

GREAT GAMES YOU PLAY ON YOUR TV

75¢ ■ JUNE 1976

Radio-Electronics

THE MAGAZINE FOR NEW IDEAS IN ELECTRONICS

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- ★ Komputer Korner
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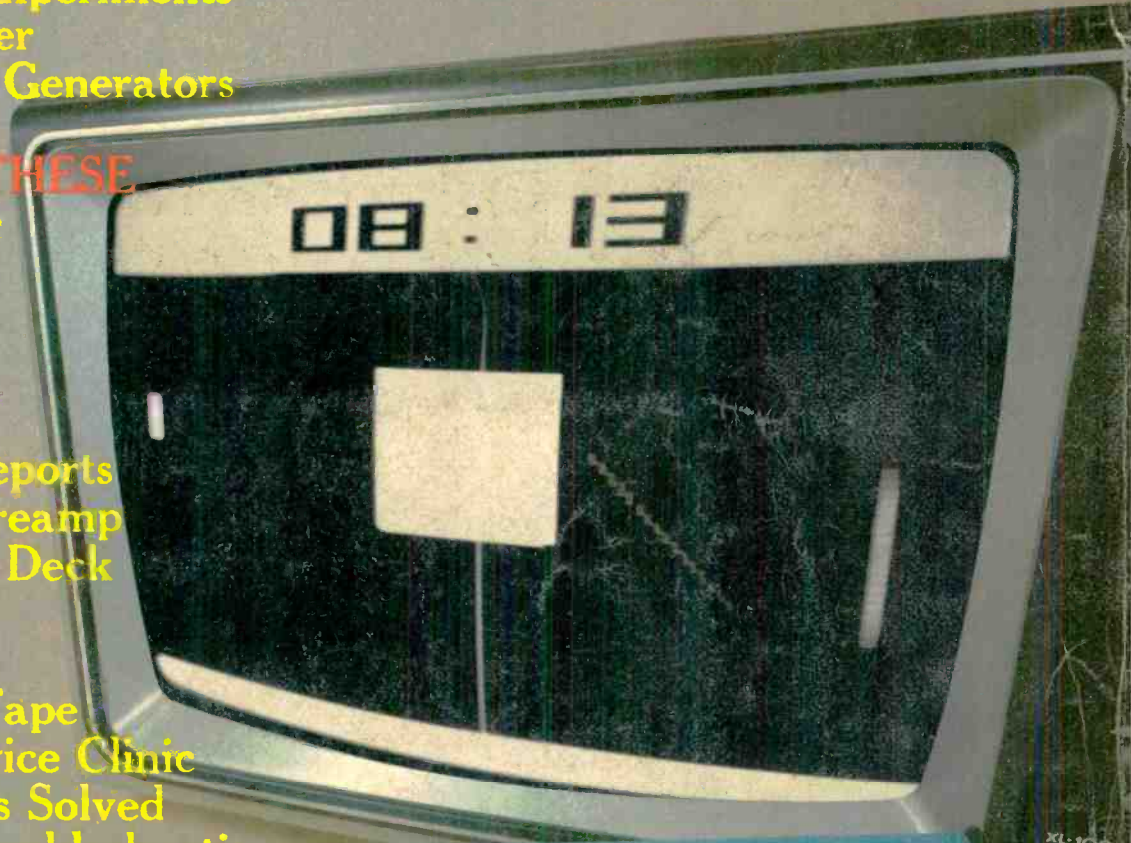
- ★ Pong & Bumper
- ★ 8080 Computer

HI-FI STEREO

- ★ Hi-Fi Test Gear
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TELEVISION

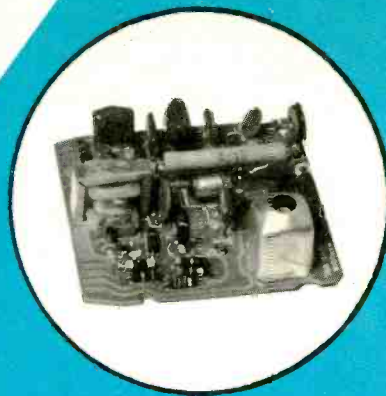
- ★ Video Discs & Tape
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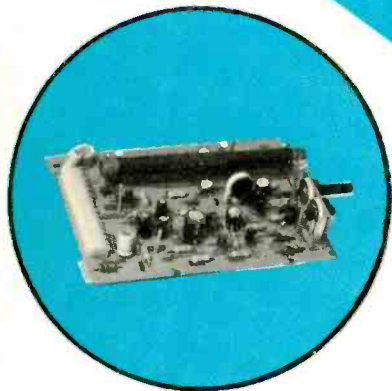
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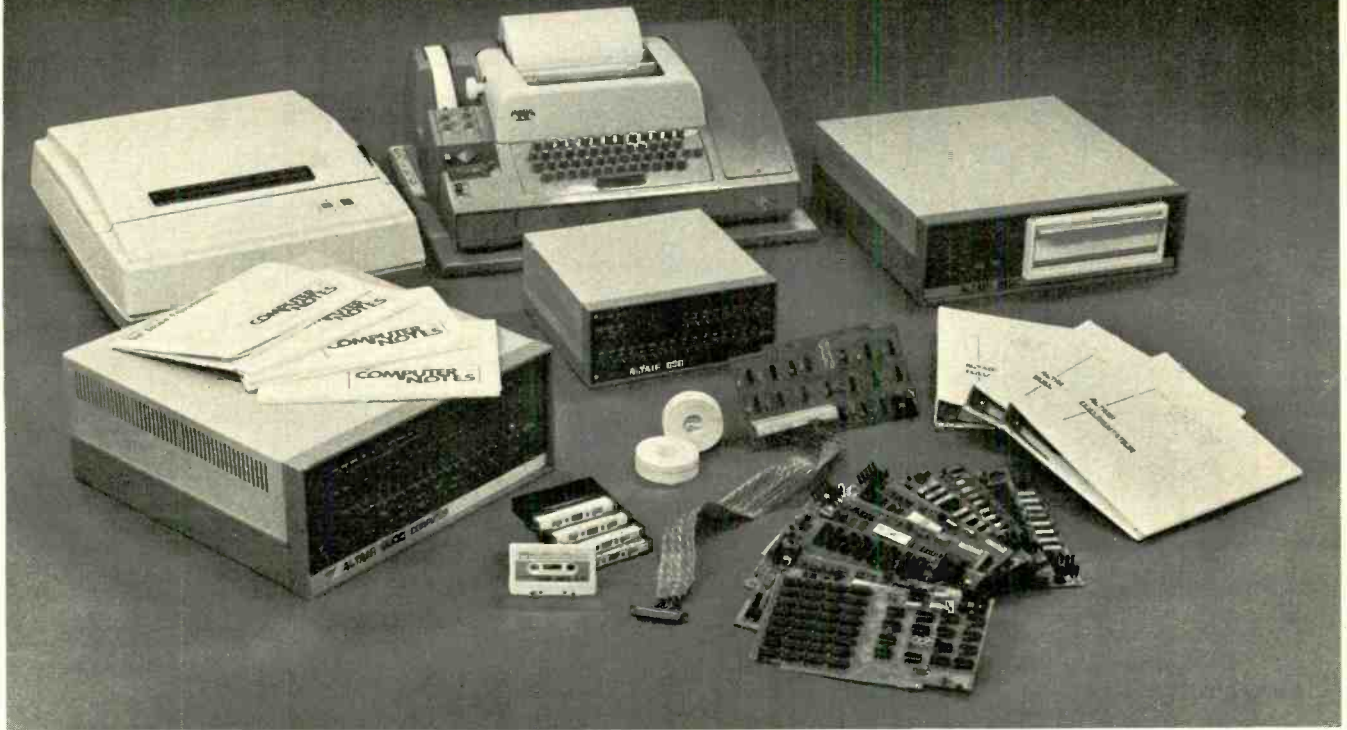
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Circle 2 on reader service card

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THE MAGAZINE FOR NEW IDEAS IN ELECTRONICS

Electronics publishers since 1908

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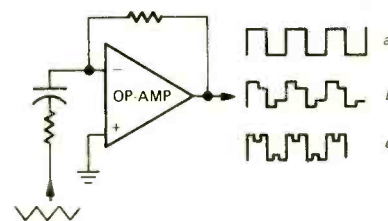
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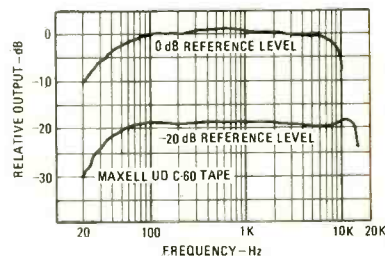
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ON THE COVER

If you've been wondering how TV games work and how you might build your own, this is the answer. We're starting this 3-part story on page 35 of this issue. We think you'll like it.



USING A FUNCTION GENERATOR to check a differentiator is a snap. Learn how in the story starting on page 56.



PERFORMANCE OF SANSUI SC-3000 with high-output ferric tape. Get all the performance specs starting on page 50.

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looking ahead

CB bombshell

Just as the entire CB equipment industry was looking to the FCC for relief from overcrowding of the current 27-MHz band through addition of more channels—which had been an almost foregone conclusion—the Commission put the kibosh on the whole idea and decided to take a new look at interference problems caused by increasing CB use. Expansion of the current band from 23 to 40 or 50 channels thus is clearly out the window at least for the time being, and the odds may even favor the eventual movement of the band out of harm's way, far upstairs to 900 MHz.

The Commission has been increasingly disturbed by geometrically mounting complaints of interference by CB equipment with television and radio receivers, including CB receivers themselves. Under the FCC's original plan to expand from 23 to 50 channels, one of the immediate problems posed was that the difference between any two channels came out to a magic number—455 kHz, which, of course, is the second IF frequency used in all AM radios, including CB. This, combined with other interference problems, added up to such a headache that the Commission decided to take another look at the whole thing.

Now this doesn't mean the end of communicating on the existing band. The Commission presumably will allow plenty of time for current equipment to wear out before moving everything upstairs—or whatever it does. But it does mean CB'ers will have to live within the current 23 channels for some time.

The FCC also approved a new CB licensing program which could eliminate those endless waits for that vital document that is necessary before you can legally push the talk button. Under the new plan, the CB dealer would give purchasers an application form incorporating a tempo-

rary license that is valid as soon as the application form is mailed to the FCC. That's the good news, such as it is. The bad news is that FCC Chairman Richard Wiley told a Congressional subcommittee he favors restoring the CB license fee from the current \$4 to the former \$20. At that rate, CB users would pay the FCC about \$100 million a year, nearly twice the entire budget of this communications regulatory body. Hardly seems fair when you consider that the FCC also regulates the telephone company and all TV and radio broadcasters.

Weighty question

The National Bureau of Standards is looking for the answer to an age-old question: What's a portable? The television industry's answer—"anything with a handle"—apparently won't do, as NBS studiously attacks the problem of the maximum weight and bulk to qualify for the appellation. Just another boon-doggle? Well, it may have some practical applications since the study is being conducted for the Federal Trade Commission that will use the results in its guidelines under the Warranty Act. Because many set manufacturers state that portables must be carried into the shop for warranty service, the Bureau's findings could affect future servicing policies. Wonder if they'll make a special classification for "hernia model?"

Betamax

Although Sony's Betamax home videocassette recorder has been on the market in color TV console form since late last year, it's now becoming available as a deck attachment—the first such deck designed exclusively for the consumer market. The deck is priced at \$1,300, including an accessory digital timer. It is

designed to record television programs while the viewer is away from home, or to record one program while another is viewed (since it has its own tuner). A one-hour cassette sells for \$15.95, a new low for videotape. The secret of Betamax's tape conservation is the elimination of the guard-band between helical tracks.

Betamax will be phased into the United States gradually, market by market. It is being promoted as a "time-shift machine," to rearrange TV schedules according to the wishes of the viewer. No accessory camera is yet available. Some pre-recorded cassette educational courses are already available from Time-Life and are being offered to Betamax users.

Unlike Sony's highly successful educational-institutional U-Matic videocassette recorder that uses ¾-inch tape, Betamax employs ½-inch cassette tape. In answer to questions about the limitation of 60 minutes per cassette, Sony officials said they are developing a cassette-changer attachment as well as a longer-playing cassette.

Brainy turntable

The latest thing in turntables is the ADC Accutrac. It uses a wireless remote control to permit the user to select up to 24 programs on 13 separate tracks of an LP disc in any sequence. An infra-red generator in the pick-up arm scans the record surface. The beam scatters when it hits the closely spaced grooves within a selection, but is reflected back to a detector in the arm when it hits the smooth surface between selections. The remote transmitter has select, play, cue and reject controls. The price of the direct-drive turntable with automatic programming is \$500.

A changer version, to be available next year, will let the user program selections and the order in which they're to be played from up to six dif-

ferent records. The concept could lead to a new type of jukebox that uses a few LP's instead of individual-selection records and which will search and locate any specific track selected by the coin-dropper.

New picture tube

That new Zenith color picture tube, reported here last month, will be introduced in a brand new 19-inch set series in August. It's a departure from standard tubes in that it's designed for automated production from glass to gun. The faceplate is a single piece of curved glass, as opposed to the traditional glass with a "skirt" or flange. This permits lower-cost glass production, automatic deposition of phosphors and more manufacturing precision. The deflection angle is 100 degrees, a compromise between the current 90 degrees and the power-consuming 110-degrees.

The tube has a new tri-potential gun with a second focusing grid that permits a spot size 60% smaller than the standard gun. This means, according to Zenith, that it can now produce high-resolution slot-mask color tubes in 19- and 25-inch sizes. The 19-inch version is about 2½ inches shorter than a conventional dot-mask 90-degree (delta-gun) 19-inch picture tube, but only about 0.6-inch shorter than the slot-mask 90-degree tube being used by most manufacturers (not including Zenith).

The net result may not be so obvious to the TV set buyer, but on first inspection the new tube provided a good clear and bright picture, comparable to other Zenith Chromacolor tubes. The prospect of complete automation of the picture-tube manufacturing operation, if realized, could eventually provide consumer benefits in terms of price and performance.

DAVID LACHENBRUCH
CONTRIBUTING EDITOR

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Sensitivity for 10 dB S+N/N: 0.5 microvolt
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Circle 3 on reader service card

Diplomatic bugs and antibugs pose embassy health problems?

Radiation in some diplomatic headquarters may be great enough to create potential health hazards, according to recent newspaper reports. These state that the Ambassador to the Soviet Union, Walter J. Stoessel Jr., personally warned the Embassy staff in Moscow that Soviet microwave transmitters were beaming high levels of energy into the Embassy. Apparently there was no evidence that the levels were so high as to cause biological damage, but obviously the possibilities were significant enough to make a warning seem advisable.

It was believed at first that the Soviet transmissions were intended to activate listening devices planted in the Embassy. A later report, in *The New York Times*, states that "the electromagnetic waves are coming—both sides privately concede—not from Soviet equipment designed to eavesdrop on the Embassy, but from Russian machinery trying to jam American listening devices in the big embassy building. . . ."

The type of bugging that requires microwave transmission is usually carried on by planting passive devices tuned to a given frequency. They will then radiate signals beamed to them on that frequency. In the famous bugging of the Great Seal hung over the desk of the U.S. Ambassador in Moscow, the device was a cylindrical chamber coupled to a 9-inch whip antenna, the system being resonant to 330 MHz. The front wall of the resonant chamber (approx. 3 inches in diameter) was a flexible metal diaphragm. Sound waves pressing against it changed the chamber dimensions slightly, causing the resonant frequency to vary from 330 MHz. Thus when a Soviet 330-MHz wave was directed at it, modulation by speech in the room would cause the resonant frequency to vary, reradiating more or less strongly as it approached and departed from the steady-state 330 MHz. Of course another strong signal at or near 330 MHz would have jammed the Soviet listening frequency, and it is that kind of jamming that is suspected in the present case.

Other kinds of bugging call for high microwave power. Theoretically, a high-power beam directed on a window pane and reflected to a receiver might carry intelligible information, much the same as the resonant chamber does. So far, no one has reported any successful experiments in this direction, but it is unlikely that successful experiments in such a field would be widely publicized.

Microwave emissions, though less dangerous than X-rays, can produce harmful biological effects, though enormous

amounts of power would be necessary to build up dangerous levels more than a few yards away from the transmitting antenna.

New multi-media technique for prison health care

The University of Miami, in cooperation with the Department of Hospitals of Dade Co., FL, and the health systems department of Westinghouse Electric Corp., is engaged in a two-and-a-half year evaluation of a new health-care technique. The new technique combines two-way audio, television and medical data links for observation of symptoms and consultation with nurse practitioners to make medical aid available to medically isolated people.

Two-way audio-visual communication links are installed between Miami's Jackson Memorial Hospital and three institutions in Dade County—the main jail, the stockade and the women's detention center. Specially trained nurse practitioners staff the three jail clinics.

Three approaches are being evaluated, a black-and-white live TV system at the main jail, a slow-scan system with video stills transmitted over the ordinary phone line every 90 seconds at the stockade, and both live and slow-scan color TV at

the women's center. Voice channels, electronic stethoscopes, electrocardiography (EKG) channels and facsimile transmitters assist in patient care.

All communication is two-way—the patient and doctor see and hear each other. The nurse also has a monitor with which she can see the picture received by the doctor.

This combination of facilities—none of them new in themselves—offers opportunities greater than have been possible with remote-care systems in the past. An example was a patient with chest pains, possibly due to a heart attack. An EKG was transmitted to the doctor who simultaneously listened to sounds from an electronic stethoscope that the nurse applied to the patient's chest and back as directed by the doctor. He was also able to watch the patient's facial expression and his neck veins as he stood up and lay down as directed while watching the EKG printout (that could have been transmitted by ordinary telephone). The result was a verdict of indigestion.

Probably most useful in isolated institutions, such as prisons, geriatric care facilities and remote military installations, this technique could also find wide use in the rural areas of developing nations.

(continued on page 12)



MULTI-MEDIA PATIENT CARE. (right) The doctor controls camera position and zoom, focus and brightness from his console, and can give instructions while receiving verbal, visual, stethoscopic, EKG and hard-copy medical information. (left) The patient can see, hear, and speak to the doctor—communication becomes face-to-face. The nurse can also see on her monitor the picture that the doctor is viewing.

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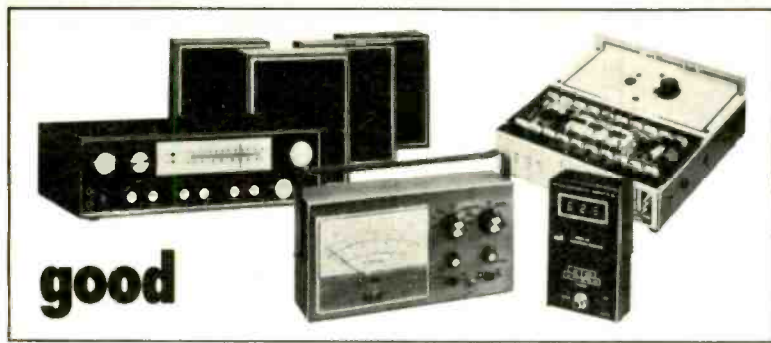
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better

11 kits: Quadraphonic Stereo and B/W TV...\$550

or low monthly terms

A complete course in B&W and Color TV Servicing, including 48 lessons (18 on color TV) 10 special reference texts and 11 training kits. Kits you build include 4-speaker Quadraphonic System, solid-state volt-ohmmeter, CMOS digital frequency counter, electronics Discovery Lab, plus a 12" diagonal solid-state black & white portable TV to build and use. At each assembly stage, you learn theory and "Power-On" application of that theory in typical solid-state TV sets.



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11 kits: 19" diagonal Color TV...

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best

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Microcomputer interfacing workshop

A three-day workshop based on the popular 8080 microprocessor will be held September 23, 24 and 25, 1976. Sponsored by the Virginia Polytechnic Institute and State University, Extension Division of the Continuing Education Center in Blacksburg, Virginia, the course will include many hours of experience in programming and interface construction with over 12 operating microcomputers for participant use. For more information, contact Dr. Norris Bell, Virginia Polytechnic Institute and State University, Continuing Education Center, Blacksburg, VA 24061, or call 703-951-6328.

Buffalo TV stations plan to jam signals to Canada

A Canadian government decision to ban all foreign commercials on Canadian cable-TV systems has led to plans to prevent U.S. signals from entering Canada in usable form. Thus Canadian cable-TV receiving stations would not be able to pick up U.S. programs for transmission to their subscribers.

More than 40 percent of Canadian households subscribe to Canadian cable-TV, which is described as the fastest growing enterprise of its kind in the world. The reason is that the cable supplies U.S. network programs to thousands of people who are too far away from the border to receive U.S. television direct. Up to the present, the American stations have been quite happy with the situation since they could allow their large Canadian audience to be reflected in their advertising rates.

Deletion of the U.S. commercials from Canadian cable programs—presumably with the object of encouraging advertisers to use Canadian broadcast stations—would cut sharply into the revenues of the Buffalo stations. Therefore, WBEN-TV, WGR-TV and WKBW-TV have applied to the FCC for experimental license to erect a relatively low-power station that will transmit signals at frequencies sufficiently different from the frequencies of the Buffalo stations to superimpose a herringbone or "hash" pattern on them that would completely destroy their entertainment value.

The geography of the area is such that a station can be erected with a directional pattern that would jam practically all the signals going into Canada, while having practically no effect on New York areas.

The Canadians are—understandably—somewhat upset by the prospect, and at last accounts were studying international radio law to discover if etheric pollution of this type is illegal. But both Canadian

TV viewers and American TV broadcasters were—at the time this was written—hoping for an amicable solution, possibly an arrangement by which the U.S. stations can share in the profits they feel they have created for the Canadian cable companies.

Marconi Fellowship goes to Japanese electronic engineer

Professor Hiroshi Inose of the University of Tokyo has been selected to receive the 1975 Marconi International Fellowship, an award of \$25,000. The award, for his "contributions to mankind through research and development in the applications of electronic computers to practical problems," will be presented to him by Prince Philip, the Duke of Edinburgh, at the Royal Society of Arts in London in early May.



PROFESSOR HIROSHI INOSE

Professor Inose was nominated for the award by Dr. John R. Pierce, California Institute of Technology, and by the Communications Society of the IEEE.

Lab for laser energetics at University of Rochester

A \$46.5 million Laboratory for Laser Energetics is being established at the University of Rochester (NY). It will be the first university-government-industry teaching and research center in laser and energy studies that will also be available to scientists all across the country.

The laboratory's principal instrument will be a 10,000-joule (a joule is a unit of energy equal to one watt applied for one second) neodymium glass laser system, which will be among the world's most powerful systems for fusion and energy research. The principal project of the lab will be to explore the feasibility of controlled nuclear fusion as a clean, abundant future energy source.

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The Monster



The new BA 5000 Power Amplifier from Sansui

The most dramatic component in Sansui's new "DEFINITION" Series, the BA 5000 solid-state power amplifier is capable of 300 watts min rms per channel into 8 ohms, both channels driven, from 20 to 20,000 Hz, with no more than 0.1% harmonic distortion in the stereo mode. What's more, the BA 5000 can be strapped for mono operation to deliver 600 watts rms under the same conditions.

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output in stereo and 4, 8 or 16 ohms plus 70 volt line output in mono. A rating of 600 watts into a 16 ohm distortion, 20 to 20,000 Hz, is simply unprecedented in transistor equipment.

The "DEFINITION" series also includes the BA 3000, our Junior Monster, and the CA 3000 a very high quality, low distortion preamplifier.

For professionals, sophisticated audiophiles and monster lovers everywhere. See it and touch it if you wish at your nearest Sansui franchised dealer or write for complete literature.

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Circle 6 on reader service card

letters

MORE ON SOUND GUARD

After reading my story about Sound Guard, the new Ball Corporation record preservative (R-E, March, 1976), several readers have written to me regarding one point which was not specifically discussed in that article. Many disc enthusiasts wondered what would happen if they used one of the liquid record cleaning products on their discs after they had been treated with the new Sound Guard coating.

I have asked the people at Ball Corporation about this and, according to their experts, it is perfectly safe to use such liquid cleaners on records that have been Sound Guard coated. They point out, however, that such treatment is apt to be required less often since Sound Guard, in addition to its preservative function, also contains a small amount of anti-static material which should reduce dust attraction significantly. They also point out that Sound Guard is soluble in some of the commercially available record cleaning solutions and therefore may be partially or entirely removed from the surface of a disc when such additional cleaning solutions are used.

The makers of Sound Guard therefore suggest that after liquid cleaning of recordings, an additional protective coating of Sound Guard be applied for continued protection and preservation of the record surface.

LEONARD FELDMAN
Contributing Hi-Fi Editor

DIGITAL STOPWATCH

Several readers have written to us stating that they have had difficulty locating the Motorola MC14571 specified for IC5 of the Electronic Stopwatch in the November 1975 and February 1976 issues. This IC was a developmental type that has since been replaced by the MC14081.

Several errors have also popped up. Mr. Tyler tells us that the battery polarity is wrong in the calculator schematic (Fig. 1 of the article.) It should have been drawn with the negative side to ground.

The stopwatch schematic (Fig. 5 in the February 1976 issue) shows two pin-5's associated with IC2. The right-hand pin-5 connected to D3 of the 6-digit display should be pin-6. There are also two D1's shown in Fig. 5. Since all the diodes are the same type-number, this shouldn't cause too much of a problem.—
Editor

WIFE TO BARDOT

Upon seeing the cover of the March, 1976, issue of R-E, specifically "Build One of These," ASCII To BARDOT Converter, I am anxiously awaiting my next

issue that, I hope, will contain a WIFE To BARDOT project.

JOHN P. SCHOENHARL
Dayton, OH

Talk about novel ideas! If any of our more ambitious readers come up with a prototype for this, please submit it. We certainly would be interested. Maybe if all our readers pool their efforts. . . .
—Editor

MINI VS. MICRO

I wish to express disagreement with J. Titus et. al., "Komputer Korner 2," Feb. 1976. They state that "microcomputers are not as sophisticated as some of the popular minicomputers and cannot easily perform certain types of data processing problems." They also imply that surrounding microcomputers with large amounts of input-output equipment is a waste of money. I disagree violently with them and feel that they should have mentioned that with \$5000 worth of equipment, a microcomputer can usually perform the tasks that \$10,000 systems by big-name manufacturers perform. This is not due to the quality of the microprocessor but is a result of the pricing structure of the big manufacturers. While flipping through the Digital Equipment Corporation's price list for PDP8A400 equipment, I find a real time clock for \$320 whereas IMS has an 8080 clock for \$138. A disk system costs either \$11,000 or \$1,500 depending on whether you want a mini or a micro.

ROBERT M. LOSEE
Chicago, IL

We still must say that it is not very wise to add a large amount of I/O equipment such as cassettes, floppy disks, etc. to a microcomputer. You may if you wish, but right now you'll spend most of your time waiting for delivery, assembling kits and debugging your system. Time is money. I think you'll find the final cost almost equal for mini and microcomputers.

I feel that the availability of software is what swings things finally to the side of the minicomputers for most data processing tasks. The PDP-8, PDP-11 and NOVA families have thousands of applications programs that just aren't available for the microcomputers. BASIC for the 8080 is a start but I have seen very few programs that really do anything.

*Disks are available in the price range you mention, but I think that you'll find that floppy disks for both minis and micros are in about the same range.—
Jonathan A. Titus*

SERVICE MATERIAL

I am glad to have a chance to write to
(continued on page 88)

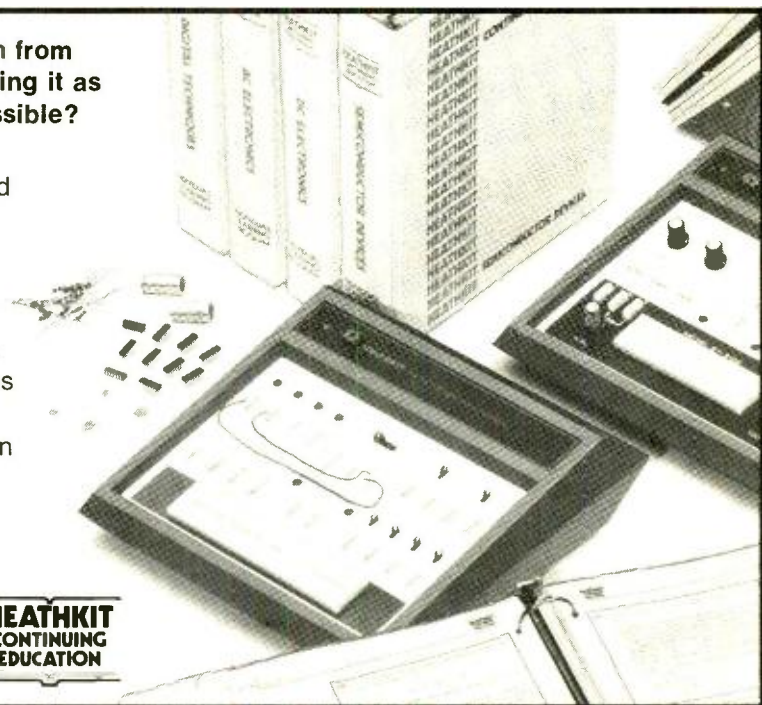
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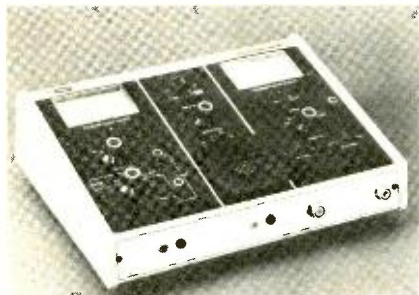
Circle 100 on reader service card

JUNE 1976

15

equipment reports

B & K MODEL 1040 CB SERVICEMASTER



Circle 88 on reader service card

CB RADIO IS GROWING. THE FCC WILL CONFIRM that this is the understatement of the century. The sheer mass of the little radios has brought on a massive demand for service facilities. Two-way radio shops are already overloaded. So, this leaves the TV shop. They have the trained men and most of the test equipment. FCC Rules state that no one but licensed technicians can make adjustments to the transmitters that will "result in unlawful operation." Translated, this means excessive RF power output or off-frequency operation. However, in most of these sets the frequency adjustments are crystal-controlled and sealed. The finals are designed so that they cannot radiate more than the legal power limit. It is *not* illegal to test the transmitters for legal power output and modulation.

So, this leaves a lot of room for legal servicing of the receivers, power supplies, antenna installation, and similar troubles. Only a small number of specialized test equipment is needed to do this type of work. The B & K Division of Dynascan, 1801 West Belle Plaine Ave., Chicago, IL 60613, has come up with a new unit—the 1040 CB Servicemaster. With this instrument plus normal TV service equipment, the TV technician can make readings of RF power output, check for standing wave ratios (SWR), read receiver power output, test for modulation and distortion, and check practically everything about them. The model 1040 is an all-in-one compact package and very simple to use. It can be used for bench testing with its built-in AC power supply, or in a vehicle with battery power from the cigarette lighter socket.

As a matter of fact, this is a real "package deal." All you need is a few test cables to hook up the CB set to the 1040 and from then on it's all pushbutton testing. A very comprehensive manual comes with the instrument. This covers not only the uses of the 1040, but what they modestly call a "short course" in CB radio servicing. All necessary tests for

both receivers and transmitters are included; even single sideband (SSB) transmitters may be checked.

Using the model 1040

The 1040 is divided into two main sections. One section is for transmitter tests. It has an RF wattmeter with ranges of 10, 50 and 100 watts. So, it can be used for testing radios in the Business band and others with higher power-output.

An internal 50-ohm load is provided. The CB set's own antenna may be used also by flipping a switch from INT to EXT RF load. All that you need is a short piece of coaxial cable with a plug on each end. This connects to the TRANSMITTER input jack of the 1040. The vehicle or fixed station antenna may be connected to the EXT. RF LOAD jack.

Now, by pressing the mike button you can read the average RF power output directly on the meter. Set the FUNCTION-SELECTOR switch to REV position and you read the reverse RF power; this is what is being reflected back from the antenna when it is mismatched. By setting the switch to SET REF position, you adjust the meter for full-scale. Turning to READ SWR gives you a direct readout of the SWR. The lower this ratio, the more efficient the antenna and the greater the output power. A ratio of 1:1 is considered ideal and most of the good commercial vehicle or fixed antennas will come very close to this.

With the external battery power (two screw terminals on the back panel, polarity-marked) the model 1040 can be used to check for SWR on antennas in vehicles. With some of the unusual configurations seen today, this is always a good idea. The transmitter can also be checked for legal RF power output. This is now 4 watts RF into the antenna.

Modulation of the transmitter may be checked in one of two ways. Switching the RF POWER switch to the PEAK position and then modulating the transmitter should show an increase in the RF power. With full modulation, the increase should be about 22%. You can look at either the unmodulated RF envelope or the modulated RF carrier by connecting an oscilloscope to the BNC jack labelled SCOPE on the back panel. You do *not* need a 35-MHz scope to do this. They thought of that—the model 1040 includes a mixer circuit that beats the 27-MHz RF carrier down to about 1.5-2.0 MHz. Practically all scopes will show the modulated carrier envelope at this frequency. Actual modulation percentage can be calculated by measuring the pattern on the scope.

The receiver section of the 1040 has two audio outputs—one is a 1,000 Hz tone and the other a 2-tone mixed signal consisting of 500 Hz and 2400 Hz. The output of either of these can be fed to a small

speaker mounted on the front panel. Volume of this is controlled by the AUDIO GAIN control just above. To get a fixed frequency AF modulation, set the switch to 1 kHz, hold the mike face-down on the speaker and press the mike-button. The modulation percentage can be varied by adjusting the AUDIO GAIN control.

Both of the audio signal outputs are available at the AUDIO OUTPUT jacks on the panel. So; they can be used for testing the mikes as well. If the transmitter has good modulation when the signal is fed directly into the audio input, but it is weak when the mike is held over the speaker, this indicates that a new mike is needed!

The 2-tone test is used for checking modulation of SSB transmitters. Many CB sets can be switched from AM to SSB. FCC Standards require a very low level of intermodulation distortion. (This is also essential for clear communications, of course!) The prescribed test is feeding in two audio-tones simultaneously. The tones must not be harmonically related in any way. The 500-Hz and 2400-Hz tones meet these specifications. The IM product of these must be a minimum of 25 dB down at the output. To make a precise test of this, a spectrum analyzer is needed. However, you can display the modulation envelope of a SSB transmitter, just as with an AM transmitter, and get a good visual check. If you can see that the modulation peaks look like the 2-tone signal looks on a scope, the chances are that the modulation is all right. The 2-tone signal can also be fed through the speaker into the mike to check it for possible distortion. I might add here for the benefit of those who are as ignorant of actual SSB test procedures as I was, watch it! On SSB you will *not* see an *unmodulated* RF carrier on the scope! In SSB, both the carrier and one sideband are suppressed. There is actually *no* RF output until it is modulated! You'll see no reading on the meter or scope until modulation is applied.

The receivers can also be checked for audio power output, distortion, sensitivity, etc. For audio tests, the 1.0 kHz tone is fed into the audio input of the receiver. The external speaker or phone jack of the CB set is connected to the RECEIVER AUDIO jacks on the panel. A LOAD SELECTOR switch lets you select the correct load impedance—4, 8 or 16 ohms. The audio power output can be read on three ranges, 0.1, 1.0 and 10 watts. For reading this, the AUDIO GAIN and VOLUME control on the set are adjusted to check for the power output on the meter. To read distortion, turn the switch to SET FULL SCALE position and adjust the control for a full-scale reading. Then turn the switch to the ADJ FOR MIN position, and adjust the % DIST control for the lowest reading. This gives

(continued on page 18)

The Black Watch Kit \$29.95



Dimensions: 1½" x 1" x 3/10"
Weight: ½ oz.
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| 4. trimmer | 9. battery-clip | |

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EQUIPMENT REPORTS

(continued from page 16)

you a direct readout of the percentage of 3rd harmonic distortion in the receiver audio stage.

This is important in two ways. Practically all of these transceivers use the receiver audio stages for the modulators. This test can be very helpful in finding the cause of distortion in the transmitted signal. For example, if you read the normal 4 watts of RF power, unmodulated, but the audio stages show a maximum output of only 2 watts audio, you will not have enough audio power to produce full modulation. This will cause a clear but weak signal. The reverse is also true. If

you read only 2 watts RF and 4 watts audio, the transmitter is being overmodulated and will garble.

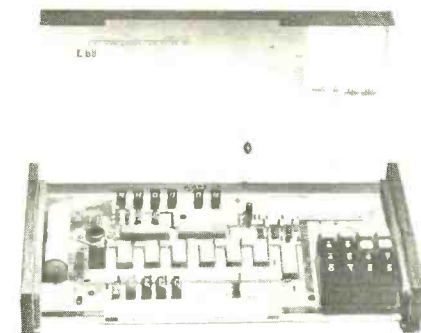
To check for sensitivity, an RF signal generator can be connected to the BNC RF GENERATOR jack on the back panel. It will feed directly into the receiver antenna. You can check for calibration and RF sensitivity if the signal generator has a calibrated RF attenuator.

The third BNC jack on the back panel can be connected to a frequency counter. Just push the mike button and read the channel frequency directly.

This is a very complete "package" for servicing of CB radios, either on the bench, car, boat, mobile home or what have you. With only a few other test instruments, usually already on the bench,

you can get into the CB radio service business in a big way for not too much money. While checking the prototype out, we had a chance to make direct comparisons with some far more expensive types of equipment, and found that the accuracy of the 1040 compared very well with these! **R-E**

EPA Micro-68 Computer



Circle 120 on reader service card

ELECTRONIC PRODUCT ASSOCIATES' answer to microcomputer fever is a self-contained system complete with power supply and a wood and smoked plastic 9 x 12 x 2 inch (229 x 305 x 51 mm) case. Plug it in and you're ready to start programming.


The Micro 68 is built around the Motorola M6800 microprocessor. It has a six-digit seven-segment display and a 16-key hexadecimal-input keyboard. The display is seven-segment, not a true hexadecimal format, so B and D are indicated by lower case representations using the seven segments. The decimal point is lit when "b" is displayed to help distinguish it from a "6."

The system is controlled by the John-Bug PROM monitor, one of the most sophisticated of the keyboard-display kind. In its basic form, the kit is intended as a learning tool or prototyping system for engineers, scientists, and laymen.

The monitor system is contained on four 1K bit PROM's for a total of 4K bits or 512 8-bit words of firmware. The lettered keys on the input keyboard double as control keys for the system. Keys A through F have been assigned the functions AUTO, BACK, CHANGE, DO, EXAMINE, and FORWARD.

To get started, press the one remaining button, the RESET button, and the display lights up with EPA uP . . . very cute. Pressing EXAMINE lights up dashes in the four leftmost places. Punching in an address puts the address in the first four digits and the two remaining digits, which are slightly separated from the rest, light up with the contents of that memory location in hexadecimal. The FORWARD key increments the address one location each time the button is depressed. BACK is an unusual feature not found in most similar systems. It decrements the address and displays memory contents. It is particularly convenient to have the address displayed simultaneously so you don't have to worry about losing your place or getting confused when sequential memory locations are loaded with the same instruction or data.

(continued on page 20)



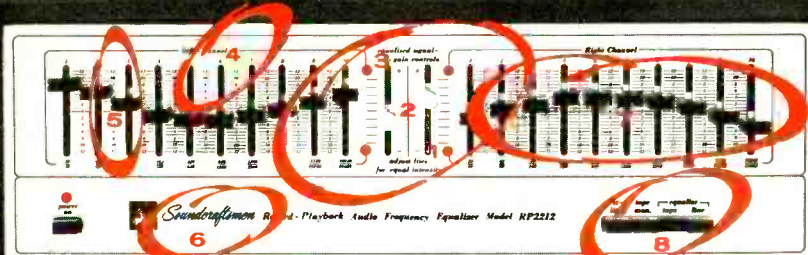
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- 3. YOU NEED AUTOMATIC/CONTINUOUS OUTPUT-OVERLOAD WARNING SIGNAL:** SOUNDCRAFTSMEN'S 2 top L.E.D.'s glow brightly, (bottom L.E.D.'s off), if output voltage is boosted excessively, thus eliminating the danger of distortion and/or damage to related equipment resulting from the high voltages that can be generated by any fine equalizer. . . .
- 4. YOU NEED A POSITIVE METHOD OF READING 1 dB SETTINGS. . . .**
- 5. YOU NEED AT LEAST 24 dB TOTAL CONTROL OF EACH OCTAVE. . . .**
- 6. YOU NEED A UNIT THAT WILL ADD ZERO NOISE AND DISTORTION:** SOUNDCRAFTSMEN'S signal-to-noise and distortion performance figures are far superior to most high fidelity components. SOUNDCRAFTSMEN products are used in professional broadcast and recording systems, assuring you of completely noise-free and distortion-free integration into your system. . . .
- 7. YOU NEED TO BE ABLE TO LOOK AT YOUR ACTUAL "EQ" CURVES. . . .**
- 8. YOU NEED THE ABILITY TO EQUALIZE TAPE RECORDINGS. . . .**



9 YOU NEED AN ACCURATE, EASY-TO-USE INSTRUCTIONAL TEST RECORDING FOR ENVIRONMENTAL EQUALIZATION: SOUNDCRAFTSMEN'S "includes Test Record recorded and designed exclusively for SOUNDCRAFTSMEN equalizers. Without any expensive test equipment or technical knowledge, you can quickly tune the acoustics of your room, just by following the announcer's step-by-step directions.

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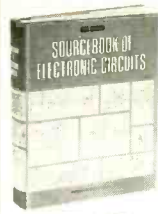
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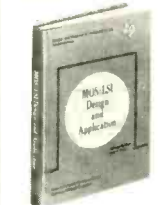
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EQUIPMENT REPORTS

(continued from page 18)

To load a program or alter something at a particular address, first get to that address using the E, F, and B keys and then press CHANGE. The rightmost display digits

are extinguished and become loaded with the new data that is keyed in. Another unusual feature is the A key that automatically enters the data, increments the address and awaits the next entry. By using the AUTO function, you can quickly enter a program by continuously keying in the instructions in hexadecimal without the

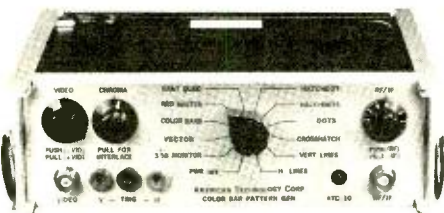
nuisance of hitting any additional keys. If you hit a wrong key or make a mistake, you can immediately correct it by pressing RESET and using the other functions to backtrack, or you can continue on and go back later. It is probably wise to examine the program when you are finished entering it and make the corrections then.

TABLE 1—COUNT SIX PROGRAM

0000 DE LDX THREE	001B 48	0036 DE LDX THREE
0001 45	001C 84 ANDA OF	0037 45
0002 4F CLRA	001D 0F	ADD 0038 A6 LDAA NBR, x
ZRONBR 0003 A7 STAA NBR, x	001E BD JSR LDDSPY	0039 48
0004 48	001F F1	003A A9 ADCA INCR, x
0005 09 DEX	0020 A5	003B 4B
0006 26 BNE ZRONBR	0021 DE LDX STORE	003C 19 DAA
0007 FB	0022 47	003D A7 STAA NBR, x
NXTCNT 0008 BD JSR CLRDSPY	0023 08 INX	003E 48
0009 F1	0024 9C CPX FOUR	003F 09 DEX
000A BA	0025 4F	0040 26 BNE ADD
000B DE LDX ONE	0026 26 BNE LDTWO	0041 F6
000C 4D	0027 E5	0042 7E JMP NXTCNT
LDTWO 000D A6 LDAA, NBR, x	0028 CE LDX 15	0043 00
000E 48	0029 00	0044 08
000F 44 LSRA	002A 15	THREE 0045 00
0010 44 LSRA	LOOP 002B DF STX STORE	0046 03
0011 44 LSRA	002C 47	STORE 0047 00
0012 44 LSRA	002D BD JSR DSPLY	0048 00
0013 DF STX STORE	002E F1	NBR+1 0049 00
0014 47	002F C7	004A 00
0015 BD JSR LDDSPY	0030 DE LDX STORE	004B 00
0016 F1	0031 47	INCR+1 004C 00
0017 A5	0032 09 DEX	ONE 004D 00
0018 DE LDX STORE	0033 26 BNE LOOP	004E 01
0019 47	0034 F6	FOUR 004F 00
001A A6 LDAA NBR, x	0035 0C CLC	0050 04

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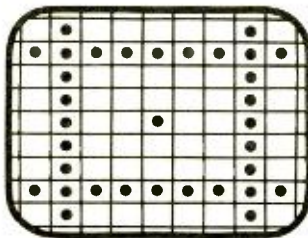


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When the program is entered and ready to go, press D and "do" lights up in the rightmost two digits. Entering the starting address starts the program as soon as the last key is released.

One more feature is the shared function of the "8" key. Next to it is printed RTI (Return To Interrupt). It is very useful for debugging programs by inserting software interrupt instruction—in your program. Each time the program encounters the instruction, the system is interrupted. The monitor dumps the MPU registers into assigned memory locations that can then be examined as well as any other memory locations. Depressing the RTI key will resume the program from where it left off or from a new condition set up by the programmer. If there is a loop in the program, it is possible to circle the loop each time the button is pressed and recheck the system status each time around.

As with most ROM or PROM monitor systems, the subroutines in the monitor can be used by the programmer. This is particularly helpful in using the display. The Micro 68 display is multiplexed (the segment lines to the six digits are all in parallel.) The software and the monitor program is used to scan the display. One assigned memory location is used as a digit mask. Setting one of the bits to a logic 1 enables a corresponding display digit. Another memory slot is loaded with the character pattern to be displayed.

I have some suggestions for the programmer, particularly the beginner, when approaching this system. Make a numeri-

(continued on page 30)

What are your opportunities in the electronics field?

Here are some eye opening facts from ETI.

Q. What about the job market in electronics?

A. It's good. In fact, it seems to be one of the few fields that stays relatively steady in bad times. Today, for example, estimates indicate that several thousand jobs will be opening up for electronics technicians each year, for years to come. One reason for this is the fact that electronics are the basis of almost all communications, and this is a communications-oriented nation.



Q. What kind of jobs are you talking about?

A. For example, there are jobs available in electronic/industrial automation, electronic equipment repair and servicing, in the broadcast and radio telephone communications field, at airports, and even in medicine and in hospitals, where electronics are rapidly increasing in importance. And there are hundreds of other jobs opening up as electronics continues to make great strides, in new ideas and developments.

Q. Can such a complicated subject as electronics be successfully taught by the home-study method?

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vided by ETI. For example, its course in the Fundamentals of Electronics features an exclusive teaching system called Autotext. And throughout all the courses the student is thoroughly monitored and carefully guided by a licensed instructor, whose professional and personal interest is to see that he masters every bit of information presented to him. Of course, we must give a lot of credit to our students themselves. They know that no matter how good the instructor and instruction may be, they have to make it work. So most of them apply themselves diligently, and they find the more they learn, the more they want to learn.

Q. But I have a job, and as much as I would like to get into electronics, I can't afford to take time off. How do I get around that?

A. You don't have to take time off from your job. You study at home, in your free time. We do advise, however, that you set aside a certain time for your study schedule and stick to it, even if it's only a couple of hours a day. The beauty of the ETI way of learning is that you work at your own pace, making sure you've completed your assignment thoroughly and completely. We think you'll find, as you go along, that learning the ETI way can be fun.

Q. But I was never very big on books and study. I like to work with my hands.

A. With your ETI course, you'll get plenty of work with your hands. In fact, the



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Q. It all sounds very interesting and inviting. But I wouldn't want to commit myself before knowing more.

A. We wouldn't want you to. In fact, we insist that you check it out first. All you do is fill out the coupon and mail it to us. We'll send you a colorful new 48-page ETI Career Book that will give you the facts and the many opportunities ETI can open up for you. If you like electronics, you'll enjoy reading this book.

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KOMPUTER KORNER

How the microcomputer controls input/output devices with software

DAVID LARSEN, PETER RONY,
and JOHN TITUS*

THIS MONTH WE WOULD LIKE TO EXPLAIN how computer instructions cause an I/O device to operate. The I/O device that we shall choose for our discussion is the optically isolated solid-state AC relay. These relays can control any AC power device within the output current ratings of the relay. Shown in Fig. 1 are typical solid-state relays that are available for prices ranging from \$5 to \$20 in quantities of one. Such relays permit a single TTL output signal (logic 0 or logic 1) to control up to 10 amperes of 220 VAC power, as is possible with the Hamlin model 7522 relay (top center of Fig. 1). Internally,

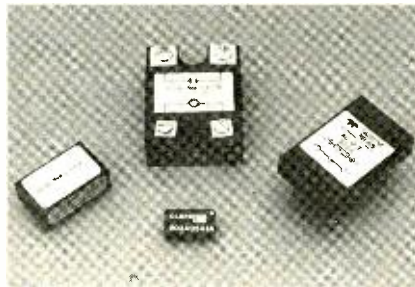


FIG. 1—TYPICAL SOLID-STATE RELAYS that are optically isolated.

each relay contains a light-emitting diode, a light-sensitive transistor, a power triac and a transparent dielectric optical path that isolates the digital and power circuitry. It can withstand a voltage difference of at least 1000 volts.

A typical microcomputer I/O circuit that employs the solid-state relay is shown in Fig. 2. Recall that the microcomputer sends synchronization pulses, called *device select pulses*, to the I/O device. In Fig. 2, these are the negative-going pulses from the SN74154 decoder circuit that, for an 8080 microcomputer, have a time duration of only 500 ns. It should be clear that a single 500 ns pulse cannot sustain the continuous operation of an AC power device. What is required is a simple "interface" between the microcomputer and the solid-state relay that would permit the AC power device to operate continuously, if it is so desired. A suitable interface is a single SN7474 positive-edge triggered flip-flop and a single buffer from a SN7407 hex buffer/driver IC. The buffer is needed since it is not good engineering practice to drive a solid-state AC relay directly from the output of a flip-flop.

With suitable software, the microcomputer and SN74154 decoder can generate individual device select pulses that either clear or set the SN7474 flip-flop. To clear the flip-flop and turn on the AC power device, only a single 500 ns pulse

*This article is reprinted courtesy American Laboratories

is needed. The flip-flop output, Q, will remain at logic 0 until a single 500 ns pulse is applied to the preset input at which time the AC device will turn off.

Any simple open-collector gate or inverter can be used as the buffer between the output of the flip-flop and the input of the solid-state relay. Suitable choices would be the SN7401 or SN7403 2-input NAND gates, the SN7405 inverter, or the SN7409 2-input AND gate.

Output instructions

We will discuss microcomputer instructions in considerable detail in subsequent columns. To summarize, there exist 78 different instructions for the 8080 microprocessor IC, and a total of 256 variations of such instructions. Each instruction contains a single 8-bit *instruction code* that indicates which type of operation or group of operations the microcomputer will execute. Some instructions contain two or three 8-bit words that are present in successive memory locations. A *byte* is defined as a group of eight bits occupying a single memory location. Thus, the 8080 microprocessor instructions are either 8-, 16-, or 24-bits long, with the first eight bits always being the instruction code.

The output instruction is a 16-bit instruction that consists of two successive bytes located in successive memory locations. The first byte, in binary code, is always 11010011. The second byte can be any 8-bit binary number from 00000000 to 11111111; this is the device code of the specific output device that will receive eight bits of data from the accumulator. The contents of the accumulator remains unchanged after the instruction is executed.

A simple program

The simplest program that incorporates the output instruction is probably the one given below:

Memory address	Instruction byte	Description
0	11010011	Send device select pulse to device given by following 8-bit device code
1	00000000	Device code for clear input to SN-7474 flip-flop
2	01110110	Halt the micro-computer

An 8080 microcomputer operating at a clock rate of 2 MHz will execute the previous program in 8.5 μ s. The AC-power device will remain on once the program has been executed. To turn off the device, a slightly different program is required:

(continued on page 24)

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(continued from page 22)

Memory address	Instruction byte	Description
0	11010011	Send device select pulse to device given by following 8-bit device code
1	00000001	Device code for preset input to SN-7474 flip-flop
2	01110110	Halt the micro-computer

after the microcomputer halts. A more practical program requires additional instructions.

Keep in mind that a memory address contains 16 bits. When we write, "memory address 0," we really mean the memory address corresponding to the following 16-bit binary word: 00000000 00000000. Note that we have split the 16 bits into two parts, the most significant 8-bits and the least significant 8-bits. The most significant 8-bits are called the HI (or H) memory address and the least significant 8-bits are called the LO (or L) memory address. Both the LO and HI ad-

relay shown in Fig. 2 will turn on and off according to various decisions made by the program. A typical microcomputer-controlled system could easily have several such relays.

In a more orderly and systematic treatment of the 8080 microprocessor, one would probably introduce the 8080 instruction set prior to the discussion of any particular instruction, such as the output instruction described this month. Since we do not believe that you are willing to wait several months until we get to the output instruction, we have decided to treat it first. In a future column, we will

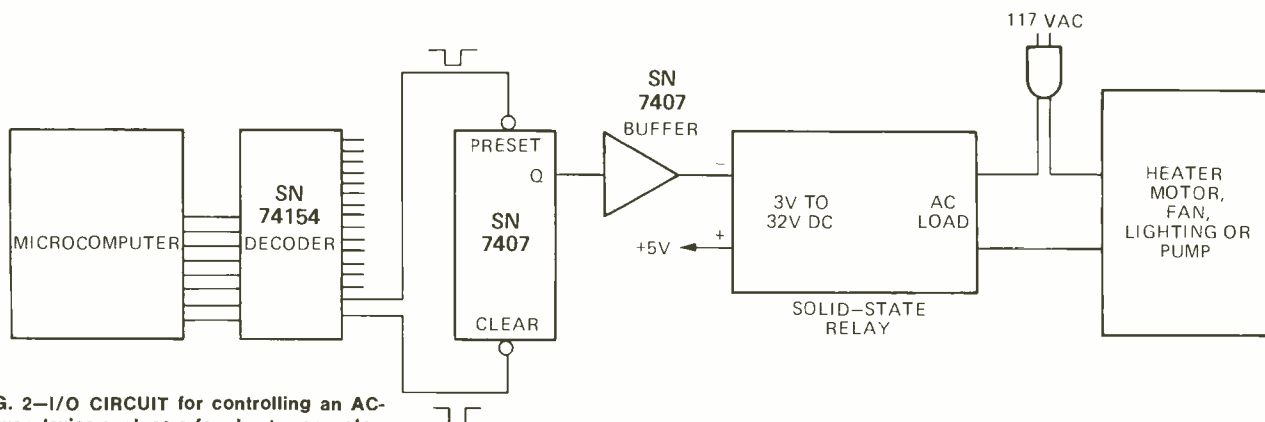


FIG. 2—I/O CIRCUIT for controlling an AC-power device such as a fan, heater or motor.

The AC-power device will turn off when the second instruction byte in the program is executed and remain off

address must be present for a memory location to be accessed.

With an actual program, the solid-state

explain how the 8-line-to-256-line decoder circuit shown in Fig. 2 generates individual device select pulses. **R-E**

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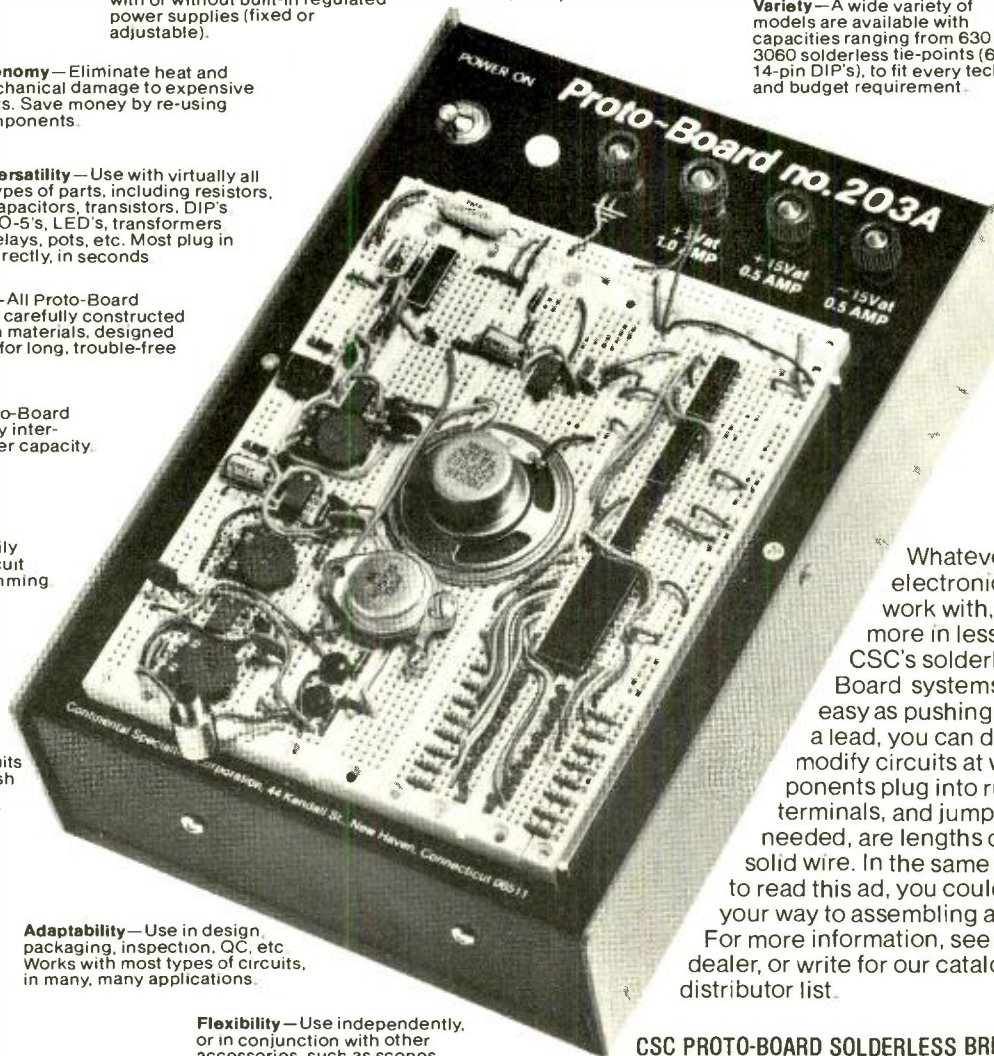
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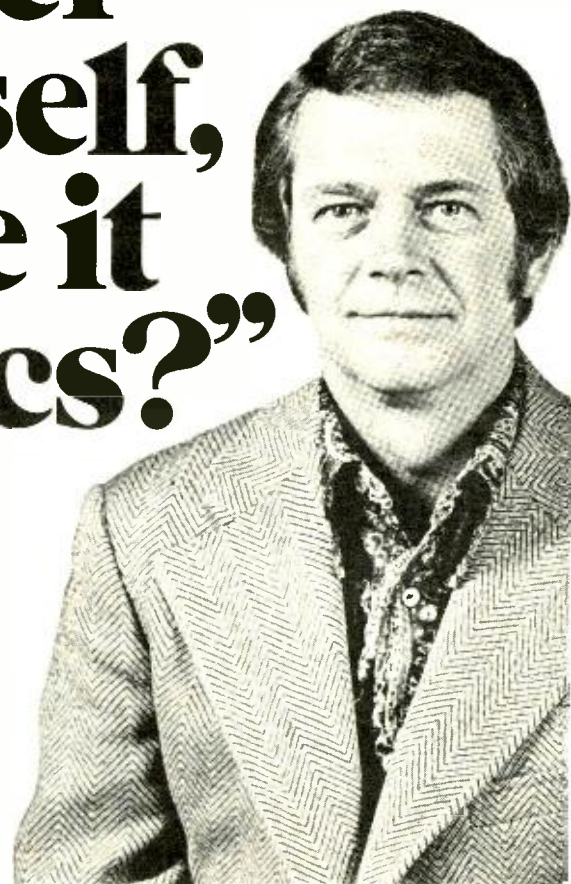
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Circle 14 on reader service card

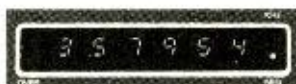
JUNE 1976

Autoranging Frequency Counting to 60 MHz with 1 Hz Resolution

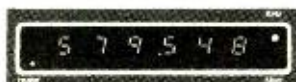


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Circle 15 on reader service card

EQUIPMENT REPORTS

(continued from page 20)

cally increasing listing of all the M6800 instructions so you can quickly analyze a program and then using the monitor, display its own contents in locations F000 through FFFF. EPA does not include a monitor listing and it will be useful to get an insight into programming techniques and to really understand what is happening when you use the subroutines in the monitor PROM.

Two Motorola/AMI 6820 Peripheral Interface Adapters are wired into the Micro 68 and are used to scan the keyboard and operate the display. The keyboard input port is wired in parallel to 16 connector pins and are also hooked to pull-up resistors. I haven't tried it, but these can probably be used as external device control outputs or inputs by the user.

If you get serious about this microcomputer, take a good look at my COUNT SIX program listing in Table 1.

The program starts with zeros displayed in all six display digits and then increments the count in steps of 1. The count is stored in the three memory locations starting at 0049, 004A, and 004B. The first eight instructions in the program are a loop that is traversed three times to load these three memory locations with their initial zero values. The bulk of the remaining instructions read these numbers out on the display. The three words consist of two digits each.

The display is set up to begin scanning from the left by the CLRDSPLY subroutine. The next loop is used three times, once for each 2-digit word. Each time around the loop displays two digits. First the left four bits of the memory word are shifted right and entered into the digit-display memory words by the LDDSPY routine. Then the same number word is recalled and the right four-bits are stored in the next memory word.

Once this procedure is complete, the actual display takes place in the next loop. The initial setting of the X register to 15 in the program determines the number of times around the loop and the rate of the display count. DSPLY does the actual scan of the six digits and includes a loop of its own, so there is a multiplication effect in the time it takes to finish this part of the program.

Finally the last part of the program increments the number by one. It is a multi-word addition that adds the 00 00 01 increment in locations 4C, 4D, and 4E.

I'm sure there are some tricks that can be pulled to shorten this program somewhat, but the display system demands some intricate programming.

As you can see, quite a few steps are taken to perform this simple exercise so the standard memory of 128 words does not go very far. Additional memory will probably be an early consideration.

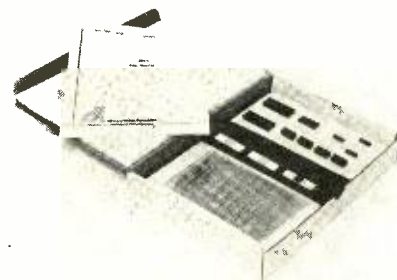
The Micro 68 documentation includes the *Motorola M6800 Systems Reference and Data Sheets Manual* and the *Micro 68 User's Manual*. Edge connectors are provided for memory expansion up to 64K words.

This system is not available as a kit.

The price of the fully assembled system is \$430. A maximum of 768 words of RAM can be contained on the main circuit board and goes for \$5.50 per 128 words. When you are ready for a data terminal, the Motorola MIK-BUG TTY monitor can be purchased for \$28.50. You will also need the \$40 TTY/RS-232C adapter in that case. An optional 8K static memory board sells for \$270.

Descriptive literature is available from Electronic Product Associates, Inc., 1157 Vega Street, San Diego, CA 92110. **R-E**

Microcomputer Associates JOLT Microcomputer



Circle 89 on reader service card

JOLT IS AN IMPRESSIVE MICROCOMPUTER designed for the serious application engineer and yet is a viable learning tool for the beginner. A fully equipped JOLT system can have as much as 32K of RAM and 128 bidirectional input/output lines. JOLT is a modular series of 4.25 x 7 inch (108 x 178 mm) PC boards that can be vertically stacked.

The minimum system configuration consists of a single \$159 CPU board. Microcomputer Associates has taken the MOS Technology NMOS MCS6502 μ P and surrounded it with a powerful complement of 12 other IC's. The JOLT CPU comes equipped with an R-C timing network that runs the on-the-chip clock oscillator at 750 kHz. A crystal can be mounted on the board for applications that call for that kind of accuracy.

Power up the CPU with a 5-volt supply and hook it to a video or printing terminal, and you have a highly usable system. It is one of the most sensible approaches I have seen so far.

How can a single small uncrowded board do such a superb job? By a rational balance between hardware and firmware. The JOLT CPU takes advantage of the family of 6500 devices. The MCS6530 Interface/Memory chip contains many of the vital system components. Some of its input/output pins are dedicated to the terminal, high-speed tape reader and other system functions, but there are still ten left over for user control. The mask programmed DEMON monitor is located in 1024 words of memory on this same chip. DEMON is allocated the top 1K of the first 32K of memory from 7000 to 73FF. It decodes the serial input from the terminal and controls the entire system operation with a minimum of added switches. . . . no control panel is needed.

Sixty-four words of RAM used as in-
(continued on page 66)

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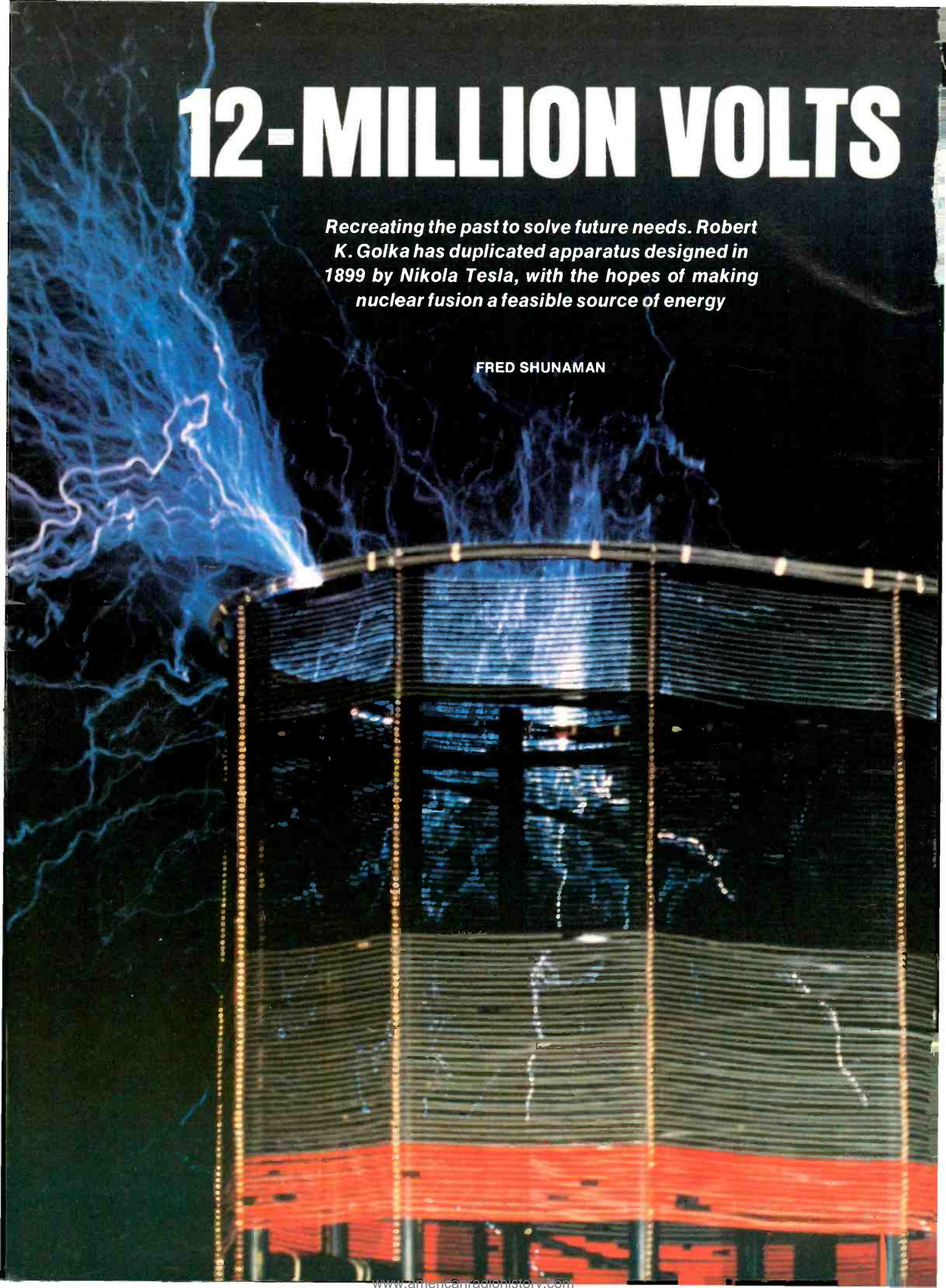
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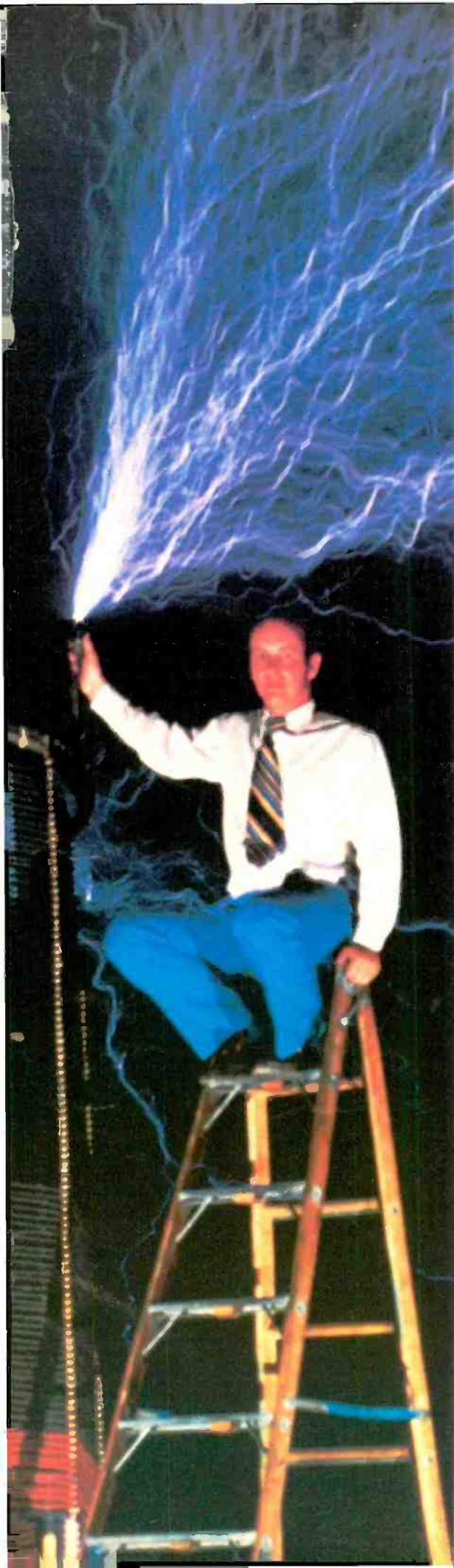
Circle 16 on reader service card

12-MILLION VOLTS

Recreating the past to solve future needs. Robert K. Golka has duplicated apparatus designed in 1899 by Nikola Tesla, with the hopes of making nuclear fusion a feasible source of energy

FRED SHUNAMAN





IN THE SUMMER OF 1899, NIKOLA TESLA, POSSIBLY THE world's greatest engineer, set up an experimental laboratory or station near Colorado Springs with the intention (he told curious reporters and residents) of "sending a telegram from Pike's Peak to Paris." It is highly possible that long-distance wireless communication was the main objective of his work there, but he was probably also interested in wireless power transmission.

Tesla used a radio-frequency transformer (Tesla coil) of unheard-of dimensions and power—at least 12-million volts were generated. He was not too communicative about his experiments—either their purposes or results—and visitors were not encouraged. (This may have been partly because of the dangerous nature of the work.) So exact details are lacking.

Today—nearly 80 years later—in an Air Force hangar at Wendover, Utah, that 12-million volt record has for the first time been equalled and possibly exceeded. The second man to generate 12-million volts is Robert K. Golka, of Golka Associates, Brockton, Massachusetts. And he is doing it with equipment designed to duplicate Tesla's as closely as possible. Mr. Golka has instituted what is now called Project Tesla to study one of the results of Tesla's experiments that the great scientist almost brushed off as an interesting but unimportant phenomenon.

The exact equipment Tesla used cannot be determined. Probably he made numerous changes, so conflicting reports may be correct for the situation at the time reported. All agree that the primary of the Tesla coil was of heavy copper wire (1½-inch thick) placed at the bottom of the secondary, which was 51 feet in diameter. The type of conductor used for the secondary and the number of turns is not quite clear, but all reports (and the photographs) agree that there was an addition to the secondary—a coil of 100 turns, 8-foot 3-inches in diameter, placed in the center of the larger coil. The main secondary appears to have had a natural resonance of about 50 kHz; the additional coil resonated at the second harmonic, 100 kHz.

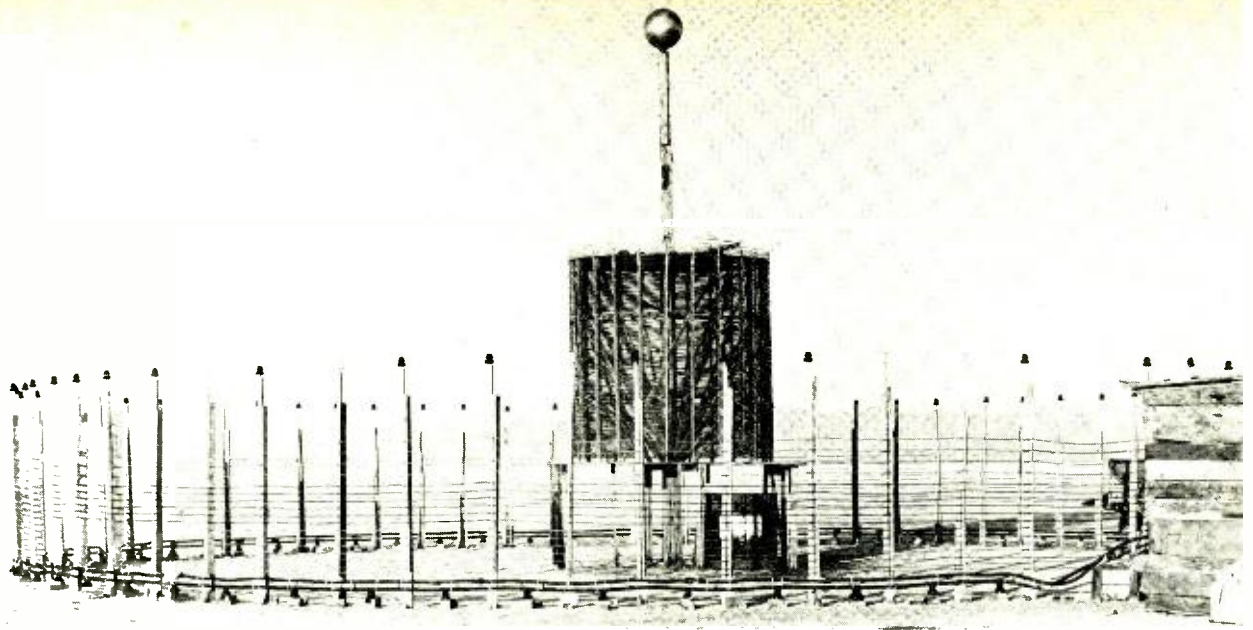
The input power was thought to be up to 50 kW, but when the coil was first energized, it blew out the generator of the Colorado Springs lighting and power system. (Tesla supervised the rebuilding). The blowout may of course have been due to a radio-frequency surge or kickback rather than to the amount of power drawn. (Of little consequence to the Colorado Springs lighting and power system.)

Two important by-products

Tesla made two important discoveries not connected with his original objective. He was an interested student of natural electricity, which the many thunderstorms of the region produced in vast abundance. He made special recording equipment to record their intensity and characteristics. These recordings gave him no room to doubt that he was observing standing waves in the earth. "Impossible as it seemed," he reported, "this planet, despite its vast extent, behaves like a conductor of limited dimensions. The tremendous significance of this fact in the transmission of energy in my system had already become quite clear to me. Not only was it possible to send telegraphic messages to any distance without wires, as I recognized long ago, but also to impress on the entire globe the faint modulation of the human voice. Far more significant is the ability to transmit power in unlimited amounts to almost any terrestrial distance and almost without loss."

To illustrate his point, Tesla lit a bank of 200 carbon-filament lamps—consuming about 10 kW—26 miles from the station, a feat that has not since been equalled. This experiment was duly witnessed and recorded by his assistant, Fritz Lowenstein, later to become a prominent electronic inventor in his own right.

(It is doubtful indeed, says Mr. Golka, that power could be sent completely around the world from one



THIS TESLA COIL created the highest voltage ever produced by mankind—12,500,000. Estimated peak current: 1,100 amps.

source, as Tesla envisioned. The resistance losses would far outweigh the power actually used. Some rocky soil has a resistance as high as 1,000 ohms per meter.)

Ball lightning

The second discovery was recorded almost as an aside by Tesla in his description of the electrical displays of the region: "Lightning discharges are, accordingly, very frequent and sometimes of inconceivable violence. . . . Many of them resembled gigantic trunks of trees with the trunks up or down. I never saw fire balls, but as a compensation for my disappointment I succeeded later in determining their mode of formation and in producing them artificially."

Fire balls, or ball lightning, have long been a puzzle to scientists. Many of the scientists have simply denied their existence (as a simple solution to a problem that appeared to have no reasonable answers). They are glowing balls apparently of electrical plasma, a foot or less in diameter, floating a few feet off the ground. Their exact composition and mode of formation is not known. They appear in the wake of thunderstorms and move slowly, bouncing when they strike the earth or a solid object.

Despite earlier doubts, the existence of ball lightning was pretty well established by Niels Bohr, who saw a fireball and reported it. (Possibly lesser scientists have also seen ball lightning but have remained discreetly silent about it, like the sea captain who remained below eating his dinner when the deck crew reported a sea serpent. "I don't want to be called a liar all the rest of my life," he said.)

A few prominent physicists have speculated and formed tentative theo-

ries about ball lightning. (Tesla was the first to try to develop a theoretical explanation.) But it was considered a special subject well away from the mainstream of scientific investigation.

All this changed with the coming of the nuclear age. Scientists have been struggling to contain and control the plasma of ionized and superheated gases resulting from the fission or fusion of nuclear materials. A constricting magnetic field in the shape of a large doughnut has been labored with for some years. Its latest name is the Tokamak, given by the Russians, meaning toroidal-confinement. In the earlier days it was known by other names! The Perhapsatron was an interesting name for an early magnetic confinement device. The Theta-Pinch and the Beta device were all variations of this idea.

Since every plasma behaves thermodynamically like a liquid, why not use surface tension to partly help in holding the plasma together? Of course other parameters will have to be exactly right for the effect to take place, but surface tension plays a predominant part, just as in the production of soap bubbles using a soapy liquid.

The various theories about ball lightning agree that it must be a plasma—a ball of ionized air or other gases. Yet it is self-contained and does show evidence of surface tension—bouncing off objects it strikes and regaining its spherical form. True, it is far from permanent, lasting about five seconds on the average—though observers have reported fire balls with a life of minutes.

Ball lightning then, might serve as a model for controlled fusion or at the very least a study of it might produce new knowledge that would be helpful in obtaining controlled fusion. But the problem of observing natural ball light-

ning is insurmountable. It is much more common in some areas (notably parts of Sweden and Australia) than others, but nowhere does it occur often enough (or long enough) for study.

The lightning maker

Robert K. Golka became interested in the subject when he read—in O'Neill's *Prodigal Genius*—that Tesla, though he had never seen natural ball lightning, had produced it artificially during his Colorado Springs experiments. Contacting Leland Anderson, long-time Tesla student and historian, he was told that little information was available, but there might be more in Tesla's notebooks in the Tesla Museum in Beograd, Yugoslavia.

After playing with the idea for a year, Golka went to Yugoslavia and was able to get permission to read the Colorado Springs diary. (Fortunately, Tesla wrote his notebooks in English, but Golka reports that the handwriting was such that reading the notebook was almost like translating from a foreign language.) A little experimenting with Tesla coils convinced Golka that he was on the right track, but that a much bigger coil than anything he could construct would be required. What was necessary, Golka believed, is the following.

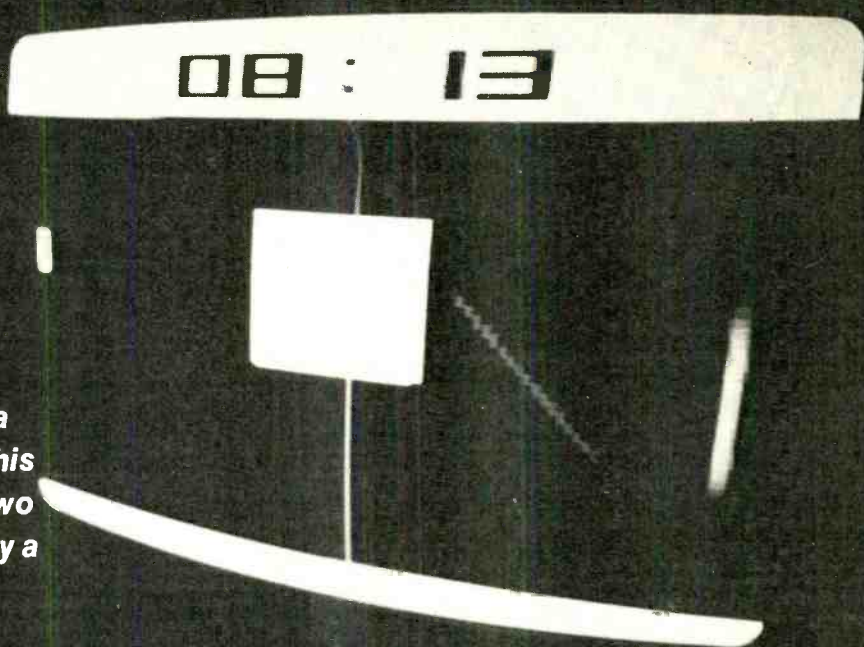
1. A generator of moderately low frequency and with enough power to be able to excite certain areas of land with standing waves.
2. Land area where electrical reflections can be set up (due to ground faults or other causes) to support standing wave phenomena.
3. High-intensity electrical discharges in which the plasma "ball" can be formed in-channel and disassociated from the discharge

(continued on page 69)

Build This Great TV Game

With on-screen digital scoring and a unique alternate "bumper" game, this ping-pong game can be played by two or four people, or it can be set to play a perfect game against you or itself.

RAY PICHULO



HERE'S ONE OF THE MOST FASCINATING AND exciting electronic projects I've ever seen. A home-built electronic ping pong game that includes a special alternate version called "bumper" (illustrated on this month's cover). The game easily connects to most TV sets and uses the TV screen as the playing field. This particular game offers a challenge for just about every level of playing skill. Here are some of the features built into this special 2-game unit.

- Both vertical and horizontal paddle movement control.
- Controlled ball motion—slam, spin or lob.
- Computer paddle control (one person can play against a machine that plays a perfect game or the machine can play against itself).
- Sound effects when the paddle hits the ball and when the ball rebounds off the game boundaries. Plus a special sound when a player scores a point.
- Randomized ball-speed ball-angle integrator.
- Displayed boundaries.
- Paddle size controls.
- On-screen scoring option.
- BUMPER—a second, built-in game.

How to play the game

The combination of vertical and horizontal paddle motion adds an extra dimension to the play. With it you can "rush the net" for a well-played power shot. Or you can chase after the ball to hit an over-the-head return. You can also try for a shot with lots of spin and angle. Or you can send a lob shot in and challenge your opponent to try and recover from that one.

The ball control built into the electronic is a unique randomizing integrator circuit

that controls both ball angle and speed. When you hit the ball, it can rebound at any one of ten different combinations of ball speed and ball angle; including straight across, either as a fast "smash" or a slow "lob".

The steeper rebound angles can make the ball bounce once, twice or even three times off the top and bottom boundaries before your opponent can try and return the ball.

The built-in computer-control circuit provides automatic feedback to one (or both) paddles. This makes it possible for a single player to match his skills against the game. When this feature is switched on, the computer-controlled paddle automatically chases after the ball and bats it back to you . . . and it never misses.

This special feature also makes the game a cinch to demonstrate as it can be set to play a perfect game against itself.

The sound effects built into the unit add to the excitement and enhance the realism. Whenever the ball hits a paddle or boundary, you hear a "bonk"; and when some-

one misses a shot the game produces a "brrappt".

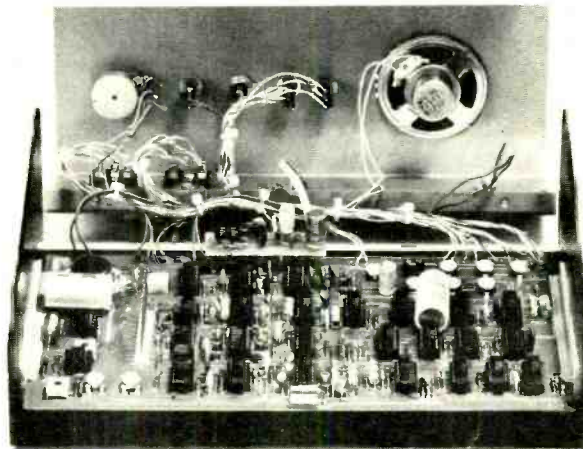
The ability to adjust the paddle size over a 3 to 1 range adds an adjustable skill level. The better you get as a player, the smaller you make the paddles; increasing the skill needed to play.

When you add on the digital scoring feature, you get a visible display on the TV screen. It is updated each time there is a score and the game ends automatically when either player reaches a score of 18. A reset button sets both players scores back at zero, and you're ready to start again.

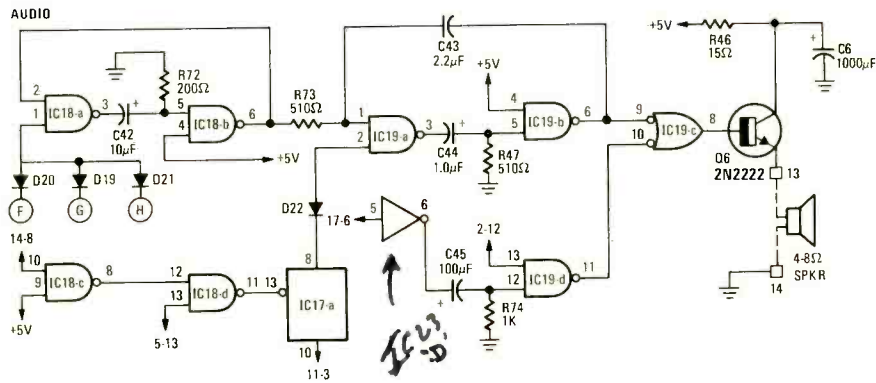
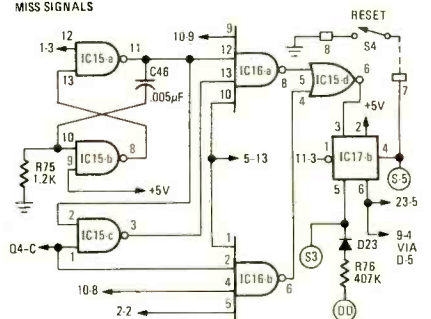
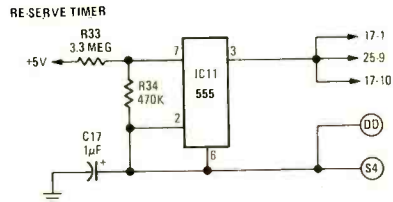
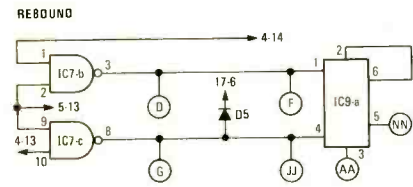
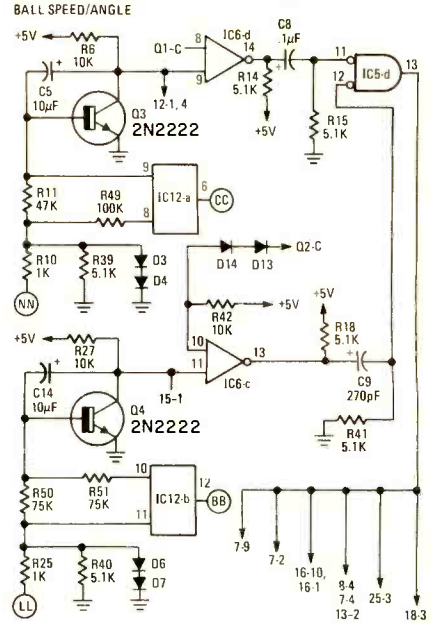
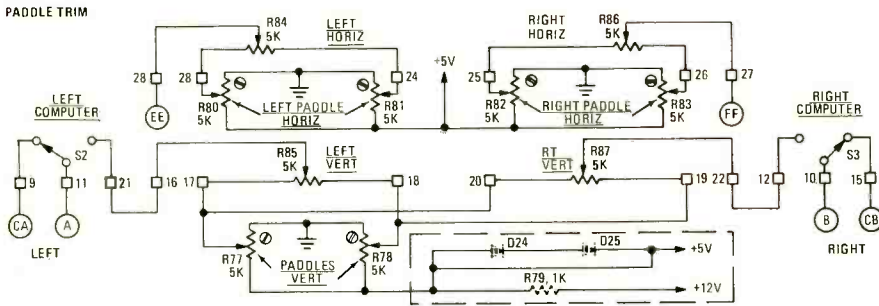
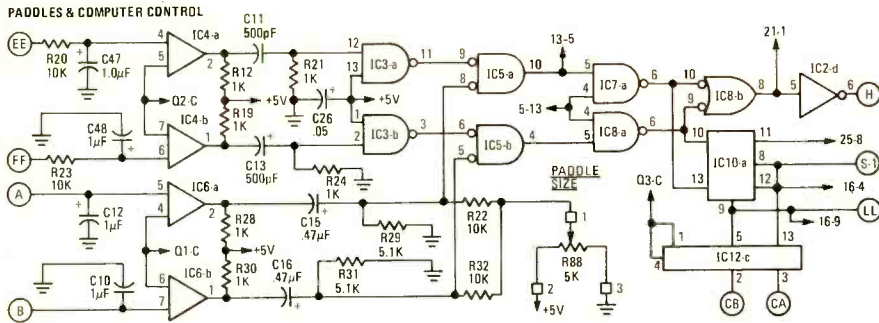
A second game

Bumper, as shown on this month's cover, adds a white "bumper" cube in the middle of the screen. This bumper adds two intriguing challenges to the game. When a player hits a ball that strikes the bumper on one of its vertical sides, the ball rebounds back to him at a random angle

*(Schematic on pages 36 & 37)
(text continues on page 79)*



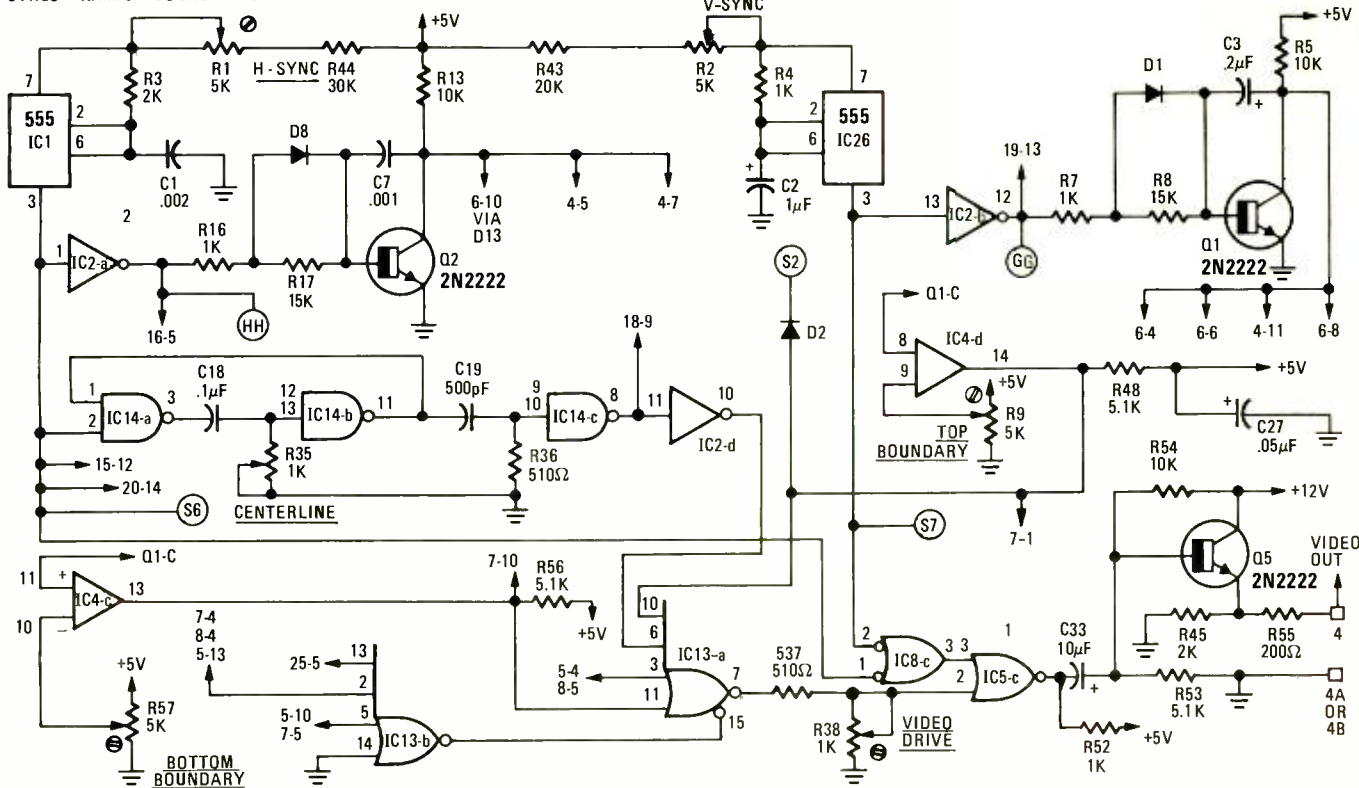
THE TV GAME is built on a single PC board. The optional scoring board (not shown) mounts on top of the main board.



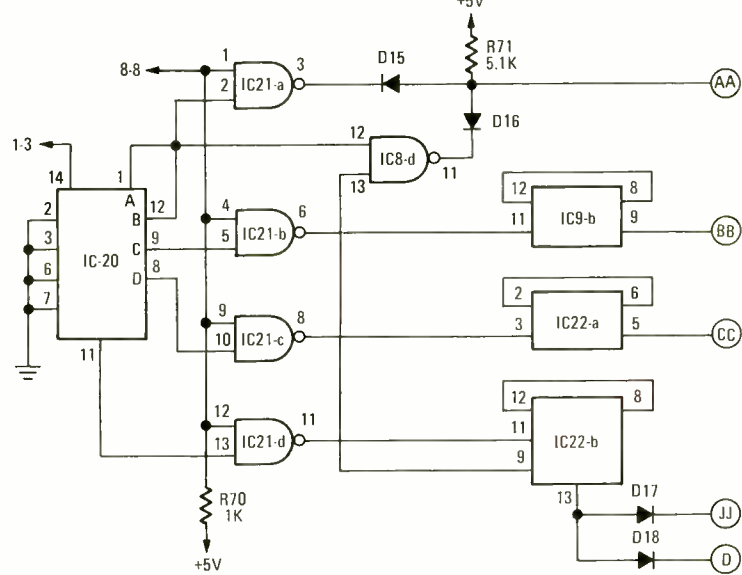
- NOTES:**
1. LETTERS WITHIN A CIRCLE INDICATE INTERCONNECTIONS BETWEEN TWO OR MORE SIMILARLY-MARKED POINTS. FOR EXAMPLE, (AA) AND (AA) ARE CONNECTED TOGETHER ON THE CIRCUIT BOARD.
 2. POINTS MARKED BY TWO NUMBERS SEPARATED BY A DASH (AS 16-9) INDICATE AN IC NUMBER AND PIN NUMBER. THUS A LEAD MARKED 6-8 CONNECTS TO TERMINAL 8 ON IC6.
 3. THE LETTER "S" FOLLOWED BY A NUMBER INDICATES A CONNECTION TO THE OPTIONAL SCORING BOARD.
 4. NUMBERS NEXT TO SQUARES AS □ ARE CONNECTION TO OFF-BOARD COMPONENTS.
 5. CAPACITORS C20-24 AND C26-31 BYPASS V_{CC} AND ARE NOT SHOWN ON THE SCHEMATICS.
 6. IC1, IC11, IC26 - 555, IC2 - 7404, IC3, IC7, IC8, IC14, IC15, IC18, IC19 - 7400, IC4, IC6 - 339, IC5 - 7402, IC9, IC22 - 74C74, IC10, IC17 - 7474, IC12 - 4066, IC13 - 7423, IC16 - 7420, IC20 - 74C90, IC21 - 74C00, IC23, IC24 - 74C04, IC25 - 74C10, Q1 - Q6 - 2N2222, D1 - D8 - 1N4148, D9 - D12 - DELETED, D13 - D25 - 1N4148 - SEE PARTS LIST

THE COMPLETE SCHEMATIC of the TV Game, minus the scoring option, is shown divided into the various functional sections. The circuit is built around the readily available 74-series IC's.

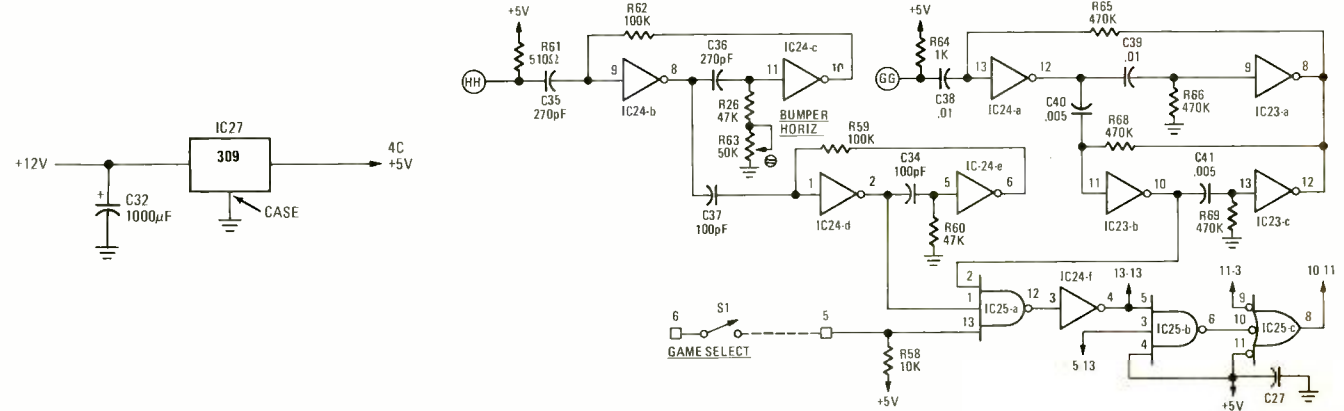
SYNCS - RAMPS - BOUNDARIES - CENTERLINE - VIDEO CIRCUITS



RANDOMIZING INTEGRATOR

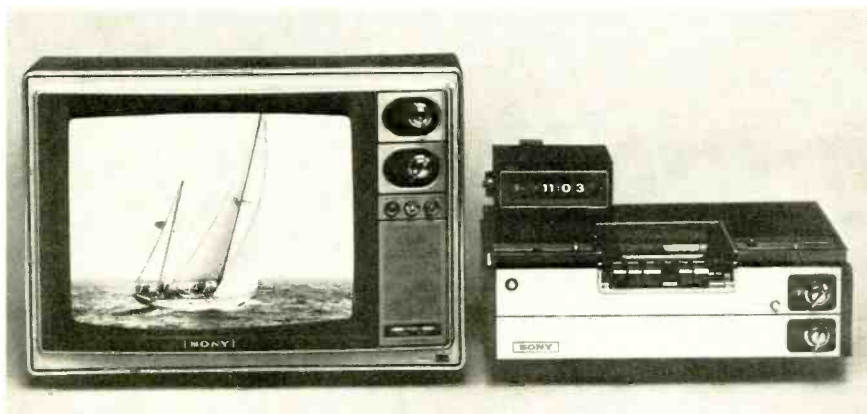


BUMPER



Videodisc- Videotape 1976

ROBERT E. GERSON



FOR THE HOME VIDEOPLAYER, THE DAY of true availability has been a long time coming. In fact, it took 14 years from the time the first home video playback gadget was demonstrated—a longitudinal-scan video tape recorder using ¼-inch tape developed in England by Westgrove—until Sony began marketing its home Betamax ½-inch cartridge VTR. The first Betamax units, combined in a console with 19-inch color receivers, became available late last fall. Betamax decks, designed to hook to the antenna terminals of standard television receivers, are just now appearing on the market.

But to many, the term videoplayer is synonymous with videodisc. To them the VTR, with its off-air and live-from-camera recording abilities, is more of a hobby than an entertainment medium. Nothing less than a play-only system, complete with an extensive library of low-cost special- and general-interest programming meets all the criteria needed to bring the "see what you want to see when you want to see it" concept to the mass market.

Even for the purists, the videoplayer era has come although on an admittedly small scale. Since early this year, RCA has been field-testing its capacitance disc system in consumer homes. About 200 of the RCA players are involved in the field-test intended to find

TAPE ECONOMY OF MAJOR VIDEO RECORDER SYSTEMS

System	Speed (IPS)	Tape Width (inches)	Square-feet per hour
ITT ¹	120	¼	18.8
Sony Betamax	1.57	½	20.6
RCA MagTape ²	1.53	¾	28.7
V-Cord	3.75	½	46.9
BASF LVR ¹	120	½	53.6
American Videonetics ²	2.88	¾	56.2
Akai	10	¼	62.5
Philips VCR	5.6	½	70.0
U-Matic	3.75	¾	70.3
EIA-Japan Type-I	7.5	½	93.8

¹Developmental, data subject to change.

²Development halted, future uncertain.

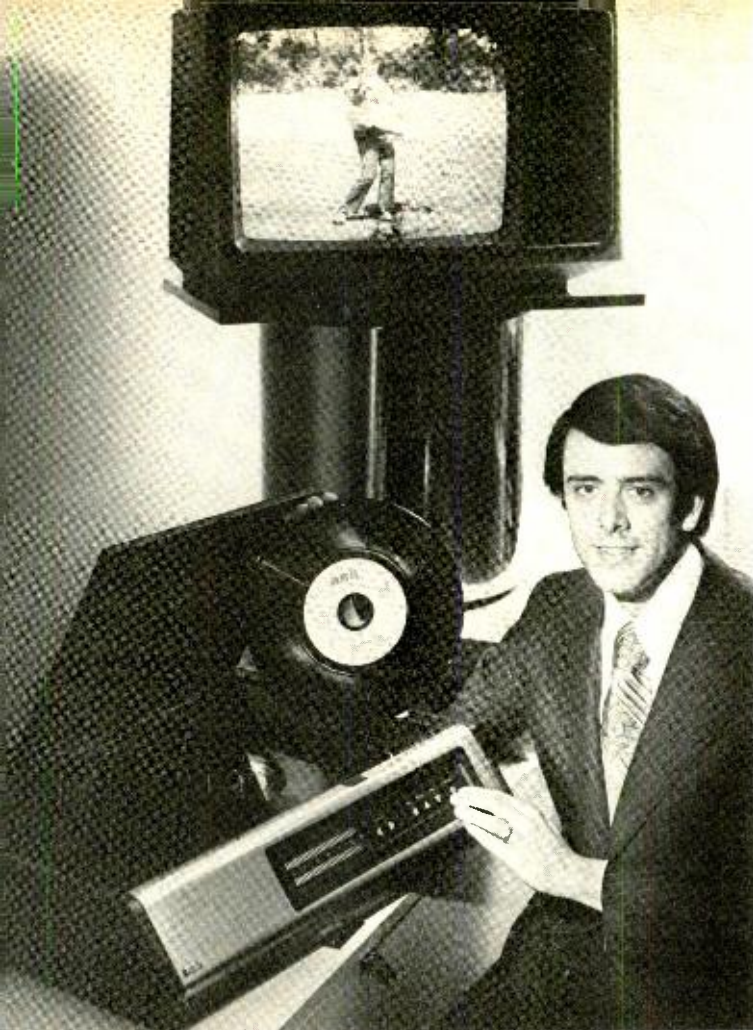
RECOMMENDED STANDARD FOR OPTICAL VIDEODISC SYSTEM*

VIDEO Modulation: FM of composite color video signal. **Blanking level reference:** 8 MHz ± 50 KHz. **Sync-tip to peak-white deviation:** 1.7 MHz ± 35 KHz.

AUDIO Modulation: FM, 2-channel. **Maximum deviation:** ± 100 KHz. **Carrier frequencies:** Left channel, approx. 2.3 MHz; right-channel, approx. 2.8 MHz. Both sound carriers are pulse-width modulated on FM video carrier.

DISC Rotation speed (for NTSC): 1,800 RPM. **Rotation:** counter-clockwise from objective lens side. **Center-hole diameter:** 35 mm. **Refractive index:** 1.5 (approx.). **Thickness:** rigid disc, 1.1 ± 0.1 mm; flexible disc, 0.2 ± 0.1 mm.

*Tentatively agreed to by MCA, Philips and Zenith.



It has been one year since our last report on the progress of commercial videodisc-videotape machines. Although the past year appears to have been static, it really wasn't. Here's a rundown on what has transpired

out how they stand up to in-home treatment. Here's a rundown on where the leading videodisc and home VTR systems stand today, and how they stack up for the future.

RCA SelectaVision

Apparently the closest to actual marketing in the U.S. is RCA's SelectaVision videodisc system, now in field tests and due for test marketing sometime in 1977. RCA's discs have a metallic layer between two plastic layers. Information, recorded in the form of grooves on the plastic, is read out by a sapphire stylus equipped with a metal electrode that measures, by capacitance, the distance from the stylus tip to the metal layer.

Since our last videodisc report (**Radio-Electronics**, June 1975), RCA has raised its estimate of the player's final price from \$400 to "under \$500." Most other specifications are unchanged: 12-inch disc revolving at 450 RPM. Information is recorded on two sides with a combined 60-minute play time. A full-hour program is to retail for about \$10.

Informed sources indicate RCA has invested close to \$100 million in its videodisc effort so far, with a good chunk of that going into programming and disc manufacture. RCA has spent in excess of \$2 million on the initial

equipping of a former audio factory in Indianapolis with disc coating, molding and inspection machinery. Additional millions have been earmarked for program acquisition—RCA says it already has rights to over 1,000 titles.

RCA's progress, and the relative simplicity of its system, has attracted the interest of the Japanese. Six manufacturers there (Clarion, General, Nippon Electric, Pioneer, Toshiba and Sharp) have all taken technology licenses from RCA. This doesn't, however, mean they have made a commitment. The licenses are free until the companies actually make and sell hardware or software.

MCA-Philips-Zenith

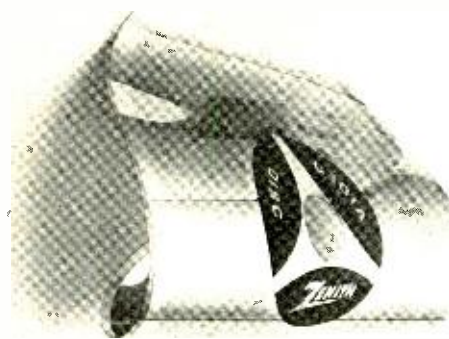
The progress of the laser-read optical videodisc system, being jointly developed by MCA in the U.S. and Philips in Holland, is currently the industry's big question mark. The problems of the MCA-Philips system are exactly the reverse of those faced by RCA. The disc production appears to be relatively simple, but the player, with its laser and servo-controlled optics, requires significant state-of-the-art advances in order to be rugged and inexpensive enough for the consumer market.

On the plus side, two announcements in the past year indicate that

work is proceeding on a schedule that may permit at least test marketing of a minimal number of units by late-1976, early-1977. One is a MCA-Philips-Zenith agreement on a proposal for a compatibility standard. The other is Philips' signing of a letter of intent to purchase several millions of dollars worth of low-cost lasers from Spectra Physics of California. The price of the laser and power supply would have to be in the \$20-\$30 range if the player is to be marketed at the targeted \$500 price, and that would require a 5-fold cut from current levels. Also an indication of progress is MCA's order of broadcast-quality VTR's to be used for disc mastering.

The MCA-Philips disc is reflective, so the laser and all the optics are on the same side of the disc. Until recently, Zenith had been working on a transmissive disc system where the laser shines right through the disc. So Zenith's participation in the standards agreement was something of a surprise. Officially, however, Zenith is fence sitting, saying only it's watching developments and that it won't choose a system to back until 1978. By that time, the market should be in the early development stages.

The MCA-Philips disc will be recorded on one side only though both could be used. Each side provides up to



ZENITH HAS DEMONSTRATED a flexible reflective laser-read disc system. The use of flexible thin discs is supported by MCA which envisions duplicating them on a web-type printing press.

30 minutes of playing time. Disc pricing should be about the same as RCA. Current plans call for MCA to turn out the software. Magnavox, Philips' U.S. subsidiary, will produce the players. MCA and Philips are setting up a corporation to offer patent licenses to other hardware and software producers.

Thomson-CSF

Zenith's former partner in the development of a transmissive optical videodisc, France's Thomson-CSF, says it's sticking to its guns and will produce and market a handful of players later this year for sale in educational and commercial markets. The major claimed advantage of the transmissive disc is that, by changing the focus of the laser, both sides can be played without the disc being turned over. No price has been quoted, but it's expected to be several times higher than that planned for the RCA or MCA-Philips players.

TeD

The first videodisc player available to consumers is the TeD, a mechanical system jointly developed by England's Decca and Telefunken of Germany. The first units were introduced in Europe in spring 1975, with players priced at \$600 and discs, with 10-minute playing times, priced from \$2 each. The initial offering of some 5,000 players met with public indifference. TeD's lack of success has been blamed on short disc playing time, high player price and poor economic conditions. Whatever the reasons, TeD has lost momentum, and is being written off as a factor by many in the industry. Sanyo, TeD's Japanese licensee, has twice cancelled production plans and is mum on its intentions for the future.

Sony

The first real home video recording system introduced by a major manufacturer is the Sony Betamax 1/2-inch cartridge recorder. It's currently available in combination with a 19-inch color receiver at \$2,295. It is also available in deck form, complete with tuner and timer (but no camera input), at \$1,300. A black-and-white camera accessory for the console combination and for future deck models, is planned at about \$400. Maximum playing time is 60 minutes (cartridge cost \$15.95), but that may be extended by 30 minutes in the near future. Sony is also working on a cartridge changer to provide up to 6 hours of record or play time.

Betamax units are hard to find, most being snapped up by commercial VTR users as substitutes for more expensive 3/4-inch cartridge U-Matic machines. The scarcity should be alleviated soon. Sony is now turning out Betamax units at a 10,000 monthly rate, and will expand to 20,000 monthly next year, and by 1977 other manufacturers should have compatible machines on the market. There's also a good chance prices will drop. In Japan, Sony sells a "no-frills" Betamax deck at about \$760.

BASF LVR

The moment of decision is arriving for the future of BASF's LVR (Longitudinal Video Recorder) system. The LVR has 28 tracks on a 1/2-inch cartridge tape. The tape speeds past the head at 120 IPS, reversing at the end of each pass. BASF is currently reviewing the success potential of its system.

IIT

Working at IIT (Illinois Institute of Technology), magnetic recording pioneer Marvin Camras has developed a



RCA'S SELECTAVISION VIDEODISCS will have handling slots as well as a center hole. The slots permit easier disc handling, thus making it easier to keep fingerprints off the disc surface.

longitudinal VTR system similar in many respects, including tape speed, to the BASF LVR. The IIT unit, however, has 40 tracks and uses an endless loop of 1/4-inch tape. IIT says a color VTR could be made to sell for \$300, and that a 30 minute tape cartridge would retail for less than \$10. There are no current production plans.

V-Cord

Basically a modification of the EIA-Japan 1/2-inch VTR standard, the V-cord cartridge system was developed in a joint effort by Japan's Toshiba and Sanyo. Its advantage is half-speed operation, which provides tape economy. Late last fall both companies began offering decks, in limited quantities, at \$860. Neither has announced plans to export units to the U.S.

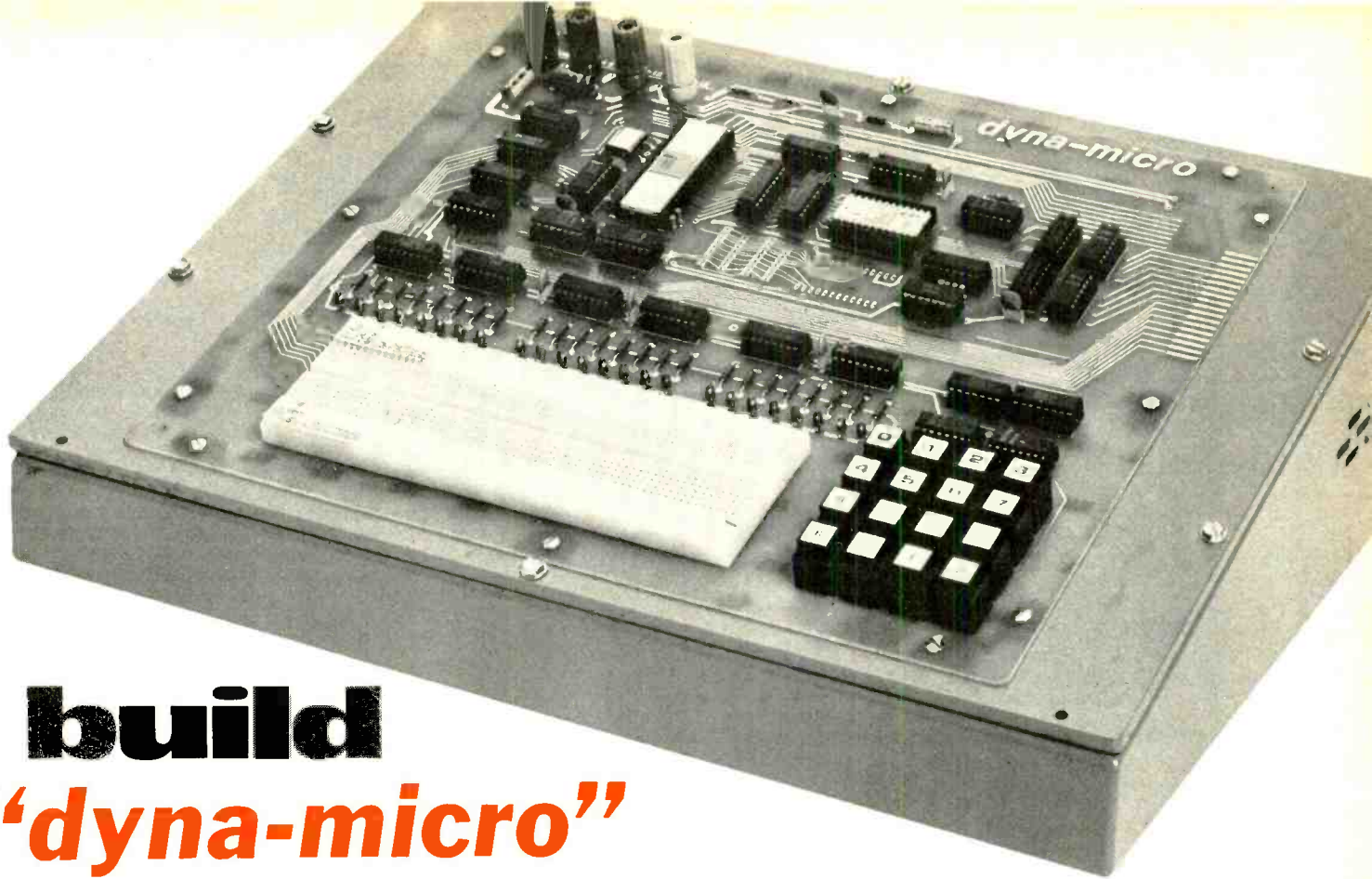
Matsushita

Still another 1/2-inch VTR format is being test marketed in Japan. This one, called National Home Video, uses a cassette. The VTR deck is being sold for \$765, with 60-minute tapes priced at \$18.50. Sales are limited to one of Japan's smaller islands, and the future of this system is uncertain.

Other systems

The past year has taken its toll of systems that once appeared to hold promise. RCA has shelved its 3/4-inch cartridge SelectaVision MagTape system to clear the way for its work on the videodisc. American Videonetics' work on a slow-speed 3/4-inch VTR has been halted by its new parent, Japan's Omron. Not a word has been heard from i/o Metrics since its February 1975 demonstration of a laser-read photographic film system. Of course

(continued on page 88)



build “dyna-micro” an 8080 microcomputer

Complete with keyboard for data entry, LED readout of the address and data, breadboard socket for experimenting, 500-bytes of PROM, 500-bytes of RAM, expandable to 65K and self-contained power supply

JOHN TITUS

LAST MONTH, PART-1 OF THIS ARTICLE described the operation of the Dyna-Micro and presented the schematic diagram and construction details.

This month, the foil patterns and component placement diagram are presented along with a description of how to use the Dyna-Micro.

Final check

All integrated circuits should now be in place, hopefully in sockets. Remove the 8080A IC and check for the correct voltages at its socket. You should find +5 volts at pin 20, +12 volts at pin 28 and -5 volts at pin 11. You should also check the PROM for -9 volts at pins 16 and 24. A PROM must be in one of the sockets for the -9 volts to be present.

Turn on the power with all the IC's in place and check the power supply voltages. They should be at their pre-set levels of +5 and ±12 volts. If these are correct, your Dyna-Micro system should be operational.

Depress the R key. The LED displays should now indicate 003 (0000011) at the HI and 000 (00000000) at the LO. The OUTPUT PORT 2 LED's may have some random data present. If this doesn't happen, remove the power and carefully check your system. Things to check for are solder bridges, cold solder-joints, unsoldered IC pins and incorrect IC orientation. Plated through holes don't have to be soldered unless there is a component or other lead going through them. Also check for +5 volts and ground at all the IC's.

If the LED's display the correct pattern, depress and release the s key.

Each time that this key is pressed, the LO address information should be incremented by 1. If this doesn't happen, check the keyboard encoder section and the I/O sections.

If the LED's are operating correctly, enter some data (0 through 7) from the keyboard. The binary codes for these keys will be entered in the Data-Register (OUTPUT PORT 2) display in the three least-significant bits. You will note that as new data is entered, the old data is shifted to the left where it finally disappears as more new data is entered. The actual operation of the KEX software to input and output data will be discussed later.

How to use the Dyna-Micro

The Keyboard Executive software is the “heart” of the Dyna-Micro system. It allows you to examine data or pro-

PARTS LIST

R1, R2, R4, R5, R6—1000 ohms,
 ¼ W, 10%
 R3—2200 ohms, ¼ W, 10%
 R7-R30—220 ohms, ¼ W, 10%
 C1—33 µF/6.3V electrolytic
 C2—5 µF/50V electrolytic
 C3, C5-C14—0.01 µF disc ceramic
 C4—3.3 µF/16V electrolytic
 D1-D24—Small red LED (Hewlett-Packard
 5082-4484, Monsanto MV5075B, or
 equal.)
 D25—1N751A, 5.1V Zener
 D26—1N746, 3.3V Zener
 IC1, IC22, IC23—SN7404 Hex inverter
 IC2, IC3, IC30—SN7400 Quad 2-input
 NAND gate
 IC4—SN74174—Quad type-D flip-flop
 IC5—8224 Clock generator (Intel)
 IC6, IC7—8216 Bus driver (Intel)
 IC8—8080A CPU (Intel) (Must be "A"
 version)
 IC9, IC10—8111-2 RAM memory (Intel)

IC13, IC17—SN74LS05 Open-collector
 hex inverter
 IC14—SN74LS155 Dual 2-to-4 line
 decoder
 IC15—1702A PROM memory (Intel)
 IC18—SN74L42 BCD to decimal converter
 IC19—SN7402 Quad 2-input NOR gate
 IC20, IC21—SN74L04 Hex inverter
 IC24-IC29—SN7475 Bistable latch
 IC31—DM8095 or SN74365 Buffer
 IC32, IC33—SN74148 8-to-3 line priority
 encoder
 S1-S16—Keyswitches with legends
 XTAL—6.750 MHz crystal, HC-18/U holder
 Solderless breadboard—SK-10 IF18
 Chassis—10" x 12" x 3" (Bud type
 AC-413)
 Misc.—Binding posts, IC sockets,
 hardware
Optional IC's for expanded memory
 IC11, IC12—8111-2 RAM memory
 IC16—1702A PROM memory

Keyswitches are available from Solid
 State Systems, Inc., P.O. Box 617, Colum-
 bia, MO 65201. Order type LM or LFW-LT,
 with legends shown in Fig. 7.

Breadboarding socket is available

from Circuit Design, Inc., Box 24, Shel-
 ton, CT 06484.

The following kits are available from
 Circuit Design, Inc., Box 24, Shelton, CT
 06484. Phone 203-735-8774. All kits, ex-

cept MMD-1IC, MMD-1 PROM, and MMD-
 1 RAM come complete with construction
 details, experiments, and tutorial ma-
 terial.

#MMD-1CBK—Etched, plated-through
 PC board, keyboard parts and bread-
 boarding socket. \$125 postpaid.

#MMD-1K—Complete kit of parts includ-
 ing 1702A PROM preprogrammed with
 KEX software and power supply. \$350
 postpaid.

#MMD-1A—Completely assembled and
 tested system. \$500 postpaid

#MMD-1IC—Microprocessor IC set in-
 cludes one 8080A CPU, one 8224
 clock generator, two 8216 bus drivers,
 two 8111-2 RAM memory, one 1702A
 PROM preprogrammed with KEX. \$100
 postpaid.

#MMD-1 PROM—Additional 256-word
 PROM (1702A). \$40 postpaid.

#MMD-1 RAM—Additional 256 words of
 RAM (8111-2). \$15 postpaid.

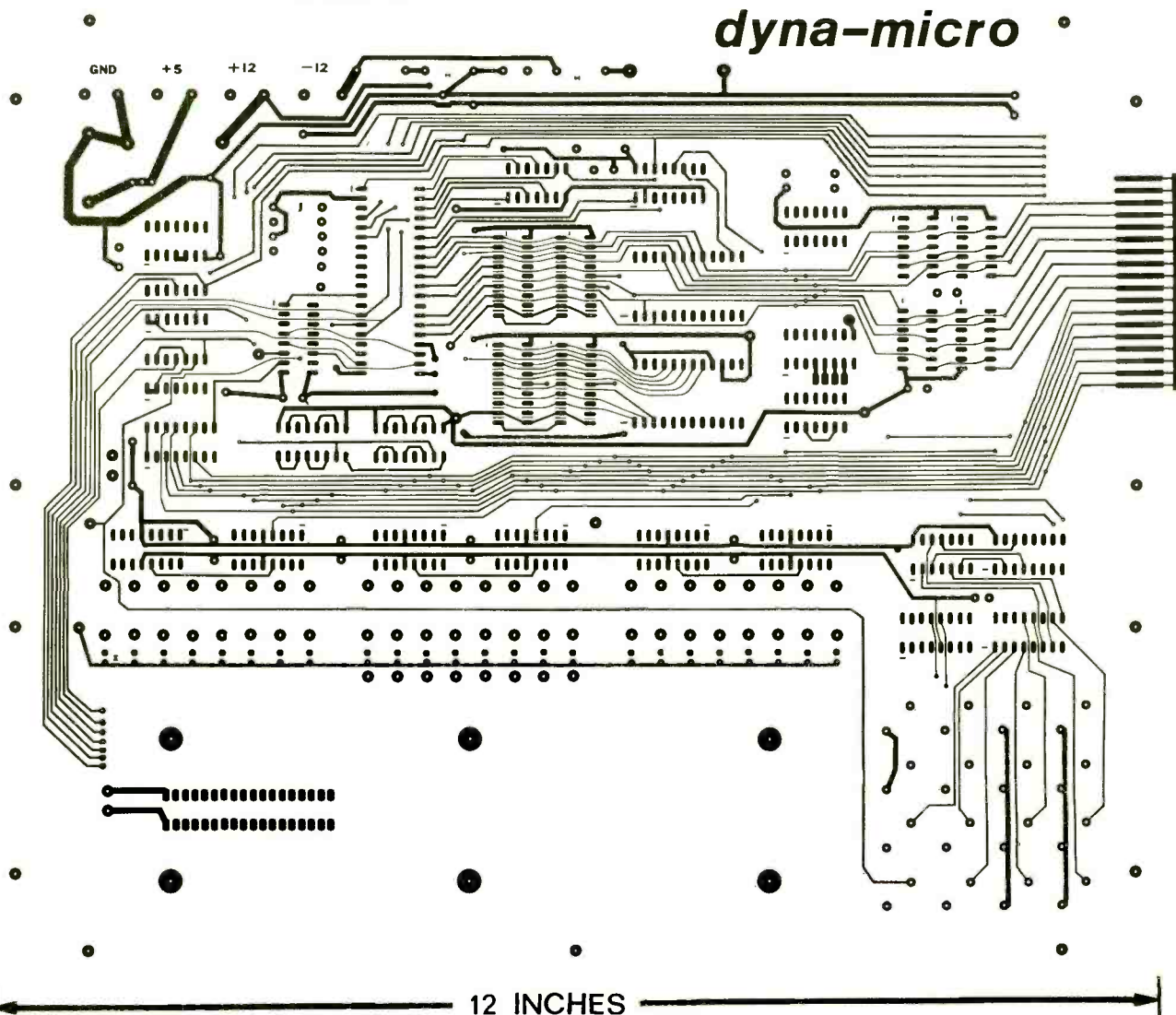


FIG. 3—FOIL PATTERN of the component-side of the double-sided board. The actual board
 measures 10 x 12 inches (254 x 305 mm.)

gram steps and to change data or program steps stored in the R/W (read/write) portion of the memory. We can also specify any address and start the program there.

The data keyswitches are labeled 0-7. When any one of these keys are depressed, data is entered in the corresponding octal format. The H key designates the HI address and the L key designates the LO address. The G represents Go and S represents See and Store. Three keys are not used by the KEX—A, B and C. The R key will always reset the computer and restart the KEX program. All manual data entry is through the keyboard in the basic Dyna-Micro system.

Whenever you want to start the system, depress keyswitch R. This will reset the KEX program and address the first location in the R/W section of the memory. This is HI=003 and LO=000. If you will only be using 256 words of R/W memory to get started, it must be in the locations allocated for IC9 and IC10. The KEX will not function without R/W memory.

To enter data, whether it will be used for new data or to address a memory location, simply depress the numbered keys as you would on a calculator. Data will be entered into the three least-significant right-most) LED's and it will shift to the left as more data is entered. If a mistake is made, simply re-enter the data. Mistakes are shifted out and lost. The data-register LED's will display the data just entered from the keyboard and this may be used as the HI address by depressing H, or it may be used as the LO address by depressing L. These keys will transfer the data to the proper LED display register and it will be used by the 8080A to address a new memory location.

Whenever a new HI or LO address is specified by depressing either the H or L keys, the KEX program will always display the contents of the specified memory location on the data-register LED's. To examine the contents in the next location, depress the S key. By depressing the S key again and again, we can examine the contents in sequential memory locations. It should be noted

that this S function follows increasing memory locations, *not* the sequential flow of a program.

To change the contents in a R/W memory location, simply load the address using the data input keys and the H and L keys. The old data presently in the location will immediately appear on the data-register LED's. Enter the new data into the data register using the numeric keys and then enter it into the R/W location by depressing the S key. After S is depressed, the new data is stored and the address is automatically incremented by one to address the next memory location. The data from the next location is now displayed on the data-register LED's.

The S key has two functions, both See and Store. How can we tell the difference? If the data has changed we will store it and see the next location. If the data hasn't changed, it will be stored in the same location that it originally came from and then the contents from the next memory location will be displayed. When we store old data back to the same location, we can't really see

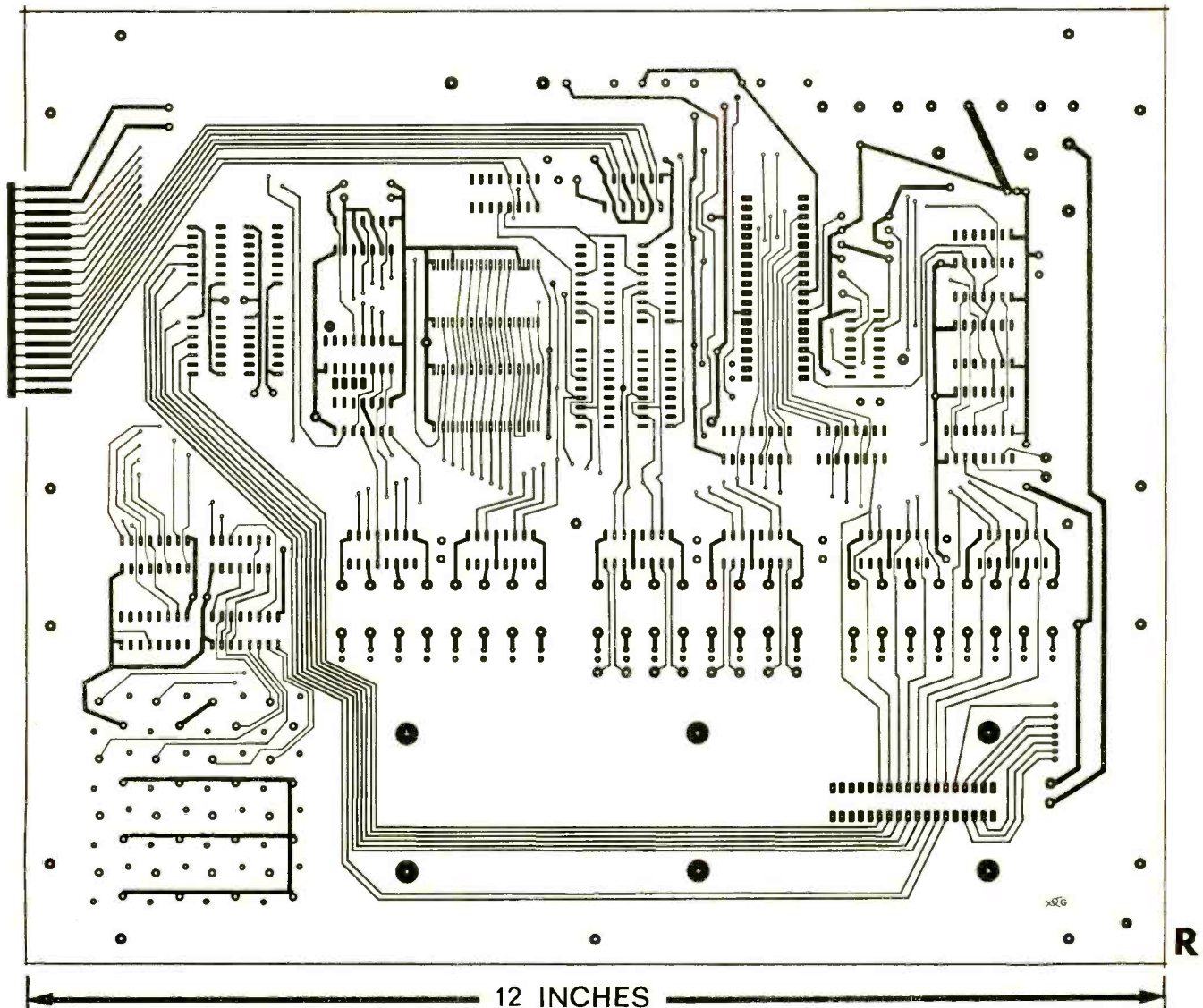


FIG. 4—FOIL PATTERN of the bottom of the double-sided board. A board with plated-through holes is recommended.

R

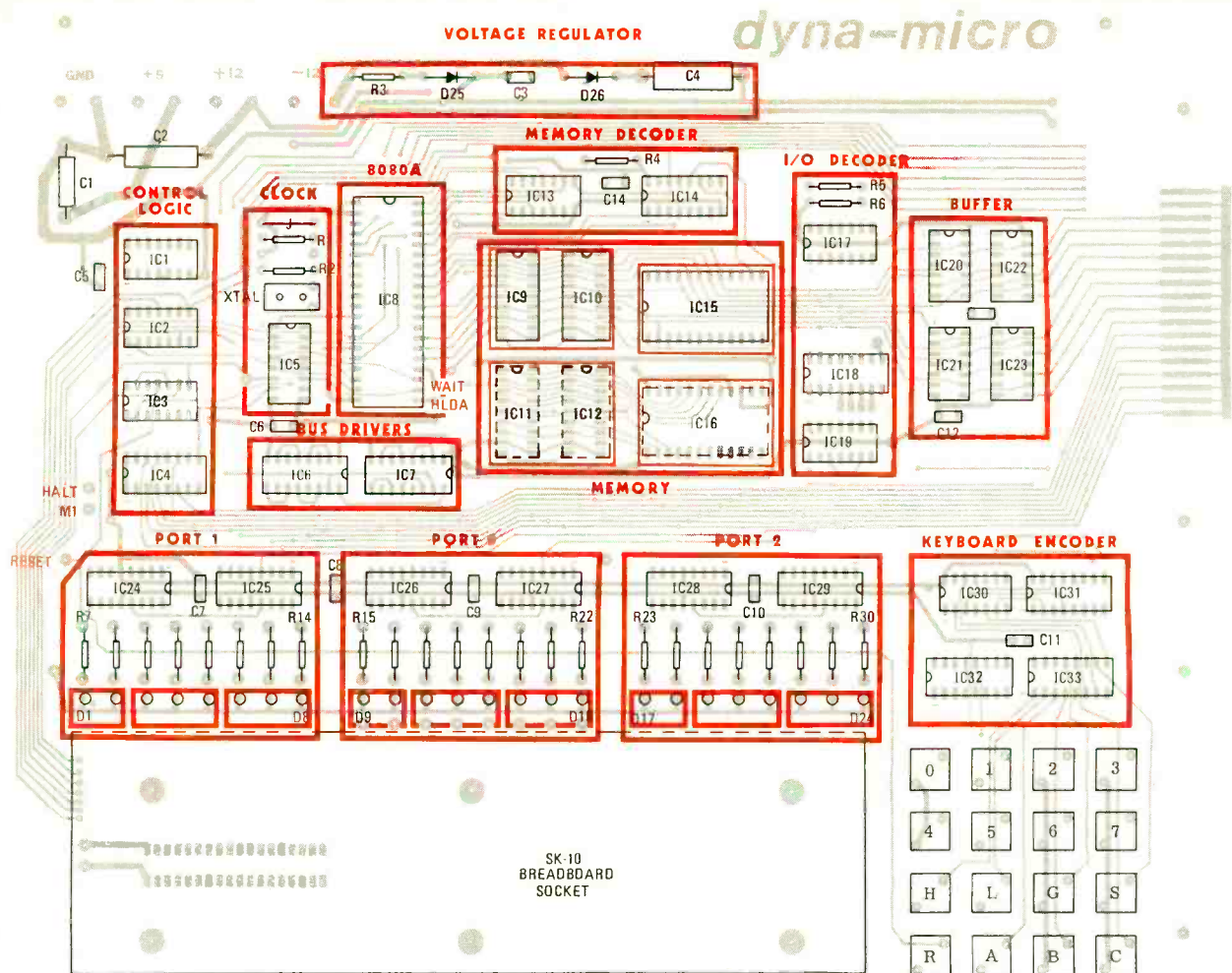


FIG. 5—COMPONENT PLACEMENT diagram. The board is shown divided into functional sections.

any change, but this is exactly what the KEX does. It displays data from a specific location, allows us to make changes and then puts it back. If no changes are made, the old data is restored to its memory location.

Once a program is entered into the computer through the keyboard, we can start it by loading our starting address and actuating the G key. This will transfer control from the KEX software to the program that we want to run. Starting addresses are loaded in the same way as previously described. Starting addresses don't have to be in R/W memory, but can just as easily be in PROM.

If your program starts at the first location in R/W memory (003 000) you can simply depress R followed by G. We can do this because KEX always resets the address back to this first R/W location.

Keys labeled A, B and C are not used by the KEX program. It should be remembered that the three LED output ports and the keyboard are not hard-wired for use with the KEX program only. They are available for you to use

in your programs. All fifteen keys may be used in any way you like, using software.

TABLE 1—MEMORY ALLOCATION

HI	LO	
000	000	KEY PROM
000	377	
001	000	
001	377	OPTIONAL PROM
002	000	
002	377	OPTIONAL R/W MEMORY
003	000	
003	377	R/W MEMORY
004	000	
377	377	AVAILABLE FOR USER EXPANSION

How KEX operates

The keyboard Executive software is contained in a single 1702A type PROM in the location allocated for IC15. This contains all the necessary

software to operate the keyboard and the LED displays. This is our software controlled "front panel", since the keys and LED's perform functions determined by the KEX software.

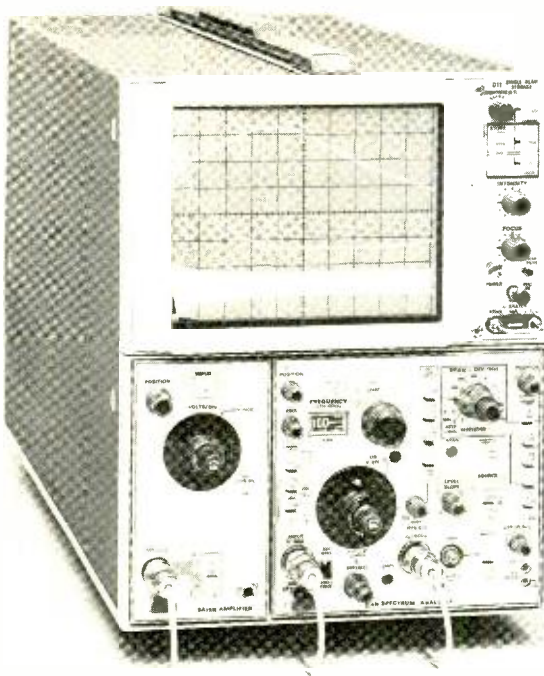
Whenever the R key is depressed, the 8080A CPU will start to execute the program that starts at location 0. Looking at the software listing for the KEX program (Table II), you will see that immediately after starting at location 0, the software instructions cause the computer to jump to location HI=000, LO=070 (HI=000 throughout the KEX program) where we start the program by pointing to the first R/W memory address (003 000.) The address and the data in that location are displayed on the three output ports. This is done between POINTA and POINTC in the program (see Table II). The software between POINTC and POINTD will do the necessary tasks to input new data from the keyboard and shift the data onto the LED's. The shifting is done inside the 8080A with software instructions. Doing this by hardware would require

(continued on page 84)

Testing HI-FI Gear

Measuring the performance of today's hi-fi gear requires state-of-the-art test equipment. Here's a rundown of the equipment and the measurements

LEN FELDMAN
CONTRIBUTING HI-FI EDITOR



TODAY'S HIGH-FIDELITY COMPONENT equipment has improved so radically in performance that the laboratory or service shop equipped with mediocre test and measuring equipment can no longer hope to measure some of the excellent specifications and features of the new audio amplifiers, tuners, record players and tape decks now available to audio enthusiasts. As recently as five years ago, an audio signal generator (a key component in any audio service shop or lab) having internally generated distortion of under 1% was considered to be a pretty good signal generator. Now, with high-powered audio amplifiers and even FM tuners boasting harmonic distortion ratings of tenths of a percent or even less, the use of such a generator for test purposes would hardly make sense. Furthermore, new measurement standards and requirements applicable to many types of components have become accepted, and these invariably require more and better test equipment than ever before. We recently compiled a list of equipment that one would need to test and measure everything from a record player to a power amp and divided the list into sub-groups needed for the various component categories. The function and purpose of each item will be described, along with some guide lines as to the minimum performance that one would expect from each piece of equipment in light of the high quality of today's hi-fi gear.

General equipment

Perhaps the most important piece of equipment you will need for checking

any hi-fi equipment is a good reliable oscilloscope. The scope is used to observe input signals, output signals, levels of distortion, hum components and more. Because we are dealing primarily with audio frequencies, the scope you choose need not have super-wideband response. A scope that is flat to 1 MHz or so will do nicely. By saving money in foregoing wideband response, you can concentrate instead on features such as dual-trace capability (which enables you to examine the outputs of two stereo channels at once, or the input and output of a single channel simultaneously, or even output plus a separate display of distortion), better triggering circuitry and more accurate calibration, plus greater vertical input sensitivity. Horizontal sweep circuitry should be accurately calibrated, too, so that the scope can be used to fairly accurately determine audio frequency.

Most hi-fi equipment used in this country is rated for operation from a 120-VAC 60-Hz power source. Unfortunately, power companies seldom deliver exactly that voltage to your wall outlet. A power amplifier connected

to a 110 volt power source may deliver considerably less audio power than its rating would indicate, so it is important to connect such equipment to a variable voltage transformer that can be adjusted to supply exactly 120 volts under all load conditions. An accurate AC voltmeter is a necessary adjunct to the variable voltage transformer and, if you are interested in measuring the power consumed by the unit-under-test, a direct-reading wattmeter is a worthwhile addition.

Two or more accurately calibrated AC VTVM's complete our list of general items needed in audio measurement work. Digital readout types are easier to read accurately, but if you choose digital AC VTVM's, make certain that their response is "flat" to at least 100 kHz and down to 10 Hz or so. The same frequency response requirement applies to conventional meter-type AC VTVM's.

Audio amplifiers

Figure 1 illustrates the major pieces of test equipment that would be required to measure some of the most important audio amplifier performance

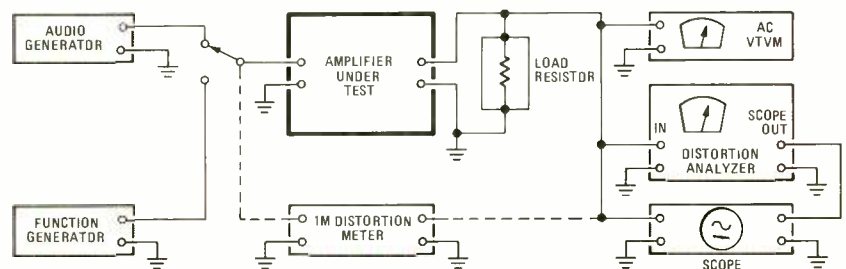


FIG. 1—TEST SETUP for measuring the performance of audio amplifiers.

specifications. The Audio Generator produces signals within and beyond the audio range. To keep pace with some of today's better audio amplifiers, its frequency range should extend at least 10 Hz to 100 kHz or even higher. More important, its own residual harmonic distortion content should be well below 0.1% and its maximum output should be in excess of 2 or 3 volts RMS. Its own frequency response should be considerably better than that of the amplifier being measured, preferably with no more than 0.1 dB amplitude variation over the audio spectrum. This generator will be used to deliver sinewaves to the amplifier for all frequency response measurements and harmonic distortion measurements.

The load resistor shown in the diagram, while perhaps the least expensive item in the overall test equipment setup, is a highly critical component. Ideally, it should be purely resistive (ordinary wirewound high-wattage resistors also have measurable inductance) and its wattage rating should be at least twice as great as the power rating of the most powerful amplifier to be measured. Resistance value should be within 1% of 8 ohms (the normal impedance at which power amplifiers are rated) and, if power measurements are to be made for 4-ohm operation, additional load resistors having that value should be used. Combinations of 8-ohm precision resistors are often connected in series or parallel for 4-ohm and 16-ohm loads, if required. To illustrate the importance of resistive accuracy, if an 8-ohm resistor were 5% on the high side and you were trying to measure 50 watts across such a load while unaware of the resistance error, you would increase output until the AC VTVM showed a reading of 20 volts RMS. (Power = $E^2/R = 20^2/8 = 400/8 = 50$ watts.) If, in fact, the load resistor were really 5% off, or 8.4 ohms in value, 20-volts developed across that resistor would really be equivalent to a power output of 47.6 watts. Accurate calibration of the AC VTVM is even more important for, if that instrument read 5% on the high side, a reading of 20 volts would really be equal to only 19 volts, and that would be equivalent to only 45.13 watts of power delivered by the amplifier.

A distortion analyzer is a device that, through the use of sharp filters, nulls out the fundamental frequency of the output signal of an amplifier under test and reads residual harmonics as a percentage of total signal. The filter nulling process can be slow and tedious, particularly if many repetitive harmonic distortion measurements are to be made. Many modern distortion analyzers are self-nulling and some automatically set the 100% reference point below which distortion is read.

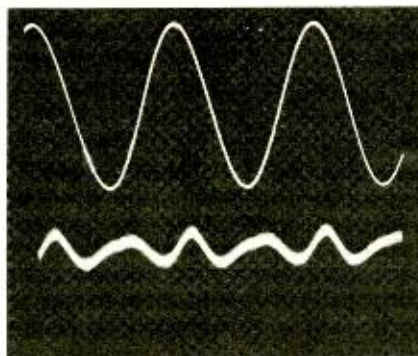


FIG. 2—DUAL-TRACE SCOPE permits simultaneous display of audio output signal and the distortion components via the distortion analyzer output.

Another form of distortion that is of interest in measuring audio equipment is intermodulation distortion. This form of distortion is produced by the addition or subtraction of two or more frequencies being processed by an amplifier, which yields sum and difference frequencies. An IM distortion meter supplies a low- and high-frequency input signal and also reads the sum and difference products produced at the output of the amplifier under test. It therefore substitutes for both the audio generator and the harmonic distortion analyzer when this test is made. The oscilloscope shown connected in parallel across the output of the amplifier serves to display the various output signals being measured.

The block diagram of Fig. 1 shows the setup for measuring the performance of a single channel of an amplifier. Since power output of audio amplifiers is measured with both channels operating, the output of the audio generator must be connected to both stereo inputs at once and loads must be connected to the output of each channel at all times. AC VTVM's are often used in pairs to monitor the signal coming out of the second channel, even if the other measuring instruments are across only one channel at a time.

The oscilloscope described earlier, as shown in Fig. 1, has one of its vertical inputs connected across the output while the other input is connected to a "scope output" terminal on the distur-

tion analyzer. This scope output presents a signal that is an amplified representation of the harmonic distortion components of the output signal and can be displayed on the scope as the second of its two available traces. Often, visual observation of the distortion components permits the technician to analyze the distortion components (e.g. third harmonic, but no second harmonic, etc.) by comparing the repetition rate of the observed waveform with that of the output signal displayed on the alternate trace. An example is shown in Fig. 2. A more precise method of harmonic distortion content evaluation involves the use of a spectrum analyzer.

FM tuner measurements

Figure 3 represents a test setup used to measure FM tuner (or the FM tuner section of a complete receiver) performance. For complete testing, two RF signal generators are required. One of these must be capable of being AM or FM modulated, while the other need not be modulated. Ideally, the primary generator should cover the range of frequencies from 10.7 MHz (the IF frequency of virtually all FM sets) to 216 MHz (twice the highest frequency in the U.S. FM frequency-band allocation). Frequencies above the FM range are needed to determine the unit's susceptibility to spurious signals. The matching network connected between the output of the generator and the antenna terminals of the receiver converts the signal from its output impedance (usually 50 ohms) to either 75 or 300 ohms, as required by the antenna input circuit of the receiver. Fixed filters must be inserted between the output of the unit under test and the various pieces of test equipment that we have already discussed. During most measurements, a band-pass filter having cutoff points at 200 Hz and 15 kHz is used, but for some measurements such as residual hum, the filter must be changed to a 15 kHz low-pass filter while for other measurements (such as residual sub-carrier output during stereo reception, and SCA rejection capability), a 200 Hz high-pass filter is

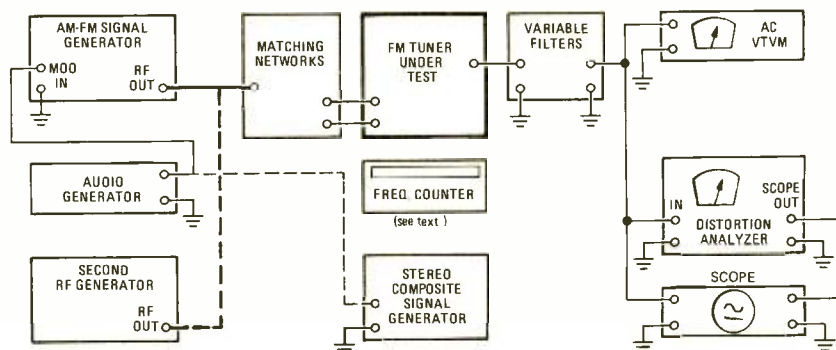


FIG. 3—TEST SETUP for measuring FM performance.

required. For this reason, many labs and shops prefer to use a variable all purpose filter that has adjustable cutoff points to meet the needs of a particular test.

Although the AM-FM generator may have a reasonably accurate frequency calibration, certain tests that use two generators require that the frequency difference between them be very precisely set. Accordingly, an accurate frequency counter capable of reading to above 108 MHz is useful and necessary if accurate results are to be obtained. Assuming both generators are stable after initial warmup, the counter need only be used to set frequency and should be disconnected when actual test measurements are made so that it will not load down the output of either generator and upset the calibrated attenuators. At least one of the generators should be capable of delivering output levels from a fraction of a microvolt to a volt or more, and if such high-level outputs are not possible, wideband or tuned RF amplifiers may be required to increase output range.

Many available FM signal generators are now equipped with internal audio generators, but these usually supply only a few frequencies for modulating the carrier. Since new FM tests involve measurements at audio frequencies from 30 Hz to 15,000 Hz, a separate audio generator may be used to externally modulate the RF generator. Some FM generators also include the necessary circuitry for developing a composite stereo signal needed to modulate the RF carrier for stereo FM measurements. If such circuitry is not part of the FM generator, a separate stereo composite signal generator would be required for making separation and other stereo FM performance measurements. Readers interested in the new measurement standards for FM tuners and receivers can obtain a copy of the new standards by sending \$6.00 to the Institute of High Fidelity, 489 5th Avenue, New York, NY 10017, and requesting a copy of IHF-T-200, 1975. This standard gives detailed information regarding exact test setup and measurement techniques that should be employed in testing FM tuners and receivers.

Turntable and tape deck measurements

An important piece of test equipment used in measuring speed variation of both turntables and tape transport mechanisms is called a wow-and-flutter meter. In the case of turntables, a special test record containing a 3000 Hz tone is used with this instrument, while in the case of tape decks, a suitable tape recording of the same frequency is used. The wow-and-flutter meter detects any cyclical variation in pitch of

that 3000 Hz tone and presents that variation as a percentage deviation from true speed, as read on a suitably calibrated meter. Some wow-and-flutter meters have certain weighting networks built in and when these are inserted the resultant reading is called the weighted wow-and-flutter reading, sometimes referred to as WRMS wow-and-flutter.

Miscellaneous accessories

In addition to the basic pieces of test equipment already listed, the properly equipped lab or test facility devoted to audio work will also own a variety of less costly accessories. These will include an assortment of test records, each designed for a specific purpose. There are test records designed for the measurement of cartridge frequency response, cartridge tracking ability, turntable rumble, and even overall hi-fi system response including the loudspeakers. Measuring loudspeaker performance, however, is a most difficult assignment and one for which there is very little agreement between experts as to the techniques that should be used. We have purposely omitted any reference to calibrated microphones, graphic chart recorders or anechoic chambers, any or all of which might be involved in any attempt to make meaningful loudspeaker performance measurements.

Certain hum-and-noise measurements for audio products involve the use of various "weighting networks". Essentially, weighting networks take the form of specific filters that modify frequency response in an attempt to take into account the response of the human ear. Normally, three types of weighting networks are commonly used, and these are designated as "A" weighting, "B" weighting and "C" weighting. The circuit shown in Fig. 4,

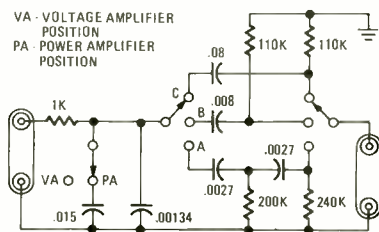


FIG. 4—WEIGHTING CIRCUIT provides A, B or C weighting curves for S/N measurements.

if built into a properly shielded enclosure, will provide the proper response for these three popular weighting filter types.

Combination test equipment

Recognizing the complexity of some of the test setups required for measuring audio products, many test-equipment manufacturers have combined some of the items shown in the block

diagram of Fig. 1 into single, multi-purpose instruments. For example, there is available a distortion analyzer that incorporates a low-distortion audio signal generator and, more recently, is available complete with an IM distortion reading circuit as well. As we noted earlier, there are also FM signal generators that have built-in stereo signal generators, thereby reducing the number of separate items required for FM product testing. One enterprising manufacturer has assembled a group of precision high-wattage load resistors with a handy switching box that permits four-channel-selection of 4-, 8- or 16-ohm loads and also incorporates a set of monitoring terminals so that any channel's output can be displayed on the oscilloscope at will.

More sophisticated testing

Referring once more to Fig. 1, note that a function generator is also included in that diagram. The function generator will, at the very least, be able to produce squarewaves within the audio range. Some manufacturers prefer to test their products by using squarewave input signals instead of pure sinusoidal tones, and a good function generator is needed to duplicate these tests. Better function generators are also capable of producing tone bursts, such as those shown in Fig. 5.

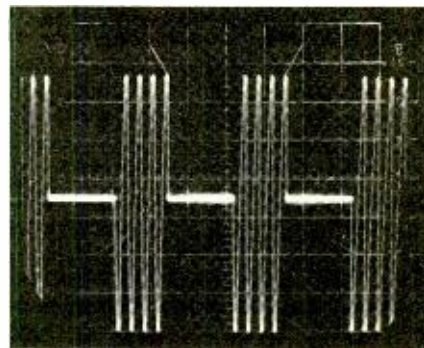


FIG. 5—TONE BURSTS produced by some function generators are useful in audio testing.

Some experts believe that such input signals are useful in analyzing certain aspects of the performance of an amplifier or a speaker system. While most function generators are also capable of producing ordinary sinewave signals, these should never be used in place of the low-distortion audio generator previously discussed. The inherent level of distortion of function-generator produced sinewaves is usually of the order of 1.0% or even higher. If the function generator covers the entire audio range, its sinewave output may be used for a quick plot of frequency response, but not for amplifier distortion or noise measurements. For this measurement, a signal generator with much lower distortion is required.

(continued on page 82)

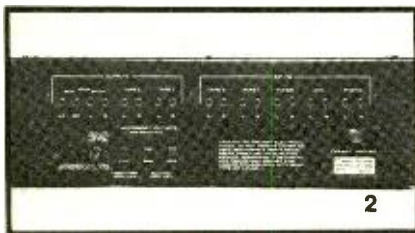
Radio-Electronics Tests Phase Linear Model 2000 Preamp



LEN FELDMAN
CONTRIBUTING HI-FI EDITOR

THE SUDDEN RENEWED INTEREST IN HIGH-powered basic amplifiers has prompted many manufacturers to design and market a variety of preamplifier-control units. Phase Linear Corporation offers two such preamplifiers, the least costly of which is the model 2000 shown in Fig. 1. Its symmetrically arranged front-panel rotary controls include a SELECTOR switch at the upper left, master VOLUME at the upper right, BALANCE control at the lower right and an AMBIENCE level control at the lower left. Smaller, centrally located rotary controls take care of individual control of bass and treble tonal compensation for each channel so that a total of four tone controls are required. Pushbutton switches along the bottom of the panel include TAPE 1 and TAPE 2 monitoring switches, a STEREO/MONO switch, AMBIENCE switch, a switch labelled EQ that adds a fixed amount of bass-boost below 50-Hz independent of any tone control settings, a pair of turnover switches that determine the frequency at which the BASS and TREBLE controls begin to boost or cut and a tone-defeat switch that bypasses tone control circuitry altogether, if desired. A tiny power indicator along the upper center of the panel tells the user that the preamp is being powered.

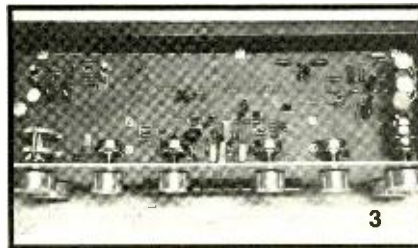
The rear panel of the 2000, shown in Fig. 2, is equipped with five pairs of input jacks (including only one pair for low-level phono inputs), dual pairs of TAPE-output jacks and a pair of FRONT and REAR channel outputs. Three AC convenience outlets (two switched, one unswitched), a



line fuse and a CHASSIS GROUND terminal are also located on the rear panel.

Circuitry

A view of the inside of the chassis is shown in Fig. 3. If circuitry seems sparse, Phase Linear can thank the makers of today's high-density integrated circuits, several of which are used in this design. The block diagram of Fig. 4 illustrates the relatively simple circuit arrangement used in this preamplifier. Of interest is the amplifier block labelled ambience that is driven with both left and right channel signals via a differential amplifier. The difference information is combined with primary channel information in such a way that the right-rear output jack con-

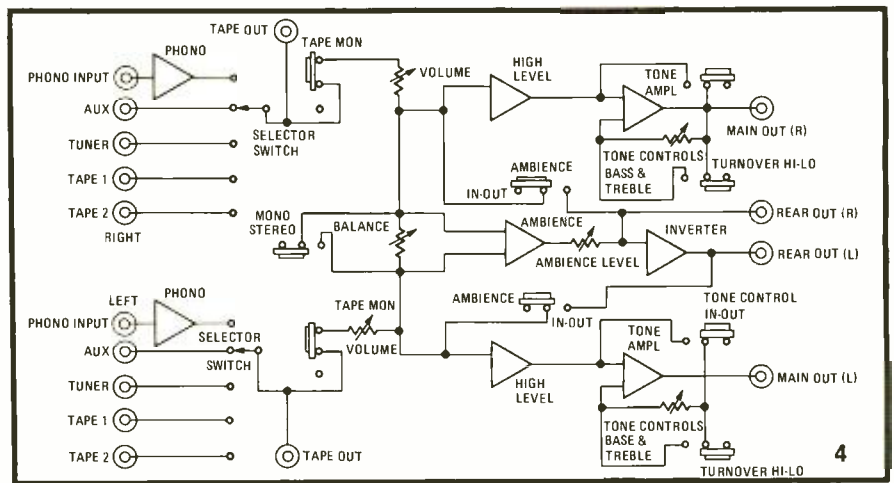


tains the R — L signal while the left-rear jack contains the L — R signal. Such signals, fed to a secondary stereo amplifier and an extra pair of speakers located behind the listener, tend to create a sense of "concert hall" ambience in listening rooms of modest proportions. It should be noted that this method of ambience derivation can also be achieved passively, as suggested some years ago by David Hafler, then of the Dynaco Company.

A circuit feature not specifically evident from the block diagram is the fixed bass-boost equalizer that Phase Linear calls an active equalizer. Effective for frequencies below 50 Hz (where many speakers require some equalization), this extra fixed bass-boost is push-button selected at the front panel.

Lab measurements

A summary of performance measurements for the Phase Linear model 2000 is listed in Table I. At nominal rated output of 2.0 volts, THD was a mere 0.022%, remaining constant at that level all the way up to 10 volts. Waveform clipping occurred at an output of 11.0 volts. While input overload on phono exceeded pub-



MANUFACTURER'S PUBLISHED SPECIFICATIONS:

Frequency Response: (phono) ± 0.5 dB of RIAA standard. **Rated Output:** 2.0 volts; maximum 10 volts into 5K load. **Total Harmonic Distortion:** Less than 0.1% at rated output. **Input Sensitivity:** (phono) 3.2 mV; (high level) 350 mV. **Phono Overload Capability:** 80 mV. **Hum and Noise:** (phono) 74-dB below 10-mV input; (high level) 88-dB. **Ambience Signals:** Left rear = L — R; Right rear = R — L. **Bass Control Range:** (50-Hz turnover) ± 11 dB @ 20 Hz; (150-Hz turnover) ± 13 dB @ 20 Hz. **Treble Range:** (5-kHz turnover) ± 10 dB @ 20 kHz; (2-kHz turnover) ± 14 dB @ 20 kHz. **Dimensions** 5½" (14 cm) high \times 19" (48.3 cm) wide \times 6" (15.2 cm) deep. **Weight:** 9-lbs (4.0 Kg), less optional walnut cabinet. **Suggested Retail Price:** \$299.00.

lished specifications (94 mV instead of 85 mV at 1 kHz). we still consider this to be a bit on the low side in terms of the dynamic range available on some current models of both preamplifiers and integrated amplifiers. Hum-and-noise in phono, reported in our tests as 70 dB, is referenced to the actual input sensitivity (4.0 mV). Translated to a 10-mV input, the figure would increase to 78 dB, or 4-dB better than claimed. RIAA equal-

TABLE I
RADIO-ELECTRONICS PRODUCT TEST REPORT

Manufacturer Phase Linear	Model 2000	
DISTORTION MEASUREMENTS	R-E	R-E
Harmonic distortion at rated output (%)	Measurements	Evaluation
Harmonic distortion at maximum output	0.022	Excellent
Output level for clipping	0.022	Superb
	11.0 volts	Very good
PHONO PREAMPLIFIER MEASUREMENTS		
Frequency response (RIAA \pm ___ dB)	0.4	Very good
Maximum input before overload (mV)	94	Average
Hum/noise referred to full output (dB) (at rated input sensitivity)	70	Very good
HIGH LEVEL INPUT MEASUREMENTS		
Frequency response (Hz-kHz, \pm ___ dB)	13-28, 1.0	Excellent
Hum/noise referred to full output (dB)	82	Good
Residual hum/noise (min. volume) (dB)	82	Average
TONAL COMPENSATION MEASUREMENTS		
Action of bass and treble controls	See Fig. 5	Excellent
Action of secondary tone controls		N/A
Action of low frequency filter(s)		N/A
Action of high frequency filter(s)		N/A
COMPONENT MATCHING MEASUREMENTS		
Input sensitivity, phono 1/phono 2 (mV)	4.0 /	
Input sensitivity, auxiliary input(s) (mV)	400.0	
Input sensitivity, tape input(s) (mV)	400.0	
Output level, tape output(s) (mV)	400.0	
Output level, headphone jack(s) (V or mW)	N/A	
EVALUATION OF CONTROLS, CONSTRUCTION AND DESIGN		
Adequacy of program source and monitor switching		Good
Adequacy of input facilities		Average
Arrangement of controls (panel layout)		Very good
Action of controls and switches		Excellent
Design and construction		Excellent
Ease of servicing		Very good
OVERALL AMPLIFIER PERFORMANCE RATING		Good

TABLE II
RADIO-ELECTRONICS PRODUCT TEST REPORT

Manufacturer Phase Linear	Model 2000	
OVERALL PRODUCT ANALYSIS		
Retail price	\$299.00	
Price category	Medium-high	
Price/performance ratio	Good	
Styling and appearance	Very good	
Sound quality	Excellent	
Mechanical performance	Very good	

Comments: The Phase Linear model 2000 is rather unusual in concept. It does not strive for complexity of controls but at the same time does not follow some of the more esoteric preamplifier designs that are conceived to be "straight wire with gain" devices either. We are rather surprised, for example, that Phase Linear would bother to include out-of-phase "difference" (L-R) terminals on a unit of this type. It seems to us that the sophisticated buyer who opts for a stereo preamp/control unit is not about to add a second amplifier and another pair of speakers for what is, at best, a pseudo-quadriphonic effect that the maker of this unit has chosen to call ambience. And, while the action of the tone controls is excellent and the choice of turnover frequencies is a feature we especially welcome, there are integrated amplifiers and even complete receivers on the market that offer as much tone control flexibility, some even adding a mid-range control. I suppose what is troubling us is that the Phase Linear unit does not quite fit into the two well defined patterns associated with separate preamps. It is neither a full-featured control unit (many less costly preamps at least offer dual pairs of phono inputs, for example), nor is it fashioned in the mold of the so-called "pure" preamps that offer virtually no tonal compensation facilities and simply provide a central program switching facility and faultless signal amplification.

Not that we could fault its signal handling and reproduction capability. Aside from the rather limited phono overload capability (in terms of what is available today on competitive units), all programs reproduced using the model 2000 were in no way colored by its presence in the circuit, as evidenced by our direct switching comparisons in which master tapes were fed directly through to a power amp and then through the combination of this preamp and the same power amp, with preamp gain set at unity. We suspect that elimination of the stages and controls needed for the ambience feature might have resulted in a lower selling price for this unit and that, in turn, might have made the model 2000 a bit more of an audio bargain than it presently seems to be.

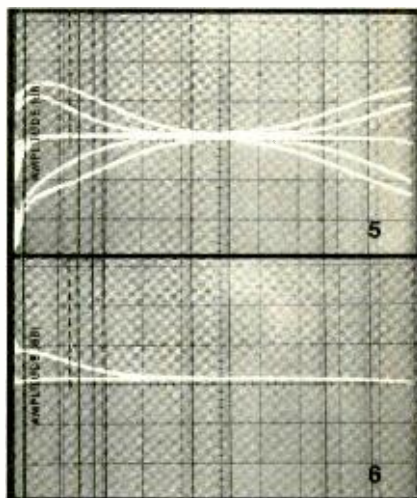
zation was accurate to within 0.4-dB from 30 Hz to 15,000 Hz and overall frequency response (via the high level inputs) was flat within 1-dB from 13 Hz to 28,000 Hz.

The scope photo in Fig. 5 shows the multiple response curves obtained by setting the bass and treble controls to their maximum clockwise and counterclockwise positions and by varying the turnover points from 50 Hz to 150 Hz (for the bass control) and from 5 kHz to 2 kHz (for the treble controls). Note that with the more extreme turnovers, frequency response in the mid-frequency region is affected only very slightly even when controls are used in their extreme positions—a very desirable characteristic.

The two traces in Fig. 6 show the response obtained with the tone controls fully bypassed and the response characteristic of the previously mentioned active equalizer.

Use and listening tests

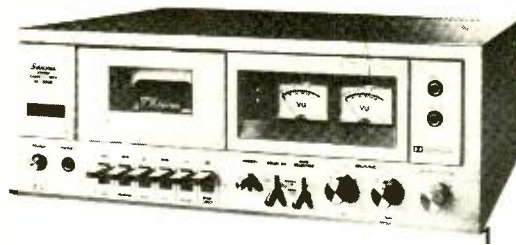
The Phase Linear model 2000 preampli-



fier is easy to install and to use. Familiarization with its controls takes only a few minutes, and the separately positioned left- and right-channel BASS and TREBLE controls are welcome after dealing with many front panels where the controls have been tandem or concentrically mounted in the interest of space conservation. Our conclusions regarding this unit are to be found along with our overall product summary in Table II, as are our evaluations of the preamplifier's "listenability." It is difficult to try to establish a proper price/performance ratio for a product such as a preamplifier. There are preamp-control units on the market that offer even fewer controls and cost considerably more. Conversely, there are preamps designed for the knob twirler that are crammed with knobs, switches and levers and cost no more than the model 2000. When it comes to the choice of a preamp, personal taste has much to do with one's final choice—as does reproduced sound quality. In the latter category, the Phase Linear 2000 certainly rates high marks. As for whether or not it has too many, or not enough controls, that's something each reader will have to judge for himself or herself. It is a matter of personal taste only.

R-E

Radio-Electronics Tests Sansui SC-3000 Cassette Tape Deck



LEN FELDMAN
CONTRIBUTING HI-FI EDITOR

WHILE OTHER MANUFACTURERS OF TAPE cassette decks rushed headlong into the new front-loading configuration for this newest of hi-fi components, Sansui took its time in analyzing the new form and only recently delivered its new model SC-3000 shown in Fig. 1. Evidently, the waiting paid off (at least mechanically), for while this new deck offers all the up-front convenience shared by its competitors there are a few aspects of the compartment design that are worth noting—and which are unique to Sansui's deck. For one, the cassette, when inserted, stands right-side up and is vertically positioned instead of sitting at an angle or horizontally. When the eject button is depressed, the entire compartment pivots forward and the tape is easily dropped in, with tape opening facing downwards. With the compartment illuminated from behind, it is easy to observe tape motion and even to read whatever you have written on the tape identification label. Also, the plastic and metal tape compartment door slips off simply to facilitate head cleaning.

Below the tape cassette compartment are six smooth-acting level controls that actuate the tape transport in its various modes (rewind, play, fast forward), place the unit in the record mode, provide pause control and stop the transport. Pressing the STOP lever a second time ejects the cassette as previously described. It is possible and perfectly safe to go from any tape motion mode to any other without pressing the STOP button in between. Power ON/OFF button and HEADPHONE jack are located to the left of the transport motion controls, while above them are a three digit counter and RESET button that can be used as a memory reset control when the associated memory lever to the right of the transport controls is actuated.

MANUFACTURER'S PUBLISHED SPECIFICATIONS:

Frequency Response (record/playback): (normal tape: 30-13,000 Hz (35 Hz to 11,000 Hz ± 3 dB); (CrO₂ tape): 30-16,000 Hz (35 to 13,000 Hz ± 3 dB). **Wow and Flutter:** 0.09% WRMS. **Signal-to-Noise Ratio** (record/playback): Better than 50 dB without Dolby; Better than 60 dB above 5 kHz with Dolby. **Erasure Factor:** More than 60 dB (at 1 kHz). **Bias Frequency:** 85 kHz. **Input Sensitivity:** (mic): 0.5 mV, 600 to 10,000 ohms. (line): 70 mV, 100,000 ohms. (DIN): 14 mV, 90,000 ohms. **Output Level:** (line): 300 mV with output control at max. **Head Type:** (record/playback): super hard Permalloy; (erase): Ferrite. **Motor:** Electronically controlled, DC. **Fast Wind Time:** Approximately 75 seconds for C-60 tape. **Dimensions:** 17 $\frac{3}{8}$ " wide by 6 $\frac{1}{4}$ " high by 11 $\frac{1}{8}$ " deep. **Net Weight:** 17.6 lbs. **Power Requirements:** 120 volts (can be altered to 220 internally) AC, 50/60 Hz, 10 watts maximum. **Suggested Retail Price:** \$360.00.

TABLE I
RADIO-ELECTRONICS PRODUCT TEST REPORT

Manufacturer: **Sansui**

Model: **SC-3000**

CASSETTE TAPE DECK MEASUREMENTS

	R-E Measurements	R-E Evaluation
FREQUENCY RESPONSE MEASUREMENTS		
Frequency response, standard tape (Hz-kHz \pm dB)	35-14, 3	Very good
Frequency response, CrO ₂ tape (Hz-kHz \pm dB)	28-13.5, 3	Good
Frequency response, other (see text) (Hz-kHz \pm dB)	—
	See Figs.	
DISTORTION MEASUREMENTS (RECORD/PLAY)		
Harmonic distortion @ -10 VU (1 kHz) (%)	0.7 (Std. Tape)	Excellent
Harmonic distortion @ -3 VU (1 kHz) (%)	1.0	Excellent
Harmonic distortion @ 0 VU (1 kHz) (%)	1.2	Very good
Harmonic distortion @ +3 VU (1 kHz) (%)	1.2	Excellent
SIGNAL-TO-NOISE RATIO MEASUREMENTS		
Standard tape, "Dolby" off (dB)	48	Very good
Standard tape, "Dolby" on (dB)	56	Very good
CrO ₂ tape, Dolby off (dB)	53	Excellent
CrO ₂ tape, Dolby on (dB)	60	Excellent
MECHANICAL PERFORMANCE MEASUREMENTS		
Wow and flutter (% WRMS)	0.08	Excellent
Fast wind and rewind time, C-60 (seconds)	65	Good
COMPONENT MATCHING CHARACTERISTICS		
Microphone input sensitivity (mV)	0.6	
Line input sensitivity (mV)	60.0	
Line output level (mV)	280.0	
Phone output level (mV)	140 (8-ohms)	
Bias frequency (kHz)	85	
TRANSPORT MECHANISM EVALUATION		
Action of transport controls		Very good
Absence of mechanical noise		Excellent
Tape head accessibility		Excellent
Construction and internal layout		Very good
Evaluation of extra features, if any		Good
CONTROL EVALUATION		
Level indicator(s)		Good
Level control action		Good
Adequacy of controls		Good
Evaluation of extra controls		Good
OVERALL TAPE DECK PERFORMANCE RATING		Very good

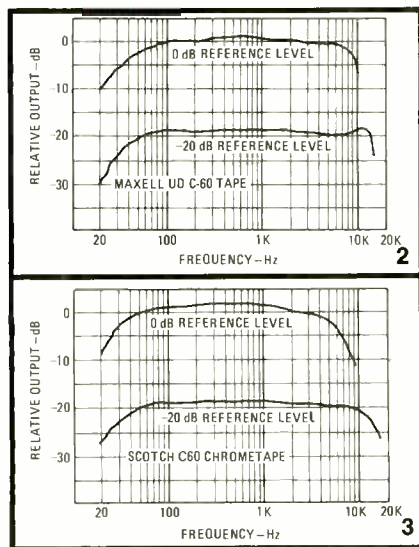
Additional control levers to the right of the MEMORY control include the DOLBY ON-OFF switch and a TAPE SELECTOR with positions for ferric and chrome tapes. Rotary controls include individual channel input record level controls and a single OUTPUT LEVEL control that adjusts the output level of both channels simultaneously. There are no provisions for microphone and line mixing, though either signal source can be connected to the appropriate input terminals.

The upper-right section of the front panel is occupied by a pair of record-level meters, calibrated from -20 VU to +3 VU (dB). To the left of the meters are three LED indicators: one to indicate that Dolby circuitry is turned on, the next serving as a record indicator and lastly, an LED that lights when the recording peaks are 6-dB higher than 0-dB as indicated on the meters. The LED will, of course, flash when transient peaks occur too quickly for the slow-acting VU meters to register. Left- and right-channel microphone inputs are also front-panel mounted at the extreme right. The rear-panel contains only the usual line input- and output-jacks (of the phono-tip variety) plus a combination 5-terminal DIN socket.

Circuit and construction highlights

The Dolby circuit portion of the Sansui deck is essentially derived from a single integrated circuit and Dolby calibration is factory adjusted with no customer-accessible controls. The equalizer-amplifier electronics consists of a two-stage negative feedback circuit and when the chrome position of the tape selector is chosen, the new equalization value of 70 microseconds with a 3180 Hz turnover frequency is in-

troduced along with the necessary increased bias for CrO₂ tapes. Each channel of the microphone preamp section consists of two low-noise transistors and the VU meters are driven by a separate two-stage transistor amplifier. The meters are designed to operate during playback as well as during record.



A high-torque DC motor, governed by an electronic control system, is used to drive the capstan and take-up reels in the SC-3000. Capstan drive includes a heavy flywheel and an electronic switch senses end-of-tape motion to disengage the drive motor and return all transport levers to their neutral positions. Total semiconductor complement includes 24 transistors, 2 IC's, 18 diodes and 3 LED's.

Laboratory measurements

Performance measurements made using the SC-3000 deck are listed in Table I, while frequency response measurements using high-output ferric tape and chrome tape are plotted in Figs. 2 and 3, respectively. Surprisingly, we saw no advantage in using chrome tape with this machine, as compared with a good grade of high-output low-noise ferric tape. While in theory the CrO₂ tape is supposed to yield better signal-to-noise ratios, in practice, at least in the case of this machine, the CrO₂ tape provides much less "headroom" than does the normal tape. This can be further understood by examining the 0-dB record level response curves for both tapes. Since S/N is measured relative to the 3% THD point, and since that point occurs at a lower record level in the case of the CrO₂ tape, the ferric tape actually turns out to be better in combined terms of S/N and THD, yielding a figure of 48-dB without Dolby (unweighted) and 56-dB with Dolby. If an "A" weighting network is used, the S/N number improves to 54-dB without Dolby, a good deal better than claimed by Sansui (which also publishes "weighted" figures). Distortion at 0-VU record level for the ferric tape measured a low 1.2% while under the same metering conditions it increased to 1.7% when CrO₂ tape samples were tried.

Wow and flutter measured 0.08% WRMS, just a bit better than the 0.9% claimed—and a very acceptable value for a deck in this price category.

Mechanical operation of the transport was smooth and silent, and the machine handled C-90 and even C-120 tapes of good quality without breaking or stretching them. Automatic sensing of end-of-tape conditions occurred within a matter of a second or two after end-of-tape was reached. In listening tests, the somewhat restricted frequency response capability of the SC-3000 was more than offset by the low noise and distortion levels heard in musical test recordings played back on the machine.

A summary of our reactions to the Sansui SC-3000 cassette tape deck is included in Table II. **R-E**

TABLE II
RADIO-ELECTRONICS PRODUCT TEST REPORT

Manufacturer: **Sansui**

Model: **SC-3000**

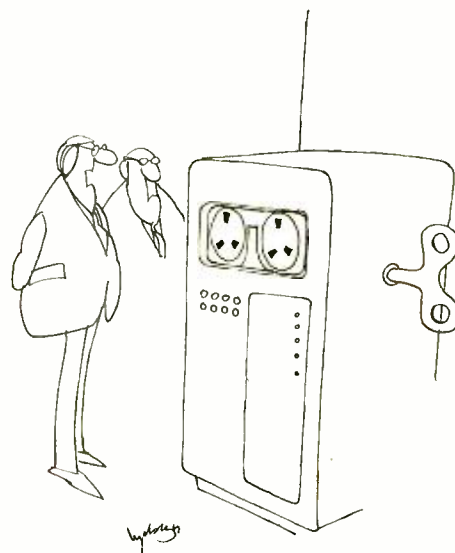
OVERALL PRODUCT ANALYSIS

Retail price	\$360.00
Price category	Medium/High
Price/performance ratio	Good
Styling and appearance	Very good
Sound quality	Very good
Mechanical performance	Excellent

Comments: In the design of any cassette tape deck, one always deals with a series of trade-offs between signal-to-noise ratio, total harmonic distortion, and frequency response. Sansui has elected to combine excellent transport motion with S/N ratio and low distortion but has given up a bit of high end response in the process. Since many new tape formulations have particularly high output at the high frequency end of the spectrum, this seems like a proper course of action to us. As far as we know, the "right side up" insertion of the cassette in this front loading deck is a first, and one that takes the fear out of having to insert the cassette (and one's hand) into the unknown recesses of a horizontally oriented compartment. Tape head cleaning is facilitated by this configuration as well.

Our single important criticism has to do with the absence of line and mic mixing facilities that we have come to expect in a unit in this price category. We would also have liked to see a tape selection position for the new Ferric-Chrome combination tapes which seem to be gaining in popularity. The excellent "headroom" provided when using standard high-output tape with this machine suggests that the use of Chrome tapes in this model may constitute an unnecessary expenditure since, with Dolby in use, signal-to-noise is more than adequate with ordinary ferric tapes and distortion is considerably lower than with the more costly CrO₂ varieties. The peak reading LED's are a useful addition, as is the memory rewind feature, though both of these are by no means exclusive in decks at this price.

All in all, the Sansui CS-3000 is a carefully engineered unit that is easy to use effectively for a variety of home recording work.



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JUNE 1976



The function generator is now occupying more service benches than ever before. This concluding part of a 2-part series of articles covers the operation and applications of this instrument

all about function generators

CHARLES GILMORE*

AS PREVIOUSLY NOTED, THE FUNCTION GENERATOR puts out a sinewave with a total harmonic distortion of 1% or so. What is unique about sinusoidal signals from a function generator is their frequency range, their ability to have controlled DC offset, and the feature that when the wave shape is selected, the output signal is of the correct shape, amplitude and frequency even during the first cycle. This feature is especially important at ultra-low frequencies where a single cycle may represent a major span of time. The sinusoidal oscillator fails in this respect; it needs a number of cycles to become truly sinusoidal and stable in amplitude.

At the upper frequency limits, the function generator is able to analyze most operational amplifier and power supply circuits for frequency response and phase shift characteristics. With the ever-increasing use of integrated operational amplifiers in consumer as well as industrial products, it is important to determine the inherent stability of these circuits in actual operating situations.

Power supplies and other devices designed with operational amplifiers are forms of closed loop servo systems. The servo system derives its high stability from large amounts of negative feedback. The proper technique for analyzing problems in servo systems is to break the loop at some convenient point and substitute a theoretically correct signal at that point.

The function generator is an ideal source of such substitute signals. Not only can it provide signals of almost any frequency, but generally at sufficiently low impedance to stimulate any source without introducing special characteristics of its own. Function generators with DC offset capability are even better suited for this job. The break in the servo loop may not occur at a point where there is no DC offset, and the substituted signal must supply not only a signal with the desired amplitude and frequency, but also a signal with the required amount of DC offset.

Once the function generator has been inserted in the loop, an oscilloscope may be used to monitor the returning signal at

the break (a dual-trace oscilloscope is very handy for this type of testing). With the function generator, the frequency can usually be increased to the point where the total phase shift through the system will be 360 degrees. At this point, the returning signal, displayed on the oscilloscope, should indicate a gain of less than one, or oscillations may occur. The loop may remain DC coupled and the test signal inserted through a capacitor. This

the generator.

Square-wave testing

The unique characteristics of the square wave from a function generator are identical to those of the sine wave. Square-wave testing of an amplifier again becomes important, as the upper and lower ranges of frequency that cannot be reached with the conventional sine/square oscillator can be reached with the function generator. Fig-

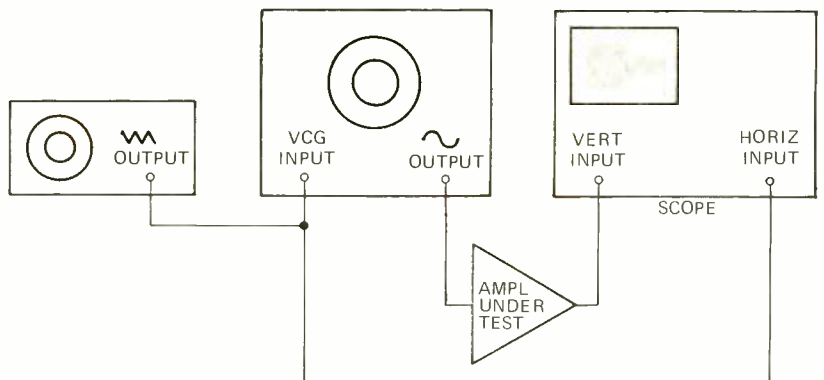


FIG. 6—TWO FUNCTION GENERATORS produce a sweep signal. The sweeping generator (left) may be of a simple type—can be the sawtooth output from an oscilloscope.

makes it unnecessary to find the DC operating point of the loop as well as the AC value for test.

As noted before, the wide tuning range of many function generators is especially useful for analyzing the frequency vs amplitude response characteristics of an amplifier. When frequency response is being tested, the flatness of the output signal is an advantage of the function generator.

Function generators with VCG (Voltage Controlled Generator) capability may be used as sweep generators if some form of a sweeping signal is available. This signal can be a sawtooth output from an oscilloscope, the signal from an internal sub-generator (if available), or, as shown in Fig. 6, one function generator can be used to sweep another using the triangle wave as the sweep signal. If this method is used, the oscilloscope or other display device must also be swept with the triangle wave. When using the sweep function, remember there may be considerable high frequency roll-off across the uppermost decade of

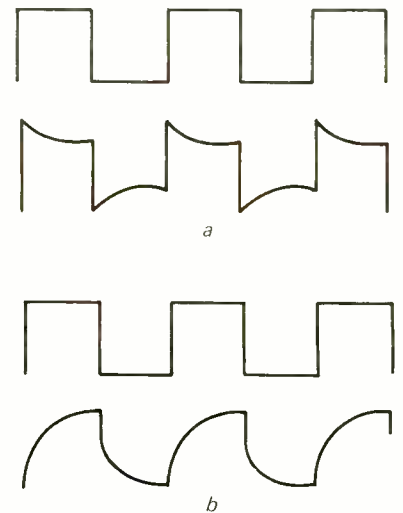


FIG. 7—SQUARE WAVE DISTORTION. The effect of poor low-frequency response is shown in a, and poor high-frequency response is shown in b.

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ure 7 shows the characteristics of overshoot and high-frequency roll-off commonly used for square-wave analysis of amplifiers.

Because of the ultra-low-frequency capability of the function generator, it is often used to drive some form of gating circuit to provide a burst or gated sinusoidal signal. Figure 8 shows a function generator being used to drive a reed relay, which is in turn being used to gate a sine-wave output from a second generator.

Figure 9 shows the square-wave output of one function generator being used to drive the VCG input of a second generator. This creates a frequency shift keyed (FSK) signal which might be used for the testing of teletype circuits, etc.

The output impedance of the function generator is usually low enough (50 ohms) to serve as a source for logic signals of the TTL, DTL, RTL, and ECL families. MOS circuits can be driven by most function generators. With most MOS circuits there is no requirement for a low-impedance drive, so the 600-ohm genera-

tors will work in this application as well. As noted before, the trigger output of many function generators is a TTL signal and may be used to drive RTL, DTL, and TTL circuits directly.

Triangle wave testing

The triangle wave is unique to the function generator and is probably more versatile for general laboratory and service work than either the sine or square waves. An amplifier driven with a triangle wave will reveal a great deal about its characteristics if the amplifier output and input waveforms are compared.

When making simple gain measurements, the exact amplitude of the triangle wave can be readily determined on an oscilloscope by measuring from tip to tip. The ambiguity evident when making this measurement with a sine wave is gone, due to the preciseness of the triangle wave peak.

Comparing the input and output triangle waves permits a linearity analysis of the amplifier. The question of whether or

not the amplifier is doing a proper job becomes simpler, for there is no argument about what the straight line of a triangle should look like, whereas there may be considerable interpretation when a sine wave is analyzed for aberrations.

A common problem on modern amplifiers with complementary output is crossover distortion. As can be seen by the examples in Fig. 10, crossover distortion becomes even more noticeable on a triangle wave. Similar improvements will be noted in the other comparative examples of Fig. 10. These show other common amplifier faults as commonly diagnosed with a sine or square wave, and are presented here with the triangle wave test for comparison.

Although much of our electronic world is becoming digital, almost all digital equipment still has to connect to the analog world. Frequently these are the most complex areas of circuitry to design and the most common causes of service problems. A circuit often used is the Schmitt trigger. The Schmitt trigger converts slowly moving analog signals, such as sine waves, to square waves with voltage levels and rise and fall times compatible with the logic being used. To avoid false triggering on noise, hysteresis is built into the Schmitt trigger. Hysteresis causes the trigger to change output state at a higher input voltage level for positive-going signals than negative-going signals. Insufficient or improperly adjusted hysteresis will cause erratic operation of the trigger. The function generator can be used to measure the hysteresis in a trigger. Figure 11 shows the measurement, using the triangle wave output of the generator and an oscilloscope.

These connections may be used to adjust the trigger sensitivity. First reduce the signal level of the generator until the trigger just fails to respond. Adjustments are then made in the circuit to cause triggering. This procedure is repeated until there is no further improvement in the sensitivity of the trigger.

The interconnections shown in Fig. 11 may also be used to measure the pull-in and drop-out voltages of a relay. The relay is swept with a low-frequency triangle wave from the function generator and the contact operation is monitored with an oscilloscope or a meter. When contact operation is detected, the value of the triangle wave amplitude is measured, yielding the respective pull-in and drop-out figures.

The triangle wave of a function generator may be used to replace a manually swept DC control signal when analyzing a circuit. For example, a manual gain control circuit is suspected of causing an amplifier problem. With the gain control disconnected, a triangle wave from the function generator is substituted. With the frequency set to a low value, such as 0.5 Hz, the gain of the amplifier may be swung through its complete range twice every second. The output of the amplifier can now be monitored with various input signals to determine if the suspected problem exists.

The triangle wave can be used as the sweep signal for either an oscilloscope or an X-Y recorder in many applications. Frequently an experimental setup will re-

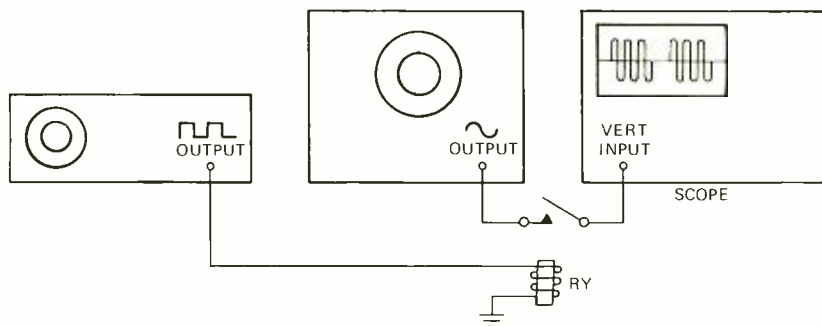


FIG. 8—LOW-FREQUENCY CAPABILITY of the function generator, plus low output impedance, permit its use in a circuit to drive a mechanical gating circuit directly.

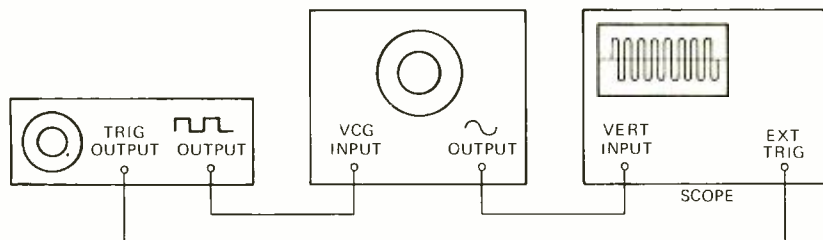


FIG. 9—A KEYED FREQUENCY SHIFT can be produced by this generator combination.

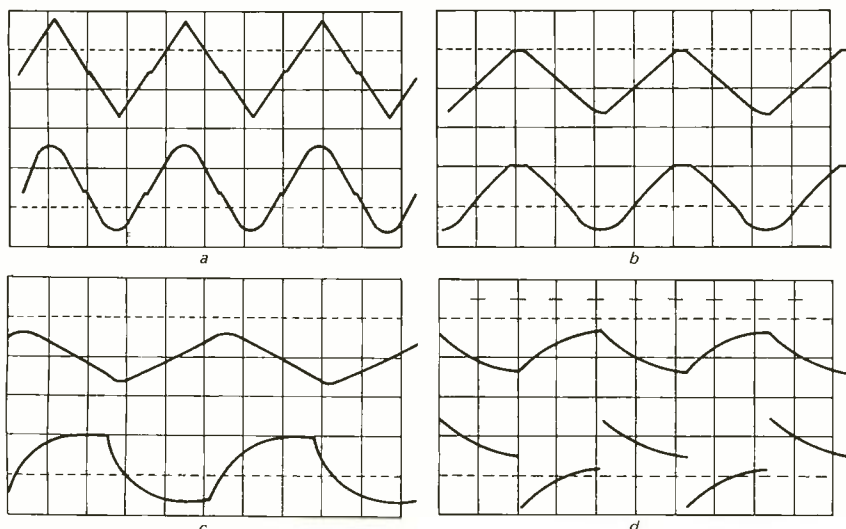


FIG. 10—COMPARISON of triangle vs sinewave testing. Effects of crossover distortion is shown in a, and clipping is shown in b. Square wave vs triangle wave testing. The effects of poor high-frequency response is shown in c, and poor low-frequency response is shown in d.

quire the signal sweeping the oscilloscope to be in exact synchronism with the signal driving the experiment. The triangle wave form is excellent for this purpose. (The user must remember the sweeping waveform is a triangle and not a sawtooth.) In some of the more sophisticated function generators, a variable time symmetry control will permit the output of the function generator to be changed from a triangle wave to a sawtooth with a 95 to 5 percent duty cycle.

In the perfect triangle wave, the rate of voltage change in time is constant between the turn-around points. The circuit of Fig.

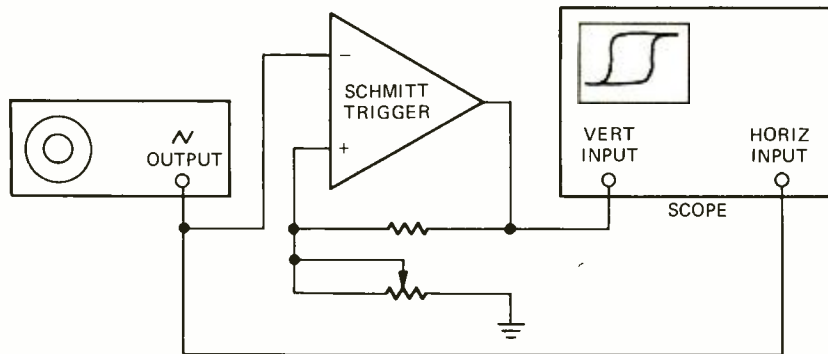


FIG. 11—TRIANGLE OUTPUT OF FUNCTION GENERATOR is used to measure and adjust hysteresis on a Schmitt trigger, as shown on the oscilloscope display.

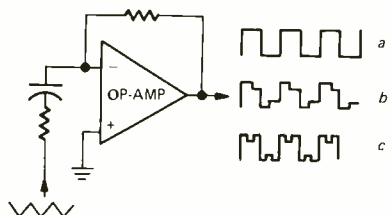


FIG. 12—A DIFFERENTIATOR CIRCUIT. Output is uniform except at crossover points if the rate of change on the input is constant. Output with perfect triangular wave at its input is shown in a. Output if input is not perfectly linear is shown in b. Effect of crossover distortion is shown in c.

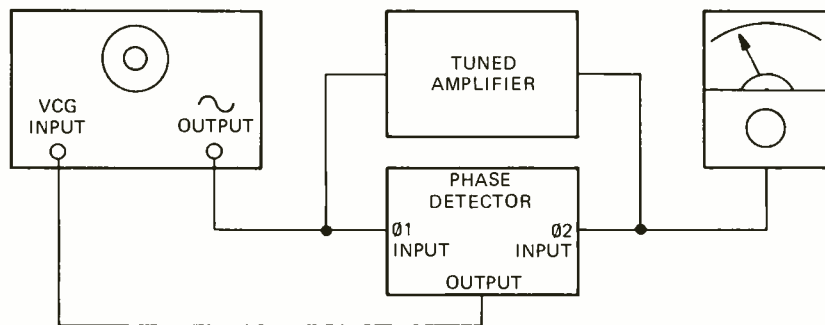


FIG. 13—TUNED AMPLIFIER TESTING. Drifts in amplifier frequency are tracked with a phase detector, output of which makes the generator track the amplifier's frequency.

12 is called a differentiator. The output of a differentiator is zero if the rate of change of the input signal is constant. If the rate of change is not constant, an output signal is developed. This circuit may be used to further improve the analysis of a linear circuit being driven with a triangle wave. If the circuit is perfectly linear, there will be no output from the differentiator circuit except at the turn-around points of the triangle. If the circuit is causing variations on the triangle due to distortion introduced in the signal at different levels, the output will no longer be zero between

turn-arounds and the aberrations can be detected. The advantage of using this circuit is that small changes can be considerably magnified.

The VCG

As noted above, the VCG (Voltage Controlled Generator) can be used to develop a sweep generator or a frequency shift keyer. There are many other uses for this versatile input to the function generator. Phase-lock-loop circuits are becoming common in electronic equipment today. One of the major building blocks in a phase-lock-loop is the voltage-controlled

oscillator. In either experimental work or service work, it may be desirable to break the loop and substitute external signals to aid the analysis. The function generator is used for this purpose. Not only can the function generator be used to substitute signals within the loop, but the function generator with VCG capabilities can be used to replace the voltage-controlled oscillator.

Some function generators offer a feature which allows the main tuning dial of the generator to control the generator frequency, even when external VCG signals are applied. This allows the user to fre-

Figure 13 shows interconnections used to test the gain stability of a tuned amplifier over a period of time. The gain of the amplifier can be measured only if the driving frequency keeps track of any drifts in the tuned circuits of the amplifier. The phase detector at the output of the amplifier detects changes in the phase of the output signal relative to the input signal. Changes in phase will occur when the resonant frequency of the tuned circuits begin to change. The output of the phase detector is connected to the VCG input of the function generator, so changes in phase at the amplifier output will be converted into corrective changes in the generator frequency.

Measurement errors

The function generator is relatively simple to operate, and only a few errors tend to surface. Errors in frequency settings are common. These errors may be of accuracy or may be of improper range. Errors of accuracy are usually caused by failure to remember that frequency setting tolerance is given as percentage of full scale. This can lead to considerable error at the lower portions of the function generator scale, especially where the tuning range is 100 or 1,000 to one. The function generator should not be considered a frequency standard. A frequency meter is always advantageous. When a generator has a wide tuning range, it is not uncommon for the user to become confused about the range setting. This often leads to operating frequency errors of an order of magnitude.

Errors in estimating the output amplitude based on attenuator setting are common. Frequently the user forgets the output level is not defined unless the generator is operating into either an open circuit or into its defined load impedance. Again, the best way to be certain of the output level of a function generator is to measure it. This is particularly easy with the function generator. As the output amplitude is constant, the amplitude can be measured at a frequency where the voltmeter is accurate, and the frequency may be then adjusted to the desired value. This should not be done if the wave shape is to be changed, as the peak amplitude between all waveshapes may not be constant. Output voltage levels may also be measured at one particular step attenuator setting and then the attenuator changed by either 10 dB to reduce the voltage to one third, or 20 dB to reduce it by a factor of ten.

A common error is improper voltage/power ratios in relationship to dB changes of attenuators. Consult the table until it is familiar.

Change in Output Attenuator	Voltage or Current Change	Power Change
- 3 dB	×0.707	×0.5
- 6 dB	×0.5	×0.25
-10 dB	×0.333	×0.1
-20 dB	×0.1	×0.01
+ 3 dB	×1.414	×2
+ 6 dB	×2	×4
+10 dB	×3	×10
+20 dB	×10	×100

When the function generator is being
(continued on page 69)

quency-modulate the generator about a center frequency, with deviation governed by the external VCG voltage.

A digital voltmeter can be created using the VCG and a digital frequency counter. The unknown voltage is applied to the VCG input of the generator, and the digital frequency meter is applied to the generator output. For example, a generator that will sweep from 100 Hz at the rate of 100 Hz per volt will give a reading of 450 Hz for a 4.5-volt DC input signal. The linearity of this voltmeter will be the linearity of the VCG.

Step-by-step

TV Troubleshooters Guide

AGC circuits may appear to be complicated, but they aren't.

By following logical troubleshooting procedures,
AGC problems can be rapidly diagnosed and cured

JACK DARR
SERVICE EDITOR

AUTOMATIC GAIN CONTROL CIRCUITS (AGC) seem to baffle a lot of novices and a few working technicians. They shouldn't. The AGC circuit is basically very simple if you boil it down. All it does is automatically adjust the gain of the "controlled stages"—IF and RF amplifiers—so that the video signal at the detector remains at the same level. It does that by developing a small DC bias voltage, which decreases the gain of those stages. If the signal level rises, the bias goes up with it, so the gain is reduced. If the signal falls, the bias is reduced and the gain increased. That's all there is to it.

The circuitry may look complicated but it isn't. It's very well adapted to step-by-step troubleshooting methods. A few simple tests will instantly identify AGC troubles, and these can be easy to find and fix.

The first and simplest form of AGC was the negative voltage developed across the video detector load resistor. Figure 1 shows this type. This voltage is, of course, directly proportional to the incoming signal strength. It was fed back to the grids of the controlled stages through a network of resistors, bypassed with capacitors (R and C in Fig. 1); this is the "AGC bus". If the signal got stronger, a higher negative voltage was produced, reducing the gain of the IF stages.

It wasn't too satisfactory. There were disadvantages; one of them was its response speed. It couldn't cope with a rapidly varying signal. Also, it "read" the whole signal, video, sync and all. So, it would fluctuate when the scene changed from dark (high modulation) to bright (low modulation). It did have the advantage of low cost; I was mildly surprised to find it still in use in a small black-and-white TV of quite recent vintage!

Keyed AGC

So we needed a more accurate system. This led to the development of a circuit called "keyed AGC" (gated AGC is the same thing.) The action was the same but the circuitry was different. In a TV signal, the horizontal sync pulses represent 100% modulation. (Really, it's "maximum modulation" since it is just a bit less than 100% modulation to avoid clipping.) The video modulation varies constantly, but the tips of the horizontal sync pulses always represent the actual maximum signal-level. So if we had a circuit that would develop AGC voltage based on the sync tips, it would be much better.

We got it. We feed the detected video

signal to the grid of a tube (see Fig. 2). This tube has no plate voltage! (This is one of the puzzling points about this circuit.) Actually, of course, it *does* have plate voltage, in the form of very sharp positive-going pulses fed to it from the flyback. So, the tube conducts *only* during the horizontal sync interval. The pulse turns it on (keys or gates it) at this time, and it is

tightly cut off during the scan period so that the varying video signal has no effect.

The keyed AGC circuit thus operates only while the horizontal sync pulses from the signal are being received on its grid. Plate current flows through a resistor, and as usual, develops a DC voltage drop across a capacitor. Now, here comes the other puzzling thing; the voltage on the plate of the tube is *negative*. How does that happen? Fig. 3 shows how.

Note that the plate load resistor goes to ground. While the keying pulse is present, the plate is highly positive; there is a signal on the grid at the same time, (the sync is positive-going to make the tube conduct). So, electrons flow from cathode to plate, and then through the resistor to ground, and back to the cathode to complete the circuit. When electrons flow through a resistor, the end they flow *into* becomes more negative than the other end. Since there is no *steadily applied positive* DC plate voltage, the plate reads *negative to ground*. The value of this negative voltage is directly proportional to the value of the video signal on the grid.

So, we did it! We got a DC voltage directly proportional to the amplitude of the video signal, and we can use it as a control bias. One more point must be remembered; the source of this voltage is a series of very short pulses. We must have a pure DC voltage for our AGC bias. So the pulses are fed into a capacitor, and charge it up to the maximum level. This is exactly the same thing that the diode and input filter capacitor are doing in the DC power supply!

One more point before we leave. The capacitor, and the resistor next in the circuit, are the two parts that determine the AGC *time constant*. This means the speed with which the AGC can react to a change of signal level. We don't want this time constant to be too long, or we'd be back with fluctuations in the picture. So it is usually pretty short. When these parts are replaced, the same values must be used.

Delayed AGC

Almost all circuits now use delayed AGC. Translated, this means that we apply our AGC voltage to the IF stages, but we leave the RF amplifier in the tuner running at maximum gain until the signal gets so high that the IF AGC cannot control it without clipping. Too much bias applied to the IF stages will cause them

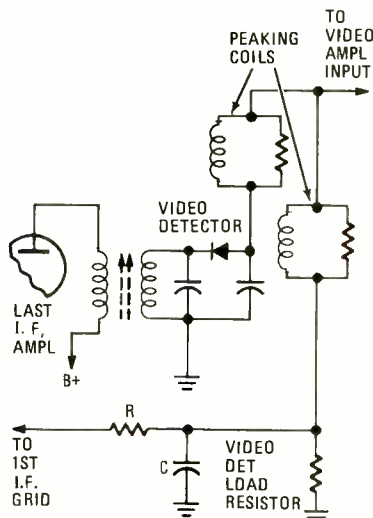


FIG. 1—EARLIEST FORM OF TV AGC. Voltage across video load resistor is filtered by R and C and applied to IF stages.

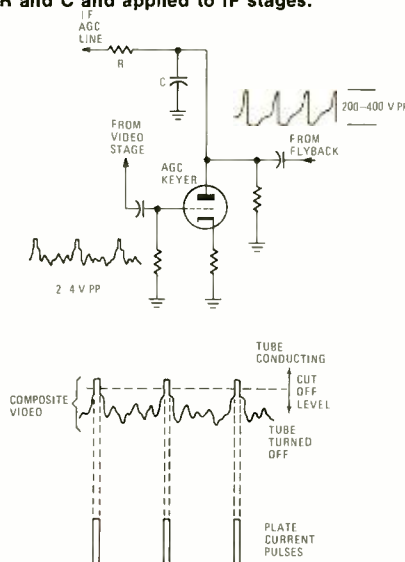


FIG. 2—A BETTER KIND: KEYED AGC. Tube works only when sync pulses are at grid.

to clip, and when that happens, the first thing that gets chopped off is the sync!

To get a delay action, we bias the RF amplifier in the tuner so that it stays at full gain until the IF AGC voltage reaches a certain level. This is easy to do; we simply feed in a very small positive voltage to the RF AGC line. Let's plug in some figures

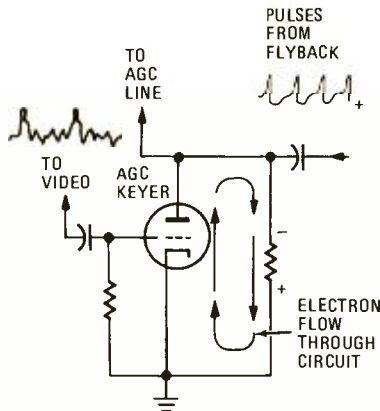


FIG. 3—WHY VOLTAGE IS NEGATIVE. The plate is grounded through a resistor, and electrons drawn to it by the heavy sync pulses have to find their way back to ground through the resistor, causing a voltage drop.

for illustration; say that the IF AGC will work OK up to a level of -5 volts. So, we make the RF AGC $+5$ volts in normal operation. If the signal goes away up, the IF AGC might go to say -7 volts. This will override the $+5$ volts on the RF amplifier, and we come out with a -2 volts of bias to reduce the gain to the point where the IF can handle it. So, we have "delayed" any RF AGC action until the IF AGC gets up to a -5 volt level.

Solid-state AGC

How does AGC work in transistor TV circuits? *Exactly the same* as in tube sets! The AGC bias developed is of a polarity that reduces the gain of the controlled stages. The only thing we need to remember is that this may be *either* positive or negative! Transistors come in two polarities, NPN and PNP. Also, there are two ways of biasing them; "forward AGC" which means applying control bias in the polarity which makes the transistor conduct more, and "reverse AGC" which is what it says; reverse polarity. Negative for NPN, positive for PNP. We don't really need to bother too much with this; you'll find the correct voltages and polarities given on the schematic diagram. In Sams Photofacts, they thoughtfully give you the *range* of AGC voltages to be expected. This is *very* helpful.

Before we go on, here is a very important point. If you forget it, you can get into a lot of confusion. To check the DC voltages around an AGC stage, always remember that the voltages given on the schematic are *no-signal* voltages! This is the only way we can get a "standard" set of test conditions. One more: these voltages will *change* when a signal is applied. (If they don't, the AGC isn't working. This is one of our most useful tests.) If the DC voltages shown on the schematic don't match what you read, look out. This usually means that the AGC isn't working

properly. The DC voltages on the controlled stages are such that the amplifiers are in a "maximum-gain" condition. Remember that one, too. We'll put it to good use in just a minute.

AGC controls

To get the best results from any TV set, we need an adjustment in the AGC circuit. This will let us set it up so that it will work best on weak signals or strong signals. Actually, the AGC control is needed more in very strong-signal metropolitan areas, to reduce the gain and prevent overload. Practically all the later TV sets have very good sensitivity, and will work in deep-fringe areas.

AGC is a gain control; so, the AGC control is a "gain control for the gain control." By varying the bias on the AGC tube or transistor, we can set it up so that the set makes the best pictures in any location.

The *reaction* of this control is one of our best and fastest tests for AGC trouble. Just turn the control from one end to the other and watch the picture. Normal reaction (tube sets) should be a "whiteout" at one end, meaning a very pale picture or even a clear, blank raster, and a "blackout" at the other. At this end, the picture will become very contrasty, and will probably bend and writhe, with a buzz in the sound. (This is "AGC buzz"). In many color TV sets, the raster will go completely dark.

The whiteout is due to too much negative bias; blackout, too much positive bias (tube sets). Somewhere in the middle, you should be able to get a good clean picture with plenty of contrast. If this control shows no reaction at all on the picture, or only a very little effect, look out. It's a very good clue that the AGC isn't working as it should.

In quite a few transistor TV sets, you'll find dual AGC controls. One will work on the IF AGC, the other on the RF AGC. You may find an unusual reaction when adjusting the IF AGC control. At one point, you'll see snow in the picture, even on a fairly strong signal; the proper setting is usually just out of the snow, where the background clears up and the picture is

sharp. This one is set up first, and the RF AGC control is then set for the best picture.

Filtering and clamping

AGC voltage is distributed to the points where it's used through a network of resistors; each point is well bypassed. The impedance of the AGC line to ground must be very very low. If one of the bypass capacitors should open, signals from one stage will get into others, causing oscillations, beats and many other symptoms.

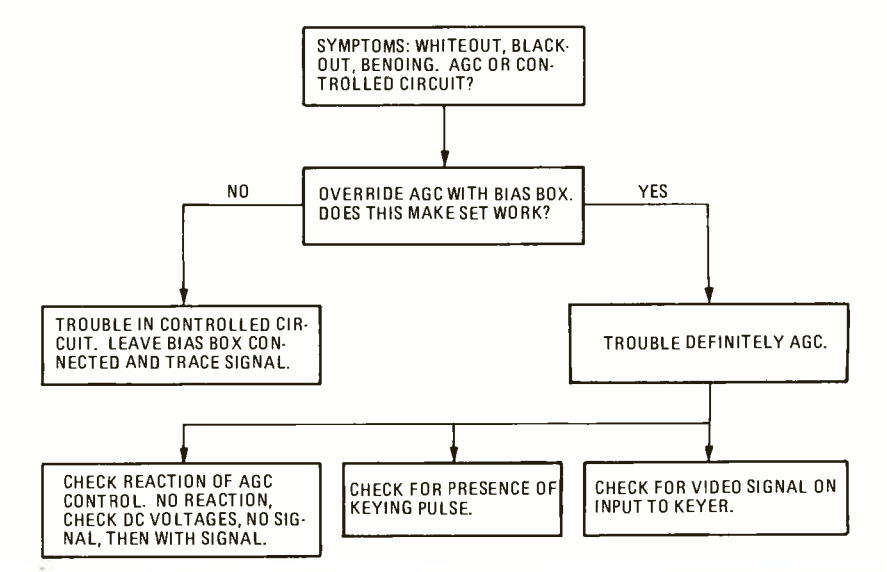
The RF AGC delay circuit is often made by connecting a high value resistor, 10 megohms or so, from a source of positive voltage to the RF AGC line. This is a "clamp" resistor; it feeds in a very small positive DC voltage to keep the RF amplifier from being affected until the IF AGC voltage reaches the desired level. Remember this one, too!

AGC testing

Testing for AGC trouble can be very easy. Check the symptoms: common troubles which can be due to AGC are whiteout or very pale picture; overloaded or bending picture, with buzz; loss of sync (usually both vertical and horizontal, but sometimes only vertical); and beats, "squiggles" and oscillation. There may be others. This multiplicity of possible symptoms might be one of the reasons why so many people have trouble with AGC.

However, there is a very simple test which will always identify AGC trouble. In all cases, the trouble could be one of *two* things; a fault in the *controlled stages*, or a fault in the control circuitry. To isolate this, simply *clamp* the AGC voltage with a bias-box. This is a small DC power supply, which can be adjusted to any voltage needed. Check the schematic to see what the no-signal voltage should be on the AGC line. Say that this is given as -2.5 volts. Connect the negative lead of the bias-box to the AGC test point, and the positive to chassis. Now, set the box to 2.5 volts and look at the picture. If your original symptom was "clean white screen, no picture," this might bring back the picture and sound. If the

TROUBLESHOOTING CHART—AGC circuits.



picture is overloaded, turn the bias-box to a higher voltage. If you can adjust the AGC voltage and get a good clear picture and sound, this makes it definite; the fault is in the AGC. If you can not get a clear picture, this clears the AGC of suspicion! The fault is in the controlled stage, somewhere. Leave the bias-box connected, set at maximum gain voltage, and you will be able to check out the IF stages, or tuner, to find out what the real cause of the trouble is.

This test should always be used if you can't get a normal reaction from turning the AGC control. Reason: it is possible to have a fake AGC fault, if there is a fault somewhere in the IF, such as a bad tube or transistor. This can upset the AGC because it causes the loss of the video signal which must be present on the AGC keyer grid (base) before the AGC circuit can work.

The DC voltages

If the trouble is definitely in the AGC, take the signal off the set. Now, read all the DC voltages around the AGC keyer stage. These should be pretty close to the values given on the schematic. If any of them are quite a bit off, trace out the circuit to find out why. In the typical set, almost all of these DC voltages will be fed through voltage-divider networks. If either of the resistors goes far off value, this will upset the DC voltages on the AGC stage and it won't work properly. You will probably have to lift one end of the resistor to get an accurate test; there are always several shunt paths in these circuits that throw the in-circuit resistance readings off.

Always check for the presence of the keying pulse on the keyer. In tube sets, this will be several hundred volts positive-going. (Make sure of this! One of the most curious troubles I ever ran into was a case where the keying pulse was present, and of the right amplitude. However, it was negative, due to an incorrect connection to a new flyback! For some reason, no one noticed the polarity for quite a while!)

In transistor circuits, the keying pulse may be positive or negative going, depending on the type of transistor. In all cases, it will be of the polarity that makes the

transistor conduct: positive if it's an NPN and negative for PNP. The peak voltage will be much lower, sometimes only 25 to 30 volts. The pulses are often fed through a diode.

A scope is the easiest way to check this. However, you can make continuity tests from the keyer plate back to the flyback, and substitute a new capacitor for the pulse-coupler. Some sets feed the keying pulse through a little coaxial cable from the flyback. Check this to make sure that it has continuity, and is not shorted; if the plastic cable has touched a hot tube, it may have melted and shorted.

In tube sets, always try a new keyer tube. A tube with low emission, or some leakage, can upset the AGC very badly. In transistor circuits, check the transistor for leakage. Also, check the pulse-coupling diode; leakage in it can cause trouble.

Always check the video waveform on the keyer grid (base). This is usually picked up in the output circuit of the video amplifier stage, but may be taken off the video driver. It will be fed through a coupling capacitor or a resistor network. Some of the video may be deliberately clipped off. Watch out for signs of clipping on the sync-side of the waveform. In a positive-going sync circuit, this will be the top. The sync pulses must be clean and sharp. If you can get a good picture on the screen by clamping the AGC, but the video signal at the keyer is missing or distorted, go back to the video stage and trace it through the network with the scope.

In cases of oscillation, beats, etc., the trouble can be due to an open bypass capacitor in the AGC circuit. Once again, the scope is the best check. It should show absolutely no sign of any signals, pulses, or other activity on the AGC line. If you see anything, bridge good capacitors across each of the original bypasses; one of them will be open.

Offset DC voltages

The normal AGC voltage in most sets will show a variation of only about 4-5 volts. If the controlled grids or bases are close to ground, this is what you'll read. However, watch out for sets that have offset bias voltages. You may read up to 35 volts or more from the AGC line to

chassis. Check the schematic; in circuits with grid or bases near ground, such a high positive voltage would definitely mean trouble. However, if you can see that the cathode voltage on the 1st IF tube is set at +35 volts, and the control grid at +34 volts, this is normal. The actual bias voltage (and AGC as well) is the difference between grid and cathode voltages. In this case, the bias is -1 volt. To override this AGC bias, set the bias box to +35 volts and you'll actually have zero bias voltage. Adjust the bias box around this point to see if you can get a good picture. Always check the no-signal DC voltages on the controlled stages, on the schematic.

The AGC reaction

There is another easy check to make sure that the AGC is or isn't working. Read the DC voltage on the AGC line, without signal. Now hook the antenna up and read the voltage again. With a strong signal, in a tube set, the AGC voltage should show a definite swing toward more negative voltage. If there is no change at all, the VTVM is telling you that the AGC definitely is not working. If it changes in the wrong direction (goes more positive in a tube set, for example), this too is a sign of trouble.

Summation

There you are. That's how an AGC circuit works. Follow the step-by-step method of testing it, and you'll be able to identify and correct any kind of AGC problem. Here they are again; see the chart, also:

1. Check the symptoms on the screen. If these could be caused by AGC trouble, try the AGC control; note its reaction.
2. If the reaction is wrong, apply override bias to AGC test point. Vary voltage. If you can get a good picture, this is definitely AGC trouble.
3. Read the no-signal DC voltages around the AGC stage. If these are off by more than 5%, check for presence of both the keying pulse and video signal on the AGC stage. Substitute new tube or transistor.
4. If there is oscillation or instability, check AGC bypass capacitors. R-E

THIN HORIZONTAL LINE

The vertical sweep on this Philco M2610 black-and-white TV is gone. Just a very thin horizontal line. Injecting a 60-Hz test signal into the vertical output grid or plate does nothing at all to the line. I don't know the resistance of the vertical output transformer or yoke.—J.G., Arlington, VA.

I had exactly the same symptom on a different brand not too long ago. Turned out to be a dead short between the ends of the vertical output transformer primary! The tube was pumping into a dead short. The normal resistance of this transformer is 160-ohms primary, 7.5-ohms secondary (yoke disconnected). The yoke winding should read 33-ohms.

Suggestion: unhook the vertical winding of the deflection yoke, feed a signal into the primary, (with the set turned off) and scope the secondary to see if the signal gets through.

OUTPUT TRANSISTORS

The output transistors in this Symphonic C-85 stereo are out. They're marked SC-4131, and are in the hex shaped heat-sinks with a stud. It had a bad hum that cleared up by

replacing the two 100-μF filter capacitors. Now we need data on those output transistors.—F.O., Mena, AR.

A HEP-245 will work with these. The cases are different but the ratings are OK. I've used them for replacements in this chassis. Be sure to get the cases tightly bolted to the chassis on general principles although I ran one for quite a while without a heat-sink just to find out!

FINAL CURE FOR SYNC PROBLEM

I tried everything I could think of to clear up a screwy sync problem on this Admiral. Then I tried everything you could think of. Finally, I tried realigning the IF's. That did it! The curve showed that the IF's were off just enough to cause the vertical sync and AGC to act up!

The scope is a marvelous invention, and thanks to Mr. Dumont! Can you tell me why a scope just sits around and we won't get off our duffs and REALLY use it?—G.Y., Yellowstone, MT.

No, I can't. I've burned out three sets of tonsils in the last 15 years yelling at people to USE a scope! It will give you vital data that you can't get with any other test instrument.

rectly from the flyback circuits. In the Sylvania circuit shown in Fig. 1, the higher DC voltages from the primary power supply feed the video output transistor, picture tube cathode and screen and the sync separator. The last was probably included to make sure that the horizontal oscillator gets started in sync just for luck!

You can trace out the primary and secondary power supplies in the circuit shown in Fig. 1. Note that the flyback winding supplies a negative-going pulse to the diode. This diode conducts during the *scan* time. If the winding is reversed so as to feed a positive going pulse to the diode, we get a "flyback" or pulse-derived supply. The diode conducts during horizontal retrace time. Figure 2 shows the difference between the two rectifier circuit types. The output is the same; the only difference is in the polarity of the applied pulses. The original of these circuits are used in the General Electric JA, QA, QB, XA and YA color chassis.

The circuit shown in Fig. 2-a can provide about 140 volts DC from a half-wave rectifier and filter. The circuit shown in Fig. 2-b can easily provide any low voltage you want from the flyback, which "has to work anyhow"! The much higher *frequency* of the flyback supply makes filtering a lot easier. Capacitors can be a lot smaller for the same filtering efficiency. The "choke" can be a 10-ohm resistor, as you can see in Fig. 1.

So if you find oddball reactions like this in any of the new sets, check to see what kind of low-voltage power supply they're using. The first thing, of course must be the primary +145 volt supply. If this isn't OK, nothing will work. If this is up to normal, then look for the eyeball-clues such as the picture-tube heater. Scope the horizontal output stage to see if it is working. They're no more difficult to service than the older types if you know what to look for. **R-E**

reader questions

VERTICAL BARS

This is a weird one! Whenever I turn this RCA CTC-16 on, I get quite a few dark, ragged vertical bars on the screen. They're "fuzzy" on the edges and make little rainbows. The real weird part is that I get the same kind of thing on other color sets that are nearby! I can stop it by turning the CTC-16 off. What the heck is going on here?—L.C., Oden, AR.

From much sad experience, I'll bet I know! Loosen the back cover of the flyback cage, lift it up, and check to make SURE that the plate-cap of the

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PC-14-	30	8.25	15.25
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PC-16-	12	8.25	15.75
PC-16-	18	8.50	16.00
PC-16-	24	8.75	16.25
PC-16-	30	9.00	16.50
PC-16-	36	9.25	16.75
PC-24-	12	12.00	25.00
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3A3 tube fits firmly into the socket on the top of the high-voltage winding. If the back cover (which has the 3A3 socket on it!) isn't precisely positioned, the 3A3 cap will miss the socket and sit on the edge. It will arc from the winding to the tube; this generates the vertical bars and all the rest of the garbage that you're radiating from it. Tighten the back cover firmly and make sure the screws are all the way to the bottom of those slots!

YOKE RETURN CAPACITOR

Capacitor C16, a 0.1 μ F, in the hori-

zontal deflection yoke return in this Magnavox T979 chassis keeps blowing out. It shorts and the raster folds up to about 3 inches wide. What can I do about this?—M.D., Chicago, IL.

Repeated failure of this capacitor indicates that either the original or the replacements haven't got enough safety factor to stay in there. I'd suggest replacing it with one of the same capacitance, but with a minimum 3-kV voltage rating! That ought to hold.

FUZZY RIM AROUND FACEPLATE

This set has a 19EYP22 picture tube.

It has a "frosty" look all the way around the outside of the faceplate; comes in about an inch or more. What causes this, and is there anything I can do about it?—H.M., Largo, FL.

This could be due to the safety glass separating from the actual faceplate of the picture tube. It's not too common, but I've heard of it. I am told that most picture tube rebuilders can re-cement a loose safety glass back in place, if the tube itself is in good shape. Check around your area and see who does this kind of work.

COLOR BAR GENERATOR PROBLEM

We built the "IC Color Pattern Generator" (R-E, January 1970). Everything works fine except the color bar pattern! I keep getting 15 or 20 horizontal rainbows between the dark vertical bars. What to do to correct this?—J.D., Diamond Bar, CA.

The original answer was "Check that 3.56 MHz crystal." The reader solved the problem by putting the crystal trimmer in series with the crystal. He had gotten a parallel-resonant type, and what was needed was a series-resonant crystal. This cleared up the problem and the 3.56 MHz oscillator is now on-frequency and making color bars.

HORIZONTAL OUTPUT PROBLEMS

I had a horizontal output problem in a Magnavox TS982. You suggested the use of a variable-voltage transformer. Thanks for that; it helped me solve it. The cause was a short in the collector of the regulator transistor. If the screw was tightened too far, it grounded the collector to the heat-sink, thus killing the 28-volt supply!

This started as an intermittent. Owner stated that original symptom was a loss of width that could be cleared up by hitting the cabinet. I found that just the right amount of tension on this screw caused a low-resistance leak which resulted in a chain reaction of blown parts. Replacing the insulator and tightening the screw properly fixed the whole thing.

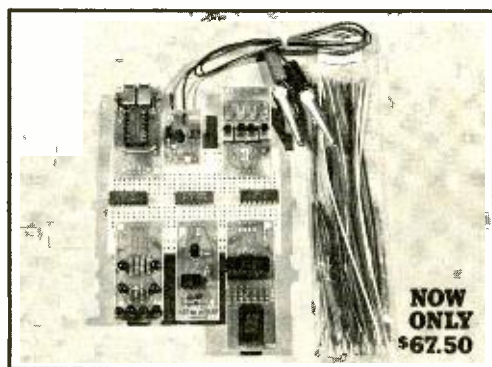
Sincere thanks to Marion R. Delfert, Bridgeton, MO, for this one.

PURPLE GREEN PIX

This RCA CTC-16 has a peculiar problem. On a B&W picture, it's purple with greenish highlights. Same on color programs. Tint and color controls have no effect at all. Voltage readings in the color difference amplifier section seem to be all right. Any help will be appreciated.—M.M., Whitestone, NY.

The crystal-ball says that your 3.58 MHz oscillator is probably dead! This will cause just such a set of symptoms in quite a few sets. The odd colors seem to be due to just a little bit of

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the burst getting through, which has a phase somewhere very close to blue-green. I have seen sets with this problem, on a color bar pattern, which looked just like a "no red at all" symptom!

TUBES WITH SPRING CLAMPS

To take 6BK4 or other tube out of an inaccessible place if it has the spring-clamps holding the base, just slide the cardboard roll out of a roll of bathroom tissue down over the tube. This will depress the clamps and the tube comes right out. Thanks to Frank Pisano, Staten Island, NY. In England, I guess this could be called a "Loo-Roll Loosener!" (Sorry about that!)

IGNITION NOISE ON FM

We've found that ignition noise on the FM band in 1970 Cadillacs can be caused by a crumbling of the material in the tower of the distributor cap. This has a carbon contact. When the plastic fails, the spring contact of the rotor rubs on a brass retainer in the cap tower generating the noise. Cure: try replacing both the distributor cap and rotor.

Thanks to H. Miller, Miller's Service, Oroville, CA. I thought that MGB's were the only cars that did this! Mine did. R-E

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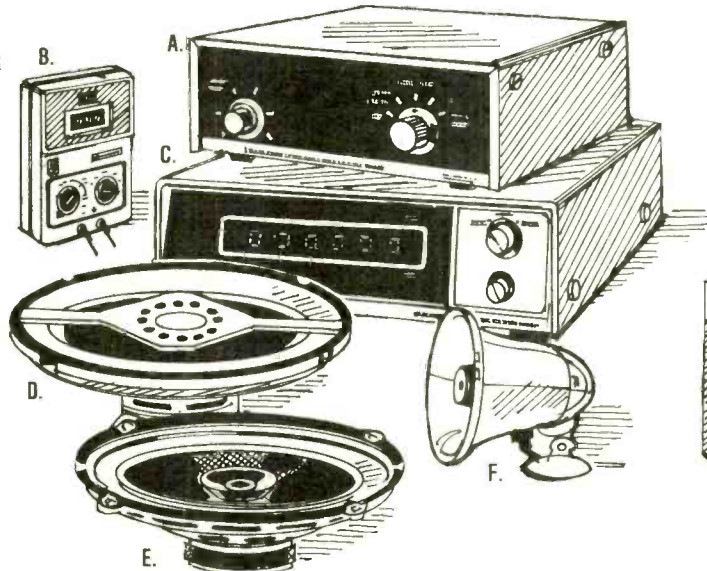
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EQUIPMENT REPORTS

(continued from page 30)

Interrupt vector locations are also on the 6530 chip. A programmed timer is the last major element which DEMON uses to time the terminal input pulses so it can automatically operate over a range of data transmission rates.

Then there is the PIA Peripheral Interface IC that adds 16 more input/output lines for a grand total of 26. Any of these can be configured as either inputs or outputs under the guidance of the programmer.

Four NMOS memory chips on the CPU board add 512 words of RAM which is on the whole available for user programs. A small part of this memory is used by DEMON. User RAM is assigned to the first 512 bytes of memory space from 0000

to 01FF. The rest of the IC's are terminal interfacing components and address decoding gates.

This effective hardware-firmware combination is supported by an apparent basic philosophy: Don't make a keyboard-display a standard CPU feature. Most serious users and even the beginner, once beyond the early phases of experimentation, will be using a data terminal. The terminal user is not saddled with the unnecessary expense of an unused feature. All bases will be covered since a keyboard-display board is under development for those who want to start out without a terminal.

The terminal interface has been designed to work with virtually any data terminal. Standard 20-mA teletype loops are handled by using an additional -10-volt supply; TTL terminals such as TV typewriters run with the single 5-volt supply. The third option, the one I used, is the

EIA interface that requires two additional supplies—+12 and -10 volts. These supplies are low current and in some cases can be tapped off the terminal itself. The only other real requirement is a SPST RESET switch. An additional MMI (Non-Maskable Interrupt) switch and debouncing circuit is a helpful add-on.

I encountered one minor problem when connecting the JOLT to my fairly sophisticated TI ASR733 terminal. I hooked everything up according to directions but the printer would not receive anything. Frankly, I suspected the microcomputer since it was the item I was least familiar with at that point. As it turned out I was missing an interconnect wire! My terminal has a data-carrier detector lead that an external modem uses to disable the printer. When a modem is not used, this pin must be tied to the DSR (Data Set Ready) lead on the JOLT board. As soon as I made

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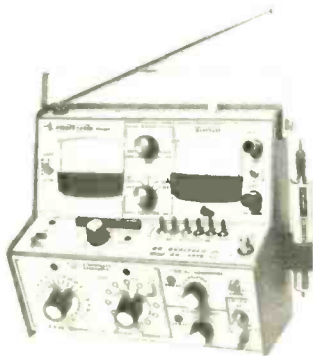
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TABLE 1—DEMONSTRATION PROGRAM

```

♦ 7052 30 40 FF 01 FF
.LH
NAMECHECK7
;180100A020A9338532205400A2008A4820E972A868AA989530CAC90A79
;1801180DD0F08A49FF8531E631A00EA95C8532205400A431A930D80B01
;10013038E5318532205400208A72004C0001700493
.
;1800304A0B250020204552454820454D414E2052554F592052455405E1
;1800484E4520455341454C50202020B13220C67288D0F86020554F08DC
;10006059204B4E414854200A0D200D0A11E11903D8
;0200F6000100F9
.G PLEASE ENTER YOUR NAME HERE JACK SPRAT
THANK YOU JACK SPRAT
♦ 013C 32 00 00 00 FF
.G PLEASE ENTER YOUR NAME HERE ABCDEFGHIJKLMNOPQRSTUVWXYZ
THANK YOU ABCDEFGHIJKLMNOPQRSTUVWXYZ
♦ 013C 32 00 00 00 FF
.M 0100 A0 20 A9 33 85 32 20 54
.M 0108 00 A2 00 8A 48 20 E9 72
.M 0110 A8 68 AA 98 95 30 CA C9
.M 0118 OD D0 F0 8A 49 FF 85 31
.M 0120 E6 31 A0 0E A9 5C 85 32
.M 0128 20 54 00 A4 31 A9 30 D8
.M 0130 38 E5 31 85 32 20 54 00
.M 0138 20 8A 72 00 4C 00 01 70
.M 0030 41 1B 15 00 20 20 45 52
.M 0038 45 48 20 45 4D 41 4E 20
.M 0040 52 55 4F 59 20 52 45 54
.M 0048 4E 45 20 45 53 41 45 4C
.M 0050 50 20 20 20 B1 32 20 C6
.M 0058 72 88 D0 F8 60 20 55 4F
.M 0060 59 20 4B 4E 41 48 54 20
.M 0068 0A 0D 20 0D 0A 11 E1 19
    
```

this connection, it took right off and worked perfectly.

Table 1 is an actual printout from my terminal. I had previously written a simple demonstration program called NAME-CHECK. Seven versions later it was finally debugged and running. About 120 words of memory are used for program and variable storage to perform an elementary task, but one that uses some interesting programming techniques. A program loop reads sequential addresses in memory for printout of text messages.

Tape, of course, is a tremendous convenience during the program development stage since it eases the job of reentering the program after power interruption or memory wipeout due to faulty program execution. My terminal has a dual tape transport built-in. I was not using an audio cassette option.

I turned on the power, pressed the RESET button and hit the carriage return key producing the first line of printout prefixed by the asterisk. DEMON measures the terminal transmission speed of the carriage return, sets some constants in memory, and echoes and transmits characters at the same rate. It adapts to speeds from 10 to 30 characters per second.

The first four-digit number is the program counter 7052 which is the next address following a BRK (break) instruction. In this case, the printout is caused by a BRK instruction in the monitor ROM at location 7051. The next number is the status condition that shows the settings of

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the various μ P flags such as the carry and interrupt flags. Next are the accumulator, the X and Y index registers and the stack pointer. The stack pointer always starts at the top of page zero at FF and decreases as the stack is filled.

The machine then printed out a period that is DEMON's prompting character telling me it is waiting for a command. The command list includes M for list memory, R for list registers, G for go, WH for write hexadecimal, WB for write binary, H for high speed reader, LH for load hexadecimal and a colon (:) for alter.

Ready to load my program, I typed LH after which the microcomputer issued a line feed and carriage return. I then started the cassette tape and fed in the next portion of the printout starting with NAME-CHECK7 and ending with the terminator -:00. The first two-digit number, 18, indicates there are going to be 18₁₆ or 24₁₆ sequential memory entries in that block. The following 0100 is the starting address where the first entry will be made. Excluding the last four characters, the rest of the line are the instructions and data in hexadecimal. The last four characters are the check-sum the computer uses for error checking. Disagreement between the computer's running count during data input and the check-sum at the end of the block causes a ? to be printed pointing out an error.

To make the program self-starting, I have included the starting address of my program on the tape. DEMON stores the program starting address in locations 00F6

and 00F7, hence the 0200F6000100F9. Using the previous format it says enter 00 at 00F6 followed by 01 at 00F7 which is the starting address 0100 in reverse order.

Now all I do is type the G command for go and the program prints out PLEASE ENTER YOUR NAME HERE and waits. Anything I type from that point on until the carriage return will be stored in memory within the space limitation I have left. So after I type JACK SPRAT, the program returns with its THANK YOU statement. A simple example that tells that things are really working. On the bottom of Table 1 is the memory printout using the M command to list the program in a more readable format. The first section of the program actually ends with the 01 at location 013E and the final "70" is just what happened to be in that memory word at system powerup. Likewise, the second block is terminated with the OD at location 0069 (the second 2-digit column in the 0068 row). Here the OD and OA in locations 006B and 006C are the results of a previous programming try. Incidentally, OD is the hexadecimal notation for a carriage return and that particular program element causes the carriage return just before the THANK YOU statement.

If the system does not have a cassette tape, the program is entered from the keyboard in an almost identical format to the memory printout. The only difference is that the alter command (:) replaces the M and you do the typing instead of the terminal.

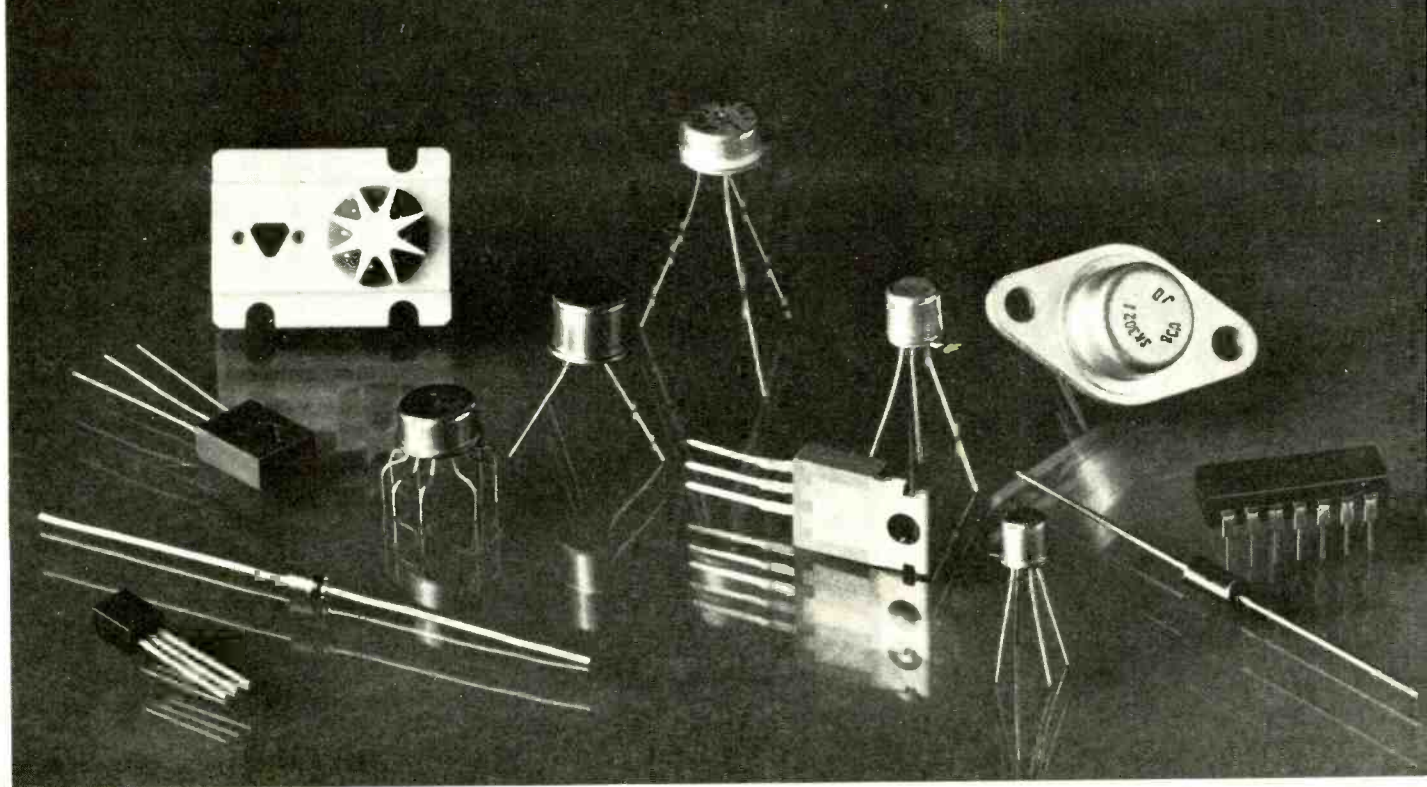
The subroutines in the monitor PROM

such as the character write and read, WRT and RDT routines are available to the programmer. For example, the write subroutine begins at address 72C6. The symbol to be printed is stored in the accumulator by a load accumulator instruction and then a JSR WRT (20 C6 72) prints the character. You can see this sequence in my program at locations 0056, 0057, and 0058 in the listing.

Inserting breakpoints using the break (00) instruction is a powerful debugging method. The break causes interruption of the program at that point followed by a register printout as shown in the first line of Table 1. Memory locations can then be examined with the M command. NAME-CHECK7 has a break instruction at location 013B (the fourth column in line 0138). The break is used to stop the program but the register printout is the same as if debugging were in progress. It is this instruction that causes the register dump at the end of the program execution starting with the asterisk and the program counter contents 013C.

As with other microcomputer kits, the assembly was straightforward and is mainly mounting IC sockets and bypass capacitors. Molex pins are used for economy. Good soldering technique is required and an experienced kit builder with a small clean iron should have no problems. A beginner should proceed a little cautiously and might seek the help of someone skilled in soldering. After assembly, use a magnifying glass to check for solder bridges, cold solder joints, and shorts be-

Now you can stock only 300 semiconductors instead of 112,000.



tween adjacent Molex pins.

One of the real nice things about the JOLT kit is that you are not left in the dark. Plenty of documentation is included in the package. The answer to your particular problem is probably somewhere in the supplied literature.

The two-volume MOS Technology manual is a \$10 option but one that I heartily recommend. It is a masterpiece. Standard documentation includes a JOLT CPU Assembly Manual, a JOLT CPU Hardware Manual, and a JOLT schematic diagram. JOLT Application Note no. 1 shows how to connect a terminal to the CPU and Application Note no. 2 provides tips on initial powerup and expansion of the system. The DEMON software manual is complete and includes a program listing with programmer's comments.

Interface boards, a power supply, and 4K RAM memories are already available. A single-pass resident assembler was recently announced. Under development are a keyboard/display board with an audio cassette interface and a TV interface board. Boards and complete systems can be purchased as kits or factory assembled.

Write for a JOLT brochure to Phaeo Corporation, JOLT Sales Agents, Micro-computer Associates, Inc., 111 Main Street, Los Altos, CA 94022. **R-E**

PC-76

5000 CB buyers, reps, and distributors filled the Las Vegas exhibition hall each of the first two days of the show. More than 200 manufacturers displayed their products.

12-MILLION VOLTS

(continued from page 34)

path by changing the primary coil frequency abruptly.

4. Reinforcement of the energy contained in the "ball."

Taking his conclusions and plans to Washington, D.C.—where more than one agency was interested in any research that might lead toward solving the problem of confining a dense highly heated plasma for thermonuclear applications—Golka succeeded in securing backing for the present Bonneville Flats installation.

The work is still in the early stages, but results are already promising. Golka has achieved voltage discharges up to 15 million (the highest yet made by man) for a period of 8 minutes, and "sparks" (or lightning bolts) rivalling the 20 to 30-footers attributed to Tesla. Already small discharges resembling ball lightning—with a life of about 0.1 second—have been observed.

This is a far cry from controlled nuclear fusion, yet there is more than a chance that—like Faraday's "new-born infant"—it may be the first step toward techniques that could have as great an effect on our future civilization as Tesla's development of alternating-current electricity has had on our present one. **R-E**

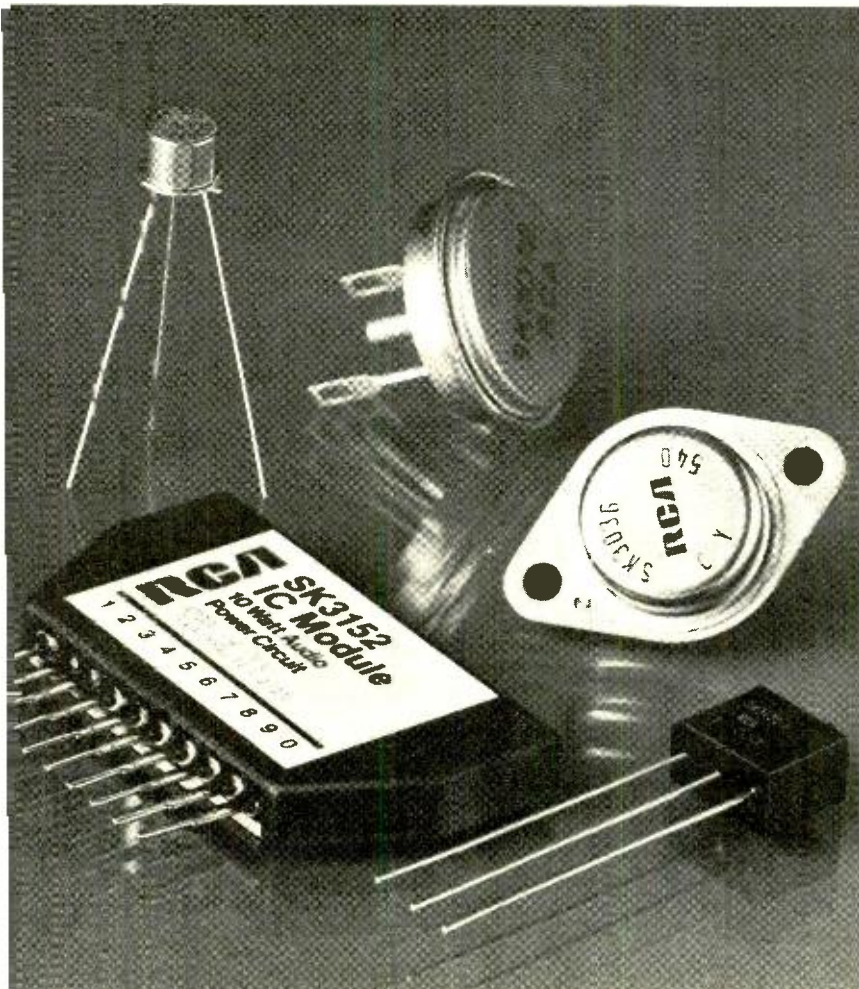
FUNCTION GENERATORS

(continued from page 58)

used with an amplifier having a frequency response less than the operating frequency of the generator, the user must be sure the correct waveform is employed. A triangle wave with some high-frequency attenuation is difficult to distinguish from a sine wave on an oscilloscope. At sufficiently high frequencies, a square wave will begin to look like a triangle wave.

With most generators it is easy to have the total peak voltage of the signal and the DC offset exceed the output capabilities of the generator's amplifier. When this happens, clipping will occur and a distorted waveform may be unknowingly created. When analysis shows clipping and DC offset is being used, suspect an error in setup.

As noted before, it is the opinion of this author and many others in the instrument industry that the function generator will soon completely replace the classical sine/square oscillator as the general-purpose laboratory and service signal source. At this time, the basic function generator has been well defined and the low-cost unit has started to make its way on the market. In the future, we should expect to see even more for the low-cost dollar. Increases in the high-frequency limits and greater continuous tuning range should be the major improvements to watch for. In any case, the simplest of function generators available today are a great improvement over the best sine/square oscillators. **R-E**



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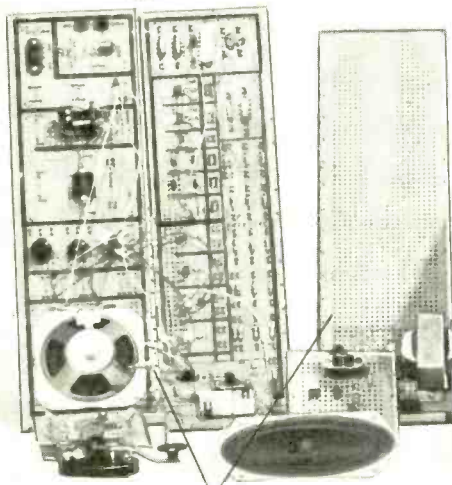
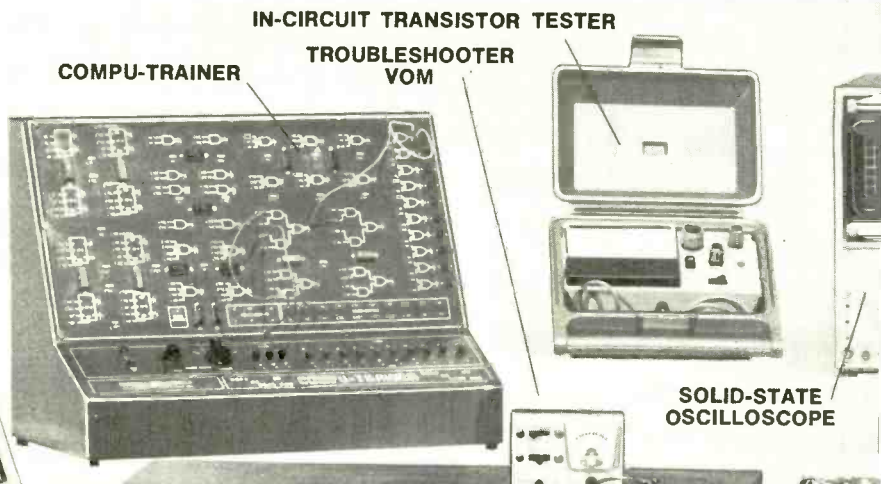
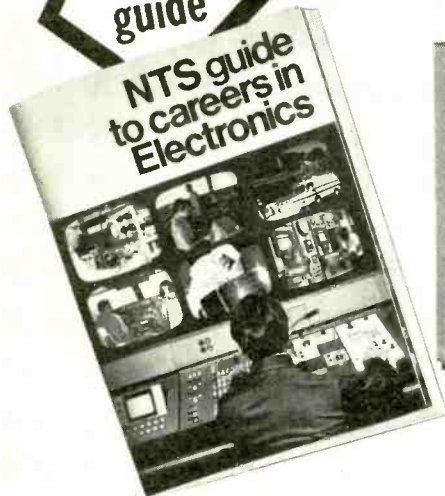
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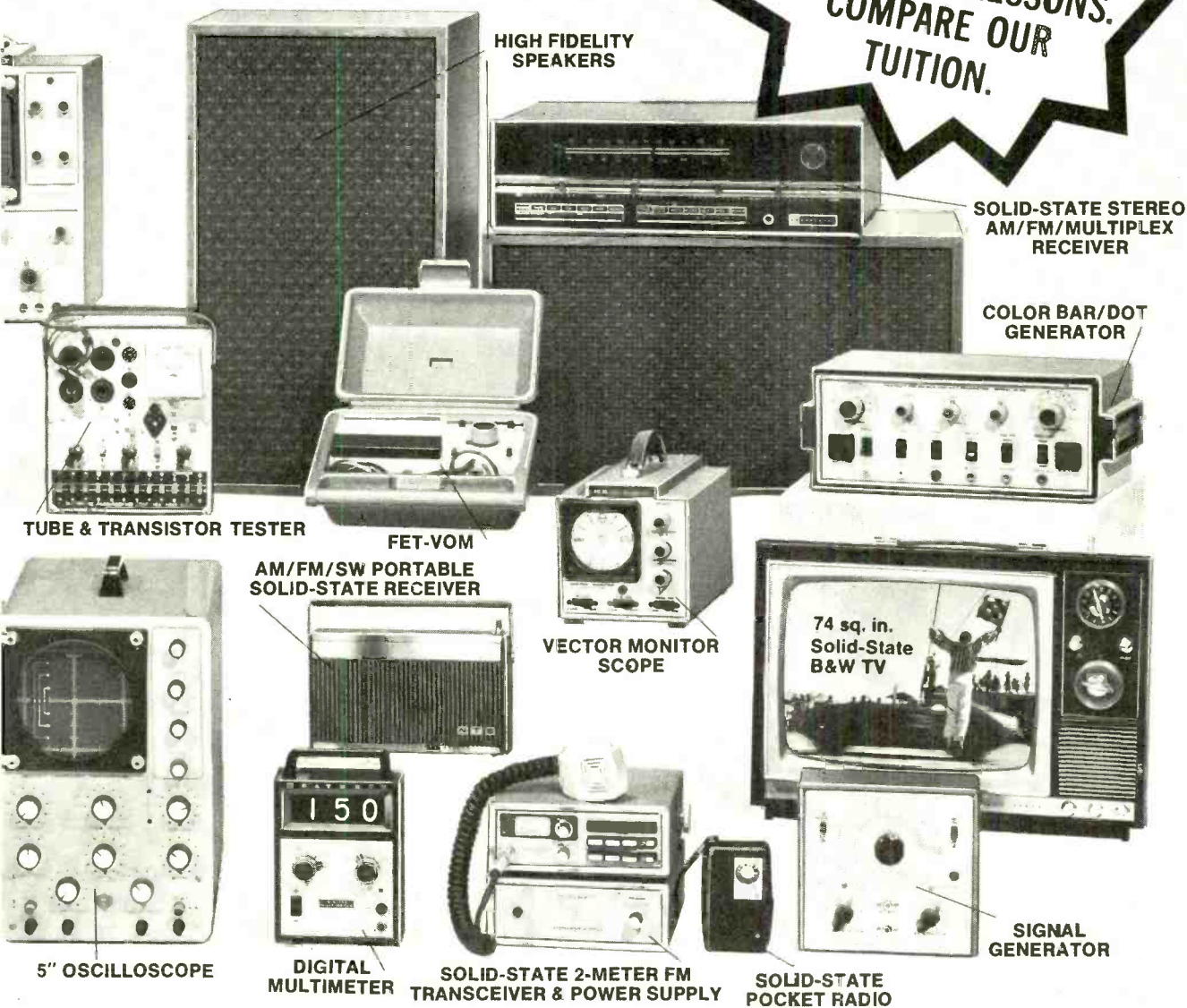
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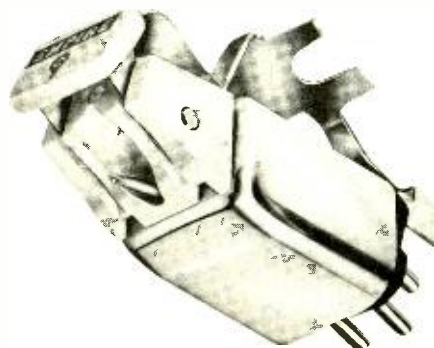
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Circle 119 on reader service card

new products

More information on new products is available from the manufacturers of items identified by a Reader Service number. Use the Reader Service Card inside the back cover.

VOM, model 60-NA, has 50 separate ranges for improved accuracy and versatility. Includes a large 4½" mirrored scale meter, DC accuracy of ±1½% of full scale value, AC accuracy of ±3%, plus a multiplier switch that permits more readings to be taken at the upper portion of the meter



scale for greater accuracy. Measures 0-1000 VDC in 16 scales. 0-1000 VAC in 10 scales, and DC current from 0-1000 mA in 10 scales. Five resistance ranges from ×1 to ×100K are provided in addition to a -20 dB to 52 dB range. AC current reading from 0-300 amps may be obtained by using a model 70-C AC adaptor with this unit. \$130.00.—**Triplet Corporation**, Bluffton, OH 45817.

Circle 31 on reader service card

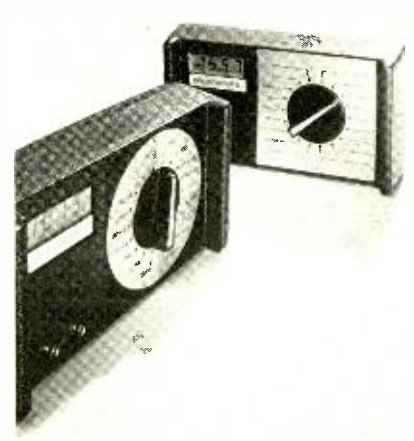
MICROPROCESSOR COMPUTER SYSTEM, model B6800, consists of a 500 character-per-minute heavy-duty printer, 42-character keyboard, tape reader, tape punch, card edge reader, card edge punch, central processing unit with memory, BEA-BUSS card extender, all cables, power supplies, and full documentation. The system can be set



up and be in operation in less than one hour. The model B6800 features up to 1 million non-memory accessing operations per second. Up to 64, 128 locations may be addressed in memory. Memory can be any combination of RAM, ROM, or PROM. Battery backup supply is available as an accessory. Memory can be expanded in 1K, 2K, 4K, 8K byte increments. Price \$1,250.00.—**Beacon Computer Corp.**, 3 Lexington Drive, Metuchen, NJ 08840.

Circle 32 on reader service card

DIGITAL MULTIMETERS, Danameter 200A and Danameter II 2100A, are two new 3½ digit multimeters for field or lab applications. Both feature a high-contrast LCD readout. DC voltage measurements from 1 mV to 1000 V, AC measurements from 1 mV to 1000 V peak, DC current capability from



10 nA to 2 A. Basic DC accuracy of the 2000A is 0.5%. DC accuracy of the 2100A is 0.25%. Both have 50-dB normal-mode noise rejection and 10 megohm input impedance. Powered by a 9V battery that will last for one year without recharging. Single control switch for easy operation.—**Dana Laboratories, Inc.**, 2401 Campus Drive, Irvine, CA 92713.

Circle 33 on reader service card

GUTTER MOUNT CB ANTENNA is ideal for beginning CB'ers. Simple to install on any vehicle rain gutter, the **INDEPENDENCE model 10-245** low-profile 27-MHz antenna



delivers plenty of talk power. Only 28 inches long, the top whip is a soft luster stainless steel and the base rod is brilliant chrome-

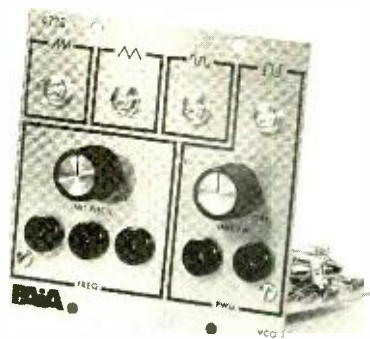
plated brass. The antenna may be mounted quickly with the corrosion-resistant, chrome-plated steel bracket designed for long wear and ample door clearance.

The whip includes a static arrester for ultra-quiet reception and has a pre-tuned heavy-duty ABS encapsulated center load coil for optimum efficiency over the entire class-D band. An auto-flex stainless steel spring relieves whip shock.

Allen wrench for fine tuning the antenna, plus a 10-foot coax cable with a PL-259 plug that mates with any standard SO-239 transceiver antenna receptacle... all for only \$22.95.—**Breaker Corp.**, Marketing Department, 1101 Great Southwest Parkway, Arlington, TX 76011.

Circle 34 on reader service card

VOLTAGE CONTROLLED OSCILLATOR KIT, model 4720, features simultaneous ramp, triangle, sine and pulse/squarewave outputs; manually-set or voltage-controlled pulse width and 16 Hz to 16 kHz frequency response corresponding to 5 volt peak control voltage. Front-panel range control allows multiple oscillators to be offset and track one another chromatically over the entire operating range. A self-zeroing front-end and active on-board voltage regulation make the 4720 extremely linear and stable.

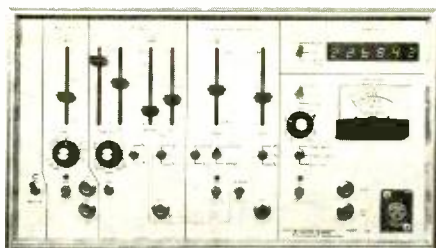


Although designed as a wide range voltage controlled oscillator for electronic music synthesizer applications the 4720 is useful as a signal generator for the test bench, an audio sweep generator for testing frequency response in amplifiers, tape recorders and other audio gear and can be applied to narrow-band frequency analysis of system equalization or room acoustics.

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PLASTIC-BLADE WIRE STRIPPER uses space-age plastic Stilan® blades with cutting edges harder than insulation, but softer than copper. This enables them to strip the insulation from wire or cable without any damage to the conductors and without separating them. The new hand wire stripper removes the insulation from twisted pairs, multi-conductor cable, ribbon cable, twin-lead antenna wire, electrical cable, automobile wiring, lamp cord and telephone wires, just as quickly and easily as it does from ordinary hook-up wire, all without separating the conductors. The *Plastic-Blade Stripper* strips at least 25% faster than manual models using steel blades. The new stripper offers these advantages over models with metal blades: The wires being stripped do not have to be carefully positioned between the stripper blades. Also, a number of different wires can be stripped at the same time. This stripper requires no adjustment for wire sizes, type, or number of conductors.



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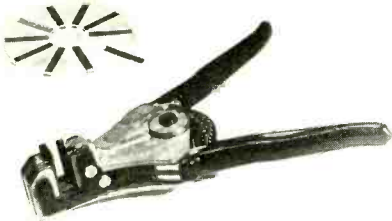
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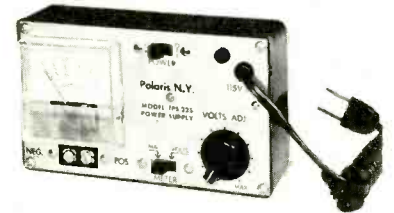


amplifier, and an unusual C/MOS output stage all on the same chip.

"Milli" comes complete in kit form with everything except battery and output lead connectors to fit your voltmeter. Available only by mail (Model P-1, \$11.95 plus \$1.00 for shipping and handling).—Dage Scientific Instruments, Box 1054, Livermore, CA 94550.

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Circle 38 on reader service card

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TV MODULE REPAIR SERVICE. Same-day service is being offered on repair of Zenith, RCA, Quasar and G-E modules at this time with plans for adding additional lines in the near future. Each module undergoes stringent testing and temperature cycling after repair and alignment to insure proper operation of module. All modules carry a one-year warranty. Repair price is \$5.95 to \$12.50 depending on type of module.—PTS Electronics, Inc., 5233 South Hwy #37, Bloomington, IN 47401.

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923332	208 (assem.)	872	8 (16's)	8	2	4 1/4 x 5 1/4	28.95		
923334	201-K (kit)	1032	12 (14's)	2	2	4 1/4 x 7	24.95		
923331	212 (assem.)	1224	12 (14's)	8	2	4 1/4 x 7	34.95		
923326	218 (assem.)	1760	18 (14's)	10	2	6 1/2 x 7 1/2	46.95		
923325	227 (assem.)	2712	27 (14's)	28	4	8 x 9 1/4	59.95		
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TV GAMES

(continued from page 35)

and speed. Then that player must hit the ball again or lose a point to his opponent.

The second challenge occurs whenever the ball touches the top or bottom of the bumper cube. Instead of rebounding, the ball enters the cube . . . and then after a brief random interval comes flying out. Both the path and speed of the ball are controlled by the randomizing integrator circuit. Also the ball may be angled from the bumper toward either player.

Look at the circuitry

The entire schematic for this game (with the exception of the scoring circuit) is shown on pages 36 and 37. The game provides a complete video image. It also generates the vertical and horizontal sync pulses necessary to provide a raster on the

IC1. The frequency of the vertical sync is determined by the combination of R2 and R43 and C2. Similarly, the horizontal sync frequency is determined by R1, R44 and C1. For long-term frequency stability both C1 and C2 are specially selected for their low temperature coefficients.

The outputs of both 555's are used to provide the required tuning signals within the game. Sync for the TV set is provided through IC8-c which is used as an OR gate to combine the vertical and horizontal sync pulses. IC8-c's output goes to the video combiner, IC5-c. This circuit will be discussed later. A vertical sync pulse defines the beginning of a TV frame, and a horizontal sync pulse defines the beginning of each line.

The vertical and horizontal sync signals are used to generate vertical and horizontal ramp signals. These are then used to provide position reference signals for

PARTS LIST

All resistors 1/4-watt 5% unless noted

R1, R2, R9, R57, R77, R78, R80, R81, R82, R83—5000 ohms, trimpot
R3, R45—2000 ohms
R4, R7, R10, R12, R16, R19, R21, R24, R25, R28, R30, R52, R64, R70, R74—1000 ohms
R5, R6, R13, R20, R22, R23, R27, R32, R42, R54, R58—10,000 ohms
R8, R17—15,000 ohms
R11, R26, R60—47,000 ohms
R14, R15, R18, R29, R31, R39, R40, R41, R48, R53, R56, R71—5100 ohms, R33—3.3 megohms
R34, R65, R66, R68, R69, R76—470,000 ohms
R35, R38—1000 ohms, trimpot
R36, R37, R47, R61, R73—510 ohms
R43—20,000 ohms nominal (V sync)
R44—30,000 ohms nominal (H sync)
R46—15 ohms
R49, R59, R62—100,000 ohms
R50, R51—75,000 ohms (or 68,000 or 82,000 ohms)
R55, R72—200 ohms
R63—50,000 ohms, trimpot (or 100,000 ohms, trimpot)
R67—Not used
R75—1200 ohms
R79—1000 ohms, optional, see text
R84, R85, R86, R87, R88—5000 ohms, potentiometer linear taper (or any value between 5000 and 25,000 ohms)

All capacitors 15 volts or more

C1—2000 pF, temp stab polystyrene
C2—1.0 or 1.2 μ F, temp stab tantalum
C3—0.2 μ F, dipped tantalum
C4—not used
C5, C14, C33, C42—10 μ F, axial
C6, C32—1000 μ F, radial
C7—.001 μ F
C8, C18—0.1 μ F, dipped tantalum
C9, C35, C36—270 pF
C10, C12, C44, C47, C48—1 μ F, axial

C11, C13, C19—500 pF or 470 pF
C15, C16—0.47 μ F, dipped tantalum
C17—1 μ F, dipped tantalum
C20, C22, C23, C24, C38, C39—.01 μ F
C21, C26, C27, C28, C29, C30, C31—.05 μ F
C25—not used
C34, C37—100 pF
C40, C41, C46—.005 μ F
C43—2.2 μ F, dipped tantalum
C45—100 μ F, radial
C49—6.8 μ F, tantalum
C50—not used

Diodes

D1 to D8—1N4148 (or any signal diode)
D9 to D12—not used
D13 to D23—1N4148 (or any signal diode)
D24, D25—1N4148 (optional for low-resistance joystick)

Transistors

Q1 to Q6—2N2222

Integrated Circuits

IC1, IC11, IC26—555
IC2—7404
IC3, IC7, IC8, IC14, IC15, IC18, IC19—7400
IC4, IC6—339
IC5—7402
IC9, IC22—74C74
IC10, IC17—7474
IC12—4066
IC13—7423
IC16—7420
IC20—74C90
IC21—74C00
IC23, IC24—74C04
IC25—74C10
IC27—LM309 (5v, 1A regulator)

Switches

S1—spst toggle
S2, S3—spdt toggle
S4—spst N.O. momentary push button
SPKR—4 to 8 ohms, 2 1/4 inch diameter

TV screen. You should think of this game as having eight separate functional areas. These are the vertical and horizontal sync, paddle circuits, playing field circuits, ball circuits, hit-and-miss circuits, audio, scoring, and video.

The vertical and horizontal sync pulses are generated by two 555 IC times (IC26 and IC11). The vertical sync frequency is generated by IC26, the horizontal sync by

the paddles, ball and both boundaries. The vertical ramp is generated by transistor Q1 and its associated components. The vertical sync pulses from IC26 are inverted by IC2-b and fed via R7 and R8 to the base of transistor Q1.


At the beginning of a frame, Q1 is momentarily turned on by the inverted vertical sync pulse, bringing the vertical ramp (continued on page 80)

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signal to 0 volts. The ramp voltage then rises as Q1 is switched off and capacitor C3 charges through R5, R8 and R7. The output of IC26 is at ground during this period.

The horizontal ramp circuit operates in a similar manner with a separate but rather identical circuit. Thus for each TV frame, the vertical ramp makes one complete cycle and, for each TV scan line, the horizontal ramp makes one complete cycle.

The following items are available from Visulex, P.O. Box 4204, Mountain View, CA 94040

Main circuit board, with pre-aligned horizontal and vertical sync oscillators soldered in place. Includes circuitry (but not components) for ball, paddle and boundary display, sound effects, computer-control module, paddle size selector, ball speed/angle randomizer, game action electronics for bumper and power filters. Order Kit MB-3: \$29.50

Component kit for main board. Contains all additional ICs, IC sockets, transistors, resistors, diodes, trimpots and 5V regulator Order kit MBK-3: \$48.50

Assembled and tested main board. Order MBA-3: \$105.00

On screen scoring circuit board, including LSI character display generator IC. Order kit SB-3: \$18.75

Component kit for scoring board contains all additional ICs, IC sockets, resistors, capacitors, diodes and trimpots. Order kit SBK-3: \$20.50

Assembled and tested scoring board. Order SBA-3: \$55.00

Accessory kit contains parts for external game control. Includes paddle potentiometers for horizontal and vertical motion, 6-wire cables for remote use of paddle motion potentiometers, paddle size potentiometer, switches for computer control and game selection, score reset push button, speaker and hook-up wire, knobs. Order kit AK-3: \$25.75

Power supply, 12 volts DC. Powers the entire game including scoring module. Order kit PS-3: \$8.70

Cases. Including main cabinet plus remote player control boxes. Order kit CC-3: \$22.50

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The playing field is comprised of the top and bottom boundaries and the centerline. The centerline is generated by three sections of IC14 (a, b and c), C18, C19, and R36. Control R35 sets the position of the



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centerline. IC14-a, IC14-b, C18, and R35 form a one-shot multivibrator, whose period is approximately 30 microseconds. This is approximately one-half the horizontal sync interval. It is triggered by the horizontal sync. Thus for each line, a 30- μ s pulse is generated. The trailing edge of this pulse is coupled through C19 and is inverted by a IC14-c to produce a very narrow low-going pulse, which is the centerline.

Since this occurs approximately midway between the horizontal sync pulses, the resulting signal, when displayed on the screen, will be at the center.

The top boundary is generated in a manner similar to the bottom boundary with one major exception; the sense of the comparator is reversed so that the output at pin 13 of IC4-c goes high when the vertical ramp voltage reaches the reference voltage. Resistor R57 supplies the fixed voltage and determines the height of the bottom boundary. The bottom boundary signal is also used to control the ball rebound. This will be described a bit further on.

The paddles

The paddles are generated by four comparator circuits, two in IC4 (a and b) and two in IC6 (a and b), and their associated logic networks. For each paddle there are two comparators. One is used to position the paddle vertically, the other horizontally. Since both paddles are generated in an identical manner only one will be discussed.

Each paddle is produced by comparing the voltages on the external vertical and horizontal player potentiometers with the vertical and horizontal ramps, respectively. When we look at the left paddle, the horizontal player potentiometer voltage is applied to pin 4 of IC4-a and the vertical voltage to pin 5 of IC6-a.

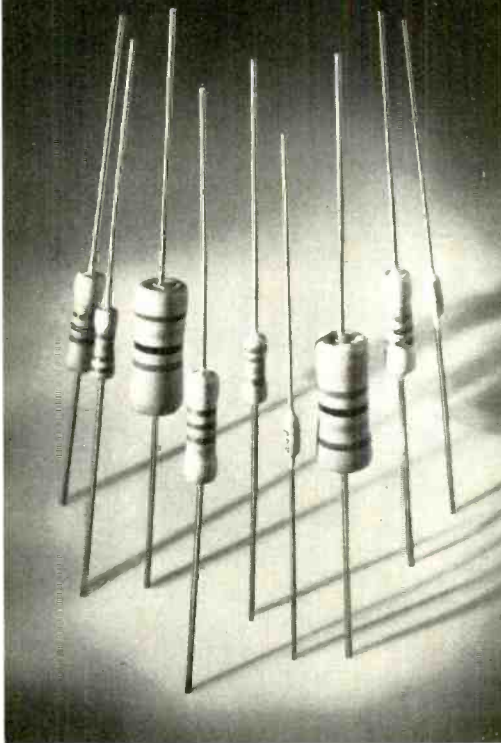
When the voltage of the horizontal ramp equals the voltage on pin 4 of IC4-a, the output at pin 2 of IC4-a goes high. The leading edge of this high-going pulse is differentiated by C11-R21 and is inverted in IC3-a, delivering a narrow negative-going pulse at pin 9 of IC5-a. This pulse appears at every scan line and gives the horizontal position of the paddle.

However, we must still determine the vertical position of the paddle. This is done by the other comparator, IC6-b. The sense of this comparator is reversed so when the vertical ramp voltage reaches the vertical player potentiometer voltage, the output from pin 2 of IC6-a goes low. This low-going signal is differentiated by C15 and R29 giving a negative pulse at pin 8 of IC5-a. The two negative pulses, at pin 8 of IC5-a and pin 9 of IC5-a, are ANDed by IC5-a to produce a series of positive pulses on output pin-10 of IC5-a. These pulses occur at the horizontal sync rate and comprise a total paddle signal. It is displayed on the screen via IC13 and is also used to determine a ball hit.

Paddle height is determined by the width of the output pulse at pin 2 of the vertical comparator IC6-a. The height of the paddle is controlled by varying the width of the pulse on pin 8 of IC5-a.

Still to come: completion of how it works, the foil patterns, component placement diagram and assembly procedure. **R-E**

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See your RCA Distributor for all the details, or write to RCA Distributor and Special Products Division, Sales Promotion Services, Cherry Hill, NJ 08101.

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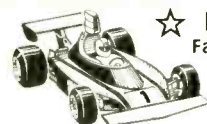
★ No Breaker-Points or Condenser to EVER wear out or need any maintenance.



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● The Allison OPTO-ELECTRIC System ELIMINATES the Points and Condenser, replacing them with an OPTO-Electronic Trigger, using a Light-Emitting Diode and Phototransistor. This System operates on a BEAM of LIGHT. There is NO "Breaker-Point Wiper-Arm" to wear down. Point bounce and erosion are completely eliminated thereby giving longer Timing ACCURACY than any System using "Mechanical" Breaker-Points (and No Timing Fluctuation as with Magnetic Impulse Units). ACCURATE Timing gives the BEST in Engine EFFICIENCY, and that's the name of the Game for the BEST in GAS MILEAGE and ECONOMY.



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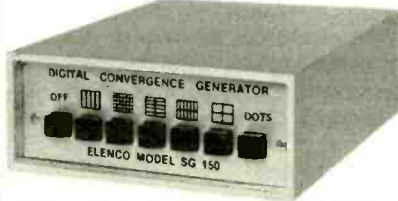
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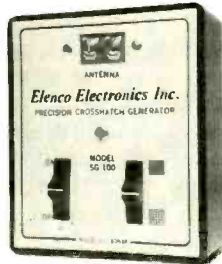
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HI-FI TEST GEAR

(continued from page 47)

Spectrum analysis

We mentioned earlier that it is possible to gain some information regarding the makeup of harmonic distortion by observing the distortion components themselves on an oscilloscope. A much more powerful tool for this purpose is a separate audio-spectrum analyzer. While such analyzers are relatively expensive, you can actually display separately the individual harmonics that constitute the total harmonic distortion figure. A spectrum analyzer also permits more detailed examination of residual noise in audio products, rapid visual plotting of frequency response, tone control action, filter response and a host of other frequency versus amplitude characteristics not possible to observe in detail with the rest of the equipment already discussed. Examples of the use of a spectrum analyzer may be found in any of the **Radio-Electronics** Hi-Fi Equipment test reports, including those in this issue.

In this article we have highlighted only the major items that go into a properly equipped audio test facility. Enterprising and innovative test equipment manufacturers constantly introduce a variety of test equipment designed to make the audio tester's job easier and more accurate. We could have included a good deal of additional equipment, but have limited this discussion to the basics. Even so, it's pretty obvious that today's better audio equipment requires test procedures and test equipment that is at least as sophisticated and complex as the products we are trying to measure and service. **R-E**

**Veteran Wireless Operators
Present awards to five**

The Lee deForest Gold Medal Audion Award of the Veteran Wireless Operators Association (VWOA) was presented this year to Francis T. Cassidy, president of the United States Transmission Systems, a subsidiary of ITT. The award was granted for "a quarter century of dedicated research and development work in the field." Mr. Cassidy holds a number of patents in communications, including the patent for the channel combiner and divider system for automatic alternate voice and data communications.

The Marconi Memorial Gold Medal of Service was given to John McKenna, president of RCA Service Operations, and to Lt. Commander Russell A. Langdon (USN Retired). The Marconi Memorial Gold Medal of Achievement went to William A. Leonard II, radio and TV broadcasting executive of the Columbia Broadcasting System (CBS). The Marconi Gold Medal of Honor went to Arthur C. Goodnow for research and development of broadcast transmitters.

Wrist-watch pulse detector provides digital readout

A new opto-electronic transducer is expected to make it possible to provide a digital watch readout of human heart-beat rates. Invented by an Englishman, Commander Thomas Orr, the transducer is a light-emitting diode (LED) mounted in the center of an annular thin-film photovoltaic detector. Light from the LED penetrates the skin into the blood-rich



THE ORR HEARTBEAT TRANSDUCER consists of a light-emitting diode surrounded by a ring-shaped photovoltaic detector. The whole is designed to fit on the back panel of a standard wrist watch.

tissue. Part of the light—modulated by changes in light absorption by the blood resulting from the arterial pulse—is reflected back to the detector. The electrical signal thus produced can then be

electronically processed and the pulse rate displayed or recorded.

The developers of the device, International Research and Development Co. of Newcastle, England, plan development of a counter that can be interfaced with a digital watch module for a digital wrist-watch readout.

RCA introduces new, fast, low-cost microprocessor

RCA has introduced the CDP1802 microprocessor, a chip measuring less than 0.2 x 0.25 inch (5.08 x 6.35 mm) and containing about 5,500 transistors. It is less than half the size of RCA's earlier microprocessor. The reduction in size was achieved by technical advances in processing, which also made it possible for the chip to execute calculations in less than 2.5 microseconds—a cycle time comparable to speeds of any MOS microprocessors currently offered.

The same technical advances have also resulted in significant cost reductions, making possible a price of less than \$25 in quantities of 100.

The power required is low, making it feasible to run a complete microprocessor system on batteries. This single microprocessor chip, in conjunction with solid-state memories and other peripherals selling in total for probably less than \$100, can now perform the same functions as some of the large computers that sold for tens of thousands of dollars less than 10 years ago.

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<input type="checkbox"/> 3—ZENITH VIDEO	2 ⁰⁰	<input type="checkbox"/> HIGH VOLTAGE POWER TRANSISTOR Equip. IIEP 707 ... List price \$16.00	2 ²⁹
<input type="checkbox"/> AMPLIFIER PART #121-743	1 ⁰⁰	<input type="checkbox"/> 1—VARCO STEREO CARTRIDGE Model TN4B with holder	2 ⁹⁵
<input type="checkbox"/> 2—SILICON NPN TRANSISTOR IIEP-80015 ... List \$1.75	1 ⁰⁰	<input type="checkbox"/> 2—ELECTROLYTIC CONDENSERS 50/100/50 MFD—150V	1 ⁰⁰
<input type="checkbox"/> 1—SILICON NPN TRANSISTOR (SK3534—IIEP 85004)	1 ⁰⁰	<input type="checkbox"/> 2—ELECTROLYTIC COND 200/30/4—mfd—350V	1 ⁰⁰
<input type="checkbox"/> 5—ZENIER DIODE	1 ⁰⁰	<input type="checkbox"/> 3—ELECTROLYTIC COND 100 mfd.—100V, 50 mfd.—75V	1 ⁰⁰
<input type="checkbox"/> IN1757A ... 1 Watt—50 V	5 ⁹⁵	<input type="checkbox"/> 2—ELECTROLYTIC COND 40 mfd—500V, 40 mfd—100V	1 ⁰⁰
<input type="checkbox"/> ZENITH SILICON STICK REC-TIFIER PART #103-215—45K PIV. also used in Electrohome, Motorola, E.D.I.	5 ⁹⁵	<input type="checkbox"/> 8—MINI PILOT BULBS With 8' Leads—6.3V 30MA (5000 Hrs)	1 ⁰⁰
<input type="checkbox"/> POWER TRANSFORMER (PT-48)—110V Pri.,—12V Sec. Used in many transistor Power supply	2 ²⁹	<input type="checkbox"/> 8—MINI PILOT BULBS With 12' Leads—6.3V, 150MA (5000 Hrs.)	1 ⁰⁰
<input type="checkbox"/> COMPLETE CONVERGENCE ASSY.—Inc. Yoke, Board & Plug Conn. Adaptable to most 90° sets	3 ⁹⁵	<input type="checkbox"/> 32—TEST PROD WIRE DELUXE QUALITY red & black	1 ⁰⁰
<input type="checkbox"/> COLOR DELAY LINE—Used in most color sets	1 ⁶⁹	<input type="checkbox"/> 1—COLOR POWER TRANSFORMER	6 ⁹⁵
<input type="checkbox"/> Silicon NPN HV TRANSISTOR RCA—SK-3021—IIEP-240	1 ⁰⁰	<input type="checkbox"/> 2—Colorburst Quartz-Crystal For most color TV sets 3579.545 KC	1 ⁸⁹
<input type="checkbox"/> RCA—SK-3026—IIEP-241 Transistor Specials—Your Choice SK3006, SK3018, SK3020 SK3122, SK3124	1 ⁰⁰	<input type="checkbox"/> 5 ASST GLOBAL VARISTOR Popular replacements for most COLOR TV	1 ⁰⁰
<input type="checkbox"/> Transistor Specials—Your Choice SK3009, SK3024, SK3040	1 ⁹⁸	<input type="checkbox"/> COLOR-TV RECTIFIER—Used in most color sets—500 kv 3 for	1 ⁹⁵
<input type="checkbox"/> WAHL-CORDLESS SOLDER IRON Complete with Auto Charger-Fast Heating-Compact	17 ⁹⁵	<input type="checkbox"/> 4—TV ALIGNMENT TOOLS #1 finest popular selection	1 ⁰⁰
<input type="checkbox"/> ZENITH TRIPLER PART #212-109 Equivalent to EG4501—33KV Out., 25000F	3 ⁹⁵	<input type="checkbox"/> For Color TV #2	1 ⁴⁹
<input type="checkbox"/> REPLACEMENT DIGITAL CLOCKS Fits—RCA, Zenith, Philco, Etc.	17 ⁹⁵	<input type="checkbox"/> 6—TV COLOR ALIGNMENT TOOLS Most popular type	2 ⁷⁹
<input type="checkbox"/> 6" UNIVERSAL SPEAKER Top quality Special Buy EA.	1 ⁵⁹	<input type="checkbox"/> TV TWIN LEAD-IN 300 ohm 500'—\$7 100'—\$1.50, 50' 250'—\$10, 100'—\$4.50, 50'	1 ⁰⁰
<input type="checkbox"/> 10"—UNIVERSAL SPEAKER Large Magnet—Top quality	4 ⁹⁵	<input type="checkbox"/> CO-AX CABLE RG59U (Black) 250'—\$10, 100'—\$4.50, 50'	2 ⁶⁹
<input type="checkbox"/> 8" UNIVERSAL SPEAKER Large Magnet—Special Buy	2 ⁹⁹	<input type="checkbox"/> 5—DUAL DIODE—MOST POPULAR TYPES Common cathode or Series connected	2 ⁵⁰
<input type="checkbox"/> 2 1/2"x4" SPEAKER Special Buy 10 for \$5 EA.	69 ⁹⁵	<input type="checkbox"/> 15—DIPPED MYLAR CAP. .01—600V	1 ⁰⁰
<input type="checkbox"/> 4"x6" "QUAM" 16 OHM SPK. Large magnet... Special Buy 110 for \$15.00	1 ⁷⁹	<input type="checkbox"/> 15—DIPPED MYLAR CAP. .033—600V	1 ⁰⁰
<input type="checkbox"/> 8"—HEAVY DUTY 10 OZ. SPEAKER Ceramic Type—8 Ohm	4 ⁵⁰	<input type="checkbox"/> 15—DIPPED MYLAR CAP. .0033—1000V	1 ⁰⁰
<input type="checkbox"/> 1—8"x9" Heavy Duty 10 oz. Speaker Ceramic Type ... 8 Ohm	4 ⁵⁰	<input type="checkbox"/> 15—DIPPED MYLAR CAP. .047—400V	1 ⁰⁰
<input type="checkbox"/> 3—ELECTROLYTIC CONDENSERS. 100/80/20 MFD—500 Volts	2 ⁰⁰	<input type="checkbox"/> 15—Molded Tubular Capacitors .056—400V	1 ⁰⁰
<input type="checkbox"/> 5—Top Brand Silicon RECT. 1 amp., 1000 PIV	1 ⁰⁰	<input type="checkbox"/> 15—DIPPED MYLAR Condensers .0039 400V	1 ⁰⁰
<input type="checkbox"/> RCA 110° FLYBACK TRANSFORMER. For Blk. & Wht. sets —18KV—For all types TV's, inc. schem. 3 FOR 10.00	3 ⁹⁵	<input type="checkbox"/> "COMBINATION SPECIAL" RCA 110° FLYBACK AND 110° DEFLECTION YOKE	6 ⁹⁵
<input type="checkbox"/> 110° TV DEFLECTION YOKE for all types TV's incl schematic	4 ⁹⁵	<input type="checkbox"/> 90° FLYBACK TRANSFORMER for all type TV's (Blk. & Wht.)	2 ⁹⁵
<input type="checkbox"/> 70° FLYBACK TRANSFORMER for all type TV's (Blk. & Wht.)	2 ⁰⁰	<input type="checkbox"/> 70° TV DEFLECTION YOKE for all type TV's (Blk. & Wht.)	2 ⁰⁰
<input type="checkbox"/> OLYMPIC & SHARP FLYBACK Part #SFT392 Equip. Stancor #110-408—Thordarson #Fly339	2 ⁰⁰	<input type="checkbox"/> 90° COLOR YOKE For all Rectangular 19 to 25" Color CRT's	7 ⁹⁵
<input type="checkbox"/> 70 COLOR YOKE For all round color CRT's	5 ⁹⁵	<input type="checkbox"/> DELMONICO HV COLOR FLYBACK Part #A20411-B	7 ⁹⁵
<input type="checkbox"/> WESTINGHOUSE FM TUNER #476-K-915D9 Transistor	3 ⁹⁹	<input type="checkbox"/> WESTINGHOUSE FM TUNER (12D78 Tube)	1 ⁰⁰
<input type="checkbox"/> UHF TUNER—Transistor Type Used in all TV sets	2 ⁹⁵	<input type="checkbox"/> G.E. UHF TUNER—TRANSISTOR TYPE Model #85N4	3 ⁹⁵
<input type="checkbox"/> G.E. UHF TUNER—TRANSISTOR TYPE Model #T94C441-3 (Transistor)	7 ⁹⁵	<input type="checkbox"/> WELLS GARDNER TUNER Part #7A 120-1 (4GS7-2HA7 Tubes)	7 ⁹⁵
<input type="checkbox"/> G.E.—TV TUNER (2GK5-4LJ8) Model #EP 86211	7 ⁹⁵	<input type="checkbox"/> PHILCO UHF/VHF TUNER Transistorized	9 ⁹⁵
<input type="checkbox"/> 100' GREY SPEAKER WIRE 2 Cond., mini zip, 101 uses	2 ⁰⁰	<input type="checkbox"/> UNIVERSAL TV Antenna Back of set mounting... 5 section rods	2 ⁹⁹
<input type="checkbox"/> BLUE LATERAL Magnet Assy. Replacement for most color TV's	1 ⁷⁹	<input type="checkbox"/> 5—10K—2 WATT BIAS SPOTS Used in solid state application	1 ⁰⁰
<input type="checkbox"/> COLOR CONVERGENCE ASSY. Universal type—good for most sets	2 ⁴⁹	<input type="checkbox"/> 3 SPEAKER—7 WAY SELECTOR SWITCH Wall Mount	1 ⁰⁰
<input type="checkbox"/> TUBE AM-FM STEREO AMPLIFIER CHASSIS. Completely assembled—with tubes AS IS needs slight adjustments	9 ⁹⁵	<input type="checkbox"/> 10—MINI ELECTROLYTIC Cond 100 For Transistor & miniature work for safe delivery at minimum cost.	1 ⁰⁰

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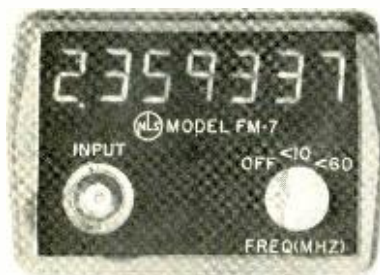
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BUILD A COMPUTER

(continued from page 44)

many more IC's, but it takes relatively few software steps.

The software routines at POINTD, POINTE, POINTF and POINTG make up what is called a command decoder. The software decodes the key-switches into real actions. Depressing

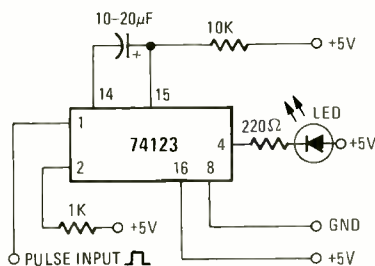


FIG. 6—MONOSTABLE-LED circuit is used for check-out of the Dyna-Micro.

0	1	2	3
4	5	6	7
H	L	G	S
R	A	B	C

FIG. 7—KEYBOARD LEGENDS are oriented as shown.

H or L causes the data temporarily stored in the 8080A as numeric key inputs to be output to either the HI or LO set of LED's. The S key causes the current or new data to be put back into the current memory location. Depressing G causes the computer to use the HI and LO address as the starting point for a new program.

The TIMOUT and KBRD software subroutines have specific tasks. The TIMOUT will count its way through various loops for about 10 milliseconds, while the KBRD subroutine will input a code from the keyboard. The KBRD subroutine has some unique features that illustrate an interesting hardware-software tradeoff. The keyswitches used in the Dyna-Micro are not bounce free, so that when the switches are opened or closed, they can often re-make or re-break the contacts. This can be confusing to the computer since it can't distinguish between a real switch closure and a bounce. We don't want

A user's group has already been formed for the Dyna-Micro. Interested people should contact:

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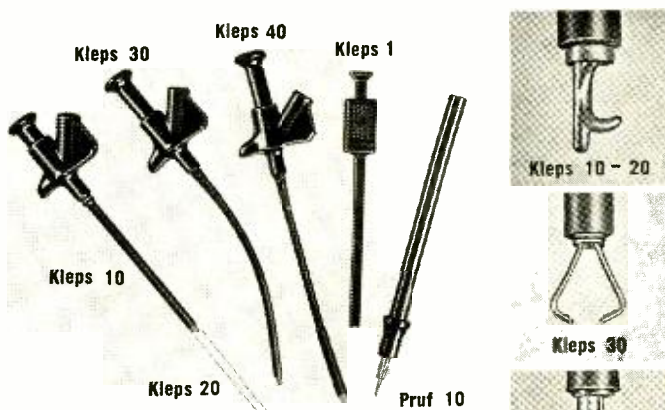
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Circle 82 on reader service card

WE GOOFED

WE SURE DID! Last month we ran the first part of this construction article on the Dyna-Micro and we erred. It seems that one or more gremlins (little green people) found their way into our editorial offices and stole—that's right, stole—74 lines of text from the article. The text was stolen between the last paragraph on page 36 and the opening paragraph on page 74. To correct this evil crime, we are reprinting the two paragraphs in italics along with the missing text. To prevent this from happening again, we have tightened security around our offices.

The clock circuit uses an Intel 8224 integrated circuit. This is a crystal clock oscillator that provides the proper MOS clock levels for the 8080 system. It also contains circuitry for a TTL level clock (Ø2), RESET and READY inputs. Construction of the clock circuit begins by inserting components R1, R2, the 6.75 MHz crystal, IC5 and the jumper. Good quality IC sockets are recommended for all the integrated circuits.

After inserting and soldering the parts, the clock section should be checked. To do this, apply power and check for voltages on the 8224 chip. You should observe +5 at pin 16, +12 at pin 9 and ground at pin 8. Clock operation can be checked at pins 10 and 11. These are the MOS level outputs that swing between +12V and ground. The signals can be observed with a good scope. The TTL output on pin 6 can also be checked with a scope or with a monostable-LED circuit. The monostable circuit can be constructed on the SK-10 socket before it is added to the system.

With the 6.75-MHz crystal, the output frequency will be 750 kHz. This is slower than the maximum 2-MHz frequency that the 8080A will operate at, but a slow frequency was chosen to allow for slow access times of the PROM's.

The output ports are constructed next by inserting and soldering all the LED's (D1 through D24). Be sure to observe the polarity as shown by the symbol near D1. Add all the 220-ohm resistors (R7 through R30) and insert the SN7475 latches. Be careful to orient the IC's in their sockets. The foil pattern has a small mark near pin 1 for all the IC's.

With the latches and parts installed and soldered, apply power to the system. All of the LED's should light. If any are not on, check the associated SN7475 latch. With power still applied, ground the input pins to the latches, one at a time. Since all the inputs are on eight common data bus-lines, only eight inputs must be grounded to check all the LED's and latches. Ground pins 2, 3, 6 and 7 on IC24 and IC25. One of the LED's in each group of eight should go out, one at a time. If this doesn't happen, again check the SN7475's.

The keyboard section consists of 16 keyswitches—15 are used to input data and one is hardwired to the 8224 chip to reset the Dyna-Micro. The key-switch closures are encoded by two SN74148 octal encoders and the encoded binary data is gated onto the bus through a three-state DM8095 or SN74365 IC.

Insert and carefully solder the keyswitches to the printed-circuit board and then insert the four integrated circuits, IC30 through IC33.

The keyboard section is tested by monitoring the data on the LED's. Carefully ground pins 1 and 15 on the three-state driver, IC31. This will cause data from the keyswitch encoders to *constantly be fed to the bus. With these two pins grounded, apply power and depress the keys, one at a time. The binary data for each keyswitch will be indicated on the LED's at all of the output-ports simultaneously. Note that the most significant bit, D7, will be on whenever one of the keys is depressed. This is often called a 'flag' since it is used to flag down the computer and tell it that one of the switches is ready with data.*

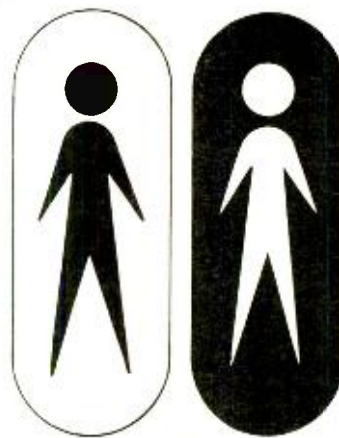
the computer to sense each bounce as a key closure so we would like some way to filter them out. Additional circuitry including latches, clocks and monostables could do this for us, but it complicates the system. We can also do the debouncing via software.

The KBRD subroutine will recognize any key closure, but it will only input the key codes after being sure that the key is closed and not bouncing. It does this by waiting after sensing a closure

and then rechecking the switch to be sure it is still closed. It also checks when we release a key to be sure that it has stopped bouncing before it tries to sense another key being depressed by the user. We have traded some additional software steps for a great deal of hardware. Since there was plenty of PROM left, it was easy to include.

The TIMOUT and KBRD software

*(Table II is on page 86)
(Text continues on page 90)*



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BUILD A COMPUTER

Text continues on page 90

TABLE II—KEYBOARD EXECUTIVE (KEX) PROGRAM

			*000 000
000 000	303		JMP
000 001	070		START
000 002	000		0
			/JUMP UP TO R/W MEMORY TO
			BE USED BY RESTARTS &
			VECTORED INTERRUPTS
			*000 010
000 010	303		JMP
000 011	010		010
000 012	003		003
			*000 020
000 020	303		JMP
000 021	020		020
000 022	003		003
			*000 030
000 030	303		JMP
000 031	030		030
000 032	003		003
			*000 040
000 040	303		JMP
000 041	040		040
000 042	003		003
			*000 050
000 050	303		JMP
000 051	050		050
000 052	003		003
			*000 060
000 060	303		JMP
000 061	060		060
000 062	003		003
			/BEGINNING OF MAIN PROGRAM
			*000 070
000 070	061	START,	LXISP /SET STACK POINTER
			TO TOP OF R/W MEM.
000 071	000		000
000 072	004		004
000 073	041		LXIH /INITIAL VALUE FOR
			H & L
000 074	000		000
000 075	003		003
000 076	116	POINT A,	MOVCM /LOAD MEM DATA INTO
			TEMP DATA BUFFER
000 077	174		MOVAH /OUTPUT HI TO LED'S
000 100	323		OUT
000 101	001		001
000 102	175		MOVAL /OUTPUT LOW TO
			LED'S
000 103	323		OUT
000 104	000		000
000 105	171	POINT B,	MOVAC /OUTPUT TEMP. DATA
			BUFFER DATA TO
			LED'S
000 106	323		OUT
000 107	002		002
000 110	315	POINT C,	CALL /WAIT & INPUT NEXT
			KEY CLOSURE
000 111	315		KBRD
000 112	000		0
000 113	376		CPI
000 114	010		010
000 115	322		JNC /JUMP IF KEY WAS <
			010
000 116	134	POINT D	/((0-7, OCTAL
			DIGIT)
000 117	000		0
000 120	107		MOVBA /SAVE KEY CODE
000 121	171		MOVAC /GET OLD VALUE
000 122	027		RAL /ROTATE 3 TIMES

```

000 123 027      RAL
000 124 027      RAL
000 125 346      ANI      /MASK OUT LEAST
                          SIG. OCTAL DIGIT

000 126 370      370
000 127. 260     ORAB     /OR IN NEW OCTAL
                          DIGIT

000 130 117      MOVCA    /PUT NEW DATA
                          BACK INTO BUFFER

000 131 303      JMP
000 132 105      POINT B
000 133 000      0
000 134 376     POINT D,  CPI
000 135 011      011     /"L" KEY
000 136 302      JNZ      /JUMP IF NOT AN "L"
000 137 145      POINT E
000 140 000      0
000 141 151      MOVLC    /PUT BUFFER DATA
                          IN L

000 142 303      JMP
000 143 076      POINT A
000 144 000      0
000 145 376     POINT E,  CPI
000 146 010      010     /"H" KEY
000 147 302      JNZ      /JUMP IF NOT AN "H"
000 150 156      POINT F
000 151 000      0
000 152 141      MOVHC    /PUT BUFFER DATA
                          IN H

000 153 303      JMP
000 154 076      POINT A
000 155 000      0
000 156 376     POINT F,  CPI
000 157 013      013     /"S" KEY
000 160 302      JNZ      /JUMP IF NOT "S"
000 161 170      POINT G
000 162 000      0
000 163 161      MOVMC    /PUT TEMP. DATA
                          INTO MEMORY
                          /INCREMENT H & L

000 164 043      INHX
000 165 303      JMP
000 166 076      POINT A
000 167 000      0
000 170 376     POINT G,  CPI
000 171 012      012     /"G" KEY
000 172 302      JNZ      /JUMP IF NOT "G"
000 173 110      POINT C
000 174 000      0
000 175 351      PCHL    /GO EXECUTE PGM
                          POINTED TO BY
                          H & L

                          /THIS 10 MSEC DELAY
                          DISTURBS NO REGISTERS OR
                          FLAG

000 277 365     TIMEOUT,  *000 277
000 300 325     PUSHPSW /SAVE REGISTERS
                          PUSHD
                          LXID    /LOAD D & E WITH
                          VALUE TO BE
                          DECREMENTED

000 301 021
000 302 046      046
000 303 001      001
000 304 033     MORE,    DCXD    /JUMP IN THIS
                          LOOP UNTIL
000 305 172      MOVAD    /D & E ARE BOTH
                          ZERO

000 306 263      ORAE
000 307 302      JNZ
000 310 304      MORE
000 311 000      0
000 312 321      POPD
000 313 361      POPPSW /RESTORE
                          REGISTERS

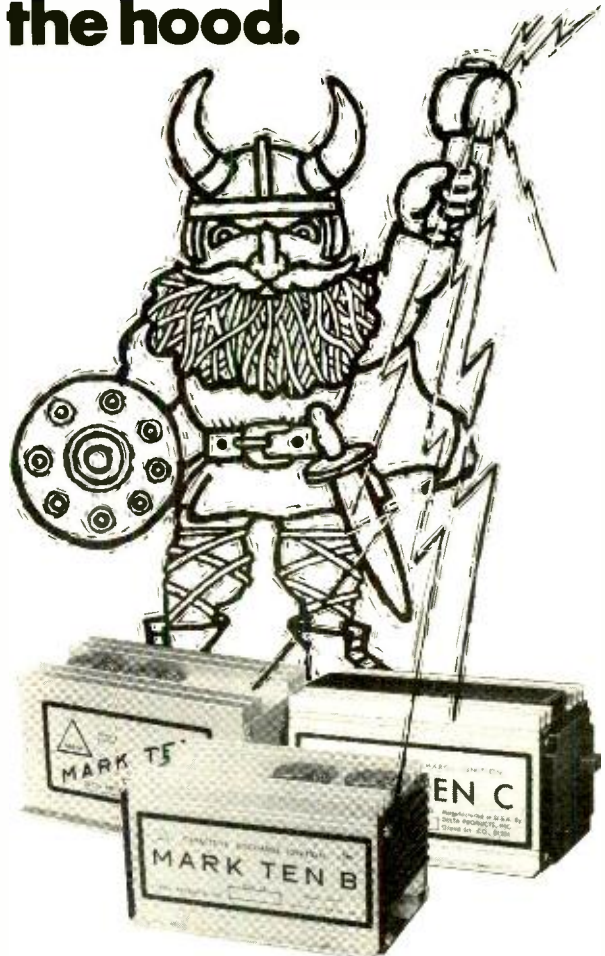
000 314 311      RET

                          /THE KBRD ROUTINE
                          DEBOUNCES KEY CLOSURES
                          /AND TRANSLATES KEY CODES

```

Table II continues on page 89 (text continues on page 90)

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VIDEO DISCS

(continued from page 40)

for every dropout there's a new system waiting in the wings. One of the latest, from Hitachi, uses a laser to read out discrete holographic images on a disc that rotates at just 6 RPM.

In any event, if RCA, MCA-Philips, Sony and their supporters stick to their present timetables, it appears that by this time next year we may have an answer to the industry's biggest question—does anybody really care? The consumer electronics industry has been searching for a new mass market product since 1964, when color television finally made the grade. To fill the bill, the videoplayer concept will have to appeal to millions of consumers. If it turns out the average consumer isn't willing to shell out \$500 to \$1,000, plus programming costs, for a substitute to the regular free TV fare, then the industry will have to look elsewhere for its future growth. **R-E**

NEXT MONTH

The July, 1976 issue of **Radio-Electronics** will feature two construction projects. One is a digital clock using a Panaplex display, and the other is a countdown timer. The timer has a built-in relay to control various external devices.

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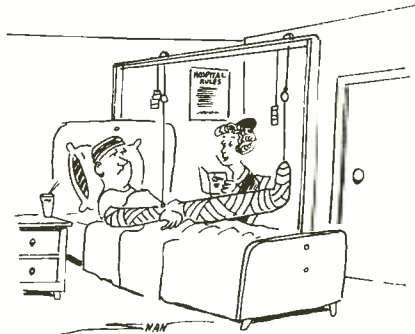
(continued from page 14)

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BUILD A COMPUTER

Table II continued from page 87
Text continues on page 90

			/FLAGS AND REG A ARE CHANGED
			/A0-A3 = CODE; A4-A7 = 0000
000 315	333	KBRD,	IN /INPUT FROM KEYBOARD ENCODERS
000 316	000		000
000 317	267		ORAA /SET FLAGS
000 320	372		JM /JUMP BACK IF LAST KEY NOT RELEASED
000 321	315		KBRD
000 322	000		0
000 323	315		CALL WAIT 10 MSEC
000 324	277		TIMOUT
000 325	000		0
000 326	333	FLAGCK,	IN
000 327	000		000
000 330	267		ORAA
000 331	362		JP /JUMP BACK TO WAIT FOR A NEW
000 332	326		FLAGCK /KEY TO BE PRESSED
000 333	000		0
000 334	315		CALL /WAIT 10 MSEC FOR BOUNCING
000 335	277		TIMOUT
000 336	000		0
000 337	333		IN
000 340	000		000
000 341	267		ORAA
000 342	362		JP /JUMP BACK IF NEW KEY NOT STILL
000 343	326		FLAGCK /PRESSED (FALSE ALARM)
000 344	000		0
000 345	346		ANI /MASK OUT ALL BUT KEY CODE
000 346	017		017
000 347	345		PUSHH /SAVE H & L
000 350	046		MVIH /ZERO H REG
000 351	000		000
000 352	306		ADI /ADD THE ADDRESS OF THE BEGINNING
000 353	360		360 /OF THE TABLE TO THE KEY CODE
000 354	157		MOVLA /
000 355	176		MOVAM /FETCH NEW VALUE FROM TABLE
000 356	341		POPH /RESTORE H & L
000 357	311		RET
			/THIS TRANSLATION TABLE CONVERTS THE CODE /GENERATED BY KEY CLOSURES TO THE CODE /USED BY THE MAIN KEX PROGRAM
000 360	000	TABLE,	000
000 361	001		001
000 362	002		002
000 363	003		003
000 364	004		004
000 365	005		005
000 366	006		006
000 367	007		007
000 370	013		013 /S
000 371	000		000 /THIS CODE CAN'T BE GENERATED
000 372	017		017 /C
000 373	012		012 /G
000 374	010		010 /H
000 375	011		011 /L
000 376	015		015 /A
000 377	016		016 /B

end of Table II (text continues on page 90)

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BUILD A COMPUTER

(continued from page 87)

segments have been set up as subroutines and can be used in your software and in the experiments. Each of these subroutines may be started with a CALL instruction, 315. The TIMEOUT subroutine does not affect any of the registers or flags and it only serves to delay the software flow by 10 ms.

An important distinction between the 8008 and the 8080 processors is in the use of subroutines. In the 8008, return-pointer addresses were stored in the 8008 IC itself. In the 8080, these return-pointer addresses are stored in a portion of the R/W memory. This is called a "stack" area. Whenever a subroutine is used, we want to execute the subroutine and then return back to the normal program flow. These return addresses are very important to the computer since they provide the only link between the subroutine and the main program. If we are to store them in a portion of R/W memory, the computer must know where this storage area is if it is to be able to use the addresses properly. In the KEX software, this is preset to be the top of the R/W memory with instructions at locations 070, 071 and 072. The LXISP instruction

loads an internal 8080 stack-pointer register to HI=004, LO=000. Since the stack-pointer register is decremented to point to a new location before anything is stored, the first stack location will be HI=003, LO=377. Check your 16" bit binary numbers if this looks a little confusing.

You can use the stack as set up by the KEX (generally a good idea) or you can put your own stack anywhere you want, just by using the LXISP instruction. Remember to avoid the stack area when writing your programs. Remember, too, that you can't put the stack in an area of non-existent memory or in PROM.

You will use the stack area and you'll see how it can also be used to temporarily store data. This will be covered in

the software modules. Let's see how the TIMEOUT and KBRD subroutines can be used in our own software. We will use the software stack already set up in KEX.

Let's input a keyboard character, add a constant to the binary code for that character and display the result. We would first CALL the KBRD subroutine to input a binary key-code, then add the constant and display the result. The software listed in Table III will do this:

You can enter this with the KEX program. Depress the R key and start entering data. Enter 000 at location 003 004 so we'll first add zero to the codes. This will let us check what values are assigned to each key. Write down the codes. Go back and restart

TABLE III

HI	LO	INSTR	MNEMONIC	
003	000	315	CALL	/Input keyboard character
003	001	315	KBRD	/Subroutine's LO address
003	002	000	0	/Subroutine's HI address
003	003	306	ADI	/Add the following DATA to
003	004	???	DATA	/the contents of register A
003	005	323	OUT	/Output data from register A to
003	006	000	000	/device 000 (LEDs)
003	007	303	JMP	/Jump back to program at
003	010	000	000	/LO address = 000
003	011	003	003	/HI address = 003

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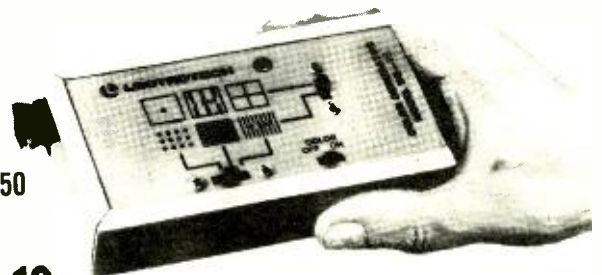
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TABLE IV

Assume HI = 003 throughout this program

LO	INSTR	MNEMONIC	
000	006	MVIB	/Load register B with the following data
001	370	370	/Data; time constant
002	315	CALL	/Call TIMEOUT subroutine at
003	277	277	/LO address = 277
004	000	000	/HI address = 000
005	005	DECB	/Decrement B by 1
006	302	JNZ	/Jump if result is not zero to
007	002	002	/LO address = 002
010	003	003	/HI address = 003
011	076	MVIA	/Load register A with the following data
012	377	377	/Data; all 1's
013	323	OUT	/Output to device,
014	000	000	/device 000 (LED's)
015	166	HLT	/Stop once you reach here

KEX and change the value in 003 004 to, say, 005. This will add 5 to each code. Restart your software and see if this is the case. Congratulations, you have just done your first software experiment! The instructions at 003 003 and 003 004 could be changed to do other things to the data. Can you suggest one?

The 10 ms delay routine, TIMEOUT, can be useful when we want a software delay that is in multiples of 10 ms. The software routine listed in Table IV will delay an output of all 1's on OUTPUT PORT 0 by about 2.5 seconds after the

program is started. Try it. Can you see how the time delay might be shortened? Can you see any use for programs like this?

The keyboard input subroutine, KBRD, is called at address 000 315 and the time delay subroutine, TIMEOUT, is called at address 000 277.

Next month, this construction article concludes with a description of the 8080A microprocessor and how the Dyna-Micro works. This will include an explanation of how the memory is accessed and how the Dyna-Micro selects input/output devices via software. **R-E**



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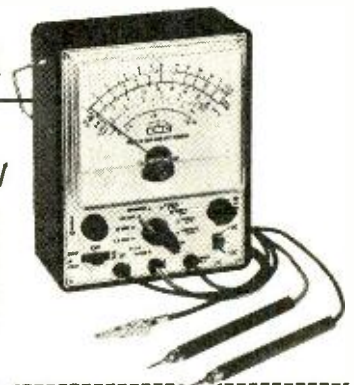
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<input type="checkbox"/> 1V2 5 for \$3.20	<input type="checkbox"/> 6HQ5 5 for \$6.75
<input type="checkbox"/> 2AV2 5 for \$4.20	<input type="checkbox"/> 6HV5 5 for \$11.80
<input type="checkbox"/> 3A3 5 for \$5.35	<input type="checkbox"/> 6JC6 5 for \$5.95
<input type="checkbox"/> 3AT2 5 for \$5.20	<input type="checkbox"/> 6JE6 5 for \$11.15
<input type="checkbox"/> 3GK5 5 for \$5.15	<input type="checkbox"/> 6JS6 5 for \$9.90
<input type="checkbox"/> 3HA5 5 for \$5.10	<input type="checkbox"/> 6JU8 5 for \$5.90
<input type="checkbox"/> 3HM5 5 for \$5.10	<input type="checkbox"/> 6KA8 5 for \$6.50
<input type="checkbox"/> 5GH8 5 for \$6.25	<input type="checkbox"/> 6KE8 5 for \$8.15
<input type="checkbox"/> 6BK4 5 for \$9.95	<input type="checkbox"/> 6KT8 5 for \$7.25
<input type="checkbox"/> 6CG3 5 for \$5.25	<input type="checkbox"/> 6KZ8 5 for \$5.25
<input type="checkbox"/> 6CJ3 5 for \$5.00	<input type="checkbox"/> 6LB6 5 for \$10.75
<input type="checkbox"/> 6DW4 5 for \$5.00	<input type="checkbox"/> 6LQ6 5 for \$11.15
<input type="checkbox"/> 6EA8 5 for \$5.25	<input type="checkbox"/> 8FQ7 5 for \$4.05
<input type="checkbox"/> 6EH7 5 for \$5.10	<input type="checkbox"/> 12BY7 5 for 7.00
<input type="checkbox"/> 6EJ7 5 for \$4.75	<input type="checkbox"/> 12GN7 5 for 7.40
<input type="checkbox"/> 6FQ7 5 for \$4.05	<input type="checkbox"/> 17JZ8 5 for \$4.75
<input type="checkbox"/> 6GF7 5 for \$7.05	<input type="checkbox"/> 23Z9 5 for \$6.35
<input type="checkbox"/> 6GH8 5 for \$4.20	<input type="checkbox"/> 33GY7 5 for \$8.05
<input type="checkbox"/> 6GJ7 5 for \$3.70	<input type="checkbox"/> 36MC6 5 for \$11.40
<input type="checkbox"/> 6GU7 5 for \$5.55	<input type="checkbox"/> 38HE7 5 for 9.75
<input type="checkbox"/> 6HA5 5 for \$5.10	<input type="checkbox"/> 38HK7 5 for 9.55

100—2.5 Amp 1000 PIV DIODES	\$ 9.95
10—15KV FOCUS RECTIFIERS	\$ 4.50
20—1N34A CRYSTAL DIODES	\$ 2.00
4—3.58 Mhz Color Crystals	\$ 2.49
RCA DAMPER DIODES REPL. 135932 Pr. ..	\$ 2.98
ZEN. VOLT TRIPLER 212-109	Each \$ 3.95

ZENITH TUNERS NEW (TUBES)

175-1118	Ea. \$ 4.50
175-1120	Ea. \$ 4.50
175-1122	Ea. \$ 4.50
175-1164	Ea. \$ 4.50

REPL. DIAMOND NEEDLES SHURE

N-3D—N44—N75—N91	Ea. \$ 2.95
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PICKERING

V-15 GREY—V-15 ORANGE	Ea. \$ 2.95
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COLOR IC CHIPS

REPL. ZEN. 221-42	4 for \$ 5.00
REPL. ZEN. 221-46—51	4 for \$ 5.00
REPL. ZEN. 221-62	4 for \$ 5.00
30 W Pencil Sold. Iron	Ea. \$ 2.19
2—2 Set Couplers 300 Ohm	\$ 3.00
2—4 Set Couplers 300 Ohm	\$ 4.50
100 Asst'd. Springs	\$ 1.79
50 Asst'd. WW Resistors	\$ 2.69
50 Asst'd. Controls	\$ 2.00
200 Asst'd. Resistors (CUTLEADS)	\$ 1.89
75—300 Ohm Match. Xfmr.	6 for \$ 5.00
6—Asst'd. UHF TUNERS	\$ 3.00
70%—COLOR YOKE (21" CRT)	\$ 3.95
8" SPEAKER (W/TWEETER)	\$ 3.00
3—C60—IRISH CASSETTE TAPES	\$ 1.49
25 Asst'd. SLIDE SWITCHES	\$ 2.00
66 MEG. HV RES. (IRC)	4 for \$ 2.00
25 Asst'd. Filter CANS	\$ 3.95
25 Asst'd. Filters (AXIAL)	\$ 3.95
50 Asst'd. Filters (TRANS. WORK) ..	\$ 4.95
Univ. CASSETTE MICROPHONE	Ea. \$ 2.19
70% COLOR CRT BOOSTERS	3 for \$11.50
90% COLOR CRT BOOSTERS	3 for \$12.50
10—RCA PHONO PLUGS	\$ 1.19
4—ASST'D. STEREO CARTRIDGES	\$ 4.95
MONO TONEARM	\$ 1.69
70% CONVERG. ASSEMBLY	\$ 1.00
90% CONVERG. ASSEMBLY	\$ 1.00
SHUNT REG. HOODS—(6JE6 etc.) ..	2 for \$ 1.19
25 Asst'd. PLATE CAPS (6JE6-6DQ6) ..	\$ 1.00
6 Asst'd. FOCUS SOCKETS	\$ 1.19
6—HV ANODE LEADS LARGE CUP	\$ 2.49
5—CRT HARNESS COLOR 19"-25" CRT ..	\$ 1.19

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NOTICE TO MAIL ORDER BUYERS

Under a new Trade Regulation Rule of the FTC that became effective February 2, 1976, mail-order merchants are required to make deliveries within a reasonable time, notify the customer if his order has to be delayed, and return his money if requested.

The rule provides that if a mail-order seller is unable to ship merchandise within the time specified in his ad (or if no time is specified, within 30 days) he must notify the buyer of the delay and give him the option of cancelling the order and having his purchase money refunded.

The buyer must be provided with a cost-free device for this purpose such as a postpaid post-card or return envelope. If the buyer does not respond, it will be assumed that he has consented to an additional 30-day delay. For any longer delay, the customer's

express consent must be gained; otherwise the money is to be refunded.

The rule also makes provision for indefinite delays if agreed to by the customer; though a refund must be made, if requested any time during the delay. It also requires sellers of mail-order merchandise to have a reasonable basis for any claims they make about shipping time.

Penalties are severe. The FTC can go to court to get an order for compliance by a company or they could have a company fined up to \$10,000 for each day of non-compliance.

The rule *does not* apply to COD orders.

If you have a documented complaint send it to: Federal Trade Commission, Bureau of Consumer Protection, Washington, DC 20580.

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TELEPHONE bugged? Don't be Watergated! Countermeasures brochure \$1.00. **NEGEYE LABORATORIES**, Box 547-RE, Pennsboro, WV 26415

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Poly Pak's BUY 'EM FROM THE "BARREL" AND SAVE!

100'S OF BARRELS PURCHASED!



EXCLUSIVE 'BARREL'

Every kit carries money back guarantee.

THE BIGGEST INFLATION-FIGHTING VALUE EVER! TEST 'EM YOURSELF 'N SAVE!

For the first time anywhere, Poly Pak merchandisers introduce a new way in buying the economical way. Raw stock from the "barrel". Remember

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runs in barrels. Poly Pak has done the same. Therefore you are getting the same type of material as the RE-TESTERS DO!

NEVER BEFORE!

U-TEST EM-N-CHOOSE EM IC'S

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Cat. No. 6R3170

Type	Sale
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SN7404	50 for 1.98
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SN7407	50 for 1.98
SN7408	50 for 1.98
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SN7413	50 for 1.98
SN7414	50 for 1.98
SN7415	50 for 1.98
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SN7437	50 for 1.98
SN7438	50 for 1.98
SN7439	50 for 1.98
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SN7448	50 for 1.98
SN7449	50 for 1.98
SN7450	50 for 1.98
SN7451	50 for 1.98
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MONEY BACK GUARANTEE PER PAK!

NEW FACTORY ARRANGEMENTS! Why mix 'em? They decided to "bag" same types, then throw bags into barrels. YOU TEST!

You test 'em yourself. Buy types of your choice at BARREL PRICES!

LINEARS

Cat. No.	Price
6R3171	
LM300H	30 for \$1.98
LM301	50 for 1.98
LM307V	40 for 1.98
LM308V	30 for 1.98
LM309	50 for 1.98
LM318V*	30 for 1.98
LM319V	30 for 1.98
LM324N	30 for 1.98
LM329N	30 for 1.98
LM351V	30 for 1.98
LM358V	30 for 1.98
LM377N	40 for 1.98
LM380N	30 for 1.98
LM380V*	30 for 1.98
LM381N	30 for 1.98
LM382N	30 for 1.98
LM383V	30 for 1.98
LM709N	50 for 1.98
LM733N	30 for 1.98
LM734V	50 for 1.98
LM747N	30 for 1.98
LM1303N	30 for 1.98
LM1304N	30 for 1.98
LM1310N	30 for 1.98
LM1459V	30 for 1.98
LM1810N	30 for 1.98
LM182N	30 for 1.98
LM2111N	30 for 1.98
LM2901N	30 for 1.98
LM2902N	30 for 1.98
LM302N	30 for 1.98
LM3612V*	30 for 1.98
LM3900N	30 for 1.98
LM392N	30 for 1.98
LM7534N	40 for 1.98
LM7535N	40 for 1.98
LM7538N	40 for 1.98
LM7514V*	40 for 1.98
LM7491N	30 for 1.98
LM75492N	30 for 1.98

BARREL KIT #1
SN7400 DIP IC'S
75 for \$1.98
Marked 14 and/or with 14 pin dips, may include gates, registers, flip flops, counters. Who knows! GUARANTEE! SATISFACTION!
Cat.No. 6R2415 Untested.

BARREL KIT #2
LINEAR OP AMPS, DIPS
75 for \$1.98
Un- tested
May include 709's, 741's, 703's, 660 series, 666 includes marked and unmarked. Cat.No. 6R2416

BARREL KIT #3
1N4148/914 SWITCHING DIODES
100 for \$1.98
You never saw this before. Imagine famous switching diodes at these prices! Un- tested. Cat.No. 6R2418

BARREL KIT #4
"4000" RECTIFIERS
100 for \$1.98
Un- tested. These are the famous micro miniature rectifiers of the 1N4000 series. May include 25, 50, 100, 200, 400, 600, 800 and 1000 volters. Cat.No. 6R2417

BARREL KIT #5
SCRS, TRIACS, QUADRACS
40 for \$1.98
All the famous plastic power tab type. Raw factory stock! All the 10 amp types. Cat.No. 6R2419 Un- tested.

BARREL KIT #7
VOLUME CONTROL BONANZA!
40 for \$1.98
100% Good
Singles, duals, variety of values, styles, big ones — small ones. Cat.No. 6R2421

BARREL KIT #8
SUBMINIATURE IF TRANSFORMERS
100 for \$1.98
Amazing, includes 400kcs, 600kcs, antenna, who knows? From transistor audio manufacturers. Cat.No. 6R2422

BARREL KIT #10
ROMS-REGISTERS
50 for \$1.98
Un- tested
28 to 40 pin devices, marked, internal factory numbers. etc. Cat.No. 6R2424

BARREL KIT #12
POWER TAB TRANSISTORS
40 for \$1.98
PNP, plastic 10220 type. Assorted 2N numbers. Cat.No. 6R2426 Un- tested.

BARREL KIT #13
RESISTOR NETWORKS
60 for \$1.98
Un- tested. By Corning Glass, in 14-pin dip paks. Cat.No. 6R2427

BARREL KIT #15
MOSFET TRANSISTORS
60 for \$1.98
All 1 leaders TO-18 case, includes 2N1F transistors too! Cat.No. 6R2429

BARREL KIT #17
LINEAR & 7400 DIPS
100 for \$1.98
Un- tested
Marked and unmarked, internal numbers of raw factory stock. Cat.No. 6R2431

BARREL KIT #19
DIPPED MYLARS
60 for \$1.98
Finest capacitors made, stony finish. Imagine factory dumping 'em in barrels. Cat.No. 6R2597 100% good.

BARREL KIT #20
LONG LEAD DISCS
150 for \$1.98
Factory distributor stock "auction sale" Prime, marked only. Long leads. Cat.No. 6R2598 100% good.

BARREL KIT #25
METAL CAN TRANSISTORS
100 for \$1.98
Un- tested. Includes TO-5, TO-18, etc. assorted 2N numbers, unmarked etc. Cat.No. 6R2603

BARREL KIT #31
METALLIC RESISTORS
100 for \$1.98
100% good.
Made mostly by Corning, the finest resistor made. Mostly 1/2 watters, 1% to 5% tol. & 1/4 barrel of values. Cat.No. 6R2609

BARREL KIT #32
TRANSISTORS WITH A HOLE IN IT
50 for \$1.98
Un- tested. Can't name factory but we bought barrels of 25 watters, some with a hole in middle. PNP's and NPN's. Cat.No. 6R2610

BARREL KIT #35
NEON LAMPS
40 for \$1.98
100% good
Famous NE-2's. All prime, but factory made millions and barrelled 'em. Your address. Cat.No. 6R2613

BARREL KIT #36
GERMANIUM DIODES
200 for \$1.98
Un- tested
Famous maker, popular item. Never grows old. But this is the way the RE-TESTERS buy 'em from the factory. Cat.No. 6R2614

BARREL KIT #37
"A BOP BULLET" RECTIFIERS
100 for \$1.98
Un- tested. Famous style, assid. voltages, silicon, axial includes all types of voltages to 1KV. Cat.No. 6R2615

BARREL KIT #46
G.E. 3.5 WATT AMPLIFIERS
25 for \$1.98
Un- tested
Hobby type, factory fallouts, we purchased them in barrels. These are unknowns. Cat.No. 6R2624

BARREL KIT #80
SIGNAL SILICON DIODES
200 for \$1.98
Includes many, many types of switching, signal silicon types, all axial leads. Some may be 709's. Cat.No. 6R2628 Un- tested.

BARREL KIT #81
HOBBY OPTO COUPLERS
40 for \$1.98
Un- tested
We bot 1,000's unknown both the sensor or transmitter may be good, or both. WE DON'T KNOW! We don't know the types. 1500V isolation. Cat.No. 6R2629

BARREL KIT #52
DISCS!
500 for \$1.98
Un- tested
Cat.No. 6R2630 100% good
The bargain of a lifetime! First time ever offered by Poly Paks for the economy-minded bargain hunters.

BARREL KIT #53
JUMBO RESISTOR PAK
100-pc. \$1.98
Un- tested
Assorted metal films, precision, carbons, metal oxide powers, from 1/4 watt to 7 watts. Color coded & 100% good. Worth \$1.00.

BARREL KIT #60
DTL'S IC'S
75 for \$1.98
Un- tested
This is prime barrel material. Who wants DTL's? 9210, 916, 946's. Your gain is our loss. They're marked too. Cat.No. 6R2728

BARREL KIT #61
POLYSTYRENE CAPS
100 for \$1.98
100% good
Finest caps made. As a gamble we bought 10 barrels from factory, mixed values; all good. Cat.No. 6R2729

BARREL KIT #65
MIXED READOUTS
15 for \$1.98
100% good
Factory returns — such numbers as MAN-1's, MAN-7's, MAN-13's, 11 barrels & no time to separate. Cat.No. 6R2733 Un- tested.

BARREL KIT #68
2 WATTERS
100 for \$1.98
100% good
Nobody seems to want 'em! So many suppliers don't count, but throw 'em in the barrel. It's a 1/2 gold mine. All marked. Cat.No. 6R2735

BARREL KIT #71
CAPACITOR SPECIAL
100 pcs. \$1.98
100% good
Emptied stockrooms into barrels of mylars, poly's, mica's, maida's, plastic, ceramics, discs, etc. Fifty up to 300 mf. Cat.No. 6R2738

BARREL KIT #76
1-WATT ZENERS
100 for \$1.98
Un- tested
Factory same as 400-mw's. Never-to-see-again offer, 8, 10, 12, 15, 18, 20, under glass. Double plug. Cat.No. 6R2741

BARREL KIT #77
"BROWN" BODY TRANSISTORS
40 for \$1.98
Un- tested
G-E 11-40 series; has voltage, Darlington's, hi-current, npn's. Factory line cleaning. Double plug. Cat.No. 6R2742 Un- tested.

BARREL KIT #78
"RED" BODY TRANSISTORS
40 for \$1.98
Un- tested
D-42 series. You test — go into your own biz! High current, hi-voltage. Cat.No. 6R2743 Un- tested.

BARREL KIT #81
SUBMINI RESISTORS
200 for \$1.98
100% good.
PC, upright type, color coded, 1/4 watt. Assat values. Same to us in a barrel. Cat.No. 6R2746

BARREL KIT #83
NATIONAL IC BONANZA
100 for \$1.98
Un- tested
Factory rejects them for length of leads. May include 5, 6, 8, 12, 15, 18, 24, voltages. Power IC's. Cat.No. 6R2635

BARREL KIT #94
"BUBBLE" READOUTS
12 for \$1.98
Un- tested
DL-33B bubble magnifiers. Saks missing. Truthfully so many of 'em we don't care. Un- tested. 3 oz. No. 6R3046

BARREL KIT #99
PHOTO ELECTRIC CELLS
10 for \$1.98
Un- tested
Assat. GE types, ODS types. Mixed by factory. Big job for us to separate. 100% good. Cat.No. 6R3052

BARREL KIT #102
CLOCK CHIPS
5 for \$1.98
Un- tested
National is dumping! MM-5216 — what's wrong with 'em, we don't know, but we got barrels. Hobby special. Wt. 2 oz.

BARREL KIT #104
SLIDE VOLUME CONTROLS
10 for \$1.98
Un- tested
Used in hi-fi, volume control maker, unloads. Assat values, what a buy. Worth \$1 ea. We've got barrels of 100% material.

BARREL KIT #107
SQUARE OHM'S
60 for \$1.98
Un- tested
Factory people are sometimes "squares" when they love prime square ohms mix 'em up in barrels. Assat values wats. Wt. 1 lb.

BARREL KIT #110
SUPPRESSOR DIODES
50 for \$1.98
Un- tested
Keeps ignition noises out axial. Un- tested, but the of your auto, car, industrial, etc. Double plug. Cat.No. 6R3137

BARREL KIT #111
MULTI DIGIT READOUTS
8 for \$1.98
Un- tested
barrels of blemished 3, 4 and/or 5 digit readouts to USA for "dump". Un- tested. Cat.No. 6R3139

BARREL KIT #112
MICRO MINI LEADS
40 for \$1.98
Un- tested
All the tiny leads, axial, upright of Monsanto, Litronix, variety of colors. Yield 60% or better. Cat.No. 6R3139

BARREL KIT #113
STABISTORS
50 for \$1.98
Un- tested
Regulator, sensing and computer circuitry. Axial double plug type. Discounted factory line. PIV 20 volts. 80% yield. U test 'n save! Cat.No. 6R3144

BARREL KIT #115
MOLEX SOCKETS
300 for \$1.98
100% good.
Calculator maker dump! We got a zillion of 'em. Used for IC sockets, etc. Cat.No. 6R3159

BARREL KIT #118
MINI SCRS
50 for \$1.98
Un- tested
UNBELIEVABLE! TO-92 plastic SCRS in barrels — rite from factory. Includes all voltages up thru 200 prv. 6R3135

BARREL KIT #110
MODULAR SWITCHES
25 for \$1.98
Un- tested
Centralab — push-on switches. TV-makers exclusive. Dpdt, 6pdt, etc. Brand new. Cat.No. 6R3150

BARREL KIT #120
TRIGGER DIODES
25 for \$1.98
Un- tested
Type ER-900, same type used to trigger screw triggers. Sometimes called "diaes". Un- tested. No. 6R3160

BARREL KIT #121
"MINI" MAGNETS
100 for \$1.98
Un- tested
Magnat circular and rectangular cuttings from a major maker — For need switches & micro-circuitry. Cat.No. 6R3168

BARREL KIT #122
OPTIC OPTICAL FIBERS
500-Ft. \$1.98
Un- tested
Pop! 10-mil size. Excellent type making light pipes, experiments, lamp arrays. Cat.No. 6R3159

BARREL KIT #127
AXIAL ELECTROS
40 for \$1.98
Un- tested
Truthfully the factories (by mixing 'em in barrels) do all of us a favor. WUT A BUY! Assat capacities and voltages. Cat.No. 6R3227

BARREL KIT #128
MINI DIP IC'S
75 for \$1.98
Un- tested
Large mfrz dumped 100's of lbs into barrels. Includes 741's, LM-390's, 703, 667, 555, 568 — but who knows? Factory to you. All mixed, you test. Wgt. 1 lb. Cat.No. 6R3245

BARREL KIT #131
TANTALUM ELECTROS
30 for \$1.98
Un- tested
Mixed, marked prime, top grade assat. values, voltages. GE, Centralab, etc. Cat.No. 6R3255

BARREL KIT #133
C-MOS IC'S
60 for \$1.98
Un- tested
Deliberately thrown in barrels, so we can't test 'em! The famous CD4000 series. How good? Who knows? Who cares? It's only 2¢ ea. Cat.No. 6R3257

BARREL KIT #126
UPRIGHT ELCTROS
40 for \$1.98
Un- tested
Wide assat. of values from 1mf to 300mf in mixture of voltages. 100% marked 'n good. Who barreled? U-test 'n buy! Cat.No. 6R3226

Terms: Add postage. Rated: net 30. Phone: Wakefield, Mass. (617) 245-3829. Retail: 16-18 Del Carmine St., Wakefield, MASS. MINIMUM ORDER — \$6.00

POLY PAKS Send for FREE Spring-Summer CATALOG

P.O. BOX 942 R-6 LYNNFIELD, MASS. 01940



DELTA ELECTRONICS CO.

P.O. BOX 2, AMESBURY, MASS. 01913

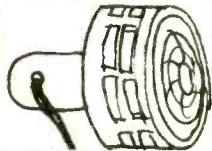
BURGLAR ALARM PARTS

This month we are featuring a variety of parts useful in burglar alarms. Use in your home, car, shop, or business.



INFRARED PHOTOTRANSISTOR. TO-18 case, red coating over lens increases IR sensitivity. Very good for fire detection.

STOCK NO. R4538 .75 each, 3/2.00



12 VOLT DC SIREN. A very powerful 12v siren, makes an ear splitting sound when energized. 4 1/2" diameter x 5 1/2" long. Shipping weight 3 lbs. Brand new.

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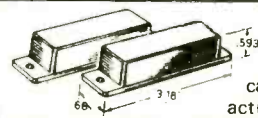
ULTRASONIC TRANSDUCERS, used in alarm circuits and remote controls. We have 2 types, operating at 23 Khz & 41.5 Khz. Both can operate as either a receiver or transmitter. We supply some basic alarm circuits and data.

R9272



R6000

STOCK NO. R9272 23 Khz \$2.00 each, 4/7.00
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PROXIMITY REED SWITCHES. One case contains an Alnico magnet, which actuates a normally open reed switch in the other case within a distance of 1". Mount on windows, doors, or on the back of valuable equipment.

STOCK NO. R5351 \$1.75/set, 4 sets/6.00, 10 sets/12.50

Send for our free catalog. Phone orders welcome, MASTERCHARGE & BANK AMERICARD accepted. ALL numbers must be included to process order. Minimum order \$5. Include sufficient postage. excess will be refunded.



Phone (617) 388-4705

Circle 92 on reader service card

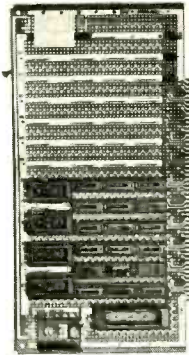
GODBOUT

UNIVERSAL PROTOTYPE BOARD: Use with Altair 8800 or homebrew computers. Accepts any DIP package; power & ground planes on opposite sides of board; onboard room for 2 regulators (1 heat sink also provided). UNIVERSALLY USEFUL FOR PERIPHERALS. Add 1 lb shipping.

Other VECTOR products:

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PRE-PUNCHED VECTORBOARD: \$8.95. Holes on .1" centers. 8 1/2" X 17". 1/16" thick epoxy glass base. Add 1 lb shipping.



new from
VECTOR
\$19.95

HOBBYWRAP TOOL.....\$41.95

Wire wrapping equipment at the right price. Comes with tool (rechargeable; no cords in tight places), bit, charger, nicads, & instructions.

WIRE WRAP SOCKETS... Perfect mate for the HOBBYWRAP tool. 3 level, gold-plated leads.
14 pin.....10/\$3.70
16 pin.....10/\$3.85
18 pin.....1/\$0.75
24 pin.....1/\$1.00
28 pin.....1/\$1.25
36 pin.....1/\$1.35
40 pin.....1/\$1.75

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2.2 uF @ 20V.....4/\$1.00
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4000 uF, 20V, PFP...1/\$0.95
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Circle 93 on reader service card

CB SPECIALS-R.F. DRIVERS-R.F. POWER OUTPUTS-FETS

2SC481	1.85	2SC767	15.75	2SC866	5.85	2SC1449-1	1.60	40081	1.50
2SC482	1.75	2SC773	.85	2SC1013	1.50	2SC1475	1.50	40082	3.00
2SC495	1.10	2SC774	1.75	2SC1014	1.50	2SC1678	5.50	2SC608	4.85
2SC502	3.75	2SC775	2.75	2SC1017	1.50	2SC1679	4.75	SK3046	2.15
2SC517	4.75	2SC776	3.00	2SC1018	1.50	2SC1728	2.15	SK3047	3.75
2SC614	3.80	2SC777	4.75	2SC1173	1.25	2SC1760	2.15	SJ2095	3.50
2SC615	3.90	2SC778	3.25	2SC1226A	1.25	2SC1816	5.50	SK3048	3.25
2SC616	4.15	2SC797	2.50	2SC1237	4.50	2SC1908	.70	SK3054	1.25
2SC617	4.25	2SC798	3.10	2SC1239	3.50	2SC1957	1.50		
2SC699	4.75	2SC781	3.00	2SC1243	1.50	2SF8	3.00	2SK19	1.75
2SC710	.70	2SC789	1.00	2SC1306	4.75	HEP-S 3001	3.25	2SK30	1.00
2SC711	.70	2SC796	3.15	2SC1306-1	4.75	2SD235	1.00	2SK33	1.20
2SC735	.70	2SC799	4.25	2SC1307	5.90	MRF8004	3.00		
2SC756	3.00	2SC802	3.75	2SC1307-1	6.00	4004	3.00	3SK40	2.75
2SC765	9.50	2SC803	4.00	2SC1377	5.50	4005	3.00	3SK45	2.75
2SC766	10.15	2SC839	.85	2SC1449	1.30	40080	1.25	3SK49	2.75

JAPANESE TRANSISTORS

2SA52	.60	2SB187	.60	2SC458	.70	2SC815	.75	2SC1569	1.25
2SA316	.75	2SB235	1.75	2SC460	.70	2SC828	.75	2SC1756	1.25
2SA473	.75	2SB303	.65	2SC478	.80	2SC829	.75		
2SA483	1.95	2SB324	1.00	2SC491	2.50	2SC830	1.60	2SD30	.95
2SA489	.80	2SB337	2.10	2SC497	1.60	2SC839	.85	2SD45	2.00
2SA490	.70	2SB367	1.60	2SC515	.80	2SC945	.85	2SD65	.75
2SA505	.70	2SB370	.65	2SC535	.75	2SC1010	.80	2SD68	.90
2SA564	.50	2SB405	.85	2SC536	.65	2SC1012	.80	2SD72	1.00
2SA628	.65	2SB407	1.65	2SC537	.70	2SC1051	2.50	2SD88	1.50
2SA643	.85	2SB415	.85	2SC563	2.50	2SC1061	1.65	2SD151	2.25
2SA647	2.75	2SB461	1.25	2SC605	1.00	2SC1079	3.75	2SD170	2.00
2SA673	.85	2SB463	1.65	2SC620	.80	2SC1096	1.20	2SD180	2.75
2SA679	3.75	2SB471	1.75	2SC627	1.75	2SC1098	1.15	2SD201	1.95
2SA682	.85	2SB474	1.50	2SC642	3.50	2SC1115	2.75	2SD218	4.75
2SA699	1.30	2SB476	1.25	2SC643	3.75	2SC1166	.70	2SD300	2.50
2SA699A	1.75	2SB481	2.10	2SC644	.70	2SC1170	4.00	2SD313	1.10
2SA705	.55	2SB492	1.25	2SC681	2.50	2SC1172B	4.25	2SD315	.75
2SA815	.85	2SB495	.95	2SC684	2.10	2SC1209	.55	2SD318	.95
2SA816	.85	2SB507	.90	2SC687	2.50	2SC1213	.75	2SD341	.95
		2SB511	.70	2SC696	2.35	2SC1226	1.25	2SD350	3.25
				2SC712	.70	2SC1243	1.50	2SD352	.80
2SB22	.65			2SC713	.70	2SC1293	.85	2SD380	5.70
2SB54	.70	2SC206	1.00	2SC732	.70	2SC1308	4.75	2SD389	.90
2SB56	.70	2SC240	1.10	2SC733	.70	2SC1347	.80	2SD-390	.75
2SB77	.70	2SC261	.65	2SC737	.70	2SC1383	.75	2SD437	5.50
2SB128	2.25	2SC291	.65	2SC739	.70	2SC1409	1.25		
2SB135	.95	2SC320	2.00	2SC715	1.75	2SC1410	1.25	MPS-U31	4.00
2SB152	4.50	2SC352	.75	2SC762	1.90	2SC1447	1.25		
2SB173	.55	2SC353	.75	2SC783	1.00	2SC1448	1.25		
2SB175	.55	2SC371	.70	2SC784	.70	2SC1448	1.25		
2SB178	1.00	2SC372	.70	2SC785	1.00	2SC1507	1.25		
2SB186	.60	2SC394	.70	2SC793	2.50	2SC1509	1.25		

POWER-TRANSISTORS HIGH-VOLT. TV. TYPE

BU204	1300V	3.90	BU207	1300V	5.40	2SC1172B	1100V	4.25
BU205	1500V	4.70	BU208	1500V	6.25	2SC1308	1100V	4.95
BU206	1700V	5.90	2SC1170	1100V	4.00	2SC1325	1100V	4.95

Circle 94 on reader service card

OEM SPECIALS

1N270	.10	2N960	.55	2N2219A	.30	2N2913	.75	2N3740	1.00	2N4401	.20
1N914	.10	2N962	.40	2N2221	.25	2N2914	1.20	2N3771	1.75	2N4402	.20
		2N967	.50	2N2221A	.30	2N2916A	3.65	2N3772	1.90	2N4403	.20
2N173	1.75	2N1136	1.35	2N2222	.25	2N3019	.50	2N3773	3.00	2N4409	.20
2N178	.90	2N1142	2.25	2N2222A	.30	2N3053	.30	2N3819	.32	2N4410	.25
2N327A	1.15	2N1302	.25	2N2270	.40	2N3054	.70	2N3823	.70	2N4416	.75
2N334	1.20	2N1305	.30	2N2322	1.00	2N3055	.75	2N3856	.20	2N4441	.85
2N336	.90	2N1377	.75	2N2323	1.00	2N3227	1.00	2N3866	.85	2N4442	.90
2N338A	1.05	2N1420	.20	2N2324	1.35	2N3247	3.40	2N3903	.20	2N4443	1.20
2N398B	.90	2N1483	.95	2N2325	2.00	2N3250	.50	2N3904	.20	2N4852	.55
2N404	.30	2N1540	.90	2N2326	2.85	2N3375	6.50	2N3905	.20	2N5061	.30
2N443	1.75	2N1543	2.70	2N2327	3.80	2N3393	.20	2N3906	.25	2N5064	.50
2N456	1.10	2N1544	.80	2N2328	4.20	2N3394	.17	2N3925	3.75	2N5130	.20
2N501A	3.00	2N1549	1.25	2N2329	4.75	2N3414	.17	2N3954	3.50	2N5133	.15
2N508A	.45	2N1551	2.50	2N2368	.25	2N3415	.18	2N3954A	3.75	2N5138	.15
2N555	.45	2N1552	3.25	2N2369	.25	2N3416	.19	2N3955	2.45	2N5198	3.75
2N652A	.85	2N1554	1.25	2N2484	.32	2N3417	.20	2N3957	1.25	2N5294	.50
2N677C	6.00	2N1557	1.15	2N2712	.18	2N3442	1.85	2N3958	1.20	2N5296	.50
2N706	.25	2N1560	2.80	2N2894	.40	2N3553	1.50	2N4037	.60	2N5306	.20
2N706B	.40	2N1605	.35	2N2903	3.30	2N3563	.20	2N4093	.85	2N5354	.20
2N711	.50	2N1613	.30	2N2904	.25	2N3565	.20	2N4124	.20	2N5369	.20
2N711B	.60	2N1711	.30	2N2904A	.30	2N3638	.20	2N4126	.20	2N5400	.40
2N718	.25	2N1907	4.10	2N2905	.25	2N3642	.20	2N4141	.20	2N5401	.50
2N718A	.30	2N2060	1.85	2N2905A	.30	2N3643	.15	2N4142	.20	2N5457	.35
2N720A	.50	2N2102	.40	2N2906	.25	2N3645	.15	2N4143	.20	2N5458	.30
2N918	.35	2N2118	.25	2N2906A	.30	2N3646	.14	2N4220A	.45	C103Y	.25
2N930	.25	2N218A	.30	2N2907	.25	2N3730	1.50	2N4234	.95	C103D	.40
2N956	.30	2N2219	.25	2N2907A	.30	2N3731	2.75	2N4400	.20	C106b1	.50
										C106d1	.75

SILICON UNIUNCTIONS

2N2646	.50	2N4871	.50
2N2647	.60	2N4891	.50
2N6027	.55	2N4892	.50
2N6028	.70	2N4893	.50
D5E37	.25	2N4894	.50
2N2160	.65	MU10	.40
2N4870	.50		

INTEGRATED CIRC.

UA703C	.40
709C OP. AMP.	.25
741C OP. AMP.	.25
7400	.15
7404n	.18
7430n	.19
9700/74LS00	.35

TTL PLASTIC DUAL-IN-LINE I.C.

SN7400N	.15	SN74126N	.49
SN7401N	.15	SN74128N	.84
SN7402N	.15	SN74132N	.99
SN7403N	.15	SN74136N	.64
SN7404N	.18	SN74141N	.93
SN7405N	.18	SN74142N	3.70
SN7406N	.34	SN74143N	3.98
SN7407N	.34	SN74144N	3.78
SN7408N	.18	SN74145N	.98
SN7409N	.18	SN74147N	2.30
SN7410N	.15	SN74148N	1.90
SN7412N	.30	SN74150N	1.94
SN7413N	.45	SN74151N	.64
SN7414N	.99	SN74153N	8.75
SN7416N	.27	SN74154N	1.04
SN7417N	.32	SN74155N	.79
SN7420N	.15	SN74156N	.74
SN7422N	.15	SN74157N	.65
SN7423N	.27	SN74159N	3.50
SN7425N	.27	SN74160N	.99
SN7426N	.24	SN74161N	.99
SN7427N	.27	SN74162N	.99
SN7428N	.39	SN74163N	.99
SN7430N	.15	SN74164N	1.10
SN7432N	.24	SN74165N	1.10
SN7433N	.37	SN74166N	1.28
SN7437N	.25	SN74167N	2.98
SN7438N	.25	SN74170N	2.15
SN7439N	.48	SN74172N	8.75
SN7442N	.48	SN74173N	1.30
SN7443N	.85	SN74174N	1.05
SN7444N	.85	SN74175N	.90
SN7445N	.79	SN74176N	.79
SN7446N	.79	SN74177N	.79
SN7447AN	.79	SN74181N	1.95
SN7448N	.79	SN74182N	.72
SN7450N	.15	SN74180N	.72
SN7451N	.15	SN74181N	2.25
SN7453N	.15	SN74182N	.69
SN7454N	.15	SN74184N	1.95
SN7460N	.15	SN74185AN	1.85
SN7470N	.28	SN74186N	13.95
SN7472N	.32	SN74188N	1.95
SN7473N	.32	SN74190N	1.15
SN7474N	.32	SN74191N	1.15
SN7475N	.48	SN74192N	1.05
SN7476N	.34	SN74193N	1.05
SN7480N	.44	SN74194N	.99
SN7481AN	.99	SN74195N	.72
SN7482N	.99	SN74196N	.99
SN7483AN	.74	SN74197N	.87
SN7484AN	1.95	SN74198N	1.69
SN7485N	.99	SN74199N	1.69
SN7486N	.33	SN74221N	1.50
SN7489N	2.24	SN74246N	1.95
SN7490AN	.47	SN74247N	1.95
SN7491AN	.69	SN74248N	1.75
SN7492AN	.48	SN74249N	1.75
SN7493AN	.47	SN74251N	1.40
SN7494N	.76	SN74256N	.85
SN7495AN	.72	SN74278N	2.45
SN7496N	.75	SN74279N	.85
SN7497N	2.85	SN74283N	1.75
SN74100N	1.20	SN74284N	4.50
SN74104N	.43	SN74285N	4.50
SN74105N	.43	SN74290N	.85
SN74107N	.30	SN74293N	.85
SN74109N	.74	SN74298N	1.98
SN74110N	.54	SN74351N	1.92
SN74111N	.74	SN74355N	.69
SN74116N	.99	SN74366N	.69
SN74120N	1.40	SN74367N	.95
SN74121N	.37	SN74368N	.69
SN74122N	.42	SN74390N	1.40
SN74123N	.68	SN74393N	1.40
SN74125N	.49	SN74490N	1.90

TTL LOW POWER SCHOTTKY PLASTIC DUAL-IN-LINE I.C.

SN74LS00N	.29	SN74LS83AN	1.49
SN74LS01N	.29	SN74LS85N	1.75
SN74LS02N	.29	SN74LS86N	.59
SN74LS03N	.29	SN74LS90N	1.15
SN74LS04N	.35	SN74LS91N	1.25
SN74LS05N	.35	SN74LS92N	1.15
SN74LS08N	.20	SN74LS93BN	1.15
SN74LS09N	.29	SN74LS95AN	1.60
SN74LS10N	.29	SN74LS96N	1.75
SN74LS11N	.29	SN74LS107N	.59
SN74LS12N	.29	SN74LS109N	.59
SN74LS13N	.35	SN74LS121N	.59
SN74LS14N	1.48	SN74LS133N	.59
SN74LS15N	.29	SN74LS144N	.59
SN74LS20N	.29	SN74LS122N	.90
SN74LS21N	.29	SN74LS123N	1.10
SN74LS22N	.29	SN74LS124N	3.00
SN74LS26N	.40	SN74LS125N	.75
SN74LS27N	.35	SN74LS126N	.75
SN74LS28N	.35	SN74LS132N	1.25
SN74LS30N	.29	SN74LS136N	.59
SN74LS32N	.40	SN74LS138N	1.68
SN74LS33N	.40	SN74LS139N	1.68
SN74LS37N	.40	SN74LS145N	1.35
SN74LS38N	.40	SN74LS151N	1.30
SN74LS40N	.35	SN74LS153N	1.30
SN74LS42N	1.20	SN74LS155N	1.45
SN74LS47A	1.20	SN74LS156N	1.45
SN74LS48N	1.20	SN74LS157N	1.35
SN74LS49N	1.20	SN74LS158N	1.25
SN74LS51N	.29	SN74LS160N	2.25
SN74LS54N	.29	SN74LS161N	2.25
SN74LS55N	.29	SN74LS162N	2.25
SN74LS63N	1.75	SN74LS163N	2.25
SN74LS73N	.49	SN74LS164N	1.98
SN74LS74N	.55	SN74LS168N	2.75
SN74LS75N	.75	SN74LS169N	2.75
SN74LS76N	.49	SN74LS170N	2.95
SN74LS78N	.49	SN74LS174N	1.45

C/MOS

CD4000AE	.15	CD4002AE	.19
CD4001AE	.19	CD4003AE	1.30
CD4002AE	.19	CD4004AE	.19
CD4006AE	1.30	CD4008AE	.99
CD4007AE	.19	CD4009AE	.48
CD4008AE	.99	CD4010AE	.48
CD4009AE	.48	CD4011AE	.19
CD4010AE	.48	CD4012AE	.19
CD4011AE	.19	CD4013AE	.42
CD4012AE	.19	CD4014AE	.42
CD4013AE	.42	CD4015AE	1.15
CD4014AE	.42	CD4016AE	.42
CD4015AE	1.15	CD4017AE	1.15
CD4016AE	.42	CD4018AE	1.19
CD4017AE	1.15	CD4019AE	.45
CD4018AE	1.19	CD4021AE	1.20
CD4019AE	.45	CD4022AE	1.05
CD4021AE	1.20	CD4023AE	.19
CD4022AE	1.05	CD4024AE	.85
CD4023AE	.19	CD4025AE	.19
CD4024AE	.85	CD4026AE	1.75
CD4025AE	.19	CD4027AE	1.75
CD4026AE	1.75	CD4028AE	.85
CD4027AE	1.75	CD4029AE	.99
CD4028AE	.85	CD4030AE	.42
CD4029AE	.99	CD4033AE	1.80
CD4030AE	.42	CD4035AE	1.20
CD4033AE	1.80	CD4040AE	1.20
CD4035AE	1.20	CD4042AE	.70
CD4040AE	1.20	CD4043AE	.35
CD4042AE	.70	CD4044AE	.50
CD4043AE	.35	CD4049AE	.45
CD4044AE	.50	CD4050AE	.45
CD4049AE	.45	CD4051AE	1.25
CD4050AE	.45	CD4052AE	1.25
CD4051AE	1.25	CD4053AE	1.25
CD4052AE	1.25	CD4055AE	1.50
CD4053AE	1.25	CD4056AE	1.50
CD4055AE	1.50	CD4060AE	1.75
CD4056AE	1.50	CD4066AE	.70
CD4060AE	1.75	CD4069AE	.29
CD4066AE	.70	CD4071AE	.35
CD4069AE	.29	CD4072AE	.25
CD4071AE	.35	CD4073AE	.35
CD4072AE	.25	CD4075AE	.35
CD4073AE	.35	CD4076AE	1.24
CD4075AE	.35	CD4081AE	.25
CD4076AE	1.24	CD4082AE	.35
CD4081AE	.25	CD40502AE	1.25
CD4082AE	.35	CD40507AE	.60
CD40502AE	1.25	CD40508AE	3.00
CD40507AE	.60	CD40510AE	1.24
CD40508AE	3.00	CD40511AE	.75
CD40510AE	1.24	CD40512AE	1.95
CD40511AE	.75	CD40514AE	2.25
CD40512AE	1.95	CD40515AE	2.25
CD40514AE	2.25	CD40516AE	1.25
CD40515AE	2.25	CD40518AE	.95
CD40516AE	1.25	CD40519AE	.95
CD40518AE	.95	CD40520AE	.99
CD40519AE	.95	CD40528AE	1.25
CD40520AE	.99	CD40585AE	1.95
CD40528AE	1.25		
CD40585AE	1.95		

LED'S

LITRONIX		DL16	6.70
DL16	6.70	DL34M	7.25
DL34M	7.25	DL44M	5.25
DL44M	5.25	DL57	6.98
DL57	6.98	DL701	1.95
DL701	1.95	DL702	1.95
DL702	1.95	DL704	2.30
DL704	2.30	DL707	1.70
DL707	1.70	DL727	4.75
DL727	4.75	DL746	2.75
DL746	2.75	DL747	2.45
DL747	2.45	DL749	2.75
DL749	2.75	DL750	2.75
DL750	2.75	IL-1	1.05
IL-1	1.05	IL-5	1.15
IL-5	1.15	IL-12	.69
IL-12	.69	IL-15	1.25
IL-15	1.25	IL-16	1.40
IL-16	1.40	IL-17A	.82
IL-17A	.82	IL-100	5.45
IL-100	5.45	ILD-74	1.61
ILD-74	1.61	ILQ-74	3.10
ILQ-74	3.10	ILA-30	1.29
ILA-30	1.29	ILA-55	1.42
ILA-55	1.42	ILCA-2-30	1.60
ILCA-2-30	1.60	ILCA-2-55	1.75
ILCA-2-55	1.75	ILCT-6	2.20
ILCT-6	2.20	RL2	.23
RL2	.23	RL2-02	.48
RL2-02	.48	RL2-03	.48
RL2-03	.48	RL2-04	.48
RL2-04	.48	RL20-02	.48
RL20-02	.48	RL20-03	.48
RL20-03	.48	RL20-04	.48
RL20-04	.48	RL21	.42
RL21	.42	RL21-02	.42
RL21-02	.42	RL1-04	.42
RL1-04	.42	RL250	.28
RL250	.28	RL50-01	.28
RL50-01	.28	RL50-02	.28
RL50-02	.28	RL50-03	.28
RL50-03	.28	RL54	.21
RL54	.21	RL55	.29
RL55	.29	RL55-5	.21
RL55-5	.21	RL209	.29
RL209	.29	RL-2000	.39
RL-2000	.39	RL-4403	.32
RL-4403	.32	RL-4415	.55
RL-4415	.55	RL-4484	.19
RL-4484	.19	RL-5054-1	.52
RL-5054-1	.52	RL-5054-2	.52
RL-5054-2	.52	RL-5054-5	.19
RL-5054-5	.19	GL-56	.60
GL-56	.60	GL-4484	.75
GL-4484	.75	GL-4850	.75
GL-4850	.75	GL-30	.33
GL-30	.33	GL-1	.30
GL-1	.30	RLC-200	.54
RLC-200	.54	RLC-201	.54
RLC-201	.54	RLC-210	.59
RLC-210	.59	RLC-400	.53
RLC-400	.53	RLC-410	.59
RLC-410	.59	IRL-40	1.30
IRL-40	1.30	IRL-60	.53
IRL-60	.53	ARL-18	3.75
ARL-18	3.75	LPT-100	.59
LPT-100	.59	LPT-100A	.69
LPT-100A	.69	LPT-100B	.84
LPT-100B	.84	LPT-110	.74
LPT-110	.74	LPT-110A	.94
LPT-110A	.94	LPT-110B	1.09
LPT-110B	1.09	OPCOA	
OPCOA		LLL7	.19
LLL7	.19	LSL16L	.35
LSL16L	.35	LSL26L	.35
LSL26L	.35	LSL13L	.30
LSL13L	.30	LSL3L	.45
LSL3L	.45	LSL4L	.75
LSL4L	.75	LSL8L-1	.65
LSL8L-1	.65	LSM6	
LSM6		OPL211	.25
OPL211	.25	OPL212	.25
OPL212	.25	OSL1	.55
OSL1	.55	OSL16L	.35
OSL16L	.35	SLA7	2.95
SLA7	2.95	TEXAS INSTRUMENTS	
TEXAS INSTRUMENTS		TL1103	7.00
TL1103	7.00	TL1111	1.20
TL1111	1.20	TL1112	.99
TL1112	.99	TL1208	.65
TL1208	.65	TL1209A	.19
TL1209A	.19	TL1211	.45
TL1211	.45	TL1220	.24
TL1220	.24	TL1221	.22
TL1221	.22	TL1222	.49
TL1222	.49	TL1223	.49
TL1223	.49	TL1302	4.95
TL1302	4.95	TL1303	4.95
TL1303	4.95	TL1304	4.95
TL1304	4.95	TL1305	7.95
TL1305	7.95	TL1306	8.95
TL1306	8.95	TL1308	8.95
TL1308	8.95	TL1309	8.95
TL1309	8.95	TL1311	11.95
TL1311	11.95	TL1312	1.70
TL1312			

CRYSTALS

THESE FREQUENCIES ONLY

Part #	Frequency	Case/Style	Price
CY1A	1.000 MHz	HC33/U	\$4.95
CY2A	2.000 MHz	HC33/U	\$4.95
CY3A	4.000 MHz	HC18/U	\$4.95
CY7A	5.000 MHz	HC18/U	\$4.95
CY12A	10.000 MHz	HC18/U	\$4.95
CY14A	14.31818 MHz	HC18/U	\$4.95
CY19A	18.000 MHz	HC18/U	\$4.95
CY22A	20.000 MHz	HC18/U	\$4.95
CY30B	32.000 MHz	HC18/U	\$4.95

CLOCK CHIPS — CALCULATOR CHIPS

MMS309	6 Digit, BCD Outputs, Reset Pin.	\$5.95
MMS311	6 Digit, DVM Outputs, 12 or 24 Hour	4.95
MMS312	4 Digit, BCD Outputs, 1PPS Output	4.95
MMS313	6 Digit, BCD Outputs, 1PPS Output	4.95
MMS314	6 Digit, 12 or 24 Hour, 50 or 60 Hz	4.95
MMS316	4 Digit, Alarm, 1PPS Output	6.95
MMS318	Video Clock Chip For Use With MMS541	9.95
CT7001	6 Digit, Calendar, Alarm, 12 or 24 Hour	6.95

CALCULATOR CHIPS

MMS725	6 Digit, Four Function, Less Decimal	\$2.95
MMS738	8 Digit, 5 Function, +, -, x, ÷, %	2.95
MMS739	8 Digit, 5 Function, Floating Decimal	2.95
CT5001	12 Digit, 4 Function	3.95
CT5005	12 Digit, 4 Function with Memory	5.95
CT5030	12 Digit, 4 Function and %	7.95

MISC. MOS

MMS320	TV Camera Sync Generator	\$19.95
MMS330	4 1/2 Digit DVM Chip	9.95
MMS369	60 Hz Timebase Circuit From 3.58 MHz	5.00
MMS841	Video Generator For MMS518	18.00
MCI-108-L7	7.88 Digital to Analog Converter	9.95
MMS207	4 Digit Counter with Latches	10.95
LD10L0111	3 1/2 Digit DVM Chip Set	25.00
95H90	100 MHz, 10 Counter For Prescalers	13.95

Continental Specialties

PROTO BOARDS

Build & test circuits as fast as you think!

PB100	10 IC Cap breadboard kit, 4 1/2 x 6.0 x 1.35"	\$19.95
PB101	10 14-DIP cap, 5-way post, 940 solderless tie points, 5.6 x 4.5"	\$29.95
PB102	12 14-DIP cap, like PB101 with 1 240 tie points, 7.0 x 4.5"	\$39.95
PB103	24 14-DIP cap, 4 5-way posts, 2 250 tie points, 8.0 x 9.0"	\$59.95
PB104	32 14-DIP cap, 3050 solderless tie points, 8.0 x 9.75"	\$79.95

PROTO-CLIP

For power-on/hands-off signal tracing. Static and dynamic logic states of TTL, TTL, HTL or CMOS DIP ICs. Pocket size \$84.95

LOGIC MONITOR

Simultaneously displays static and dynamic logic states of TTL, TTL, HTL or CMOS DIP ICs. Pocket size \$84.95

SOCKETS & BUS STRIPS

Plug in wire test, modify or expand without patch cords or solder. Snap together to form breadboard needed.

Part Description	Pin	18	24	30	36	42	48	54	60	66	72	78	84	90	96	102	108	114	120
DT595 Socket	5.5	6.2	7.0	7.8	8.6	9.4	10.2	11.0	11.8	12.6	13.4	14.2	15.0	15.8	16.6	17.4	18.2	19.0	19.8
DT598 Bus	6.5	5.2	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0
DT475 Socket	5.3	5.0	4.7	4.4	4.1	3.8	3.5	3.2	2.9	2.6	2.3	2.0	1.7	1.4	1.1	0.8	0.5	0.2	0.0
DT478 Bus	5.3	5.0	4.7	4.4	4.1	3.8	3.5	3.2	2.9	2.6	2.3	2.0	1.7	1.4	1.1	0.8	0.5	0.2	0.0
DT355 Socket	4.1	3.8	3.5	3.2	2.9	2.6	2.3	2.0	1.7	1.4	1.1	0.8	0.5	0.2	0.0	0.0	0.0	0.0	0.0
DT358 Bus	4.1	3.8	3.5	3.2	2.9	2.6	2.3	2.0	1.7	1.4	1.1	0.8	0.5	0.2	0.0	0.0	0.0	0.0	0.0
DT185 Socket	2.4	2.1	1.8	1.5	1.2	0.9	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
DT185 Socket	1.8	1.5	1.2	0.9	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
DT185 Socket	1.4	1.1	0.8	0.5	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
DT75 Socket	1.3	1.0	0.7	0.4	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

1/16 VECTOR BOARD

Material	Part No.	50 pins	75 pins	100 pins	125 pins	150 pins	175 pins	200 pins
PHENOLIC	64P44 062XXXP	4.50	6.50	1.72	1.54			
	169P44 02XXXXP	4.50	17.00	3.69	3.32			
EPKDY	64P44 062	4.50	6.50	2.07	1.86			
GLASS	84P44 062	4.50	8.50	2.56	2.31			
	169P44 062	4.50	17.00	5.04	4.53			
	169P44 062	8.50	17.00	9.23	8.26			
EPKDY GLASS COPPER CLAD	169P44 062C1	4.50	17.00	6.80	6.12			

VECTOR TERMINALS

Series	Part No.	Finish	Post Size	Gold	Tin	Gold	Tin	50 pins
T44	T44-1	T14	025 sq	1.50 lot	1.00 lot	2.75 lot	1.75 lot	1.75 lot
T46	T46-1	T46	028 sq	1.75 lot	1.25 lot	3.00 lot	2.25 lot	2.25 lot
T49	T49A	T49	025 sq	1.75 lot	1.25 lot	3.10 lot	2.25 lot	2.25 lot

VECTOR WIRING PENCIL

Vector Wiring Pencil P173 consists of a hand held leather-wrapped (under one ounce) tool which is used to guide and wrap insulated wire, fast off a self-contained replaceable bobbin, onto component leads or terminals installed on pre-punched "P" Pattern Vectorboards. Connections between the wrapped wire and component leads, pads or terminals are made by soldering. Complete with 250 FT of wire pencil.

\$9.50

REPLACEMENT WIRE — BOBBINS FOR WIRING PENCIL

W36-3-A-Pkg	3	250 ft. 36 AWG GREEN	\$2.40
W36-3-B-Pkg	3	250 ft. 36 AWG RED	\$2.40
W36-3-C-Pkg	3	250 ft. 36 AWG CLEAR	\$2.40
W36-3-D-Pkg	3	250 ft. 36 AWG BLUE	\$2.40

100 PER STRIP

MOLEX PINS

Intended for use as an inexpensive substitute for IC sockets. Also perfect for use as board connectors and in subassemblies.

SPECIAL — 100/1.49 — 1000/12.00

64 KEY KEYBOARD

The ideal item for the real homebrew computer hobbyist. This keyboard features 64 unenclosed SPST keys, unattached to any kind of P.C.B. A very solid molded plastic 13" x 4" base suits most applications.

\$24.95 ea.

JOYSTICK

These joysticks feature 100K potentiometers, that vary resistance proportional to the angle of the stick. Sturdy metal construction with plastics components only at the movable joint. Perfect for electronic games and instrumentation.

\$9.95 ea.

MICROPROCESSOR COMPONENTS

8080A \$37.95

8080 SUPPORT DEVICES

8212	8 BIT INPUT/OUTPUT PORT FOR 8080	\$ 5.95
8224	CLOCK GENERATOR AND DRIVER FOR 8080	12.95
8228	SYSTEM CONTROLLER AND BUS DRIVER FOR 8080	12.95

Part #	CPU'S	Price	RAM'S	Price	
8008	8 BIT CPU	\$19.95	256 x 1	FAST \$ 5.00	
8080	Super 8008	24.95	256 x 1	Static \$ 2.25	
8080A	Super 8008	37.95	1024 x 1	Dynamic 2.95	
			256 x 1	Static 6.95	
			1024 x 1	Static 1.95	
2504	1024 Dynamic	\$ 9.00	4096 x 1	Dynamic 19.95	
2518	Hex 32 BIT	7.00	2111	256 x 4	Static 7.95
2519	Hex 40 BIT	4.00	7010	1024 x 4	MNOS 29.95
2524	512 Dynamic	2.95	7489	18 x 4	Static 2.49
2525	1024 Dynamic	6.00	8101	256 x 4	Static 7.95
2527	Dual 256 BIT	3.95	8111	256 x 4	Static 7.95
2529	Dual 512 BIT	4.00	8599	16 x 4	Static 3.49
2532	Quad 80 BIT	3.95	91102	1024 x 1	Static 2.49
2533	1024 Static	7.95	74200	256 x 1	Static 6.95
3341	Flo	6.95	93410	256 x 1	Static 1.75
74LS670	16 x 4 RGT	3.95	5262	2048 x 1	Dynamic 2.95
					HPROM 5.00
AY-5-1013	20K Baud	\$ 6.95	1024	1024 x 1	FAMOS \$15.95
					FAMOS 14.95
2513	Char Gen	\$11.00	2048	32 x 8	Ouen C 5.00
7488	Random Bits	3.90	82523	32 x 8	Tristate 5.00
					825123 32 x 8 5.00

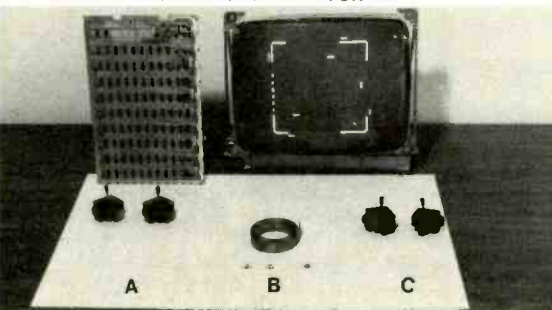
BUILD YOUR OWN JOLT MICROCOMPUTER IN JUST 3 HOURS OR LESS FOR \$159.95

A COMPLETE MICROCOMPUTER IN A SINGLE CPU KIT INCLUDES: • An MOS Technology MCS6502 NMOS microprocessor • 512 bytes of program RAM, and 64 bytes of interrupt vector RAM • 1K bytes of mask programmed ROM containing DEMON, a powerful debug monitor • 26 programmable I/O lines • Internal RC clock, or crystal controlled clock with user supplied crystal • Serial I/O ports for use with a teleprinter current loop drive/receiver, or an EIA standard driver/receiver • Expandable address and data buses • Hardware interrupt • Control panel interface lines available on card connector • Complete assembly manuals and sample programs

JOLT ACCESSORY KITS

JOLT RAM CARD — Fully static 4,096 bytes of RAM with 1 microsecond access time and on-board decoding \$199.95
JOLT I/O Card (Peripheral Interface Adapter) — 2 PIA LSI chips, 32 I/O lines, four interrupt lines, on-board decoding and standard TTL drive. Fully programmable \$95.50
JOLT Power Supply — Operates at +5, +12 and -10 Volts. Supports JOLT CPU, 4K bytes of RAM and JOLT I/O card, or CPU and 8 I/O cards. \$99.95
JOLT +5V Booster Option — Fits onto JOLT Power Supply card. Supports CPU, 8K bytes RAM and 8 I/O CPU and cards. \$24.95
JOLT Universal Card — Same size (4 1/4" x 7"), same form factor as other JOLT cards. Completely blank, drilled to accept 14, 16, 24 or 40 pin sockets, 24.95
JOLT Accessory Bag — Contains enough hardware to connect one JOLT card to another, flat cable, connectors, card spacers, hardware, etc. \$39.95
JOLT Resident Assembler — Fully symbolic, single pass resident assembler, all memories compatible with timesharing assemblers. Delivered on four 1702A PROMs, ready for plugging into JOLT PROM card. \$149.95
JOLT 1702A PROM Card — Sockets for 2,048 bytes of PROM memory. Place anywhere in memory with jumper selectable addresses. \$99.95

NOW: YOUR OWN VIDEO GAME FOR THE ENTIRE FAMILY



This game comes pre-tested with two PROFESSIONAL Kraft joysticks. Joysticks allow 2 dimensional player control (rather than only one dimension, such as up and down.) If you require more than two players, order extra joysticks. All that's required is a 5V/2A power supply, a harness, and speaker. Comes with schematics, wiring information, and all necessary documentation. Game gives TV composite video output, perfect for any TV monitor. Game designed so one, two, three, or four players can play at the same time. You can even play against the HOUSE. Score for each person is shown on TV-set. These boards are production over runs of a well known video game manufacturer, and are not rejects, or in any way inferior to one presently being sold in games for over \$1,000.00.

KIT A — \$179.95 PROFESSIONAL game P.C. board, and 2 PROFESSIONAL joysticks. P.C. board size is 10 1/2" x 17". This is the same PROFESSIONAL game as seen in commercial establishments. Don't confuse it with the simple games sold in stores, or with analog kits.
ACCESSORY B — \$3.95 Six feet of ribbon cable, three SPST switches (coin simulator, house/player, and start switch), for those of you who don't have extra wire or switches to build the harness.
ACCESSORY C — \$39.95 Two additional PROFESSIONAL Kraft joysticks, for third and fourth player.

DIGITAL CLOCK KIT — 3 1/2 INCH DIGITS

This clock features big 3 1/2" high digits for viewing in offices, auditoriums, etc. Each digit is formed by 31 bright 0.2" LED's. The clock operates from 117 VAC, has either 12 or 24 hr. operation. The 6 digit versions are 2 1/2" x 3 1/2" x 1 1/2", and the 4 digit is 1 1/2" x 3 1/2" x 1 1/2". Kits come complete with all components, case and transformer.
4 DIGIT KIT \$49.95 **4 DIGIT ASSEMBLED \$59.95**
6 DIGIT KIT \$69.95 **6 DIGIT ASSEMBLED \$79.95**
 Specify 12 Or 24 Hr. When Ordering

Satisfaction Guaranteed. \$5.00 Min. Order. U.S. Funds.
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AUTOTEL™ WARNING LIGHTS ARE NOT ENOUGH



AN AUDIBLE ALARM INDICATING POTENTIAL ENGINE DAMAGE

AUTOTEL is an efficient (15 ma current standby) device by which every owner of an automobile, truck or vehicle equipped with indicator lights for temperature and oil pressure can be assured of a reliable warning before an impending failure.

AUTOTEL, by means of an audible signal (70 db pulsing) immediately forewarns the vehicle operator of a malfunction or failure, allowing time to correct and prevent major engine failures. It is programmed so there is no sound during normal operating conditions.

AUTOTEL features CMOS circuitry, packaged in a 2 1/2" sq. x 1/2" case. The kit comes complete with all components, hardware and case to hook directly into your car's warning light system.

\$14.95 Assembled \$9.95 Per Kit

3 1/2 DIGIT DVM KIT



This 0-2 VDC, 0.5 percent digital voltmeter features the Motorola 3 1/2 digit DVM chip set. It has a 4" LED display and operates from a single +5V power supply. The unit is provided complete with an injection molded black plastic case complete with Bezel. An optional power supply is available which fits into the same case as the 0-2V DVM allowing 117 VAC operation.

A. 0-2V DVM with Case \$49.95
B. 5V Power Supply \$14.95

JE700 CLOCK

The JE700 is a low cost digital clock, but is a very high quality unit. The unit features a simulated walnut case with dimensions of 6" x 2 1/2" x 1 1/2". It utilizes a MAN72 high brightness readout, and the MMS314 clock chip.

12 or 24 Hour \$19.95

Liquid Crystal Temperature Display
 Six Digit Light Emitting Diode Display DL 33 Display

This clock makes an attractive addition to any desk. It has an extruded, black anodized aluminum case. It displays hours, minutes, and seconds with 11 inch displays, and comes complete with a liquid crystal thermometer. It operates off 115 VAC at 50 or 60 Hz. \$24.95

KIT - ALL COMPONENTS & CASE \$34.95 WIRED & ASSEMBLED \$39.95

This large digit clock (6" hours & minutes, 3" seconds) features the MMS314 clock chip. It operates from 117 VAC, and will operate in either a 12 or 24 hour mode. The clock is complete with a walnut grain case, and has fast set, slow set, and hold time set features.

KIT - ALL COMPONENTS & CASE \$34.95
 WIRED & ASSEMBLED \$39.95

JE803 PROBE

The Logic Probe is a unit which is for the most part indispensable in trouble shooting logic families. TTL, TTL, HTL, CMOS. It derives the circuit under test, drawing a scan 10 mA max. It uses a MAN72 readout to indicate any of the following states by these symbols: (H) - 1 (LOW) - 0 (PULSE) - P. The Probe can detect high frequency pulses to

7400N TTL

SN7400N*	13	SN7453N	27	SN74150N	100
SN7401N	16	SN7454N	20	SN74151N	99
SN7402N	21	SN7455A	22	SN74152N	89
SN7403N	16	SN7460N	22	SN74154N*	1.25
SN7404N*	16	SN7470N	45	SN74155N	99
SN7405N	24	SN7471N*	69	SN74156N	99
SN7406N	20	SN7472N*	39	SN74157N	99
SN7407N	29	SN7473N*	37	SN74160N	1.25
SN7408N	25	SN7474N*	32	SN74161N	99
SN7409N	25	SN7475N*	50	SN74163N	99
SN7410N*	16	SN7476N*	32	SN74165N	1.10
SN7411N	30	SN7479N*	5.00	SN74166N	1.25
SN7412N	33	SN7480N	50	SN74167N	1.25
SN7413N	45	SN7482N	98	SN74167N	5.50
SN7414N	70	SN7483N	70	SN74172N	2.10
SN7416N	35	SN7484N	89	SN74172N	11.75
SN7417N	35	SN7486N	39	SN74173N	1.50
SN7420N	21	SN7488N	3.50	SN74174N	1.25
SN7421N	33	SN7489N	2.25	SN74175N	99
SN7422N*	49	SN7490N	45	SN74182N	99
SN7423N*	27	SN7491N	75	SN74177N	90
SN7425N	39	SN7492N	48	SN74180N	99
SN7426N	29	SN7493N*	49	SN74181N	2.49
SN7427N	37	SN7494N	79	SN74182N	99
SN7429N	42	SN7495N	79	SN74184N	1.95
SN7430N	36	SN7496N	89	SN74185N	2.20
SN7432N	31	SN7497N*	4.00	SN74186N	5.00
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MAN 2	MAN 3	MAN 7

DL707	DL707	DL707
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24 pin	5-17	16	15
24 pin	20	19	18
24 pin	22	21	20
24 pin	29	28	27
24 pin	37	36	35

24 pin	1-24	25-49	50-100
24 pin	5-17	16	15
24 pin	20	19	18
24 pin	22	21	20
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7443	63	74153	65	75454	61	4042	79	NE565A	128
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100uf/25v .11 1.10/10	33uf/16v .12 1.00/10	1000uf/25v .56 4.50/10
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1N4002	66/10	5.60/C	1N4006	90/10	7.75/C
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100uf/500v .04 37/10		
220uf/500v .04 37/10		
100uf/500v .04 37/10		
30uf/500v .06 50/10		
1uf/500v .03 24/10		
0.047uf/25v .03 28/10		
0.047uf/25v .05 42/10		
1uf/25v .08 62/10		

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1N5278B 3.3v .15 \$11/C	1N5238B 9.1v .15 \$11/C
1N5278B 3.3v .15 \$11/C	1N5239B 10v .15 \$11/C
1N5278B 3.3v .15 \$11/C	1N5240B 10v .15 \$11/C
1N5278B 3.3v .15 \$11/C	1N5241B 11v .15 \$11/C
1N5278B 3.3v .15 \$11/C	1N5242B 12v .15 \$11/C
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3.3	5	100	10	1.5K	10	15K	10	150K	10	2.2M	5	2.2M	5
6.8	5	150	10	2.2K	20	22K	10	220K	10	3.3M	5	3.3M	5
10	10	220	10	2.7K	10	27K	10	270K	10	4.7M	5	4.7M	5
15	5	270	5	3.3K	10	33K	10	330K	10				
22	5	330	10	3.9K	10	39K	10	390K	10				
33	5	470	20	4.7K	10	47K	10	470K	10				
47	10	680	10	6.8K	10	68K	10	680K	20				

RESISTOR ASSORTMENT

R (OHMS)

R QTY R QTY R QTY R QTY R QTY

R QTY R QTY R QTY R QTY R QTY

R QTY R QTY R QTY R QTY R QTY

R QTY R QTY R QTY R QTY R QTY

R QTY R QTY R QTY R QTY R QTY

R QTY R QTY R QTY R QTY R QTY

R QTY R QTY R QTY R QTY R QTY

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IN 756A	Zener	8.2V	.25	10/ 1.50
IN 904	Sw. Diode	30V	.10	10/ .65
IN 914	Sw. Diode	100V	.10	10/ .75
IN 967B	Zener	18V	.25	10/ 1.50
IN 2990A	Zener	33V	.25	10/ 1.50
	(Stud Mt.)	1.25	10/ 7.50	
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IN 3600	Sw. Diode	50V	.20	10/ 1.40
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IN 4148	Sw. Diode	75V	.10	10/ .65
IN 4858	Zener	120V	.25	10/ 1.50
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EACH MINIMUM 10 MINIMUM 100
PER VALUE PER VALUE

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100 - 1000	..	.10	\$0.09
1000 -	..	.10	.08

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23.7	78.7	187	1.15K	13.0K	45.3K
25.5	84.5	191	1.5K	15.0K	48.7K
30.9	105	205	2.49K	18.2K	54.9K
34.8	110	232	3.57K	19.1K	60.4K
40.2	115	243	4.75K	19.6K	64.9K
45.3	127	499	5.49K	22.6K	69.8K
51.1	147	604	6.04K	24.9K	84.5K
61.5	158	715	7.15K	28.0K	
64.9	178	806	8.25K	37.4K	

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7409	.19	7475	.57	74165	1.59
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7413	.55	7485	1.10	74173	1.49
7416	.35	7486	.40	74174	1.62
7417	.35	7489	2.48	74175	1.39
7420	.16	7490	.59	74176	.89
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7423	.29	7492	.71	74180	.90
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7441	.98	74122	.45	74193	1.19
7442	.77	74123	.85	74194	1.25
7443	.87	74125	.54	74195	.89
7444	.87	74126	.63	74196	1.25
7445	.89	74141	1.04	74197	.89
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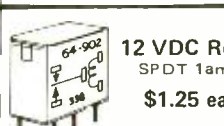
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Time Display	12 Hour	X	X	X	X
	24 Hour	X	X	X	X
Duplicate Register	Alarm Counter	X	X	X	X
	Date Counter	X	X	X	X
	Minute Timer	X	X	X	X
	Second Timer	X	X	X	X
Alarm Signal	Tone	X	X	X	X
	DC Level	X	X	X	X
Alarm Output	Modulated @ 2 GHz	X	X	X	X
	Not Modulated	X	X	X	X
Alarm at Power Failure	ON	X	X	X	X
	OFF	X	X	X	X
Segment Output Polarity	Vss for Display	X	X	X	X
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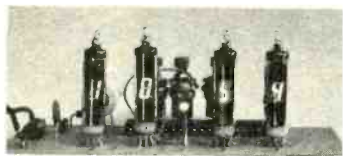
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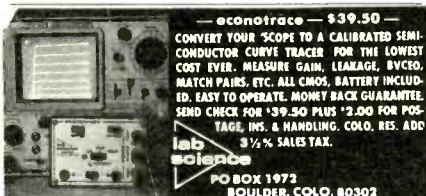
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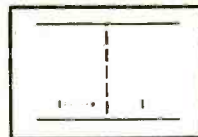
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Let's start with a Tennis "MATCH". Fun for all, particularly beginners. This is the game that started the craze.

Scores to 12 points



GAME 2

Then go to the "PRO MATCH". You'll need 3 paddles to return the ball on this one, almost as fast as a Hockey Puck. A challenge for the 2 players this is designed for.

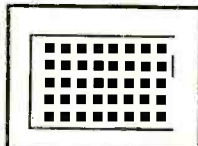
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GAME 3

Now to deflate the ego's of the "Pros" put them to a "GRAVITY MATCH". A bouncing ball adds more fun and excitement plus it plays havoc with the skill of the 2 players.

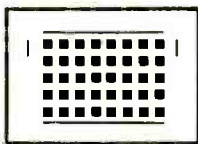
Scores to 12 points.



GAME 4

WIPE OUT I

A game for a single player. Test your reflexes and see how many squares you can knock out. As your score increases so does the speed of the ball. Top Score is 2400 points in 6 tries.



GAME 5

WIPE OUT II

If you can't beat the machine by yourself, get someone to help you. Together you can (that is if it is possible to) score 2800 points in 6 tries.

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566M		2.50
567M	Tone Decoder	2.50
702H	Linear	1.50
703H	RF IF Amp	1.50
709H	Op Amp	1.25
709N	Op Amp	2/1.25
710H	V Comp	1.00
711H	Dual Comp	1.00
711N	Dual Comp	2.00
723H	V Reg	2/1.25
723N	Reg	2/1.25
725H	Ins Op Amp	3.75
733H	Dif Vid Amp	1.00
733N	Dif Vid Amp	1.00
739N	Dual Aud Pre Amp	1.00
740H	FET Op Amp	7.00
741H	Op Amp	2/1.00
741M	Op Amp	2/1.00
747H	Dual Op Amp	1.00
747N	Dual Op Amp	1.50
748H	Op Amp	3/1.25
748M	Op Amp	3/1.25
749N	Dual Aud Pre Amp	1.50
760N	Dif V Comp	3.00
761N	Op Amp	2/1.00
809H	Buffer	3.00
1458M	Dual Op Amp	2/1.15
2909N	Quad Amp	1.00
3085H	TV Snd Sys	2/1.50
3900N	Quad Amp	1.00
4136N	Quad 741	2.00
4558M	Dual 741	1.00

TTL IC's

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74L00	3/1.25
74L02	3/1.25
74L03	2/1.00
74L04	3/1.25
74L10	3/1.25
74L20	3/1.25
74L30	3/1.25
74L42A	2.25
74L51	3/1.25
74L54	3/1.25
74L55	3/1.25
74L71	2/1.25
74L73	2/1.00
74L75	2/1.25
74L86	2/1.35
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74L93	1.50
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74L123	1.00
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	Low Pro	Standard	Wire Wrap
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16	4/1.25	3/1.00	3/1.25
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28	--	3/1.25	2/1.25

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1N747A	3.6V	7/1.00	100/11.00
1N748A	3.9V	7/1.00	100/11.00
1N749A	4.3V	7/1.00	100/11.00
1N750A	4.7V	7/1.00	100/11.00
1N751A	5.1V	6/1.00	100/13.00
1N752A	5.6V	6/1.00	100/13.00
1N753A	6.2V	6/1.00	100/13.00
1N754A	6.8V	6/1.00	100/13.00
1N755A	7.5V	6/1.00	100/13.00
1N756A	8.2V	5/1.00	100/15.00
1N757A	9.1V	5/1.00	100/15.00
1N758A	10V	5/1.00	100/15.00
1N759A	12V	5/1.00	100/15.00

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Asst. 2	
10 each of 5.6, 18, 27, 180, 200, 270, 360, 10K, 470K and 8.2M Ohm Values.	
Asst. 3	
10 each of 10, 18, 51, 180, 360, 1.8K, 3.3K, 18K, 470K, and 1.8M Ohm Values.	
Asst. 4	
10 each of 11, 20, 30, 75, 240, 360, 820, 1.1K, 3.3K, and 120K Ohm Values.	
Asst. 5	
10 each of 10, 18, 75, 150, 180, 270, 330, 910, 4.7K, and 470K Ohm Values.	
Asst. 6	
10 each of 13, 24, 27, 33, 39, 43, 56, 62, 75, 160, and 200 Ohm Values.	
Asst. 7	
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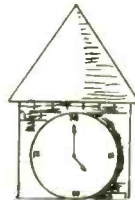
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LM308	95	LM381	1.57	75451	39	555	75		
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7404-22	7491-.79
7405-22	7492-.60
7406-35	7493-.60
7407-33	7494-.80
7408-22	7495-.85
7409-25	7496-.79
7410-22	74107-34
7411-25	74121-50
7412-30	74123-.85
7413-60	74125-.70
7414-1.45	74126-.90
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All PC display boards are multiplexed for adding additional digits.

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FEATURES:

Direct drive display outputs, *Current control regulation on chip, *Low power brightness control on chip, *RFI eliminating slowup circuitry, *Sleep radio feature, *24 hour snooze alarm, *Independent digit setting, *Non multiplexed output circuitry. 12VAC CT 1/2 amp transformer for Kit No. 1 **\$2.00**

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CSC 100
NEW Proto Board \$19.95
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We now offer a full line of Continental Specialties Proto Boards, Clips, Monitors, etc.

LOOK!

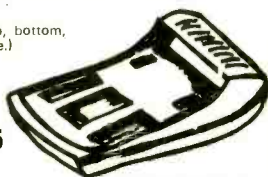
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Kit includes Components: PC board, Transf., Fuse, Pilot Light
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Ideal for Frequency counter case, function generator, etc. Overall height 4", length 12", width 7 1/2".

(Includes top, bottom, and hardware.)



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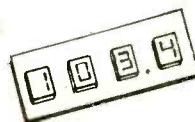
(Example) Set your alarm for 7: a.m., set timer for 15 min. At exactly 7: a.m., the appliance will start; at 7:15, your clock alarm will wake you.

Kit includes all components, PC Board and instructions for interfacing with THE KING 6-digit alarm clock. Addition Number 2

FATIMA \$19.95
4-DIGIT TEMP. KIT

Features 4-digit temperature display; farenheit or Centigrade; complete C-Mos application; uses 7002 4-digit counter.

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THE KING FEATURES:

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- Kit No. 70250-2R (DL727 readout) ... **\$28.50**
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All kits include components. PC Boards. Transformer, case, and construction manual.

TTL



- 7400 -16
- 7402 -16
- 7404 -16
- 7406 -24
- 7408 -16
- 7410 -16
- 7413 -49
- 7420 -16
- 7427 -24
- 7430 -16
- 7437 -39
- 7438 -35
- 7440 -16
- 7442 -69
- 7447 -89
- 7448 -89
- 7453 -16
- 7473 -37
- 7474 -37
- 7475 -65
- 7476 -39

- 7483 -85
- 7490 -69
- 7492 -75
- 7493 -75
- 7495 -75
- 7496 -75
- 74121 -38
- 74123 -75
- 74151 -75
- 74153 -89
- 74154 -95
- 74161 -99
- 74163 -119
- 74164 -189
- 74165 -149
- 74174 -129
- 74175 -139
- 74181 -275
- 74192 -125
- 74193 -125
- 74195 -79
- 74197 -79

CMOS



- 4000 -24
- 4001 -24
- 4002 -24
- 4006 -149
- 4007 -24
- 4008 -1.15
- 4009 -59
- 4010 -55
- 4011 -24
- 4012 -24
- 4013 -59
- 4014 -149
- 4015 -119
- 4016 -59
- 4017 -129
- 4018 -149
- 4019 -59
- 4020 -159
- 4021 -149
- 4022 -119
- 4023 -24
- 4024 -99
- 4025 -24

- 4026 -149
- 4027 -59
- 4028 -99
- 4029 -139
- 4030 -49
- 4032 -24
- 4033 -149
- 4034 -325
- 4035 -139
- 4037 -450
- 4040 -159
- 4041 -89
- 4042 -79
- 4043 -80
- 4044 -59
- 4047 -59
- 4049 -59
- 4050 -59
- 4066 -99
- 4077 -39
- 74C92 -29
- 74C04 -29
- 74C107 -129

LSI INTEGRATION



- MM5316 - 4.6 digit alarm clock 40 pin dip w/spec..... **\$ 4.25**
- 7002 - 4 digit counter/latch decoder; 7 segment and BCD outputs. 28 pin dip w/spec..... **\$12.50**
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- 75491 - segment driver..... **\$ 0.35**
- 75492 - digit driver..... **\$ 0.45**
- 7020 - 6 function calculator chip with direct segment drive. 8 digit..... **\$ 2.25**

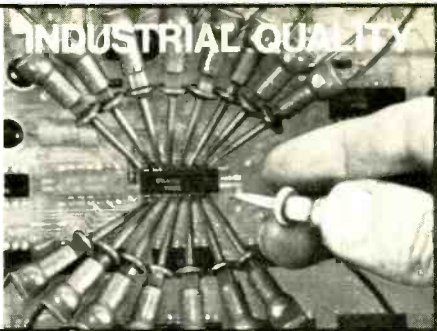
LINEARS



- 555 Timer Mini dip 0.45
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- RCA 3043 FM IF, Aud. Preamp. 1.20
- 565 Phase Lock Loop 1.95
- 567V Tone Decoder 1.50
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E-Z Hooks have been designed and field tested throughout the industry to save time and money in commercial electronic production and servicing. The spring-loaded hook attaches firmly, yet so gently it will not damage component — frees hands while testing. Durably constructed and fully insulated to a single contact point assuring true readings. Meets exacting laboratory and space age computer technology requirements. AVAILABLE IN 10 RETMA COLORS: Red, black, blue, green, orange, yellow, white, violet, brown or gray. The most unique field-serviceable test connectors available. Fast, safe, sure and trouble-free. NOW AVAILABLE FROM ANCRONA . . . the source you can trust for fine quality, industrial-grade electronic components and accessories.



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Specify color.

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Specify color.

MICRO HOOK

XM Micro Hook (1.75" long, <1 gram) for difficult IC Testing. Permits hookups to delicate wires where weight and leverage may damage component. \$.80 ea.

Specify color. ORDER P/N XM

MINI HOOK

X100W Mini Hook (2.25" long) combines rugged construction, miniature size and Finger-eze Hypo Action for all the best test connections. The hook is large enough for component leads, yet small enough to get into tight places. \$.75 ea.

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Jumper, XM Micro Hook to Banana Plug

Order No.	Length	Price
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EXTRA LONG MINI HOOK

XL-1 Mini Hook (5.0" long) combines all the proven features of the X100W with an extra long body. It will make safe, short-free test connections in card racks and through deep wiring nest up to 4". \$1.25 ea. ORDER P/N XL-1

Jumper X-100W Mini Hook to Stacking Banana Plug**

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Specify color.

Jumper, XL-1 Mini Hook to Stacking Banana Plug**

Order No.	Length	Price
201XL-1*	32"	\$1.95

Specify color.

*Specify color. **Square hole tip for hooking laterally to leads or vertically over square wire-wrap pins

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A TYPICAL TRANSCEIVER SYSTEM

SSB transmitters and receivers of the same type contain many identical components. Therefore, by a little signal switching, it is possible to make one set of filters and SL1600 devices perform alternately as a transmitter and as a receiver — i.e. as a transceiver. This, of course, results in a real cost saving, both on SL1600 devices (which in any case are relatively inexpensive) and on filters (which are not!). These points are illustrated by the Figure above, a typical SSB transceiver, and also in Applications Manual Appendices B and D.

<p>RF AMP</p> <p>Low noise, low distortion, amplifiers with integral supply line decoupling and AGC. SL1610 has voltage gain of 10 and bandwidth of 140MHz; the SL1611 has voltage gain of 20 and bandwidth of 100MHz. Both have 50dB AGC range with max signal handling of 250 mV rms. Both offer high input impedance and low output impedance. SL1610, SL1611 . . . \$2.03</p>	<p>DOUBLE BALANCE MODULATOR</p> <p>Replaces diode ring modulator, in RF/communications systems up to 75MHz. At 30 MHz, carrier and signal leaks are typically -40 dB referred to the desired output product frequency. Intermodulation products are -45dB with a 50 mV rms input signal. SL1641 is similar for receiver mixer applications w/low noise figure and power consumption. SL1640, SL1641 . . . \$2.03</p>	<p>AF AMP, VOGAD SIDETONE</p> <p>Accepts signals from a low-sensitivity microphone providing an essentially constant output signal for a 60 dB range of input. Constant gain amplifier provides an amplitude limited output for sidetone in mobile transmitter/receiver applications. 10 lead TO-5 operates from a 6 to 12 volt supply. Produces an independent supply line at 4.7 Volts stabilized. SL1622 . . . \$3.01</p>	<p>IF AMP</p> <p>Low noise, low distortion amplifier similar to SL1610 and SL1611 with voltage gain of 50, bandwidth of 15MHz and 20mW power consumption. 70dB AGC range with max signal handling of 250mV rms. SL1612 . . . \$2.03</p>
<p>LIMITING AMP/DET</p> <p>A low noise limiting amplifier for use as an RF clipper, a limiting stage in IF amplifiers, or an RF Compressor in SSB transmitters. Detector detects AM or AGC. Gain of 12 dB when not limiting, upper and lower 3 dB points of 150 MHz and 5 MHz. Limits when input exceeds 120 mV rms. Detected output during limiting is 1 mA. SL1613 . . . \$2.45</p>	<p>AGC GEN</p> <p>SL1620 VOGAD, is an AGC generator for use with the SL1630 in microphone amplifier. Maintains amplifier output between 70mV and 87mV rms over 35 dB range. One second 'hold' period prevents increase of background noise during pauses in speech. SL1621 is for use in SSB receivers with SL1621, SL1611 and SL1612. Generates a suitable AGC voltage from the detected audio waveform, provides a 'hold' period, is immune to noise interference. Smoothly follows fading HF signals. SL1620, SL1621 . . . \$2.58</p>		
<p>AM DET, AGC AMP SSB DEMOD</p> <p>For use in SSB/AM receivers with SL1610, SL1611 and SL1612. Complementary to the SL1621. AGC voltage is generated directly from detected carrier signal independent of depth of modulation. Follows the most rapidly fading signals. SL1610 and SL1612 maintains the output within a 5 dB range for a 90 dB range of receiver input signal. SL1623 . . . \$3.01</p>			
<p>MULTIMODE DET</p> <p>Detects AM, FM, SSB or CW, acting as a synchronous detector, a quadrature detector and a product detector with built-in oscillator. Contains a voltage-controlled gain system and a separate audio amplifier capable of driving a single transistor output stage. Does not give an output on broad band IF noise when used following a block filter and a broadband IF amplifier. SL1624 . . . \$2.91</p>			

MICROPHONE/HEADPHONE AMP

Offers a voltage gain of 100, accepts balanced or unbalanced inputs, and can deliver up to 250 mW output from a class AB push-pull output stage. Loggain control allows AGC to be applied when the device is used as a microphone amplifier, and also allows remote volume control with a linear potentiometer. Gain reduction of 100 dB may be obtained. SL1630 . . . \$3.85

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IN5224B	2.8 45 40	IN5247B	17 45 40
IN5225B	3.0 45 40	IN5248B	18 45 40
IN5226B	3.3 45 40	IN5249B	19 45 40
IN5227B	3.6 45 40	IN5250B	20 45 40
IN5228B	3.9 45 40	IN5251B	22 45 40
IN5229B	4.3 45 40	IN5252B	24 45 40
IN5230B	4.7 45 40	IN5253B	25 45 40
IN5231B	5.1 45 40	IN5254B	27 45 40
IN5232B	5.6 45 40	IN5255B	28 45 40
IN5233B	6.2 45 40	IN5256B	30 45 40
IN5234B	6.8 45 40	IN5257B	33 45 40
IN5235B	7.5 45 40	IN5258B	35 45 40
IN5236B	8.2 45 40	IN5259B	39 45 40
IN5237B	9.0 45 40	IN5260B	43 45 40
IN5238B	9.7 45 40	IN5261B	47 45 40
IN5239B	10.5 45 40	IN5262B	51 45 40
IN5240B	11.4 45 40	IN5263B	56 55 50
IN5241B	12.4 45 40	IN5264B	60 55 50
IN5242B	13.5 45 40	IN5265B	65 55 50
IN5243B	14.7 45 40	IN5266B	68 55 50
IN5244B	16.1 45 40	IN5267B	75 55 50
IN5245B	17.7 45 40		

7400N TTL

1-9 10up	1-9 10up	1-9 10up	
7400N	14	7470N	30
7401N	18	7471N	40
7402N	18	7472N	40
7403N	18	7473N	40
7404N	20	7474N	40
7405N	20	7475N	40
7406N	20	7476N	40
7407N	20	7477N	40
7408N	20	7478N	40
7409N	20	7479N	40
7410N	22	7480N	40
7411N	26	7481N	40
7412N	34	7482N	40
7413N	45	7483N	40
7414N	98	7484N	40
7415N	35	7485N	40
7416N	35	7486N	40
7417N	35	7487N	40
7418N	35	7488N	40
7419N	35	7489N	40
7420N	35	7490N	40
7421N	35	7491N	40
7422N	35	7492N	40
7423N	35	7493N	40
7424N	35	7494N	40
7425N	35	7495N	40
7426N	35	7496N	40
7427N	35	7497N	40
7428N	35	7498N	40
7429N	35	7499N	40
7430N	35	7500N	40
7431N	35	7501N	40
7432N	35	7502N	40
7433N	44	7503N	40
7434N	44	7504N	40
7435N	44	7505N	40
7436N	44	7506N	40
7437N	44	7507N	40
7438N	44	7508N	40
7439N	44	7509N	40
7440N	44	7510N	40
7441N	44	7511N	40
7442N	44	7512N	40
7443N	44	7513N	40
7444N	44	7514N	40
7445N	44	7515N	40
7446N	44	7516N	40
7447N	44	7517N	40
7448N	44	7518N	40
7449N	44	7519N	40
7450N	44	7520N	40
7451N	44	7521N	40
7452N	44	7522N	40
7453N	44	7523N	40
7454N	44	7524N	40
7455N	44	7525N	40
7456N	44	7526N	40
7457N	44	7527N	40
7458N	44	7528N	40
7459N	44	7529N	40
7460N	44	7530N	40

HIGH SPEED TTL

74H00N	74H01N	74H02N	74H03N	74H04N	74H05N	74H06N	74H07N	74H08N	74H09N	74H10N	74H11N
33	33	33	33	33	33	33	33	33	33	33	33
74H12N	33	74H13N	33	74H14N	33	74H15N	33	74H16N	33	74H17N	33
74H18N	33	74H19N	33	74H20N	33	74H21N	33	74H22N	33	74H23N	33
74H24N	33	74H25N	33	74H26N	33	74H27N	33	74H28N	33	74H29N	33
74H30N	33	74H31N	33	74H32N	33	74H33N	33	74H34N	33	74H35N	33
74H36N	33	74H37N	33	74H38N	33	74H39N	33	74H40N	33	74H41N	33
74H42N	33	74H43N	33	74H44N	33	74H45N	33	74H46N	33	74H47N	33
74H48N	33	74H49N	33	74H50N	33	74H51N	33	74H52N	33	74H53N	33
74H54N	33	74H55N	33	74H56N	33	74H57N	33	74H58N	33	74H59N	33
74H60N	33	74H61N	33	74H62N	33	74H63N	33	74H64N	33	74H65N	33
74H66N	33	74H67N	33	74H68N	33	74H69N	33	74H70N	33	74H71N	33
74H72N	33	74H73N	33	74H74N	33	74H75N	33	74H76N	33	74H77N	33
74H78N	33	74H79N	33	74H80N	33	74H81N	33	74H82N	33	74H83N	33
74H84N	33	74H85N	33	74H86N	33	74H87N	33	74H88N	33	74H89N	33
74H90N	33	74H91N	33	74H92N	33	74H93N	33	74H94N	33	74H95N	33
74H96N	33	74H97N	33	74H98N	33	74H99N	33	74H00N	33	74H01N	33

LOW POWER TTL

74L00N	74L01N	74L02N	74L03N	74L04N	74L05N	74L06N	74L07N	74L08N	74L09N	74L10N	74L11N
24	24	24	24	24	24	24	24	24	24	24	24
74L12N	24	74L13N	24	74L14N	24	74L15N	24	74L16N	24	74L17N	24
74L18N	24	74L19N	24	74L20N	24	74L21N	24	74L22N	24	74L23N	24
74L24N	24	74L25N	24	74L26N	24	74L27N	24	74L28N	24	74L29N	24
74L30N	24	74L31N	24	74L32N	24	74L33N	24	74L34N	24	74L35N	24
74L36N	24	74L37N	24	74L38N	24	74L39N	24	74L40N	24	74L41N	24
74L42N	24	74L43N	24	74L44N	24	74L45N	24	74L46N	24	74L47N	24
74L48N	24	74L49N	24	74L50N	24	74L51N	24	74L52N	24	74L53N	24
74L54N	24	74L55N	24	74L56N	24	74L57N	24	74L58N	24	74L59N	24
74L60N	24	74L61N	24	74L62N	24	74L63N	24	74L64N	24	74L65N	24
74L66N	24	74L67N	24	74L68N	24	74L69N	24	74L70N	24	74L71N	24
74L72N	24	74L73N	24	74L74N	24	74L75N	24	74L76N	24	74L77N	24
74L78N	24	74L79N	24	74L80N	24	74L81N	24	74L82N	24	74L83N	24
74L84N	24	74L85N	24	74L86N	24	74L87N	24	74L88N	24	74L89N	24
74L90N	24	74L91N	24	74L92N	24	74L93N	24	74L94N	24	74L95N	24
74L96N	24	74L97N	24	74L98N	24	74L99N	24	74L00N	24	74L01N	24

9300 SERIES

9300PC	9301PC	9302PC	9303PC	9304PC	9305PC	9306PC	9307PC	9308PC	9309PC	9310PC	9311PC	9312PC	9313PC	9314PC	9315PC
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9324PC	4.00	9325PC	4.50	9326PC	5.00	9327PC	5.50	9328PC	6.00	9329PC	6.50	9330PC	7.00	9331PC	7.50
9332PC	8.00	9333PC	8.50	9334PC	9.00	9335PC	9.50	9336PC	10.00	9337PC	10.50	9338PC	11.00	9339PC	11.50
9340PC	12.00	9341PC	12.50	9342PC	13.00	9343PC	13.50	9344PC	14.00	9345PC	14.50	9346PC	15.00	9347PC	15.50

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LM108H	4.90	LM311D	90	LM710CN	90
LM114H	3.00	LM311M	1.75	LM711CH	90
LM300H	1.20	LM312N	1.75	LM711CN	90
LM300M	1.20	LM312P	1.50	LM712CH	90
LM301AH	80	LM318M	2.40	LM718CD	4.60
LM301AM	80	LM324N	1.90	LM723CH	.60
LM301AN	1.10	LM331N	1.25	LM723CN	.65
LM301M	1.30	LM333N	1.25	LM725CH	6.00
LM302H	1.40	LM339N	2.20	LM725CN	6.00
LM302M	1.40	LM320-5T	2.90	LM733CH	1.40
LM304H	1.20	LM320-5T	2.50	LM733CD	3.50
LM305H	.85	LM320-12K	2.90	LM733CN	1.30
LM305M	1.75	LM320-12K	2.50	LM741CH	1.50
LM305N	1.00	LM340-5E	2.60	LM741CD	1.25
LM306N	.95	LM340-6E	2.60	LM741CN	.39
LM307H	.60	LM340-8K	2.60	LM747CH	.75
LM307M	1.50	LM340-12K	2.50	LM747CN	90
LM308H	.85	LM340-15K	2.60	LM747CM	5.5
LM308AH	5.00	LM340-18K	2.60	LM777CH	2.15
LM308D	2.25	LM340-24K	2.60	LM777CN	90
LM308M	1.00	LM555CM	.70	LM3046CN	2.15
LM309H	1.50	LM555M	1.75	LM3054CN	90
LM309M	1.50	LM567CM	1.70	SG4501T	2.40
LM310H	1.50	LM709CH	.75	SG4501N	2.40
LM310M	1.80	LM709CN	.75	LM5000K	7.50

CMOS

1-9 10up	1-9 10up	1-9 10up	
4000AE	18	4021BE	1.35
4000AF	18	4022BE	1.35
4000AG	18	4023BE	1.35
4000AH	18	4024BE	1.35
4000AJ	18	4025BE	1.35
4000AK	18	4026BE	1.35
4000AL	18	4027BE	1.35
4000AM	18	4028BE	1.35
4000AN	18	4029BE	1.35
4000AO	18	4030BE	1.35
4000AP	18	4031BE	1.35
4000AQ	18	4032BE	1.35
4000AR	18	4033BE	1.35
4000AS	18	4034BE	1.35
4000AT	18	4035BE	1.35
4000AU	18	4036BE	1.35
4000AV	18	4037BE	1.35
4000AW	18	4038BE	1.35
4000AX	18	4039BE	1.35
4000AY	18	4040BE	1.35
4000AZ	18	4041BE	1.35
4000BA	18	4042BE	1.35
4000BB	18	4043BE	1.35
4000BC	18	4044BE	1.35
4000BD	18	4045BE	1.35
4000BE	18	4046BE	1.35
4000BF	18	4047BE	1.35
4000BG	18	4048BE	1.35
4000BH	18	4049BE	1.35
4000BI	18	4050BE	1.35
4000BJ	18	4051BE	1.35
4000BK	18	4052BE	1.35
4000BL	18	4053BE	1.35
4000BM	18	4054BE	1.35
4000BN	18	4055BE	1.35

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7404	.25	7437	.47	74107	.46	74164	1.79
7405	.27	7438	.47	74121	.52	74174	1.50
7406	.40	7440	.26	74122	.87	74175	2.10
7408	.27	7442	.99	74123	.95	74176	1.80
7410	.25	7450	.27	74150	1.56	74177	1.80
7416	.44	7473	.44	74151	1.05	74180	1.10
7417	.62	7474	.40	74153	1.30	74191	1.75
7418	.26	7475	.80	74154	2.00	74192	1.40
7420	.27	7476	.57	74155	1.39	74194	1.50
7425	.40	7483	1.35			74195	1.75

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4007	29	4025	34	74C10N	72
4009	59	4029	1.50	74C20N	.72
4010	59	4049	79	74C42N	2.37
4011	29	4050		74C74	1.26
4013	69	74C00N	.43	74C107N	1.38
4016	69	74C02N	.60	74C161	3.58
4017	1.75				

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XR205	8.40	XR567CP	1.75
XR100K	80.00		

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 - 1 - 9N06 TTL Hex Inverter
 - 1 PC Card to Facilitate Device Hook-up
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3814DC**

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.68	35	30	25	20	15.0	35	35	26	64
1.0	35	30	25	20	22.0	16	40	32	26
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13	130	1.3K	13K	130K	1.3M
15	150	1.5K	15K	150K	1.5M
16	160	1.6K	16K	160K	1.6M
18	180	1.8K	18K	180K	1.8M
20	200	2K	20K	200K	2M
22	220	2.2K	22K	220K	2.2M
24	240	2.4K	24K	240K	2.4M
27	270	2.7K	27K	270K	2.7M
30	300	3K	30K	300K	3M
33	330	3.3K	33K	330K	3.3M
36	360	3.6K	36K	360K	3.6M
39	390	3.9K	39K	390K	3.9M
43	430	4.3K	43K	430K	4.3M
47	470	4.7K	47K	470K	4.7M
51	510	5.1K	51K	510K	5.1M
56	560	5.6K	56K	560K	5.6M
62	620	6.2K	62K	620K	6.2M
68	680	6.8K	68K	680K	6.8M
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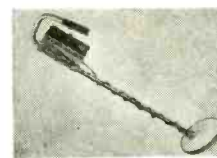
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