-80 Color Computer II to 64K. Fits DOS or OS-9 required to utilize full 64K RAM on all computers.

TRS-64K-2 \$38.95

INDUSTRIES Protect Yourself... DATASHIELD® Surge Protector

- Eliminates voltage spikes and EMI-RFI noise before it can damage your equipment or cause data loss
- 6 month warranty
- Power dissipation (100 microseconds), 1,000,000 watts
- 6 sockets
- 6 foot power cord
- Normal line voltage indicator light
- Brown out/back up reset switch

Model 100 \$69.95

Protect Yourself... DATASHIELD® Back-Up Power Source

Provides up to 30 minutes of continuous 120 VAC 60Hz power to your computer system (load dependent) when you have a black out or voltage sag

- Six month warranty
- Weight (PC200): 24 lbs - (XT300): 37.5 lbs

PC200 (Output rating: 200 watts) \$299.95
XT300 (Output rating: 300 watts) \$399.95

PROMETHEUS Intelligent 300/1200 Baud Telephone Modem with Real Time Clock/Calendar

The ProModem™ is a Bell 212A (300/1200 baud) intelligent stand-alone modem. Full featured expandable modem. Standard features include Auto Answer and Auto Dial, Help Commands, Programmable Intelligent Dialing, Touch Tone™ and Pulse Dialing & More. Hayes command set compatible plus an additional extended command set. Shown w/alphanumeric display option.

Part No.	Description	Price
PM1200	RS-232 Stand Alone Unit	\$349.95
PM1200A	Apple II, II+ and IIe Internal Unit	\$369.95
PM1200B	IBM PC and Compatible Internal Unit	\$269.95
PM1200BS	IBM PC & Comp. Int. Unit w/ProCom Software	\$319.95
MAC PAC	Macintosh Package (Includes PM1200, Cable, & ProCom Software)	\$399.95

OPTIONS FOR ProModem 1200

PM-COM	Description	Price
PM-COM	(ProCom Communication Software)	\$79.95
PM-OP	Please specify Operating System (Options Processor)	\$79.95
PMO-16K	(Options Processor Memory - 16K)	\$10.95
PMO-32K	(Options Processor Memory - 32K)	\$20.95
PMO-64K	(Options Processor Memory - 64K)	\$39.95
PM-ALP	(Alphanumeric Display)	\$79.95
PM-CC	(Apple IIc to PM1200 Cable)	\$29.95
PM-MC	(Macintosh to PM1200 Cable)	\$29.95

KEYBOARDS



Mitsumi 54-Key Unenclosed All-Purpose Keyboard

- SPST keyswitches
- 20 pin ribbon cable connection
- Low profile keys
- Features: cursor controls, control, Caps (lock), function, enter and shift keys
- Color (keycaps): grey - 1 lb. Pinout included

KB54 \$14.95



76-Key Serial ASCII Keyboard

- Simple serial interface
- SPST mechanical switching
- One touch (black/beige) self-enclosed case
- Five user function keys: F1-F5
- Six finger edge card connection
- Color (keys): tan
- Weight: 2 lbs.
- Data incl. KB76

KB76 \$29.95



Apple Keyboard and Case for Apple II and II+

- Keyboard: Direct connection with 16-pin ribbon connector
- 26 special functions
- Size: 14 1/4" x 5 1/2" x 1 1/4" H
- Case: Accommodates KB-A68
- Pop-up lid for easy access
- Size: 15 1/2" x 18" D x 4 1/4" H

Part No.	Description	Price
KB-EA1	Keyboard and Case (pictured above)	\$134.95
KB-A68	68-Key Apple Keyboard only	\$ 79.95
EAEC-1	Expanded Apple Enclosure Case only	\$ 59.95

POWER SUPPLIES

TRANSACTION TECHNOLOGY, INC. 5VDC @ 1 AMP Regulated Power Supply

- Output: +5VDC @ 1.0 amp (also +30VDC regulated)
- Input: 115VAC, 60 Hz
- Two tone (black/beige) self-enclosed case
- 6 foot, 3-conductor black power cord
- Size: 6 1/2" L x 7 1/2" W x 2 1/4" H
- Weight: 3 lbs

PS51194 \$14.95

Power/Mate Corp. REGULATED POWER SUPPLY

- Input: 105-125/210-250 VAC at 47-63 Hz
- Line regulation: ±0.05%
- Three mounting surfaces
- Overvoltage protection
- UL recognized
- CSA certified

Part No.	Output	Size	Weight	Price
EMAS/6B	5V@6A/6V@2.5A	4 1/4" L x 4" W x 2 1/4" H	2 lbs	\$29.95
EMAS/6C	5V@6A/6V@5A	5 1/4" L x 4 1/4" W x 2 1/4" H	4 lbs	\$39.95

POWER PAC INC. REGULATED POWER SUPPLY

- Perfect for computer systems
- Output: +5VDC @ 11 Amps
- 5VDC @ 1 Amp
- +12VDC @ 2 Amps
- 12VDC @ 0.5 Amp
- +24VDC @ 3 Amps
- Over-voltage protection
- Size: 12 1/2" L x 8 1/2" W x 4 1/4" H
- Weight: 17 lbs
- Spec incl.

PS2922 \$69.95

4-CHANNEL SWITCHING POWER SUPPLY

- Microprocessor, mini-computer, terminal, medical equipment and process control applications
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- Line regulation: ±0.2%
- Ripple: 30mV p-p
- Load regulation: ±1%
- Overcurrent protection
- Adj. 5V main output ±10%
- Size: 6 1/2" L x 1 1/2" W x 4-15/16" H
- Weight: 1 1/2 lbs

FCS-604A \$69.95

Switching Power Supply for APPLE II, II+ & IIe™

- Can drive four floppy disk drives and up to eight expansion cards
- Short circuit and overload protection
- Fits inside Apple computer
- Fully regulated +5V @ 5A, +12V @ 1.5A, -5V @ 0.5A, -12V @ 0.5A
- Direct plug-in power cord included
- Size: 9 1/8" L x 3 1/2" W x 2 1/4" H
- Weight: 2 lbs

KHP4007 (SPS-109) \$59.95

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The ADD-514 Disk Drive uses Shugart SA390 mechanics - 143K format disk storage - 35 tracks - Compatible with Apple Controller & ACC-1 Controller. The drive comes complete with connector and cable - just plug into your disk controller card. Size: 6 1/2" L x 3 1/2" W x 8-9/16" D. Weight: 4 1/2 lbs.

ADD-514 (Disk Drive) \$169.95
ACC-1 (Controller Card) \$ 49.95

More Apple Compatible Add-Ons...

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KB-A68 (Keyboard w/Keypad for II & II+) \$79.95
MON-12G (12" Green Monitor for II, II+, IIe, IIc) \$99.95
JE864 (80 Col. + 64K RAM for IIe) \$89.95
ADD-12 (5 1/4" Half-Height Disk Drive) \$179.95

DISK DRIVES



RFD480	(Remex 5 1/4" full-hl.)	\$129.95
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PKC-5	(5 1/4" Power Cable Kit)	\$2.95
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UV-EPROM Eraser



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1 Chip - 15 Minutes

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DE-4 UV-EPROM Eraser \$74.95
UVS-11EL Replacement Bulb \$16.95



JE664 EPROM PROGRAMMER
8K to 64K EPROMS - 24 & 28 Pin Packages

Completely Self-Contained - Requires No Additional Systems for Operation

- Programs and validates EPROMs
- Checks for properly erased EPROMs
- Emulates EPROMs on RAMs
- RS232C Computer Interface for editing and program loading
- Loads data into RAM by keyboard
- Changes data in RAM by keyboard
- Loads RAM from an EPROM
- Compares EPROMs for content differences
- Copies EPROMs
- Power input: 15VAC, 60Hz, less than 10W power consumption
- Enclosure: Color-coordinated light tan panels with molded and pieces in mocha brown
- Size: 15 1/4" L x 8 1/4" D x 3 1/4" H
- Weight: 5 1/2 lbs.

The JE664 EPROM Programmer erases and programs various 8-Bit Word EPROMs from 8K to 64K. Its memory capacity. Data can be entered into the JE664's internal 8K x 8-Bit RAM in three ways: 1) from an EPROM or EPROM (2) from an external EPROM via the optional JE665 RS232C BUS. (3) from its panel keyboard. The JE664's RAMs may be accessed by emulator outputs from the panel's test socket for an external microprocessor, for programming and emulation. The JE664 allows for examination, change and validation of program content. The JE664's RAMs can be programmed quickly by all 1's or any values, allowing unused addresses in the EPROM to be programmed later without necessity of "1W" erasing. The JE664 displays DATA and ADDRESS in convenient hexadecimal (alphanumeric) format. A "DISPLAY EPROM DATA" button changes the DATA readout from RAM words to EPROM words and is displayed in both hexadecimal and binary code. The front panel features a convenient operating guide. The JE664 Programmer includes one JM168 jumper Module (as listed below).

JE664-A EPROM Programmer \$995.00
Assembled & Tested (includes JM168 Module)

JE665 - RS232C INTERFACE OPTION - The RS232C Interface Option implements computer access to the JE664's RAM. This allows the computer to manipulate, store and transfer EPROM data to and from the JE664. A sample program listing is supplied. IBMASK for CP/M computers. Documentation is provided to allow the software to other computers with an RS232C port. 9600 Baud. 8 bit word, odd parity with 2 stop bits.

EPROM Programmer w/JE665 Option JE664-ARS \$1195.00
Assembled & Tested (includes JM168 Module)

EPROM JUMPER MODULES - The JE664's JUMPER MODULE (Personality Module) is a plug-in module that sets the JE664 for the proper programming pulses to the EPROM and completes the EPROM's socket connections for that particular EPROM.

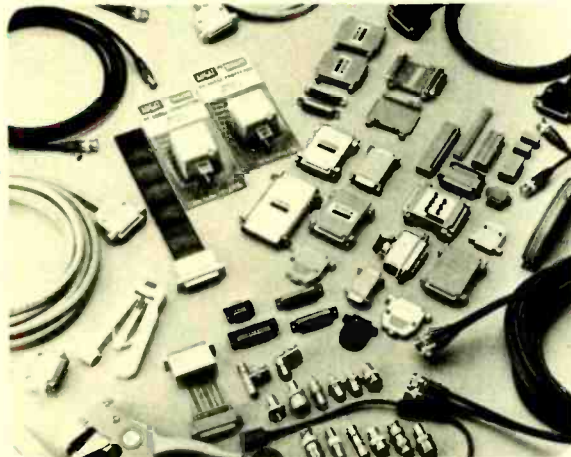
8-BIT EPROM	MANUFACTURER	PROGRAMMING VOLTAGE	PROGRAMMING RATE	PRICE
JM168A	2716	7V	AMD, Motorola, Intel, Intel, TI	\$14.95
JM168B	2716	12V	AMD, Motorola, Intel, Intel, TI	\$14.95
JM168C	76C02	5V	Intel	\$14.95
JM168D	76C02	5V	Intel	\$14.95
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DELUXE 46 CHANNEL CABLE TV CONVERTER



With Fine Tuning Dial

- Shifts all cable channels to UHF
- Extend pay TV to all your TV sets without extra monthly fee
- Allows taping pay TV (decoder required) while viewing another channel
- Restores TV remote control and VCR programming ability

\$24.95

BICYCLE COMPUTER

A Dashboard for your Bike

Handsome matte black console with keyboard input. Displays your speed, distance & calories burned on 2.8" LCD screen. Quartz clock/stopwatch built in. Complete with MAG pickup & all mounts.



\$49.95

Upgrade any bike to a deluxe exercise machine

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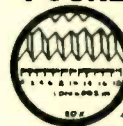


Lab accuracy at an everyday price
...reads 1 gram or 1 oz.

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10X has 265 in. field; 005 in. scale divisions
20X has 190 in. field; .002 in. scale divisions

4 x 40 Screw Tap Spooly 10X or 20X **\$14.95**



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ACTIVE RECEIVING ANTENNA

Gives excellent reception,
50 KHz to 30 MHz.

New MFJ-1024 Active Receiving Antenna mounts outdoors away from electrical noise for maximum signal. Gives excellent reception of 50 KHz to 30 MHz signals. Equivalent to wire hundreds of feet long. Use any SWL, MW, BCB, VLF or Ham receiver.

High dynamic range RF amplifier. 54 in. whip. 50 foot coax. 20 dB attenuator prevents receiver overload. Switch between two receivers. Select auxiliary or active antenna. Gain control. "ON" LED. Remote unit, 3x2x4 in. Control, 6x2x5 in. 12 VDC or 110 VAC with optional adapter, MFJ-1312, \$9.95.



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Build anything from computers to LED flashers... any project you want the fast, easy, fun way. Use HANDY solderless breadboards to build, test, modify and expand your ideas.

**SATISFACTION GUARANTEED
OR YOUR MONEY BACK!**

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- Full contact labeling — simplifies component layouts
- New durable clip design assures reliable, low resistance, corrosion-free interconnections
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- Self-adhesive backing — mounts anywhere
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- Expands horizontally and vertically

HB-0100. 1 Buss Strip.
100 tie points. Compares
at \$3.00!

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IC capacity. Compares at
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Posts. 3260 tie points.
36 14-pin IC capacity.
Compares at \$89.00!

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1 Buss Strip. 2 Binding
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18 14-pin IC capacity.

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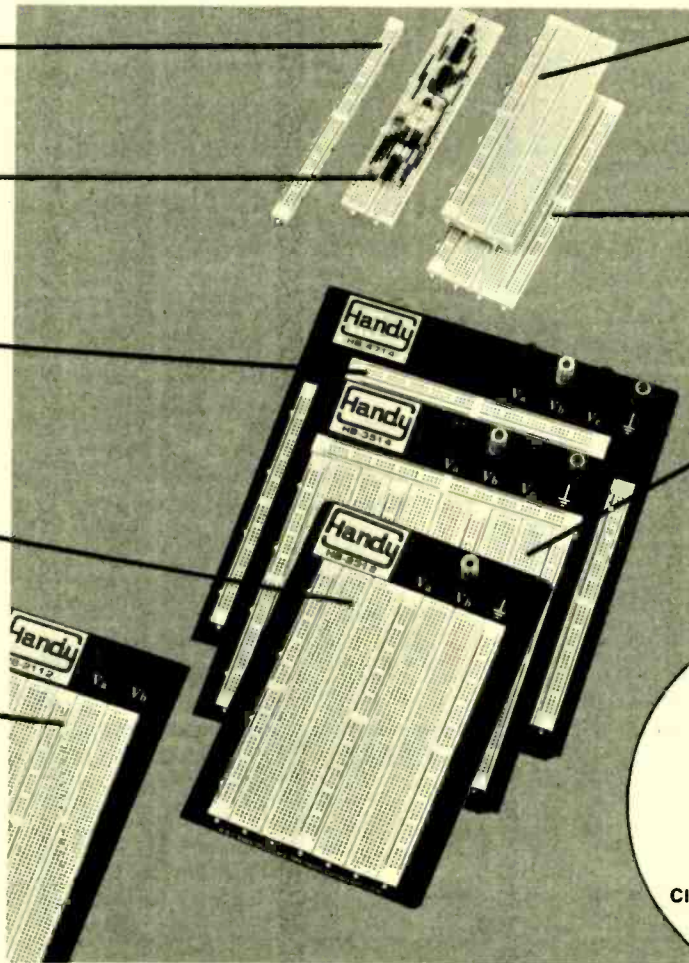
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CIRCLE 71 ON FREE INFORMATION CARD

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2112	256x4 (450ns)	2.99
2114	1024x4 (450ns)	8/9.95
2114-25	1024x4 (250ns)	8/10.95
2114L-4	1024x4 (450ns)(LP)	8/12.95
2114L-3	1024x4 (300ns)(LP)	8/13.45
2114L-2	1024x4 (200ns)(LP)	8/13.95
TMM2016-200	2048x8 (200ns)	4.15
TMM2016-150	2048x8 (150ns)	4.95
TMM2016-100	2048x8 (100ns)	6.15
HM6116-4	2048x8 (200ns)(cmos)	4.75
HM6116-3	2048x8 (150ns)(cmos)	4.95
HM6116LP-4	2048x8 (200ns)(cmos)(LP)	5.95
HM6116LP-3	2048x8 (150ns)(cmos)(LP)	6.95
HM6264P-15	8192x8 (150ns)(cmos)(LP)	34.95

LP = Low Power

DYNAMIC RAMS

4116-250	16384x1 (250ns)	8/7.95
4116-200	16384x1 (200ns)	8/12.95
4116-150	16384x1 (150ns)	8/14.95
4164-200	65536x1 (200ns)(5v)	9/44.95
4164-150	65536x1 (150ns)(5v)	9/49.00
TMS4164	65536x1 (150ns)(5v)	8.95

5v = Single 5 Volt Supply

EPROMS

2708	1024x8 (450ns)	3.95
2716	2048x8 (450ns)(5v)	3.95
2716-1	2048x8 (350ns)(5v)	5.95
TMS2532	4096x8 (450ns)(5v)	5.95
2732	4096x8 (450ns)(5v)	4.95
2732-250	4096x8 (250ns)(5v)	8.95
2732-200	4096x8 (200ns)(5v)	11.95
2732A	4096x8 (250ns)(5v)(21vPGM)	9.95
2732A-2	4096x8 (200ns)(5v)(21vPGM)	13.95
2764	8192x8 (450ns)(5v)	6.95
2764-250	8192x8 (250ns)(5v)	7.95
2764-200	8192x8 (200ns)(5v)	19.95
27128-30	16384x8 (300ns)(5v)	22.95

5v = Single 5 Volt Supply
21vPGM = Program at 21 Volts

SPECTRONICS CORPORATION

EPROM ERASERS

	Timer	Chip Capacity	Intensity (uW/Cm ²)	
PE-14		9	8,000	83.00
PE-14T	X	9	8,000	119.00
PE-24T	X	9	9,600	175.00

8000

8035	5.95
8039	5.95
8080	3.95
8085	4.95
8085A-2	11.95
8087	175.00
8088	29.95
8155	6.95
8155-2	7.95
8156	6.95
8748	24.95
8755	24.95

8200

8203	39.95
8205	3.50
8212	1.80
8216	1.75
8228	3.49
8237-5	21.95
8243	4.45
8250	10.95
8251	4.49
8253	6.95
8253-5	7.95
8255	4.49
8255-5	5.25
8259	6.90
8259-5	7.50
8272	39.95
8275	29.95
8279	8.95
8282	6.50
8284	5.50
8286	6.50
8288	25.00

Z80

2.5 Mhz

Z80-CPU	3.95
Z80-CTC	3.95
Z80-PIO	3.95
Z80-SIO/0	11.95

4.0 Mhz

Z80A-CPU	4.49
Z80A-CTC	4.95
Z80A-DART	9.95
Z80A-PIO	4.49
Z80A-SIO/0	12.95

6.0 Mhz

Z80B-CPU	9.95
----------	------

6500

6502	4.95
6520	4.35
6522	6.95
6532	9.95
6551A	11.85
6502A	6.95
6522A	9.95
6551A	11.95

6800

68000-8	49.95
6800	2.95
6802	7.95
6809E	14.95
6809	11.95
6821	2.95
6845	12.95
6850	3.25
6883	22.95

DISK CONTR

1771	15.95
1791	23.95
1793	23.95
UPD765	19.95

INTERFACE

8T26	1.59
8T28	1.98
DM8131	2.95
DP8304	2.29

CLOCK CHIPS

MM5314	4.95
MM5369	3.95
MM58167	12.95
MMS5832	3.95

DATA ACQ

ADC0804	3.49
ADC0809	4.49
ADC0817	9.95
DAC0808	2.95
MC1408LB	2.95

SOUND CHIPS

76477	3.95
76488	5.95
AY3-8910	12.95
SSI263	39.95

74LS00

74LS00	.24	74LS157	.65
74LS01	.25	74LS158	.59
74LS02	.25	74LS160	.69
74LS03	.25	74LS161	.65
74LS04	.24	74LS163	.65
74LS05	.25	74LS164	.69
74LS08	.28	74LS165	.95
74LS09	.29	74LS166	.95
74LS10	.25	74LS169	1.75
74LS11	.35	74LS173	.69
74LS12	.35	74LS174	.55
74LS13	.45	74LS191	.89
74LS14	.59	74LS192	.79
74LS20	.25	74LS193	.75
74LS21	.29	74LS194	.69
74LS26	.29	74LS195	.69
74LS27	.29	74LS197	.79
74LS32	.29	74LS221	.89
74LS33	.55	74LS240	.95
74LS37	.35	74LS241	.99
74LS38	.35	74LS242	.99
74LS40	.25	74LS243	.99
74LS42	.49	74LS244	1.29
74LS47	.75	74LS245	1.49
74LS51	.25	74LS251	.59
74LS73	.39	74LS253	.59
74LS74	.35	74LS257	.59
74LS75	.39	74LS258	.59
74LS76	.39	74LS259	2.75
74LS85	.69	74LS260	.59
74LS86	.39	74LS266	.55
74LS90	.55	74LS279	.49
74LS92	.55	74LS280	1.98
74LS93	.55	74LS283	.69
74LS107	.39	74LS290	.89
74LS109	.39	74LS293	.89
74LS112	.39	74LS299	1.75
74LS122	.45	74LS323	3.50
74LS123	.79	74LS365	.49
74LS124	2.90	74LS367	.45
74LS125	.49	74LS368	.45
74LS126	.49	74LS373	1.39
74LS132	.59	74LS374	1.39
74LS136	.39	74LS377	1.39
74LS138	.55	74LS390	1.19
74LS139	.55	74LS393	1.19
74LS145	1.20	74LS640	2.20
74LS148	1.35	74LS645	2.20
74LS151	.55	74LS670	1.49
74LS153	.55	74LS682	3.20
74LS154	1.90	74LS688	2.40
74LS155	.69	81LS95	1.49
74LS156	.69	25LS2521	2.80

7400

7400	.19	7492	.50
7401	.19	7493	.35
7402	.19	74100	1.75
7403	.19	74107	.30
7404	.19	74116	1.55
7405	.25	74121	.29
7406	.29	74122	.45
7407	.29	74123	.49
7408	.24	74125	.45
7409	.19	74126	.45
7410	.19	74132	.45
7411	.25	74145	.60
7413	.35	74148	1.20
7414	.49	74150	1.35
7416	.25	74151	.55
7417	.25	74153	.55
7420	.19	74154	1.25
7421	.35	74155	.75
7425	.29	74157	.65
7427	.29	74159	1.65
7430	.19	74161	.69
7432	.29	74163	.69
7437	.29	74164	.85
7438	.29	74165	.85
7442	.49	74166	1.00
7445	.69	74173	.75
7447	.96	74174	.89
7448	.69	74175	.89
7473	.34	74185	2.00
7474	.33	74192	.79
7475	.45	74193	.79
7476	.35	74194	.85
7483	.50	74259	2.25
7485	.59	74367	.65
7489	2.15	74368	.66
7490	.35	74393	1.35

74S00

74S00	.32
74S02	.35
74S04	.35
74S05	.35
74S08	.35
74S10	.35
74S11	.35
74S20	.36
74S32	.40
74S37	.88
74S74	.50
74S86	.50
74S112	.50
74S124	2.75
74S132	1.24
74S133	.45
74S138	.85
74S139	.85
74S140	.55
74S151	.95
74S153	.95
74S157	.95
74S158	.95
74S161	1.95
74S163	1.95
74S174	.95
74S175	.95
74S240	2.20
74S241	2.20
74S244	2.20
74S280	1.95
74S287	1.90
74S288	1.90
74S373	2.45
74S374	2.45
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- LOW POWER-8ma OPERATION, 10 MICROAMP STANDBY
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5.0	2.95
5.0688	2.95
6.0	2.95
6.144	2.95
8.0	2.95
10.0	2.95
10.738635	2.95
14.31818	2.95
15.0	2.95
16.0	2.95
17.430	2.95
18.432	2.95
20.0	2.95

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AY5-1013	3.95
AY3-1015	6.95
TR1602	3.95
2651	8.95
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4702	12.95
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MC3470	4.95
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TL084	2.19	NE564	2.95
LM301	.34	LM565	.99
LM307	.45	LM566	1.49
LM308	.69	NE592	2.75
LM309K	1.25	LM733	.98
LM310	1.75	LM741	.35
LM311	.64	LM747	.69
LM317T	1.19	LM1310	1.49
LM317K	3.95	MC1330	1.69
LM318	1.49	MC1372	6.95
LM323K	4.95	LM1458	.59
LM324	.59	LM1488	.69
LM331	3.95	LM1489	.69
LM334	1.19	LM1496	.85
LM335	1.40	LM1800	2.37
LM336	1.75	LM1812	8.25
LM337T	1.95	LM1889	1.95
LM338K	3.95	ULN2003	2.49
LM339	.99	XR2006	3.75
LM348	.99		

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.47uf	50v .14	10	50v .16
10	50v .15	22	16v .14
47	35v .18	47	50v .20
100	16v .18	100	15v .20
220	35v .20	150	25v .25

50v MONOLITHIC

.01uf	.14	.1	.05
.047	.15	.47	.25

50v DISC

10pf	.05	470	.05
22	.05	560	.05
25	.05	680	.05
27	.05	820	.05
33	.05	.001uf	.05
47	.05	.0015	.05
56	.05	.0022	.05
68	.05	.005	.05
82	.05	.01	.07
100	.05	.02	.07
220	.05	.05	.07
330	.05	.1	.12

SPECIALS ON BYPASS CAPS

.01uf disc	50v	100/6.00
.1uf disc	12v	100/8.00
.01uf mono	50v	100/12.00
.1uf mono	50v	100/15.00

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MAXIMIZER Memory Multifunction	259.95
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ZENITH ZVM-123 15 MHz Green Monitor	105.00
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BMC BM-AU9191U Comp. 13" Color Monitor	279.00
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VERBATIM DATALIFE DISKETTES DS/DD	34.95
DISKETTE FILE Holds 70 Diskettes	16.99

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***NASHUA DISKETTES**
5 1/4" SOFT SECTOR
DOUBLE SIDED, DOUBLE DENSITY
WITH HUB RINGS
BULKED PACKED IN FACTORY SEALED BAGS OF 50.
INCLUDES DISKETTE SLEEVES AND WRITE PROTECT TABS.
IDEAL FOR SCHOOLS, CLUBS, AND USERS GROUPS. THIS IS
A SPECIAL PURCHASE. 80 QUANTITIES ARE LIMITED. THIS IS
A 3 YEAR WARRANTY.

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\$1.49 ea. QTY 100
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*NASHUA DISKETTES WERE JUDGED TO HAVE THE HIGHEST
POLISH AND RECORDED AMPLITUDE OF ANY DISKETTES TESTED.
(SEE "COMPARING FLOPPY DISKS", BYTE 9/84)

DISKETTE FILE \$8.95

BY DEALING DIRECT WITH THE FACTORY WE CAN MAKE
THIS UNBEATABLE OFFER!
* ATTRACTIVE SMOCKED ACRYLIC CASE
WITH 6 INDEXED DIVIDERS
* RUGGED, HIGH QUALITY
CONSTRUCTION
* HOLDS 70 5 1/4" DISKETTES
WITH ROOM TO SPARE
**ORDER 50 NASHUA DISKETTES, AND GET THIS
DISKETTE FILE FOR ONLY \$8.95**

SPECIALS END 11/30/84

5 1/4" DISK DRIVES

TANDON TM100-2	DS/DD	199.00
SHUGART SA400L	SS/DD	199.95
MPI B52	DS/DD	139.95
TEAC FD55B 1/2 Ht.	DS/DD	159.00
TEAC FD55F 1/2 Ht.	DS/Quad	200.00

8" DISK DRIVES

SIEMENS FD200-8	DS/DD	195.00
SIEMENS FD100-8	SS/DD	149.95

SWITCHING POWER SUPPLIES

KEPCO/TDK	ASTEC
MODEL MRM174KF	MODEL AA11190
+5V @ 5A	+5V @ 4A
+12V @ 2A	+12V @ 2.5A
+12V @ 2.8A	-5V @ 25A
-12V @ .5A	-12V @ .30A
49.95	39.95

LIGHT EMITTING DIODES JUMBO DISPLAYS

RED	1-99	100-up	MAN-72 CA 3"	.99
GREEN	.10	.09	MAN-74 CC 3"	.99
YELLOW	.18	.15	FND-500 CC 5"	1.49
			FND-507 CA 5"	1.49

IC SOCKETS/DIP CONNECTORS

LEADS	LOW PROFILE SOLDERTAIL		3 LEVEL WIREWRAP		TEXTTOOL ZERO INSERTION		COMPONENT CARRIES		IDC PLUG RIBBON CABLE	
	1-99pcs.	100&up	1-99pcs.	100&up	ZIFxx	IC Cxx	IDPxx	IDPxx		
8	.13	.11	.59	.49	---	.65	---	---		
14	.15	.12	.69	.52	5.95	.75	1.45	---		
16	.17	.13	.69	.58	5.95	.85	1.65	---		
18	.20	.18	.99	.90	---	1.00	---	---		
20	.29	.27	1.09	.98	---	1.25	---	---		
22	.30	.27	1.39	1.28	---	1.25	---	---		
24	.30	.27	1.49	1.35	7.95	1.35	2.50	---		
28	.40	.32	1.69	1.49	8.95	1.50	---	---		
40	.49	.39	1.99	1.80	10.95	2.10	4.15	---		
64	4.25	---	---	---	---	---	---	---		

IDC CONNECTORS

DESCRIPTION	ORDER BY	CONTACTS				
		20	26	34	40	50
RIBBON HEADER SOCKET	IDRxx	1.86	2.43	3.15	3.73	4.65
RIBBON EDGE CARD	IDExx	2.36	2.65	3.25	3.80	4.74

ORDERING INSTRUCTIONS: Insert the number of contacts in the position marked "xx" of the "order by" part number listed. EXMAMPLE: A 20 pin ribbon edge card would be IDE 20.

D-SUBMINIATURE

DESCRIPTION	ORDER BY	CONTACTS			
		9	15	25	37
SOLDER CUPS MALE	DBxxP	2.08	2.69	2.50	4.80
SOLDER CUPS FEMALE	DBxxS	2.68	3.63	3.25	7.11
RT. ANGLE MALE	DBxxPR	1.65	2.20	3.00	4.83
PC SOLDER FEMALE	DBxxSR	2.18	3.03	4.42	6.19
IDC MALE	IDBxxP	3.37	4.70	6.23	9.22
RIBBON CABLE FEMALE	IDBxxS	3.69	5.13	6.84	10.08
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4016	.39	4047	.95	4093	.49	74C14	.59
4017	.69	4049	.35	4503	.65	74C74	.65
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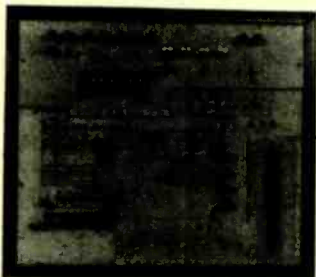


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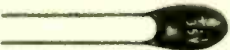
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330	271-1315	47k	271-1342
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