FEBRUARY 1955

RADIO-ELECTRONICS

TELEVISION • SERVICING • HIGH FIDELITY

HUGO GERNSBACK, *Editor*

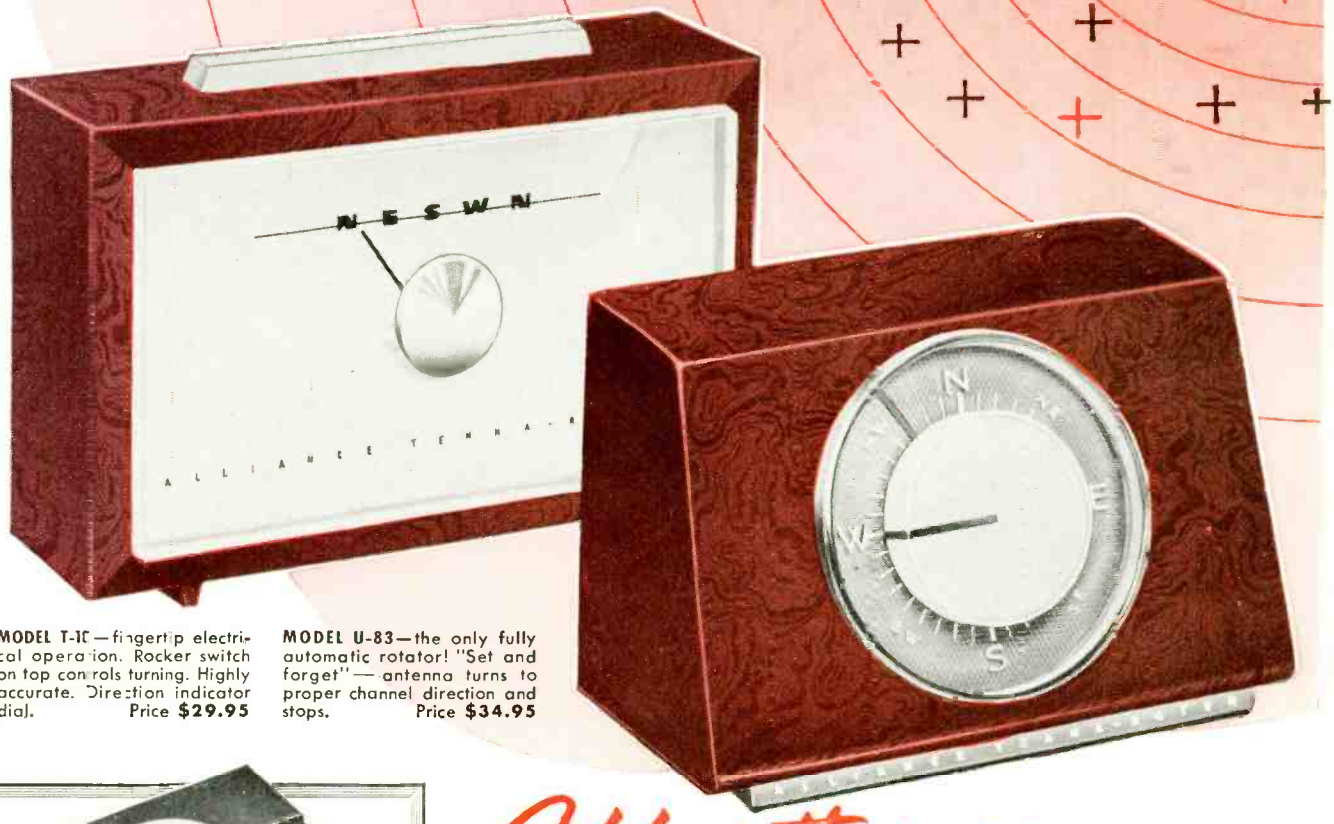
In this issue:

35¢
U. S. and CANADA

New Electronic Piano

(See Page 4)

It pays to sell ALLIANCE



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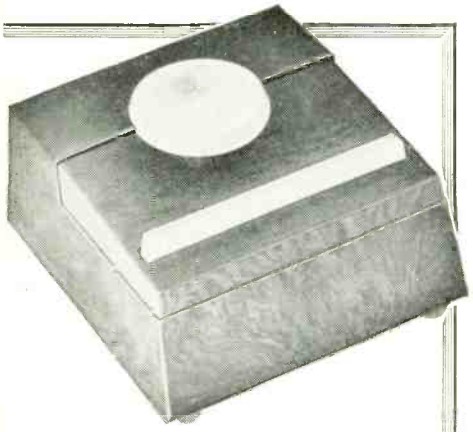
MODEL U-83—the only fully automatic rotator! "Set and forget"—antenna turns to proper channel direction and stops. Price **$34.95**



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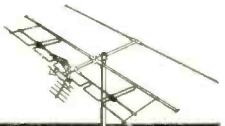

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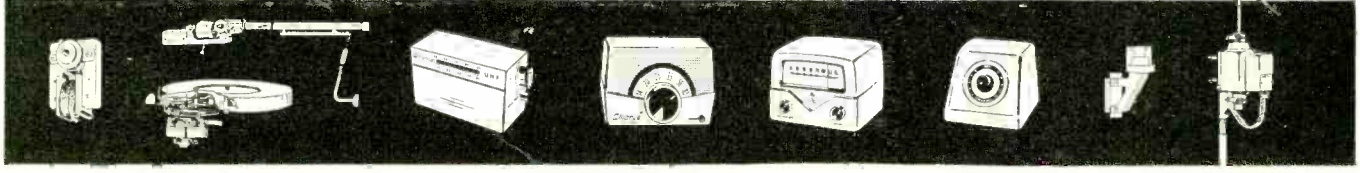

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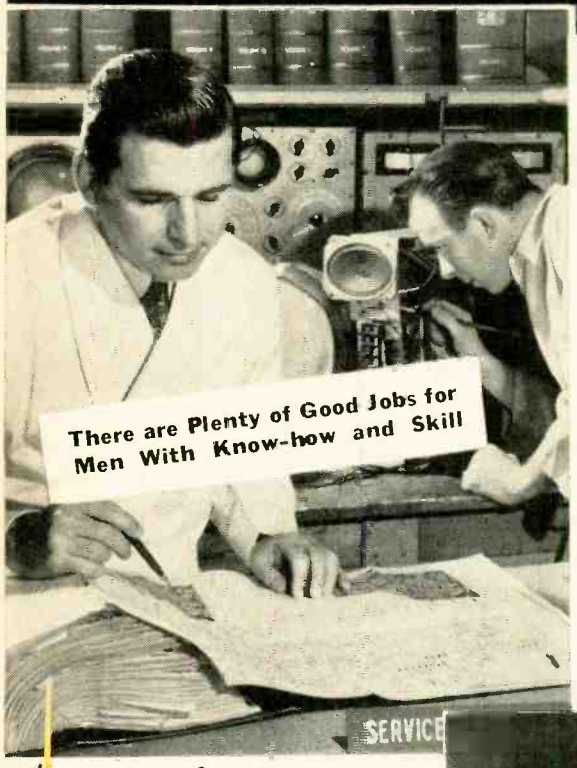

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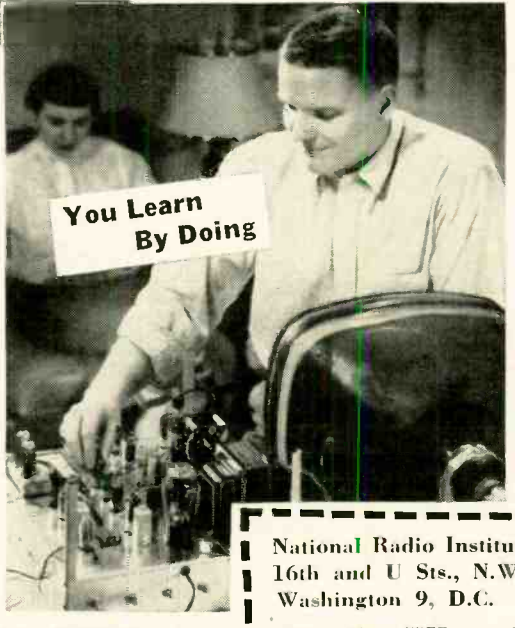

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ON THE COVER (Story on page 64) Model Carol Evans plucks one of the reeds of the Miessner electronic piano. *Color original by Daniel R. Rubin.*

(We regret that a credit was overlooked on last month's cover. The TV tube shown was supplied through the courtesy of Sylvania Electric Products, to whom our thanks are due.)

CONTENTS — FEBRUARY 1955

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the Radio month

LIGHT AMPLIFIER demonstrated by General Electric Co. may in the future solve the problem of "picture-on-the-wall" television receivers.

The light amplifier consists of a thin phosphor film between two electrodes. The front electrode is transparent, to permit incident and amplified light to pass, and is made of conductive glass. A voltage in the order of 100, supplied by an ordinary B battery, is connected across the electrodes, putting the phosphor in an electrostatic field.

Light striking atoms of a phosphor cause them to emit electrons, which produce light by collision with other atoms in the phosphor. In the light amplifier, the electrons are speeded up and given more energy by the direct voltage across the phosphor, thus producing more light than would otherwise be the case.

In the demonstration, a small lantern-slide image projected by ultra-violet light on a phosphor screen was brightened gradually from bare visibility to a bright picture by turning the voltage up from 0 to 120.

Amplification was strictly proportional, dark portions of the screen remaining black and the brightest portions coming up to highest brilliance. A total increase of 10 times was reported achieved, but theoretical limits are far beyond present accomplishment.

Drs. Williams and Cusano, who developed the amplifier, were extremely cautious about predicting practical applications for it in the near future. Asked about television screens, they pointed out that practical problems of obtaining phosphors of short enough persistence, producing large enough screens and modulating them with a TV signal were still to be solved.

CANADIAN TV STATIONS AS OF DEC. 20, 1954

CHCT-TV	Calgary, Alta.	2
CFRN-TV	Edmonton, Alta.	3
CBUT	Vancouver, B.C.	2
CBWT	Winnipeg, Man.	4
CKCW-TV	Moncton, N.B.	2
CHSJ-TV	St. John, N.B.	4
CBHT	Halifax, N.S.	3
CJCB-TV	Sydney, N.S.	4
CHCH-TV	Hamilton, Ont.	11
CKWS-TV	Kingston, Ont.	11
CKCO-TV	Kitchener, Ont.	13
CFPL-TV	London, Ont.	10
CBOT	Ottawa, Ont.	4
CFPA-TV	Port Arthur, Ont.	2
CJIC-TV	Sault Ste. Marie, Ont.	2
CKSO-TV	Sudbury, Ont.	5
CBLT	Toronto, Ont.	9
CKLW-TV	Windsor, Ont.	9
CBFT	Montreal, Que.	2
CBMT	Montreal, Que.	6
CFCM-TV	Quebec City, Que.	4
CJBR-TV	Rimouski, Que.	3
CKCK-TV	Regina, Sask.	2
CFQC-TV	Saskatoon, Sask.	8

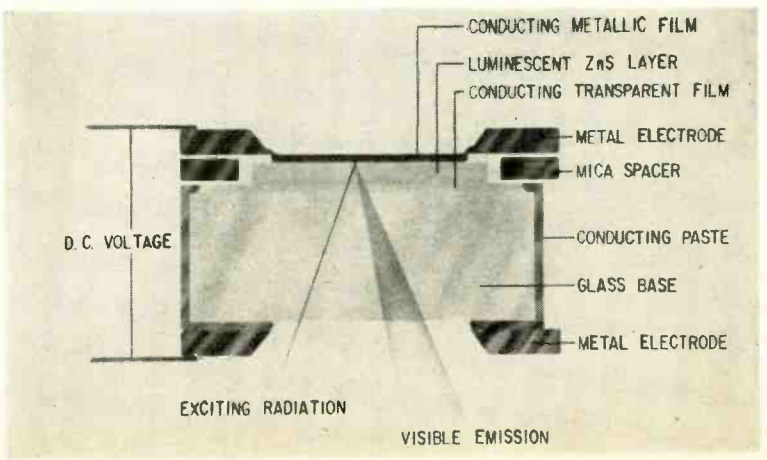
SEVEN NEW TV STATIONS have gone on the air since our January report. These are:

WEDM	Munford, Ala.	7
WPFA-TV	Pensacola, Fla.	15
WIRI	Plattsburg, N.Y.	5
WFMZ-TV	Allentown, Pa.	67
KTRK-TV	Houston, Tex.	13
KCTS	Seattle, Wash.	9
WOAY-TV	Oak Hill, W.Va.	4

Two stations have gone off the air:

KCEB	Tulsa, Okla.	23
WNAM-TV	Neenah, Wis.	42

Five new Canadian stations have gone on the air: CKCW-TV, Moncton, N.B., channel 2; CKWS-TV, Kingston, Ont., channel 11; CJIC-TV, Sault Ste. Marie, Ont., channel 2; CJBR-TV, Rimouski, Quebec, channel 3, and CFQC-TV, Saskatoon, Sask., channel 8. (New list of Canadian stations above includes these).



IRE PRESIDENT FOR 1955 is John D. Ryder (see photo), dean of the School of Engineering at Michigan State College. His election carried with it one of the nation's highest professional honors. Ryder succeeds William R. Hewlett, vice president of Hewlett-Packard Co., as head of the international society of 40,000 radio engineers and scientists.

Holder of numerous patents and author of three textbooks on electronics and networks, Ryder, a Fellow of the IRE, has long been active in that organization's affairs.

FIRST TV STATION to operate without any local programming was authorized to broadcast on chanel 9 from Lufkin, Tex. The station, it was stated, would rebroadcast programs of KPRC-TV (channel 2), Houston. In dissenting from the FCC grant, Commissioner Frieda Hennock stated, "By this action the commission for the first time has authorized the use of a v.h.f. channel by a station operating as a satellite of another v.h.f. station and carrying exclusively the programs of the parent station, which is licensed to serve a distant city.

"On Aug. 5, 1954, the commission announced a new policy under which it will consider applications for stations in the u.h.f. band which do not propose to originate any local programs. No reference was made to the possible use of v.h.f. channels for satellite stations operating off v.h.f. parent stations and carrying exclusively the programs of the latter. The grant thus extends the scope of the Aug. 5 policy and the limits then announced."

GEORGE ASHLEY CAMPBELL, scientist and inventor in the field of electrical communications, died Nov. 11, 1954. The 83-year-old mathematical physicist was a staff member of Bell Telephone Labs until his retirement in 1935.

Campbell is credited with contributing to the invention of the loaded line, which made possible long-distance telephone calls. His inventions also include the electric wave filter, which for the first time permitted the sending of many conversations over the same electrical circuit, and the shielded balance, a measuring apparatus.

In 1936 Dr. Campbell received the Medal of Honor of the Institute of Radio Engineers. He joined the American Bell Telephone Co. in Boston in 1897.

(Continued)

NEW COLOR TV RECEIVER has been demonstrated by Hazeltine. The receiver, which of course works on the NTSC system, is a projection model using three C-R tubes. Each tube produces one primary color: red, blue or green. The optical assembly contains three 2½-inch projection tubes and a system of lenses and mirrors. It combines and enlarges the outputs of the tubes and projects the color picture on a flat screen slightly larger than the face of a 21-inch direct-view tube. The receiver also operates on monochrome.

The optical assembly containing the three tubes and the necessary lenses and mirrors is a compact unit intended to be adjusted at the factory. It will then maintain adjustment and registry until it becomes necessary to replace one of the color tubes. At that time simple adjustments, of a type which can easily be made by a skilled service technician, would be needed.

It was estimated that the cost of the receiver would be comparable to that of sets using tricolor picture tubes. One outstanding advantage of this set is the cost of picture-tube replacement—the price of the small tubes being many times less than that of the present types of tricolor picture tubes.

CBS LICENSES RCA to manufacture direct-view color TV picture tubes of the curved screen mask type, a development of CBS-Hytron. The agreement, a 5-year pact, grants RCA rights to use the original patent as well as other CBS patents that may issue from pending applications. CBS officials announced the move as a definite step toward long-sought-after tube standardization in the color TV field.

RCA's recent announcement of limited commercial production of color TV sets using the company's new 21-inch tricolor tube (21AXP22) was the first use of the licensing agreement. The tube was described as a 21-inch round metal type using a curved screen mask. RCA had previously made tubes of the flat or planar mask type.

NINE ARRESTS were the result of a Miami, Fla., drive on dishonest television repair practices. The campaign was due to cooperative action by city and county officials, the local Radio and Television Technicians Guild and the Miami Better Business Bureau. Those arrested were accused of obtaining money by trick and petty larceny. Methods were said to include making unnecessary repairs, charging for parts not installed, inflating bills with labor not performed and substituting used parts for new ones. END

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Omar Bibbs, 1320 E. 27th St., Kansas City, Mo.	1st Class	34 Weeks
Kenneth Rue, Dresser, Wisconsin	2nd Class	20 Weeks
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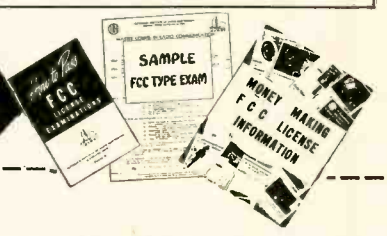

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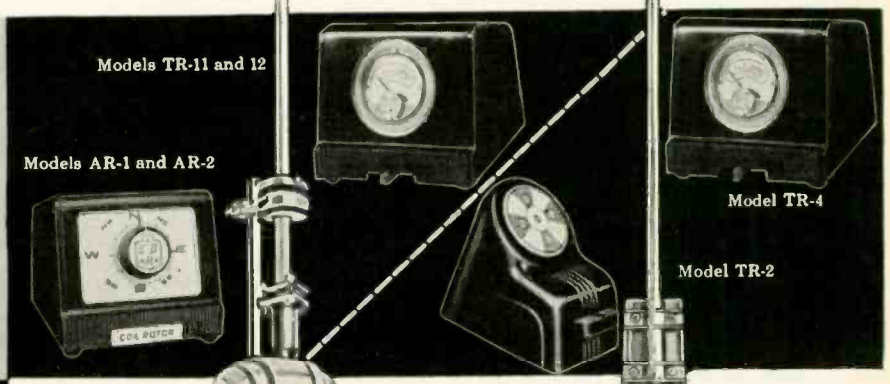

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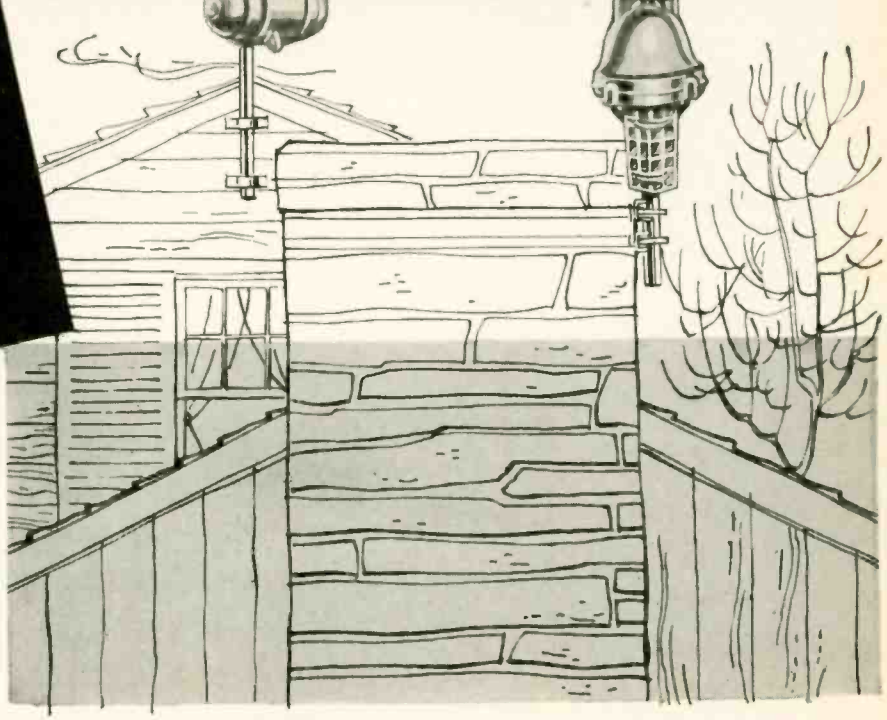

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VOTE OF CONFIDENCE

Dear Editor:

Congratulations on your bold stand in the Correspondence column of the December issue. I too feel that information is often needlessly kept out of more general use simply because of the very poor manner of its presentation. Highly involved articles might delight Mr. Holm but leave most people pretty much in the dark.

I feel that any subject can be presented in such a manner that the content can be grasped on the first reading. And more power to you and RADIO-ELECTRONICS which seems dedicated to this wholesome idea.

ELBERT ROBBERSON
Port Washington, N. Y.

REBUTTAL

Dear Editor:

I think Mr. Holm, in your December Correspondence column, has a legitimate criticism. By your own reply, the article was intended for persons "who would like to have a thorough look into the purposes, ingredients and techniques." You also stated that articles should be "interesting and understandable to the average and intelligent radio-TV technician."

I submit that the average intelligent radio-TV technician is capable of withstanding the shock of hearing that power is not always equal to E times I. If he cannot assimilate this—indeed, if he does not already know this—he has no business in radio-TV servicing.

I have not read the article to which Mr. Holm refers and so cannot say that there are errors in it, and there can be no argument with the editors' position that to communicate information the material must be clear and in language the reader understands. But if this information is *misinformation*, it is worse than none at all.

I think it is perfectly possible to write articles that are simple and accurate. Your magazine publishes one now and then! Such an article is that of D. J. Tomcik in the December, 1954, issue. It proceeds in a clear, logical manner without being overly technical. He adequately lays the groundwork for the concept of critical damping resistance, then discusses the things which affect its value. He even gives a simple mathematical (horrors!) summary of the things he has stated.

(NAME WITHHELD BY REQUEST)
Huntsville, Ala.

(*Continued on page* 16)

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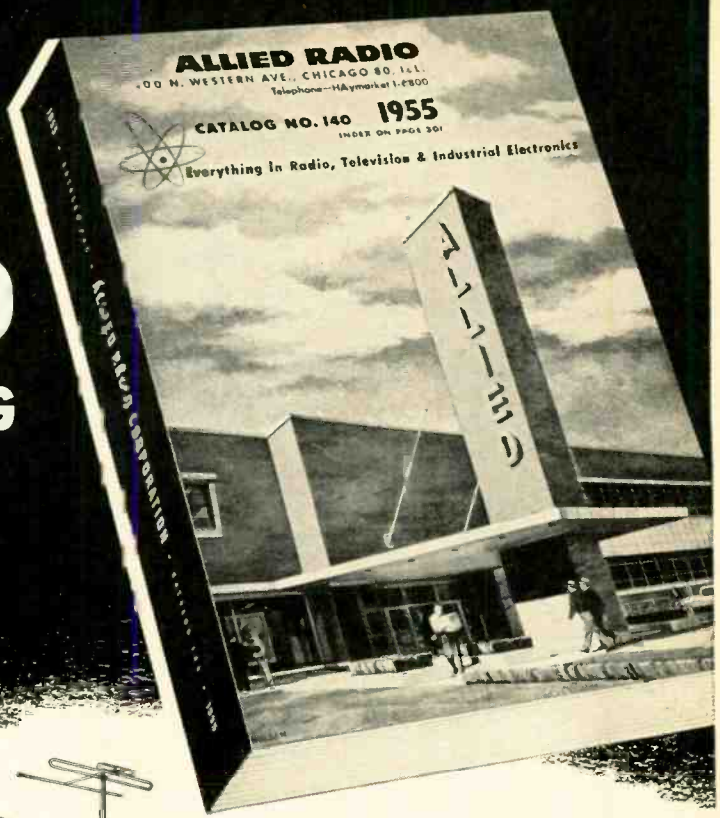

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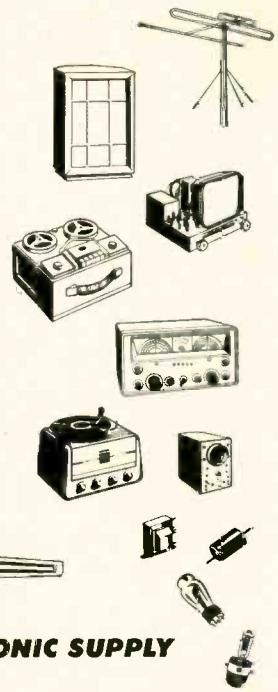

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Another demonstration of confidence in CBS-Hytron advanced-engineering

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CBS-HYTRON Main Office: Danvers, Massachusetts
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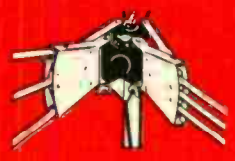
BRAND NEW FEATURES

THAT MAKE TRIO THE LEADER IN '55

HEAVIEST BOOMS!

Thick - wall, extra - sturdy 1¼" diameter Booms. Nothing approaching them for strength! Now used on ALL lowband yagis.



New "VARI-CON" HEAD

Four Hi-strength aluminum adjusting arms. Interlocking Butterfly sections. Heavier snap-action spring assembly. The "Vari-Con" is the only antenna with spring dampeners to lessen vibration and breakage. The "Vari-Con" head also used on the popular TRIO 88 Series.

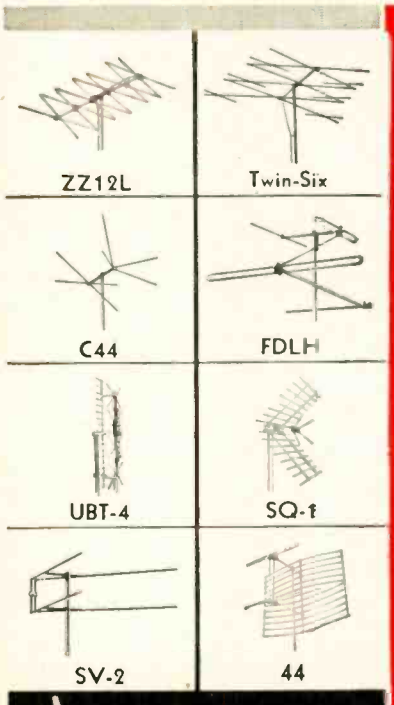
Sensational INSTA-LOK CLAMP (Good-Bye Nuts)

This revolutionary clamp permits instant flip-out assembly, permanent alignment with ultra strength. Nothing stronger — nothing faster! Insta-Lok employed on ALL TRIO Antennas that have parasitic elements.

New MINIT-UP CONICAL HEAD

Swing out element mounting plates, fan out elements into snap-fastenings and it's set! Used throughout conical line.

New MYCASTYRENE INSULATORS USED THROUGHOUT TRIO LINE

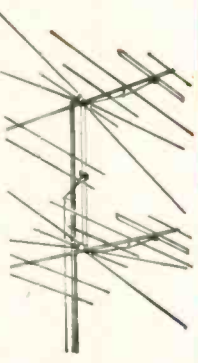


New TRIO ARISTOCRAT ROTATOR

NOW AVAILABLE IN **FOUR** GLORIOUS COLORS!

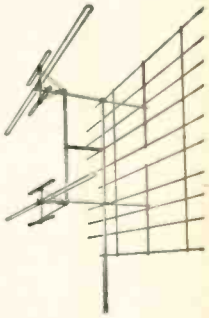
TRIO 88

Far superior construction. Rugged, foolproof — easily installed. Parasitic elements supported by TRIO's revolutionary new "Insta-Lok" clamps. Low channel dipoles supported by the strongest conical head made. No vibration — No element shedding. Completely pre-assembled. Available in single or two bay models.



TRIO 66

Three dipoles provide exceptionally high gain on all VHF channels. Exclusive TRIO grid reflector gives improved performance. Extremely rugged yet lightweight. Pre-assembled — simply unfold and tighten reflector and dipole assemblies. Three vertical braces on reflector screen for increased strength. Available in single or two bay models.



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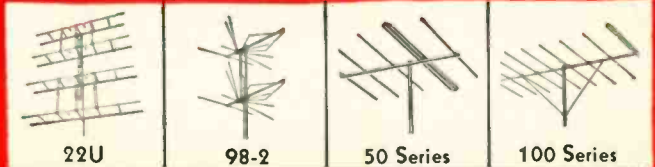
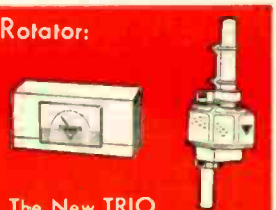


TRIO *Leader in Antenna Development*



The New TRIO "ARISTOCRAT"

CORRESPONDENCE *(Continued)*

VOICE FROM THE WEST

Dear Editor:

Hallelujah!!! is the only way I can open this letter, and I am referring to the controversy between the editors and Mr. Holm.

I am one of the would-be learners that Mr. Holm would deny knowledge to because I haven't sufficient mathematical training. Despite this handicap I am at present studying electronics at a trade school and find that when properly presented, I am capable of understanding technical articles.

I want to thank the editors of RADIO-ELECTRONICS for punching back. It is the first time I have ever read where editors weren't apologizing all over the place. The challenge you presented to Mr. Holm is very commendable.

ARTHUR L. RUTSCHMAN

Silverton, Ore.

AN AUTHOR COMPLAINS

Dear Editor:

I have been writing articles for RADIO-ELECTRONICS for some years. The articles have been—I like to think—clear, concise and timely. Most of them have had schematics and construction details. They were written on the premise that most readers of the magazine would have—at least—a knowledge of the fundamentals of electronics.

For some years now I have been receiving letters from the readers of RADIO-ELECTRONICS. They have led me to believe that perhaps I wasn't clear, concise and possessed of much knowledge. Or, is it that too many readers do not really *read*—especially schematics?

Recently I received a letter that went into a detailed explanation of how the writer had built an amplifier I described in a recent article, but he couldn't make the thing work. Could I help? I could and did. But the trouble wasn't in the amplifier at all. He had not studied the text of the article and had looked at the schematic *only* when he began to wire the parts. The title of the article or the editorial blurb had caught his fancy and he'd decided to build the amplifier. But if he had read the article he would have known of my caution about what *not* to do!

And another: The parts list indicated one value for a resistor and the schematic showed another. Which one to use? Now, I didn't mind straightening him out on this. But any tube manual could have told him the approximate value for a cathode bias resistor for this particular tube.

Did I use a gimmick on the whatsis? Well, the text of that particular article said it could be used but was not recommended. Yet, I received a three-page letter asking me if, in my learned opinion, the gimmick could be used!

So I wonder: have I been clear?

Well, I can make a mistake. The editors can make one, too. The drafting department is not immune to errors either. But usually when the editor accepts an article for RADIO-ELEC-

The data that Launched Thousands of Careers is yours FREE to show

HOW YOU CAN BE SUCCESSFUL IN RADIO-TV-ELECTRONICS

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YOU CAN plod along for years, getting a paltry increase now and then, enjoying little security, finding your work dull and drab.

Then something happens. Things look up. You become more confident. Your earnings rise. You feel more important.

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"Contacts," others may suggest.

But in your heart, you will know the answer: "Training." And it all may have started the moment you filled out a coupon requesting a copy of a free booklet named "Your Future in the New World of Electronics." From this data you get knowledge of where you stand in Electronics. Tremendous expansion leaves this gigantic industry pleading for trained men. Top manufacturers sold billions of dollars worth of electronic merchandise in 1953. By 1960, the radio-electronics industry should do no less than 10 billion dollars per year, not counting military orders.

Today there are over 97,000 radio-equipped police cars; an even larger number of taxis are radio equipped (at least 87,000); 32,000 civilian planes have radio; 35,000 American ships have radio.

Today there are over 120,000,000 radios in use. There are 28,000,000 TV sets and 381 TV stations in operation. Color TV is coming into its own. Countless positions must be filled—in development, research, design, production, testing and inspection, manufacture, broadcasting, telecasting and servicing. To fill these posts, trained men are needed—men who somewhere along the line take time to improve their knowledge, their skills. Men who, today, perhaps, take two minutes to send for a booklet.

"Your Future in the New World of Electronics" shows you how CREI Home Study leads the way to greater earnings through the inviting opportunities described above.

However, CREI does not promise you a "snap." With an accredited technical school such as this, you must *study* to convert your ambition into technical knowledge you can sell in the fabulous Electronics market.

Since its founding in 1927, CREI has provided thousands of professional radio men with technical educations. During World War II CREI trained thousands for the Armed Services. Leading firms choose CREI courses for group training in electronics, at company expense, among them United Air Lines, Canadian Broadcasting Corporation, Trans-Canada Airlines, Sears, Roebuck and Co., Bendix Products Division, All-American Cables and Radio, Inc., and Radio Corporation of America.

CREI courses are prepared by recognized experts in a practical, easily understood manner. You get the benefit of time-tested materials, under the personal supervision of a CREI Staff Instructor, who *knows* and *teaches* you what industry wants. This is accomplished on your own time, during hours selected by you, and controlled by your own will power. This complete training is the reason that graduates find their CREI diplomas keys-to-success in Radio, TV and Electronics. CREI alumni hold top positions in America's leading firms. At your service is the CREI Placement Bureau, which finds positions for advanced students and graduates. Although CREI does not guarantee jobs, requests for personnel far exceed current supply.

CREI resident instruction (day or night) is offered in Washington, D.C. New classes start once a month.
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Now is the time of decision for you. Luck will not propel you forward unless it finds you trained. Contacts won't budge you an inch unless you have the skill to back them up. The answer is: Technical Training . . . and willingness to learn. Together they will bring you increased earning in this new Age of Electronics. Fill out the coupon below and mail it now. We'll promptly send you your free copy of "Your Future in the New World of Electronics." The rest--your future—is up to you.

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To help us answer your request intelligently, please give the following information:

EMPLOYED BY.....

TYPE OF PRESENT WORK.....

SCHOOL BACKGROUND.....

ELECTRONICS EXPERIENCE.....

IN WHAT BRANCH OF ELECTRONICS ARE YOU MOST INTERESTED?.....

TRONICS he is pretty sure the author has something that works, written up so that it can be understood. And he is reasonably certain that most of his readers will like the article and will want to build whatever is described.

The letters I receive—and I've had several for every article—show that articles get read. But I think some of them must have been read with one eye on the TV screen and the other gazing into space at the finished product before the soldering iron gets hot.

So this is a plea, for myself and all authors:

Read the text of the article several times, especially if you're going to build something.

Study the diagrams. Are there any possible mistakes? Some puzzling use of circuitry? New tubes, techniques?

Don't start changing things before you've even tried the author's values.

And if you must write, remember the author is flattered to receive letters (he has readers!) but write so he can read! Use a typewriter, if possible, and *refer to the page and issue* of RADIO-ELECTRONICS as well as the title of the article. Outline your trouble, ask your questions or make your comments. But keep it short and to the point. And let the author know you've *really read* the article.

DON V. R. DRENNER
Coffeyville, Kans.

CAPACITORS

Dear Editor:

Mr. Rogers' article, "A Low-Cost Crossover Network," in the November, 1954, issue was just what I have been looking for. But—other articles on cross-over networks have stated that paper capacitors should be used in such circuits. Mr. Rogers used electrolytics.

MAJ. JESSE D. THOMPSON
Wright-Patterson A. F. B., Ohio

(Theoretically paper capacitors are superior. Actually it has been recognized for many years that electrolytics can be used like paper capacitors where voltages are low. Each unit should be measured, however, since capacitance tolerances are greater than for paper capacitors. The old Solar capacitor checker—and presumably most of the others of the same general type—tested and measured electrolytics with a low-voltage alternating current. Electrolytics have been used in cross-over networks where their greater convenience may outweigh any possible disadvantages. One of the late E. T. Flewelling's prized souvenirs of a certain type of engineering mentality was a set of electrolytics from the network of his audio system, the patent on which he had just sold to a large radio company. The company's engineer had clipped them out immediately, because "paper capacitors should be used," in spite of the fact that they had performed sufficiently well in the equipment to sell the idea to the company! —*Editor*)

the KEY to your problem

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"555" metal-cased MULTIMETERS

the NEW LOOK in

POCKET SIZE WITH A 4 7/8" LENGTH SCALE

WE LEAVE IT TO YOU

WOULD YOU BUY A PLASTIC-CASED WRIST WATCH . . .

if you *could* buy the finest movement in a magnetically shielded metal case?

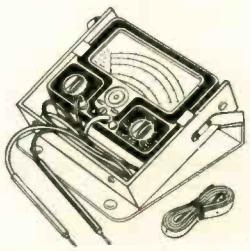
Phaostron, world famous manufacturer of ENVIRONMENT FREE PRECISION AIRCRAFT EQUIPMENT for Military and Industrial uses introduces a new concept in Multimeters. This magnetically shielded, metal-cased "555" compares with plastic-cased multimeters as a fine watch in a precious metal case would compare with a plastic wrist watch.

The shielded, shatterproof and anti-magnetic case insures continued accuracy and integrity of this instrument for years to come.

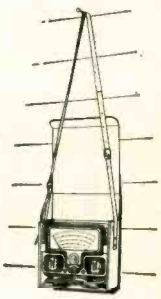
Phaostron "555" Multimeter incorporates more ranges, including AC current, greater visibility, simplified and functional controls and the greatest value offered to date.

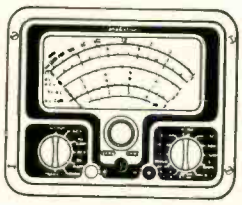
See the Phaostron "555", note its many outstanding features, its beautiful satin chrome case, its compactness and light weight, and you will know why

AC CURRENT RANGES
SEPARATE RANGE & FUNCTION SWITCHES
ONLY 2 JACKS



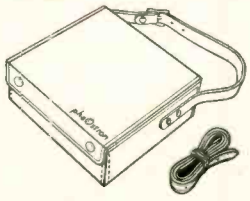
ACCURACY 3% DC, 4% AC





Panel Mounting Adapter $1.50

Genuine Leather Carrying Case $4.95



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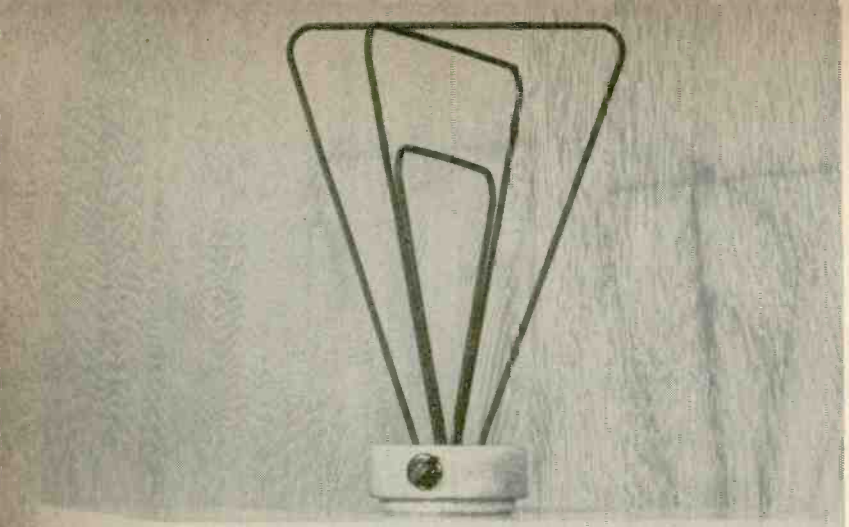


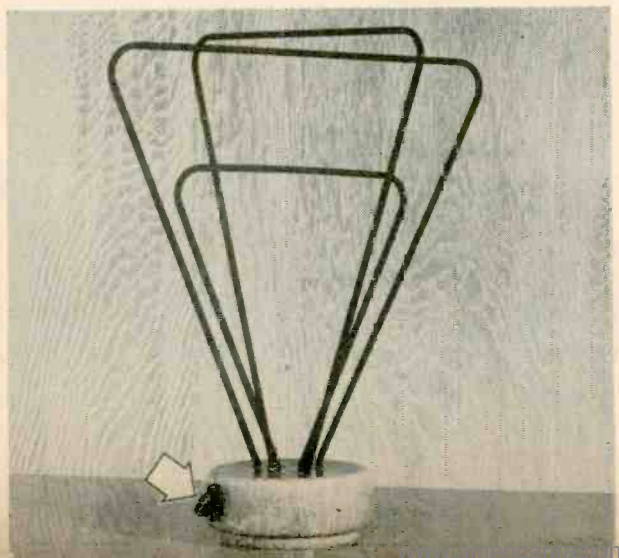
SPECIAL REPORT

Introducing the WALSCO Star...*

FIRST INDOOR ANTENNA TO BE COMPARED WITH OUTDOOR INSTALLATIONS

Attractive, compact in design...the new Walsco *Star* doesn't stick out like a sore thumb. Smart styling and distinctive colors (chartreuse, sand, green) are being recommended by interior decorators. No ugly rods to manipulate. Proven comparable in performance to a good *outdoor* antenna in most metropolitan and suburban areas.

Electronic tuner selects right combination of elements automatically for crystal-clear picture reception. Receives VHF and UHF stations in opposite directions or on widely separated channels. The Walsco *Star* is the most advanced indoor antenna ever built.



Los Angeles...A new standard in the design and performance of indoor antennas can be found in two new models recently introduced by Walsco. This is the first indoor antenna with a built-in, electronic rotating and tuning control that changes its directivity. Without moving, twisting or pulling, the new Walsco *Star* can be positioned perfectly by a simple turn of the control. Ghosts and interference are reduced or eliminated completely...and the correct combination of elements provides perfect reception on each channel.

The sharp, clear performance of the Walsco *Star* has made it the only indoor antenna that can, in most cases, be compared with a good *outdoor* installation. It was designed specifically for outstanding VHF and UHF reception in metropolitan and suburban areas. List price is $12.95. The Walsco *Starlet* (without tuning control), for use in strong signal areas, lists for $10.95. Available at jobbers everywhere in 3 smart, decorator colors.

Walsco Electronics Corporation, 3602 Crenshaw Blvd., Los Angeles 16, California.

* *Patent Applied For*

PUT YOURSELF IN THE *High-Paying* TELEVISION PICTURE.....

R Radio T Television T Training A Association

Today, when demand for trained men is higher than ever before, pay is higher than ever before, you can train AT HOME in your SPARE TIME to become a Television Technician.

E. C. Lane, B.S., M.A.
President, Radio-Television Training Association. Executive Director, Pierce School of Radio & Television.

PREPARE FOR A BRIGHTER FUTURE AS A TV TECHNICIAN

You can hold down a full-time job and still train AT HOME by the same successful methods I used to help hundreds of men—many with no more than grammar school training—master television!

NO EXPERIENCE NEEDED . . . I'LL TRAIN YOU AT HOME IN YOUR SPARE TIME

VETERANS!

My School fully approved to train veterans under new Korean G.I. Bill. Write discharge date on coupon.

GOOD SPARE TIME EARNINGS

Almost from the very start you can earn extra money while learning by repairing radio-TV sets for friends and neighbors. Many of my students earn up to $25 a week . . . pay for their entire training from spare time earnings . . . start their own profitable service business.

EXPERT FM-TV TECHNICIAN TRAINING

My FM-TV Technician Course can save you months of training if you have previous Armed Forces or civilian radio experience! Train at home with kits of parts, plus equipment to build BIG SCREEN TV RECEIVER. ALL FURNISHED AT NO EXTRA COST!

NEW! PRACTICAL TV CAMERAMAN & STUDIO COURSE

(For men with previous radio & TV training)

I train you at home for an exciting big pay job as the man behind the TV camera. Work with TV stars in the TV studios or "on location" at remote pick-ups! Available if you want it . . . one-week course of practical work on TV studio equipment at Pierce School of Radio & TV, our associate resident school in New York City.

OPTIONAL: 2 WEEKS TRAINING IN NEW YORK CITY AT NO EXTRA COST

You get two weeks, 50 hours, of intensive laboratory work on modern electronic equipment at our associate school in New York City — Pierce School of Radio and Television. And I give you this AT NO EXTRA COST whatsoever, after you finish your home study training in the Radio-FM-TV Technician Course and FM-TV Technician Course. However, your home study course is complete even without this two-week laboratory session. It is only one of the many Extras available to you from RTTA if you want it.

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As part of your training, I give you all the equipment you need to prepare for BETTER PAY TV job. You build and keep a professional GIANT SCREEN TV RECEIVER complete with big picture tube (designed and engineered to take any size up to 21-inch) . . . also a Super-Het Radio Receiver, RF Signal Generator, Combination Voltmeter-Ammeter-Ohmmeter, C-W Telephone Transmitter, Public Address System, AC-DC Power Supply. Everything supplied, including all tubes.

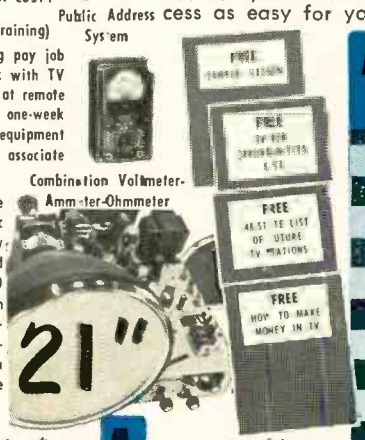
C-W Telephone Transmitter

RF Signal Generator

Super-Het Radio Receiver

Public Address System

Combination Voltmeter-Ammeter-Ohmmeter



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MY 4 FREE AIDS SHOW YOU HOW AND WHERE TO GET A BETTER PAY JOB IN TELEVISION.

See for yourself how my simple, practical methods can make success as easy for you as they have for my hundreds of graduates.

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Mr. Leonard C. Lane, President
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Dear Mr. Lane: Mail me your NEW FREE BOOK, FREE SAMPLE LESSON, and FREE aids that will show me how I can make BIG MONEY IN TELEVISION. I understand I am under no obligation and no salesman will call.

(PLEASE PRINT PLAINLY)

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I AM INTERESTED IN:
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VETERANS! Write discharge date

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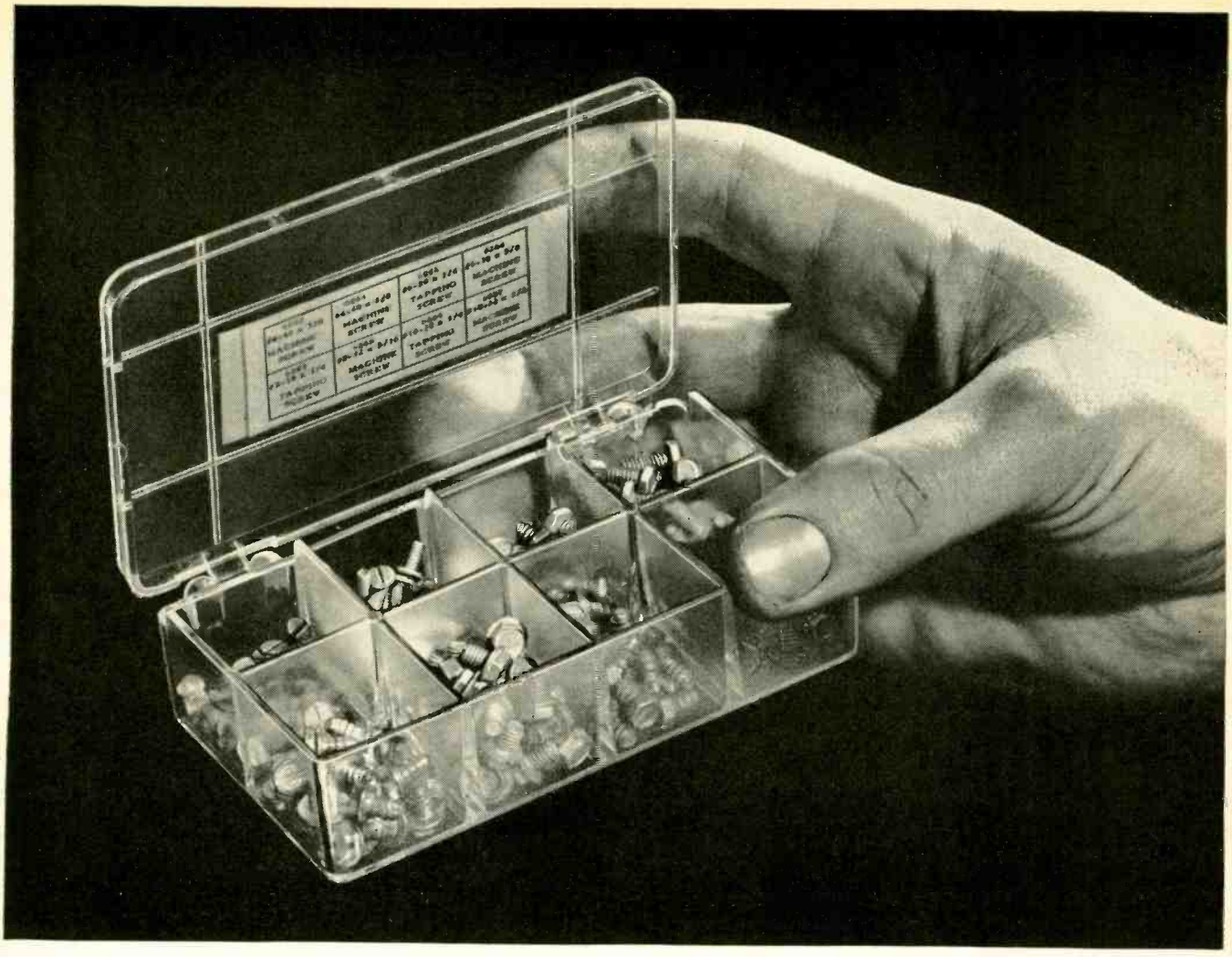

Now...Delco offers **POCKET-SIZE** kits that keep replacement hardware at your fingertips

A GREAT NEW CONVENIENCE FOR AUTO RADIO TECHNICIANS!

For quicker, easier servicing of Delco auto radios, a large assortment of replacement hardware—from tuner bearings to case screws—is now available in *four* clear polystyrene kits.

There's no more fumbling in a dark drawer when you need a hardware replacement part. You can see it immediately in these transparent kits. And each part fits your repair need exactly.

A handy chart attached to the inside cover of the box shows the contents of each of the eight compartments—a convenience when ordering refills for the compartments in plastic bags.

You can obtain these convenient pocket-size kits through your UMS Delco Electronics Parts Distributor today.

A GENERAL MOTORS PRODUCT — A UNITED MOTORS LINE

DISTRIBUTED BY ELECTRONICS DISTRIBUTORS EVERYWHERE

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This color television course was planned and developed through the combined efforts of instructors of RCA Institutes, engineers of RCA Laboratories, and training specialists of RCA Service Company. You get the benefit of years of RCA research and development in color television.

Because of its highly specialized nature, this course is offered only to those already experienced in radio-television servicing. Color TV Servicing will open the door to the big opportunity you've always hoped for. Find out how easy it is to cash in on Color TV. *Mail coupon today.*

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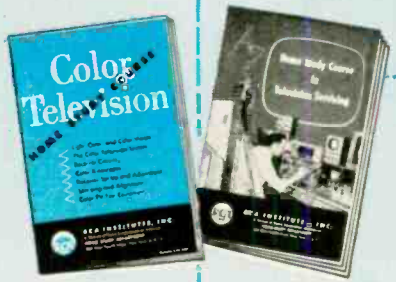
Mail coupon in envelope or paste on postal card. Check course you are interested in. We will send you a booklet that gives you complete information. *No salesman will call.*



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the fabulous VHF-UHF antenna that actually *sells itself with performance!*

CHAMPION **RAINBOW***

What do America's servicemen think of Channel Master's RAINBOW antenna? Here are their very words†:

"The RAINBOW brings metropolitan reception to isolated areas."

"Gets more stations in this fringe area than any other antenna made."

"Just what our customers have been waiting for -- a powerful, sturdy, economical antenna."

†*Just a few of the many letters of praise we receive daily.*

LOOK at the RAINBOW'S unique design, so deceptively simple, yet so unbelievably efficient. ***LOOK*** at its advanced features: New *Spacing Formula*, new *Triple-Section* High Band elements, new full-efficiency *Intermix Design*, and the brilliant triple-power TRI-POLE! ***LOOK*** at its remarkable Yagi performance on every channel, its sharp single lobe. ***LOOK*** at its rugged, durable 100% aluminum construction, reinforced at all stress points. ***LOOK*** at its trigger-fast "Snap-Lock" Action, Channel Master's fabulous preassembly that snaps open, *locks* open, without hardware or tightening.

With every installation, Channel Master's RAINBOW again proves itself *the most powerful TV antenna yet developed by modern science*. Bay for bay, it out-performs every all-channel antenna on the market today!

Get In On This High-Powered Advertising Deal

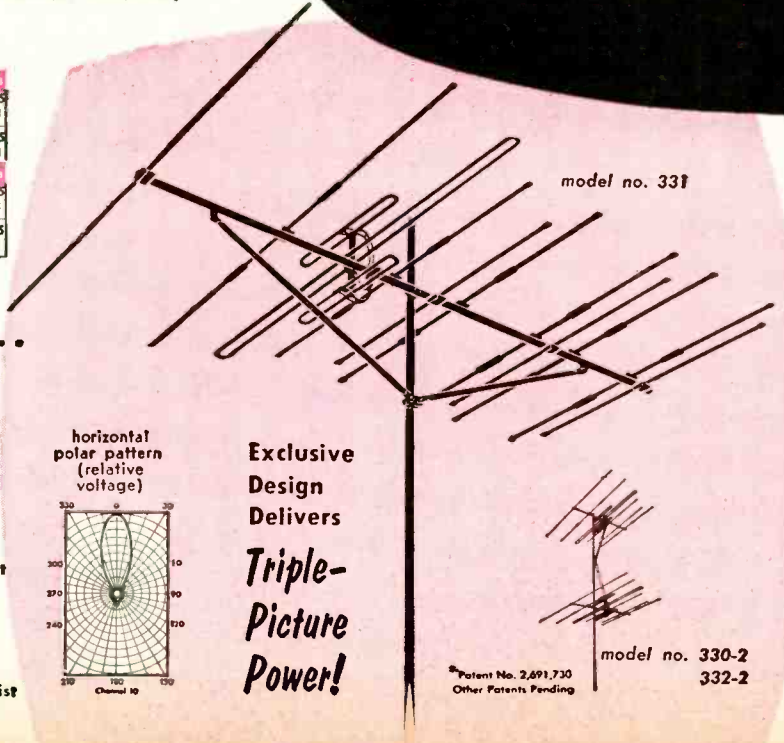
Your Channel Master distributor offers you a hard-hitting promotion program which includes TV spot films, newspaper mat ads, radio ads, full-color display material, and consumer literature. *Advertise* and *install* America's best known, most wanted antenna.

don't kid me!

NOTHING outperforms CHANNEL MASTER

Here's how the RAINBOW out-performs the famous Champion:

	CHANNEL	2	3	4	5	6	7	8	9	10	11	12	13
Gain Over 1-Bay Champion	1-Bay RAINBOW	0 DB	0 DB	0 DB	+1 DB	+2 DB	+3 DB	+2.5 DB	+1 DB	+.5 DB	+.5 DB	+1.5 DB	+2.5 DB
	1-Bay SUPER RAINBOW	+1 DB	+1 DB	+1.5 DB	+2.5 DB	+3.5 DB	+3.5 DB	+3 DB	+2 DB	+1.5 DB	+2 DB	+3.5 DB	+4.5 DB
	CHANNEL	2	3	4	5	6	7	8	9	10	11	12	13
Gain Over Stacked Champion	Stacked RAINBOW	+1.5 DB	+2 DB	+1.5 DB	+1.5 DB	+2 DB	+.5 DB	+.5 DB	+0 DB	+0 DB	+0 DB	+1 DB	+1.5 DB
	Stacked SUPER RAINBOW	+2 DB	+2.5 DB	+3 DB	+3 DB	+4 DB	+.5 DB	+1 DB	+1 DB	+2 DB	+2 DB	+2.5 DB	+3.5 DB



There's a RAINBOW model for every area . . . for every purse!

For fringe and super-fringe areas:

Super RAINBOW model no. 331, $37.50 list

stacked Super RAINBOW model no. 331-2, $75.70 list

For suburban and near-fringe areas:

Champion *RAINBOW model no. 330,* $23.60 list

stacked **Champion** *RAINBOW model no. 330-2,* $48.60 list

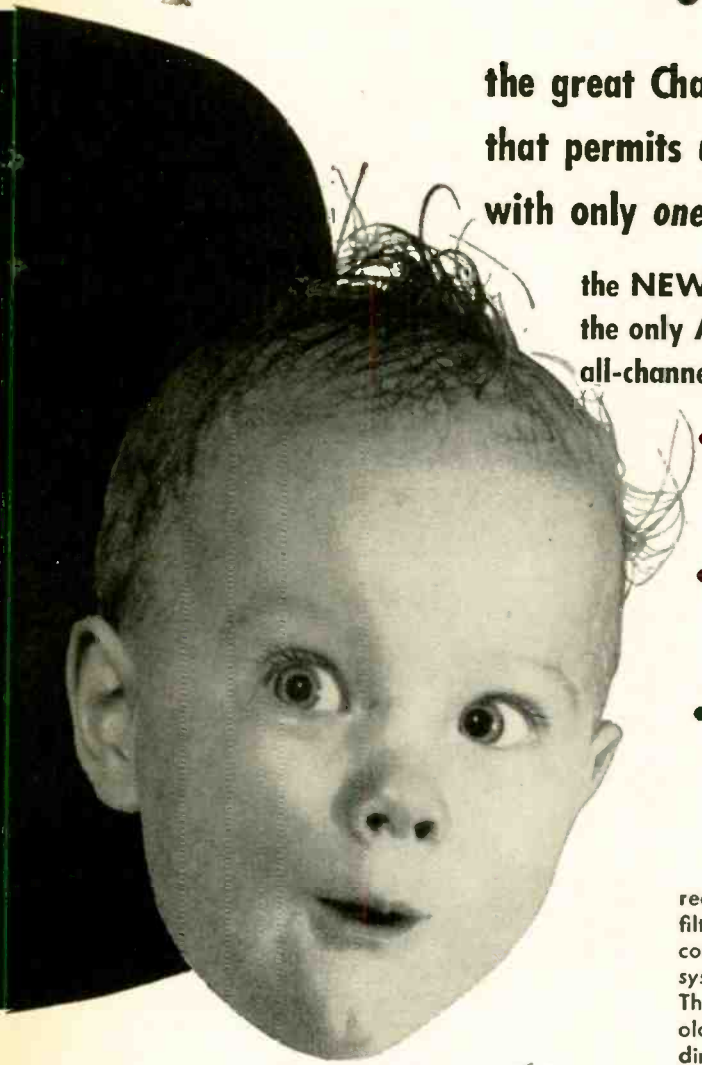
For economy installations:
(featuring butted tubing)

Challenger *RAINBOW model no. 332,* $18.06 list

stacked **Challenger** *RAINBOW model no. 332-2,* $37.50 list

a major step forward in installation procedures —

CHANNEL MASTER'S SELECTENNA coupling system



the great Channel Master development that permits *unlimited antenna combinations* with only *one* transmission line to the set!

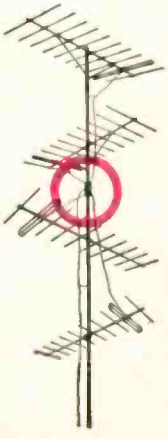
the NEW WAY, the BEST WAY, the only AUTOMATIC WAY to get all-channel, all-direction reception . . .

- ***Without rotators!***
  SelecTenna means: no extra control unit on the set; no moving parts to get out of order; antennas are always in perfect orientation.
- ***Without switches!***
  SelecTenna means: no manual switches to bother with; better performance because couplers have less insertion loss than switches.
- ***Without multiple lead-in wires!***
  SelecTenna means: neater, more professional installations, because no complicated wiring enters the home. Only one *lead* connects to the set.

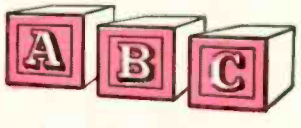
This modern way to obtain multi-directional reception — with its individual band-pass filter networks — offers the consumer great convenience advantages possible *in no other system*. There's never been anything like it! The SelecTenna System is rapidly replacing all older methods. Use it on your next "multi-direction" instal ation!

FREE TECHNICAL ADVISORY SERVICE

Our engineers will tell you the correct hook-up for your area. Merely list the channels you expect to receive, as well as the different antennas you would like to hook up. No charge or obligation.



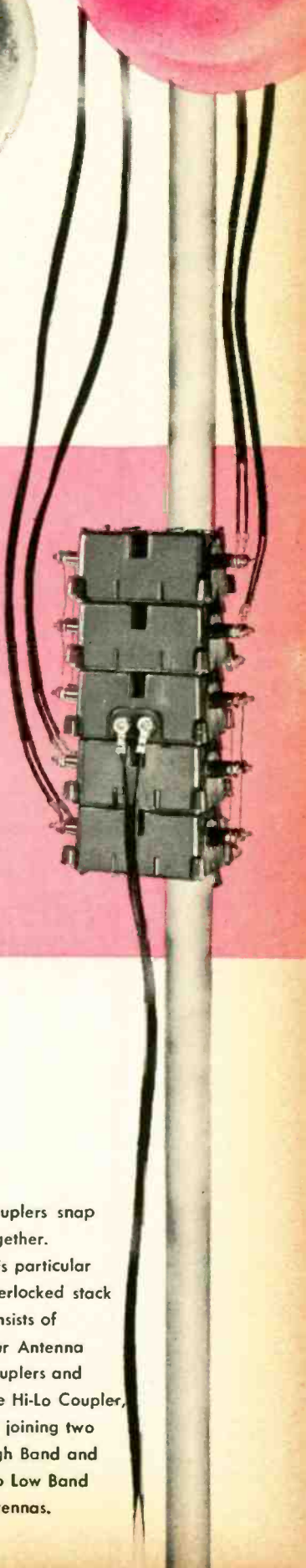
Simple as:



Simply select your channel on the set--- the right signal is always there!

list price: $5.42 each

Including mounting hardware and connecting wire.



Couplers snap together. This particular interlocked stack consists of four Antenna Couplers and one Hi-Lo Coupler, for joining two High Band and two Low Band antennas.

CHANNEL MASTER CORP. ELLENVILLE, N. Y.
The World's Largest Manufacturer of Television Antennas and Accessories.

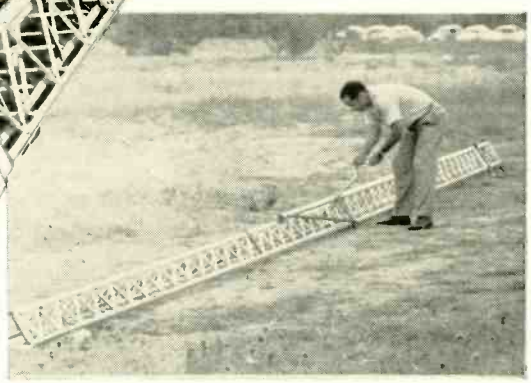
The Only TV Tower

ALPRODCO'S POP-UP TOWERS

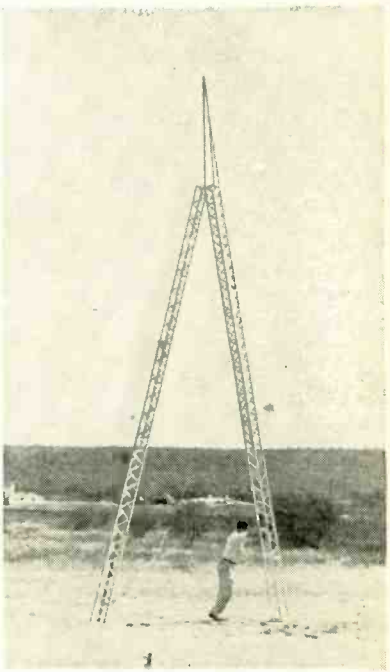
THE ANSWER! YOU BET! For the first time since **TV** started, we have a tower that solves all the problems! It comes in a package! It is pre-assembled! One man can erect it easily! Install antenna and rotator on the ground! Raise and lower it in seconds! It is guaranteed! And look at the low, low cost. Yes, **POP-UP** is the answer!

POP-UP's CONSTRUCTION: It is a beautiful combination of Alprodco's famous aluminum and steel towers. The lower section is Alprodco's triangular hot-dip galvanized steel and the top section is Aircraft Aluminum joined at the "elbow" with a strong A-frame. You get the whole "Ball-o-wax" including 1. hinged base, 2. ground anchors, 3. Aluminum and steel towers, 4. winch, 5. cable, 6. A-frame, 7. guy-brackets, 8. top-trim, 9. mast kit, ***and*** 10. a 9 foot telescoping aluminum mast.

1. POP-UP TOWER package—neat, compact and delivered without damage. Lay the tower out on location, bolt the sections together and it's ready to **POP-UP.**



2. ASSEMBLED: Use temporary guys at right angle to the raising position and **POP-UP** can be pushed up by one man. The top aluminum tower serves as a "reverse" boom.



3. PUSH POP-UP up. Pick the tower up at the "A"-frame "Elbow" and work back on the top half as the tower jack-knifes up. While the tower is in this position, secure the third guy and then plumb the lower tower.

WORLD'S LARGEST PRODUCER OF ALUMINUM TV, AM AND FM TOWERS

ALPRODCO, INC.
ELECTRONICS DIVISION

TOWERS • ANTENNAS

MINERAL WELLS, TEXAS

One Man Can Erect!

PRE-ASSEMBLED POP-UP TOWERS are delivered with all parts assembled. Bolt the sections together and it's ready to POP-UP.

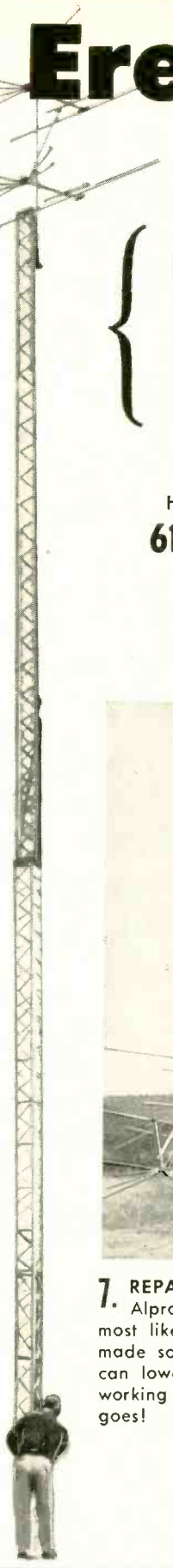
SAVES STORAGE SPACE. The aluminum tower is nested inside the lower steel tower and requires less than half the usual storage space.

COMPLETE INSTRUCTIONS with each tower. Simple, easy to follow instructions guide correct **ASSEMBLY, ERECTION,** guying, installing antenna, lead wire and any make rotator.

Alprodco **PAYS COST OF SHIPPING** right to your door. No hidden costs when you get 5 or more **POP-UP** Towers.

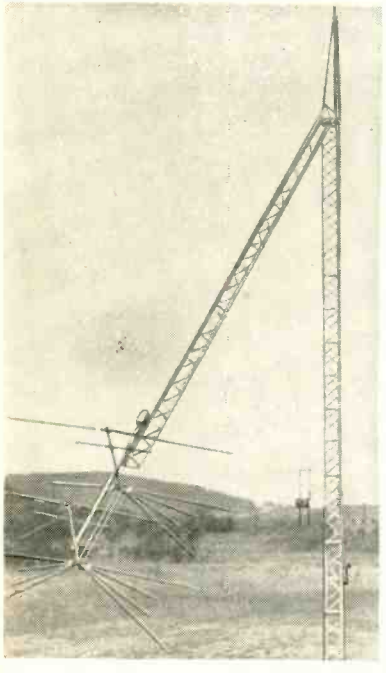
GUARANTEED to withstand up to 90 mile wind and storm load when guyed according to factory recommendations.

POP-UP'S DEALER PRICE: 49 ft.—$53.25; 61 ft.—$64.45; 73 ft.—$75.65. Full freight paid on 5 or more towers assorted. (The demand for this new tower has swamped our production department—so please allow as much lead time as possible on delivery.)

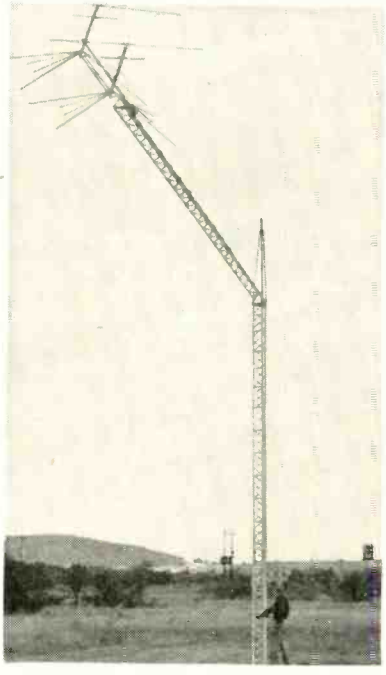


6. POP-UP is UP. Fasten the top guys and walk away from the easiest tower job you've had yet! And boy, isn't she a B-E-A-U-T-Y? Let winds and storm blow . . . no worries when you use Alprodco's **POP-UP** Tower.

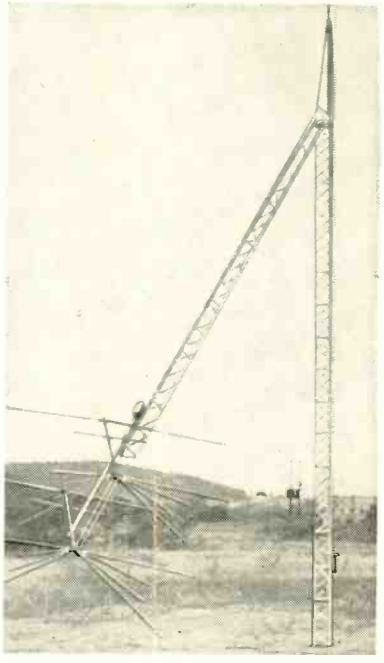
HEIGHT
61 feet



4. Attach an **ALPRODCO ROTATOR** if available, and an **ALPRODCO ANTENNA**, and it's all ready to go up. Pull the antenna away from the tower base to get winch leverage and crank.



5. JUST TURN THE CRANK and up she goes! Honest now—have you ever seen such a sweet deal! The Answer! You bet it's the answer! **POP-UP** is the service man's dream!



7. REPAIRS? If you haven't used an Alprodco Antenna and rotator, most likely there are repairs to be made soon. So—in 10 seconds you can lower the antenna to a handy working position. All done? Up she goes!

ROTATORS • SLIP-UP MASTS

KEMPTON, INDIANA • DUBLIN, GEORGIA

RADIO-ELECTRONICS
Hugo Gernsback, Editor

TEC-TELEDUCATION

. . . U.S. Technical Graduates are Decreasing Alarmingly . . .

IT is no longer news that the Soviet Union is rapidly overtaking the United States in technical education. I have called attention to this very serious state of affairs in an article recently.* Many stories in the press continue to sound the alarm at an ever-increasing tempo, with an overtone of despair and frustration.† Reading these, it would appear that there is no remedy in sight, because of fundamental shortcomings in our educational setup for training technicians.

We are told over and over that due to our traditional underpaying of teachers we cannot hope now to reverse quickly the trend of teacher-instructor defection. We cannot hold the thousands who abandon their poorly paid jobs to take more lucrative positions in industry or elsewhere.

New instructors—even if we finally see the light and pay them attractive salaries—cannot be recruited overnight. *It takes years to develop a good teacher or educator.* Not all the money in the world can undo the harm already perpetrated by our past *laissez-faire.*

The security of our country is based on technology and science. *These are, in fact, our national lifeblood.* Yet since 1950 the number of our technical graduates and scientists has decreased constantly. Within a few short years—if we don't reverse the trend—we will be running far behind the Soviet Union.

Today the United States, with 160 million inhabitants, has a scant 700,000 engineer-scientists. The Soviet Union, with a population of 213 millions, has almost 600,000. While our yearly number of technical graduates is rapidly decreasing, the Russians are *increasing* theirs as rapidly.

By the end of this year, THE SOVIETS WILL HAVE SURPASSED US BY FAR.

What the effect of this will be on our economy, our war potential and our very survival can be readily imagined. What is the answer?

Since 1950, I have been advocating *mass* education via television.‡ This was spearheaded by an editorial article I wrote for RADIO-ELECTRONICS, September, 1951, entitled "Teleducation." The Board of Education of New York City evinced interest in the idea; but so far it has not been adopted, evidently due to lack of funds.

The idea in its simplest terms can be described as follows: Instead of more—and often mediocre—teachers and instructors, we need fewer but *outstanding* ones, men who are the very best in the land. *These educators will teach millions of pupil-students at the same time by television,* from one *Central Teletorium* which could be located say in New York, Chicago, Washington or anywhere else. Classrooms all over the country would be interconnected by a closed-circuit wire or microwave relay system to the Central Teletorium.

Because of the magnitude of such a national universal educational undertaking, it would of necessity have to be a Federally built one. The Government would not operate such a system, but finance it through the states.

While the fundamental idea of teleducation is simple in concept, I can visualize endless ramifications. For a better understanding of its scope, I will enumerate here only a few of its aspects.

Emanating from a single Central Teletorium, a number of teaching programs can be broadcast over the closed circuits. Thus one set of teachers can teach grade schools. Another group will teach higher grades. A third can teach science for the lower grades. For high school purposes, there will be specially selected and more diversified science programs, such as, the fundamentals of mechanics, chemistry, electricity-electronics, astronomy, etc.

The local schools all will have large projection type TV screens, so no pupil will have to strain his eyes to see the distant lecturer. Loudspeakers placed around the classroom will reproduce the voice of the teleteacher loudly and clearly.

Teleducation will not displace present teachers—it will supplement and augment them. Thus, the teleducation programs can be broadcast into the classrooms *every other hour.* The hours in between are left open for the local teacher for individual instruction, blackboard work, supervision during tests, etc. It will be seen from this that the system can be made as flexible as required.

Time difference between remote points of the country and the Central Teletorium is no problem. The programs can be repeated to remote towns via film or tape, as we do today in commercial TV.

Most important, however, for the future of our country is the aspect of technology in teleducation.

Just as we have a national closed-circuit TV network for grade and high schools, there will be a similar one for colleges and universities, covering the entire country. In principle, it will be similar. The faculties of the various colleges and universities will remain as they are, but they will be *augmented and amplified* by scientific and technological giants of the world from the Central Teletorium.

No single university could possibly afford a constant stream of our country's and the world's greatest scientists, which can now be summoned either in person or by remote control and connected into the national *Tec-Teleducation* university hookup. How foolish we once were, our children will say in the future, to allow our great scientists to talk only to a few dozen or perhaps a few hundred pupils when the great man could lecture to 500,000 at the same time! And what student would wish to be absent when the latest Nobel-prize scientist or the Einstein of his day speaks?

Fortunately for America, we have in our hands today the technical means of making teleducation a reality in the *immediate* future. We need not wait for a new development to make it possible—*all the necessary elements are here now.* All we have to do is bring the new system into being. We do not have to be outclassed and outdistanced by any other country in the world. —*H.G.*

*RADIO-ELECTRONICS, February, 1954, "Wanted: Technicians."
†NEW YORK TIMES, Nov. 7, 1954, "Russia Is Overtaking U. S. in Training of Technicians."
‡See article in NEWSPEEK, December, 1950, "Few Teachers Reach Many Via TV."

NEW COLOR BAR and WHITE DOT GENERATORS

Circuit layout and operation of two popular color TV test instruments

By ROBERT F. SCOTT
TECHNICAL EDITOR

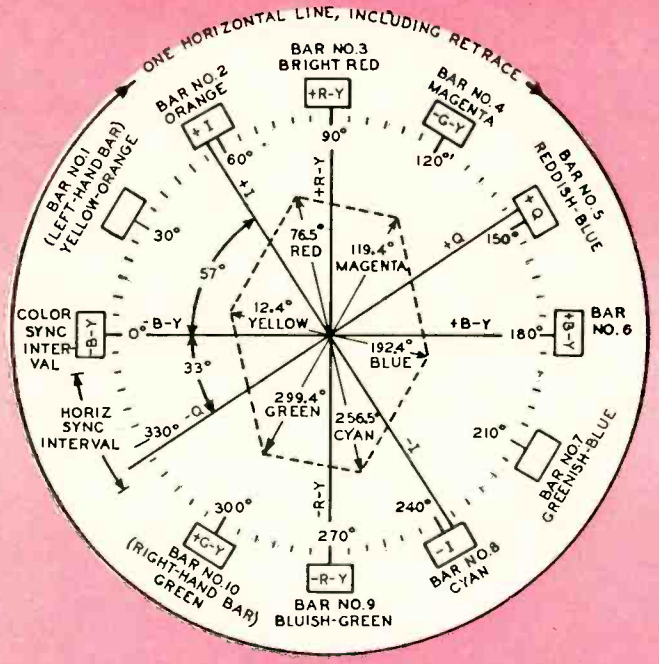


Fig. 1—Color-vector diagram showing phase relationships of color signals produced by the WR-61A. Shaded area shows phase angles and relative amplitudes.

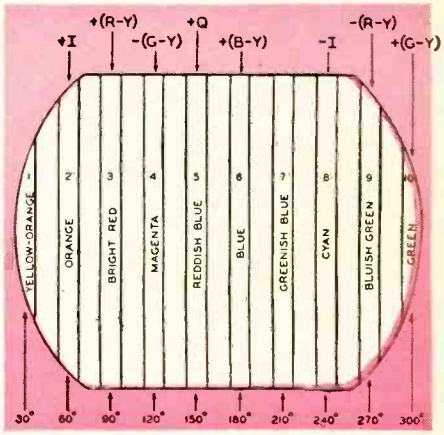


Fig. 2—Pattern shows order of color bars, their phase angles and axis relationship.

THE color bar and white dot generators are two new types of test equipment essential to rapid and efficient servicing and installation of color TV receivers. This article discusses the theory of operation and use of the new RCA WR-61A color bar generator and the Hickok model 650 video generator as modified for producing white dots for checking and adjusting convergence in color TV sets.

The RCA model WR-61A (see photo) produces 10 vertical color bars on a color TV receiver by shifting the frequency of the color-burst (subcarrier) oscillator by 15,750 cycles so that for each horizontal line there is a frequency difference of one cycle between the subcarrier and color-reference oscillator in the receiver. This shift of 360°—one cycle equals 360°—produces a continuous spectrum of vertical bars across the TV receiver's screen. Fig. 1 shows the phase relationships of the I, Q, R − Y, B − Y and G − Y axes. Note that the I and Q axes are separated from the B − Y and R − Y axes by only 30° instead of 33° as specified by NTSC standards. This slight phase difference can be counteracted by adjusting the hue control—also called color-phase control—in the TV receiver.

Since the WR-61A produces 12 bars spaced 30° apart, the color-burst oscillator must be keyed at 12 times the horizontal rate (12 × 15,750) or 189 kc. Only 10 bars appear on the screen of the receiver because the eleventh occurs during the horizontal retrace and the twelfth during the color-sync period. This can be seen by comparing Figs. 1 and 2. The bar immediately following the horizontal sync pulse (Fig. 1) serves as the color-sync burst in the receiver.

Circuit of the WR-61A

The diagram of the WR-61A is shown in Fig. 3. The subcarrier oscillator V3-b is a triode crystal-controlled type operating on 3,563,795 cycles (3.563795 mc). The bar oscillator is a Pierce crystal type using the control and screen grids of V1-a and operating on 189 kc. A part of the signal is tapped off the screen and synchronizes the 15,750-cycle horizontal sync multivibrator (V6).

In early models of the WR-61A the horizontal hold control permits the horizontal sync multivibrator frequency to be varied from below 15,750 cycles to above 31,500 cycles. In later models the hold control restricts the variable range to a narrow band around 15,750 cycles. The output of the multivibrator is tapped off the plate of V6-b and fed to the paralleled grids of clamp tube V2-a and horizontal sync shaper V2-b. The latter shapes the signal to have a duration of about 5 microseconds. V2-a eliminates the twelfth bar that occurs during the color sync period.

The 189-kc signal from the grid of V1-a goes to the input of bar shaper V1-b. Burst and bar width are determined by the preset adjustment of the variable resistor in the grid circuit. Signals from the burst, horizontal sync and subcarrier oscillators are fed simultaneously to the grid of the subcarrier keyer (V3-a). The circuit operates so its output consists of a series of 8-cycle blocks of 3.56-mc signal. These subcarrier blocks are applied to one control grid of mixer V4 across the SUBCARRIER AMPLITUDE control. The horizontal sync pulse from the sync shaper and a 60-cycle voltage from one side of the heater string are fed to the grid and cathode, respectively, of V4-b.

The SUBCARRIER AMPLITUDE control sets the amplitude of the subcarrier burst. In normal color transmission, the amplitudes of the color sync burst and the horizontal sync pulse are equal. If the amplitude of the burst is attenuated by a frequency-selective narrow-band antenna, improper receiver alignment, multipath reception that causes frequency-selective signal cancellation, or other defects or maladjustments, the color hold circuits in the receiver become unstable or lose sync completely. This control enables the technician to check quickly color sync circuits in the receiver and determine whether color sync instability is caused by a defect in the receiver or some outside trouble.

The subcarrier level control in the

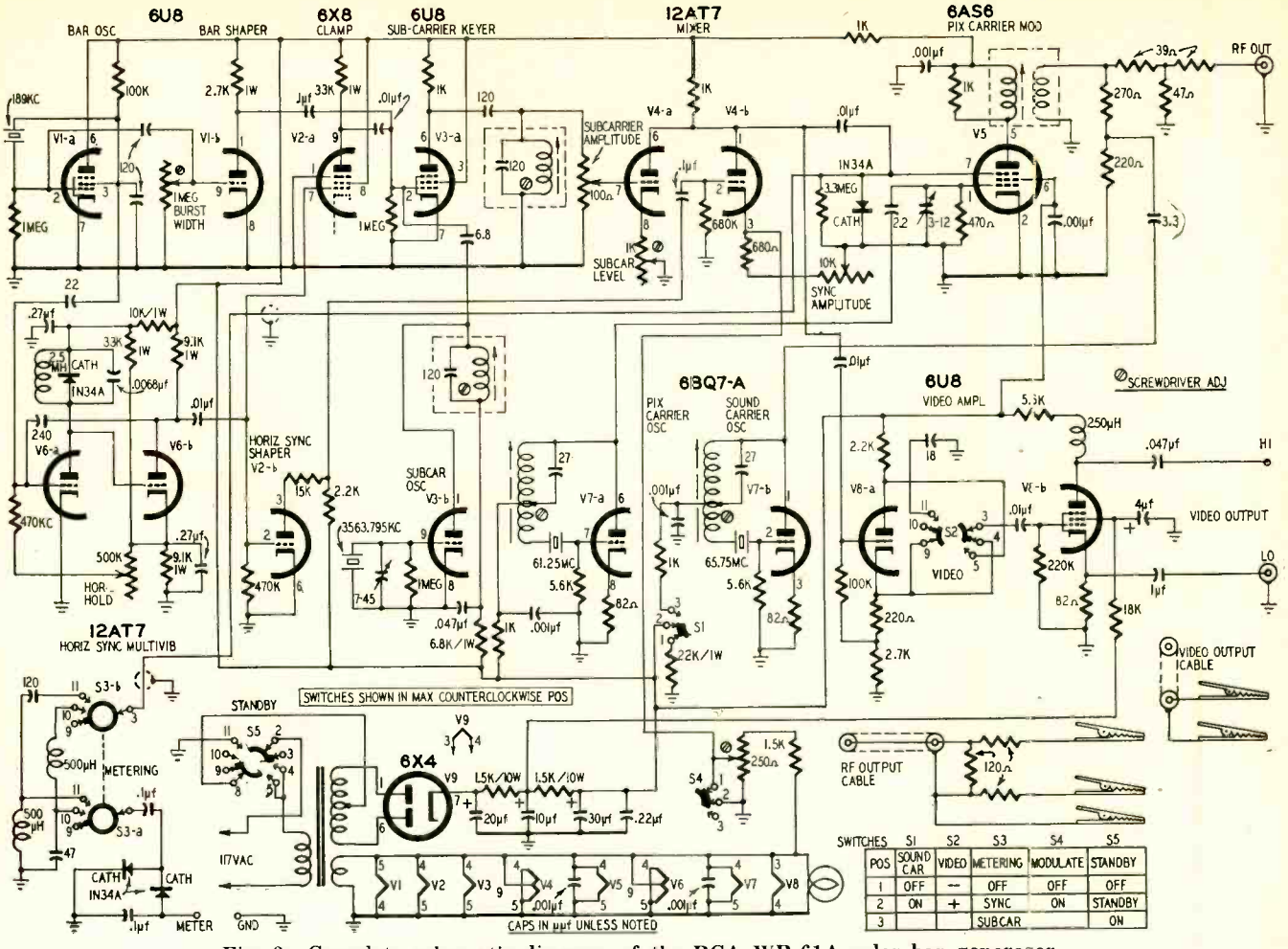


Fig. 3—Complete schematic diagram of the RCA WR-61A color bar generator.

cathode circuit of V4-a sets the maximum amplitudes of the subcarrier burst and color bar signals. It is normally adjusted for 1.2 volts on the suppressor of the 6AS6 modulator.

The SYNC AMPLITUDE control in the cathode of V4-b varies the amplitude of the horizontal sync pulses and controls the brightness of the color pattern. When the 60-CYCLE MOD control (S4) is closed, a 60-cycle voltage modulates the color bar signals by shifting their axes with respect to the sync tips. The modulation produces light and dark areas in the color bars. In a normal receiver the hue remains the same in light and dark areas. A variation in hue indicates amplitude distortion in the receiver.

The composite color video signal appears across the 1,000-ohm mixer plate load resistor. This signal is applied to a 6U8 video amplifier (V8) with its triode and pentode sections connected in cascade. This stage is provided with high- and low-impedance output circuits for signal tracing in receiver circuits following the video detector. If the receiver does not operate properly when a composite r.f. picture signal is fed into the tuner, the video may be fed to the video amplifier's input to determine whether the fault is before or after the video detector. The high-impedance output delivers 8 volts peak-to-peak across 4,700 ohms and the low-impedance output 0.25 volt peak-to-peak across 75 ohms.

A circuit-reversing switch between the halves of the 6U8 permits the technician to select either negative or positive video polarity. The position of the switch indicates polarity at the high-impedance video output terminal. A signal of opposite polarity is available at the low-impedance terminal.

The composite color video signal from the mixer and the 61.25-mc (channel 3) picture carrier are fed to the suppressor and control grids, respectively, of the 6AS6 modulator. The carrier is modulated by the video signal and is applied to the r.f. output terminal. The output impedance is 300 ohms and the signal level at least .01 volt peak-to-peak.

A crystal-controlled unmodulated sound carrier (65.75 mc produced by V7-b) is fed to the output network. The frequency of the color burst oscillator is selected so the beat (approximately 900 kc) between the subcarrier and 4.5-mc sound i.f. does not cancel as it does in color telecasts. This beat appears in the color bars so it can be used for critical adjustment of the receiver's fine tuning control and in checking the sound i.f. attenuation circuits. The beat can be recognized by turning the sound carrier on and off while watching the sound bars.

The output of the WR-61A contains a luminance signal for checking color registration. This signal appears as a thin dark vertical line on the left and a thin light line on the right of each color bar. If registration is off, some or all of the color bars will be shifted into or beyond the luminance lines. This condition may be caused by improper alignment of r.f. or i.f. amplifiers, demodulator output or bandpass filters or a defective delay line.

A built-in metering circuit using a pair of 1N34-A's and meter terminals are provided so an external v.t.v.m. can be used to measure and adjust the amplitudes of the subcarrier and sync pulses. The METERING switch permits meter connection to sync or subcarrier circuits.

Hickok 650 video generator

Hickok model 650 is a combination bar and dot generator producing stable patterns of 15 horizontal and 20 vertical bars or a series of 300 dots arranged in 15 equally spaced horizontal rows. Its output signal is available as a composite video signal and as video-modulated r.f. on channels 2 through 13. The early 650 produces black patterns on a white background for monochrome receiver servicing. When servicing or installing color TV receivers with trigun tubes, the adjustment of the various controls affecting convergence is made easier by using a

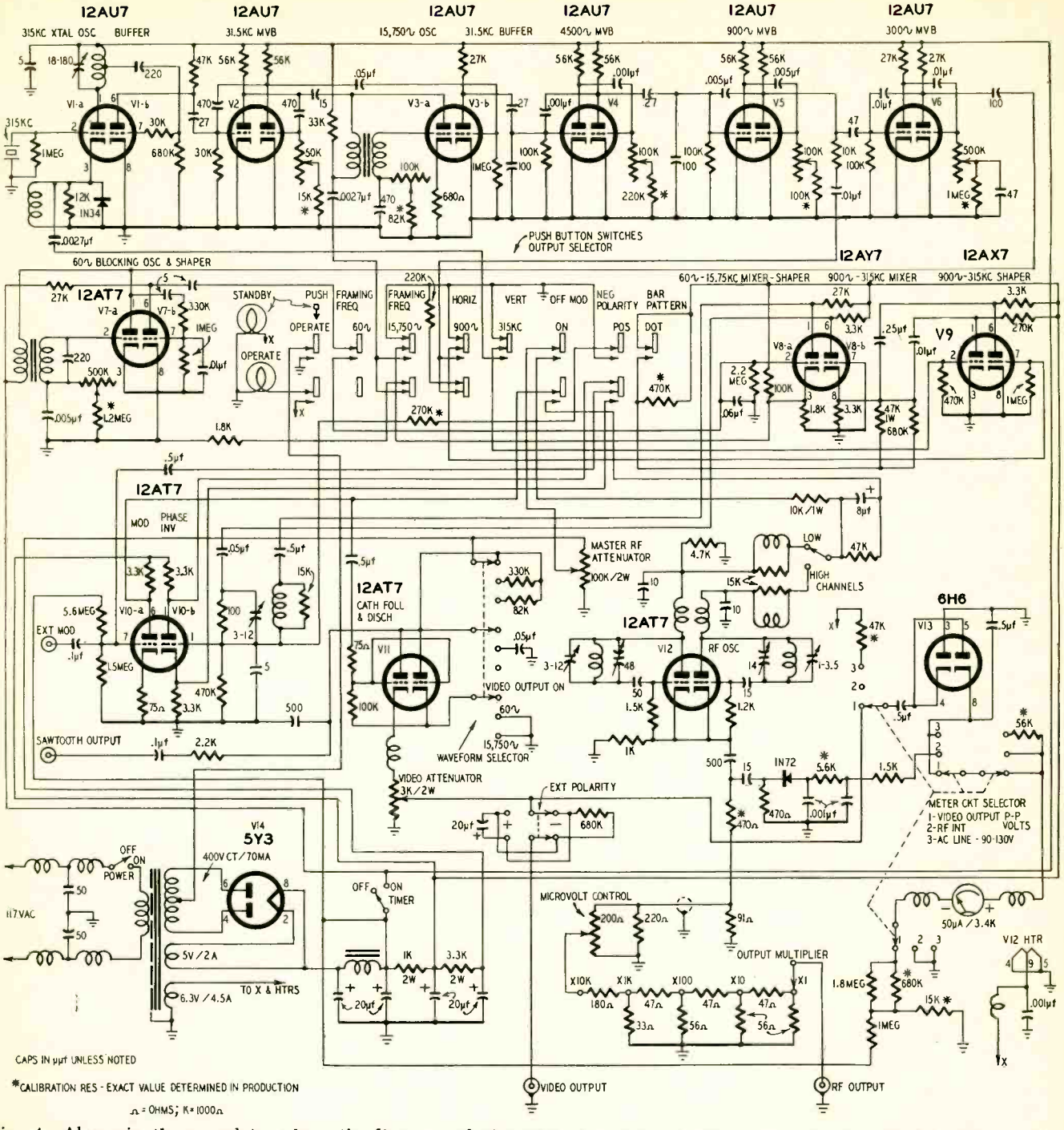


Fig. 4—Above is the complete schematic diagram of the Hickok model 650 video generator described in this article.

white dot signal such as is provided by the recently developed 650-C or an earlier model with a video phase inverting color adapter added.

Circuit operation

The heart of the 650 (Fig. 4) is the 315-kc crystal-controlled oscillator, V1-a. The germanium diode in the cathode circuit of the oscillator is a pulse-shaping device. It rectifies the unsymmetrical signal appearing at the cathode and shapes the positive half for later use as a sync pulse. A portion of the oscillator output is fed from the plate circuit to input of buffer V1-b where it is further shaped and amplified. V1-b feeds a multivibrator frequency divider with a stepdown of 10 to provide a 31.5-kc signal. The output of this circuit takes two paths. One leads to frequency-halving blocking oscillator V3-a. The other path feeds the signal through buffer V3-b to a chain of frequency dividers (V4, V5, V6 and V7-a) that reduces the frequency in steps of 7, 5, 3 and 5 to produce timing signals of 4,500, 900, 300 and 60 cycles.

When the HORIZ and VERT buttons of the OUTPUT SELECTOR switch are pressed, the 900-cycle and 315-kc signals are fed from the 900-cycle multivibrator and 315-kc master timing oscillator to the control grids of shaper V9. After shaping, the 900-cycle and 315-kc signals are mixed in the cathode circuit of V8-b, a grounded-grid amplifier.

The 60- and 15,750-cycle signals are fed into the grid and cathode, respectively, of V8-a. A video signal consisting of 60- and 15,750-cycle sync and 900-cycle and 315-kc blanking pulses are fed through isolation and shaping networks to the grid of phase inverter V10-b. This stage is coupled through the POLARITY section of the OUTPUT SELECTOR to the grid of modulator V10-a that modulates the section of r.f. oscillator V12 selected by the CHANNELS switch.

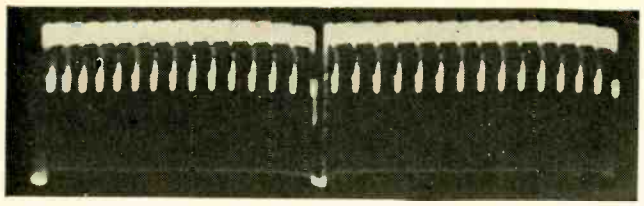


Fig. 5—Composite video signal when generator is producing a cross-bar pattern.

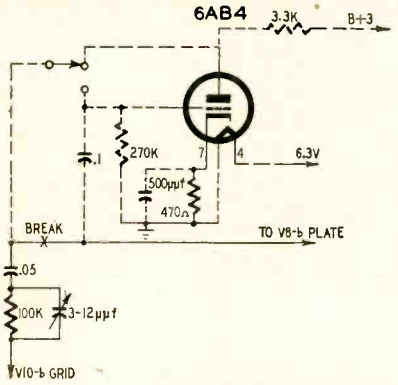


Fig. 6—Color adaptor in Hickok 650-C.

The r.f. signal appears across the cathode resistor common to both sections of oscillator V12 and is applied to the RF OUTPUT connector through fine and coarse attenuators. A metering circuit is provided for adjusting the oscillator signal level so the output corresponds to the calibrations on the fine (MICROVOLT CONTROL) and coarse (OUTPUT MULTIPLIER) attenuators. The oscillator B plus voltage is adjusted with the MASTER RF ATTENUATOR so the output is approximately 10,000 microvolts with the fine and coarse attenuators set for maximum output. The r.f. metering circuit consists of a 1N72 germanium diode, an R-C filter and a 50-μa d.c. meter.

The coarse attenuator is a five-stage ladder type with output impedance constant at approximately 5 ohms except on the × 10,000 range where it varies from 50 to 0 ohms, depending on the setting of the fine attenuator.

When the PATTERN section of the OUTPUT SELECTOR is open, V8-b is supplied with a normal value of cathode bias from a B plus voltage divider consisting of a 470,000-ohm resistor, 47,000- and 680,000-ohm resistors in parallel and the 3,300-ohm cathode resistor. Thus V8-b conducts continuously and the 900-cycle and 315-kc signals modulate the r.f. oscillator to produce a cross-bar pattern.

Closing the PATTERN switch shorts out the 470,000-ohm resistor increasing the bias on V8-b so it operates near cutoff and conducts only on the negative peaks of the signals applied to its cathode. Now the output signal consists of chains of 20 sharp pulses recurring at intervals to produce 15 horizontal lines of dots on the screen of the receiver.

Normally the horizontal bars and dots cover three and a half to five scanning lines, depending on the receiver under test. Fig. 5 shows the composite video signal developed when the generator is producing a cross-bar pattern. The wide pulses in the center and at the extreme right are 60-cycle vertical sync signals. The dim lines of equal amplitude are the 15,750-cycle horizontal sync signals. The lower-amplitude heavy pulses between the vertical sync pulses have a frequency of 900 cycles and are used to produce the horizontal bars. The 315-kc signals for producing the vertical bars are of equal amplitude but are not visible in the photograph.

The r.f. oscillators can also be modulated by an external signal applied to the EXT MOD connector when the 3.5-kc and 60-, 900- and 15,750-cycle sections of the OUTPUT SELECTOR are open. Modulation level is determined by the master r.f. level control.

Video signal output circuit

The output of modulator V10-a is applied to the input of cathode follower V11. The output is taken off the VIDEO ATTENUATOR in the cathode circuit when the WAVEFORM SELECTOR is set to VIDEO OUTPUT ON. This signal is used for servicing and signal-tracing in amplifier circuits following the video detector.

The output of V11 is also fed to V13 connected as a peak-to-peak rectifier and then applied to the meter. Output is variable from 0 to 30 volts.

The EXTERNAL POLARITY selector is used to polarize correctly the 20-μf electrolytic coupling capacitor for proper operation when the cathode follower is connected directly to a load that has a d.c. potential with respect to ground. When the video output jack is connected to a load that is positive with respect to ground, the switch must be placed in the PLUS position so the positive terminal of the electrolytic connects to the load. When the generator feeds a circuit such as the video amplifier grid that may be at a high negative potential, the switch must be placed in the NEGATIVE position. The 680,000-ohm resistor across the switch discharges the capacitor to remove the possibility of shock to the operator and damage to external circuits to which the 650 is connected.

When the WAVEFORM SELECTOR is set for 60- and 15,750-cycle sawtooth output and the corresponding section of the OUTPUT SELECTOR is closed, the cathode of V11 is grounded and a resistor and discharge capacitor are inserted in the plate circuit. With a sine wave applied to its grid, V11 acts as discharge tube, developing a sawtooth voltage in its plate circuit. These voltages can be used for signal tracing and substitution in the deflection circuits of TV receivers.

The color adapter

Fig. 6 shows the circuit that is included in the 650-C to provide white dots on a black background by inverting the phase of the 900-cycle and 315-kc signals before they are applied to the input of V10-b. The 6AB4 and components shown in dashed lines are included in the color adapter.

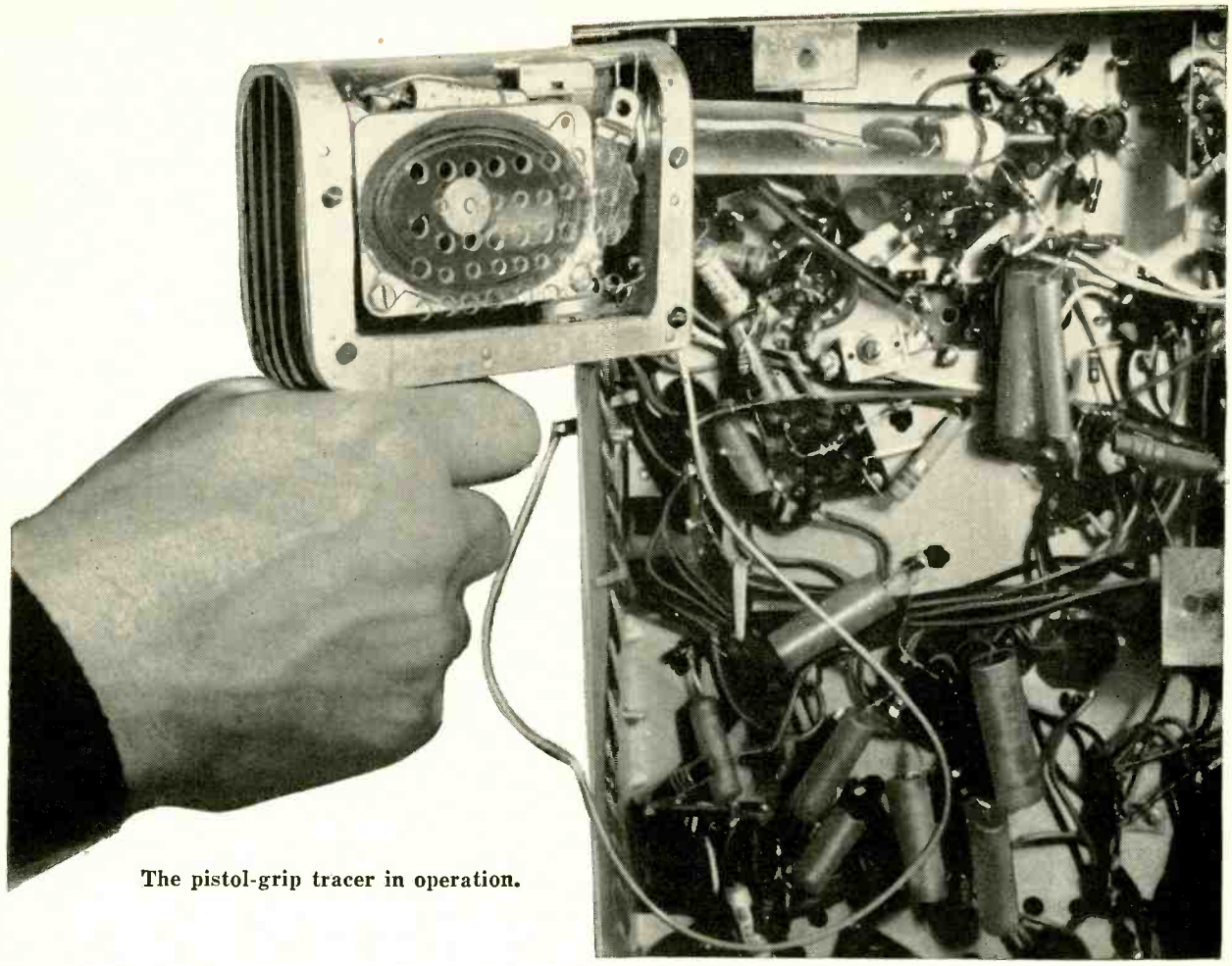
A conversion kit—called the 60-C—may be ordered from Hickok for converting 650 generators to 650-C's. It contains the 6AB4, mounting bracket, socket, terminal strip and all other mechanical and electrical components necessary for the conversion as well as full instructions and diagrams. The mechanical operations are minor. The .06-μf shaping capacitor in the grid circuit of V8-a must be relocated to make room for mounting the adapter bracket. Two small holes are drilled for self-tapping screws used to mount the adapter bracket. A half-inch hole is drilled in the top of the case for operating the rotary switch used for the changeover from black to white dots. This switch has a slotted shaft adjusted with a screwdriver through the hole in the cabinet. A snap-in plug closes the hole against dust and other foreign bodies. The switch is wired so it must be turned clockwise for black dots or bars on a white background and counterclockwise for white dots or bars.

If white dots or bars of greater intensity are needed, reduce the resistance in the grid circuit of the 315-kc section of shaper V9 by connecting a 100,000-ohm, ½-watt resistor from pin 2 to ground as described in the Hickok notes.

END

The RCA WR-61A color bar generator.

The Hickok 650 video generator.



The pistol-grip tracer in operation.

PISTOL-GRIP SIGNAL TRACER

This small and compact transistorized instrument features unique design, yet is easy to construct

By HOMER L. DAVIDSON

THIS little transistorized signal tracer resembles the pistol type soldering iron used by many experimenters and service technicians. It is compact and has only one outside lead—an alligator grounding clip. The nozzle or pointer of the tracer is touched to the circuit being tested; the signal is rectified and amplified, then reproduced through a 2-inch speaker.

A .001-μf disc type capacitor couples the incoming signal to the amplifier. A 1N34 crystal rectifies any r.f. signal picked up and feeds it to a volume control. This control is used to reduce signal strength when necessary. It is a standard type but a midget unit could have been used. Had that been done, the d.p.s.t. switch could have been placed on the control instead of at the top of the unit.

A midget electrolytic capacitor couples the incoming signal to transistor V1. Both transistors used in this signal tracer are CK722's. They are mounted in hearing-aid tube sockets that were lying around, although regular sockets can be used. Be careful when wiring the leads because heat from a soldering iron can easily damage transistors. A good trick is to let long-nose pliers absorb the heat. This also applies to the 1N34.

Resistor R1 is a base return and develops bias for this stage. Since transistor characteristics vary, R2 should be chosen for the value that provides maximum volume within the applied current limits. To find the correct value, use a 500,000-ohm potentiometer in place of R1 and vary it for maximum signal. At the same time, connect a milliammeter in series—the current should not rise higher than 5 ma. The audio amplifier stage is

transformer-coupled to the output stage. This little transformer is a Stancor UM-113: primary impedance 20,000 ohms, secondary impedance 1,000 ohms. It was designed primarily for transistor amplifying stages. A standard interstage transformer could be used if the signal tracer is constructed on a chassis where space is not limited. A 10-μf electrolytic capacitor couples the signal to the base of V2. The base-return resistor R2 was measured before being placed in the circuit as R1 was. A small output transformer steps down the amplified signal and feeds it into a 2-inch speaker.

Wiring the unit

When wiring the signal tracer be sure the transistors are properly connected—and be sure neither one draws more than 5 ma. The wiring is not critical but all leads and components must be closely spaced with the leads as short as possible. There isn't any separate chassis, the two transistor sockets being soldered to the speaker frame. Pins 3, 4, and 5 of the hearing aid sockets are soldered together. A heavy piece of brass wire is soldered to both sockets and then anchored to the 2-inch speaker frame. Also, the positive lug on the small 22.5-volt hearing aid battery is soldered directly to the 1-inch bolt fastened directly to the speaker frame.

The transistor sockets are soldered directly together. When plugging the CK722 transistors into their sockets, be sure both red dots or pins are plugged in properly. A d.p.s.t. push type switch is mounted on top.

Construction of the gun holder is easy. Get a few scraps of three-ply wood and draw a gun on each piece. On two of the pieces cut off the handle. Place the other piece between these handleless pieces and glue and nail them together. After the assembly dries, round the edges, carve and sand, giving it the appearance of a pistol. The middle section of the pistol is not sawed or cut out until the plastic is formed around it.

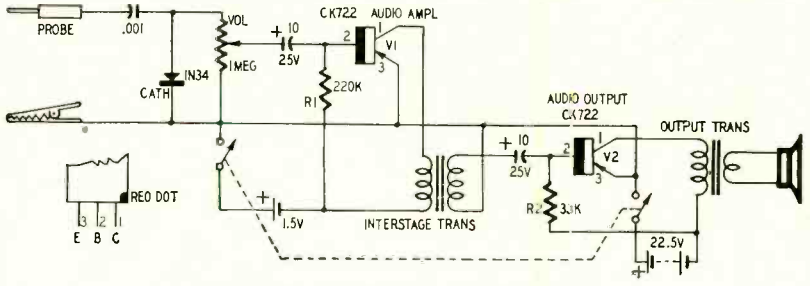
A small piece of Lucite is used as a cover for the pistol signal tracer. It is fitted around the pistol assembly while heat is applied from a gas flame. Be sure to hold the plastic away from the flame. Then the plastic can be formed around the gun assembly and held there until it sets. The speaker holes can be drilled before or after the plastic is bent. All protruding corners are then cut and rounded off to fit snugly around the wooden assembly.

At this point the center of the gun assembly is sawed out. Only a narrow border is left and the plastic piece is screwed to it. A ⅜-inch hole is drilled into the bottom for the volume control, which resembles a trigger. A 1-inch hole is then drilled for the pistol barrel. The barrel consists of a 1-inch piece of round plastic tubing with a plastic bottle cap and 2-inch bolt fastened into the end as the test probe. To save mounting space the small coupling capacitor and the 1N34 can be mounted in the plastic tube.

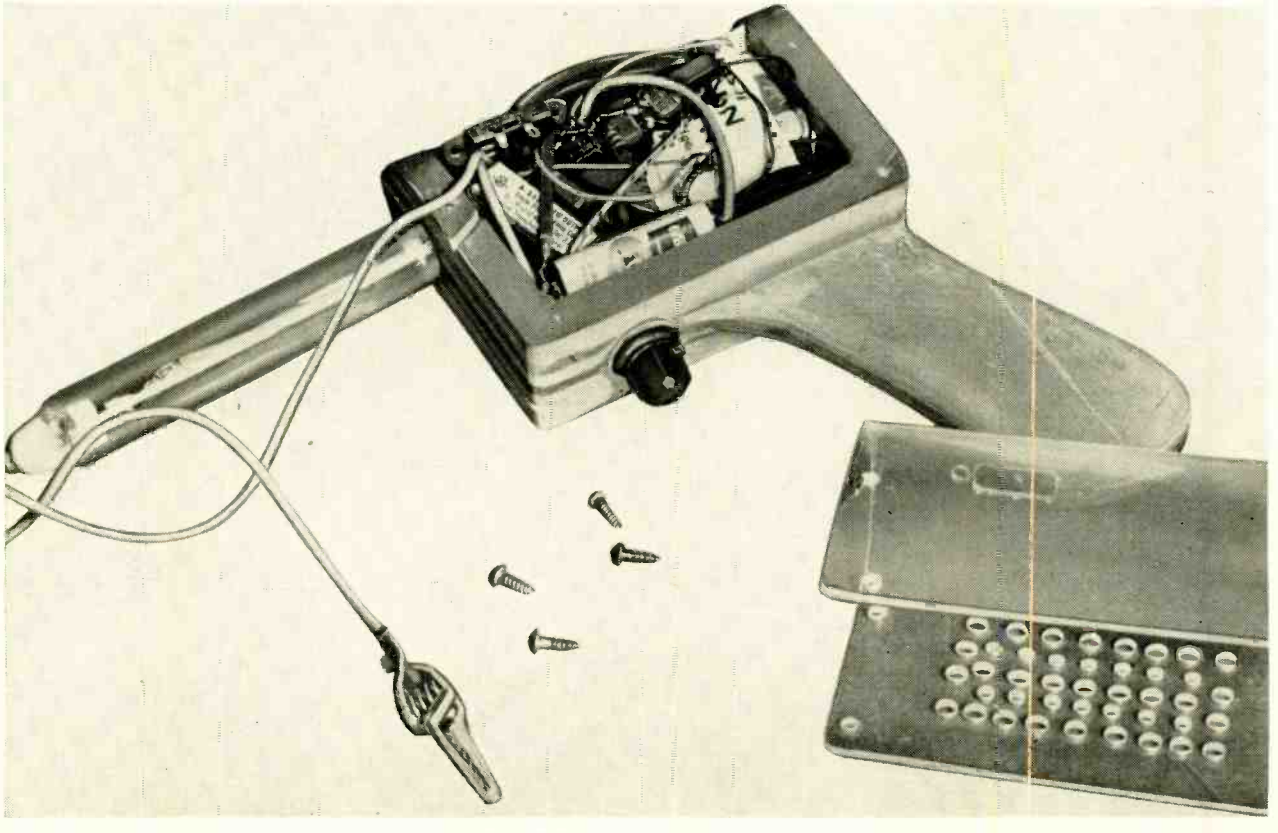
The results obtained from the small transistor signal tracer were surprising. Troubles were easily located in small radios, TV sets and amplifiers. END

Parts for signal tracer

1—33,000, 1—220,000 ohms, resistors; 1—1 megohm, potentiometer; 1—.001 μf, ceramic disc capacitor; 2—10 μf, 25 volts, electrolytic capacitor (small as possible); 1—interstage transformer, primary impedance 20,000 ohms, secondary impedance 1,000 ohms (Stancor UM-113 or equivalent); 1—output transformer, primary impedance 2,000 ohms, secondary 3.2 ohms (Stancor A-3332 or equivalent); 2—hearing-aid or transistor sockets; 2—CK722 transistors; 1—sheet of plastic; 3—pieces of 3-ply plywood; 1—2-inch speaker; 1—d.p.s.t. switch (see text); 1—1N34; 1—alligator clip; 1—plastic tubing; 1—22.5-volt hearing-aid battery.



Schematic pistol-grip signal tracer.



Assembly of the signal tracer—unit is compact; completed plastic cover at right.

DIODE WATTMETER

By RONALD L. IVES

AUDIO-frequency wattmeters, for use at medium and high power levels, are difficult to obtain commercially, and few of them have been made for use in custom-built and commercial installations. The wattmeter described in this article (Fig. 1) is extremely well suited for use in amateur modulators to indicate the a.f. output and in better-quality amplifiers and public-address systems where human ability to judge power output seems to vary inversely with the tone quality.

This a.f. wattmeter can be used with any standard line and is based on the formula $W = I^2R$ or $W = \frac{E^2}{R}$. The line resistance (or impedance) R is a constant, so wattage varies with the voltage across the line.

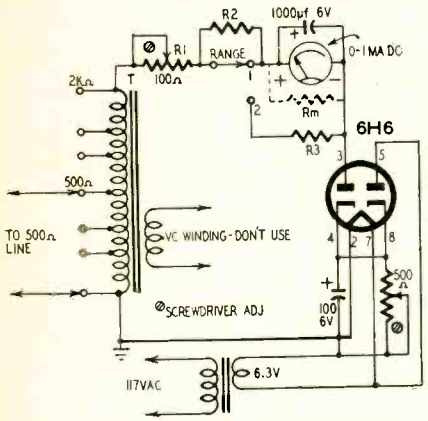


Fig. 1—Diode wattmeter schematic.

When the a.f. voltage is rectified, and the wattage computed from the measured voltage and the line impedance, a wattmeter scale (Fig. 2) can be made. Any rectifier may be used within a limited frequency range. For the great range of a.f. signals normally used, a diode such as one half of a 6H6 which has constant characteristics from below 80 microamperes to above 8 milliamperes will be most satisfactory.

Unlike dry rectifiers, such as selenium or germanium units, thermionic diodes have an appreciable contact potential which will interfere with wattmeter zeroing unless it is "bucked out." This is done by rectifying the heater voltage in the other half of the 6H6 and injecting it into the meter circuit through the common cathode resistor, which is adjusted until the meter zeros with no signal. Once adjusted, the zero setting holds for approximately the life of the tube.

The zero setting remains constant only as long as the circuit resistance is not changed. Thus, a second wattage range, if desired, must be so designed that the total resistance remains the same. Likewise, the damping of the meter circuit will be a constant only so long as the resistance in shunt with the 1,000-μf damping capacitor also remains constant.

Resistor R1 is set so that the meter reads full scale at 10 milliwatts. To produce a 100-mw range while keeping the total circuit resistance constant and also maintaining the damping R-C as high as possible, a resistor is inserted in series with the meter and a shunt placed across the pair. Values for these resistors were arrived at as follows:

To keep circuit resistance constant, the network consisting of R3 in parallel with R2 and R_m (the meter resistance, 52 ohms in this case) must be equal to R_m. Also, at 100 mw, current through the meter must be the same as at 10 mw (1 ma in this case). Voltage across the meter and its resistors will be increased by 3.16, since $W = \frac{E^2}{R}$ and $10W = \frac{(\sqrt{10}\,E)^2}{R} = \frac{(3.16\,E)^2}{R}$. Thus, the sum of R2 and R_m must be 3.16 R_m, and R2 will be 2.16 R_m (110 ohms in this case). The value of R3 can be determined by the usual parallel-resistance rules, giving a value of 72 ohms. Currents in the two arms of the circuit should be in the ratio of 1 (meter), to 2.16 (shunt), and checking by Ohm's law show that they are.

Effect of the shunt and series resistors on the time constant of the meter circuit is not great and can be computed by Kirchoff's law, using R_m as one arm of the parallel circuit and R3 plus R2 as the other. The resistance across the damping capacitor is now 40.5 ohms, and the time constant (with a 1,000-μf capacitor) has been reduced from .052 to .040 second. A 300-μf capacitor may be added, by use of another arm on the range switch, if desired.

Because a 6H6 diode can carry 8 ma steadily, a third wattage range, 1 watt, can be added. The resistance values will be, with a 52-ohm meter, R2 = 468 ohms, R3 = 57.8 ohms, R-C = .047 second.

Measurement of meter resistance may be difficult, as an ordinary ohmmeter will usually produce a badly slammed pointer or a burned-out moving coil. The best procedure is to connect the meter, a variable high resistance and a small battery in series. Adjust the resistor until the meter reads full scale and note the resistance value (disconnect the meter and measure the resistance with an ohmmeter). Then adjust the resistor again until the meter reads exactly half scale. Measure the new resistance value

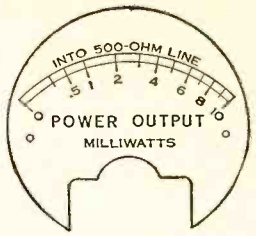


Fig. 2—Calibrated wattmeter scale.

(with meter out of circuit). This second resistance value minus twice the first is the meter resistance.

Because the average thermionic diode, such as a 6H6, has a high resistance, a voltage stepup is necessary to obtain a full-scale reading at low power levels. This is most simply done by connecting the diode between ground and a high-impedance tap of a small matching transformer or autotransformer, such as a Stancor A-7947, Thordarson TS-

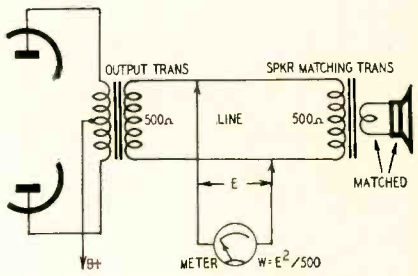


Fig. 3—Meter hookup for 500 ohms.

24-S66, UTC S-12 or an equivalent transformer. A similar effect can be obtained, at higher cost, with a more sensitive instrument, such as a 0–100 microammeter (which will also require different resistance and capacitance values).

The wattmeter is calibrated directly. Measured voltages are applied across the line with the speaker (or other load) connected. A convenient place to insert these voltages is across the 500-ohm winding, values then being in accord with the table.

This will give correct wattage values with a 1-ma instrument at the frequency of the inserted voltage only if the load is connected to the correct tap. If the matching transformer has a good frequency characteristic, values will be accurate at all audible frequencies. If its characteristic looks like a profile of

Wattmeter Calibration

Mw	E	Mw	E	Mw	E	Scale
0.25	0.353	2.5	1.13	25	3.53	0.157
0.5	0.500	5	1.57	50	5.00	0.224
1	0.707	10	2.24	100	7.07	0.316
2	1.00	20	3.16	200	10.0	0.446
3	1.22	30	3.83	300	12.2	0.544
4	1.41	40	4.45	400	14.1	0.630
5	1.57	50	4.96	500	15.7	0.700
6	1.73	60	5.46	600	17.3	0.774
7	1.87	70	5.91	700	18.7	0.835
8	2.00	80	6.32	800	20.0	0.895
9	2.12	90	6.70	900	21.2	0.95
10	2.24	100	7.07	1000	22.4	1.0

the Rocky Mountains, accuracy of power indications will vary accordingly with frequency. In the table, the scale column gives the reading of the original instrument scale (0–1 ma) corresponding to the wattage in the first column. Within the power ranges involved, the higher scales may be read in the same fashion, adding zeros for the higher ranges. For ease and rapidity of reading, it is usually advisable to make up a new instrument scale.

If a more sensitive meter movement is used or higher powers are involved, separate calibrations may be needed for each range, as a 6H6 has a nearly straight characteristic only between .08 and 8 ma.

Tests of this type of wattmeter indicate that it will work very well in a.f. service for an indefinite period, holding calibration and zero satisfactorily. The first model constructed is still in service, with all the original components, after 1,400 hours of operation (more than the rated tube life). It has needed no adjustment.

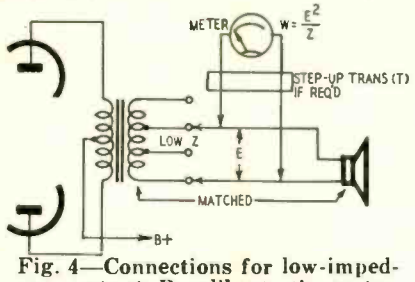


Fig. 4—Connections for low-impedance output. Recalibrate the meter.

Choice and arrangement of components are apparently not at all critical. Standard components (of the better grades) can be used throughout with a reasonable margin of safety allowed. All resistors were rated at 2 watts and all capacitors at 6 volts. With a space requirement of less than 100 cubic inches (without crowding) this wattmeter can be built into any convenient chassis or can be wholly contained within a small utility case.

Connecting the meter

Fig. 3 shows how the meter is connected across a 500-ohm audio line. The 500-ohm taps on transformer T (Fig. 1) connect across the line. Calibrations are correct only when the speaker or other load is connected and properly matched to the line.

Corrections are needed when the amplifier's output impedance is other than 500 ohms. If the impedance is lower than 500 ohms, correct corresponding taps of T across the load as in Fig. 4. If the output transformer has taps at 500 ohms and some higher impedance, you may connect the meter directly across the higher impedance tap without using transformer T. In any event, the meter must be calibrated in terms of load impedance and voltage across it. Use a v.t.v.m. or calibrated scope to measure the voltage across the load. Ordinary a.c. voltmeters have too low an impedance and their accuracy varies with frequency. END

TRANSISTOR VOLTMETER DESIGN PROBLEMS

By I. QUEEN

FIG. 1 is the basic circuit of a transistor voltmeter. Such instruments have been described before by this author and Rufus Turner among others. R1 is the multiplier resistor, R2 the input resistor and R3 controls the reverse current through the meter. When this current equals cutoff, the meter rests at zero.

There are a few difficulties, however. The meter not only reads in proportion to signal (base) current, but also varies with every change in resistance between base and emitter. When R2 is very small, collector cutoff (zero input) current may be a few microamps. It may jump to over 200 μa if the resistance is large.

There are two ways to reduce this error. First, you can choose a transistor with very low cutoff current. One CK722 tried showed only 5 μa with the input terminals open. The current fell to 3 μa with the terminals shorted. This variation is so small it can be ignored. A second way is to use a meter with a high full-scale reading, for example 1 ma. (See "Transistor Microammeter" in the June, 1953, issue.) Unfortunately, such a meter cannot make very sensitive measurements.

Now how about actual values for R1, R2 and R3? Those shown in Fig. 2 proved suitable for a voltmeter using a 100-μa d.c. meter and a type 2N34 high-gain transistor.

As already stated, R2 controls the cutoff current. If it is too low, it reduces the gain. If too high, the cutoff current will be considerable, and ambient temperature will have too great an effect. A resistance of about 100,000 ohms was found suitable. It reduced the cutoff current to about 110 μa at 70°. In practice, R2 is an 82,000-ohm resistor and a 50,000-ohm potentiometer in series. The gain can be varied about 5% with this arrangement, and the potentiometer is used as a calibration control.

R1 is determined by experiment. An 8.2-megohm resistor provided nearly full-scale deflection with 10 volts input. The deflection was then set to exactly full scale with the calibration control. (Note that this instrument has an input resistance of more than 800,000 ohms per volt!) For a 1-volt scale the multiplier is 820,000 ohms, and for a 100-volt scale R1 is of course 82 megohms. Multipliers should be hand-picked for high accuracy but need not be precision types.

Temperature effects

If transistor cutoff did not vary with temperature, R3 would be no problem at all. It would simply have to pass a

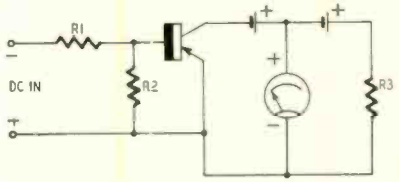


Fig. 1—The basic voltmeter.

current equal to the cutoff current of the transistor. But temperature does affect transistors. A rise of 20°F may almost double the cutoff current, so R3 must be variable over a wide range to compensate for operation at different temperatures. The arrangement in Fig. 2 is made up of a 3,300-ohm fixed unit, a 10,000-ohm potentiometer and an 8,200-ohm resistor that can be

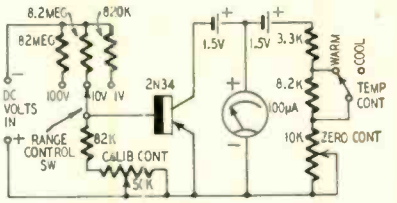


Fig. 2—Sensitive transistor voltmeter in three ranges.

switched in and out. This has enough leeway to cover wide temperature variations. The switch is opened or closed to compensate for wide temperature difference, and is calibrated with a "warm" and a "cool" position.

Fortunately the ambient temperature error is usually very small. Measurements were made on a hot summer day, with the sun falling directly on the instrument, then after chilling in a refrigerator. The "hot" reading was only about 5% lower than the "cool" measurement. END

NEW CHROMATIC AMPLIFIER

The high-gain wide-band Chromatic Amplifier.

Here is a highly useful "tool" for checking low-gain circuits in color receivers

By ROBERT G. MIDDLETON*

THE new Simpson model 406 Chromatic Amplifier simplifies various tests in low-gain chroma circuits of color TV receivers. It is also useful in certain other tests in conjunction with a low-gain wide-band scope.

The Chromatic Amplifier does not have to be used in all color receiver circuit checks. When the circuit under test provides some gain, rather than loss, the amplifier becomes superfluous; for example, tests of the red, blue and green video amplifiers do not require signal boost. However, tests of the Y channel or the matrix elements require amplification to obtain full-screen deflection (unless a very substantial input signal or a very high-gain scope is used). The circuit diagram of the amplifier (Fig. 1) appears somewhat elementary, but the experienced operator will perceive that there is more here than meets the eye. An amplifier of this type operates from 8 kc to 4.5 mc. The plate circuits require compensation to maintain a flat response over this wide range and to develop a desirable gain figure. The arrangement shown in Fig. 1 develops a gain of approximately 50.

Because the plate circuit is compensated, it acts as a low-pass filter which will operate properly only when working into the proper load — the input impedance of the demodulator probe. Any other load value will alter the frequency response of the amplifier. Hence it should be used only to drive the probe, and the probe used should have characteristics equivalent to the Simpson peak-to-peak high-frequency probe (Fig. 2). Otherwise, a flat response will not be obtained from the amplifier.

Using the amplifier

Fig. 3 shows the three possible arrangements for an amplifier when used to boost the signal into or out of a circuit under test or out of a probe to obtain full-screen deflection on a low-gain scope or for testing a very low-gain circuit. Fig. 3-a is satisfactory from the standpoint of operating stability, but is more costly because the amplifier must work into a different circuit impedance for each test. Circuit impedances may vary from that of a 500-ohm contrast control to the grid circuit of the chroma amplifier. The shunt capacitance values in such circuits vary considerably. Hence, if this method is used, a second tube is required in the amplifier so that a very low output impedance (such as 75 ohms) can be obtained. However, the use of an extra tube should be avoided if another method will prove more practical.

The second arrangement (Fig. 3-b) offers a very attractive feature in that the amplifier may now work into a constant load impedance, the input impedance of the probe. If the specified probe is used with the amplifier, a pentode-triode will develop the desired gain with response flat within ±½ db over the range of 8 kc to 4.5 mc in all tests.

Placing the amplifier between probe and scope might make it possible to use a relatively narrow-band amplifier, requiring one less section in the tube envelope. This arrangement (Fig. 3-c), however, is not practical for service work. Although the amplifier need not have a frequency response above 50 kc for the intended purpose, the low-frequency response of the amplifier must be extended to 20 cycles because a demodulated signal is now being amplified. With a low-frequency response of

*Field Engineer, Simpson Electric Co.

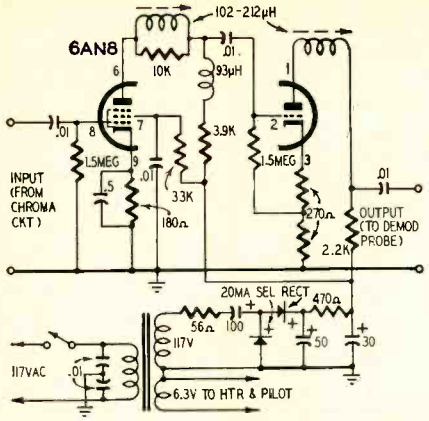


Fig. 1—Diagram of the Chromatic Amplifier. Unit operates from 8 kc to 4.5 mc.

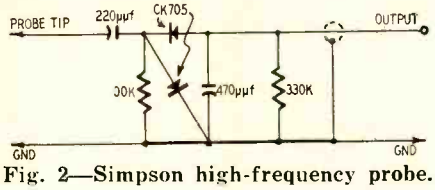


Fig. 2—Simpson high-frequency probe.

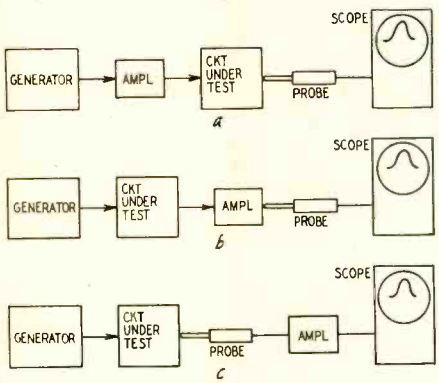


Fig. 3—Possible amplifier arrangements

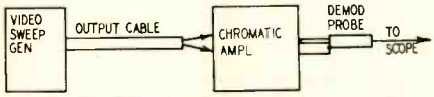


Fig. 4—Checking generator output.

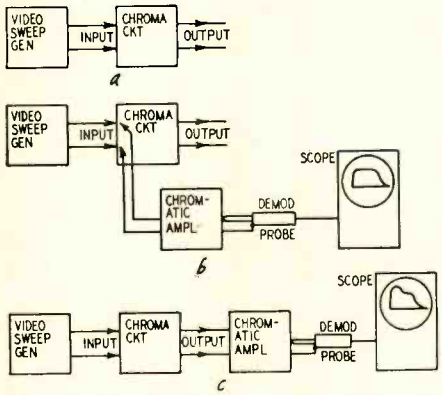


Fig. 5—Checking chroma circuit input.

this type, "bounce" becomes a severe problem since any small variation of line voltage, such as is caused by snapping a light switch on or off, causes the pattern to bounce off-screen. The difficulty can be avoided by operating the receiver under test from an automatic line-voltage regulating transformer. Service shops do not commonly have this type of transformer available for bench work, so the arrangement shown in Fig. 3-b represents the most economical method for the service bench.

The amplifier does not respond to changes in source impedance, thus the input voltage from the circuit under test may be obtained from a low-impedance source such as the cathode of a phase-splitter tube or from a high-impedance one such as the grid of a picture tube, without disturbing the amplifier response. However, the input capacitance of the amplifier is important *to the circuit under test* since unsuitable test leads may shunt so much capacitance across a high-impedance TV circuit that its operation is disturbed and a distorted response curve obtained.

A shielded input cable has much more capacitance than does a pair of open test leads, but it is effective in minimizing the possibility of stray-field pickup such as flyback pulses. Whenever a shielded cable is to be used in a high-impedance circuit, the possibility of circuit loading must be kept in mind. It is better to "kill" the horizontal sweep section of the receiver and use a pair of open test leads rather than take the chance of disturbing the normal operation of a high-impedance circuit with a shielded cable. Fortunately the majority of signal takeoff points in a color TV chassis can be obtained at low-impedance circuit points.

The amplifier pentode (Fig. 1) is series–shunt-peaked, and the triode is series-peaked, with negative feedback in the cathode circuit. The triode grid leak is connected to the midpoint of the feedback resistor to obtain the proper operating point. The series peaking coil of the pentode is damped to flatten out the frequency response and avoid excessive high-frequency peaking. However, the series peaking coil of the triode section is undamped because of the lower plate resistance of the triode.

The series peaking coils have adjustable cores to permit equalizing of the frequency response in case the 6AN8 is replaced. They also compensate for slight tolerances in the factory wiring. By slight stagger-peaking for a 4-mc rise, the over-all frequency response is flat within $\pm\frac{1}{2}$ db to 4.5 mc. This figure meets or exceeds that of any service instrument which has come to my attention.

Flat response below 8 kc is unnecessary because the output capability of video sweep generators or the Chromatic Probe (see January, 1955, issue) does not extend below this figure. In fact, the demodulating capability of most service probes extends down to only 50 kc.

Amplifier filtering

An important function of the amplifier, which may not be immediately recognized, is its filter action. By making the test shown in Fig. 4, the technician can determine whether the output from his video sweep generator is sufficiently flat. The pattern obtained on the scope screen should be an essentially flat line if the generator output voltage is uniform. Otherwise, the generator output will have to be corrected, as a distorted response curve will result if the generator lacks a flat output.

Fig. 5 shows the steps to be followed in checking the flatness of the sweep input to a chroma circuit. The sweep generator signal is applied to the input of the chroma circuit under test (Fig. 5-a). The Chromatic Amplifier is also connected to the input of the chroma circuit under test (Fig. 5-b), and the output from the amplifier is applied to a peak-to-peak demodulator probe that feeds the scope. The scope trace should be a straight horizontal line. Finally, the Chromatic Amplifier is connected to the output of the chroma circuit under test (Fig. 5-c) to obtain the circuit's frequency response.

The amplifier serves primarily as a low-pass filter, removing all frequencies except the video-frequency signal used in making the chroma circuit check. This is done because a video sweep generator must operate on a beat-frequency principle to cover the wide frequency range required (50 kc to 4.5 mc). All beat-frequency generators develop a sum as well as a difference frequency and feed-through frequencies. A few generators have a low-pass filter in the output circuit, but the majority do not. Hence, the filter function must be provided by the technician if he is to obtain a valid flatness check.

It is sometimes assumed that if one of the signals in the output of a sweep generator is flat, all must be flat, or *vice versa*. But this is not true. It is possible for the sum frequency and the feed-through frequencies to be flat, and for the difference frequency to show distortion such as a low-frequency dropoff. Thus only the type of test shown in Fig. 4 (or an equivalent filtering arrangement) will provide the technician with the information he seeks. The exact procedure to be followed is shown in Fig. 5.

The present trend is toward the use of wide-band scopes that provide full gain at the color subcarrier frequency, and of course the gain of such scopes is relatively low. When such a scope is used for alignment work, the Chromatic Amplifier will be required for a greater number of tests. Some wide-band scopes, however, provide a dual-band arrangement, so that the input circuit can be converted by switching for high-gain narrow-band response. In such case, alignment checks can be made in the high-gain position of the switch, and the Chromatic Amplifier will be called upon less often to boost the test signal. END

tv dx in 1954

What's what and who's who in long distance TV reception

By E. P. TILTON, W1HDQ*

THOUGH this is the fourth yearly summary of TV dx observations, most casual television viewers are still unaware that TV signals can on occasion be received over distances of 1,000 miles or more. Even when they encounter their first dx, a typical reaction may be "So what? It's the same program I get on the local channel!" And many a proud dx-er, calling in a neighbor to witness one of his prize catches, has been rebuffed with "Lots of snow on it, isn't there?" But to a growing army of enthusiasts the logging of TV dx is a fascinating, if sometimes exasperating, hobby.

The TV dx-er is a reincarnation of the radio dx bug of a generation ago. He carries on in the same tradition; no hour is too late or too early for his brand of fishing, if it will add a new call to his reception log. He watches the vagaries of nature, until he can predict with a fair degree of accuracy when "conditions" will be just right. Program content means nothing; he lives only for the moment when call letters are flashed on the screen or announced by voice. (And he'll tell you that this is done all too haphazardly to suit his requirements!)

The true dx-er keeps an accurate log, and this is important. As in many other fields of scientific endeavor, the amateur TV dx observer is in a position to make real contributions to our knowledge of v.h.f. wave propagation. It is with this thought in mind that RADIO-ELECTRONICS has encouraged the careful observation and detailed reporting of TV dx reception. Reports are gone over for information of general interest and then made available for study by individuals or agencies interested in v.h.f. propagation. (See "The Effect of Sporadic E on TV Reception" in the June, 1953, issue.)

The January issues of this magazine for the past three years have carried detailed analyses of these reports, together with explanations of the various forms of dx likely to be encountered. Readers who want to know more about the nature of TV dx are urged to read these articles. Otherwise some of the terms that follow may seem so much Greek.

*V.h.f. Editor, QST.

1954 in review

We need only stack the 1954 reports alongside those for previous years to see that there was a marked upturn in TV dx this year. There was also an increase in the number of reporters, and in the skill of the old hands. Anyone not experienced in this hobby might think it impossible to log 64 different stations in a lifetime, but one of our observers identified that many *in a single day!* At least eight have logged more than 100 stations and one fellow, who has been at it for 5 years, is up to 202.

The major season for sporadic-E dx was longer in 1954. Where heretofore there has been little doing before late April, a fair number of openings were caught in March. The dx season lasted well through August, and there were more openings in all the other "off months" than in previous years. It would be too repetitious to sort out the 1954 reports by station and date, as we have done previously, but spot checks of the more complete and accurate logs show that, except for the longer summer season, dx followed closely the well-established geographical and seasonal patterns.

The 1954 file runs to several thousand individual observations from nearly every state of the Union and from Yellowknife, Northwest Territory, to Buenos Aires, Argentina. TV stations of 10 countries were identified. As before, stations in the lower latitudes were reported most often, with the Cubans well up toward the top of the list. All forms of dx were reported most often by observers in the Gulf states, with the Great Lakes region and the coastal states, east and west, following close behind.

Some rare dx

With an ever greater number of stations on the air, and with programming now running to full-day proportions, the chance of catching extreme dx would seem to be diminishing. Even so, several South American stations have been logged by our keener observers. PRF-3, Sao Paulo, Brazil, takes the prize among the South Americans. This station has been reported several times before, but never so often or widely as in 1954. If you can recognize the difference between Spanish and Portuguese when you hear it spoken, watch any Latin-American reception closely. This aid enabled G. P. Oberto, Richmond, Va., to dig out PRF-3 on May 17, at 7:30 pm, E.S.T., and May 20, at 7:05 pm.

Bob Seybold, Dunkirk, N. Y., also caught PRF-3 on May 17 and again on June 17. Ronn deNeuf, Ithaca, N. Y., picked it up on May 20, also around 7:30 pm, E.S.T. Fred L. Hall, Wichita, Kans., saw it on July 18. Harry Nelson, Winchester, Va., saw PRF-3 back on Sept. 10, 1952, but had not reported it previously. What is probably a world TV dx record was the achievement of Bob Cooper, who reports 16 minutes of PRG-3, Rio de Janeiro, Brazil, July 22, beginning at 11:47 P.S.T. A distance of more than 6,600 miles, it is approached (to our knowledge) only by the South African reception of the BBC, back in the high sunspot years of 1946-48. And that, of course, was under highly unusual atmospheric conditions.

These South American reports are of special interest to hams who work the amateur 50-mc band, as sporadic-E communication between North and South America has been practically nonexistent. It would appear that with proper coordination of effort, some very

nice amateur dx might be possible on 50 mc at times other than during the high sunspot years.

We continue to get scattered high-band TV dx reports that also have no counterpart in amateur communications experience, Ernest J. Smith, Bennettsville, S. C., reports reception of KGGM, Albuquerque, N. M., on channel 13, but gives no details. This is about 1,200 miles, a distance that has been equaled by hams on 144 mc, but never approached on 220 mc, which is just outside the high edge of channel 13. Tommy Larkins, Clarkville, Tenn., reports WATV-13, Newark, N. J., at 11:30 pm, Dec. 29, 1953. This is some 750 miles, at a season when high-band dx is a rarity. Reception of high-band stuff from Havana and Galveston, Tex., is reported by Dorsey Akers of Charleston, W. Va.

High-band dx of a tropospheric nature is common in the warmer months, with September and October perhaps the best. Albert Brant, Salem, Ore. logged KFMB-8, San Diego, about 950 miles, in October. The advantage held by the Gulf states in regard to tropospheric dx is shown in the logs of Weems and Betterworth of State College, Miss.; Blalock, Tallahassee, Fla.; Sherman, Sinton, Tex.; Doss, Dallas; Walker, Daytona Beach; Bondurant, Tampa; Hopwood, Miami, Fla., and many others. These observers find it not uncommon for channels 7 to 13 to be open across the Gulf, at distances up to 750 miles or so, even in January and February. The reports of a score of Gulf states observers indicate that the period of Feb. 25 to 27, for instance, was equal to almost anything that the summer had to offer.

The Southerners don't have it all, however. L. A. Canning, Halifax, N. S., found signals from New York to Washington, D. C., on all channels the night of April 20. He got WATV-13 and saw a picture from WPIX-11 for the first time. These are in the New York area, more than 500 miles away. Canning is one of the very few observers who have definitely identified auroral propagation in TV reception. On Sept. 30, he found broad mushy signals coming from 5 degrees west of north. Both audio and horizontal sync were badly garbled on signals picked up on channels 2, 3, 4, 5 and 10. Indications were that they were New York and Philadelphia stations, from what little audio could be copied. He lists a new Canadian station for dx-ers to shoot for: CJCB-4, Sydney, N. S.

Another far-north station, as yet unreported in the States, is KFIA-2, Anchorage, Alaska. This was logged on Aug. 28 and 29 by Glick, of Yellowknife, Northwest Territory.

The Southern record is held by Middleton of Sanford, Fla., who logged LVD, Buenos Aires, on July 8, 1953, between 5 and 6:15 pm E.S.T. Another interesting Latin American report, possibly a case of mistaken identity: "HGLO" reported by Aldridge, Winston-Salem, N. C. According to international prefix assignments, this would be in Colombia, but we have not heard of it from other observers.

YVKA, Caracas, Venezuela, was picked up by Akers, Charleston, W. Va., on both channels 2 and 5, at 5:12 and 6:18 pm E.S.T. on May 13, and on channel 5 June 11 and 15. A channel 2 station with the call CR5J was intercepted along with YVKA on May 13. Anyone know more of this one? In the international prefix table this sequence is reserved for Portuguese colonies.

Some u.h.f. dx, too

When u.h.f. stations first came on the air, 50 miles was considered good dx for channels 14 to 83. As we gain more experience with it, u.h.f. is turning up stuff almost equal to the best observed on 7 to 13. Seybold, Dunkirk, N. Y., has 10 u.h.f. stations more than 200 miles distant, with WEEK-43, Peoria, Ill., 480 miles, and WWOR-14, Worcester, Mass., 350 miles, as his best west and east. Reception up to nearly 400 miles was fairly common during the fall tropospheric bending periods. Bob uses stacked corner reflector antennas 70 feet above ground for his u.h.f. reception.

Four stacked bowties and a hilltop location help Louis Matullo, Washington, Pa., in pulling in plenty of u.h.f. dx, including just about every u.h.f. station out to Waterloo and Ft. Wayne, Ind. Lou keeps perhaps the most complete record of weather and reception conditions of any dx-er we know of, and he's watching the TV channels night and day, whether he is at work (as a TV service technician) or at home.

Burst reception

Several observers report occasional bursts of short duration, when conditions do not appear to be favorable for dx. A lot remains to be learned about this sort of thing, but we know of at least two natural phenomena that can be responsible. Ionized trails formed by the passing of meteors through the E region of the ionosphere are known to reflect frequencies up to at least 150 mc, possibly higher. Such bursts are usually of so short duration that they are useless for normal reception. Occasionally they may hold on for long enough to permit identification. They have been known to last for nearly 2 minutes, probably because of the overlapping of several individual bursts. They may bring in flash signals from distances up to 1,200 miles or more.

Lightning flashes, too, have been shown to develop sufficient ionization to reflect v.h.f. waves. The reflecting region is lower, in this case, so the distance over which its effect is noticeable is shorter. Usually lightning effects show up as sudden enhancement of the strength of a signal you're already seeing, whereas the meteor burst is usually a flash of signal from beyond even the best tropospheric range.

Bursts have been reported by Matullo; Ross, River John, N. S.; Erickson, Havre, Mont.; Chadwick, Wilcox, Sask., and DeGeer, Tulsa, Okla. We welcome more observations of this nature, particularly in high-band or u.h.f. reception.

What it takes to receive dx

Many correspondents ask for details of equipment used by outstanding dx-ers. No doubt these readers feel that the more successful observers must have some magic formula to account for their superior results. A good high antenna, a clear quiet location far from sources of man-made noise, nearness to large bodies of water—these are all helpful factors. But we think the red-hot TV dx enthusiast's real secret weapon is perseverance. Knowledge of the most likely times for dx (we've covered this information several times in the past, and RADIO-ELECTRONICS carries quarterly forecasts) and familiarity with the correlation between weather variations and dx propagation are important aids, but it takes time and patience to run up impressive totals.

At least one fellow we know went to some trouble to get a good antenna, too. Grant Ross, Marathon, Ont., was more than 300 miles from the nearest TV station, Green Bay, Wis. To get a better shot in that direction, he erected a large rhombic array on a 300-foot hill and ran an 1,800-foot transmission line down into the valley. This enabled him to get excellent signals from WBAY-2 at least 40% of the time. Poor or useless reception prevails only 20% of the time. The rhombic also serves him well whenever dx is coming through.

Over fifty TV dx club

Listed below are the records of some of the outstanding observers. This information was taken only from reports where totals were compiled by the correspondent himself. We know that it passes up much excellent work done by others. If you'd like to have your record in this section the next time it is published, please include your totals when you report.

NAME	LOCATION	TOTAL	U.H.F.	BEST DX
Dorsey W. Akers	Charleston, W. Va.	202		1,200*
Robert Seybold	Dunkirk, N. Y.	163	19	4,900
Bedford Brown, Jr.	Hot Springs, Ark.	162		
Fred Von Gunten	Berne, Ind.	154†	20	
Louis Matullo	Washington, Pa.	146	19	
Russell Ashworth	New Bedford, Mass.	121	22	
Robert Weems, Jr.	State College, Miss.	102		
Art Collins	Buffalo, N. Y.	100		
Roger Anderson	Madison, S. D.	99	26	
Bob Cooper	Lafayette, Calif.	92		6,600
F. E. DeGroat	Salamanca, N. Y.	90		
Douglas Bryan	Otey, Tex.	86		
Ronn deNeuf	Ithaca, N. Y.	83	12	
Ernest J. Smith	Bennettsville, S. C.	83		2,300
Alton Caldwell	Brockton, Mass.	81	4	
Paul Mitschler	Marysville, Kan.	81		
Toby Chambers	Miami, Fla.	76	1	
Joe Foyer	Westville, Ill.	72	15	
Mrs. Wm. Callan	Altoona, Pa.	72		
Kenneth C. Bush	Buffalo, N. Y.	71		
James M. Homan	Biloxi, Miss.	70		
Ross Brown	Tupperville, Ont.	66		
Tommy Larkins	Clarkville, Tenn.	66		
Danny Startzman	Bennington, Kan.	64		
R. A. Wilson	Detroit Lakes, Minn.	62		
Carl F. Lupton	Shelbyville, Ill.	61		
Harry Wieskamp	Holland, Mich.	58	14	
Kenneth M. Neal	Hamlin, Tex.	55		
M. W. DeGeer	Tulsa, Okla.	55		
Karl Kleintop	Bowmantown, Pa.	52	8	
Richard Gleitz	York, Pa.	52	11	
W. C. Sherman	Sinton, Tex.	50		

* High band—CMBF-7 and KGUL-11
† 126 photographed.

END

COLOR TV CIRCUITS

Part IX—The Lawrence strip type tube; its operation and circuitry

By KEN KLEIDON* and PHIL STEINBERG*

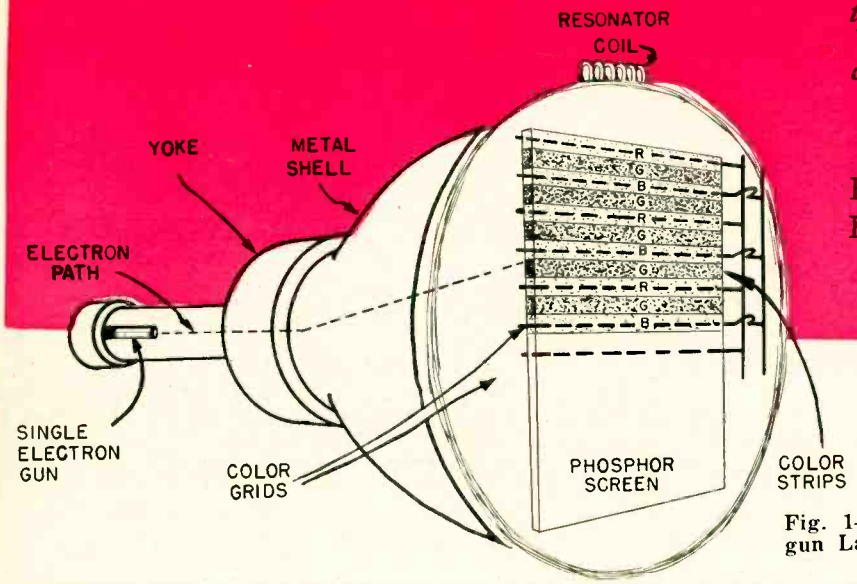


Fig. 1—The single-gun Lawrence tube.

ALTHOUGH the three-gun dot type color picture tube is predominant at present in commercial color receiver production, many feel that the Lawrence strip type tube will eventually be used for a lower-cost, mass-produced color set. The disadvantages of the strip type color tube, which discouraged its early use, were excessive 3.58-mc radiation, poor vertical resolution especially on single color fields and limited production facilities. According to the tube licenser, the first two disadvantages have been remedied and production facilities will soon be improved.

The Lawrence tube has, according to the manufacturer, a number of distinct advantages over the three-gun tube, including:

Advantages to consumer:

1. Larger color pictures
2. More brilliant picture because tube makes maximum use of electron stream
3. Stable color pictures because of simplicity of receiver circuits
4. Better and sharper black-and-white pictures
5. Simpler controls

Advantages to receiver manufacturer:

1. Smaller cabinet—tube is shorter due to its wide deflection angle
2. Standard deflection and focus components
3. Low raster scanning power
4. Simple low-cost circuitry
5. No high-voltage regulation required
6. No purity or convergence components
7. Quick circuit alignment
8. No mu-metal shield needed to shield tube from stray magnetic fields

Advantages to tube manufacturer:

1. Lower scrap rate and easier manufacturing because design allows greater tolerances than other type color tubes
2. Manufacturing techniques parallel those for black-and-white tubes
3. Less expensive and fewer component parts
4. Lower manufacturing cost for larger color pictures
5. Greater profit margins

Because of these advantages, the Lawrence type color tube is worthy of serious consideration by the television technician.

The single-gun tube

The Lawrence tube differs greatly from the three-gun dot type color tube in that it contains only one electron gun and the face of the tube is composed of phosphor strips rather than dots. Also, a grid structure is located directly behind the phosphor strips in place of the shadow mask. Fig. 1 illustrates the Lawrence tube and its major components. The single gun serves as the electron source to excite the red, blue and green phosphor strips. These are arranged in the sequence, from top to bottom, of red, green, blue, green, red, green, blue, green, red, etc. There are an equal number of red and blue strips and twice as many green strips as there are blue and red strips. The width of the strips is shown out of proportion in the illustration for the purpose of clarity—there are hundreds of horizontal phosphor strips on the tube face.

Located directly behind the phosphor screen is a grid structure composed of two sections in the same plane, termed color grids. One section of the color grid has a grid wire positioned directly behind each red phosphor strip and the other a grid wire positioned directly behind each blue phosphor strip. Connections to the two color grids are provided by terminals at the top of the tube. A resonator coil is connected to these, and with the internal capacitance presented by the color grids, will resonate at a frequency of 3.58 mc. Its function is to modulate vertically at a sinusoidal rate each horizontal scanning line. This resonator coil is driven by a power amplifier and is shielded to prevent radiation of the 3.58-mc signal.

The deflection yoke is almost identical to the type used for a conventional black-and-white receiver and, since no yoke purity adjustment is required as with a three-gun tube, its adjustment or positioning is not as critical. The high-voltage requirement is about 18 kv, unregulated, and is applied to the phosphor screen. A potential of 5 kv is applied to the color grids.

Fig. 2 shows a side view of the color grids and the phosphor screen for three different conditions. Since the color grids for the blue phosphor strips are connected to one end of the resonator

*Raytheon Manufacturing Company, Television and Radio Division.

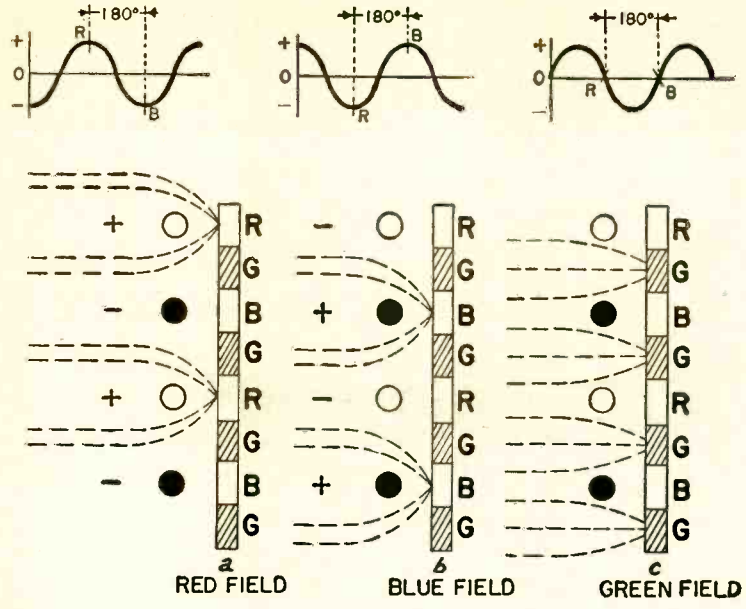


Fig. 2—Side view of grids and screen of a post-deflection focus tube.

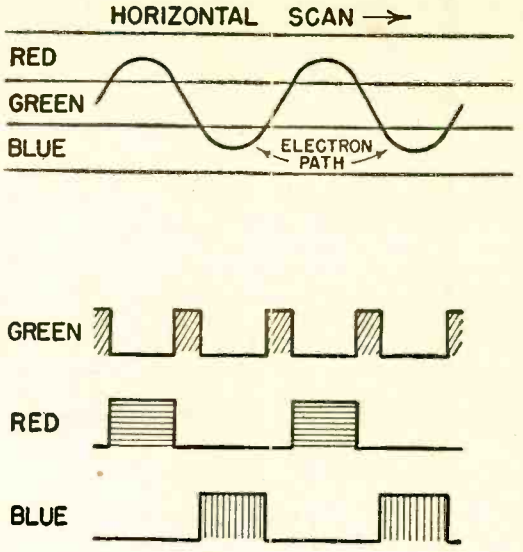


Fig. 3—Path of the electron beam due to action of the resonator coil. Also shown is the color gate time intervals.

coil, and the red grids are connected to the other, the grids are 180° out of phase. Fig. 2-a illustrates a resonator-coil polarity condition when the red grids are positive due to the resonator sine-wave phase and the blue grids are negative, since the grids are 180° out of phase. For this polarity, the electrons strike only the red phosphor strips. The combination of electrostatic fields caused by the color-grid polarities and the focusing action due to the 13-kv difference in potential between the color grids and phosphor screen prevent electrons from striking the green or blue strips.

Fig. 2-b shows the opposite condition—the blue grids are positive, the red grids negative. Thus, the electrons will strike only the blue phosphor strips.

When the grids are at the same potential (Fig. 2-c), the electrons strike only the green phosphor strips. The focusing action which takes place due to the 13-kv difference in potential between the color grids and phosphor screen prevents the electrons from striking the red or blue strips.

Fig. 3 shows the effect of the resonator coil on the path of the electron beam during a portion of one horizontal scanning line. The horizontal deflection voltage applied to the yoke moves the electrons from left to right across the face to the picture tube, as in any monochrome picture tube. However, at the same time, a sinusoidal deflection voltage is applied to both sets of color grids by the resonator coil as described previously. This deflects the path of the electron beam in a sine-wave displacement and the electron beam scans three strips in the following sequence: green, red, green, blue, green, red, etc. As with a monochrome picture tube, vertical deflection voltage is applied to the yoke at the same time so that the electron beam will move down to scan the next lower set of strips for the next horizontal scan period.

The last step necessary to produce a color picture on the Lawrence strip type tube is to control the electron beam so that, when the beam is striking the red phosphor strip, the red video signal will be modulating the electron beam, and the same for blue and green. To separate the three primary colors in the receiver the picture tube is gated. By gating, we mean that only green video information is allowed to modulate the electron beam while it is crossing the green strip, only blue video information is allowed to modulate the electron beam while it is crossing the blue strip and similarly for the red video information.

Fig. 3 also shows the time intervals required for gating the green, red and blue signals for proper modulation of the electron beam. The gating process in the receiver is controlled by the same type of 3.58-mc color oscillator, synchronized by the color burst signal, as in the three-gun-tube color receiver.

Single-gun circuitry

A block diagram of the circuitry for a Lawrence tube color receiver (Fig. 4) shows that most of the color circuitry is similar to that for a three-gun color picture tube. The first and second video amplifiers, bandpass amplifier, demodulators, color oscillator and control, and the matrix circuits are nearly identical for both three-gun and single-gun circuitry. Red, green and blue video signals are obtained from the matrix, as for the three-gun tube, and are applied to their respective gate circuits and then to the Chromatron cathode. Differences do exist between

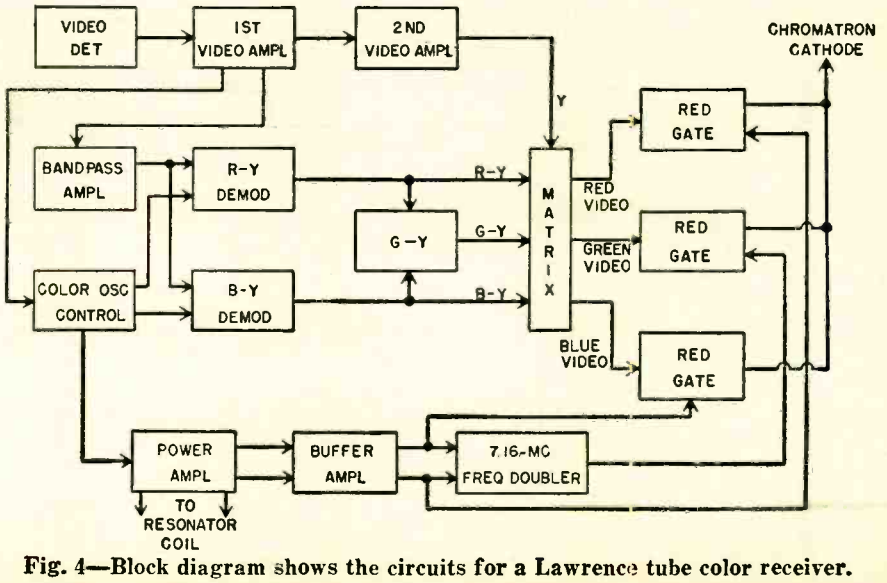


Fig. 4—Block diagram shows the circuits for a Lawrence tube color receiver.

the 3.58-mc color oscillator output circuit of the three-gun and single-gun tubes. In the single-gun Lawrence circuitry an additional oscillator signal, at the second harmonic of 3.58-mc (7.16-mc), is coupled to the green gating circuit.

A gating circuit is nothing more than an amplifier with a video signal coupled to its control grid and a gating signal applied to its screen grid. The gating signal is the oscillator signal and the stage is designed to allow the amplifier to conduct only on the positive peaks of the 3.58-mc (7.16-mc for green gate) sine-wave oscillator signal applied to the screen grid.

Referring to Fig. 3 again, the gating time intervals are shown for the red, blue and green gating circuits. This shows that the red gate will conduct or allow the red video information to pass to the color picture tube only during the time period shaded with horizontal lines, which corresponds to the time that the electron beam is exciting the red phosphor strip.

An action that is similar to this occurs for the blue gate, the only difference being that since the electron beam, traveling according to a sine wave, passes the blue strip 180° after passing the red strip, the blue gating signal must be 180° out of phase with the red gating signal. The blue gate conducts or allows the blue video information to pass to the color picture tube only during the time period shaded with vertical lines.

Since the red and blue gating time intervals occur once for every cycle of the 3.58-mc sine-wave electron-beam deflection, the frequency of the gate action must also be 3.58-mc. The green gate, however, must operate twice for every cycle of the electron-beam sine-wave deflection. Therefore, the green gate signal must be twice the frequency of the red or blue gating signal ($2 \times 3.58\text{-mc} = 7.16\text{-mc}$). Also, the green gating signal must be 90° out of phase with the red screen gating signal as the electron beam passes the green strip 90° after it passes the red strip. For proper phase relationships, the screen gating signals are obtained from the same 3.58-mc power amplifier which drives the resonator coil.

Fig. 3 also shows that the width of the green gating interval is half that of the red and blue gating intervals, which are equal. Since the green gating interval occurs twice as often as the red and blue and is only half as wide, all three phosphor strips will receive equal electron-beam excitation.

The action of the gating circuit is such that for a single color field, red for example, the blue and green gating circuits prevent blue and green video signals from reaching the cathode of the picture tube. When the gate circuits are closed, they bias the picture tube beyond cut off during the gating intervals and no electrons are emitted from the cathode during the time the sinusoidal electron beam strikes the blue and green phosphor strips. The red gate allows excitation of only red phosphor strips and results in a red field.

Variations of the circuit shown in Fig. 4 are possible in the same manner as for a three-gun picture tube. For example, gated R − Y, B − Y and G − Y color-difference signals can be applied to the cathode of the color picture tube while the Y signal can be applied to the control grid. For a black-and-white picture with this arrangement, the outputs from the three gating circuits are equivalent to bias voltages for the electron gun, sufficiently high so that only the Y signal controls the electron beam. The Y signal as described in a previous article is equivalent to the black-and-white portion of the composite color video signal. If the amplitude of the sinusoidal deflection voltage is adjusted properly, the red, blue and green phosphor strips will be excited equally and result in a monochrome picture.

The next and final article will consist of a summary of the previous articles and practical color service information. TO BE CONTINUED

Note: More detailed information on Lawrence tube circuitry will be presented in a forthcoming book, *Color TV Circuitry* by the authors of this series of articles and available through the publishers of RADIO-ELECTRONICS magazine some time in 1955.

Viewer Injured as TV Receiver Implodes

A housewife suffered superficial cuts on her arms and legs as the result of a violent implosion of the picture tube in her television receiver (see photo). Mrs. Bonnie Patlon of Harbor Hill, Fla., was watching television in her living room. At 9:30 in the evening she heard a frying sound. As she continued to watch, the picture flashed bright, accompanied by "a loud popping noise that sounded like a light bulb exploding."

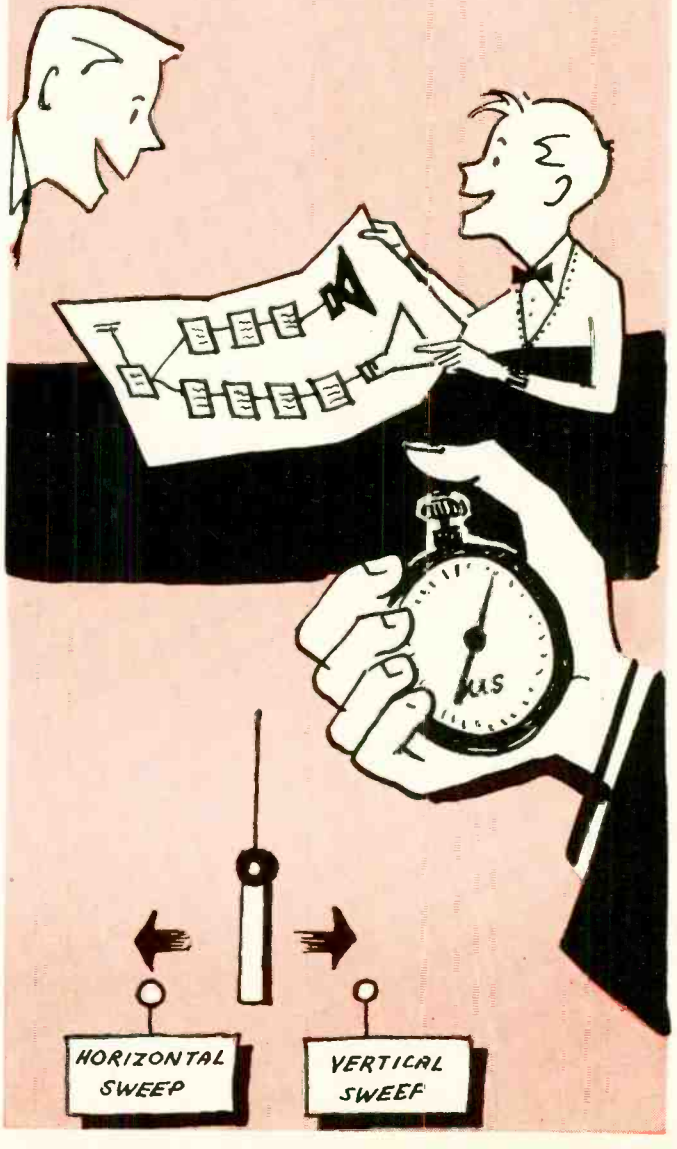
Mrs. Patlon started for the television receiver to turn off the power, but as she passed in front of it, the blast occurred. She was thrown back into a chair as glass showered across the 12-foot room and out onto an adjoining porch. The entire picture tube and safety glass was blown into the room.

The local police chief reported he could find no reason for the implosion. Just why the police chief was sent for was not explained.

TELEVISION . . . *it's a cinch*

By E. AISBERG

Fifteenth conversation, first part: Separating the sync signal, why, where and how; diode and pentode separators



WILL—Now I'm sure I know it all!

KEN—Your usual modest self, I see! But just what prompted that remark?

WILL—What I mean is—now I know the televiser from end to end—from first r.f. to last v.f. And besides that, I haven't forgotten the time bases. So, I know all the circuitry of . . .

KEN—Don't get excited, Will! You've still plenty to learn! For example, how are you going to go about synchronizing those time bases?

WILL—Now that you mention it, I remember that the vertical and horizontal sweep circuits are synchronized by the sync pulses we studied a long time ago. But where's the problem? If you just apply the composite video signal to the sweep oscillators . . .

KEN—. . . you'd get into plenty of trouble! The mixture of video signals with the horizontal and vertical sync pulses would keep triggering the sweep circuits at the wrong times! When you figure your time in microseconds, everything has to be neat and clean. Each sweep oscillator has to receive its own sync pulses, free from any other signal whatever. Those sweep circuits can often be started into action by the least fluctuation of the voltage on the grid of the tube that triggers them.

WILL—I see what you're coming to: you have to separate the sync from the picture signals. Because I remember when you first drew a block diagram of a televiser, you had a block marked "sync separator."

KEN—I hope, then, that you'll have no trouble figuring out how such a circuit would work?

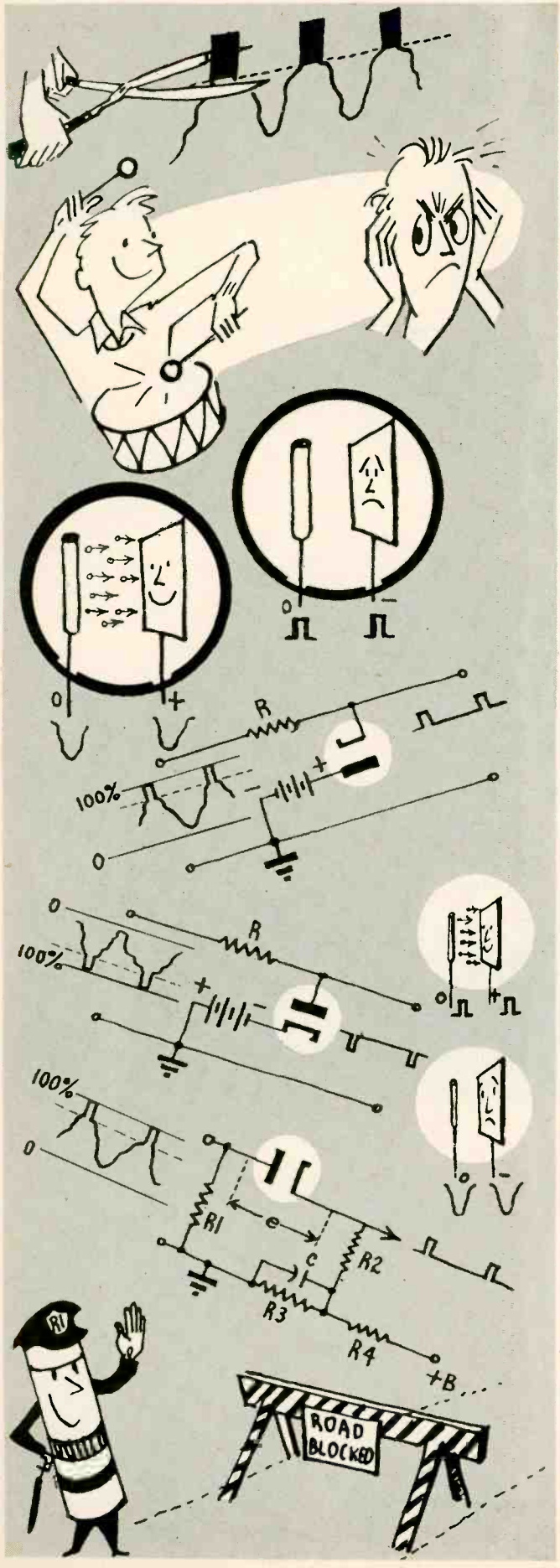
WILL—I suppose we'll have to have some kind of electronic switch that applies the signals to the right sweep circuit at the right time. For example, at the end of each line, the voltage is applied to the horizontal sweep, and . . .

KEN—No, Will. First of all, how would you synchronize your electronic switch? Can't you see another way of capturing the pulses from the video signal—a method based on some fundamental difference between the two sorts of signals?

WILL—Well, the main difference is in their amplitudes . . .

KEN—You're on the right track. Keep going!

WILL—The sync pulses occupy the top 25% of the composite video signal. Voltages below that represent the video image, ranging from black to white. So all you have to do



is cut off the top 25% and you then have only the pulses.

KEN—Excellent, Will! Only instead of cutting, it's called clipping.

WILL—But just how can you clip the top off a wave?

The limits of patience

KEN—It's easy. Just apply the signal to a tube that will function perfectly up to a given point, but absolutely refuses to pass that limit.

WILL—H'mm, something like my Uncle Jack. He never did like much racket, so I was always a little worried when I was practicing as a Boy Scout bugler. He never said a word; but the day I started to train for a drummer, he blew his top! But what kind of tube acts like that?

KEN—You use pentodes, generally. But a triode could be made to work, and in many setups a simple diode does the job—fairly well at that.

WILL—And where do you put this separator?

KEN—Theoretically, you could separate the sync signal before the detector, for the signal would be detected while you were clipping it. But it's an unreliable way in practice. So it's usually put at the output of the video amplifier, or at least after the first video stage.

WILL—And of course the signal can be either positive or negative, according to whether you apply it to the grid or cathode of the separator.

KEN—You can have either polarity of signal, though there are several circuit tricks that are better than applying an input signal to the cathode.

WILL—Now suppose we have a positive signal, so the first 75% of the voltage is below the sync level. How is a diode going to clip off the top 25%?

KEN—There's more than one way to do it. The easiest is to use a diode biased so that its cathode is more negative than the plate at all voltages below the point where you intend to begin clipping. You shunt your diode across a source of composite video signal. The diode short-circuits all voltages up to that which makes the cathode more positive than the plate. So the sync signals, which are more positive, stop the diode conducting and pass on to the output.

WILL—I can see that the diode should be biased so the plate is a little more positive than the highest video signal voltage—a little above the black or pedestal level, whatever you like to call it. Then you are sure to short all the picture signals through the tube. But what's this resistance R in your hookup?

KEN—It keeps the diode from shorting the stage that supplies the signal. You are getting your signal from some point in the video circuits and you can't permit your sync separator to affect the signal going to the picture tube. The picture tube has to get all the picture signal without distortion, and also the sync signal to black out the return trace.

WILL—Of course—I just didn't think of it . . . But now can you draw me a circuit for negative-going signals?

KEN—Certainly. We just turn the diode around and make the cathode more negative than the plate again. If you have the right bias, it remains more negative through the range of picture signals so the diode shorts them out. But the sync pulses drive the plate more negative than the cathode, conduction stops and the sync signal passes through. And that's how a shunt type separator works.

WILL—You give me the idea there must be a series type separator as well.

KEN—There is. One circuit is like this. The cathode is connected into a voltage divider (R3, R4) that makes it a little more positive than the plate. If the bias is right, only sync pulses can pass through the tube. You take the output pulses off R2, and C passes any alternating component.

WILL—What's R1 for?

KEN—It's just to give you a closed diode circuit—makes it possible to connect to your signal supply source through a capacitor. It may have other uses, as you'll see later.

WILL—I think I see how this works. If the bias voltage is about the same as the video signal at the black level, no picture signals can get through. But when the sync pulses raise the voltage higher, the plate is more positive than

the cathode, the circuit conducts and the pulses go through.

KEN—Good reasoning, Will. And the output of the circuit —the voltages across R2—consists of nothing but a series of positive pulses.

WILL—Would this work for negative pulses?

KEN—Well, if you need to make a positive signal out of a negative one, you can always use a triode as a phase inverter. But this circuit will work with negative signals, if you reverse the diode like this. Your cathode is now more positive than the plate except when the very negative pulses come through. They drive it more negative and the pulses are passed.

WILL—One thing I don't like about these circuits—the batteries you keep throwing in. This is an all-electric age—can't you make them all work with voltage dividers to bias your diode elements?

KEN—I just used the batteries to simplify the drawing. They wouldn't be used in a television receiver. Take a look at this circuit. You apply the positive-going composite video signal through C1. Each pulse attracts electrons from the cathode, which have to flow back through R1. That biases the diode so the plate is more negative than the cathode. By choosing the right values for C1, R1 and R2, you can adjust the bias so that the tube begins to conduct just at the black level. The sync pulses then appear as voltage pulses across R2. The great feature of this circuit is that it is self-adjusting to different signal strengths. If you get your components adjusted so the diode just triggers at the right level on a medium-strength signal, stronger signals will increase the bias and weaker ones decrease it, because of the change in current through R1. So both weak and strong signals will clip at the right point.

With three grids or more

WILL—The bias batteries would never do that. One good thing about the diode—it doesn't change the polarity of the pulses. And the circuits are simple. I wonder why anyone would want to use pentodes?

KEN—Simplicity doesn't always mean perfection! Our diode separators are weak in many ways. The separation is imperfect, for the high-frequency picture signals—those that represent very rapid variations of intensity—work their way into the sweep circuit time bases through the interelectrode capacitance of the diode. That can give you sync trouble. Another thing—a diode doesn't give out with more signal than you put into it, and never quite all of that. So, it's only natural to take advantage of the pentode because it amplifies. Besides, its grid-anode capacitance is very small, so little or no high-frequency picture signal can get through.

WILL—But how do you limit the patience of a pentode?

KEN—Its patience—actually, its plate current—can be limited at either end. We can make our tube blow its top at the least provocation or we can push it so far it will give up and tolerate anything. Take a look at this grid-voltage–plate-current characteristic curve. Right down here—in the negative-voltage region—you have a bend. And again—near zero volts—there's another very sharp bend followed by a long level stretch.

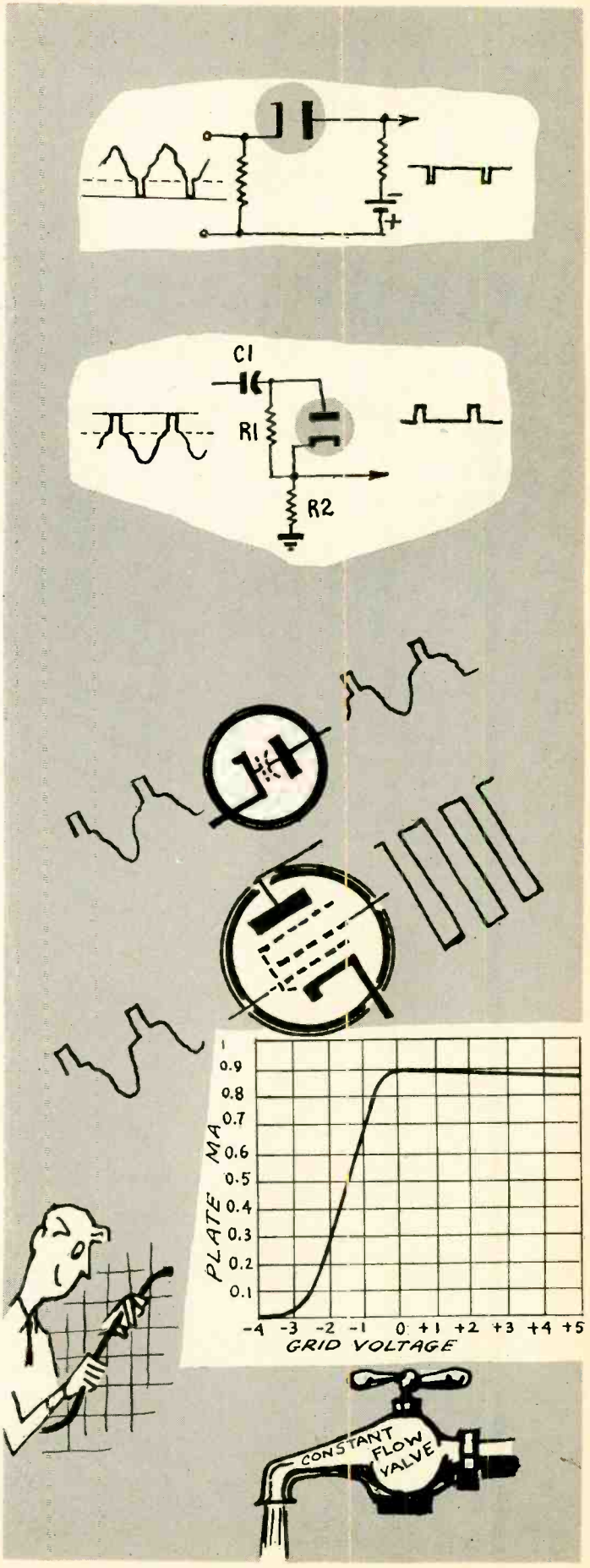
WILL—So that any increase of grid voltage from that point won't affect the plate current?

KEN—Exactly, and that applies to any reduction of grid voltage beyond the lower—or plate cutoff—bend. Since the plate current reaches zero at that point, it has to stay at zero if the grid goes more negative.

WILL—I'm beginning to see just how you could use those two limits of patience. But that curve doesn't look too standard to me. Just how do you model that kind of a grid-voltage–plate-current characteristic?

KEN—By applying the right voltages to the screen and plate. The idea is to prevent the plate from receiving more than a certain amount of current, however wide you may open that electron valve we call the grid. So you put a very low voltage on the plate and a higher one on the screen. Or you can tackle the problem from the opposite direction and put normal voltage on the plate but very low voltage on the screen.

TO BE CONTINUED



TED TACKLES TOUGH TV PROBLEMS

By WALLACE WANER

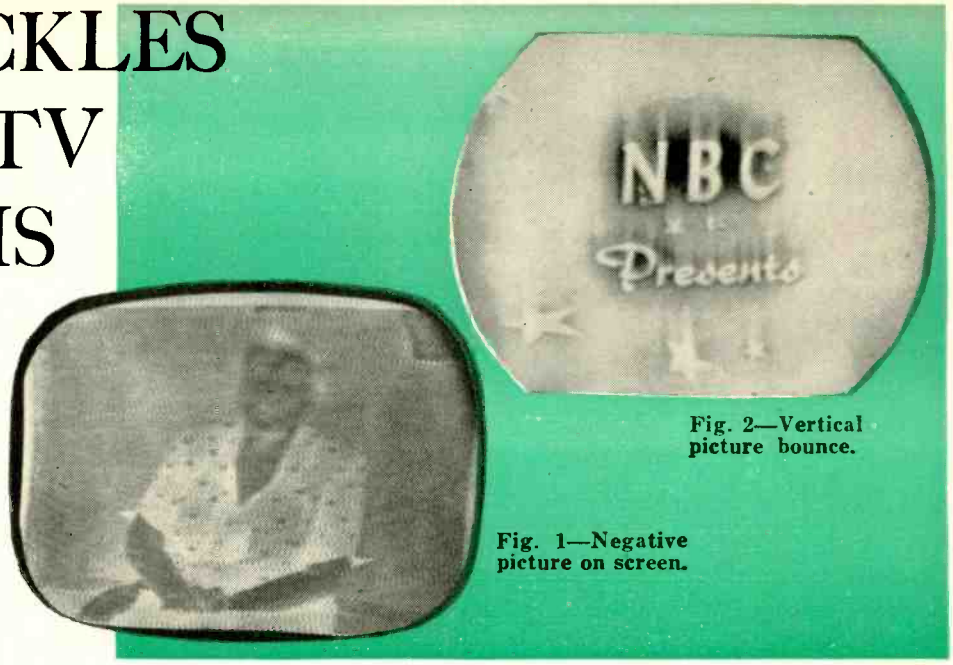


Fig. 2—Vertical picture bounce.

Fig. 1—Negative picture on screen.

WHEN I hired Ted a few months ago, he was green from a local television school. His only practical experience had been a few minor repairs on his own receiver or those of his relatives, plus what little lab work he got at school. The kid's sharp though and when he learns new things, he doesn't forget them.

Our Main Street shop is small and our personnel consists only of Ted, our outside man Jim, and myself. On occasion I help Ted with the bench work, but the business end of the organization doesn't allow me too much time to tinker. So Ted is on his own for the most part and calls me in consultation only when he gets a sticker.

We service a variety of sets, so we often run across unusual or freak troubles, and I have standing orders with Ted to call me before he tackles any toughie.

Case of the negative pix

Only a few weeks ago Ted called me while I was sitting at my desk absorbed in a modern scientific treatise.

"Say, boss," he remarked casually, "I think I got one that would interest you."

Ted was at that age where he considered any show of emotion as immature. The more he acted like Jack Webb, the more excited he really was. Reluctantly I laid aside the summary of the latest Kinsey report and followed him into the workshop. The receiver was an RCA 7T143. A negative picture appeared on the screen and (while I wasn't unduly impressed) I got my camera and took a picture (Fig. 1) so Ted wouldn't be disappointed.

"What's the unusual angle?" I asked him. "It just looks like a bad a.g.c. system and picture overload."

"No, sir," Ted replied. "It isn't a bad picture tube either, nor is the alignment off!"

"O.K.," I told him. I'll tackle it and see what I can come up with."

Ted shrugged ever so casually. "That's not necessary. I've found the trouble. It's a bad first video amplifier tube."

"Oh, I see," I said hastily. I didn't want him to hog the spotlight exclusively. You got to bring these kids along slowly, even if they're talented, otherwise they'll get a swelled head. I took my time lighting a cigarette to give myself a better chance to review mentally some of my theoretical knowledge of the composite video signal. After the first slow exhale, I felt sure I had the right answer.

"With a dead tube," I pointed out, "capacitance still exists between the tube elements and the signal can still be transferred across it even with an open heater. This is particularly true of triode tubes in a strong signal area. The dead stage will not give a phase reversal of the signal as a live stage would. Therefore, the signal arrives at the picture tube with incorrect polarity for proper whites and blacks. Result, a negative picture!"

"It sounds logical," Ted said. "Anyway, I put in a new tube before you came in and it did result in a positive picture."

I smiled. "Did you put this old tube back just so I could take a picture, or were you trying to stump me on a rough one?"

"Oh no," he assured me. "I really wanted to know the theory behind the symptom, but you don't always give out with explanations unless I trick you into it. I heard you mention once that this was a television repair shop and not a training school."

I shrugged and walked away.

Case of the vertical bounce

Only a few days later Ted again called me to the workshop. I hated to be interrupted because I was trying to solve a perplexing business problem while resting my eyes on a Marilyn Monroe calendar. Reluctantly I tore myself away from my problem and followed Ted.

The set was a Westinghouse model H-746-K21 which had the nicest picture bounce (Fig. 2) you ever saw. Since movement cannot be photographed in a still picture, you will have to visualize the appearance. The picture jiggled up and down like a 5-year-old who has waited too long.

I watched the screen in silence for a few minutes trying to figure what in blue blazes could cause this. I stalled for time with my cigarette lighting routine but still didn't come up with an answer. So I hedged for time by asking Ted if he had made any preliminary checks.

"Yes, sir," he replied. "I've checked all tubes, voltages, and component parts. Everything in the vertical section and in the associated circuits seems to be in order."

"So what did you find is causing it?" I asked, trying to make it sound as though *I* knew but just wanted to know if *he* knew.

Ted shook his head. "I haven't been able to find the trouble this time and I thought you would help out."

Well, to make a long story longer, I rechecked everything Ted had checked and could find nothing wrong. After a couple of hours my usually serene disposition was beginning to fray slightly at the edges so I shut the set off and went to the receiver service notes to find out whether the manufacturer had any hints for this trouble.

For the first five minutes I couldn't

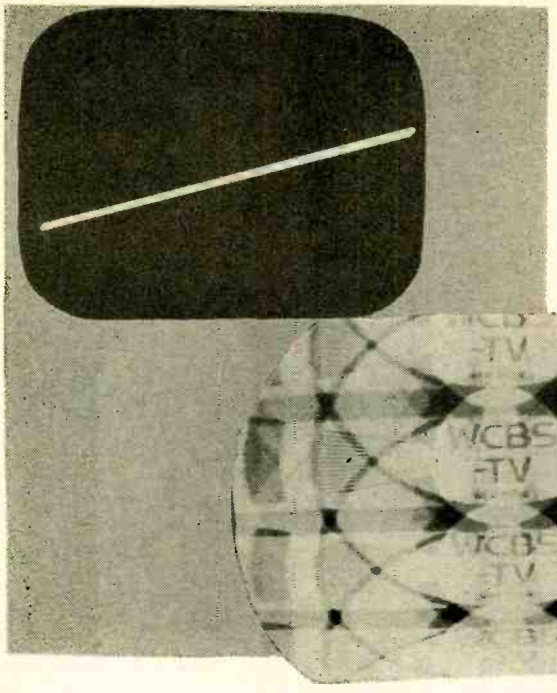


Fig. 3—Unusual diagonal pattern.

Fig. 4—Multiple vertical pattern.

concentrate, but I solved that problem by turning the calendar to the wall. After that it didn't take me long to get to the solution, and I must admit that I dropped my becoming dignity a trifle as I ran into the shop brandishing the service notes in my left fist.

The notes specified that a jumpy picture may result if the white a.g.c. lead that ties from the 12AT7 sync amplifier and sync control tube is not dressed away from the 6BK5 audio output tube socket. This helped to emphasize to us how the signals of one circuit can interfere with the operation of another by capacitive coupling when critical wires are dressed too closely to each other!

Case of the oblique line

The third odd trouble happened in a Philco model 52-T2100. This time Ted interrupted me while I was critically analyzing three new wrinkles which had appeared in my face. I was wondering whether this was the reason I hadn't been able to date any blondes in the last three days to help me show off my new red convertible. (And it doesn't make sense to date a brunette for a red convertible!)

When I got into the shop Ted showed me the receiver. The screen was dark —the only thing visible being a diagonal white line as shown in Fig. 3.

"What do you think of that?" Ted chortled. This was a little out of character for dead-pan Ted, but it is hard to gloat in a monotone.

I always like my employes to be happy so I fed his obvious glee at being able to show me such a peculiar symptom by saying: "That really *is* something. I've seen a horizontal line when the vertical sweep collapsed and I have also seen a vertical line when the horizontal sweep failed in a receiver with an r.f. high-voltage power supply. I must admit, however, that I've never seen a diagonal line."

"What do you think it is, boss?" Ted asked. "I just turned it on and haven't even opened the back."

"Well, it couldn't be any shorted turns in the yoke, because that would produce a keystoned pattern," I hedged, thinking aloud in this fashion while desperately hoping to arrive at a solution. "At the same time it would seem that we have neither vertical nor horizontal deflection, yet the bar indicates that there must still be some sort of deflection!"

I didn't want Ted to think I was losing my touch in trouble-shooting. It was bad enough that I felt I was losing out in acquiring the necessary accessories to go with red convertibles. Suddenly a thought struck me.

"You know, kid, there really is only one solution when you think of it. The vertical sweep has failed in this receiver and the yoke is tilted."

"But, boss, the yokes are bolted pretty tightly and can't move by themselves. I am sure the customer didn't loosen the brackets because he said the set hadn't been touched."

I smiled patronizingly. No matter how bright these young fellows are, they can't compete with years of experience in this business.

"Ted," I said learnedly, "don't you believe them. They all say that even when they bring the set in with all the parts loose in a basket. Let's take the back off and see what is what."

Three minutes later Ted stared at the tilted yoke in speechless surprise. Since he was duly impressed, I couldn't help driving home the object lesson.

"My boy," I said. (There is no better way to feel superior than to start off by saying "my boy.") "Let this be a lesson to you. Always listen carefully to what the customer has to say but in the final analysis rely on your knowledge of circuit theory and your practical experience!"

Case of the multiple image

The fourth trouble happened during the time I was trying to memorize the figures 3.5795. (No, you're wrong—it's the exact frequency by which the color-burst frequency is separated from the carrier in color television.) I wanted to have this number at my mental fingertips so I could work it into a conversation with Ted sometime and impress him.

This time the picture resembled that shown in Fig. 4, and the set was a Du Mont RA-117A.

"This one really has me stumped," Ted said to me. "The original trouble was vertical roll. I found a bad 390,000-ohm resistor in series with the hold control pot and replaced it with a new one. Now the picture has the multiple image you see, yet voltages, tubes, and all the other parts check O.K."

"But, Ted," I objected, "you know that the trouble must be in the vertical oscillator circuit, so everything can't be all right."

"Well," Ted replied, "if there is something wrong in that stage, it sure has got away from me. I checked everything several times and everything is exactly like the schematic."

"In that case," I told him, "the only thing that could be wrong is that you replaced the 390,000-ohm resistor in the hold circuit with one of incorrect value. That would upset the R-C constant and reduce the vertical oscillator frequency."

Ted shook his head. "No, that couldn't be it. See, the color code says orange, white, yellow for 390,000. The resistor is plainly marked in these colors."

I didn't even look closely at the resistor, because I'm partially color blind. I pulled over a v.t.v.m. and clipped the leads to the resistor scale. "Here's your trouble," I announced, "your 390,000-ohm resistor reads well over a megohm."

Ted muttered something like "I'll be darned," only stronger. "Hereafter I'll test every new part I put into a set.

With that I walked back to my office, sat down at my desk and again opened my little black book. Gloomily I paged through it and noted where I had checked off each blonde. With a sigh of resignation I picked up the phone and called Brenda, my favorite *brunette*.

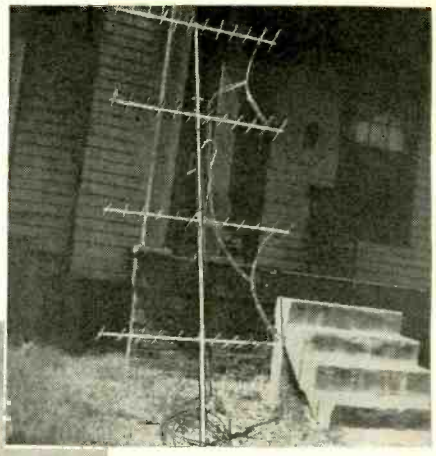
"Honey," I said, "how about a date tonight with me and my new red convertible?"

"I'd love to," she crooned, "but you may not like me anymore. I have just had a conversion job done on my hair and I'm now a decided blonde!"

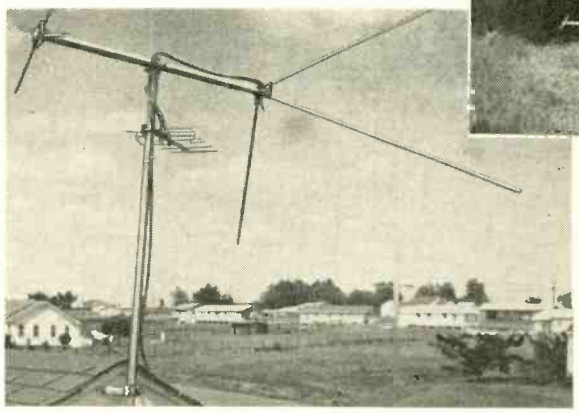
I hung up and sank back in my chair with a happy sigh. A wonderful business, this television repair game!! END

U.H.F. INSTALLATION TECHNIQUES

By HAROLD DAVIS



Stacked Yagis ready for installation.



Conical and Yagi mounted on common mast.

WHEN the first u.h.f. station went on the air in Portland, Ore., over two years ago, TV personnel from all over flocked to the West Coast to see this new system the FCC had devised for making television available to every nook and corner. What they found was a highly elusive and not too strong signal that often skipped over large areas and bounced off buildings and obstacles.

Since then technicians have made thousands of u.h.f. installations. Installing antennas for the u.h.f. channels is now a simple routine job.

Unlike v.h.f., u.h.f. fringe areas are where you find them. For instance, in St. Petersburg, Fla., there is a fringe area in the southern part of the city and in Jackson, Miss., there is one within sight of the tower. The man who goes into these areas and makes an ordinary installation will get nothing but trouble. Technicians don't have to be told where these bad spots are; they have only to look around at other installations to tell what the condition is. When you start seeing 20-foot-and-higher masts loaded with stacked Yagis, that's it.

To make a good ordinary installation in areas where the signal strength is normal only requires following a few simple rules.

A normal *u.h.f.* installation in most cities consists of anything from a bow-tie to a 12-element Yagi mounted on a 5- or 10-foot mast on a housetop.

The type of antenna is unimportant from the u.h.f. standpoint. However, because most viewers now have or will have v.h.f. available, combination v.h.f.–u.h.f. antennas are highly desirable. The most popular of these is the stacked-V. This antenna costs less than most other types, permitting the all-important low-cost installation. It may be stacked to provide increased signal strength in weak areas and, being not too directional, it will receive signals well from the sides and back.

The transmission line

Having selected the antenna, we must now select our lead-in and standoffs. In strong signal areas lead-in is no problem except in coastal areas. I have made hundreds of successful installations with flat lead-in. However, when the going gets rough, don't take chances! Use a good grade of oval, making sure the top is looped with the end down to prevent rain from collecting. In coastal areas seal the line to keep out the salt atmosphere. Then coat all connections with a good preservative.

Run the lead-in through standoffs that do not have a metal ring passing around the lead-in. Many a good u.h.f. signal is lost between the antenna and set because of this ring. Crooks and turns, particularly foldbacks, must be kept at a minimum, which makes selecting a spot for the antenna highly important.

The antenna should be located so that there is a short, direct lead to the set, requiring only two or three well placed standoffs. Never tape a lead-in to anything. To splice (Fig. 1), tape only the insulation with plastic tape. Leave the ends of the wires sticking out, twist and solder them, and then coat with a preservative.

Lightning arresters must be watched as a source of trouble. Underwriters Laboratories accept either a grounded mast or a lightning arrester. The grounded mast is preferable where city ordinances permit it. Finally, the u.h.f. lead-in must not terminate in loops lying behind the set.

In fringe areas, either local or out of town, the procedure changes somewhat —locating the antenna becomes the most important factor. The signal is usually there; it is just a matter of finding it. The area must be searched both vertically and horizontally. The only intelligent way to do this is with a field-strength meter.

When probing for a signal, first try all spots where the antenna can be conveniently mounted. There is no use finding a good signal at a spot where the antenna cannot be placed.

In probing, avoid reflected signals because they are unstable, have poor quality and at times will disappear completely. Engineers at u.h.f. stations are constantly working to improve their patterns, and with the electrically tilted antennas and other devices the field can change. Reflected signals can be recognized by rotating the antenna. The reflected signal will come from a different direction than the direct one.

Contrary to what has been said many times, I have never been able to gather direct evidence that trees deflect u.h.f. signals. The only way to tell for sure

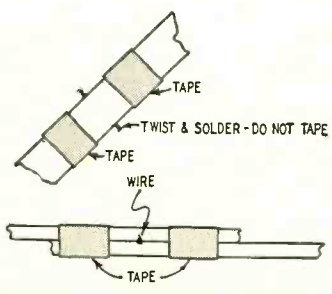


Fig. 1—Splicing transmission line.

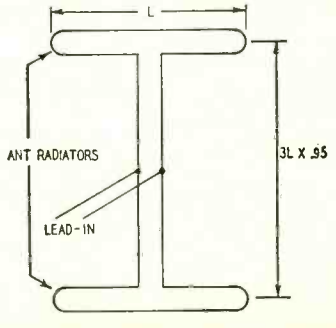


Fig. 2—Computing antenna spacing.

Probing for maximum signal strength.

would be to chop the trees down, since moving the antenna may have accomplished the desired result whether the trees have been there or not. In fact, I have seen good u.h.f. reception with the antenna directly facing a solid brick wall between it and the station.

Stacking antennas

If it is impossible to find a good signal, take the best you can find and see what can be done with it. If the signal contains only a slight trace of snow, changing to a higher-gain type antenna may do the trick. If using a stacked-V, change to a 12-element Yagi; and in most cases you should stack two of them. The gain of an antenna expressed in db looks good on paper, but those of us who climb house tops for a living know that it takes a bit of doing to undo a little snow.

In stacking u.h.f. Yagis, the best distance between them was found to be different from v.h.f. After painstaking trial and error, it was found that for frequencies below channel 40, the best distance is 5% less than *3 halfwaves*. You don't have to delve into intricate mathematics to find this distance. Simply consider the driven element as a halfwave (Fig. 2); multiply it by 3 and subtract 5%. For channels above 40, use slightly greater distances — subtract 2–4%. For 60 to 80, use 3 halfwaves.

Consider a 4-bay Yagi for channel 25. The bays are spaced 31.5 inches or slightly less than 3 half-wavelengths apart and are connected together in pairs as shown with open-wire line cut to fit. The length of the transmission line connecting the top pair of bays to the bottom pair is not important as long as the lead-in connects to the exact center. We make it just long enough to permit anchoring to a standoff insulator on the mast. This usually runs around 72 inches for a channel-25 antenna.

The difference between local and distant fringes in u.h.f. is that, locally, the signal is around somewhere if you can find it. In distant fringe areas, which start as near as 15 miles out, the signal starts decreasing in field strength.

Here, the "dos and don'ts" become still more important. Every db available must be carefully preserved. Everything said before must now be taken with emphasis. In addition, height now becomes the most important factor. In areas where the station has been operating for some time, the best practical height probably is already established. If all the other antennas are mounted on a 40-foot mast, you are wasting time if you start by trying a 20-foot unit.

In fringe areas the horizontal positioning of the antenna is not so critical, but any terrain advantage is highly desirable. Towns 50 and 100 feet higher than others get better u.h.f. reception even with lower antennas.

Deep fringe areas are found about 40 miles out. Here it is almost impossible to get an absolutely snow-free picture, but one nearly snow-free may be had with a good installation. For the deep fringe area use Yagis stacked four deep. The 5%-less-than-3-halfwaves distance is used between each antenna, and here again we vary from the v.h.f. hookup. For better reception the best hookup is shown in Fig. 3. The top two antennas are connected together, as are the bottom two. Open-wire transmission line connects the pairs together and the lead-in is in turn connected to the center of this. The connecting open-wire line may be sufficiently long to permit anchoring it to a standoff against the mast. Solder all connections. Use a minimum amount of standoffs, and they should now be placed with a field-strength meter. In fact, take the meter up on the house so that you can watch the result of everything that is done to the line.

After finishing on the housetop, move the meter to the porch or window and continue to watch every move to see that no signal is lost. Do not use any type of crossover network—there is loss in all of them. Use a field-strength meter to check the signal at the set. In case of poor reception, the meter will isolate the trouble either in the set or the antenna installation.

As with everything else, there are tricks that can be done with u.h.f. To remove a small trace of snow, it is often quicker and cheaper to stick another bowtie or other type u.h.f. antenna on the mast than to fool around trying to locate the trouble. The second antenna (Fig. 4) can be connected to the present one, even to a v.h.f. antenna, with a piece of lead-in whose length is a quarterwave of the lowest channel v.h.f. station being received.

Many sets have separate u.h.f. and v.h.f. antenna inputs. In strong signal areas both these inputs may be connected to a single antenna by installing the lead-in on the v.h.f. posts and connecting it to the u.h.f. input with a piece of lead-in whose length is a quarterwave of the lowest channel v.h.f. station to be received (Fig. 5). Sometimes this may have to be changed to the weakest v.h.f. station.

The v.h.f. input is a high impedance to the u.h.f. signal and will affect it very little. The low impedance of the u.h.f. input at the end of the quarterwave stub does not affect the v.h.f. signal. In fact, in some cases, it actually improves it as does a quarterwave stub. This should not be done in fringe areas, and the direct connecting of antennas and input posts very often introduces ghosts. In such cases, run separate lines and use a mechanical switch. END

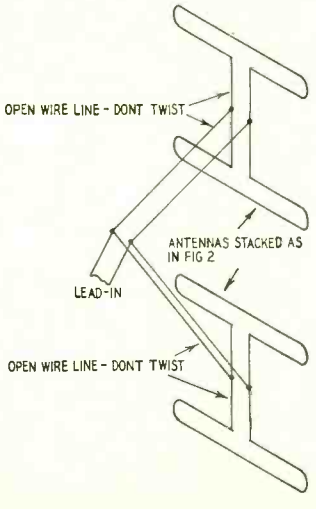


Fig. 3—Connecting stacked antennas.

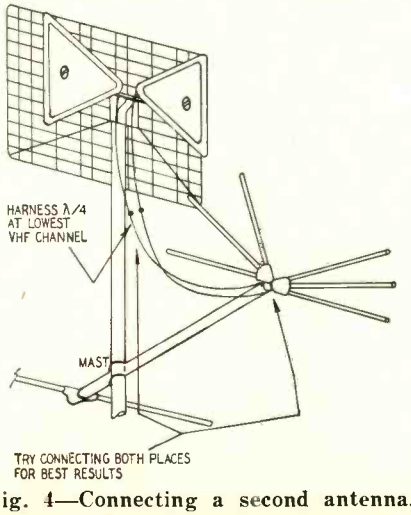


Fig. 4—Connecting a second antenna.

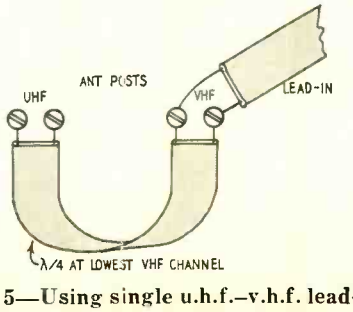


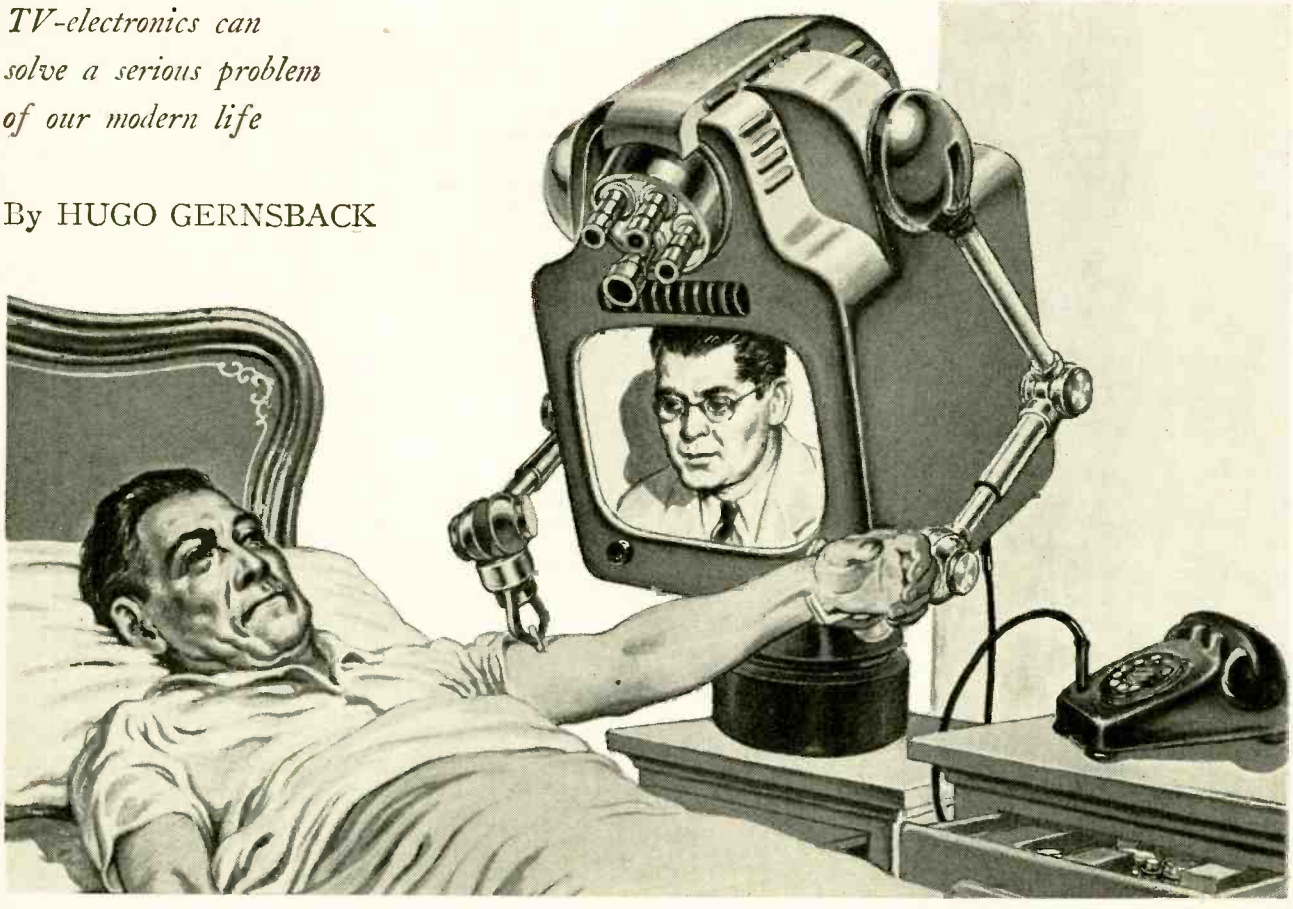
Fig. 5—Using single u.h.f.–v.h.f. lead-in.

TELEVISION

the teledoctor

TV-electronics can solve a serious problem of our modern life

By HUGO GERNSBACK



PROJECTION of the senses over a distance began early in the animal world. The cries uttered by alarmed prehistoric reptiles, saurians or birds were transmitted over a distance to warn others. A highly developed and sensitized olfactory sense brought the smell of an enemy creature to the nostrils of early mammals who could then flee promptly, thus avoiding destruction. The sense of sight, too, became sharply developed in many animals and especially birds which could then observe potential enemies—or their own prey—often from a point many miles away.

Modern man, with new scientific techniques, has greatly improved the projection of some of his senses, not only over a few, but over hundreds and thousands of miles. By telephone, we can hear and speak to distant friends around the world. Via television, we can see across continents.

As I have pointed out in earlier articles, it will be possible in the future to smell and taste half-way around the globe—and further.* But science does not stop with this. There is the far more important conception of *the projection of the self at a distance*. This means nothing less than the possibility now dawning for *man to be in two places at the same time*.

I will give here but one example of this revolutionary concept, which, incidentally, is NOT in the future—it can be realized today, with the technical means available *now*.

The average medical doctor today is overworked and short-lived. There are never enough doctors anywhere for the world's constantly multiplying population. Many patients die because the doctor cannot reach them in time, particularly at night and in remote or isolated regions.

Furthermore, the doctor wastes a terrific amount of time visiting patients in person—he can see only a few during a day. With increasing traffic congestion, many doctors refuse to make personal calls—except in emergencies. Even then they arrive often too late. Much of this dilemma will be archaic in the near future, thanks to the *Teledoctor*.†

I imagine this innovation as follows: Incorporated as an integral part into a combination television camera and receiver is a set of *mechanical hands*. The latter are now routinely manufactured by General Electric and other manufacturers. These incredibly sensitive hands are primarily used in atomic plants where scientists handle dangerous, "hot" atomic substances from a distance, without personally exposing themselves to danger. With these *telehands*, the scientist can do almost anything at a distance—writing, weighing, pouring liquids, unscrewing covers of "hot" containers—yes, even diapering a baby, miles away, including putting on the safety pins. *The sense of touch has been projected over a distance!* The action, of course, is watched via television.

*See "Telebiovision." *Forecast 1952*, page 22.

†See also article on the same subject: "The Radio Teledactyl" by H. Gernsback, *Science & Invention* magazine, February, 1925, page 978.

The teledoctor of the near future now becomes an actual projection of the doctor. In front of his television transmitter-receiver is a panel with a number of instruments which indicate blood pressure, pulse, respiration and other data routinely required in most examinations of patients.

Now let us see how you, the patient of tomorrow, "visit" your doctor, 15 miles away. Suppose you come down with a fever. You or your wife make a call to the local druggist, who is the agent for the teledoctor corporation which stocks the special TV transmitter-receiver equipped with its telehands.

These instruments are never sold, only rented to the sick, say for $3.50 a day. They are used only for closed-circuit work. The rubber-wheeled mechanism is delivered quickly to your home and rolled in front of the bed. Located in the drawer of the cabinet, right under the TV set, you will find a thermometer, blood-pressure appliance, sterile bandages, prescription blanks, fever chart (with instructions), tongue depressors, adhesive tapes and other items routinely found in every doctor's black bag. A cord with a telephone plug attached to the teledoctor instrument is now plugged into a special jack on your telephone. Future telephones will be provided with this facility. The TV signals and telehand electronic signals, etc., will all travel over the closed circuit telephone lines.§

Next you dial your physician's telephone number. He or his nurse takes the call. You give your name and state that your teledoctor instrument is plugged in and ready. The doctor now plugs his own set into the telephone and in a few seconds two-way communication is established. The doctor by electronic telecontrol moves *your* instrument into the best position, raising or lowering your set, which has a swivel mechanism for that purpose.

The *color* camera is now trained on you and the doctor looks you over. He listens to your heart—not with a stethoscope, *but with the back of his right telehand.* This has a sensitive microphone which the doctor places over your heart. He hears your heartbeat, now strongly amplified, over his loudspeaker.

He next takes your blood pressure, looks into your throat or examines any part of you. If he wants to inject you with penicillin or other medication, he will ask you to place a prescription blank into a holder arranged for this purpose. He picks up a special pencil from the drawer and writes out a prescription, then signs it. You are to get this from your drugstore as soon as feasible. When you have received it, you call the doctor once more. He places the special injection cartridge, *now on the market* called *Busher,* into his telehand and presses it against your skin. By spring action, the medication is shot into the arm quickly.

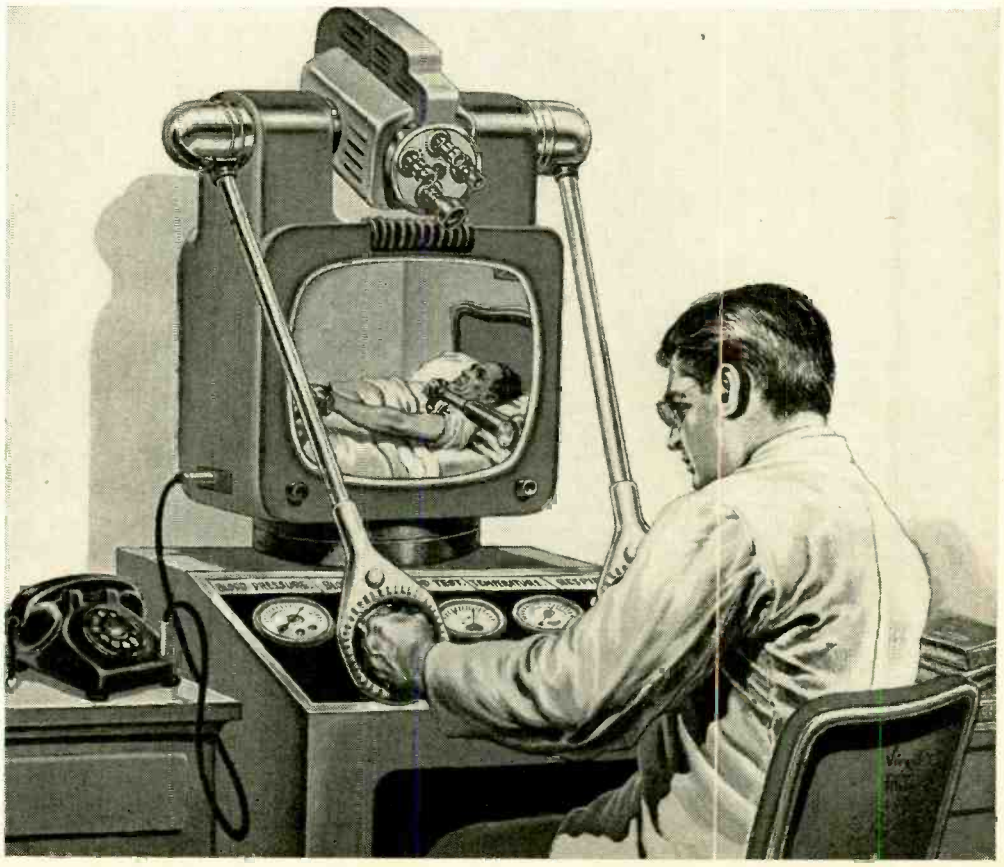
The doctor then gives you whatever other instructions are required and promises to "visit" you again early in the evening. When you are well again, phone your druggist who will call for the teledoctor instrument.

It should be noted that, short of a serious operation, the doctor of the future will be able to do almost anything by teledoctoring that he can do in person. He can remove your bandages after an operation, bandage you, remove stitches post-operationally, swab wounds, all at a distance.

In the more distant future, he will even be able to perform emergency long-distance operations, provided a nurse or nurses can be secured to assist him.

Soon, your doctor will be able to see far more patients with infinitely greater efficiency. He will not only save untold lives, and generate better health for his patients, but his own life will be made far easier and he will himself live longer and so serve suffering humanity far better than was ever possible before. END

§*Technical note.* At the present state of the art, it is not possible to transmit a 525-line TV signal over existing telephone lines. A good picture of 250–350 lines, however, can be phone-transmitted today. Such a picture would give sufficient definition for the proper operation of the teledoctor.



Patient and distant doctor are connected by telephone and closed circuit TV as illustrated on this and facing page. Doctor can treat ten times as many patients via teledoctoring as in person.

TELEVISION broadcasting stations transmit a series of synchronizing pulses together with the video information to control the receivers' scanning generators and form an intelligible image. In the receiver these timing pulses are removed from the composite video signal and used to synchronize vertical and horizontal sweep generators with those of the broadcast station. Appropriately, the circuit that performs this function is called the sync separator.

The sync separator does not separate the horizontal and vertical pulses from each other—this is done by integrating and differentiating networks. The prime function of the sync separator is to separate—as thoroughly as possible—the sync pulses from the video signal.

The separation process begins with the feeding of a portion of the composite video signal, taken from any point between the video detector output and the grid or cathode of the picture tube, into a "clipper" circuit. Since it is generally advantageous to work with as large a signal as possible, it is common to find the plate circuit of the final video amplifier as the point of "sync takeoff." In addition, the video amplifier increases the signal-to-noise ratio.

With the sync pulses transmitted at a constant amplitude and occupying the upper 25% of the composite video signal—the blacker-than-black region—they can be easily removed by amplitude discrimination. For maximum sync strength it would be ideal if the clipping were done exactly at the 75% level. But for practicality clipping usually takes place at a slightly higher level to avoid the possibility of components changing in value and lowering the clipping level, allowing portions of the video to pass through the separator and hamper proper synchronization.

There are several methods of separating the synchronizing pulses from the picture, however the principle is always the same. The circuit is biased so that no plate current will flow until the signal exceeds its blanking level. Usually the clipper stage develops a

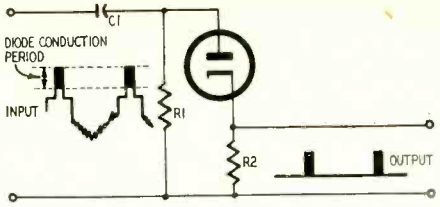


Fig. 1—A simple diode sync clipper.

negative bias and the signal applied to the circuit is of such polarity that the sync pulses represent the most positive portion of the signal, hence current will flow only during the sync pulses. Since the picture information is below the blanking level, it will not appear in the clipper output signal. The clipper can be a diode, triode or pentode type.

Diode clipper

Fig. 1 is a diode clipper, with C1-R1 forming a grid-leak type network. Their values are such as to maintain a high negative bias voltage between plate and cathode. When the composite video signal is applied, the plate draws current and C1 charges to the peak value of the input signal. As the signal falls to a lower value, C1 discharges slowly through R1, creating the negative bias voltage. The bias voltage keeps the tube cut off until the signal becomes sufficiently positive to overcome it. This will occur only when the signal rises above the blanking level.

A weakness of the diode clipper is its inability to separate completely the sync pulses from the picture information. As a result it must usually be followed by one or more clipper-amplifiers and shaping circuits.

Since this circuit passes both vertical and horizontal sync pulses, a defect will usually produce both vertical and horizontal instability.

The first check of over-all sync instability should be replacement of the diode. Follow this by measuring R1. If R1 is open, no sync pulses will appear across R2 (an oscilloscope across R2 may show extremely small pulses). If R1 becomes very much less than its normal value, C1 discharges quickly to a lower than normal level between sync pulses. This lowers the bias voltage and allows a portion of the video signal to pass through along with the sync pulses, causing unstable synchronization. An oscilloscope across R2 under these circumstances will show considerable video information in the output signal.

If R1 increases in value, the negative bias developed will be larger and the sync output smaller. When this occurs, the horizontal and vertical hold controls will become very critical because the small sync pulses will not be able to "hold" the horizontal and vertical oscillators. Thus if R1 becomes too large, a scope across R2 will show smaller than normal pulses. An open, leaky or shorted C1 will prevent proper separation and cause poor sync stability.

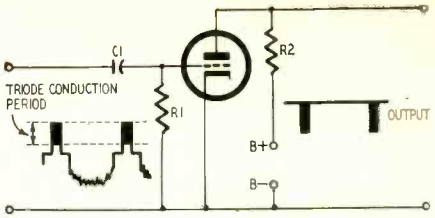


Fig. 2—A triode sync clipper amplifies and inverts polarity of signal.

Being the output load resistor, R2 open will prevent the passage of any sync signal. If under this condition a scope is placed across this resistor, a deceiving situation can arise—the internal resistance of the scope becomes R2 and may restore normal operation of the TV set. To prevent this, make this check with a 0.5-μf capacitor in series with one of the scope leads.

Should R2 decrease in value, the sync output will also be decreased. If it increases appreciably (more than 10%) in value, C1 will not charge to its proper value. This lowers the bias voltage and permits video signals to pass through. In addition, the sync pulses in the output will be larger than normal, causing the picture to tear on strong signals.

Triode clipper

Fig. 2 is typical of a triode circuit used for sync separation. Since a triode can perform the same function as a diode while having the additional advantage of amplification, it has proven a more popular circuit.

The plate voltage in this circuit is usually extremely low (15 to 40 volts), permitting plate current to be cut off with very little grid bias. See Fig. 3. This circuit is very similar to that of Fig. 1, with the grid and cathode performing the same function as the plate and cathode of Fig. 1. When the grid becomes positive, C1 charges to the peak value of the input signal. The time constant R1-C1 is again very long compared to the time between sync pulses. As a result, very little of the charge on C1 will leak off before another pulse arrives to recharge it to its peak value. This establishes a steady bias on the tube so that only about the upper 20% of the input signal will be passed (leaving a 5% safety margin and preventing the black signals from riding through). Since the plate voltage on the tube is so very low, plate current will be cut off shortly after the input signal falls below the peak value of the sync pulses.

With only the tips of the sync pulses drawing grid current, the pulses in the plate circuit are clamped to the same level. Thus, in effect, we have d.c. restoration. This circuit can operate only with the sync pulses representing the most positive portion of the input signal.

The triode has the advantage of greater output than the diode clipper. Still higher output can be had with a pentode. The trend in modern receivers is toward pentodes because they pro-

vide a fairly constant output despite sizable variations in the input signal. In addition, the pentode with its lower grid-to-plate capacitance permits very little video information to be capacitively coupled through it.

As with the diode, initial servicing of sync instability should begin with replacement of the triode, usually a sharp-cutoff tube. Any defect in the R1-C1 grid-bias network that reduces its time constant will reduce the bias voltage, permitting video information to pass through the separator and cause premature triggering of the sweep circuits. Any defect that increases the time constant will cause an excessive bias to be developed. This will permit only the extreme tips of the sync pulses to be amplified, reducing the output across R2.

The problem of an increase or decrease in the value of R2 is the same as in the diode load of Fig. 1. However, in addition, there is the problem of varying plate voltage (d.c.). If R2 decreases in value, permitting an increase in plate voltage, the tube's grid bias may be insufficient to prevent the amplification of the dark portions of the video signal. Video-signals will appear across R2, ruining synchronization. If R2 increases in value, the plate voltage will be too low and the output signal extremely weak. Should there be any voltage dropping resistor between R2 and the B plus supply, be sure that it is properly decoupled. Poor decoupling will cause a fluctuating d.c. potential on the plate, resulting in output pulses of varying amplitude and poor synchronization.

The output of a clipper circuit is usually not large enough to feed the oscillator and a.f.c. circuits properly. A larger output can be obtained by following the sync separator with a stage of sync amplification. The sync amplifier often acts as a limiter to provide pulses of constant amplitude.

In some chassis, such as the Admiral 23E1Z, the sync separator is followed by a clipper circuit. The negative sync pulses in the output of the separator drive the clipper into cutoff, producing splendid amplitude limiting action.

Common sync troubles

Defective capacitors are a major source of trouble in the sync circuits. Slight leakage is often enough to change operating voltages and upset sync stability. With tubes in the sync circuits operating over so narrow a portion of their characteristic curve, even the slightest tube defect or change in the shape of the characteristic can cause unstable sync. Tube troubles can consist of faulty cathode emission or changes in the interelectrode capacitances. Thus tubes in this circuit should be checked by direct replacement only.

The horizontal pulse frequency is 262.5 times the vertical pulse frequency. As a result, defective coupling capacitors may not pass the low-frequency vertical pulses while offering little reactance to horizontal pulses. This will often divert suspicion from a faulty sync separator because the horizontal sweep system will operate perfectly.

We have said very little concerning the amplitude of the sync pulses because the peak-to-peak voltages vary greatly with different receivers. These voltages should be carefully compared with those given on manufacturers' schematics. Often this is the quickest method of determining whether the sync separator is operating properly.

Increase in high voltage

I recently got a TV set that absolutely defies identification. It appears to have been built in kit form and bears no code or chassis numbers. Even the major components are unmarked. Needless to say, I do not have a schematic for this set. The complaint is insufficient brightness. I checked it as best I could and the only trouble seems to be insufficient high voltage. The sound is perfect. When I substitute high voltage from another chassis, the picture has good linearity and contrast. The voltage I substituted is about 1,000 more than the set has at present. Rather than replace the flyback transformer which might require still other changes, I would like to know if there is any way of increasing the present high voltage the additional 1,000 volts without any major changes.—M. P. R., Trenton, N. J.

There are several ways to obtain the voltage increase you desire, but should they prove insufficient in your set, replacement of the flyback transformer with a "universal" type is not difficult since these units have taps to match a wide range of deflection yokes.

Try moving the low side of the high-voltage filter capacitor—usually connected to ground—to the plate of the damper tube. In an autotransformer type circuit the connection will usually be to the cathode of the damper. Increase the voltage on the screen grid of the horizontal output tube by decreasing the value of the screen dropping resistor. If the high voltage is still below what is needed, try reducing the bias slightly on the output tube and increasing the grid drive. In making these changes keep your eye on the cathode current and screen-grid power input. See that they do not exceed the recommended ranges for the output tube used.

Weak horizontal sync

In a G-E model 21T27 receiver the horizontal synchronization has been getting steadily worse. Until recently the sync was weak but adjustment of the horizontal hold control brought the picture back in. Now the slightest line fluctuation or even switch in cameras throws the horizontal sync out and it takes careful adjustment to restore it. At some times it gets so bad that synchronization cannot be obtained despite complete rotation of the hold control.

The vertical sync is very steady and has never required adjustment. The picture is good and the sound seems normal. Needless to say, I have tried every possible adjustment including alignment of the entire receiver. With the vertical sync steady I have concentrated on checking the horizontal circuit.—A. H., Alameda, Calif.

Measure the amplitude of the sync input to the phase detector tube (Fig. 4). A peak-to-peak reading of approximately 63 volts should be expected. If you read appreciably less, trouble-shoot the phase splitter to find the cause of the low output. Only when the proper sync input is obtained and the trouble still exists, should you go on.

Replace the 12AU7 phase detector. Check multivibrator components C260, R263 and R266. Check the waveform feedback components R279, R278, C256 and C270. Measure the resistance of the horizontal stabilizer coil, L251. It should read approximately 67 ohms. Another strong possibility is an open C259 or R260. END

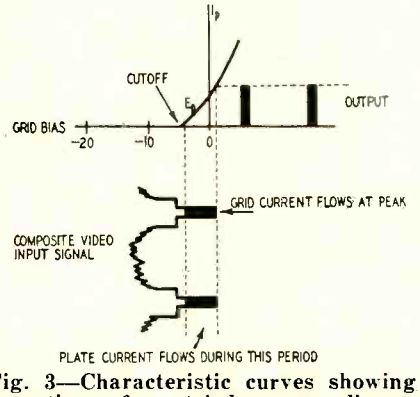


Fig. 3—Characteristic curves showing operation of a triode sync clipper.

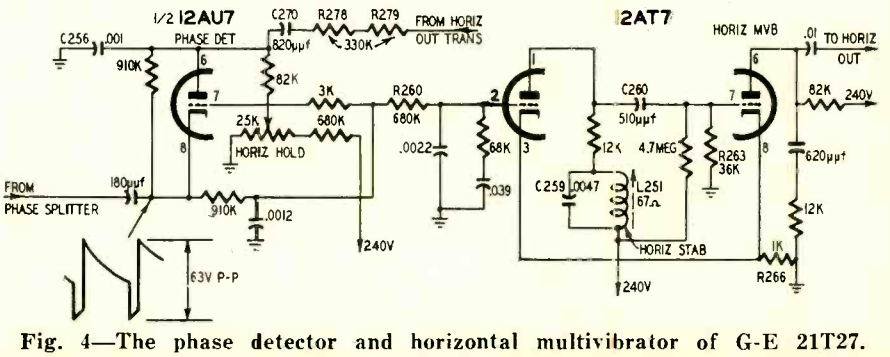
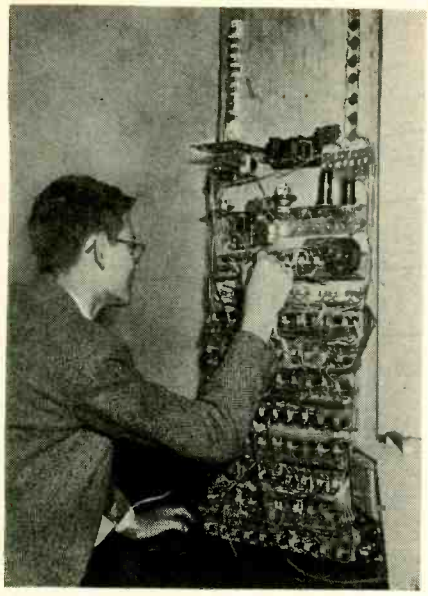


Fig. 4—The phase detector and horizontal multivibrator of G-E 21T27.



The author working on the 120-relay computer referred to in this article.

How a Computer Works

These simple basic circuits make it easier to understand how the more complex instruments operate

By DAVID B. MUMFORD

THIS is the story of a miniature relay computer designed and built by the author. It is the last in a series of progressively more complex computers starting from one containing 20 relays and ending with 120. Up to 1,500 feet of wire as well as a mechanical tape reader of our own design went into the largest model.

First, I shall describe the original computer in the series used as one section of the last and most powerful one. It performed the single operation of addition. It required you to give it numbers in binary notation (see box) and gave its answers likewise in binary. Since only two symbols are used in binary, 0 and 1, this system adapts itself readily to 2-position switches or relays, each position corresponding to a symbol. Furthermore, this system has a very simple addition table.

Next I will show how the original circuit can be modified to economize relays—a necessity when numbers of several digits are to be added. No constructional data on the 120-relay machine will be given—the diagram is too large and complex to print in a magazine article. What will be described is exactly how a simple circuit works and how it can be built into progressively more complicated circuits to handle bigger numbers, with a quick view of the final computer.

This—it is hoped—will interest the technician who would like to know how these circuits work but does not want to build one. It will also be helpful to the would-be computer constructor, who can use the information (and will need a great deal of additional study) to build a sizable machine of his own.

A simple adding circuit

Consider first the problem of adding 1-digit numbers or the first (smallest or right-hand) digit of larger numbers. The addition table page gives us the answers for the four input combinations: 0 + 0, 1 + 0, 0 + 1, 1 + 1. The circuit of Fig. 1 gives the correct answers when traced: 0, 1, 1, 0 + carry 1 to next digit. If either the first or second numbers are 1, the sum 1 appears (top lamp lights). If both are 1, the result is a 2-digit number 10. The top lamp goes out indicating zero and bottom one lights, indicating a carry to the second digit, and giving the sum, 10 (2 in decimal notation).

To add larger numbers, these elementary circuits are combined. To add 2-digit numbers, for instance, an identical circuit adds the second digits of the numbers and a third circuit adds the carry from the first digit to this result. The sums from the first and the second digits form the first and second digits of the sum, respectively, while the carry from the second digit forms the third digit of the sum. Rectifiers are added between circuits to prevent improper interaction. A 3-unit circuit is shown in Fig. 2.

Suppose the two figures 11 and 11 (3 and 3 in decimal notation) are to be added. The first digit (the unit, or smaller number) is entered at input A of unit I. The lower contact of relay Z1 is closed, lighting lamp 1. The second digit, entered at input 1, is entered at input A of unit II (the 2's unit). It closes the lower contact of relay Y1 and lights lamp 2 through the lower contact of X1.

The second 11 is entered at input 2. Its first digit goes to input B of unit I, drawing down both armatures of relay Z2. Since the armature of Z1 is down, drawing down Z2's upper armature has no effect; but the lower armature is drawn away from its upper contact, and

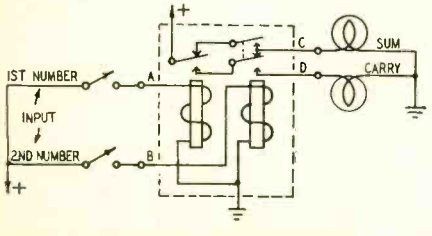


Fig. 1—The simplest addition circuit.

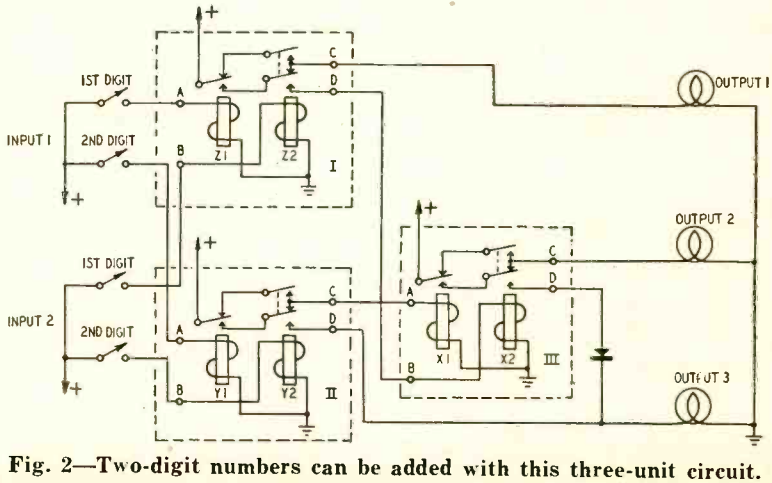


Fig. 2—Two-digit numbers can be added with this three-unit circuit.

lamp 1 goes out. Current flows through output D and through relay X2. Both armatures of X2 are drawn down, and lamp 2 extinguished as the lower armature of X2 is disconnected from C and connected to D. Lamp 3 lights.

The second digit enters at B of unit II, drawing down both armatures of Y2. The lower armature breaks the contact through output C, releasing the armature of X1. This permits current to flow through the C output of unit 3, again lighting lamp 2. The sum is then 110.

The reader may find it easier to follow the problem by drawing Fig. 2 on tracing paper, then drawing and erasing the armatures to indicate the correct positions as each digit is entered.

Techniques of design

Although these circuits are comparitively easy to trace, to verify that they give the correct answer, you may wonder how they are designed. Unfortunately there is no simple answer. Trial and error are useful in many cases and familiarize one with the results of simple combinations. Some authors attempt to systematize these basic circuits as well as some others for common uses[1] while others feel that the technique of Boolean algebra solves many problems.[2] However, some simplifications and original circuits are very difficult to discover by either of these methods, leaving the success of the final circuit to the ingenuity and inspiration of the designer.

The development and modification of the circuit given above to add larger binary numbers are a good example of the evolution of a relay circuit. In its original form, it employs two relays for the first digit and four more for each successive digit. Ultimately we can reduce it to only two relays for each digit. The first simplification is to eliminate the first relay of the second block in each digit (unit III in Fig. 2, for example). But the function of that relay was to keep one circuit closed when there *was* power on the lead A which closes it, and another when there *was not* power. Therefore, if we eliminate the relay, it becomes necessary to have a second lead (A′ in Fig. 3) which has power when and only when A has no power. These two leads will take the place of the wires coming from the contacts of the eliminated relay. The result may be verified by tracing as with Fig. 2.

A second simplification eliminates the second relay of the second block in each digit. However, the carry from the digit before closes this relay. So just as we needed the A′ lead above, we now need a second lead from the preceding digit which will supply power when and only when there is *no* carry. Therefore, we must also add a circuit to provide this so-called no-carry lead for the next digit. When the contacts of the resulting circuit are combined, the result may be seen in Fig. 4, which is best verified by tracing.

Programmed computers

If all large computers had to be designed with this type of direct circuit, giving you the answer with no further instruction from the operator, their power would be strictly limited by the ingenuity of the designer and the number of operations he could build into a circuit. Large computers use a second type of circuit, called "sequential"[3] because they accomplish their result in a series of steps, as opposed to the "combinational" circuits described above. In these circuits, a simple computer of the combinational type is retained to perform each of the steps, which consist of simple operations.

Memories must be added to store intermediate results between operations. A common set of wires called a "bus," connected to each memory and to the input and output of the computing unit within the enlarged calculator, transfers numbers within the whole framework of the computer.

To control this transfer of numbers as well as the operation being performed by the computing unit, a continuous set of instructions called "programming" is fed the computer through the control unit. The actual numbers to be operated with are given to the computer separately, so that this programming will be fixed for a particular sequence of operations—such as involved in solving a quadratic equation, for example.

The 120-relay equipment

It was on this plan that the main computer illustrated in the photograph was designed. Six-digit binary numbers were taken as the base in which all computations were performed: the memories stored six-digit numbers, the bus carried six-digit numbers, the computing unit operated on six-digit numbers. Rather than breaking the working of the machine down into steps of one operation each, it was further broken into cycles. In each cycle, a number may be taken from one section (e.g. memory, input, output, computing unit or instructions) of the computer and put in another. Thus a step would consist of several cycles which would: 1, put the numbers to be operated on in the computing unit; 2, put the code for the correct operation to be performed in the

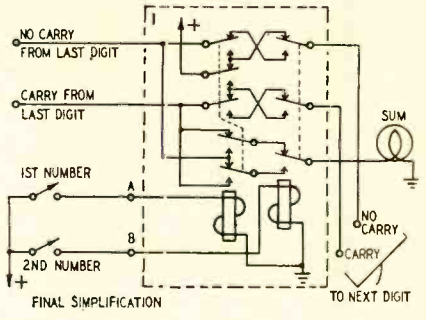


Fig. 4—Another relay is eliminated.

computing unit from the instructions; 3, take the answer from the computing unit to a memory. The actual computation within the unit is performed automatically once the numbers are at hand. A rough block diagram is given in Fig. 5.

Paper tape was used for the programming, giving the necessary instructions for each cycle in three entries. The first entry determines the section of the computer which is to receive the number. The second determines the section containing the number to be sent and actually connects these through the bus, thus transferring the number. The last entry is provided in case the number to be sent is not in the computer, in which case it will be automatically sent if put on the instructions in this entry. Actually there is another means of putting a new number in the computer: if it is stopped in the middle of the cycle by a special code, a number may be manually connected to the bus with switches as in the simple unit described in Fig. 1.

Memory circuits

The memory (Fig. 6) is the simplest of the individual units within the computer and illustrates the principles for transferring numbers. The actual process of remembering is accomplished by what is called a "holding" circuit. When the relay is temporarily closed by voltage from the bus, a path from the relay

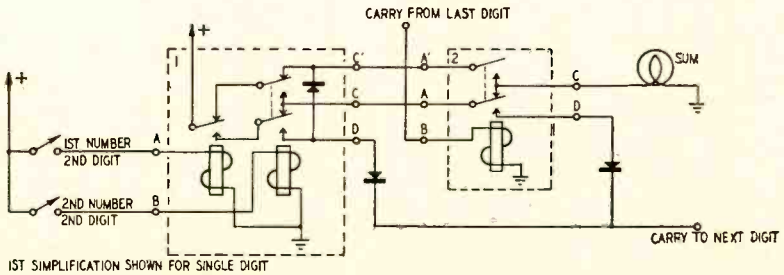


Fig. 3—This simplification eliminates one relay in the second block.

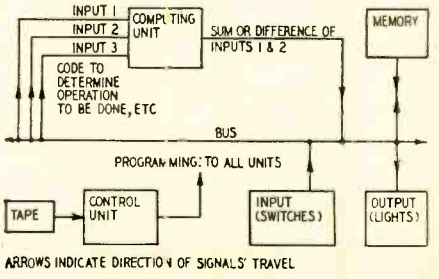


Fig. 5—An elementary block diagram of a programmed type of computor.

coil through the relay contacts to the voltage source is completed, thus permanently connecting the relay coil to the voltage unless this path should be broken elsewhere. This path—called a hold lead—controls the operation of the memory. When it has voltage on it, the relays remember; when it does not, they forget. In a single memory (that is, for six relays in the computer illustrated), the hold leads are generally connected together and are disconnected only when another number is to be put in the memory. A single relay is used in this computer to connect the relays of a memory to the corresponding wires of the bus, both for sending and receiving a number.

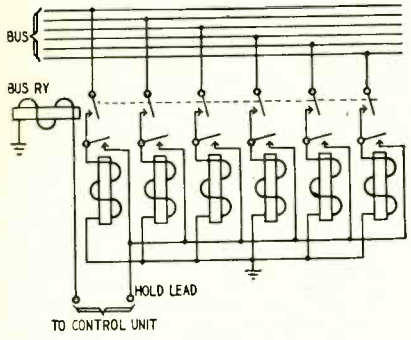


Fig. 6—Circuit of relay memory.

The computing unit is very similar to the simple combinational computer discussed above. Two sets of relays working as memories replace switches for storing input numbers. Lights on the output are replaced by a relay connecting the answer wires directly to the bus. This computing unit will perform three operations instead of one: addition, subtraction and selection. The purpose of the selection circuit is to select one of two numbers, depending on whether a third is 0 or 1. This is an important function in larger computers.

We have studied in this article the detail design of one type of circuit—the addition circuit—and some of the general principles that apply to the design of larger calculators. Some of these same ideas can be applied, moreover, to the construction of checker playing machines, mechanical turtles, automatic oil refineries, and immense telephone exchanges. Below is a short bibliography for those of our readers who would like to delve farther into this far-reaching field: END

BINARY NOTATION

This system writes numbers to the base 2 rather than 10. It uses two symbols (0 and 1) rather than 10 symbols (0, 1, 2, 3, 4, 5, 6, 7, 8, 9). Thus a number expressed in decimals as:

$$45 = 4 \times 10^1 + 5 \times 10^0$$

is expressed in binary as:

$$101101 = 1 \times 2^5 + 0 \times 2^4 + 1 \times 2^3 + 1 \times 2^2 + 0 \times 2^1 + 1 \times 2^0$$

In both cases, the number is made up from the coefficients of the terms. Similarly

1, 2, 3, 4, 5, 6, 7, 8, 9, 10 . . .

is expressed in binary as:

1, 10, 11, 100, 101, 110, 111, 1000, 1001, 1010, . . .

Rather than a complicated addition table, in binary we have:

$$0 + 0 = 0$$
$$0 + 1 = 1$$
$$1 + 0 = 1$$
$$1 + 1 = 10$$

(or 0 with a carry of 1 to next digit) A larger addition is carried out just as in decimal notation: The first and smallest digits are added first, then the second digits plus the carry from the first, etc. For example:

$$101 = 5$$
$$111 = 7$$
$$1100 = 12$$

References

[1]Keister, Alistair and Washburn, *The Design of Switching Circuits*, New York: D. Van Nostrand Co.

[2]Berkeley, RADIO-ELECTRONICS, October, 1950, through October, 1951; also December, 1951, and February, 1952.

[3]*Scientific American*, Automatic Control issue, September, 1952.

NOVEL HIGH-VOLTAGE SUPPLY

MANY instruments for detecting and measuring nuclear radiation require high-voltage low-current power supplies to provide a polarizing voltage for the ion chambers or G-M tubes. This voltage is usually obtained from miniature high-voltage batteries used directly or in combination with capacitors charged in parallel and discharged in series, from an r.f. type supply using a high-frequency oscillator and rectifier, or from a vibrator supply. (For details on these types of high-voltage supplies, see "Counters for Prospectors" in the October, 1949, issue.)

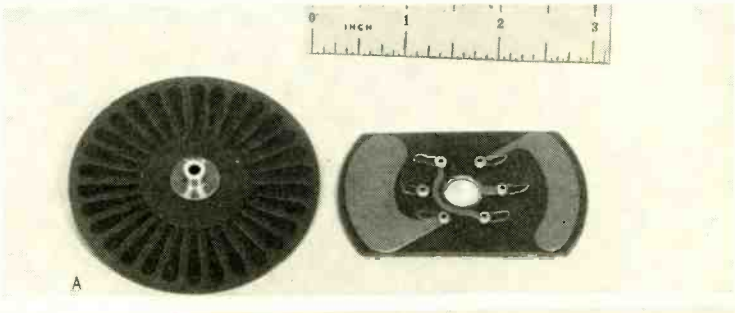
A new miniature electrostatic type high-voltage low-current supply has been developed by S. R. Gilford, S. Saito, and J. L. Herson of the National Bureau of Standards. This generator is simpler to construct, is potentially less expensive, has fewer components, and does not require special batteries that may be hard to obtain.

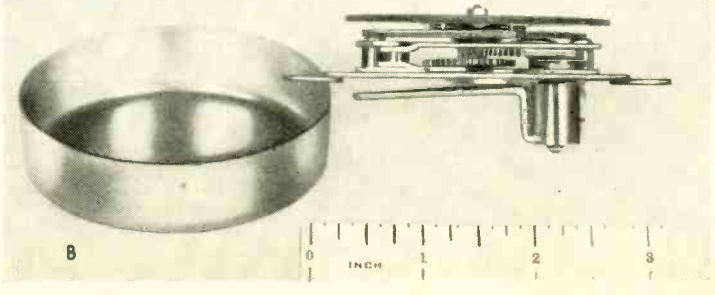
The electrostatic supply consists basically of a stator of two field plate conductors and a rotor with a number of of pairs of conducting sectors. (See photo A. The rotor is on the left and the stator on the right. These parts are fabricated by printed-circuit techniques using copper foil laminated phenolic etched to produce the desired patterns.)

The rotor is driven at speeds up to 6,000 r.p.m. by a lever-operated reciprocating drive system. Several sets of brushes transfer the electrical charge to the storage capacitors. The NBS generator with its reciprocating drive system is shown in photo B.

The problem of establishing a constant output polarity was solved by using a small external bias voltage to precharge the storage capacitor. This voltage is obtained from a supply used with the electronic equipment.

The NBS electrostatic generator can charge an .02-μf capacitor to 2,000 volts in about 15 seconds. In a survey instrument requiring a current of 10^{-12} to 10^{-14} amperes, the storage capacitor needs to be recharged only occasionally to make up for a leakage loss of about 100 volts. This charge can be restored with a single operation of the instrument's driving lever. END

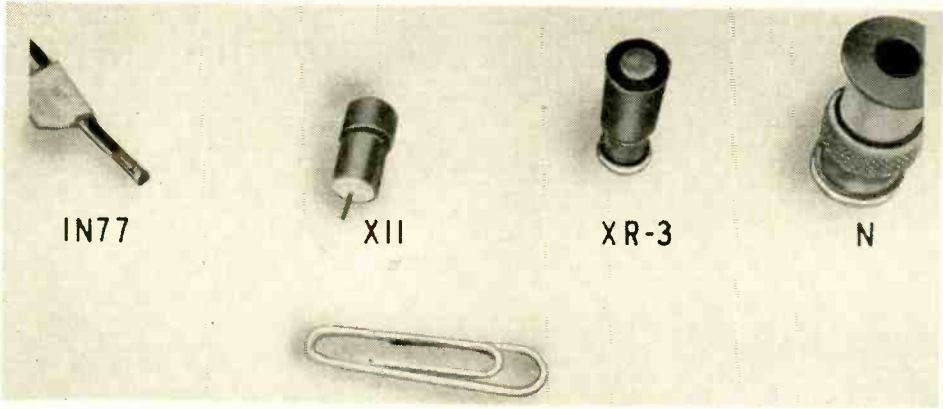




Phototransistors and Photoelectrets

Interesting developments in solid-state materials

By EDWARD D. PADGETT



Left, smallest photodiode commercially available. Photo also shows experimental "wide-area junction photocells."

THE phototransistor and photoelectret are electronic devices of unusual interest. Due to a saturation characteristic, they are useful as electronic switches which can be triggered on and off by a light beam. Other potential uses are as the light-sensitive element in photoelectric recording equipment, talk switches in communications equipment, pulse generators and TV projection apparatus, and, in many cases, as auxiliary elements for phototubes in computers and industrial electronic equipment.

Phototransistors (RADIO-ELECTRONICS, November, 1954, page 96) are photocells of semiconducting materials of relatively *low resistivity*. Although much information is available about phototransistors, very little is known about the photoelectret. According to the literature, a photoelectret is a dielectric material of relatively *high resistivity* that can be polarized by light. For reference, the resistivities of various semiconductors and dielectrics are shown in the table. Photoelectrets will be discussed later.

The phototransistor

It is very easy to change the electronic nature of semiconductors. A phototransistor works as it does because light energy, absorbed by the semiconductor, changes the conductivity of the material. Phototransistors are said to be photoconductive. The importance of this photoconductive effect is shown in Fig. 1. When a light beam is absorbed by a crystal, the energy in the beam is spent in raising electrons from an *almost filled* to an *almost empty* energy band. In other words, the absorption of light produces free electrons and positive holes in the semiconductor. The liberation and movement of these charges cause the photocurrent of a phototransistor. Electrons ejected from the surface of the crystal by the light beam do not contribute to the photocurrent.

A simplified sketch of a phototransistor is shown in Fig. 2. The collector is a catswhisker of 10-mil phosphor bronze wire, pressed against a thin germanium pellet about .005 inch thick. The incoming light energy injects holes into the semiconductor. The collector is biased negatively so that the positive holes will flow in the right direction. The photocurrent is read with a 1-ma meter. When no light falls on the germanium, the meter will read a small "dark current," due to the normal conductivity of the material. Germanium pellets from burned out or obsolete transistors can be recovered and used to make experimental photocells.

However, phototransistors are available commercially. Most of them use doped germanium as the semiconductor. The devices are called phototransistors, germanium photocells or germanium photodiodes by their manufacturers. In the *point-contact* type, the photosensitive pellet and pointed collector electrode are mounted in a coaxial housing (or imbedded in a plastic cylinder) of very small size. The *junction* type is also called the "wide-area junction

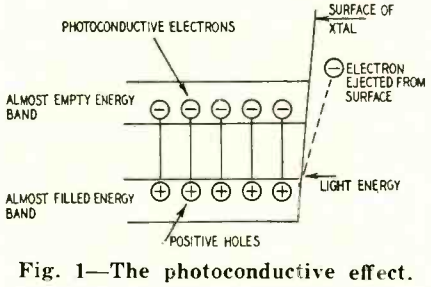


Fig. 1—The photoconductive effect.

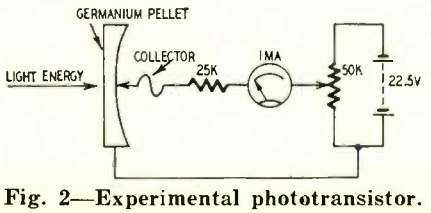


Fig. 2—Experimental phototransistor.

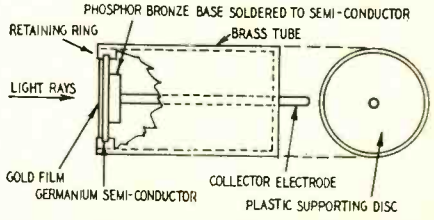
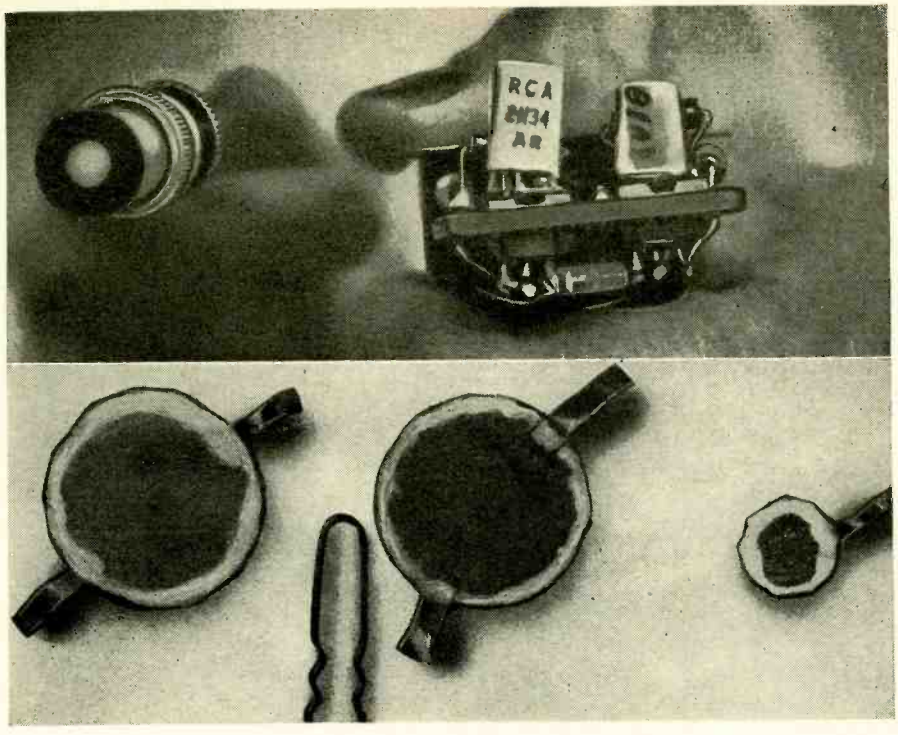


Fig. 3—Diagram of the coaxial gold-on-germanium junction photocell.



Junction transistor amplifier — unit is used with junction photocells.

Typical experimental photoelectrets.

photocell" or the "gold-on-germanium junction photocell." It consists of a thin circular piece of semiconductor (about 0.25 to 0.5 inch in diameter), mounted in the end of a brass tube (see Fig. 3). A thin film of gold is evaporated onto the large surface of the germanium. The gold diffuses into the semiconductor and forms a p-n junction. An important advantage of this design is that it gives the cell a photovoltaic property. That is, the light energy that strikes the junction is converted into a voltage (about 20 to 40 millivolts as measured between collector and brass case). It means that the gold-on-germanium junction photocell requires no biasing voltage or power supply for its operation. Because of its photovoltaic property, small size and good signal-to-noise ratio, the device can be mounted anyplace, the output signal amplified with a suitable amplifier, and used in photoelectric and industrial electronic applications.

Junction photocells are low-impedance devices. Their output impedance varies from about 500 to 1,000 ohms, depending on design. The input impedance of a grounded-emitter, junction transistor stage is about 600 ohms. For most practical purposes this slight impedance mismatch is not important. As a matter of fact, if the brass case is grounded, the collector of a junction photocell can be capacitance-coupled to the base of the transistor. Here the phototransistor is used as a current generator; the signal current is injected into the base of the junction transistor through a capacitor. The circuit diagram of a two-stage junction transistor amplifier suitable for such purposes is shown in Fig. 4. Best results will be obtained if the first stage is a high-alpha 2N34 unit. The 68,000- and 100,000-ohm resistors between collector and base provide bias and stabilization. R-C coupling is used throughout. Large paper capacitors are used since this is a low-frequency amplifier.

The collector resistors are shown as 50,000-ohm potentiometers to allow for optimum adjustment of the load of each transistor. A single 22.5-volt hearing-aid battery is an adequate power supply. The output of the last stage (either a 2N34 or a hermetically sealed 2N38 junction transistor) may be capacitance-coupled to a peak-reading v.t.v.m. or oscilloscope for analysis of the output signal. For convenience, the light source is shown as a 2-watt 120-volt lamp. The blades of a rotating electric fan, placed in front of the lamp, "chop" the light into pulses.

Since gold-on-germanium photocells require no external biasing voltage, a great amount of research is going on to determine if other semiconductors possess the photovoltaic property. Work on semiconducting intermetallic compounds at Battelle Memorial Institute is being sponsored by the Bradley Mining Co., San Francisco, Calif. At the April, 1953, meeting of the Electrochemical Society in New York City R. K. Willardson, A. C. Beers and A. E. Middleton of Battelle described the photoelectric properties of a semiconducting intermetallic known as antimony aluminum (other intermetallics, like antimony indium and antimony sulphur, possess semiconducting prop-

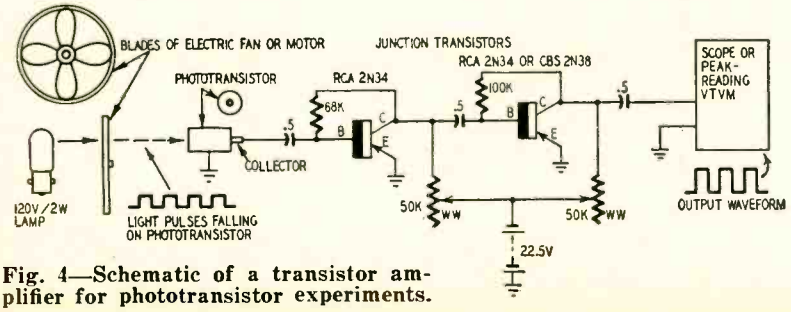


Fig. 4—Schematic of a transistor amplifier for phototransistor experiments.

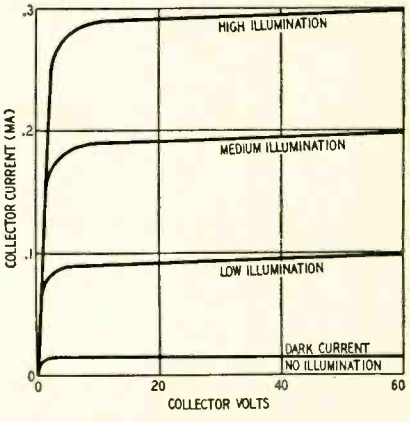


Fig. 5—The photoelectric properties of an intermetallic p-n junction.

erties). The photoelectric properties of an intermetallic p-n junction are shown in Fig. 5. The saturation characteristic is useful in various applications, as already mentioned. Hence, transistors and photocells made from semiconductors other than germanium and silicon should be available in the near future, especially so since the intermetallics are more economical than germanium or silicon.

The photoelectret

Our industrial economy is demanding the development of new or improved photoconducting materials. It is interesting to note that in spite of important progress in transistors and solid-state materials, no one has become interested in the ideas and experiments of G. Nadjakoff, a physicist at the University of Sofia. Nor has anyone tried to verify his experiments. According to Nadjakoff, a photoelectret consists of a dielectric material that can be "polarized" and "depolarized" by light energy.[1] His graphs and descriptions suggest that he uses the word *polarized*

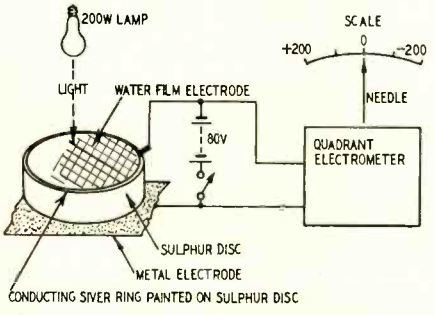


Fig. 6—Sulphur-disc photoelectret.

to mean "charged," and *depolarized* to mean "discharged." He does not use these words to describe the physical condition of some of the grain or boundary-oriented substances (such as antimony sulphur) that are being used in photoelectric experiments at the present time.

The Balkan scientist used pure sulphur as the dielectric material for his photoelectrets. The molten material (melting point about 114.5° C) was allowed to solidify in the form of small discs—approximately 1.7 millimeters thick and 10 square centimeters in area. As shown in Fig. 6, one surface of a sulphur disc was attached to a metal electrode. The electrode on the other surface consisted of a transparent film of water[2] and a conducting ring.

Nadjakoff applied 80 volts to the electrodes on the disc. The electric field strength through the disc would be 470 volts per centimeter. When the water-film electrode was illuminated with a 200-watt lamp, he noticed that a strong photocurrent was produced. This polarizing (or charging) current increased from a very small dark value to a maximum of between 200 and 250 units as read on the calibrated scale of an electrometer (a device for measuring the presence of electric charge). The sequence of events is summarized in Fig. 7, which shows the charge-discharge characteristics of a photoelectret.

Four minutes after the electric field was applied to the disc, the water film was illuminated with the electric lamp. The light energy triggered the photocurrent into its highest or saturation value. After reaching saturation, the current then decreased slowly with time. Eleven minutes later the lamp was turned off, leaving the electret in darkness, and the current dropped to its original low value. Then the electric field was removed from the electrodes and left off for the rest of the test. These events placed the photoelectret in its polarized state. After 19 minutes, the sulphur disc was illuminated again. A strong depolarizing (or discharge) current appeared, which was

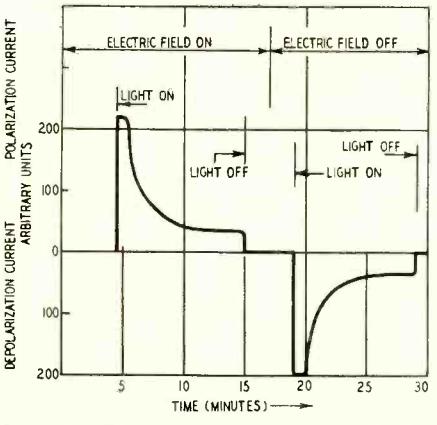


Fig. 7—Charge-discharge characteristic of the sulphur-disc photoelectret.

opposite in direction to the polarizing current. This current likewise reached a saturation value (between 200 and 250 units on the electrometer scale) and then decreased slowly with time. The light was turned off after 29 minutes and the current dropped to its original low value. This was the end of the depolarization.

Nadjakoff demonstrated that the polarization of his photoelectrets had a certain amount of permanence. The results are shown in Fig. 8. He plotted the photodepolarization current as a function of time immediately after photopolarization. After the data were taken, the disc was polarized again; the electric field was removed, the elec-

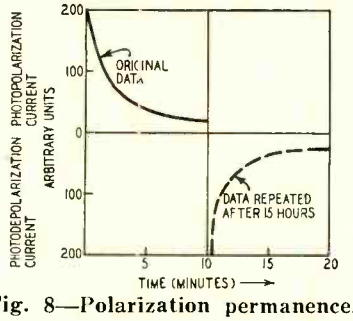


Fig. 8—Polarization permanence.

trodes were short-circuited and the disc was placed in darkness for 15 hours. Then the photodepolarization measurements were repeated. The data (dashes) so closely followed his original curve that he concluded that as long as the polarized dielectric was kept in darkness a condition of permanent polarization remained.

I have attempted to verify some of Nadjakoff's experiments. The results are summarized in the table. Since conductivity of monoclinic sulphur is about three times that of rhombic sulphur, it is believed that Nadjakoff made photoelectrets from it. (The ordinary wax type electret has no photoelectric properties.) If the radiation that falls on the photoelectret is too intense, the current does not return to its original value immediately (as shown in Fig. 7). In other words, this type of photoelectret can be oversaturated. The photodepolarization curve is complicated, difficult to interpret and to reproduce. Several authorities have suggested that Nadjakoff's original photodepolarization effect may have been due to boundary or semiconducting properties of the water-film electrode, rather than a property of the dielectric. If so, then Nadjakoff probably was the first man to make a phototransistor.

To investigate this situation further, photoelectrets were made from other substances and other film materials. Pieces of modified germanium, antimony sulphur and ceramic materials such as titanium and germanium oxide were used. Films of Aquadag (colloidal graphite), gold and indium were used instead of the water-film electrode. A barium titanate photoelectret (or modified antimony sulphur) with an Aquadag electrode would generate usable signals across the output terminals when an electric lamp or hot soldering iron was held near the surface. Further tests showed that the germanium device was not a photoelectret. Since the germanium used was not a dielectric, this device turned out to be our old friend, the junction photocell, discussed earlier in this article. END

RESISTIVITY OF VARIOUS SEMICONDUCTORS AND DIELECTRICS

MATERIAL	RESISTIVITY (Ohms per cc)
Semiconductor	
Doped antimony-aluminum	0.01 to 35
Doped silicon	0.01 to 40
Doped germanium	1.0 to 60
Dielectric	
Ivory	2×10^{8}
Halowax 1001	2×10^{13}
Ordinary glass	9×10^{13}
Carnauba wax	6×10^{14} (30°C)
Sulphur	8×10^{15} to 10^{17}
Rosin	5×10^{16}

The resistivity of copper is 1.7×10^{-6} ohms per cc.

References

[1] G. Nadjakoff, in *Physik Zeitschrift*, Vol. 39, pages 226–227, 1938

[2] W. Conrad Roentgen, in *Ann. d. Phys.*, Vol. 64, page 1, 1921.

COVER FEATURE

New ELECTRONIC PIANO

BENJAMIN F. MIESSNER

Benjamin Franklin Miessner has devoted most of his life to audio engineering, particularly to the development of electronic musical instruments. His patents have been the basis of organs by Everett, Minshall and Wurlitzer, and pianos by Hardman & Peck, Story & Clark (Storytone) and Ansley.

Author with Mrs. Miessner at the electronic piano.

Before founding his laboratory in 1930, Miessner had made important contributions to the art of electronic sound recording and reproduction as chief engineer of Brunswick-Balke-Collender, and at an even earlier date invented the first noise-canceling microphone for airplane use.

Other developments and inventions of Miessner include work on guided missiles with John Hays Hammond before World War I, at which time he invented and built the ancestor of our present-day electronic "turtles" and "squirrels," an "Electric Dog" which would follow a light. He also developed a one-control radio receiver before 1920, and produced (for Garod Radio Co.) some of the first a.c. receivers.

HUNDREDS of millions of dollars' worth of electronic organs have been sold since their introduction in 1935.

Electronic guitars have been produced in great numbers since the early 1930's, and today no popular orchestra is complete without one. The electronic "steel" guitar has made possible tremendous advances in artistic performance.

Electronic carillons have supplanted cast bells and have made feasible a great many installations where the cost of cast bells would have been prohibitive.

In spite of all these electronic advances in music, the piano has been technically static for at least 50 years; the industry as a whole has never welcomed new tone-production methods. Yet the piano was at one time a well-nigh universal instrument, found in almost every home that could afford one. When (in 1930) I set up my first laboratory, exclusively for the application of electronics to musical instruments, my very first developments were directed toward the piano in an effort to simplify the age-old tone-production methods and to provide a variety of tonal types. Though I already had a 25-year background of training and experience in radio and electro-acoustics, another 25 years of almost constant research and development were to be necessary to produce my greatest achievement, the stringless electronic piano that is the subject of this article.

Early experiments

The very first vibrators used in those early days were reeds. Then tuning forks, rods and bars were tried. But their output lacked the great complexity and overtone richness of piano tones.

Hammer-struck strings were next used. Much more realistic, they yet lacked essential details of tonal perfection. Such nuisances as periodic retuning were still unsolved.

Conventional pianos were then tried, with the soundboard cut away to minimize direct acoustic tone, and magnetic, electrostatic and other types of string vibration pickups. Their performance, though interesting, was not suitable because the tones did not subside fast enough for clearness in rapid passages. The effect was such as is heard on conventional pianos when too much sustaining pedal is used.

I went back to reeds again in my recently developed electronic piano. They are simple, rugged and can hold their tuning for decades.

Problems with reeds

Reeds have been successful only when maintained in continuous vibration, as in reed organs, accordions or orchestral reed instruments. They have never been found useful in true musical instruments of the percussion family. Their overtones are few and completely inharmonious with one another. This may come as a surprise to the electronic

technician who is used to thinking of overtones and harmonics as synonymous. Yet the frequency of the second partial (overtone) is 6.267 times the fundamental; that of the third, 17.548; the fourth, 34.387, and the fifth a little more than 56 times the fundamental.

A reed fixed at one end and free at the other has only one nodal point—the fixed end—when vibrating at its fundamental. It has an additional node for each partial generated. For the second partial, the node is at 0.2261 of the length from the free end; for the third partial, the nodes are at 0.1321 and 0.4999 the length from the free end.

However, reeds do offer great and tempting advantages. They are simple, rugged, and can hold their tuning over many years. The trick is to make a "silk purse" out of this traditional "sow's ear" of the musical field.

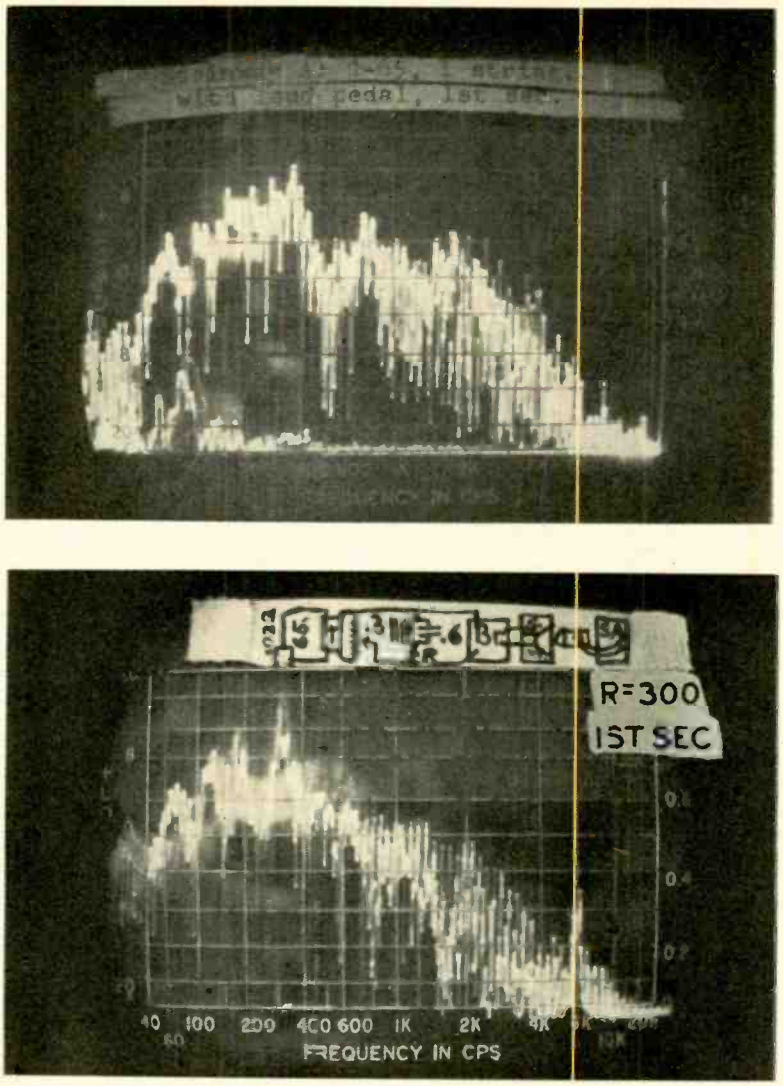
The path of research in the effort to solve the problems of using the musically lowly, hammer-struck free reed as a producer of truly beautiful tones was a long one, covering 25 years and staked out by more than 40 issued and pending patents. The solution comprises several tricky steps:

1. Striking the reeds at their third-partial nodal points to eliminate this discordant component of the reed vibration.

2. Placing the pickups at the second partial's nodal point and thus eliminating this partial, also badly discordant. This leaves only the fundamental vibration to be translated by the pickups.

3. Designing and adjusting the pickups so they themselves—with their connected circuitry—develop a complete series of precisely in-tune overtone (harmonic) currents. These can be completely characteristic of piano tones and can produce *better* tone quality than conventional pianos.

4. Further control of the harmonic content of the complex tone currents by formant circuitry to realize some of the characteristic effects of soundboards in string pianos, to produce pianistic tones throughout the entire pitch range.



Above is the output of a Steinway model A grand and, below, that of the new Miessner electronic piano. The photos show the first five partials in closely agreeing amplitude ratios, followed by higher-frequency partials up to nearly 20,000 cycles. This can be compared with the similar tone shown in Fig. 4.

Some piano characteristics

The suggestion that an electronic instrument can improve the tone quality of the piano may shock some who are used to thinking of the piano as a standard instrument, to be imitated rather than surpassed. Yet the piano is far from being a perfect instrument, for the following reasons, among others:

Tensioned-string piano tones are imperfect because their overtones become musically sharper as their harmonic number increases, so they are not strictly in tune with one another. This is due to inherent stiffness in the strings, which should have no stiffness other than that due to tension.

Further imperfections are caused by a series of jingling, inharmonic overtones set up by longitudinal vibrations in the strings, especially noticeable in the lower registers and at a frequency about four octaves above the normal transverse vibration pitch of the string.

The piano soundboard tends to cut off at about 100 vibrations per second—roughly two octaves above the lowest string's fundamental vibration.

The soundboard does not vibrate in the same direction over its whole surface; various areas vibrate in phase opposition and cancel one another. The soundboard also "amplifies" the string vibrations unevenly, so the tone quality shifts rather abruptly in many instruments from one note to another.

The right-hand end of the soundboard responds best to frequencies of about 500 per second, so the tones at the top of the scale (between about 3,000 and 4,000 vibrations per second) are very fleeting and contain more hammer noises than musical tones.

The piano has certain mechanical weaknesses as well, including the fantastically complicated hammer action, worthy of Rube Goldberg at his best. There is also the necessity of keeping over 200 strings under from 160 to 180 pounds of precisely adjusted tension. This necessitates massive iron plate and woodwork buttresses to hold in check the aggregate crumpling force of over 20 tons. In spite of this pianos require frequent retuning.

The new reed piano

The new stringless piano uses small steel reeds 0.25 inch wide and .032 inch thick, struck by key-actuated hammers and stopped by very simple dampers. This key action has about one-tenth as many parts as a conventional piano action, yet performs better. The principle of the dashpot is substituted for the complex friction-damping mechanism invented by Christofori in 1709 and

improved and complicated greatly since.

Machined brass pickups (Fig. 1) are positioned near the free ends of the reeds. They act as stators of variable capacitors of which the reeds are the moving plates. The changes in capacitance caused by reed vibration are used to vary the frequency of an oscillator, producing a frequency-modulated signal which is detected by a discriminator.

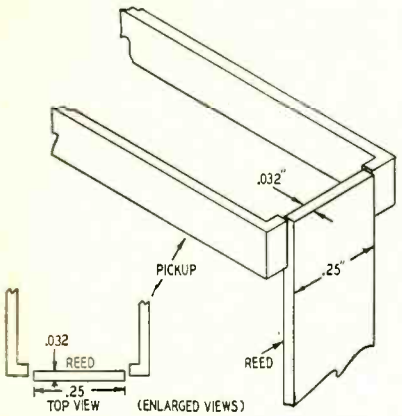


Fig. 1—Positioning of pickup and reed.

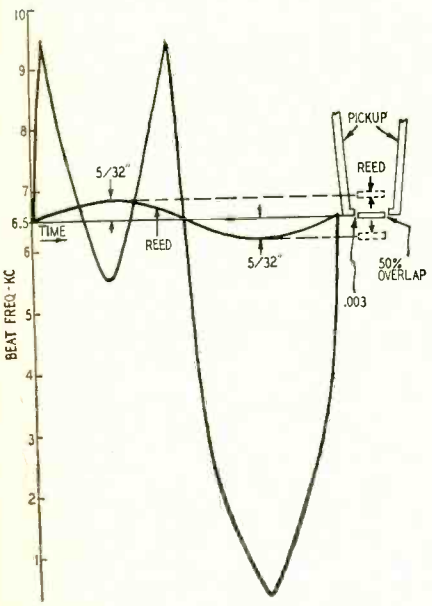


Fig. 2—End view of reed, with diagram of its excursion and voltage generated.

The oscillator, discriminator and an audio stage form a preamplifier contained in the piano itself. Its output produces loud tones in a headset, making it possible for a student to practice on a (to others) silent piano. For room-level output, the piano may be plugged into an amplifier or even the home radio, TV or phonograph system.

The pickups are the same thickness as the reed and are so adjusted that they overlap the reed's edge about one-half its thickness. The output tone quality may be adjusted by varying the amount of this overlap. If pickup and reed are set flush with no overlap (maximum capacitance), the output will be double the reed frequency. The half-way overlap gives exact frequency reproduction.

If the pickup is moved farther away from the normal half-lap position, the fundamental's strength relative to the higher partials will increase. Moving it still farther away increases the damping rate, since the low-amplitude vibrations—as these decrease to minute values—will not be picked up. The tone quality can also be changed by changing the shape of the pickup.

The pickups are so constructed that each has two faces, one positioned at each edge of its reed. This neutralizes any effects that might be caused by sidewise motion or vibration. The normal capacitance between reed and pickup is about 4 $\mu\mu$f. This increases to a maximum of 8 $\mu\mu$f as the reed moves to a position opposite the pickup faces, then decreases rapidly as the reed moves on past the pickup faces and toward maximum deflection. As the reed moves back toward its noral rest position, capacitance again increases rapidly, then falls to a very low value as the reed swings in the opposite direction. The asymmetrical variation in capacitance thus produced generates a wave rich in harmonics.

At lower reed amplitudes the pickup acts more like a variable-area pickup and the output contains only the fundamental and a few partials. This is very important, since piano tones change similarly in tone quality with amplitude.

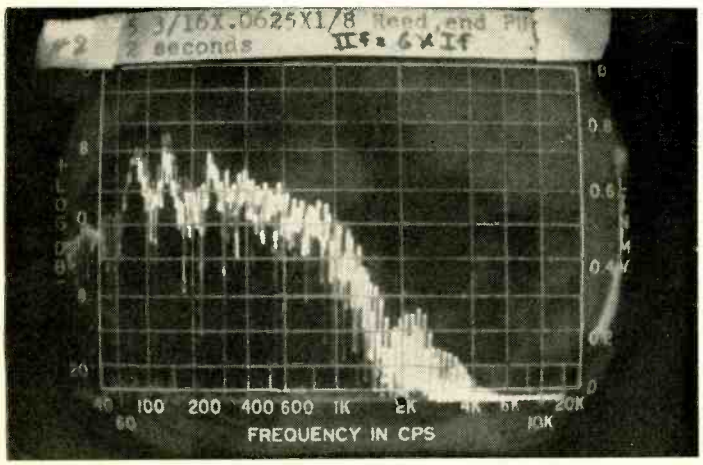


Fig. 3—Waveform produced by the reed and fed into tone-forming circuits.

The actual capacitance changes are very small. The total capacitance of reeds to pickups in a 73-note reed piano is only 280 $\mu\mu$f with all reeds in the rest position. Coupled as the frequency-determining element of an L-C circuit for a 5-mc oscillator, the vibration of a single reed modulates the oscillator up to more than 10,000 cycles.

The curve marked "Reed" in Fig. 2 is the sinusoidal vibration of partial 1 (the fundamental frequency) of the reed at an amplitude of 5/32 inch (average) on each side of its normal position. The pickup faces next to the reed edges are 1/32 inch wide and ⅛ inch long (along the reed edges). The air gaps are about .003 inch long, but adjustable by bending the pickup arms, for "voicing" the amplitude of the output tone.

The other curve shows the frequency modulation of the oscillator as the reed is moved up to 5/32-inch deflection, back down to 5/32-inch downward deflection and back up again to its normal position in completing one cycle of vibration.

This frequency-modulation curve was obtained by beating the FM oscillator of the preamplifier with a fixed-frequency r.f. oscillator and measuring the resulting a.f. beat-note frequency. The actual frequency modulation of the FM oscillator is 3,000 cycles above and 7,000 cycles below its norm of 5 mc, or 10,000 cycles over-all at the 5/32-inch reed vibration amplitude. This amounts to 0.2% modulation.

The effect of this sharply peaked change of pickup capacitance within a cycle of reed vibration is to set up, in the preamplifier circuit, a long series of both even- and odd-numbered precisely harmonic a.f. partials having a fundamental frequency the same as partial 1 of the reed. A sonic spectrogram of this output tone is shown in Fig. 3.

When modified by a suitable a.f. tone-forming circuit, this spectrum is changed to that shown in Fig. 4, which is a very fine piano tone of 65 cycles.

The preamplifier

The oscillator just referred to — a 6BA7 — is the first tube of the three-tube preamplifier contained in the piano (Fig. 5). The 6BA7's output goes to a 6AL5 hooked up as an FM discriminator. The audio signal thus detected is amplified by a 6AG5. The preamplifier output may be further amplified with ordinary amplifiers as previously stated, but ideally is applied to the input of a special amplifier.

This amplifier contains broadband L-C formant circuits to stimulate the tonal effects of the piano soundboard, which cuts off rather sharply around 100 cycles at the low end.

Because of the low-frequency cutoff it is both desirable and economical to use an amplifier and speaker system with limited low-frequency response—one which starts to cut off at about 100 cycles. The high-frequency characteristics must be very good, however, and

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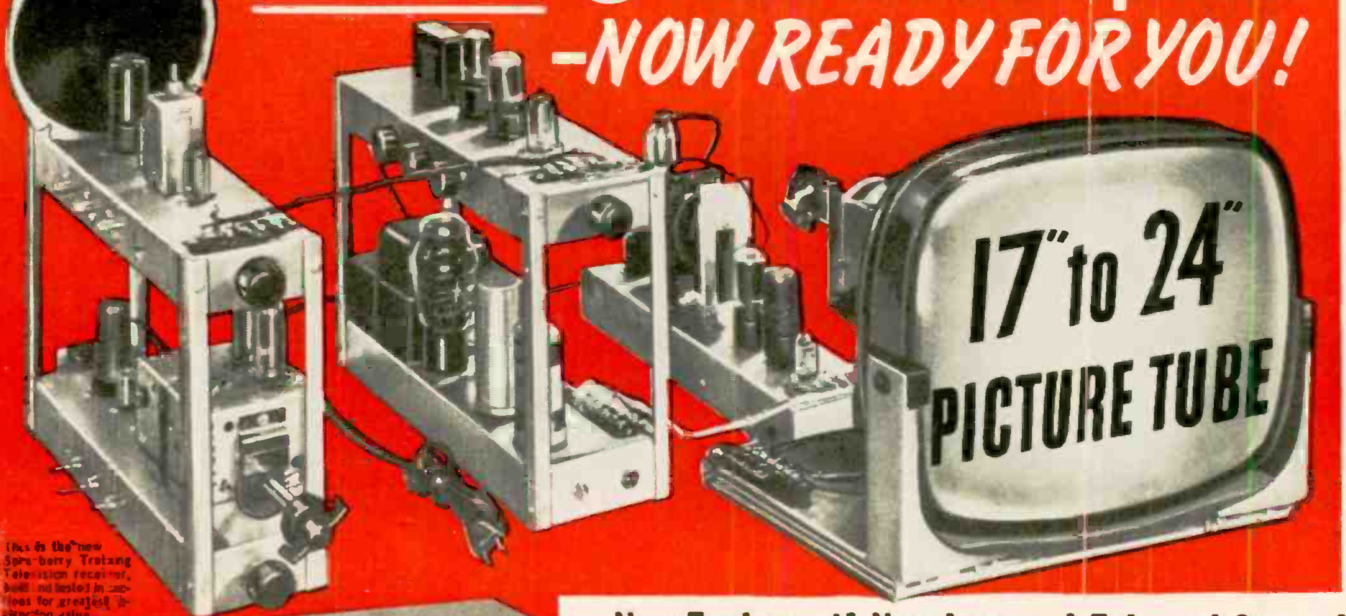

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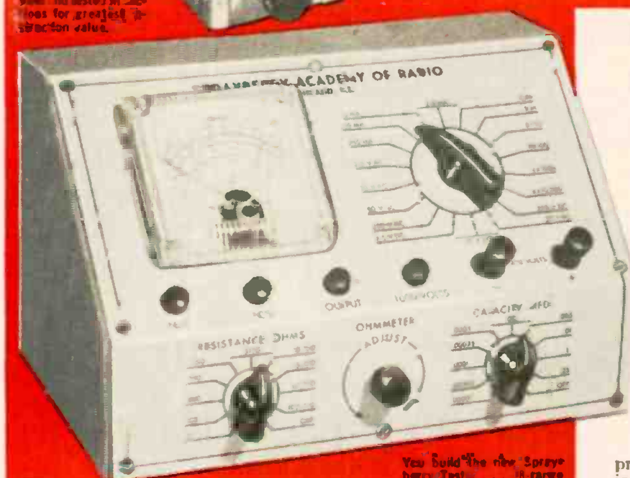

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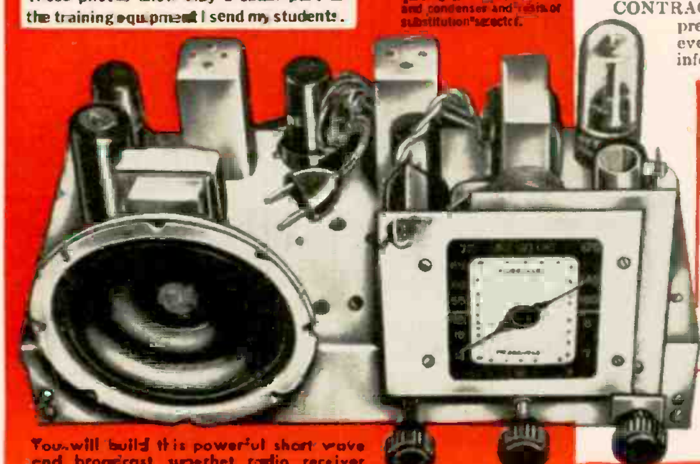

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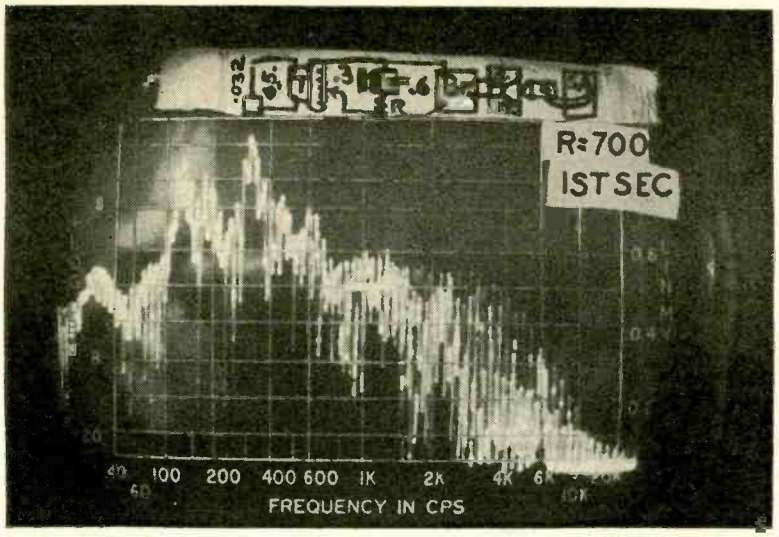


Fig. 4—Fig. 3 pattern as modified in the audio-frequency amplifier circuits.

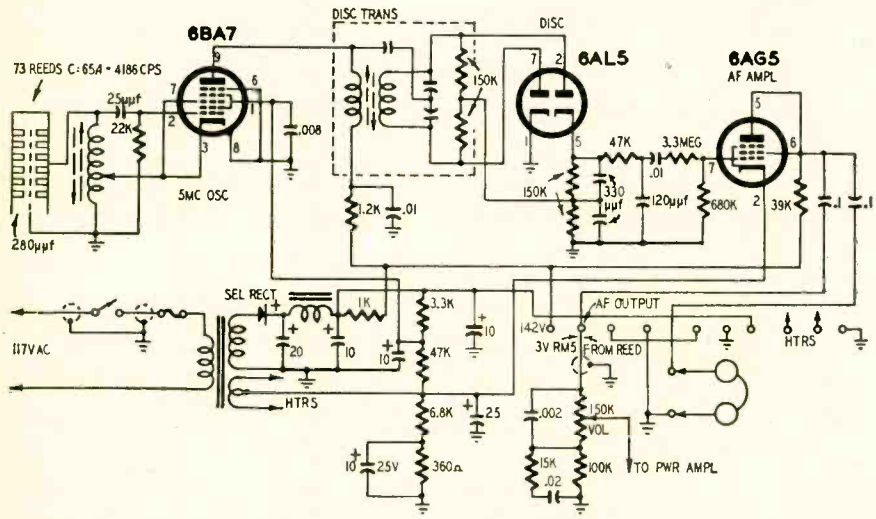


Fig. 5—The piano-contained FM oscillator, discriminator and a.f. amplifier.

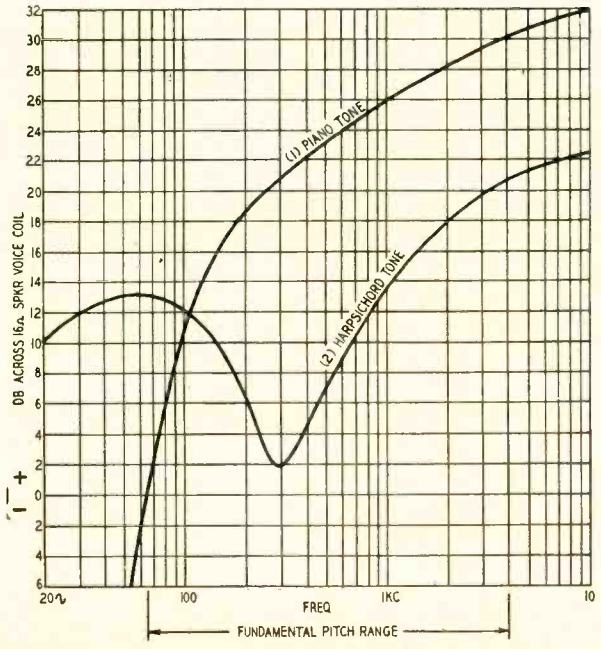


Fig. 6—Two of several frequency characteristics obtained with the new piano

the damping characteristics must be such that there is little or no overhang vibration. The speaker cone must be as nearly critically damped as possible to insure clean tones in rapid passages. Fig. 6 shows the frequency characteristics of the entire audio system from the grid of the 6AG5 to the voice coil of the speaker. Curve 1 produces very fine piano tones and curve 2 produces tones characteristic of the harpsichord. These tone characteristics can be varied by a panel control, which varies the ratio of inductance and capacitance in a circuit at the output of the preamplifier.

Other types of tone in great variation may be produced by further variations of the L-C-R elements of the tuned a.f. circuit across the grid input of the a.f. power amplifier. These adjustments change the shape of the over-all frequency characteristic of the a.f. system.

The complete piano

The electronic piano can be much smaller, lighter and cheaper than its predecessors. The basic model, cabinet containing keys, action, reed-pickup assembly and FM preamplifier, weighs 75 pounds and can be handled easily by one man. This reduction in weight, bulk and cost is due to the reed action, which makes it possible to abandon the long strings with their aggregate tension of about 20 tons which necessitates the heavy cast-iron plate and bulky wood buttressing. The large-area soundboard is also abandoned.

Power amplifiers for the portable types can be handled as separate units or placed, with the speaker, in a cabinet or console attached underneath the basic unit, in a portable cabinet (as with guitars), or even in the piano bench.

A cheaper instrument for child or student use may be placed on a table top. A most important feature to the student is the provision for headphones which make piano exercises inaudible to anyone but the player.

Present models provide only piano performance. Other types of tone can be included in later models. These can include organ (by feedback maintenance of reed vibration) and percussive tonal types with different damping rates and timbres, such as harp, banjo, xylophone and even drum. The various damping rates are obtainable with constantly acting dampers or by degenerative feedback. By adding another set of pickups of a different type near the fixed ends of the reeds, or by using hard hammers, it is possible to produce chime or bell tones.

This new stringless piano may be the forerunner of a whole new class of electronic musical instruments of widely differing tonal performance. The lowly fixed-free reed, virtually the "sow's ear" among musical vibrators, has become the "silk purse" of electronic design and technique with the great advantages of low cost, weight and bulk, silence when desired, and the ability to stay in tune for many decades. END

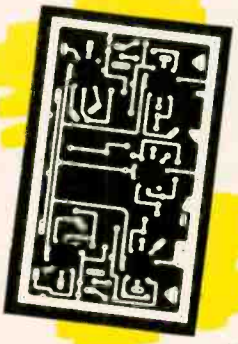
NEW 1955

Heathkit

Engineering Features

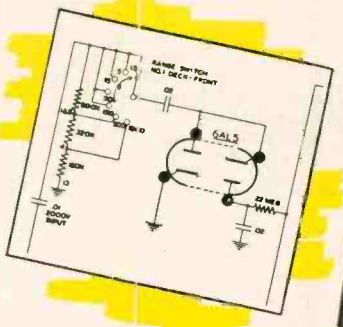
New PRINTED CIRCUITS

One of the many tremendous improvements in the new 1955 Heathkits is the use of an etched metal process printed circuit board. Printed circuits will be used in Heathkits whenever they will affect construction simplification, performance stabilization, and lend themselves to instrument design. Now for the *first* time a kit instrument company offers the advantages of modern printed circuit instrument construction technique. For the *first* time consideration has been given toward reducing kit assembly time. Also this is the *first* time that printed circuit boards have been hand soldered on a volume basis. Offered only by Heathkit, the pioneer and leader in kit instrument design.



New PEAK-TO-PEAK VTVM CIRCUIT

New 6AL5 full wave rectifier in AC input circuit permits full scale peak-to-peak measurements. Seven ranges — upper limits 4000 volts peak-to-peak. Just the thing you TV servicemen have needed in making TV circuit voltage checks. Precision resistor voltage divider limits AC RMS level to 150 volts. Prevents overloading the rectifier—extends upper limit AC RMS ranges to 1500 volts—further protects meter and circuitry against AC flash-over or arcing. Another definite example of continuing Heathkit design leadership in the kit instrument field.



New HIGH READABILITY PANELS

New 1955 Heathkits feature complete panel redesign. Sharp white lettering applied to the beautiful charcoal gray panels, provide a new high in readability. Lettering is easy-to-read open style and panel calibrations are vividly clear against the pleasing soft gray background. New knobs of exclusive Heathkit design.

New 3" UTILITY SCOPE

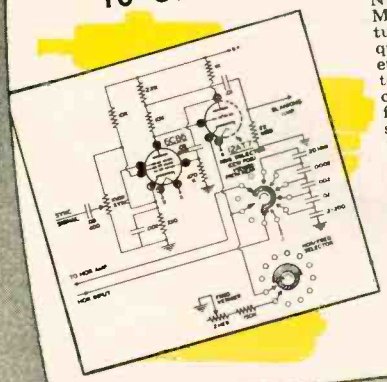
The new 3" Scope is a "natural" for the well rounded line of Heathkit instruments. Small in size, 11¾" deep, 6½" wide, 9½" high, yet big in performance. Just think of the value, an Oscilloscope for $29.50. Brilliant intensity, sharp focusing, wide positioning range. An ideal portable Scope for the TV serviceman—a second shop scope—modulation monitor for you hams (deflection plate terminals in rear of cabinet). Performance to spare for all general scope applications. See specifications on following page.

New STYLING New COLOR

New styling and coloring is responsible for tremendous improvement in Heathkit appearance. The new instrument panel color combination is high definition white lettering in a soft charcoal gray panel. Cabinet color is a lighter feather gray. The satin gold baked enamel cabinet for the WA-P2 Preamplifier is further indicative of the modern pacesetting trend in Heathkit styling.

New SCOPE SWEEP CIRCUIT 10 CYCLES — 500 KC

New 1955 Heathkit Model 0-10 Scope features a new wide frequency range sweep generator covering 10 cycles to 500,000 cycles. This coverage is available in five virtually decading sweep ranges and is five times greater than the sweep frequency range usually available. Excellent retrace time characteristics, actually less than 20% at 500 KC. Use of the free running Heath circuit provides a larger margin of stability and a new high in Heathkit Scope performance.



Continuing PROGRESS FUTURE LINE EXPANSION

The outstanding improvements featured in the 1955 Heathkit line are representative of the progress characterized by Heath Company operation. Long range planning will provide a continuing succession of new kit releases to further expand the Heathkit line which already represents the world's greatest selection of electronic kits. The innovations in the 1955 line, are representative of additional new models scheduled for release for the coming years.

SEE THE INSTRUMENTS ON THE FOLLOWING PAGES

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AUDIO-HIGH FIDELITY

HIGH-FIDELITY DICTIONARY

A compilation of commonly used audio terminology

By ED BUKSTEIN*

HIGH fidelity is a hobby that claims an ever-growing following and represents a considerable portion of the electronics industry in this country. The public, having learned the meaning and pleasure of high fidelity, is no longer content with the 100–5,000-cycle response once considered satisfactory. The technician called upon to install or repair a high-fidelity system finds the customer entirely capable of intelligent discussion of sound reproduction.

For personal satisfaction and business reasons, the technician should acquaint himself with the techniques of high-fidelity sound reproduction. The following definitions indicate the extent of the subject, and the areas in which further study would be advisable.

Acoustical labyrinth enclosure

A loudspeaker enclosure in which partitions are used to increase the length of the air path of the rear radiation of the loudspeaker (Fig. 1).

*Northwestern Television and Electronics Institute, Minneapolis, Minn.

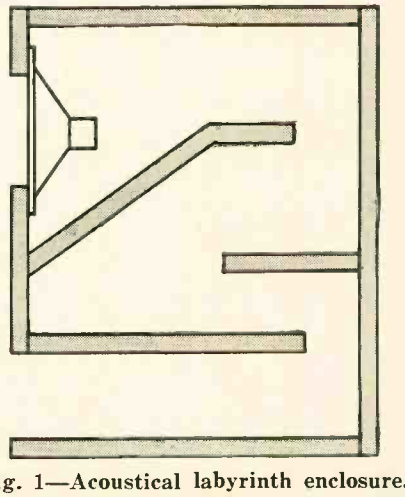


Fig. 1—Acoustical labyrinth enclosure.

NEW *Heathkit* 5" PUSH-PULL OSCILLOSCOPE KIT FOR COLOR TV

First color television service Oscilloscope with necessary high sensitivity and full 5 megacycle bandwidth.

New 5UP1 CR tube

New printed circuit construction, all components mounted on high insulation surface resulting in uniformly low circuit capacities.

New type wide frequency range Heath sweep generator. 10 cycles to 500,000 cycles.

New cabinet styling and color harmony—charcoal gray panel with high readability white lettering.

BRAND NEW DESIGN: The new Heathkit Model O-10 Oscilloscope would be something special at any price, but is almost unbelievable at $69.50. Completely re-designed scope has broadband amplifiers for color TV work and offers brilliant overall performance. Vertical frequency response within 5 db from 5 cps to 5 mc. Even more astounding, the response is down less than 1½ db at 3.58 mc. the color TV sync burst frequency. It is essential that scopes for color work have these broadband characteristics.

PRINTED CIRCUITS: Two printed circuit boards used in this fine instrument to insure stable, consistent performance. Problems solved by pre-engineering of boards, and their use guarantees completed unit that will have same characteristics as lab development model. Printed circuits simplify construction and save labor.

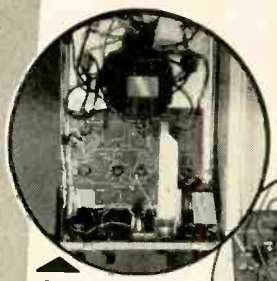
NEW SWEEP CIRCUIT: Sweep circuit operates with exceptionally good linearity from 20 cps to over 500,000 cps. 5 times the usual range for scopes in this price range. An entirely new circuit introduced for the first time in any Heathkit.

New electronic positioning controls for instantaneous, definite positioning without bounce or overshoot.

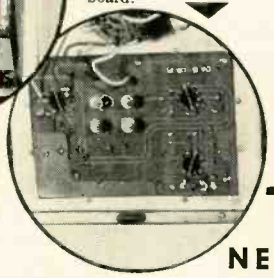
MODEL O-10

$69.50

Shpg. Wt 27 lbs.



Simplified, standardized construction technique of vertical and horizontal amplifier construction made possible through the use of a single *printed circuit* board.



Clean, open, under-chassis construction and wiring. Possible only through use of pre-cabled wiring harness, and simplified printed circuit boards.

FEATURES: Other outstanding characteristics of this professional oscilloscope are: Built-in 1V peak-to-peak reference for calibration of plastic CRT face-plate; 5" 5UP1 CRT; push-pull hor. and vert. deflection amplifiers; hor. trace width expandable to 3 times diameter of CR tube to allow inspection of any small portion of the signal; deflection sensitivity, .025 volts per inch; wiring harness pre-formed and cabled to save construction time and insure professional appearance and operation. Incorporates efficient retrace blanking. Frequency compensated step attenuator at the vertical input. Entire tube face useable. No foldover on vertical over-load. Performance obtainable only in much more expensive laboratory models.

Uses 5UP1, 6AB4, 6BQ7, 12BH7, 6CB6, 12AT7, 2-12AU7, 6X4, 1V2, and 6C4. Quality components used throughout so that outstanding performance characteristics may be maintained for years to come. Plastic molded condensers are used in all coupling and by-pass applications. The "new-look" in Heathkit styling produces professional appearance in keeping with the professional performance of this instrument.

3GP1 CR TUBE

NEW *Heathkit* 3" PRINTED CIRCUIT OSCILLOSCOPE KIT

MODEL OL-1

$29.50 Shpg. Wt. 15 lbs.

New compact utility Scope—lightweight—portable for service work.

Deflection plate terminals—ideal for ham transmitter modulation monitoring.

New easy-to-build printed circuit board with high insulation factor.

New Heathkit instrument styling—charcoal gray panel with high readability white lettering.

New Heath twin triode sweep generator 15–100,000 cycle sweep.

EXCEPTIONAL VALUE: The brand new Model OL-1 Utility Oscilloscope is designed especially for portable applications so that outside servicemen or persons performing field tests can have the advantages of a scope available. Then too, it is ideal for home workshop, the ham-shack, or as an "extra" scope for the service shop. It is compact, light in weight, and surprisingly versatile in operation. An outstanding instrument for the price.

Front panel controls are "bench-tested" for ease of operation and convenience. Printed circuit board used for constant circuit performance. Assembly time cut in half!

SPECIFICATIONS: Vertical amplifiers feature frequency response within 1 db from 10 cps to 100 kc, and within 5 db from 5 cps to 500 kc. Vertical sensitivity .2 volts per inch at 1 kc, with input impedance of 12 mmfd shunting 10 megohms.

Horizontal response within 1 db from 10 cps to 200 kc, and within 5 db from 6 cps to 500 kc. Hor. sensitivity .25 volts per inch at 1 kc, input impedance of 15 mmfd shunting 10 megohms. Sweep generator covers 10 cps to 100,000 cps with stable positive lock-in circuit. Cathode follower input in both vert. and hor. amplifiers; push-pull vertical and horizontal deflection amplifiers; 3" CRT; electronic positioning controls for wide range of vertical and horizontal spot deflection; provision for internal and external sync; 60 cycle line sweep. New modern color styling and unusual performance make this instrument an outstanding value.

NEW *Heathkit* 5" PRINTED CIRCUIT OSCILLOSCOPE KIT

5BP1 CR TUBE

MODEL OM-1

$39.50 Shpg. Wt. 24 lbs.

VERSATILE INSTRUMENT: The new Model OM-1 general purpose Oscilloscope represents an outstanding dollar value in reliable test equipment. Full 5 inch CRT. Printed circuit boards for ease of assembly, constant circuit characteristics, and rugged component mounting. Includes all the design features necessary for servicemen, students, experimenters, radio amateurs, etc. Frequency response of amplifiers flat within 1 db from 10 cps to .00 kc, and down only 7 db from 10 cps to 500 kc. Sweep generator range from 20 cps to 100,000 cps. Also features new Heathkit color styling with charcoal gray panel and high definition white lettering for readability even under subdued lighting conditions.

DESIGN FEATURES: A full-size, versatile oscilloscope at a price you can afford. Other features are: adjustable spot shape control; RF connections to deflection plates; direct coupled centering controls; external and internal sweep and sync; 60 cycle line sync; built in 1 volt peak-to-peak panel terminal reference voltage; professional appearance of cabinet, panel, and knob styling.

HEATH company

BENTON HARBOR 20, MICHIGAN

AUDIO—HIGH FIDELITY

Amplitude distortion

The result of nonlinearity of an amplifier with respect to signal amplitude. This results from driving a tube beyond the linear portion of its characteristic so that, for example, a two-fold increase of input-signal amplitude will not double the amplitude of the output. Since this type of distortion introduces harmonics not present in the input, it is also known as *harmonic distortion.*

Attenuator

Attenuation is the opposite of amplification, and an attenuator is therefore a component or network designed to reduce the amplitude of a signal applied to it. In its simplest form this would be a potentiometer, but a more elaborate network of resistances is often used to provide also impedance matching.

Audio range

The range of frequencies to which the human ear will respond. This range varies with individuals, age, state of health, etc. and is approximately 16 to 16,000 cycles.

Baffle

A structure, usually wooden, used to lengthen the air path of the rear radiation of a loudspeaker. In its simplest form, the baffle is a flat piece of wood with an opening for the loudspeaker. By increasing the air-path length of rear radiation, it reduces the cancellation of sound waves by out-of-phase components of front and rear radiation. Because, the dimensions of a flat baffle adequate for low-frequency response are excessively large, this type is not commonly used.

Bass boost

The characteristic of a circuit that results in increased gain at lower frequencies. Bass-boost circuits are generally designed to increase the low-frequency gain at a rate of 6 db per octave.

Bass-reflex enclosure

A loudspeaker enclosure consisting

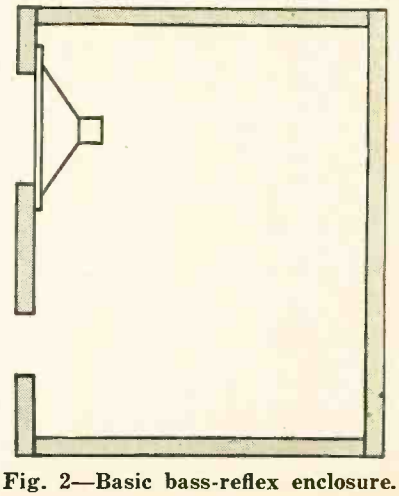


Fig. 2—Basic bass-reflex enclosure.

NEW Heathkit VACUUM TUBE VOLTMETER KIT

PRINTED CIRCUIT DESIGN

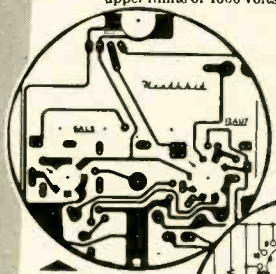
New charcoal gray baked enamel panel with high readability, white lettering. New soft feather gray cabinet, subdued pilot light indicator.

New printed circuit board for faster, easier construction—exact duplication of Lab development model.

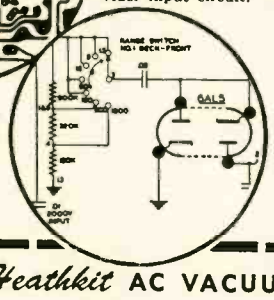
Another outstanding example of continuing Heath Company pioneering and leadership in the kit instrument field. A new **printed circuit** VTVM. New peak-to-peak circuit—new styling and new panel design. A prewired, prefabricated printed circuit board eliminates chassis wiring, cuts assembly time in half, assures duplication of Engineering pilot model specifications, and virtually eliminates possibility of construction error.

CIRCUIT:

A 6AL5 tube operated as a full wave AC input rectifier permits seven peak-to-peak voltage ranges with upper limits of 4000 volts P—P. Just the ticket for you TV servicemen. Voltage divider in the 6AL5 input circuit limits applied AC input to a safe level. This circuitry and the isolation of the meter in the cathode of the 12AU7 bridge circuit affords a high degree of protection to the sensitive 200 microampere meter.



Full wave rectifier in AC input circuit. Read peak-to-peak and RMS volts with upper limit of 4000 P—P and 1500 volts RMS. Voltage divider input circuit.



The first kit instrument to offer a labor-saving, error-free *printed circuit* board. Your instrument an exact wiring replica of Engineering development model.

RANGES:

Seven voltage ranges. 1.5, 5, 15, 50, 150, 500 and 1,500 volts DC and AC RMS. Peak-to-peak ranges 4, 14, 40, 140, 400, 1400, 4000. Ohmmeter ranges X1, X10, X100, X1000, X10K, X100K, X1 meg. Additional features are a db scale, a center scale zero position, and a polarity reversal switch.

New easy-to-read open panel layout. Off-on switch now incorporated in the selector switch.

MODEL V-7

$24.50

Shpg Wt 7 lbs.

IMPORTANT FEATURES:

High impedance 11 megohm input—transformer operated—1% precision resistors, 6AL5 and 12AU7 tube—selenium power rectifier— individual AC and DC calibrations—smoother improved zero adjust control action—new panel styling and color—new placement of pilot light—new positive contact battery mounting —new knobs—test leads included.

The new V-7 also sets the pace as a kit instrument style leader. Smart, good-looking charcoal gray panel and soft feather gray cabinet. High readability panel with sharply contrasting white calibrations. The pleasing, eye catching, modern styling is in harmonious balance with the outstanding circuit design improvements. Easily the best buy in kit instruments.

New peak-to-peak meter scale—new color harmony—new knobs.

Heathkit AC VACUUM TUBE

VOLTMETER KIT

MODEL AV-2

$29.50 Shpg. Wt. 5 lbs.

Extreme sensitivity has been emphasized in the design of the Heathkit AC VTVM. Ten full scale RMS ranges are .01, .03, .1, .3, 1, 3, 10, 30, 100, and 300 volts. Frequency response is substantially flat from 10 cycles per second to 50 KC with input impedance of 1 megohm at 1 KC. Will accurately measure as low as 1 millivolt at high impedance. Total db range is —52 db to +52 db. An excellent kit for measuring the output of phono cartridges and the gain of amplifier stages. Use it also to check power supply ripple, as a sensitive null detector, and for compiling frequency response data. Features one knob operation, 200 microampere Simpson meter and precision resistors.

Heathkit 30,000 VOLTS DC

PROBE KIT

Measure up to 30,000 volts DC with the Heathkit VTVM and the 336 high voltage Probe. Precision resistor provides multiplication factor of 100. Can be used with any 11 megohm input VTVM. Housed in a Polystyrene two color sleek plastic probe body for safety of operation.

No. 336

$4.50

Shpg. Wt. 1 lb.

Heathkit PEAK-TO-PEAK

PROBE KIT

No. 338-C

$5.50

Shpg. Wt. 2 lbs.

Peak-to-peak values not exceeding 80 volts at a DC level of not more than 600 volts, can now be read directly by using 338-C Probe with previous model Heathkit VTVM's or any VTVM with 11 megohm input resistance. Probe construction features a modern printed circuit board for easy assembly. Frequency range 5 KC to 5 MC.

Heathkit RF PROBE KIT

The Heathkit RF Probe will permit the measurement of RF voltages up to 250 MC with an accuracy of ±10%. The limits are 30 volts AC and a DC level of 500 volts. Designed for any 11 megohm input VTVM. Modern styling, Polystyrene aluminum housing, Polystyrene insulation, and printed circuit board for easy assembly.

No. 309-C

$3.50 Shpg. Wt. 1 lb.

Heathkit

AUDIO WATTMETER KIT

MODEL AW-1

$29.50

Shpg. Wt. 6 lbs.

Read audio power output directly without using external load resistors with the new Heathkit Audio Wattmeter. Built-in non-inductive load resistors provide impedances of 4, 8, 16, and 600 ohms. Flat response from 10 CPS to 250 KC. Full scale power ranges are 0–5 MW, 0–50 MW, 0–500 MW, 0–5 W and 0–50 W. Model AW-1 will operate continuously at 25 watts and has a duty cycle of 3 minutes at 50 watts. Total db range in five positions is —50 db to +48 db, using the standard 1 milliwatt 600 ohms.

HEATH company

BENTON HARBOR 20, MICHIGAN

of a closed-back box having an opening in addition to the one behind which the speaker is mounted. The additional opening, known as a port, is generally located directly beneath the loudspeaker. The internal volume of the enclosure and the size of the port are such that the sound waves emitted from the port and from the speaker opening are in phase at the low frequencies, thereby improving the low-frequency response (Fig. 2).

Binaural

A sound-reproducing system for duplicating the realism of the original sound by providing a separate signal for each ear. The sound is picked up by two microphones spaced a short distance apart to represent the two ears of the listener. The signals are amplified separately and ultimately applied to a pair of headphones, one signal to each unit. Because of the inconvenience of headphones, loudspeakers are often substituted. This, however, is no longer a *pure* binaural system since sound from the "left-ear" loudspeaker can reach the right ear of the listener and vice versa.

Cabinet resonance

The acoustical resonance of the loudspeaker enclosure. The frequency of resonance is determined by the internal volume of the enclosure and gives rise to a booming effect sometimes known as one-note bass. Although it is sometimes possible to use cabinet resonance to compensate or fill in a low spot in the frequency response of the loudspeaker, it is generally desirable to minimize such resonance.

Capacitive pickup

A pickup element containing two metal plates, one stationary and the other actuated by the stylus. As the stylus rides in the groove, its movements are coupled to the movable metal plate. In this way, the plate spacing and capacitance vary in accordance with the modulation of the groove.

Capacitive loudspeaker

A type of loudspeaker consisting of two closely spaced metal plates, one rigid and the other thin and flexible. The audio signal is applied to these plates in series with a steady d.c. potential known as the polarizing voltage. As the flexible plate becomes alternately positive and negative it is alternately attracted and repelled by the fixed plate. The flexible plate corresponds to the cone of a conventional loudspeaker, and its vibration sets up sound waves. The capacitor loudspeaker is also known as an *electrostatic loudspeaker* since it operates on the principle of electrostatic attraction and repulsion.

Cartridge

In a pickup, the unit which converts the motion of the stylus into a corresponding electrical signal. (See Cera-

NEW *Heathkit* TV ALIGNMENT GENERATOR KIT

Controllable inductor sweep oscillator with output entirely on fundamentals.

Triple marker system 4.5 MC crystal controlled—3 sets of low loss, low capacity shielded cables included.

Electronically operated smooth continuously variable sweep circuit. No vibration, hum or noise.

Here is the most radically improved Sweep Generator in the history of the TV service industry. The basic design follows latest high frequency techniques which result in a combination of performance features not found in any other sweep generator.

SWEEP:

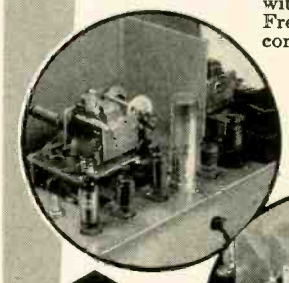
Sweep action is obtained electronically through the use of a newly developed controllable inductor, thereby eliminating all moving parts with their resultant hum, vibration, fatigue, etc. Frequency coverage entirely on fundamentals, is continuous from 4 MC to 220 MC at an output level well over a measurable .1 volt.

Frequency coverage: 4 MC—220 MC continuous including FM spectrum. RF output well over .1 volt.

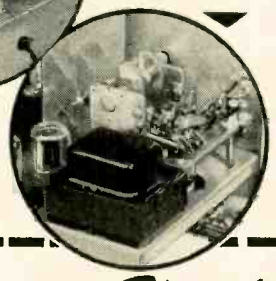
MODEL TS-3

$44.50

Shpg. Wt. 18 lbs.



Triple marker system, 4.5 MC crystal controlled marker—continuously variable marker—provisions for external marker.



Automatic amplitude control circuit—constant output voltage regulated power supply.

MARKER:

The same instrument incorporates a triple marker system with a crystal controlled reference. A variable marker provides accurate coverage from 19 to 60 MC on fundamentals, and 57 to 180 MC on calibrated harmonics. A separate fixed crystal controlled 4.5 MC marker can be used for checking IF, bandpass, calibration, reference, etc. Provisions are also made for external marker use. A 4.5 MC crystal is supplied with the kit.

POWER SUPPLY:

The transformer operated Power Supply features voltage regulation for stable oscillator operation. Three sets of shielded cables are furnished with the kit. Sweep range is completely and smoothly controllable from zero up to a maximum of 50 MC, depending upon base frequency.

Here is a TV Sweep Generator that truly no serviceman can afford to be without for rapid, accurate, TV alignment work.

NEW *Heathkit* SIGNAL GENERATOR KIT

MODEL SG-8

$19.50 Shpg. Wt. 8 lbs.

The new Heathkit service type Signal Generator, Model SG-8 incorporates many design features not usually found in this instrument price range. Frequency coverage is from 160 KC to 110 MC in five ranges, all on fundamentals, with useful calibrated harmonics up to 220 MC. The RF output level is well in excess of 100,000 microvolts throughout the frequency range. The oscillator circuit consists of a twin triode tube, one-half used as a Colpitts oscillator, and the other half as a cathode follower output which acts as a buffer between the oscillator and external load, thereby eliminating oscillator frequency shift usually caused by external loading.

All coils are factory wound and adjusted, thereby completely eliminating the need for individual calibration and the use of additional calibrating equipment. The stable, low impedance output, features step and variable attenuation for complete control of RF level. A separate 6C4 triode acts as a 400 cycle sine wave oscillator, and a panel mounted switching system permits choice of either external or internal modulation.

Heathkit LABORATORY GENERATOR KIT

The new Heathkit Laboratory type Signal Generator definitely establishes a new performance standard for a kit instrument. An outstanding feature involves the use of a panel mounted 200 microampere meter calibrated both in microvolts and percent modulation, thereby providing a definite reference level for using the Signal Generator in design work, gain measurements, selectivity, frequency response checks.

MODEL LG-1

$39.50

Shpg. Wt. 16 lbs.

DESIGN:

Additional design features are copper plated shield enclosure for oscillator and buffer stages resulting in effective double shielding. Fibre panel control shaft extensions in RF carrying circuits, thorough AC line filtering, careful shielding of the attenuator network, voltage regulated B plus supply, selenium rectifier, etc.

RANGES:

Frequency coverage from 150 KC to 30 MC all on fundamentals in five separate ranges. Output voltage .1 volt with provisions for metered external or internal modulation. Output impedance termination 50 ohms. Transformer operated power supply.

Investigate the many dollar stretching features offered by the LG-1 before investing in any generator for Laboratory or Service work.

NEW *Heathkit* BAR GENERATOR KIT

MODEL BG-1

$14.50 Shpg. Wt. 4 lbs.

The Heathkit BG-1 produces a series of horizontal or vertical bars on a TV screen. Since these bars are equally spaced, they will quickly indicate picture linearity of the receiver under test without waiting for transmitted test patterns. Panel switch provides "standby—horizontal and vertical position." The oscillator unit uses a 12AT7 twin triode for the RF oscillator and video carrier frequencies. A neon relaxation oscillator provides low frequency for vertical linearity tests. The instrument will also provide an indication of horizontal and vertical sync circuit stability as well as overall picture size. Operation is simple and merely requires connection to the TV receiver antenna terminal. Transformer operated for safety.

HEATH company

BENTON HARBOR 20, MICHIGAN

AUDIO—HIGH FIDELITY

mic, Crystal, Dynamic, Strain and Variable-reluctance pickup.)

Ceramic pickup

A pickup cartridge using the piezoelectric properties of a ceramic material such as barium titanate. The stylus movement applies a twisting motion to the ceramic element which translates this motion to a corresponding voltage variation. Ceramic pickups are practically unaffected by temperature and humidity.

Chip

The thread of material cut out of a disc by the stylus during recording.

Coaxial loudspeaker

Two loudspeakers mounted on the same longitudinal axis, usually one within the other. One of these speakers is smaller and is designed to reproduce the higher audio frequencies.

Compression

A type of nonlinearity intentionally introduced into a recording. The high-amplitude portions of the signal are reduced prior to recording and the low-amplitude portions are increased. This technique prevents high-amplitude signals from causing the stylus to cut into adjacent grooves, and prevents the signal-to-noise ratio from becoming excessively small during low-amplitude portions of the signal. (Not generally used in present-day high-fidelity recording.) The playback amplifier must be so designed that its gain will vary directly with the amplitude of the signal, or the loudness range will be smaller than that of the sound recorded (loud sounds will be quieter than they should be and quiet sounds louder). This type of compensation is known as volume expansion.

Cone resonance

The increased response of a loudspeaker at the natural frequency of vibration of its cone. This frequency is determined by such factors as cone size, shape, suspension, etc. and produces a peak in the response curve of the loudspeaker. In some cases this peak can be used to fill in a hole or low spot in the response of associated equipment.

Conical horn

A loudspeaker horn whose flare or taper is such that its cross-sectional area increases as the square of the distance from the throat.

Constant-amplitude recording

A disc recording technique in which, for equal signal voltages, the lateral

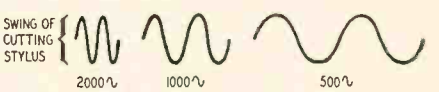


Fig. 3—Constant-amplitude recording.

movement of the cutting stylus will be equal for all recorded frequencies (Fig. 3).

TO BE CONTINUED

Heathkit TUBE CHECKER KIT

The Heathkit TC-2 Tube Checker was primarily designed for the convenience of radio and TV servicemen and will check the operating quality of tubes commonly encountered in this type of work. Test set-up procedure is simplified, rapid, and flexible. Panel sockets accommodate 4, 5, 6, and 7 pin tubes, octal and loctal, 7 and 9 pin miniatures, 5 pin Hytron, and a blank socket for new tubes. Built-in neon short indicator, individual 3-position lever switch for each tube element, spring return test switch, 14 filament voltage ranges, and line-set control to compensate for supply voltage variations, all represent features of the TC-2.

Results of tube tests are read directly from the large 4½" Simpson 3-color meter. Checks emission, shorted elements, open elements, and continuity. Wiring procedure has been simplified through the use of multi-wired color coded cable providing a harness type installation between tube sockets and lever switches. This procedure insures standard assembly and imparts a "factory built" appearance to the instrument. New Construction Manual furnishes detailed information regarding tube set-up procedure for testing of new or unlisted tube types. No delay necessary for release of factory data.

MODEL TC-2
$29.50
Shpg. Wt. 12 lbs.

Heathkit PORTABLE TUBE CHECKER KIT

The portable model is supplied with a strikingly attractive two-tone cabinet finished in rich maroon proxylin impregnated fabric covering with a contrasting gray on the inside of the detachable cover.

MODEL TC-2P
$34.50
Shpg. Wt. 15 lbs.

Heathkit REGULATED POWER SUPPLY KIT

MODEL PS-2
$33.50 Shpg. Wt 15 lbs.

Here is a source of regulated D.C. voltage for circuit development work. Power supply voltage and current drain to the circuit under test are constantly monitored by the 4½" panel mounted meter. Separate 6.3 volt at 4 ampere A.C. filament source available. The regulated and variable output voltage will be constant over wide load variations, and hum ripple will not exceed .012% at 250 volts under a 50 MA load. Completely isolated circuit, standby switch, and other desirable features, make the Model PS-2 extremely useful in a wide variety of applications.

Heathkit TV PICTURE TUBE TEST ADAPTER

The Heathkit TV Picture Tube Test Adapter used with the Heathkit Tube Checker Kit, will quickly check picture tubes for emission, shorts, etc. and determine tube quality. Consists of standard 12-pin TV tube socket, four feet of cable, octal socket connector, and data sheet.

No. 355
$4.50 Shpg. Wt. 1 lb.

Heathkit DECADE RESISTANCE KIT

MODEL DR-1
$19.50
Shpg. Wt. 4 lbs.

Twenty 1% resistors are decaded in 1 ohm steps to provide any value between 1 ohm and 99,999 ohms. Sturdy ceramic switches with silver plated contacts insure reliable service. Use the Decade Resistance in bridge circuits, meter multipliers, calibrations, or any application requiring a wide range of precision resistance values.

Heathkit AUDIO GENERATOR KIT

Here is an Audio Generator with features generally found only in the most expensive instruments. Sine wave coverage from 20 cycles to 1 Megacycle—response flat ±1 db from 20 cycles to 400 Kc—continuously variable and step attenuated output. Because the output voltage is relatively constant over wide frequency ranges, the AG-8 is ideal for running frequency response curves in audio circuits. Once set by means of the attenuator, this voltage may be relied upon for accuracy within ± 1 db. Instrument features low impedance 600 ohm output circuit and distortion less than .4 of 1% from 100 CPS through audible range.

MODEL AG-8
$29.50
Shpg. Wt. 11 lbs.

Heathkit DECADE CONDENSER KIT

The Heathkit Decade Condenser provides a ready source of capacity values from 100 mmf to .111 mfd inclusive in capacity steps of 100 mmf. Silver plated contacts on husky ceramic switches, assure positive contact for each switch position. Precision silver mica condensers ±1% accuracy for close tolerance accurate work.

MODEL DC-1
$16.50
Shpg. Wt. 3 lbs.

HEATH company
BENTON HARBOR 20, MICHIGAN

NEW *Heathkit* HIGH FIDELITY PREAMPLIFIER KIT

Here is the exciting new Heathkit Preamplifier with all of the features you Audiophiles have asked for and at a down-to-earth price level. Beautiful satin gold baked enamel finish, striking control knobs and arrangement, attractive custom appearance and entirely functional design.

DESIGN:
Uses three twin triode tubes in a shock mounted chassis, 2-12AX7 and 1-12AU7. Features tube shielding, plastic sealed color coded capacitors, smooth acting controls, good filtering, excellent decoupling, low hum and noise level, and all aluminum cabinet. Special balancing control for absolute minimum hum level. Cathode follower, low impedance output circuit for complete installation flexibility.

SPECIFICATIONS:
Provides five switch selected inputs, 3 high level, and two low level, each with individual level controls—4 position LP, RIAA, AES, and early 78 equalization switch—4 position roll-off switch, 8, 12, 16 with one flat position. Separate tone controls, bass 18 db boost and 12 db cut at 50 CPS, treble 15 db boost, and 20 db cut at 15,000 CPS. Power requirements from Heathkit Williamson Type Amplifier power supply 6.3 volts AC at 1 ampere, and 300 volts DC at 10 MA. Over-all dimensions 12⅛" wide x 5⅞" deep x 3⅝" high.

APPLICATION:
The new Heathkit WA-P2 Preamplifier has been designed to operate with any of the Heathkit Williamson Type Amplifiers and is directly interchangeable with the previous Model WA-P1 Preamplifier unit. Order your kit today and enjoy completely smooth control over the operation of your Hi-Fi system. Obtain the exact tonal balance of bass and treble with the precise degree of equalization you want. Note that the design of the WA-P2 accommodates the newly established RIAA curve.

MODEL WA-P2
$19.75
Shpg. Wt. 7 lbs.

HAM EQUIPMENT

Heathkit AMATEUR TRANSMITTER KIT

The Heathkit AT-1 Transmitter has established a high reputation and has been enthusiastically accepted by hundreds of experienced operators as well as beginners. Power input up to 35 watts for the novice and suitable as a standby exciter for your higher powered rig later on.

Model AT-1 can be crystal or VFO excited and operates on 80, 40, 20, 15, 11 and 10 meters. The prewound coils with the oscillator and amplifier are switched simultaneously by the rugged band switch. Meter switch allows a reading of the final grid and plate current on the panel mounted meter. Modulator input and VFO power sockets are provided as well as a key jack for CW operation. Other features include a crystal socket, standby switch, key click filter, AC line filter, good shielding and a 52 ohm coaxial output. The 425 volt, 100 milliampere power supply and 5U4 rectifier are more than adequate for the 6AG7 oscillator multiplier and 6L6 amplifier doubler.

MODEL AT-1
$29.50
Shpg. Wt. 16 lbs.

Brand NEW

HEATHKIT VFO KIT

The new Heathkit VFO is the perfect companion to the Heathkit Model AT-1 Transmitter and it has sufficient output to drive any multi-stage transmitter of modern design. Good mechanical and electrical design insures operating stability. Coils are wound on stable, heavy duty, ceramic forms using Litz or double cellulose wire coated with Polystyrene cement and baked for humidity protection. Variable capacitor of differential type construction, especially designed for maximum bandspread. Kit is furnished with a carefully precalibrated scale which provides well over two feet of scale length. Smooth acting vernier reduction drive and illuminated dial provides easy tuning and zero beating.

Power requirements 6.3 volts AC at .45 amperes, and 250 volts DC at 15 mils. Just plug it into the power receptacle provided on the rear of the AT-1 Transmitter. Seven band coverage 160 through 10 meters with 10 volt average RF output. Uses 6AU6 electron coupled Clapp oscillator and OA2 voltage regulator.

MODEL VF-1
$19.50
Shpg. Wt. 7 lbs.

Heathkit GRID DIP METER KIT

The invaluable instrument for Hams, servicemen and experimenters. Useful in TV service work, for alignment of traps, filters, IF stages, peaking compensation networks, etc. Locates spurious oscillation, provides a relative indication of power in transmitter stages. Use it for neutralization, locating parasitics, correcting TVI, measuring CL and Q of components, and determining RF circuit resonant frequencies. The variable meter sensitivity control, headphone jack, 500 microampere Simpson meter, continuous frequency coverage from 2 MC to 250 MC. Prewound coil kit and rack included.

LOW FREQUENCY COILS:
Low frequency range extended to 355 KC by the use of two additional coils. Complete with dial correlation curves. Set 341-A for GD-1B and set 341 for GD-1A. Shipg. wt. 1 lb. Price $3.00

MODEL GD-1B
$19.50 Shpg. Wt. 4 lbs.

Heathkit ANTENNA IMPEDANCE METER KIT

MODEL AM-1
$14.50
Shpg. Wt. 2 lbs.

Determine antenna resonance and resistance, transmission line surge impedance, and receiver input impedance. Works with one-half and one-quarter wave lines, half wave and folded dipoles, harmonic mobile and beam antennas. Resistance type SWR bridge —100 microampere meter—frequency range 0-150 MC—impedance range 0-600 ohms.

Heathkit ANTENNA COUPLER KIT

MODEL AC-1
$14.50
Shpg. Wt. 4 lbs.

For the Heathkit AT-1 Transmitter or any comparable Amateur Transmitter. Will handle power up to 75 watts at its 52 ohm coaxial input. Matches a wide range of antenna impedances with its L type tuning network and neon indicator. A tapped inductance provides coarse adjustment and a transmitting type variable condenser sets it "right on the nose." Will operate on the 10 through 80 meter bands.

HEATH company
BENTON HARBOR 20, MICHIGAN

New LOW PRICED HEATHKIT SINGLE UNIT Williamson Type *High* Fidelity AMPLIFIER KIT

Here is the newest Heathkit Hi-Fi Amplifier at the lowest price ever quoted for a complete Williamson Type Amplifier circuit. The W-4 Model has been designed for single chassis construction, and only for the new Chicago Transformer Company Model BO-13 "super range" high fidelity output transformer. This transformer, a new development in the Hi-Fi field, is being offered at substantial saving over transformers of comparable quality. It is outstanding in performance and on the basis of our tests, we find it equal in every respect to transformers used in the W-2 and W-3 Heathkit series.

LOW PRICES:

Through utilization of a single chassis with resultant economy obtained through elimination of duplicate sheet metal fabrication, connecting cables, plugs, sockets, and a new Chicago "super range" output transformer, a 20% price reduction has been made possible without sacrificing kit quality.

COMPONENTS:

The new Heathkit W-4 uses the same heavy duty power transformer and choke. It has all of the features of previous models including individual jacks and a wire wound control to balance the output tubes—plastic high quality capacitors and the exact circuitry previously utilized in Williamson Type Amplifiers. Intermodulation distortion and harmonic distortion are both at the same low level as in the W-2 and W-3 models.

CONSTRUCTION:

Here is the opportunity for even the economy minded Hi-Fi enthusiast to enjoy all of the advantages offered through Hi-Fi reproduction of fine recorded music. Simplified step-by-step Construction Manual completely eliminates necessity of electronic knowledge or special equipment. Assemble this Amplifier in a few pleasant hours.

COMBINATIONS AVAILABLE

W-4M with Chicago "super-range" transformer only. Single chassis main amplifier and power supply. Shipping weight 28 lbs. Express only **$39.75**

COMBINATION W-4 with Chicago "super-range" transformer only includes single chassis main amplifier and power supply with WA-P2 preamplifier kit. Shpg. wt. 35 lbs. Express only **$59.50**

NEW *Heathkit* 20 WATT High Fidelity AMPLIFIER KIT

MODEL A-9B

$35.50

Shpg. Wt. 24 lbs.

In keeping with the progressive policy of the Heath Company, further improvement has been made in the already famous Heathkit High Fidelity 20 Watt Amplifier. Additional reserve power has been obtained by using a heavier power transformer. A new output transformer designed and manufactured especially for the Heath Company, now provides output impedances of 4, 8, 16 and 500 ohms. The harmonic distortion level will not exceed 1% at the rated output.

FEATURES:

Outstanding features of the Heathkit 20 watt Amplifier include frequency response of ±1 db from 20 CPS to 20 KC. Separate (boost and cut) bass and treble tone controls. Four switch selected input jacks and a special hum balancing control. Flexibility is emphasized in the input circuits and proper equalization for all input devices is incorporated.

TUBE LINEUP:

12AX7 magnetic preamplifier and first audio amplifier. 12AU7 two stage amplifier with tone controls. 12AU7 voltage amplifier and phase splitter. Two 6L6 push-pull beam power output and 5U4G rectifier.

The Heathkit Model A-9B is excellent for custom installation and is designed for outstanding service at a very reasonable cost.

Heathkit SIX WATT AMPLIFIER KIT

MODEL A-7B

$15.50

Shpg. Wt. 10 lbs.

An outstanding value, this economically priced 5 watt Amplifier is capable of performance expected only in much more expensive units. Only 2 or 3 watts output will ever be used in normal home applications and Model A-7B will be more than adequate for this purpose.

SPECIFICATIONS:

Two switch selected inputs are available for crystal and ceramic phono pickups, tuner, TV audio, tape recorder, and carbon type microphone. Model A-7B features separate bass and treble tone controls, push-pull balanced output stages, output impedances of 4, 8, and 15 ohms, and extremely wide frequency range ±1½ db from 20 CPS to 20 KC. Not just a souped up AC-DC job. Full wave rectification, transformer operated power supply and good filtering, result in exceptionally low hum level.

MODEL A-7C

Provides a preamplifier stage and proper compensation for the variable reluctance cartridge and low level microphone. $17.50

Heathkit WILLIAMSON TYPE AMPLIFIER KIT

Here is the famous kit form Williamson Type *high fidelity* Amplifier that has deservedly earned highest praise from every strata of Hi-Fi music lovers. Virtually distortionless, clean musical reproduction, full range frequency response, and more than adequate power reserve.

OUTPUT TRANSFORMERS:

This outstanding Williamson Type Hi-Fidelity Amplifier is supplied with the famous Acrosound TO-300 output transformer. This quality transformer features the popular "ultra-linear" output circuit for clean maximum power level. Separate chassis for amplifier and power supply.

SPECIFICATIONS:

Frequency response within 1 db from 10 cycles to 100,000 cycles. Harmonic distortion at 5 watt output less than .5% between 20 cycles and 20,000 cycles. IM distortion at 5 watts equivalent output .5% using 60 and 3,000 cycles. Output impedances of 4, 8, or 16 ohms. Overall dimensions for each unit 7" high x 5½" wide x 11½" long.

CONSTRUCTION MANUAL:

This fine kit is supplied with a completely detailed step-by-step Construction Manual and the only effort required is the assembly and wiring of the pre-engineered kit. Even the complete novice can successfully construct this Amplifier and have fun building it.

COMBINATIONS AVAILABLE:

W-3 Amplifier Kit (Includes Main Amplifier with Acrosound Output Transformer, Power Supply and WA-P2 Preamplifier.) Shipping weight 37 lbs. Shipped express only..... **$69.50**

W-3M Amplifier Kit (Includes Main Amplifier with Acrosound Output Transformer and Power Supply.) Shipping weight 29 lbs. Express only **$49.75**

HEATH company
BENTON HARBOR 20, MICHIGAN

Heathkit COMMUNICATIONS RECEIVER KIT

Separate BFO oscillator tube and circuit.

Continuous coverage 550 KC—35 MC on 4 Bands.

MODEL AR-2

$25.50

(Less Cabinet)

Shpg. Wt. 12 lbs.

Phone—standby—CW panel switch.

RF gain control with AGC on-off switch.

Electrical bandspread tuning with logging scales.

An excellent example of typical Heath Company ability to produce top quality kit merchandise at ridiculously low prices, is the AR-2 Communications Receiver. Here is a transformer operated all-wave receiver with all of the desired features and none of the disadvantages commonly encountered in so-called "economy sets."

Receiver employs high gain miniature tubes and IF transformers, chassis mounted 5½" PM speaker, headphone jack, slide rule dial with Ham Bands plainly identified, and easy tuning with direct planetary drive. Continuous frequency coverage from 550 KC to 35 MC on 4 Bands, with electrical bandspread tuning and logging scales. Other features are RF gain control with AGC on-off switch—phone-standby-CW panel switch—prewound coils in a shielded turret assembly and copper plated chassis and shielding.

Uses 12BE6 mixer-oscillator, 12BA6 IF amplifier, 12AV6 detector-first audio, 12A6 beam power output, 12BA6 BFO oscillator, and 5Y3 rectifier. A lettered control plate is provided for the cabinet of your choice or you can order the optional Heathkit cabinet featuring the full size aluminum panel.

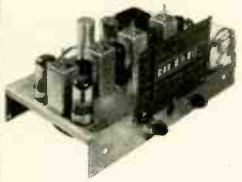
RECEIVER CABINETS

Proxylin impregnated fabric covered plywood cabinet available for BR-2 and AR-2 receivers. Includes aluminum panel, flocked reinforced speaker grill and protective rubber feet.

For BR-2 Receiver, Cabinet 91-9
Shipping weight 5 lbs. **$4.50**

AR-2 Receiver, Cabinet 91-10
Shipping weight 5 lbs. **$4.50**

Heathkit FM TUNER KIT



MODEL FM-2

$22.50

Shpg. Wt. 8 lbs.

Here is an FM Tuner that can be operated with your Hi-Fi Amplifier or through the "phono" section of the ordinary radio. Completely AC operated to eliminate problems usually encountered in "economy type" AC-DC tuner circuits. Features 8 tube circuit with separate mixer and oscillator, 3 double tuned IF stages followed by a limiter discriminator providing maximum sensitivity and selectivity across the full FM frequency band of 88 MC to 108 MC. The tuning unit is factory assembled and adjusted, thus eliminating tedious critical "front end" alignment problems. The attractive slide rule dial and vernier tuning combine to make the Heathkit FM-2 Tuner simple to operate.

Heathkit BROADCAST BAND RECEIVER KIT

MODEL BR-2

$17.50

(Less Cabinet)

Shpg. Wt. 10 lbs.

The Model BR-2 Broadcast Band Receiver is designed especially for the beginner without any sacrifice of quality. This receiver features a transformer operated power supply, high gain miniature tubes, sharply tuned IF transformers, new rod type built-in antenna, and a trouble-free planetary tuning system. Exceptional performance with unusually high sensitivity, good selectivity, and excellent tone quality from the 5½" PM chassis mounted speaker. Can be used either as a receiver, tuner, or phono amplifier. Uses 12BE6 mixer-oscillator, 12BA6 IF amplifier, 12AV6 detector, 12A6 beam power output, and 5Y3 rectifier.

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FOR GOLDEN EARS ONLY

The G-E Golden Treasure cartridge; RCA LC-1A and SL-12 loudspeakers; new records review

By MONITOR

WHEN introduced just after the war, the General Electric cartridge created a revolution. It is still the workhorse of high-fidelity, and deserves its popularity. So far as I can determine there is no difference between the Golden Treasure and the cheaper standard cartridge. It comes equipped with one or two diamond instead of sapphire needles. The needle mount is the new double-twist type with six damping elements.

Fig. 1 shows the response curve of the cartridge with the 1-mil needle to the Cook series 10LP test record with a 100,000-ohm load into a preamplifier flat within 1 db from 20 to 20,000 cycles.

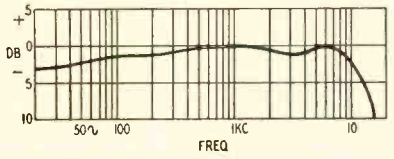

Fig. 1—Response of the G-E cartridge.

As the curve shows, the maximum departure is −2.5 db at 10,000 cycles and −3 db at 20 cycles and within 1.5 db between 100 and 9,000 cycles. Some of the departure is due to the test record and some to the preamp. I have obtained a similar slope beyond 10 kc with every G-E cartridge I have ever used.

Now this is very good indeed, particularly the absence of any peaks, and the slope beyond 10 kc is not as serious for most uses as it might appear. It takes a very sharp ear to discern the difference between the G-E with its slope and the Ferranti with its flat response to 20,000 cycles, and the difference is revealed not so much in direct loss of highs as in better definition and transient response. Part of the loss can be compensated for by placing a series resistance of about 500,000 ohms in the output of the preamp and shunting this resistance with a capacitor of between 50 and 500 $\mu\mu$f. The capacitor should be chosen by trial and error to produce the flattest curve beyond 10 kc without producing a peak or rising slope below 10 kc. By careful choice, it is possible to obtain a considerable improvement beyond 10 kc in this way. This method does produce reduced output below 10 kc but usually this loss is not important.

Hum pickup is sometimes a problem with the G-E cartridge as it is with all high-impedance low-level cartridges. The Baton pickup arm minimizes this. It has a twisted-pair cable running through the tube of the arm to the base, producing shielding with low capacitance. If a shielded lead is run from the base to the preamp and is well oriented, over-all hum is low enough to be completely tolerable.

In any case, the G-E cartridge produces excellent quality and, purely from a listening point of view, is pretty hard to beat when all things, including price, are considered.

RCA LC-1A and SL-12 loudspeakers

Dr. H. F. Olson of RCA has designed a series of interesting loudspeakers culminating in the LC-1A and the inexpensive SL series. The LC-1A (see photo) has found considerable use in broadcasting and recording studios as a monitor, but its high price has limited its use in home systems and relatively few audiophiles have had an opportunity to hear it. I was, therefore, very pleased when RCA made one available to me for testing.

In designing this series of speakers Dr. Olson has been less concerned with obtaining an extreme bandwidth than reducing distortion, producing a smooth response curve and obtaining a wide and more or less uniform angle of dispersion throughout the frequency range covered. The curves of Figs. 2, 3, 4, supplied by RCA with the speaker, indicate the degree to which these ideals have been approximated. I have no accurate way of checking them, but my tests, by instruments and ears, give me no reason to doubt or question them.

The response curve is unusually smooth for a loudspeaker, particularly in that it is remarkably free of steep peaks or dips. The distortion at any normal home listening level is well under 2% down to 60 cycles. The directional characteristics are extremely uniform to 7,000 cycles; above that the loss at wide angles off center is very slight.

The response at the high end falls off steeply beyond around 13,000 cycles and cuts off at around 17,000. The resonance in free space of the speaker I tested was around 45 cycles. In the Karlson enclosure the speaker produced a response with a very large component of fundamental down to 20 cycles. In a wall type infinite baffle the response was smooth to 35 cycles and sloped severely below that, cutting off at around 30 cycles.

Personal taste, prejudice and preference play a larger part in judging loudspeakers than any other portion of a hi-fi system. Moreover, loudspeakers are musical instruments in effect and almost all have a distinctive personal

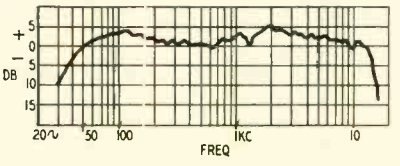

Fig. 2—Response of the LC-1A speaker.

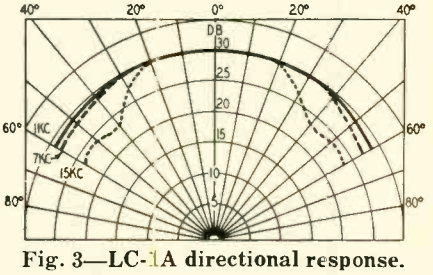

Fig. 3—LC-1A directional response.

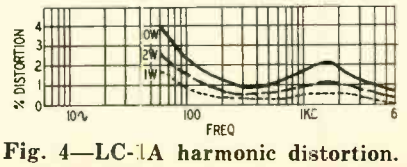

Fig. 4—LC-1A harmonic distortion.

The LC-1A duo-cone hi-fi loudspeaker.

SL-12 extended-range 12-inch speaker.

character and color. There is plenty of room for differences of opinion in judging them and it is dangerous to make categorical statements. Keeping all this in mind, I liked the sound produced by the LC-1A very much indeed. It was very clean, very smooth and personally I thought the balance between highs and lows and mid-range very fine, although it is possible that people accustomed to exaggerated highs or a higher proportion of distortion in the high end may think it is somewhat lacking in high-highs.

It also seemed to me that the LC-1A added less of its own character to the over-all sound than most speakers, and that it reproduced the most subtle differences between various amplifiers, pickups and recordings more clearly than most speakers. Some, no doubt, will like it more or less than others, but I think there is no doubt it is a great speaker and deserves its reputation.

The characteristics are the result of some very novel design features. The LC-1A is a duo-cone speaker. Both cones are independent and the cross-over is electrical. A real novelty is that the bass voice coil is used as the inductance in the crossover network. This requires a bigger and heavier voice coil than usual but the increased mass does not appear, to my ears, to have any significant effect on the audible performance. The transient response is very fine at all frequencies.

Another novelty is the use of a foam-rubber ring as a damping element on the outer edge of the cone. "This," to quote the specifications, "prevents reflections from the outer cone housing from combining with directly radiated sound to produce dips and peaks in the response." The smooth response curve appears to testify to its effectiveness.

Even more novel and certainly the most striking thing about this speaker are the "acoustic domes" cemented to the cone. Their purpose is to break up the symmetry of the cone at higher frequencies, minimize resonance and force the cone to act as a single stiff piston at low frequencies. Again, the smooth response seems to testify to the effectiveness of this novelty. Butterfly dispersing vanes are used on the high-frequency cone to obtain a wide angle of distribution, minimizing the hole-in-the-wall effect of sharply directive tweeters.

The LC-1A is supposed to be somewhat less efficient than comparable speakers of other makes. But I did not notice any difference and I found that the speaker will deliver all the volume any household can stand with less than 1 watt of electrical input and normal living room volume on less than 50 milliwatts. A commendable feature is that the LC-1A can be serviced, adjusted and repaired by a competent technician according to simple instructions which accompany the speaker.

The inexpensive SL-12 (see photo) which I was also able to test resembles the LC-1A only in the use of the foam-rubber damping ring. It is a single-cone radiator of conventional design. The speaker had a resonance of about 75 cycles. In the Karlson enclosure it produced excellent response down to around 35 cycles; in the infinite baffle, there was a severe slope below 50 cycles. To my ears the response seemed to slope upward at the high end, and cutoff occurred somewhere between 14,000 and 16,000 cycles. The reproduction is not in the same class as that of the LC-1A, but I found it excellent and entirely pleasing. The transient response was very good and, though as I have noted the high-highs seemed somewhat pre-emphasized as compared with the LC-1A, I found the response at normal listening levels smooth and the distortion commendably low. It offers a lot of quality and fidelity for its price.

New records

TCHAIKOVSKY: ***Symphony No. 5***
Stokowski and His Orchestra
RCA Victor LM 1780

RICHARD STRAUSS: ***Don Quixote***
Munch and Boston Symphony
RCA Victor LM 1781

Of these two discs, the Strauss is by far the more spectacular principally because the music offers more opportunity for hi-fi effects. Though the high-highs are not as magnificent as in some competing discs, they are very sharp and clean except in the crescendos where some distortion is audible. The balance between highs and lows seems quite natural. The solo cello passages are extremely good and the pizzicato measures are most natural. The definition is very fine and the over-all sound is stunning. The record would, therefore, make an excellent showoff or demonstration selection.

The Tchaikovsky at first sounds dull in contrast but this is because the music itself is more mellow and offers few openings for the high-highs to sparkle. The most encouraging thing to me was the quality of the bass on the first side.

The record has a fine rich sound which will be impressive to the layman who does not reject a record simply because it lacks spectacular highs. I can recommend it for demonstration and showoff in such cases. There is an amusing example of miking effects in the Third Movement when some kind of woodwind blows its nose right into one's face. The double basses on side A are notable in spots, particularly in the pizzicato passages. The highs are very clean and without any harsh sounds, though there are very few high-highs to demonstrate.

MOZART: ***Adagio and Rondo for Glass Harmonica (K617)***
Concerto for Flute and Harp (K299)
Andante for Flute and Orchestra (K315)
Pro Musica Chamber Orchestra of Vienna
Vox PL 8550

For years I have been looking for a record capable of offering a conclusive test for the masking effects of rumble, hum and other noises. This is very important because the dynamic range of a playback system is principally limited, not by its ability to reproduce the peaks, but its ability to reproduce perfectly the softest pianissimo passages. There are all sorts of records with very pianissimo passages, but they don't offer a clear and conclusive test. Here at last in the *Adagio and Rondo* is the perfect record for this purpose.

This was written originally for Ben Franklin's glass harmonica but since none are now in existence it is played here by the celeste. The celeste is an instrument of very low power output and high noise level — that is, the volume of the musical tones is so soft that the noises produced by the keys, hammers, fingers, etc., are clearly audible at close range. These noises are faithfully reproduced on this record even in the softest passages. The test, therefore, is very simple and foolproof: at the volume level normal for average listening in a specific room, all the noises should be completely audible without straining the ears or shoving the head into the speakers. With the best of today's turntables, pickups, preamps, etc., they will be; but any significant hum, rumble, hiss or scratch will mask the noises seriously. Aside from this specific quality, this is a wonderful disc for demonstrating the high end. The tones of the celeste are beautifully clear and clean, and the music is so lovely that it is likely to produce a favorable reaction in all listeners.

Soft Light Music: **The Club Orchestra**
Vox VX 580 (10 inch)

Here is a recording of popular music nearly on a par in hi-fi quality with symphonic works. The music is typical supper music. It involves strings, electronic organ, guitar, harp and percussives. The high-highs of the brushed cymbals are nicely prominent, the bass good though not sensational, the balance excellent. There is enough room res-

onance to produce an intimate effect of presence. There are only slight touches of distortion in the peaks. The record should make any system sound good to those who prefer popular music.

***Echoes of Broadway*: George Fever, piano with rhythm accompaniment**
Vox VX 650 (10-inch)

Though not as varied in the quality of the sound as *Soft Light Music*, this will also make a good showoff record. Nor are the high-highs as prominent, but the piano is excellent. Again a slight touch of distortion on the peaks, but far superior to the average pops.

***Millstein Recital*: Improvisations on and excerpts from violin works of Pergolesi, Schumann, Brahms, Suk, Bloch and Paganini.**
Nathan Millstein with piano accompaniment. Capitol 8259

The violin can sound more spectacularily natural and present on a fine system than any other instrument. This recording is exceptional in this respect and offers, in addition, some really remarkable fiddling by one of the great virtuosi of the day. On the best systems Millstein will appear to be in the same room. The tone and subtle coloration of the violin, as well as the very wide range of tone coloring of which it is capable in fine hands, are very well recorded. The odd harmonics are the dominant ones in the violin and the rather rough, biting quality which this imparts to the violin comes through with great naturalness. The definition is excellent and the violinists and critics who listen to this will clearly appreciate the wizardry of Millstein's playing for the simple reason that even the most complex effects are clearly audible.

HARL MacDONALD: *Suite from Childhood*
ANDRE CAPLET: *The Red Mask of Death*
Anne Mason Stockton, harp, and Concert Arts Orchestra Capitol 8255

Pleasant and, in portions, brilliant music for showoff, particularly on the MacDonald side which is based on familiar childhood tunes. Both sides present a very fine recording of the harp, full of nice transients. The pianissimo passages are good for checking hum and rumble.

BARTOK: *Piano Concerto No. 3*
PROKOFIEFF: *Piano Concerto No. 3*
Leonard Pennario and St. Louis Symphony Capitol P8253

The music will interest the most advanced listeners most; but portions of this are notable for hi-fi quality. The opening of the Bartok, for example, has some excellent double bass. The piano tone is fine and very individual in its dryness. Occasional bursts of triangles and sharply muted brasses establish high-frequency response. The polyphonic writing provides good measures for definition. Over-all sound is very impressive and the recording is very clean. END

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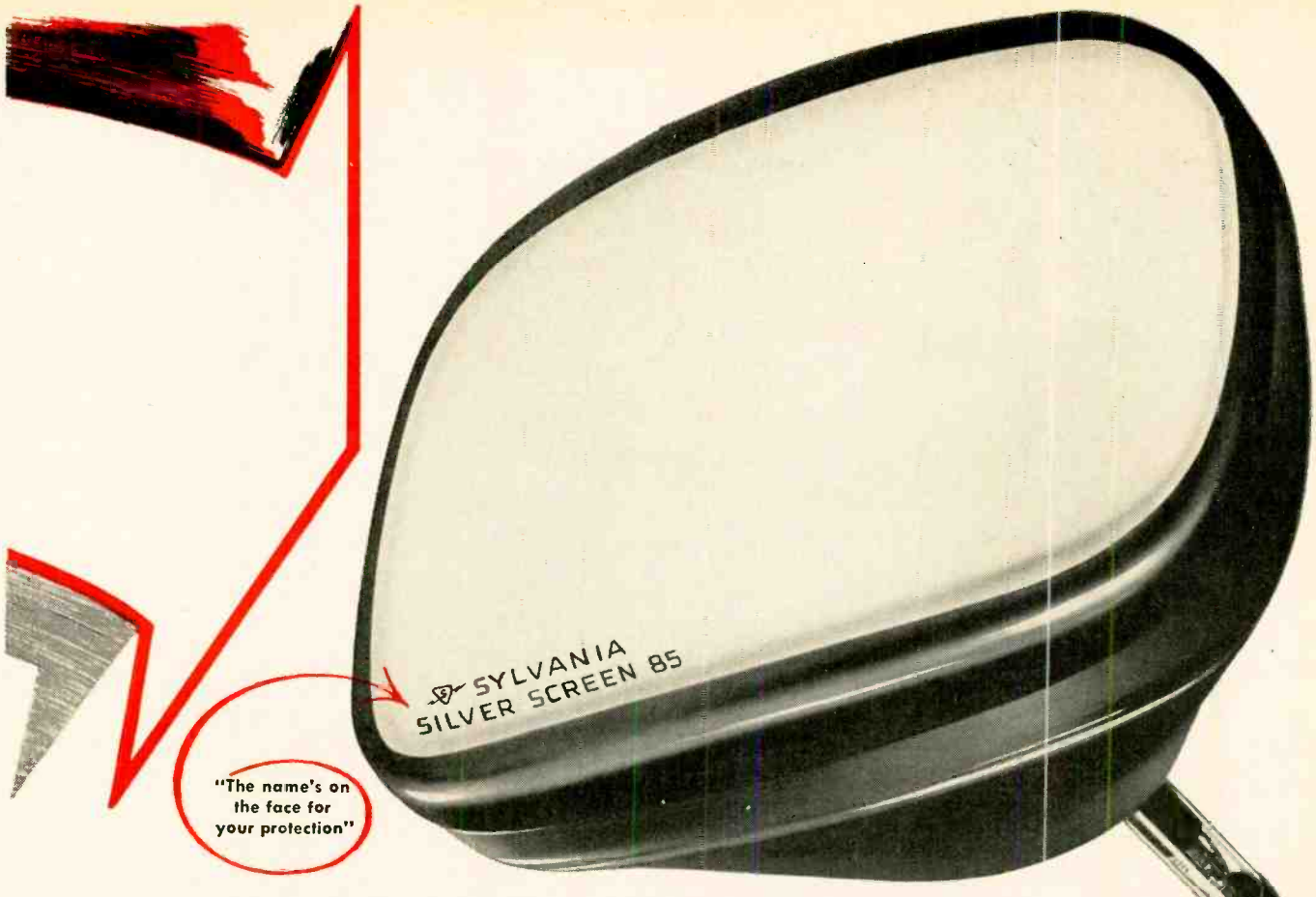

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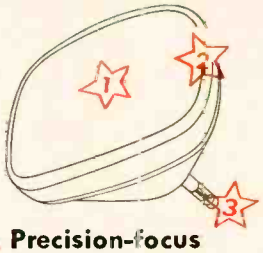

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By ALBERT STRATMOEN

ANYONE interested in constructing audio equipment will find this amplifier easy to build. It requires few shielded leads and a minimum of stages because of the mixing system used. Distortion is low, due partly to the inverter used and to the stabilizing of the output tubes' screen voltage. Also included are features that will appeal to professionals, such as a built-in output meter, headphone jack with volume control and plenty of output terminals.

For each input channel (see diagram) there is only one stage, a 6J7, whose gain is controlled by adjusting the cathode voltage. The plates of all four input tubes are connected together and the mixed output is fed to the second stage, a 6SJ7, through a volume control used as the master gain control. The 6SN7 phase inverter is conventional except for its adjustable feature and drives the 6L6 output tubes, delivering 16 watts in the voice coil at 0.7% distortion. A type 79 is used as a voltage stabilizer, controlling the screen voltage of the 6L6's and, to a lesser degree, their cathode voltage. The 79 and 6Y7-G are not common types today but I used them because their high plate dissipation and amplification factors are ideally suited to the application. Other twin triodes such as the 6N7 and 6J6 are unsatisfactory in this particular amplifier circuit.

The most popular tubes for low-level audio work are probably 6J7's, usually operated with fixed bias. They are sharp cutoff tubes; but if the screen voltage is allowed to rise with increasing cathode voltage, they act like remote cutoff types. If only a series resistor were used, there would be almost no gain variation but in this circuit R3 permits it to rise only moderately. The change in bias is obtained from R2, some additional voltage being obtained from the plate supply through R4. The bias is prevented by R1 from becoming too low at maximum gain setting. Linear wirewound controls are used and the attenuation is more rapid at low settings, the rate of change becoming progressively less toward maximum gain. The scales for these controls are those furnished with Daven LA350 attenuators and are linear, so they are only approximately correct. Tapered carbon controls, such as IRC F taper, would provide a much more linear attenuation.

Due to a peculiarity of pentode tubes (plate current is practically independent of the plate voltage), it is possible to use a common plate resistor, R5. The settings of the gain controls of all four input tubes affect the plate voltage, causing it to vary widely. This would cause serious interaction if the tubes were triodes, but with pentodes it is very slight. It could be eliminated entirely by using separate resistors and blocking capacitors for each channel. Because the plate resistance of pentodes

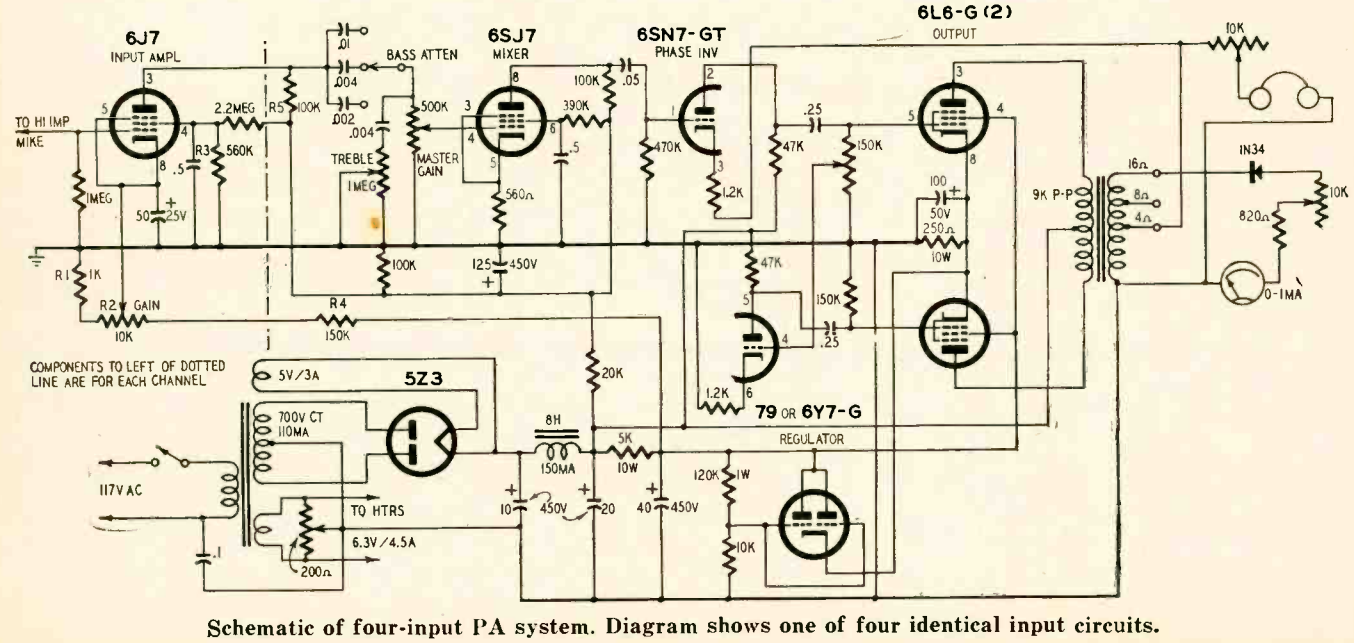
Parts for four-input amplifier

Resistors: 1—560, 1—820, 4—1,000, 2—1,200, 1—10,000, 1—20,000, 2—47,000, 3—100,000, 2—150,000, 1—390,000, 1—470,000, 4—560,000, 4—1 megohm, 4—2.2 megohms, ½ watt; 1—120,000, 1 watt; 1—250, 1—5,000, 10 watts.

Potentiometers: 1—200, wirewound; 4—10,000, F taper; 2—10,000, wirewound; 1—150,000; 1—500,000, audio taper; 1—1 megohm, carbon.

Capacitors: 1—.002 μf, 2—.004 μf, 1—.01 μf, 1—.05 μf, 1—0.1 μf, 2—0.25 μf, 600 volts, paper; 5—0.5 μf, 400 volts, paper; 1—10 μf, 1—20 μf, 1—40 μf, 1—125 μf, 450 volts, electrolytic; 4—50 μf, 25 volts, electrolytic; 1—100 μf, 50 volts, electrolytic.

Miscellaneous: 4—6J7, 1—6SJ7, 1—6SN7-GT, 2—6L6-G, 1—5Z3, 1—79, tubes; 8—octal sockets; 1—4-prong socket; 1—6-prong socket; 4—grid shields; 4—small grid clips; 1—large grid clip; 1—power transformer, 700 volts c.t. @ 110 ma, 6.3 volts @ 4.5 amp, 5 volts @ 3 amp; 1—filter choke, 8 h @ 150 ma; 1—meter, 1 ma d.c.; 1—output transformer, primary 9,000 ohms c.t., secondary 4, 8, 16 ohms, potted (Acrosound TO-280); 1—2 feet of shielded grid wire; 1—IN34; 1—single-pole 3-position switch; 1—s.p.s.t. switch; 1—phone jack; 4—input jacks; 1—4-terminal barrier strip; 1—chassis



Schematic of four-input PA system. Diagram shows one of four identical input circuits.

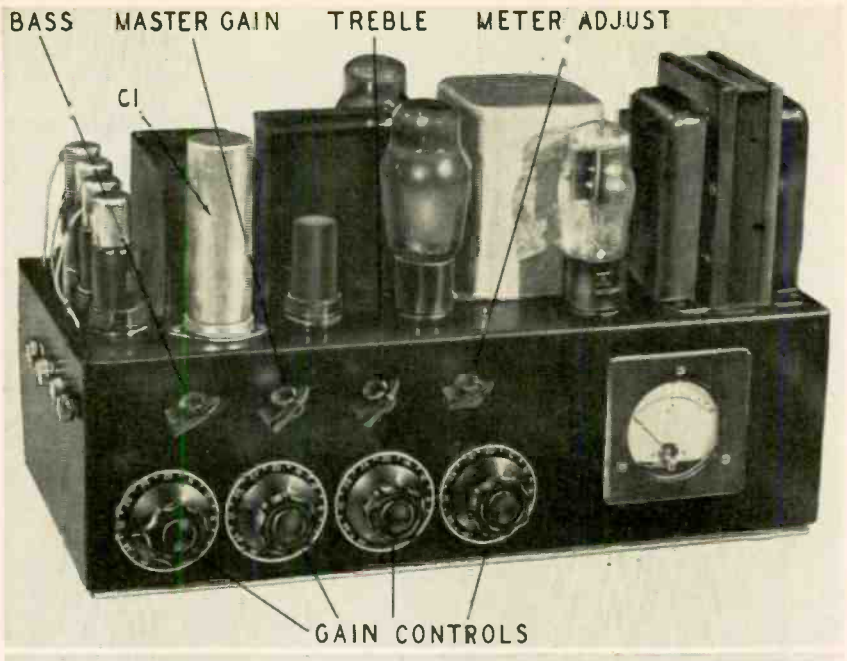
is much greater than the recommended load resistance, one tube will not act as a load on another, and so the gain remains independent on the number of channels used.

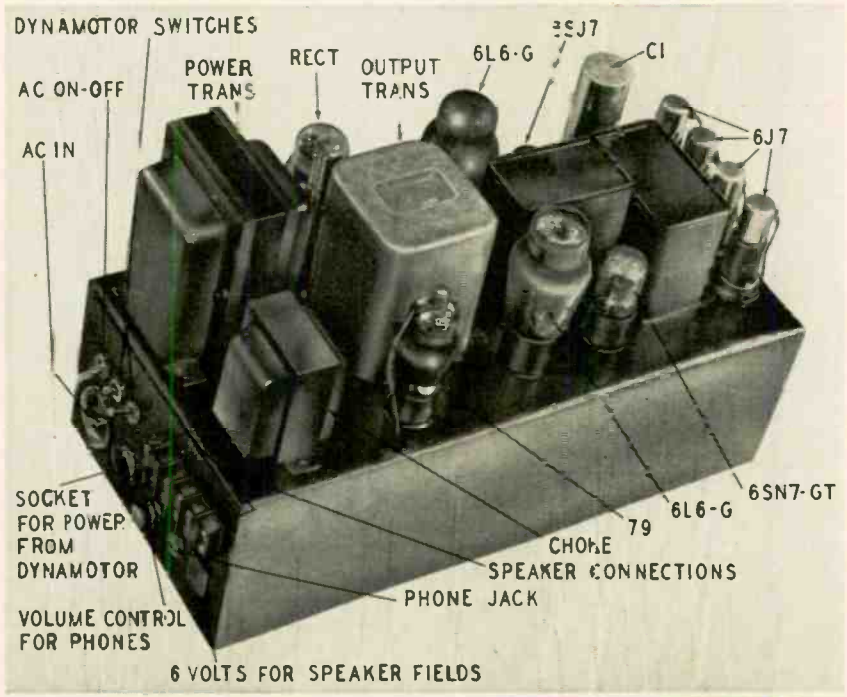
The over-all sensitivity can be varied by changing the value of the common plate resistor. Using a 100,000-ohm resistor an input voltage of 4 mv drives the amplifier to full output—16 volts across a 16-ohm load. Increasing the resistance increases the sensitivity and vice versa. But it should not be made too low as the gain controls would lose their effectiveness. It is not necessary to make any changes in the cathode or screen circuits when changing sensitivity by this method.

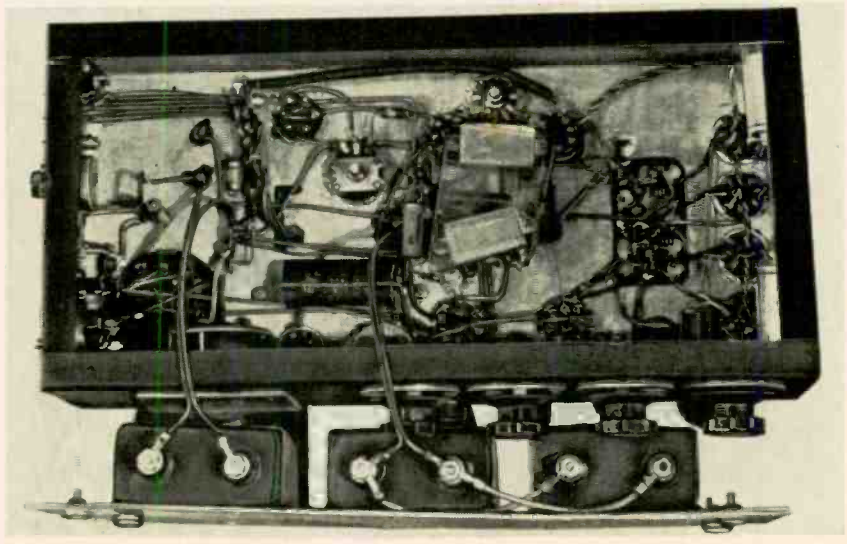
This system of gain control lends itself to remote operation, and could be used in home music amplifiers. For best fidelity the gain variations in the first stage should be minimized, using the master control to set the approximate level. A 20-db range is permissible if the signal level is less than 15 mv. Large signals cause rectification at low gain settings and therefore harmonic distortion. If these suggestions are followed, the maximum increase in harmonic distortion will be about 0.25%.

The phase-inverter circuit used has been the target for a lot of adverse criticism, chiefly because it is not self-balancing. The balance depends on feeding just the right voltage to the second tube, and that depends on the ratio of the resistors in the grid circuit of the following stage. But even such circuits as the phase splitter do not insure perfect balance where it counts—in the plate circuit of the output tubes. Mismatched tubes or an imperfectly balanced output transformer would produce harmonic distortion. By making the inverted voltage variable, the disadvantage of this circuit becomes an advantage.

A low-distortion oscillator and a distortion meter are needed to adjust the inverter. These were scarce articles a few years ago, but since the FCC now requires yearly proof-of-performance tests by broadcast stations they have become plentiful. Radio engineers being a kindly lot, probably the local station will permit you to use its equipment. If not, set the resistance for about 17,000 ohms to ground and you will not be far off. A frequency of about 200 cycles is best as the balance changes with frequency and this value gives the best compromise. The distortion goes down to about 0.4% at the balance frequency but increases as the frequency is changed.







Top—Front view of the amplifier. Type 82 rectifier has been replaced by a 5Z3. Center—Rear view showing all major components. Two toggle switches and octal and Jones connectors are for dynamotor operation and are not discussed or shown in diagram. Bottom—An underchassis view. Oil-filled capacitors on chassis coverplate parallel others to form some of the capacitance values specified on the schematic.

AUDIO—HIGH FIDELITY

The type 79 stabilizer tube takes the place of two voltage-regulator tubes but has the disadvantage that it requires heater current. It cuts off at high signal levels though, so it is more economical as far as d.c. power is concerned. It is operated at about zero bias and draws 10 milliamperes at no signal. As the signal is increased the screen current of the 6L6's increases, resulting in lower screen voltage. This increases the bias on the 79 and its plate current falls, thus tending to keep the screen voltage constant. At the same time the cathode voltage of the 6L6's rises due to an increase in plate current. This also increases the bias on the 79 and thus stabilizes the screen voltage.

Because the increase in screen current comes from the plate current of the 79, the current through the cathode resistor is more nearly constant so some cathode voltage stabilization results too. The cutoff occurs at about 18 watts output; above this level no further regulation is possible. The effect of the stabilizer tube is to increase both gain and fidelity.

It is common practice to connect the chassis to both sides of the a.c. line through capacitors. This places the chassis midway between line voltage and ground. Less hum results if only one capacitor is used and the a.c. plug is inserted the way that causes the least hum.

The tone controls provide attenuation of either highs or lows or both. The bass attenuation is obtained by decreasing the size of the blocking capacitors. This method does not give continuous control but does produce a desirable attenuation curve. The smallest capacitor is for use with speakers having a high cutoff frequency or for setups where a high-pitched output helps to overcome noise. It is best to reduce the master gain when changing the bass response, otherwise a definite thud will be heard. (Resistors of several megohms from each of the switch contacts to chassis will minimize this condition.—*Editor*) To use the amplifier for high-quality music a fourth tap should be added with an .05-μf capacitor. This will extend the response to much lower frequencies.

The potentiometer across the heater supply balances out hum. It should be adjusted with one channel and the master gain on full. If 6SJ7's are used, this adjustment is very necessary as these are inferior to 6J7's both as to hum and microphonics. It is necessary to use shields over the grid caps, especially if the amplifier is not shielded.

The output meter enables the operator to maintain a constant level. Thus the scale used isn't very important. The meter shown in the photo has two scales, one linear and the other calibrated in db. The db calibration is useful on a sound truck in areas having ordinances specifying the maximum audio level. Of course, the sound level would also depend on the efficiency of

the speakers. The meter is mounted on the inside of the chassis and a piece of plexiglas on the outside protects the glass.

Because oil capacitors are used, the chassis size (8 x 17 x 5 inches) is rather large. It is constructed of 20-gauge galvanized iron. Two oil capacitors were soldered on before it was painted. Because paint often does not adhere well to galvanized iron, other constructors may prefer using electrolytic capacitors and a smaller, standard-size chassis. The oil-capacitor block, obtained from a type C1 Autopilot amplifier, is very convenient to mount resistors on and reduces congestion around the front end of the chassis. The extra-large decoupling capacitor C1 costs only about a dollar more than a 40-μf unit and greatly reduces hum. If you want to extend the low-frequency response, this capacitor will help prevent motorboating at extremely low frequencies. The Acrosound transformer seems to have a healthy output down to 2 or 3 cycles and it takes a large capacitor to be effective at that frequency.

The headphone circuit is intended for 500-ohm war-surplus phones. If high-impedance phones are used, it may be necessary to use a higher resistance control and to obtain the voltage from the 16-ohm tap.

Performance of the amplifier is good although the power output is a little low, perhaps because the output transformer is designed for fidelity rather than efficiency. Up to 16 watts the distortion does not exceed 0.7% from 50 to 7,500 cycles. At 20 watts, distortion is 5% or more; a relatively low percentage.

With all gain controls at minimum, the noise level is 70 db below 16 watts. With the master gain on full but all channels off, the level is 60 db down. With one channel wide open, it is 50 db. This is definitely audible but not annoying: it is a rushing sound originating in the grid resistor of the first stage. Any low-resistance input source, such as a dynamic microphone or a magnetic cartridge, would reduce this noise by shorting out the grid resistor. If a crystal pickup is used, it could be connected to the top of the master gain control. A more satisfactory method would be to use a voltage divider to cut its output to 6 or 8 millivolts and use it on one of the microphone channels.

Feedback howl is one of the sound man's greatest problems. The most important factor causing this is a peak in the response from microphone to room acoustics. A high-fidelity amplifier with a lot of feedback from the speaker voice coils will not only be peak-free itself but will correct the speakers, reducing their peaks. This will permit a higher usable sound output. Good-quality cardioid type microphones and careful speaker placement will complete a satisfactory sound installation. END

AUDIO—HIGH FIDELITY

ELECTROSTATIC TWEETER

By MARVIN HOBBS*

THE new low-voltage electrostatic speakers now used in some sets (see "New Electrostatic Speakers" in the October 1954 issue) are usually connected to the plate of one of the output tubes through a high-pass dividing network. This connection is impractical for home audio enthusiasts who may wish to add one or more electrostatic tweeters to their existing system. There is the danger of postive feedback resulting from coupling between the amplifier input and the tweeter and its coupling network. Too, there is a considerable variation in the d.c. voltage available at the plates of output tubes in popular equipment. A further disadvantage is that the speaker does not receive full

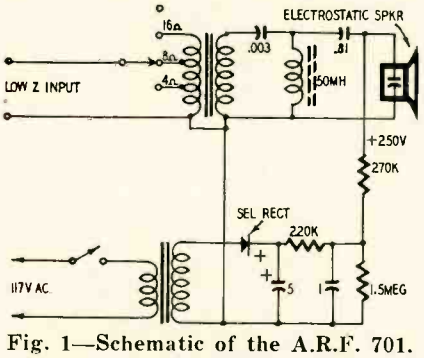


Fig. 1—Schematic of the A.R.F. 701.

benefit of the even-harmonic cancellation characteristic of the push-pull output circuit.

To minimize these effects in adapting electrostatic tweeters to existing equipment, A.R.F. Products has introduced the series 701 and 702 electrostatic tweeters with built-in power supply and low-impedance input. Fig. 1 shows the circuit of the 701, a single-tweeter unit, with crossover around 6 kc. Audio for the tweeter is taken from the *secondary* of the amplifier's output transformer. A step-up transformer in the tweeter package matches a 4-, 8- or 16-ohm input and develops the maximum drive of about 60 volts r.m.s. in the range of 7 to 20 kc. Polarizing voltage—about 250 d.c.—is supplied by a small power transformer and rectifier. Fig. 2 shows the chassis of the model 702, using dual electrostatic tweeters.

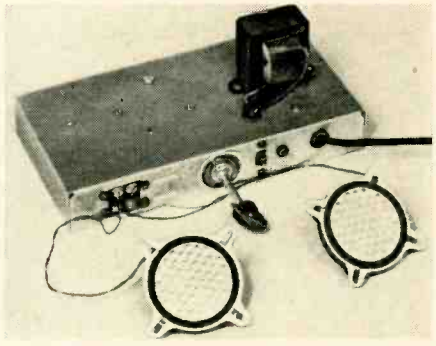


Fig. 2—The 702 using dual tweeters.

The electrostatic tweeters are flat with an area of approximately 8.5 square inches each. They may be used with any amplifier delivering up to 10 watts. The response of the tweeters is flat within 3 db from 7,000 to 20,000 cycles.

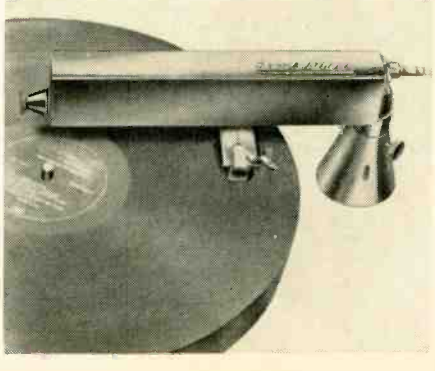
The single- and dual-tweeter packages are supplied with matching transformer and crossover network. Both are available with and without polarizing supply and cabinet. The speaker in the 701 is tilted from the vertical in its cabinet to increase high-frequency distribution when placed atop a low-frequency enclosure of medium height. In the 702 the tweeters are also set at slight angles to the front to increase the horizontal spread. END

*Consulting Engineer, A.R.F. Products

CONSTANT-TRACKING PLAYBACK ARM

A new and revolutionary playback tone arm resembling an overhead drive recording lathe is a recent development of Kral Products, of Philadelphia, Pa. Called the *Trans Linear*, the new arm continually follows the tracking angle of the recorder, thereby eliminating tracking distortion on playback.

Available in 12- and 16-inch models, the arm is easily installed on any turntable. Height, stylus pressure and leveling adjustments are simple. Standard cartridges like the Fairchild, G-E and Pickering are simply slipped into place and clamped with a thumb lock. A calibrated indexing strip may be fastened to the front of the housing to simplify pin-point positioning of the stylus in any band or groove on the record. Accidental damage to the record or stylus in the play and off positions is prevented by a safety lock. The arm swings to one side for easy record placement and removal.



GILDING THE GOLDEN EARS

Improving the performance of the Junior and Milady's Golden Ear amplifiers

By JOSEPH MARSHALL

ANY design is capable of improvement and Golden Ear amplifiers are no exceptions. The original articles in RADIO-ELECTRONICS produced an unusually large number of letters with comments and reports from readers who either had constructed a Golden Ear amplifier or were doing so. A few letters reported troubles, a very large number reported happy results, and some suggested improvements or modifications. Inspired by this interest I have been doing a great deal more work with and made several improvements in the circuit. Some of these were included in "Milady's Golden Ear" (April, 1954) and others will be found in a new laboratory model which I hope to describe in this magazine shortly. Meanwhile, it seemed appropriate to report on the improvements and how they can be applied to existing Golden Ears.

Outer Feedback Loop

Several correspondents noted that there was a limit to the improvement in reducing distortion which could be obtained by increasing feedback in the outer loop. In most cases applying 14 db or a little more in the outer loop, in addition to the 14 db in the inner loop, produced a reduction in distortion. But in some instances, an increase beyond 14 db did not produce any further improvement and sometimes even increased distortion. There are two reasons for this and two cures.

In the original design the outer loop applied feedback from the voice coil of the output transformer to one of the cathodes of the input pair of cathode followers. This places the feedback resistor and the voice coil in shunt with the cathode resistor and, therefore, reduces the net or effective cathode resistance. This produces unbalance. The unbalance can be corrected by the balance control. However, the size of the feedback resistor decreases as feedback is increased. If the resistor is too small, the cathode resistance of the input tube is reduced to the point that the tube is underbiased. This is not likely to occur with the Junior version (November, 1953) which takes feedback from a 500-ohm tap and therefore uses a high value of feedback resistor. But when a 16- or 8-ohm tap is used, the feedback resistor may be as low as 10,000 ohms and even less; and this does throw the input stage out of its normal bias range.

There is a very simple solution. Feedback can be applied to the grid of the bottom tube—the off-grid—through a voltage divider as indicated in Figs. 1, 2. This way the feedback network has no influence whatever on the static values of the input stages. The voltage fed back must be *in phase* with the signal, rather than out of phase as is the case with normal types of feedback. The feedback action here is obtained through the fact that the inverter is a differential amplifier. When in-phase signals of the same frequency are fed into both grids, the weaker subtracts from the stronger; if both are equal, they cancel each other out completely.

When an amplifier is wired, there is a 50–50 chance that the voltage from the top end of the voice coil will be in phase. If it is, feedback will be negative. This will be evidenced by lower volume or output level. If the applied signal is out of phase, you will get positive feedback, evidenced by a rise in volume or, more probably, motorboating. When this occurs, the phase must be reversed. The easiest way to do this is to reverse the input grids. Phase can also be reversed by reversing the primary leads on the output transformer but it is usually simpler to reverse the input grids.

The values specified in the diagrams were suggested by Dave Hafler of Acrosound—who first applied this scheme after mutual discussion—and work very well. There is no reason to suppose, however, that other values wouldn't work as well. To determine the optimum value of feedback resistor the following is recommended:

Connect temporarily a potentiometer of around 10,000 ohms (for 8- or 16-ohm voice coils) or 25,000 ohms maximum for 500-ohm voice coils as a feedback control. Apply a resistive load or, if you must use a speaker load, disconnect the tweeters. Adjust the potentiometer downward until the amplifier breaks into parasitic oscillation. This condition can be determined by hooking up the a.c. probe of a v.t.v.m. across the voice coil. Adjust any signal input to produce say a 1-volt reading on the v.t.v.m. Now reduce the value of the potentiometer resistance. The

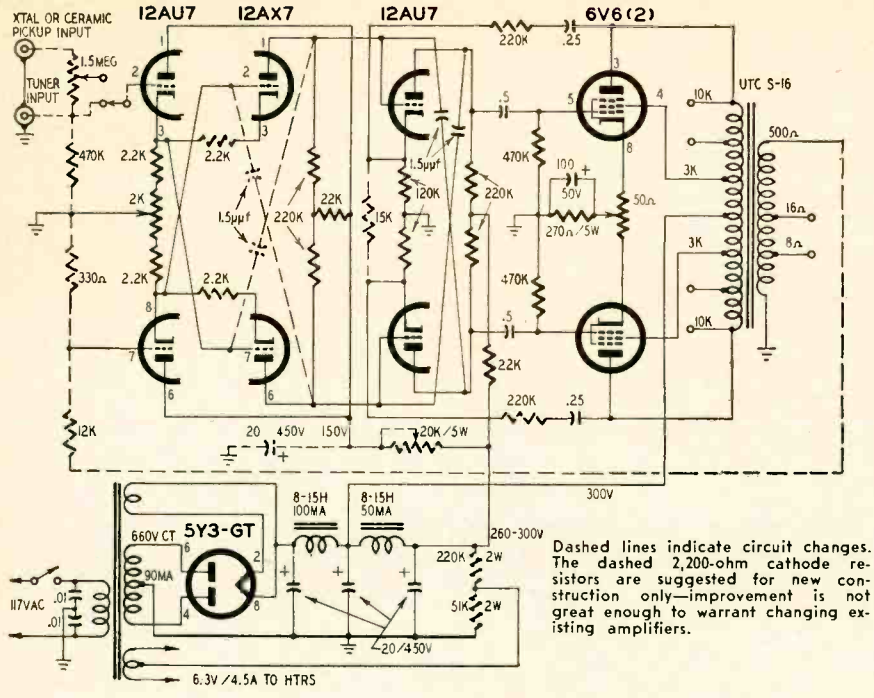


Fig. 1—Schematic diagram of the revised Junior Golden Ear amplifier.

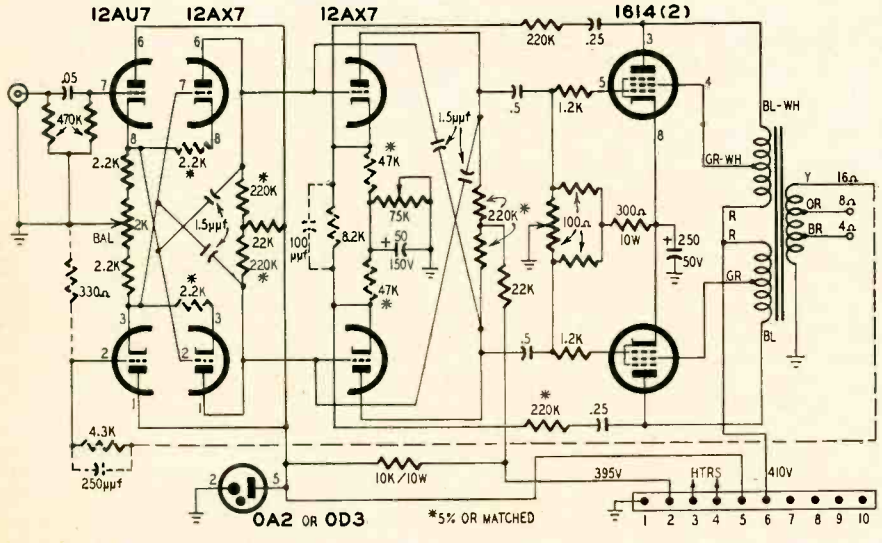


Fig. 2—Schematic diagram of the improved Milady's Golden Ear amplifier.

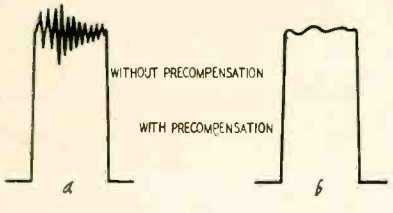


Fig. 3—Checking feedback phase shift.

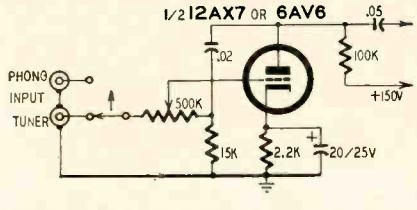


Fig. 4—Hi-fi ceramic pickup equalizer.

reading on the v.t.v.m. will decrease to a point and then it will either rise violently, which will indicate ultrasonic oscillation, or oscillate slowly, indicating subsonic oscillation. Now back off until the oscillation ceases. To be absolutely sure of stability, you can leave the v.t.v.m. connected while playing a few records. If the needle of the meter doesn't take a sudden rise and does not begin to oscillate, the feedback is O.K. If oscillation is produced, however, by a sudden shock or peak input, back off a little more and try again. Measure the used portion of the potentiometer and wire in a resistor of about the same, but not lower, value.

Any Golden Ear should take 14 db or a little more with no sign of instability. This will be provided by a resistor of around 4,300 to 4,700 ohms with a 16-ohm voice coil. Under no circumstances try this procedure with the tweeters connected to the amplifier —the oscillation may burn them out.

Increasing gain of Junior Golden Ear

I have already confessed (in the article describing Milady's Golden Ear) that I deliberately held down the gain of the Junior Golden Ear amplifier in favor of a large amount of current feedback to raise the high-frequency response. I reasoned that most people, and certainly my sister for whom the amplifier was originally designed, never used more than 500 milliwatts of output. It turned out that many readers wanted 6 to 8 watts with a reasonable input voltage. There are several ways in which the gain can be increased and of these I recommend two.

The first requires no change in tubes and only a slight change in circuit (Fig. 1). The principal changes from the original circuit are: shunting the cathodes of the 12AU7 drivers with a 15,000-ohm resistor, reducing current feedback to 6 db; and reducing the value of the feedback resistors in the inner loop to 220,000 ohms. The feedback capacitors remain the same. This combination produces about 14 db of feedback. The bass boost is increased and therefore the phase shift is even more compensated. As a result the new version is even flatter at the low end. Indeed, the 20-cycle square-wave response will astonish anyone who sees it and notes the size of the output transformer producing it. I have also included the new outer feedback loop in this new version.

In the original Junior a bleeder was used in the power supply to reduce voltages for the input stages. This bleeder increased the current drain and heating. The new version uses a simple series dropping resistor and a high-resistance divider for the filament biasing. Some would like to add a VR tube for decoupling. This is easily done by replacing the capacitor with a VR tube (Fig. 2).

Even greater sensitivity is possible by using a 12AX7 or 6SL7 driver instead of the 12AU7 or 6SN7. This is the same front end used in Milady and now standard for all Golden Ears. In the new version the inverter tube, as well as the driver, is neutralized. This improves the high-frequency response.

Many readers have asked if the UTC S-16 transformer which is larger and has a 30% ratio of primary taps wouldn't be a better choice than the S-15 originally specified. The answer is yes; but the S-15 works fine. The Acrosound TO-310 can also be used. The only change will be in the feedback resistor of the outer loop, which should be around 4,300 ohms, from the 16-ohm terminal.

If you want to use a loudness control with these more sensitive versions, the Centralab Senior Compentrol is recom-

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300 ohm impedance for 100% signal transfer.

Highest Front-to-Back Ratio ever in Broad Band design

Chan.	DB	Rel. Volt.
2	17.	7:1
3	22.	12.5:1
4	21.	11.5:1
5	20.	10:1
6	20.	10:1
7	10.5	3.5:1

Chan.	DB	Rel. Volt.
8	18.	8:1
9	19.	9:1
10	25.	18:1
11	22.	12.5:1
12	25.	18:1
13	13.	4.5:1

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Current Distribution (Channels 2-6)

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Full sized low band half wave folded dipole develops maximum in-phase current across its length on low band channels 2 to 6. Entire dipole length acts as effective capturing device because it operates totally on fundamental frequency unimpeded by additional radiating devices used in other broad band systems to raise high band gain.

Current Distribution (Channels 7-13) Without Helix

ON HIGH BAND

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Current Distribution resulting from connection of Helix (channels 7-13)

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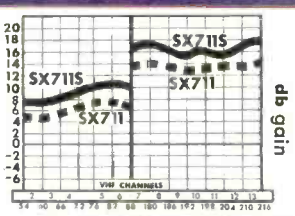
	ANTENNA	CHANNELS 2	3	4	5	6	7	8	9	10	11	12	13
	"STAR-HELIX" SX711	4.75	5.	6.25	7.25	7.	14.5	14.	13.25	13.5	13.75	13.75	14.5
	"STAR-HELIX" SX711S	8.	8.5	9.	10.5	10.5	17.5	17.	15.75	16.	16.	16.	17.5
	"DODO" Screen Type REFLECTOR	4.75	4.5	7.2	7.1	7	11.	11.2	11.8	11.5	11.1	12.1	12.
	"SUPER DODO" Screen Type REFLECTOR	6.3	6.8	8.8	7.8	7.5	9.5	11.2	11.8	12.	11.1	12.1	12.
	Broad Band Yagi with Phasing Stubs	4.3	5.7	4.5	7.1	9.	13.	14.	13.5	14.	13.	14.	15.
	Inline Yagi with Phasing Stubs	5.2	5.5	6	8.	8.	11.5	9.5	10.	9.	11.	11.5	11.8
	Inline Yagi with Triple Dipole	5.25	6.25	7.	7.5	7.75	10.5	10.25	8.75	9.5	10.25	11.	11.75
	Super Inline Yagi with Triple Dipole	6.75	7	9.2	9.	10.	11.5	12.2	12.8	13.5	13.1	14.6	15.5

65.6% S/N Figure of Merit*

**The S/N Figure of Merit sums up the major individual characteristics of an antenna in one concise value. Write for S/N Figure of Merit engineering folder No. 315 for complete details.*

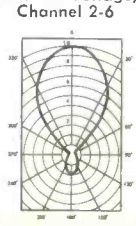
Gain Represents That Over ½ Wave Reference Folded Dipole



Up to 18 db on High Band* **Up to 11 db on Low Band***

*Tested in strict accordance with RETMA antenna measuring standards

Horizontal Pattern (Relative Voltage) Channel 2-6



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mended. The gain is so much higher that the input signal may well have to be cut to one-half or less. This might produce too much boosting of highs or lows with the Junior Compentrol. The Senior Compentrol allows adjustment of both level and compensation.

If you now have an amplifier using pentode-connected 6V6's, 6K6's or 6L6's, or an output transformer which does not have taps for Ultra-Linear operation, the circuit is easily modified. The only change is that of providing proper screen voltage. Since in most cases the screens can operate with the same voltages as the plates, connecting the screens to the center tap of the transformer primary will be O.K. Otherwise the circuit remains unchanged.

Extending high-frequency response

In Milady's Golden Ear and other versions using Acrosound output transformers flat to about 100 kc and having resonant peaks between 120 and 200 kc, the amount of feedback possible in the outer loop is limited by the phase shift in the ultrasonic region; after a certain point the amplifier bursts into oscillation. Moreover, even when outright and continuous oscillation does not occur, the transient response suffers. A 20-kc square wave may have very steep sides but the top, instead of being flat, may be extremely unstable (Fig. 3-a). The cure for this is to reduce the phase shift at the high end so that even at the resonant frequency it is less than 180°. A common way is to build a phase-shift network into the feedback loop by shunting the feedback resistor with a suitable capacitor, as indicated in the feedback loop of Fig. 2.

The exact value of this capacitor will vary with the circumstances and the transformer. With most Acrosound transformers a combination of R-C having a constant of 10 microseconds will do the job. This will be achieved if the resistance of the feedback resistor in *ohms* and the capacitance in *microfarads* produce the product 1. For example, a 4,700-ohm resistor will need a capacitor of about .0002 μf; a 4,000-ohm resistor, .00025 μf, and a 3,000-ohm resistor, .00033 μf.

A more exact correction can be obtained with the help of a scope and a 10-kc or 20-kc square wave. The scope will show, not a flat top, but one with a great deal of wiggle. Try various capacitances across the feedback resistor and choose the one which produces the flattest top and the least wiggle.

This measure is not always fully effective, especially if a large amount of feedback is desired. The Golden Ear circuit however produces a unique opportunity for a further improvement by precompensating the phase shift at the high end. All that is necessary is a small capacitance from cathode to cathode of the driver stage. Here is how it works:

AUDIO—HIGH FIDELITY

The capacitor shunts the feedback loop and therefore limits the feedback. But the shunt varies with frequency. At low frequencies the reactance is so high that it has little or no shunting effect; but at very high frequencies the reactance may be so low that the feedback loop is completely shorted out and gain at these frequencies is increased by up to 20 db. By choosing the right value it is possible to taper the feedback beyond, let us say, 50 kc, thus increasing gain beyond this point rapidly. The increase in gain slows the phase shift so that whereas previously it may have been 180° at 150 kc, it may now be much less—enough less to prevent positive feedback.

Here, too, the best way of proportioning this compensation is with a scope and a 20-kc square wave, choosing the capacitor which either eliminates ringing entirely or minimizes it most completely. I have not yet determined optimum values, but a value of around 100 $\mu\mu$f appears to be a good average for Golden Ears using the Acrosound T-300 transformer and between 16 and 20 db of feedback in the outer loop. Fig. 3-b shows the improvement produced by the combination of these two means in the revised circuit of Milady (Fig. 2), with 20 db feedback in the outer loop in addition to the 14 db in the inner loop.

Adjusting balance

In my experiments I discovered a most effective method of adjusting amplifier balance precisely. It involves the use of an IM analyzer or meter. Adjust the balance roughly by the usual means. Set up the IM analyzer and take an IM reading at about 1 watt. Now adjust the balance control carefully on both sides of the rough balance position for minimum reading on the IM meter. You will find the IM falls as the balance control is moved to one end or the other. However, if you switch to the *carrier set* position of the analyzer, you will see that the output has fallen. The correct minimum is somewhere near mid-rotation and will provide a distinct improvement in IM with no decrease—or even with an increase—in output.

This method can produce an almost perfect balance and can reduce distortion to one-half, one-third or even less.

The IM meter can also be used the same way for adjusting the bias of the 12AX7 driver in Milady's Golden Ear or others using the same front end. This time, however, take an IM reading close to maximum output and then adjust bias for minimum IM.

Modifying Williamson kits

Several correspondents have pointed out that Williamson type kits are available at prices 50% or less than the cost of parts for Milady and have asked if such kits could be modified. The answer is yes and usually very easily. Aside from the fact that a couple of

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tubes, some resistors and capacitors may have to be bought, the main problem is to find space and provide holes for two more tubes. The two-chassis versions of the Williamson kit have an additional hole on each chassis to take interconnecting plugs. These holes can be used for tube sockets and the interconnecting cable run through grommet-lined holes easily drilled. Single-chassis models will usually require punching another socket hole. If you use a miniature tube (it is all right to use a 12AX7 in combination with a 6SN7), the hole is small and can be made very easily with a ⅝- or ¾-inch drill.

Some Williamson kits use the triode instead of the Ultra-Linear circuitry in the output stage and the transformers provided will not have taps for Ultra-Linear use. The only modification necessary is to reduce the feedback resistors in both loops to two-thirds the value for Ultra-Linear operation. Triodes have only about two-thirds the gain of Ultra-Linear pentodes and to get the same feedback factor more voltage has to be fed back.

There are also several Williamson 6V6 kits—Heathkit A-7B, Knight, etc.—which can be converted into Junior Golden Ears. The models which include a phono-preamp will provide enough holes for tube sockets.

Equalizer for hi-fi ceramic pickups

Several readers have asked if there is any simple way of modifying the input of Junior to permit the use of hi-fi ceramic phono cartridges like the Sonotone and Electro-Voice Ultra-Linear. I offer two possibilities which will provide good equalization of the new RIAA curve and adequate results on other curves. The first is very simple and is included in the input of Fig. 1. It consists of a switch and a 1.5-megohm potentiometer so that the input resistance in the phono channel is 2 megohms, but only 500,000 ohms in the other channel.

The second equalizer (Fig. 4) provides exact and variable equalization, but requires an additional tube. With the volume control about two-thirds on, the equalization complements the RIAA curve beautifully. As the control is turned lower, you get more bass and less treble; and as it is turned further up, you get more treble and less bass. Actually the curve remains fairly flat no matter what the position of the control. It is merely revolved around a pivot at around 1,000 cycles to provide varying slopes. The circuit has very little net gain when the control is less than two-thirds full on. The control could be placed on the panel to provide continuous equalization control to suit the record or taste. If a switch is provided as indicated, the circuit will give loudness control of bass when the tuner is used, as in the Golden Ear Control Unit from which the circuit was developed. The circuit can be used with any amplifier or control unit. END

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Saves time, protects the cabinet.
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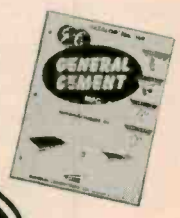

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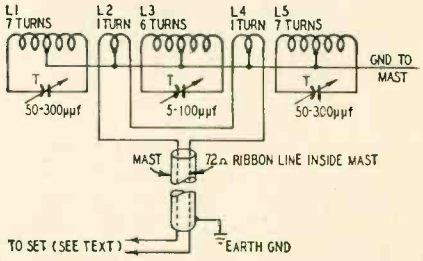
RADIO

ROTATABLE LOOP ANTENNA FOR BROADCAST RECEPTION

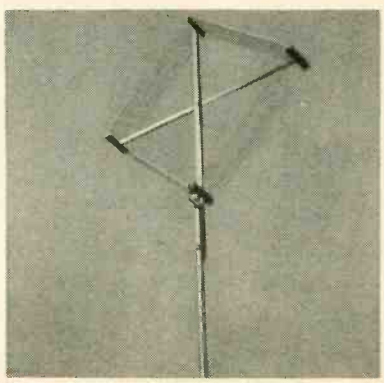
A ROOF-TOP rotatable loop antenna greatly improves broadcast reception in outlying areas where induction interference is a problem. It eliminates or minimiezs co-channel interference when so rotated that the unwanted station is in the null of its response pattern. The loop shown in the photo and diagram can be rotated to eliminate either of two co-channel stations of equal strength when they are separated by 30° or more. When a good line filter is used at the a.c. input to the receiver, the antenna system is completely noise-free, even with a brush type motor operating on the same circuit.

Because tuning a remote loop antenna for maximum signal pickup is awkward, a novel system was used. The antenna actually consists of three separate loops (L1, L3 and L5 in the diagram) that are closely coupled and tuned to different frequencies for broad-band performance.

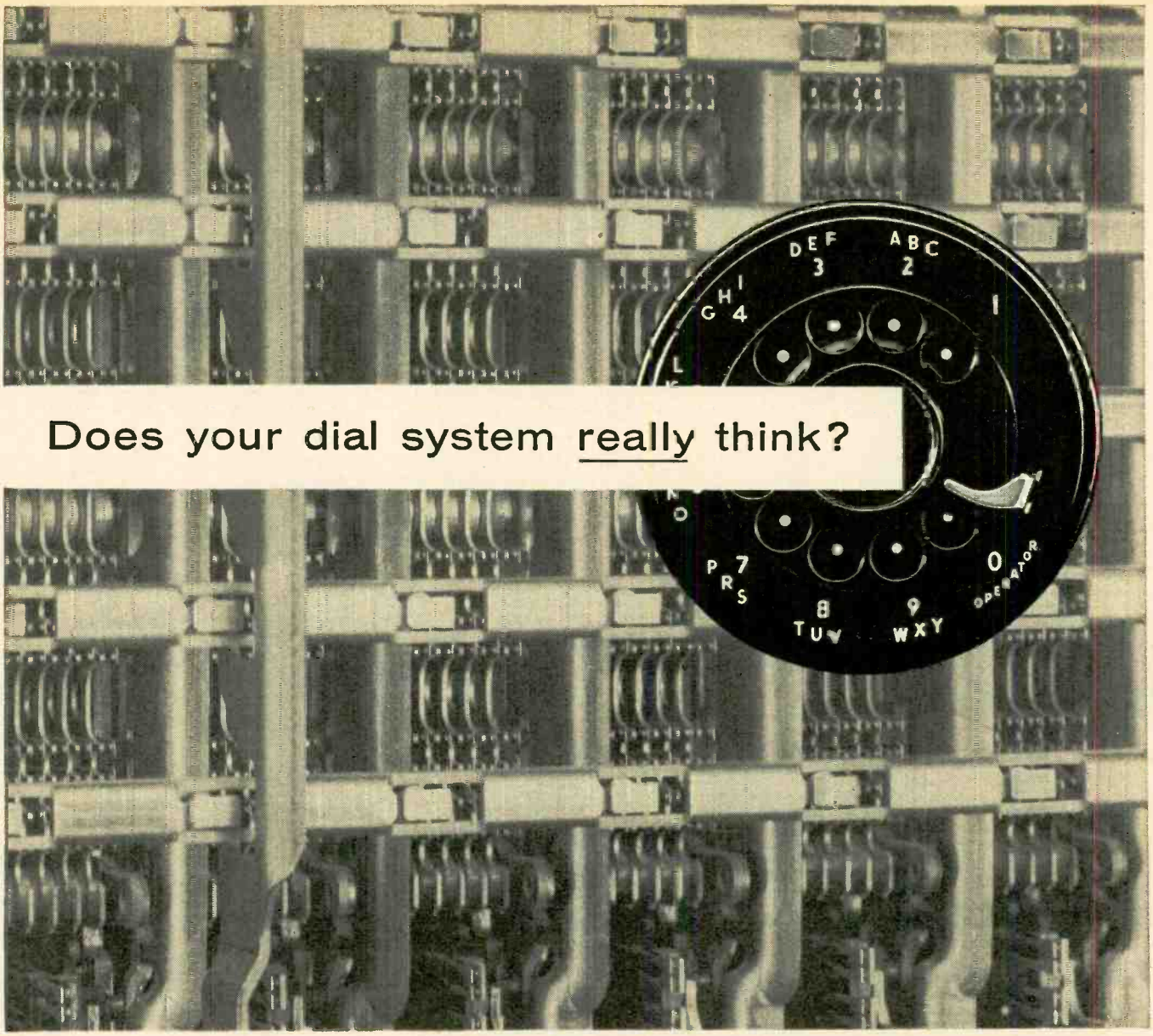


The antenna is wound with No. 20 enameled wire forming two 7-turn outside windings (L1 and L5) and a 6-turn center winding (L3). Pickup loops L2 and L4 have one turn each and are wound betwen L3 and the two outer windings. All coils are center-tapped. L1, L3 and L5 are tuned by small trimmer capacitors. Response is good across the band when the coils are tuned to my favorite stations on 690, 860 and 1560 kc.

The windings form the sides of a square with 6-foot diagonals. The frame is made from one 8- and one 6-foot length of 1¾ x 1-inch pine. The end pieces are ¼-inch birch plywood notched every ½ inch to hold the wire in place.



View of the rotatable loop antenna.



Does your dial system really think?

Part of the control equipment of a modern dial system—dial telephony's equivalent of a brain. It goes into action the instant you dial a call, selecting the telephone you want to reach and directing the switches that set up the connection . . . just as the brain directs the muscular actions of the body.

This question can't be answered until we learn more about the nature of thought. But dial telephone systems *do* simulate many of the processes of the human brain. For example, when a number is dialed, Bell's newest switching system—

COUNTS the dial pulses

REMEMBERS them

DECIDES ON the best route to a nearby town or across the nation

TESTS to see if the route is clear

SELECTS an alternate if the first route is busy

REPORTS difficulties in circuits, if any

Today's automatic switching reflects the creative thinking of many scientists and engineers at Bell Telephone Laboratories. Each year your dial telephone is able to do more for you. And this is but one phase of the continuing effort to keep your Bell telephone service the world's best.

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RADIO

Several coats of varnish provide insulation and weatherproofing.

The three trimmers are in an i.f. can mounted close to the bottom of the loop. The loop should be tuned and the i.f. can be weatherproofed with hard-setting wax before the antenna is erected on the roof.

The extra 2 feet on the longer piece of the framework permits clamping the antenna to the 1¼-inch TV mast used to support it. The centers of all windings are connected to the mast, which is grounded for lightning protection. The 1¼-inch metal mast is fastened to the eaves with strapping and sits in a socket drilled in a 2 x 4 nailed to the window sill. It can be turned manually from the window, or an antenna rotator motor could be used. Rotating the loop through 180° is sufficient.

Couple the transmission line to the radio through a primary of about 25 turns of fine wire in place of the ordinary primary. The new coil is wound either on the same form as the secondary or on one that will slip over it.

A Faraday shield gives a sharper null but greatly decreases the signal input so it is not recommended for weak-signal areas. The lead-in is brought down inside the mast to provide shielding. It may be necessary to slip a grounded shielded braid over the 72-ohm line from the mast base to the receiver if the run is long. The first r.f. stage of the receiver should be well shielded to prevent stray pickup. The signal output from a loop antenna is lower than from a long-wire type so a sensitive receiver is required for good performance.—*John A. Dewar*

INVENTIONS NEEDED

The National Inventors Council, in cooperation with the armed forces, has published a list of technical problems confronting the military services. The list is published with the hope that the publicity given to these problems will lead to satisfactory solutions or suggestions that can be developed into solutions. Included in the list are a group of subjects—not strictly problems—where general technological advances are desirable. This list is issued periodically and can be obtained free of charge from: National Inventors Council, U. S. Department of Commerce, Washington 25, D. C.

The following are subjects pertaining to the electronic field extracted from the list:

Long-life batteries
High-power microwave oscillator
High-frequency recorder
Coaxial r.f. switch
Semiconductor material
Rugged portable ammeter
Magnetostriction units
Miniature batteries
Miniature radio equipment construction
Electronic telegraph printer
High-quality synthetic quartz crystals
High-power electron tubes
Radiation measuring equipment
Method of heating dry batteries
High-voltage power supplies
Memory circuits
Homing navigation system
Ultra-lightweight antenna masts
Converting heat into electrical energy
Converting light into electrical energy
Improved electrolytes

WATCH FOR OUR MARCH ISSUE
ON SALE FEB. 24

Protect your TRANSISTORS

By HAROLD REED*

I WAS quite proud when I got my first transistor. None of my associates could claim ownership to one of these intriguing devices and I proudly related what I knew of its characteristics and applications, emphasizing its minute size, low voltage and current drain requirements and how simply it could be applied in different electronic circuits.

In my first experiment everything seemed to go well. A more elaborate circuit arrangement was tried and then I experienced that sinking feeling in the abdomen and almost lost my pride and joy. Something got crossed up, possibly due to my long association with electron tubes (not too helpful when working with transistors). The experimental circuit did not behave as expected and when, accidentally, the transistor came into physical contact with the hand, it was found to be about as hot as the 35-watt soldering iron used in wiring the circuit. The battery supply was hastily disconnected!

Transistors are easily ruined, but this little fellow must have been exceptionally rugged. It withstood the extremely high current flow and to this day still performs as well as later additions to my increasing collection.

This experience is similar to that known to experimenters in the "good old days" when triode vacuum tubes were selling at prices equivalent to the transistors of today and the B plus side of the power supply sneaked into the 6-volt filament circuit.

I resolved to attempt to eliminate all possible conditions that might prove disastrous to transistors when used in untried experimental circuits. It was decided to have complete variable control over all battery potentials applied to transistors. This is especially desirable if battery voltages are near or above maximum rating of the transistor. This condition was satisfied by the setup shown in Fig. 1-a. A variation using two controls, providing individual adjustment of the positive and negative potentials of the battery is shown in Fig. 1-b.

The small 4 x 2¼-inch bakelite panel (Fig. 2) on which is mounted the on-off switch, variable control, fuse holder and terminals, is equipped with two small angle brackets, slotted at one end so they may be slipped under the battery binding posts. The supply leads from the battery have spade lugs that also slip under the battery posts. Thus, with the 5308 Burgess battery, used in this instance, the supply potential is variable from 0 to 22.5 or 45 volts. When the battery is run down, the panel and lugs may be slipped onto a new battery of the same type. Also, polarity of the output terminals of the panel can be reversed simply by slipping the slotted brackets and lead lugs under the battery binding posts from the opposite side of the battery. The small fuse in the circuit is of the instrument protection type. Available in many different sizes, it should be chosen according to the maximum current rating of the transistors in the circuit.

The current drain on the battery, limited by the 250,000-ohm control at 22.5 volts, will be about 90 microamperes; at 45 volts, 180 microamperes. Actual measured currents are a little under these Ohm's-law figures. A heavy-duty battery of the type shown is usually not required for transistor applications. I used it because this type is kept on hand for remote broadcast amplifiers and, when replaced, its capacity is still adequate for most experimental work. This same idea, of course, is applicable to any type battery available and even lower current drain can be obtained with a higher resistance control. With a 500,000-ohm potentiometer across 45 volts, the current drain will be around 90 microamperes; while using the 22.5-volt tap, the current will be under 45 microamperes. If the transistor circuit being tested is to be developed into a permanent device, after the correct operating potentials are established, small batteries with voltages near the correct values may then be substituted for the test battery.

In dealing with untried transistor circuits, particularly when working near maximum rated values, it is unwise to obtain these values instantaneously. Approach them gradually.

I considered it necessary to know all operating values of the circuit, not just the current flowing through a single path in the transistor. A vacuum-tube voltmeter should be used to check battery voltages; d.c. voltmeters of at least 1,000 ohms per volt can be used if the voltage drop due to loading can be tolerated. When working close to the maximum voltage rating, be careful that this rating is not exceeded when the load of the voltmeter is removed from the circuit. Low-range milliammeters or microammeters are inserted in the three current paths of the transistor to give constant indication of the operating conditions with changes in component parts of the circuit and adjustments.

The layout used in developing a transistor audio amplifier (see photo) is a typical haywire breadboard setup. Nevertheless, the transistors are protected.

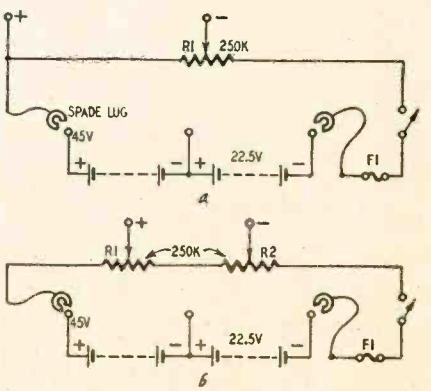


Fig. 1—Circuits for obtaining variable battery voltages for transistors.

*Chief engineer, station WOL, Washington, D.C.

Fig. 2—Front and rear views of voltage control unit shown in Fig. 1-a.

Radio technicians and experimenters are aware of the devastating effect of extremely high temperatures to germanium diodes because they have been widely used. Transistors are similarly affected. Heat from the soldering iron must be dissipated so it is not carried into the transistor via the leads. If the transistor is being wired into a circuit permanently, each lead may be gripped between the iron and transistor by a pair of long-nose pliers to reduce heat transmission. Where transistors are to be used repeatedly in experimental circuits, the mountings shown in Fig. 3 may prove helpful.

To the left is shown a Raytheon CK722 transistor with its 2 x .016-inch leads and a miniature socket (Cinch Nos. 14148 or 14273 may be used). Even with a socket a small soldering iron should be used quickly. Two methods used to protect the CK722 in numerous experimental circuits are shown at the right of the picture. One way is to use the full length of the leads, threading them down through and under a narrow strip of insulating material, then up through the opposite end, fanning the ends for soldering into any circuit, and applying cellulose cement to obtain rigidity. This also prevents breakage of the leads where they enter the transistor. Should they break at the end of the insulating strip, additional leads can be soldered on without damage to the transistor. The other mounting shown is a square of bakelite with three relatively large soldering terminals. The transistor leads were cut to suitable size, covered with spaghetti tubing and soldered to the terminals. The bakelite square is always mounted so that the terminals are above the transistor leads to minimize heat transfer to the transistor.

When soldering the transistor leads into a circuit, *observe battery polarity*. Incorrect polarity can easily damage a transistor permanently.

After that almost fatal experience with my first transistor, the procedures described were put into effect. Since then many tried and untried transistor circuits have been investigated with no transistor tragedies. END

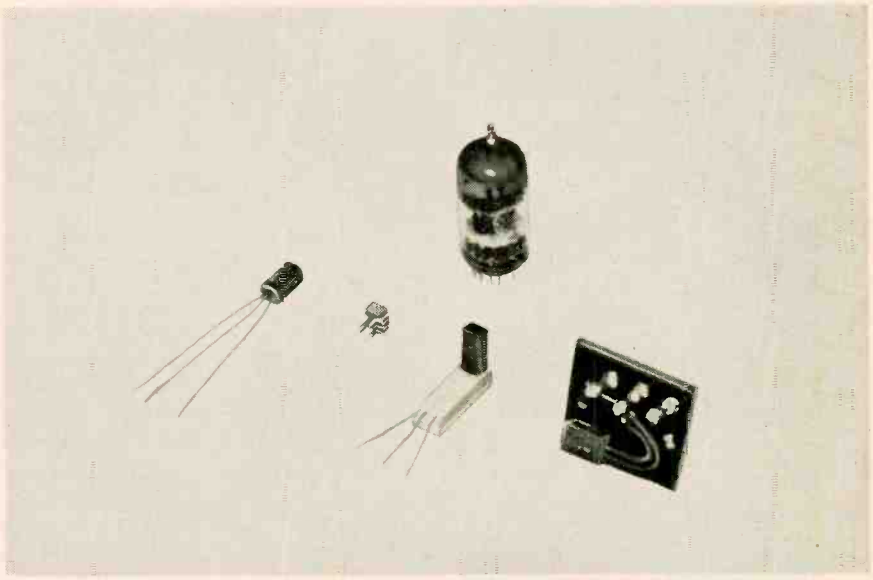
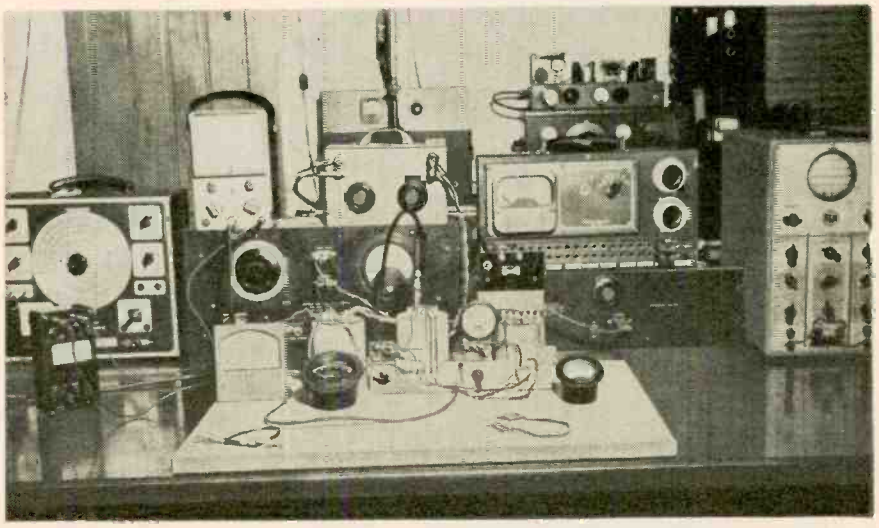
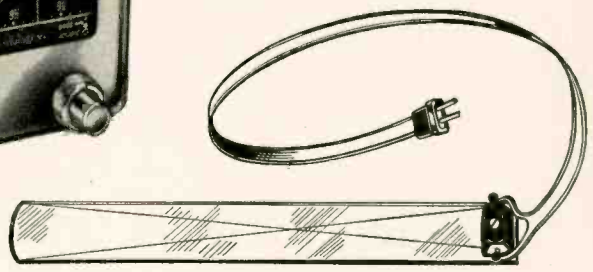


Fig. 3—Photo shows (left to right) a CK722 transistor, Cinch socket and two methods of mounting transistors. Miniature tube shows relative sizes.



Layout used for transistor experiments. Haywire-looking—but saves transistor.

HI-FI FM *for your car*



Above, Hastings FM car receiver. Below, compact antenna assembly.

FOR years the average American motorist has listened to his favorite music, sportcasts, plays and news on an AM auto radio while roaming the highways and byways. Leaky power lines, atmospheric disturbances and unsuppressed ignition systems in other cars often interfere with his reception. His enjoyment of the program material suffers by conscious or unconscious comparison with the interference-free reproduction on his FM receiver at home.

A line of FM broadcast receivers and tuners for automobile installations (introduced by Hastings Products, Inc., of Boston, Mass.) may well bring auto reception up to the home quality level. Four different models are made. The CT-6 and CT-12 (conversion types) are tuners using the power supply and audio amplifier circuits of the automobile's 6- or 12-volt AM radio receiver.

The PS-6 and PS-12 are complete FM broadcast receivers operating from 6- and 12-volt d.c. supplies. They consist of a tuner chassis, a separate power supply and audio chassis and a high-fidelity 8-inch PM speaker for rear deck mounting. The audio output circuit uses push-pull 6AQ5's (or 12AQ5's in the 12-volt model) and a 12AT7 phase inverter in a high-fidelity circuit. Response is said to be flat within 1.5 db from 20 to 20,000 cycles. Total distortion is less than 0.5% at normal listening levels and less than 2% at full output. Inverse feedback voltage is tapped off the secondary of the output transformer and fed to the phase inverter.

The tuners and receivers cover from 87 to 109 mc. An r.f. amplifier, three i.f. amplifiers, a pair of crystal diode

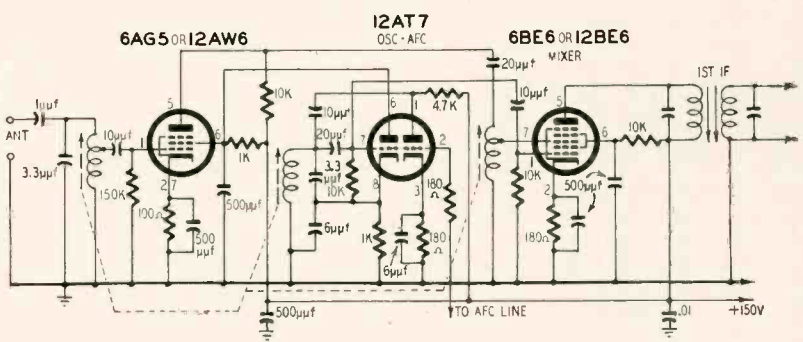


Fig. 1—The r.f. and a.f.c. circuits in the Hastings FM automobile radios.

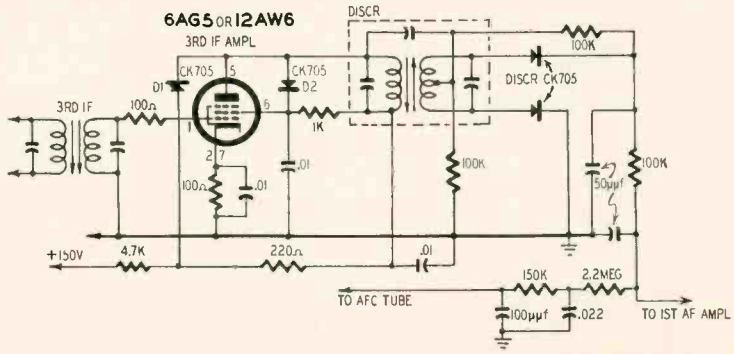


Fig. 2—Four germanium diodes replace tubes to reduce drain on the battery.

limiters and a Foster-Seeley discriminator provide 2 microvolts sensitivity with full limiting at 5 microvolts input. Automatic frequency control minimizes drift and simplifies tuning. The i.f. bandwidth is 200 kc with adjacent-channel response 60 db down. The discriminator feeds a 12AT7 2-stage voltage amplifier and bass-boost tone-control stage through a standard de-emphasis network.

The tuners and tuner chassis of the receivers are identical. They are unusually compact, considering the number of tubes and the circuitry. The cases, designed for suspension under the dashboard, are 6½ inches wide, 4 inches high and 9⅝ inches deep, including control knobs and a power plug in the rear. The PA-6 and PA-12 amplifier-power units measure 7 x 6 x 5¾ inches and are mounted on the firewall behind the dashboard.

Circuit features

Fig. 1 is the diagram of the front end used in the sets. The tube lineup depends on the battery voltage. Models for cars with 6-volt batteries use a 6AG5 r.f. amplifier, 12AT7 oscillator and a.f.c., and a 6BE6 mixer. The 12-volt models use a 12AW6 r.f. amplifier and 12BE6 mixer. A reactance-modulator type a.f.c. circuit shunts the oscillator tank circuit. A d.c. control voltage from the discriminator varies the effective reactance of the a.f.c. tube to hold the oscillator on frequency. The amount of control is carefully engineered to minimize drift without permitting a strong signal to capture the receiver and make it impossible to tune in a weak station on an adjacent channel.

The mixer feeds a conventional 3-stage 10.7-mc i.f. amplifier using 6AG5's or 12AW6's, depending on the heater voltage. A pair of germanium diodes (Fig. 2) are used as limiters. D1 is a dynamic limiter and D2 is a positive peak clipper. The diodes are biased by an R-C network that provides a variable threshold extending down to the level of the weakest signals. This combination provides efficient quieting and suppression of interchannel noise.

The audio detector is a Foster-Seeley discriminator using a pair of germanium diodes. The d.c. component of the discriminator output is filtered and used to vary the reactance of the a.f.c. tube. The a.f. output of the discriminator goes to the 2-stage 12AT7 voltage amplifier and bass-boost tone-control circuit, then to the audio circuit of the AM receiver or the high-fidelity amplifier in the deluxe installations. The latter type can be supplied with an Altec 400-B, University 308, Electro-Voice SP8B or equivalent 8-inch speaker with escutcheon plate and grille cloth for mounting on the rear deck.

A special nondirectional antenna for use with these receivers and tuners consists of a tuned circuit imbedded in a thin transparent plastic strip that is fastened on the side of the car's windshield. END

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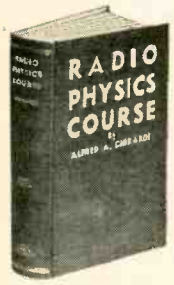

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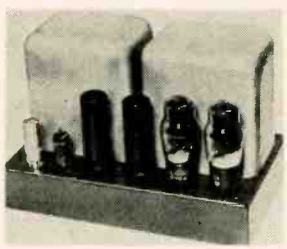

ment for minimum distortion, proper phase inversion and dynamic balance of output tubes to be made aurally without any test equipment. Good stability under varying load conditions —important where three-way or multiple speaker installations are used.—**Fairchild Recording Equipment Co.,** 154th St. and 7th Ave., Whitestone, N.Y.

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HI-FI AMPLIFIER and preamplifier (remote controlled) Newcomb *Classic 2500-R* features *Audi-Balance* which enables the user to find out by simply pressing a button if amplifier is operating at minimum distor-

tion. Less than .01% distortion up to 10 watts, less than 0.2% at 20 watts; 10–100,000-cycle response, within 0.1 db from 10–30,000 cycles; dual-range tone controls; bass range −16 db to +23 db; treble range −25 db to +23 db; d.c.-operated preamplifier.—**Newcomb Audio Products Co.,** 6824 Lexington Ave., Hollywood 38, Calif.

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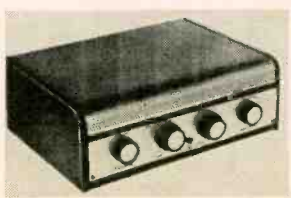
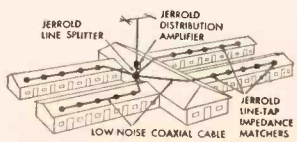


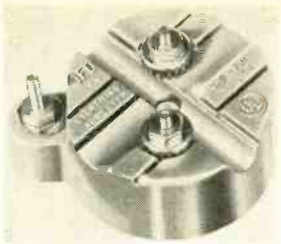


less than 1%. Intermodulation distortion less than 2% at rated output. Hum and noise level 80 db below rated output.—**Pilot Radio Corp.**, 37-06 36th St., Long Island City, N. Y.

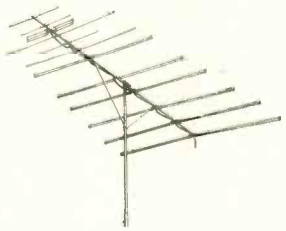
TENNA-ROTOR, *Alliance K-22*, consists of a rotator and a control unit in a plastic case. Rotator unit mounted on antenna mast; control box placed on or

adjacent to receiver. Unit's speed approximately 2 r.p.m. Die-cast housing of rotator unit has been strengthened and magnetic brake added to prevent drifting.—**Alliance Manufacturing Co.**, Alliance, Ohio.

LIGHTNING ARRESTER, *JFD AT130*, for v.h.f. and u.h.f. utilizes new material with less capacitance and less inductance which results in no line loading on u.h.f. Case of AT130 is weatherproof plastic. Patented sawtooth washers provide permanent and positive electrical contact without requiring striping of lead-in wires. AT130 can be used with 300-ohm v.h.f. or u.h.f. flat or tubular transmission or open wire.—**JFD Manufacturing Co.**, 6101 16th Ave., Brooklyn 4, N. Y.

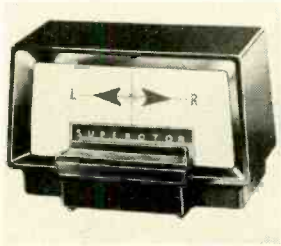


ALL-CHANNEL V.H.F. ANTENNA, *Kay-Townes' Rear Guard*, uses no reflectors or screens. Front-to-back ratios of better than 25–1 (some chan-



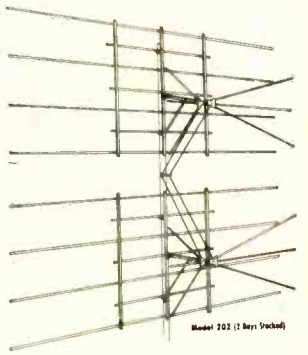
nels up to 100–1) with narrow forward lobe of 35° with a forward gain of 8 db or better, obtained electronically by a phasing system using seven folded dipoles.—**Kay-Townes Antenna Co.**, 1511 Dean Ave., Rome, Ga.

TWIN-LIGHT CONTROL UNIT for *Leader Superotor* antenna rotator features two arrows on dial face, pointing left and right, that light up automatically when the antenna is rotated. By observing relative brilliance of arrows, user can determine direction of antenna rotation. A de luxe unit with a NESW directional scale on dial face also being offered.—**Leader Electronics Corp.**, 2925 E. 55th St., Cleveland 27, Ohio.



VEST POCKET BEAM, *Mosley*, two-element unit, has loading coils at element centers which permit rotary beam performance on 40-meter band. Supporting boom is 14½ feet long and element lengths approximately 33½ feet. Weatherproof link winding on radiator coil designed to match 50-ohm coaxial feed line. Tests indicate standing-wave ratios as low as 1.07/1. Front-to-back ratios in the order of 19 db. Beam is pretuned to 7210 kc.—**Mosley Electronics Inc.**, 8622 St. Charles Rock Road, St. Louis, Mo.

TV ANTENNAS, *Telrex King Pin models 201* and *202* use conical-V-beam dipoles to achieve directivity and match (to 200- or 300-ohm line) over its entire operating band. Screen reflectors dimensioned to provide a compact, in-line, single-lobed directional pattern in horizontal and vertical planes at all frequencies. *Model 201*, single-bay unit, can be elaborated into two-bay structure, *Model 202*, by addition of stacking transformer.—**Telrex Inc.**, Asbury Park, N. J.



TV ANTENNAS, *Telco Mity-V* and *Bonnie-V*. *Mity-V* an adjustable u.h.f.–v.h.f unit for close-in reception areas. Twin elements are adjustable 60° to 90° for best performance.

Bonnie-V, a streamlined antenna strictly for local reception areas.—**Television Hardware Manufacturing Co.**, Division of General Cement Mfg. Co., 919 Taylor Ave., Rockford, Ill.

(*Contd. on page* 114)

Now!

KAY-TOWNES
brings you complete

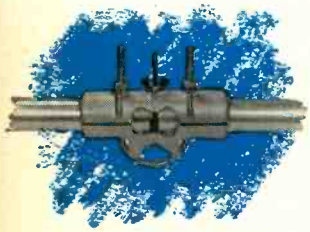
Protection from the Rear

Plus

Quick Rig!

THE first SNAP-OUT ANTENNA WITH THE EXCLUSIVE DOUBLE LOCK FEATURE!

Boom alsa falds ta take less room in storage and for ease of installatian. Sure-grip mast clamp halds in gale-force winds . . . will not slip or crush.

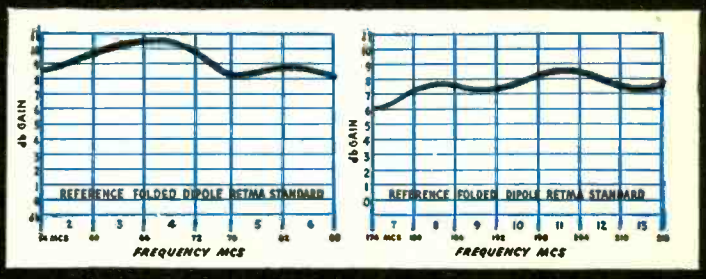


Exclusive with KAY-TOWNES Elements will nat droop, sag or fold up on a Kay-Townes Antenna . . . they're nested and *double locked* in position to stay in position.

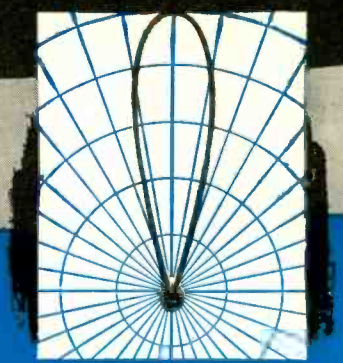
Patents applied for

New features that make the K-T "REAR-GUARD" America's most advanced TV Antenna!

- ★ *Completely Preassembled, it's mechanically safe!*
- ★ *It snaps in place to stay in place! Elements are double locked in position! A K-T Exclusive!*
- ★ *No bolts or nuts to tighten on elements!*



Front to back ratio is better than 25/1 forward lobe 30° or better standing wave ratio 1.2:1 average.

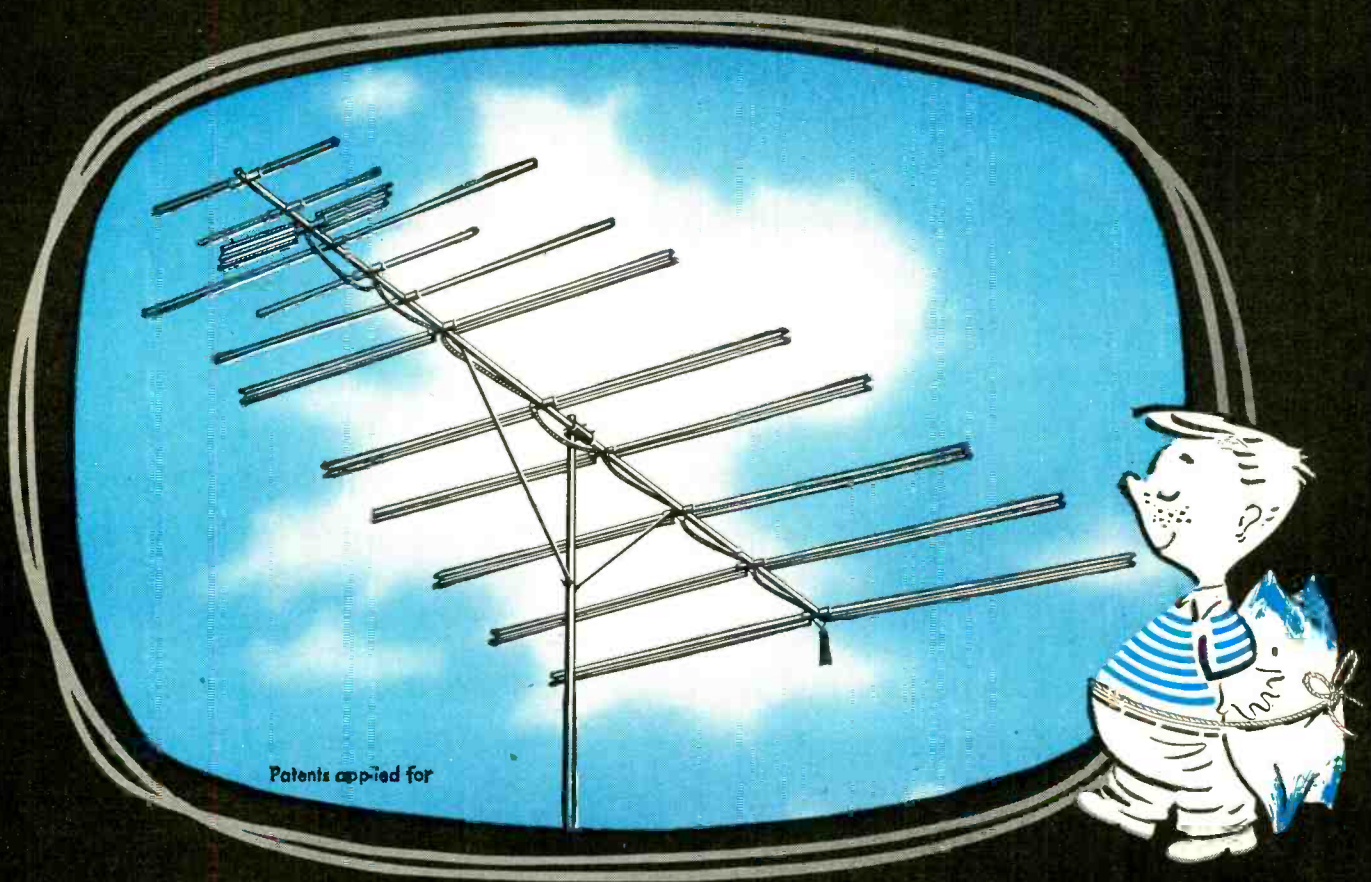


CHANNEL 2 THROUGH 13
RADIATION CURVE
REPRESENTING ALL
VHF CHANNELS
Over 20 to 1 ratio on ALL Channels

For Quality . . .

Manufactured and distributed in Canada by
Delhi Metal Products, Ltd.
Delhi, Ontario

REAR GUARD



THE ANTENNA DESIGNED TO REJECT UNWANTED SIGNALS FROM REAR AND SIDES!

In areas where many local stations or stations from near-by cities interfere with reception, ordinary antennas cannot filter out unwanted signals from sides and rear . . . *BUT* the KAY-TOWNES REAR-GUARD, with a front to back ratio far in excess of 20 to 1, is designed for *this* particular job . . . to give quality reception even in problem areas.

Add to the REAR-GUARD'S pin point selectivity such *exclusive* K-T features as double locked and nested elements that cannot droop or sag, Sure-Grip Mast Clamp that holds in gale-force winds without slipping or crushing, extra rigid construction and wood dowel pins and crimped ends that relieve metal fatigue due to vibration . . . they all add up to *America's most wanted TV Antenna.*

. . . for Performance look to KAY-TOWNES!

The First Name in TV Antennas

KAY-TOWNES

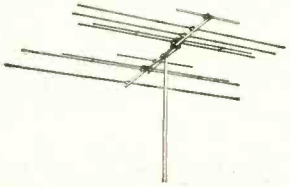
ANTENNA COMPANY

BOX 593B, ROME, GEORGIA

Use the K-T Line of television accessories

(Continued)

FRINGE-AREA ANTENNA, *Welco Sabre Senior,* has high gain on all v.h.f. channels. *Miracle Phase* isolates and minimizes interaction and loading



of phased elements. Coupling of working elements makes it possible to feed received signal to set for clear pictures in fringe areas.—**Welco Manufacturing Co.,** Burlington, Iowa.

U.H.F. CONVERTER, *Alliance model UC-2,* has coaxial tuner for smooth operation. Low-noise amplification assures good reception in any area.—**The Alliance Manufacturing Co.,** Alliance, Ohio.

VOLTMETER KIT, *Franklin model FV-1,* includes tubes, assembly material, test leads and detailed assembly manual. Fast measurements with greater accuracy on 1.5-volt low scale—more than 2⅛-inch scale length

per volt. A.c.-d.c. ranges: 0, 1.5, 5, 15, 50, 150, 500, 1,500 volts (1,000-volt maximum on a.c.). Ohmmeter range from ×1 to ×100,000 ohms and ×1 megohm. Measures 0.1 ohm to 1,000 megohms.—**Franklin Electronics,** King St., Franklin Park, Ill.

NEW KIT, *General Cement Glo-Bar Filament Resistor Kit,* comprises two washer type thermistors suitable for replacement on any well known brand of TV receiver (such as Motorola, General Electric, etc.) using series-tube heater string.—**General Cement Manufacturing Co.,** 919 Taylor Ave., Rockford, Ill.

PORTABLE OSCILLOSCOPE KIT, *Heath model OL-1* employs 3-inch cathode-ray tube to perform all utility scope functions. Has push-pull deflection amplifiers. Sweep operation up to 100,000 cycles.—**Heath Co.,** Benton Harbor 20, Mich.

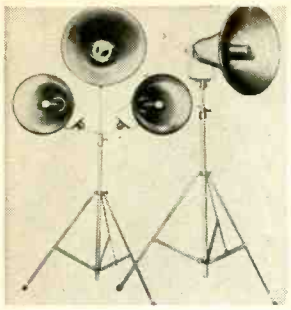
NEW KITS, *Tech-Master* amplifier kit *TM-15A* and preamplifier-equalizer kit *TM-15P.* Amplifier kit based on Williamson circuit with modifications—has been increased in output from 15 to 20 watts. Distortion less than 0.25% at normal listening levels, with good transient characteristics.

Preamplifier kit has four input channels, selector switch for FM, AM or TV tuner; crystal or reluctance style pickup; tape recorder or other signal sources; contains a cathode-follower output stage.

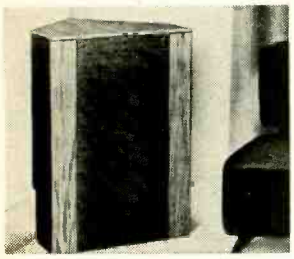
Both units complete with all components, step-by-step instructions and premounted tube sockets, and terminal strips.—**Tech-Master Corp.,** 75 Front St., Brooklyn 1, N. Y.

PORTABLE KIT, *Xcelite* No. 77 contains seven nut drivers 3/16 to 3/8 inch with different colored handles to identify size.—**Xcelite, Inc.,** Orchard Park, N. Y.

LOUDSPEAKER SUPPORT STAND, *Atlas model SS-2,* has been redesigned to accommodate U-brackets of all makes and types of loudspeaker projectors. Top bracket adapter permits attachment or removal of a projector without unscrewing top adapter or using any tools. Base stability is adequate for support of cluster of speakers even under adverse wind conditions. Supports several hundred pounds, has height extension of 5 to 10 feet and weighs 20 lb.—**Atlas Sound Corp.,** 1451 39th St., Brooklyn 18, N. Y.



SPEAKER ENCLOSURE, *Klipsch Rebel 3,* G & H Wood, has been added to their line which already includes Rebel 4 and 5. Stems in design from the

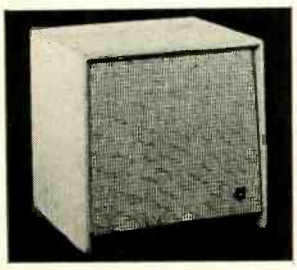


Klipschorn. Maximum performance per cubic foot possible through use of the same principles of mirror images produced by walls in a room corner as in Klipschorn.—**G & H Wood Products,** 75 North 11th St., Brooklyn 11, N. Y.

ADAPHONE INSTRUMENT, *Fenton,* permits listening to radio and TV without disturbing others by using earpiece set in the unit. A 5-ohm load replaces

speech coil when loudspeaker is switched off. Provides hearing aid for hard-of-hearing listener or a silent listener for night owls. Has a 15-foot extension cord. Additional earpiece set or an earphone embedded in a 12 x 9 x 2½-inch foam-rubber pillow also available.—**Fenton Co.,** 15 Moore St., New York 4, N. Y.

ENCLOSURE, nonresonant, for use with the *Hartley 215* loud speaker. Has two-stage acoustic filter and measures 18 x 18 x 16



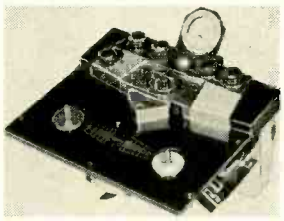
inches in unfinished gumwood, sanded ready for staining or painting.—**H. A. Hartley Co. Inc.,** 521 E. 162nd St., New York, N. Y.

INDUSTRIAL METERS, *Phaostron,* incorporate most ruggedized features demanded by military under specification MIL-M-10304. Sturdy, metal-

cased, with easy-to-read front zero adjustments. Available in 2½- and 3½-inch round or square bezels. A.c. and d.c. models. **Phaostron Co.,** 151 Pasadena Ave., South Pasadena, Calif.

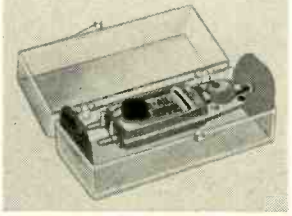
49 PANEL METERS, *Simpson,* have four ranges in microammeters d.c.: 25–0–25, 50–0–50, 100–0–100, 500–0–500; three ranges in ammeters d.c.: 0–75, 0–100, 0–150.—**Simpson Electric Co.,** 5200 W. Kinzie St., Chicago 44, Ill.

TAPE RECORDER, *Symphotone model 212,* two-speed record-playback mechanism records at 3¾ and 7½ i.p.s. with twin-track recording head. Frequency response 40 to 13,000 cycles at 7½ i.p.s. One control selects fast, forward, standard forward, fast rewind and stop. Other controls select playing speed,



record-playback, volume, on and off and speaker cutout. Two inputs available—high-impedance jack for microphone and high-impedance input on terminal strip for phono or radio tuner.—**Webster Electric Co.,** 1900 Clark St., Racine, Wis.

REPLACEMENT CARTRIDGE, *Turner* universal phonograph pickup, can be used to replace 95% of all 78-r.p.m. pickups in use. Available in two models, *AU* and *A. Model AU* has an externally mounted capacitor for low-voltage (2.0 volts or lower



output) replacements. The capacitor may be slipped off for high-voltage replacements. *Model A,* same cartridge as *AU,* but furnished without the external capacitor.—**The Turner Co.,** 933 17th St. N. E., Cedar Rapids, Iowa. END

All specifications given on these pages are from manufacturer's data.

Technicians' News

NATESA MAKES LIST

To encourage the practice of distributor selling to service technicians only, the National Alliance of Television and Electronic Service Associations has planned a list of bona fide radio-TV service firms, Frank Moch, NATESA president, reports.

The list will contain names of all genuine service businesses, whether members of NATESA affiliates or not, Mr. Moch explained, adding that he hoped it might be used one day by distributors as the sole guide to genuine service shop owners. Jobbers will be urged to restrict dealer discounts to that list, possibly offering other and smaller discounts to some other types of customers.

A Chicago list, in preparation by TISA, is expected to be ready shortly.

NEW YORK LICENSING

Arguments for and against a bill to license New York City TV and radio repair were heard at a City Council hearing Nov. 30 last. The bill (see Radio Month), a local law sponsored by Councilmen Cunningham, Kranis and Issacs, was passed by the Council in 1951 but was later declared ineffective for technical (legal) reasons.

Among those favoring the proposed local law were representatives of a local organization, the Associated Radio and Television Servicemen of New York (City) (ARTSNY); the District Attorney of Brooklyn, Edward S. Silver, and representatives of a number of out-of-town and even out-of-state groups. The representatives of Philadelphia groups stated that their interest in the subject was due to the influence that passing of a service bill in New York City would have on the rest of the country.

Leading opponent of the bill was Glen McDaniel, president of the Radio-Electronic-Television Manufacturers Association and a representative of the Commerce and Industry Association of New York. Two small radio-TV service associations, one an alumni group of the local RETMA training program and the other a TV service group from Staten Island, also opposed the bill, while another, an appliance and TV-radio servicing organization, favored it. In all 12 voices were heard in favor of the proposition and 8 opposed.

Opposition was based on governmental interference in private industry, possibility of political angles and

alleged greater cost to the customer due to limiting of the number of technicians through licensing. Advocates cited the possibility of controlling the unethical service technician without the difficult expedient of issuing complaints and resorting to a court of law, the advantage to the customer of knowing that his repairman is qualified and an increase in prestige to the service trade in general. District Attorney Silver was especially explicit on the weaknesses of legal redress, pointing out that few set owners would swear out a complaint and take the necessary time to testify in court, preferring to pocket their losses rather than incur the larger ones inevitable in the effort to bring fraudulent operators to justice.

UTAH ON LICENSES

License proposals would be put before the State Legislature of Utah during the 1955 session, the assistant Salt Lake City attorney reported recently. This, he stated in a report to the city commission, appeared to be the best answer to the problems of radio-TV servicing.

The report was the result of a meeting with a committee of service technicians and the local BBB.

TISA-ILLINOIS ELECTS

The Television Installation Service Association, Chicago, Ill., has unanimously re-elected Frank J. Moch (Aide Service Corp.) president. Walt Krzak (Television Engineers, Inc.) was named first vice president, Russ Havill (Havill's TV) second vice president, Larry Corlew (Electronic Engineers, Inc.) secretary, George Hingson (Courtesy TV Service) treasurer and Mel Brown (B & M Radio and TV Service) sergeant at arms.

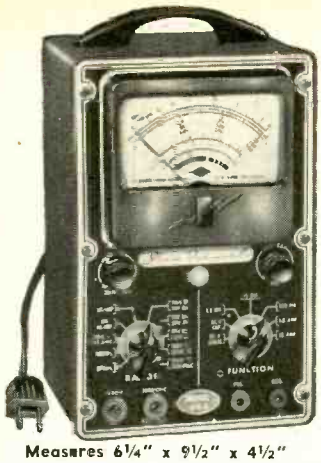
President Moch outlined accomplishments of 1954 and proposed certain changes for 1955. These included creation of a third vice presidency, whose incumbent would act as coordinator of membership drives, and making the NATESA delegate and alternate elective offices.

New TISA officials, left to right: Larry Corlew, Russ Havill, Mel Brown, Frank Moch, Walt Krzak, Geo. Hingson.

$2.7 BILLION SERVICE FEE

Installation and maintenance of TV and radio equipment for the home is now a major contribution to the total industry income, RCA Executive Vice President Charles M. Odorizzi told a Cleveland meeting recently.

(Continued on page 120)



Measures 6¼" x 9½" x 4½"

Superior's new Model 670-A

SUPER METER

A COMBINATION VOLT-OHM MILLIAMMETER PLUS CAPACITY REACTANCE INDUCTANCE AND DECIBEL MEASUREMENTS

SPECIFICATIONS:

D.C. VOLTS: 0 to 7.5/15/75/150/750/1,500/7,500 Volts
A.C. VOLTS: 0 to 15/30/150/300/1,500/3,000 Volts
OUTPUT VOLTS: 0 to 15/30/150/300/1,500/3,000 Volts
D.C. CURRENT: 0 to 1.5/15/150 Ma. 0 to 1.5/15 Amperes
RESISTANCE: 0 to 1,000/100,000 Ohms 0 to 10 Megohms
CAPACITY: .001 to 1 Mfd. 1 to 50 Mfd. (Good-Bad scale for checking quality of electrolytic condensers.)
REACTANCE: 50 to 2,500 Ohms 2,500 Ohms to 2.5 Megohms
INDUCTANCE: .15 to 7 Henries 7 to 7,000 Henries
DECIBELS: −6 to +18 +14 to +38 +34 to +58

ADDED FEATURE:
Built-in ISOLATION TRANSFORMER reduces possibility of burning out meter through misuse.

The Model 670-A comes housed, in a rugged crackle-finished steel cabinet complete with test leads and operating instructions.

$28.40 NET

Superior's new Model TV-11

TUBE TESTER

SPECIFICATIONS:

★ Tests all tubes including 4, 5, 6, 7, Octal, Lock-in, Peanut, Bantam, Hearing Aid, Thyratron Miniatures, Sub-miniatures, Novals, Sub-minars, Proximity fuse types, etc.

★ Uses the new self-cleaning Lever Action Switches for individual element testing. Because *all elements are numbered according to pin-number in the RMA base numbering system,* the user can instantly identify which element is under test. Tubes having tapped filaments and tubes with filaments terminating in more than one pin are truly tested with the Model TV-11 as any of the pins may be placed in the neutral position when necessary.

★ The Model TV-11 does not use any combination type sockets. Instead individual sockets are used for each type of tube. Thus *it is impossible to damage a tube by inserting it in the wrong socket.*

★ Free-moving built-in roll chart provides complete data for all tubes.

★ Newly designed Line Voltage Control compensates for variation of any Line Voltage between 105 Volts and 130 Volts.

★ NOISE TEST: Phono-jack on front panel for plugging in either phones or external amplifier will detect microphonic tubes or noise due to faulty elements and loose internal connections.

EXTRA SERVICE — The Model TV-11 may be used as an extremely sensitive Condenser Leakage Checker. A relaxation type oscillator incorporated in this model will detect leakages even when the frequency is one per minute.

The model TV-11 operates on 105-130 Volt 60 Cycles A.C. Comes housed in a beautiful hand-rubbed oak cabinet complete with portable cover

$47.50 NET

SUPERIOR'S NEW MODEL TV-40

C.R.T. TUBE TESTER

★ **A complete picture tube tester for little more than the price of a "make-shift" adapter!!**

★ **Tests *all* magnetically deflected tubes . . . in the set . . . out of the set . . . in the carton!!**

The Model TV-40 is absolutely complete! Self-contained, including built-in power supply, it tests picture tubes in the only practical way to efficiently test such tubes: that is by the use of a separate instrument which is designed exclusively to test the ever increasing number of picture tubes!

EASY TO USE:

Simply insert line cord into any 110 volt A.C. outlet, then attach tester socket to tube base *(Ion Trap Need Not Be on Tube).* Throw switch up for quality test . . . read direct on Good-Bad scale. Throw switch down for all leakage tests.

SPECIFICATIONS:

- Tests ALL magnetically deflected picture tubes from 7 inch to 30 inch types.
- Tests for quality by the well established emission method. All readings on "Good-Bad" scale.
- Tests for inter-element shorts and leakages up to 5 megohms.
- Tests for open elements.

Model TV-40 C.R.T. Tube Tester comes absolutely complete—nothing else to buy. Housed in round cornered, molded bakelite case. Only.....

$15.85 NET

SHIPPED ON APPROVAL

NO MONEY WITH ORDER — NO C.O.D.

Try any of the above instruments for 10 days before you buy. If completely satisfied *then* send down payment and pay balance as indicated on coupon. **No Interest or Finance Charges Added!** If not completely satisfied return unit to us, no explanation necessary.

MOSS ELECTRONIC DISTRIBUTING CO., INC.
Dept. D-97, 3849 Tenth Ave., New York 34, N.Y.

Please send me the units checked. I agree to pay down payment within 10 days and to pay the monthly balance as shown. It is understood there will be no finance, interest or any other charges, provided I send my monthly payments when due. It is further understood that should I fail to make payment when due, the full unpaid balance shall become immediately due and payable.

Name .....

Address .....

City..... Zone..... State.....

☐ Model 670-A.....Total Price $28.40 $7.40 within 10 days. Balance $3.50 monthly for 6 months.

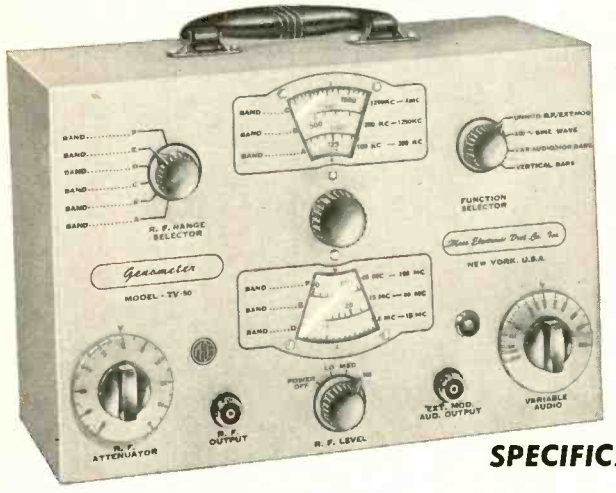
☐ Model TV-11.....Total Price $47.50 $11.50 within 10 days. Balance $6.00 monthly for 6 months.

☐ Model TV-40.....Total Price $15.85 $3.85 within 10 days. Balance $4.00 monthly for 3 months.

The Model TV-50 GENOMETER

A versatile all-inclusive GENERATOR which provides ALL the outputs for servicing:

A. M. Radio F. M. Radio Amplifiers Black and White TV Color TV



7 Signal Generators in One!

- R. F. Signal Generator for A.M.
- R. F. Signal Generator for F.M.
- Audio Frequency Generator
- Bar Generator
- Cross Hatch Generator
- Color Dot Pattern Generator
- Marker Generator

SPECIFICATIONS:

R. F. SIGNAL GENERATOR:

The Model TV-50 Genometer provides *complete* coverage for A.M. and F.M. alignment. Generates Radio Frequencies from 100 Kilocycles to 60 Megacycles on fundamentals and from 60 Megacycles to 180 Megacycles on powerful harmonics. Accuracy and stability are assured by use of permeability trimmed Hi-Q coils. R.F. is available *separately,* modulated by the fixed *400 cycle sine-wave* audio or modulated by the *variable* 300 cycle to 20,000 cycle variable audio. Provision has also been made for injection of any external modulating source.

VARIABLE AUDIO FREQUENCY GENERATOR:

In addition to a fixed 400 cycle sine-wave audio, the Model TV-50 Genometer provides a variable 300 cycle to 20,000 cycle peaked wave audio signal. This service is used for checking distortion in amplifiers, measuring amplifier gain, trouble shooting hearing aids, etc.

BAR GENERATOR:

This feature of the Model TV-50 Genometer will permit you to throw an actual Bar Pattern on any TV Receiver Screen. Pattern will consist of 4 to 16 horizontal bars or 7 to 20 vertical bars. A Bar Generator is acknowledged to provide the quickest and most efficient way of adjusting TV linearity controls. The Model TV-50 employs a recently improved Bar Generator circuit which assures stable never-shifting vertical and horizontal bars.

CROSS HATCH GENERATOR:

The Model TV-50 Genometer will project a cross-hatch pattern on any TV picture tube. The pattern will consist of non-shifting, horizontal and vertical lines *interlaced* to provide a stable cross-hatch effect. This service is used primarily for correct ion trap positioning and for adjustment of linearity.

DOT PATTERN GENERATOR *(For Color TV)*

Although you will be able to use most of your regular standard equipment for servicing Color TV, the one addition which is a "must" is a Dot Pattern Generator. The Dot Pattern projected on any color TV Receiver tube by the Model TV-50 will enable you to adjust for *proper color convergence.* When all controls and circuits are in proper alignment, the resulting pattern will consist of a sharp white dot pattern on a black background. One or more circuit or control deviations will result in a dot pattern out of convergence, with the blue, red and green dots in overlapping dot patterns.

MARKER GENERATOR:

The Model TV-50 includes *all* the most frequently needed marker points. Because of the ever-changing and ever-increasing number of such points required, we decided against using crystal holders. We instead adjust each marker point against precise laboratory standards. The following markers are provided: 189 Kc., 262.5 Kc., 456 Kc., 600 Kc., 1000 Kc., 1400 Kc., 1600 Kc., 2000 Kc., 2500 Kc., 3579 Kc., 4.5 Mc., 5 Mc., 10.7 Mc. (3579 Kc. is the color burst frequency.)

The Model TV-50 comes absolutely complete with shielded leads and operating instructions. Only .....

$47.50 NET

SHIPPED ON APPROVAL

NO MONEY WITH ORDER — NO C.O.D.

Try it for 10 days before you buy. If completely satisfied *then* send $11.50 and pay balance at rate of $6.00 per month for 6 months. **No Interest or Finance Charges Added!** If not completely satisfied return unit to us, no explanation necessary.

MOSS ELECTRONIC DISTRIBUTING CO., INC.
Dept. D-97, 3849 Tenth Ave., New York 34, N.Y.

Please rush one Model TV-50. I agree to pay $11.50 within 10 days and to pay $6.00 per month thereafter. It is understood there will be no finance, interest or any other charges, provided I send my monthly payments when due. It is further understood that should I fail to make payment when due, the full unpaid balance shall become immediately due and payable.

Name .....

Address .....

City ..... Zone ..... State .....

TECHNICIANS' NEWS *(Continued)*

In 1953, Mr. Odorizzi stated, the industry employed nearly 100,000 service technicians, the income from home service alone was $1.4 billions and by the end of 1957 will increase to approximately $2.7 billions. As the use of electronic apparatus increases with automation and application of electronic controls to industry, plus the spread of television service, the importance of service will increase accordingly. "Service," he said, "therefore has become an important facet of the nation's business structure."

N. H. GROUP ELECTS

The New Hampshire Radio and Television Association, meeting at the New Hampshire Technical Institute, Manchester, N. H., has re-elected Harvey O'Dowd of Goffstown as president for the 1955 term. Other officers elected were Paul Frost, Concord, first vice president; George Bennett, Manchester, second vice president; Ernest Tetrault, Manchester, treasurer; Emile R. Gelinas, Manchester, executive secretary, and Warren Davis, Hampton, secretary.

MINTSE MOVES

A meeting was held in Minneapolis on Dec. 9, 1954, "to organize an association to improve service (radio and TV) to the public." The meeting was sponsored by the Minnesota Television Service Engineers and the Minnesota State Department of Business Development as well as the State Bureau of Labor. The Minnesota Television Service Engineers is a group formed by members of existing service associations for the purpose of launching the statewide organization.

The meeting was addressed by State Gov. C. Elmer Anderson, Commissioner Clark of the Department of Business Development and others. Howard Sams, slated to speak, could not reach the meeting, but sent a telegram of encouragement, as did District Attorney Silver of Brooklyn, N. Y. A heavy storm the night before and slippery roads reduced attendance, but representatives from 18 Minnesota communities were present as well as visitors from two Wisconsin localities. Since the idea of MINTSE was new to many, it was decided to postpone action for 90 days, during which time an informational campaign would be carried out. Then a meeting of representatives would be held to formulate proposals which would be submitted for final action to a large meeting in the late spring.

Of the approximately 15 persons heard from during the meeting, only one opposed the idea of the new statewide association. Matters of detail were of course held in abeyance, but the consensus was that the organization would follow generally the industry standards set up by NATESA—grading service personnel from engineer to apprentice. END

radio-electronic Circuits

SSB RECEIVING ADAPTER

Many amateurs and SWL's use the receiver's b.f.o. to reinsert the carrier of SSB (single-sideband, suppressed-carrier) transmissions so the signals are readable. Since reinserted carrier must be within 50 cycles of the correct frequency for reasonably distortion-free reception, the receiver's high-frequency and beat-frequency oscillators must be highly stable. Frequency drift with temperature or voltage changes greatly increases distortion and makes frequent retuning necessary for good readability.

Reception of SSB signals is easier and readability is greater when the receiver is fitted with an SSB adapter. The usual SSB adapter (commonly called a signal slicer) converts the conventional communications receiver to a double superhet with a very selective 50-kc i.f. system. The second i.f. is sharp enough to permit the operator to select either one of the sidebands present in the receiver's normal i.f. selectivity curve and completely reject the other. The adapter is equally useful in receiving AM, PM, NBFM, and CW signals.

Most SSB adapters that have been described in the past have used complex filters or phase-shift networks that are difficult for the average constructor to obtain or duplicate. This difficulty has been eliminated by the introduction of the new type S-15000 single-sideband filter produced by Burnell & Co. of Yonkers, N. Y. The diagram in Fig. 1 shows the circuit of a signal slicer designed around this filter.

A length of coaxial cable couples the plate of the last i.f. amplifier in the receiver to the grid of mixer V1 through a 10-$\mu\mu$f capacitor. V2 is a Pierce oscillator, with crystals Y1 and Y2 selected by switch S1. The frequencies of the crystals depend on the i.f. of the receiver. One is 50 kc below and the other 50 kc above the i.f. Surplus FT-241 type crystals marked with the frequency of the 54th harmonic are suitable. The higher-frequency crystal is used for receiving the lower sideband when the receiver's high-frequency oscillator is above the signal frequency.

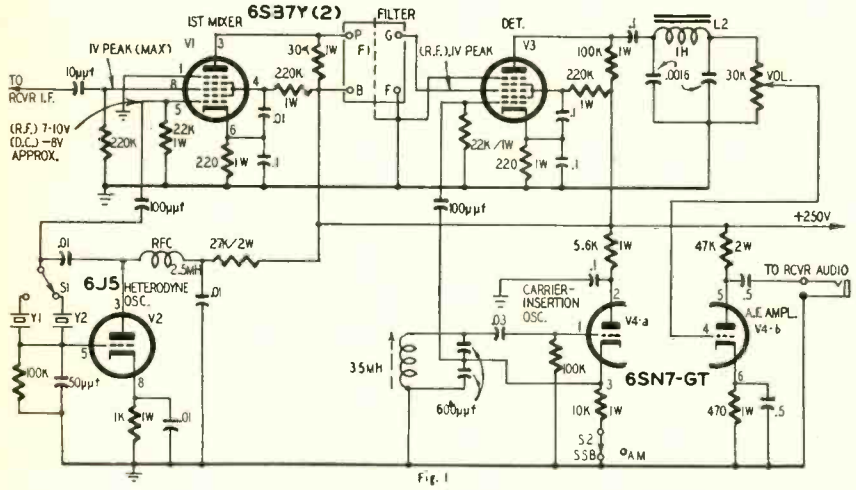


Fig. 1

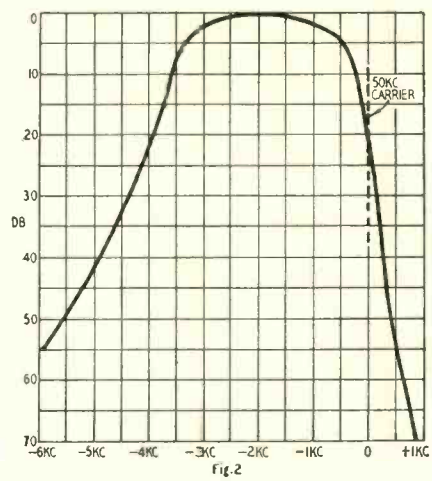


Fig. 2

The 30,000-ohm plate-load resistor for V1 provides the proper input impedance for the S-15000 filter. (Because the input impedance is not too critical, a standard 33,000-ohm unit can be used at this point.) The filter is designed to pass the 50-kc carrier and frequencies 2,500 cycles below it. The selectivity curve is shown in Fig. 2.

A 50-kc signal of about 0.1 volt peak appears on the grid of V3. This tube is used as a heterodyne detector (converter or mixer) for SSB signals and as a plate detector for AM and NBFM signals. Closing S2 for SSB reception completes the cathode circuit of V4-a, the 50-kc carrier-insertion oscillator. The oscillator circuit is a Colpitts, tuned by a variable-inductance 35-mh r.f. choke. The oscillator must be tuned to exactly 50 kc by checking it against an accurate frequency meter such as the BC-221.

The output of the detector (V3) passes through a low-pass filter (L2 and the two .0016-μf capacitors) that eliminates the 50-kc component in the output. L2 may be a Burnell type S-1676 toroid or a 1-henry air-wound choke. The filter is terminated by the 30,000-ohm volume control in the grid circuit of a.f. amplifier V4-b.

Parts for SSB adapter

Resistors: 1—33,000, 2—100,000, 1—220,000 ohms, ½ watt; 2—220, 1—470, 1—1,000, 1—5,600, 1—10,000, 2—22,000, 1—30,000, 1—100,000, 2—220,000 ohms, 1 watt; 1—27,000, 1—47,00 ohms, 2 watts.

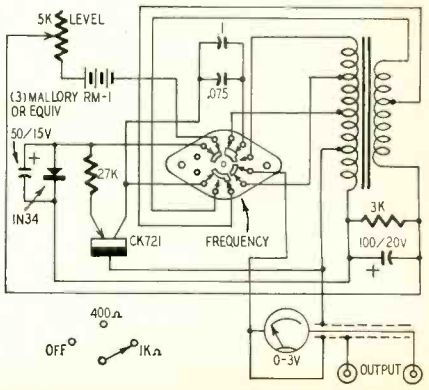
Capacitors: (Paper) 1—.03, 5—0.1, 2—0.5 μf, 600 volts; (mica) 1—10, 1—50, 2—100, 2—600 μμf; 2—.0016 μf, 500 volts; (disc ceramic) 4—.01μf, 600 volts.

Miscellaneous: 1—2.5-mh r.f. choke, 1—35-mh adjustable r.f. choke, 1—1-henry toroid or air-core inductor; 1—s.p.d.t. wafer switch, 1—s.p.s.t. toggle switch; 1—Burnell S-15000 filter; 2—FT-241 type low-frequency crystals (see text); 2—6SB7Y, 1—6J5, 1—6SN7-GT tube. Chassis, hardware, hookup wire.

Additional details on this receiving adapter and a circuit and details on the construction of a SSB generator for amateur transmitters are given in a 17-page booklet, *Single Sideband for the Amateur*, available from Burnell & Co., 45 Warburton Ave., Yonkers 2, N. Y.

TRANSISTOR OSCILLATOR

Experimenters and laboratory workers have adapted the transistor for many uses but until now its commercial applications have been limited almost entirely to hearing aids (and receivers, recently). General Radio Co. has just



entered the field of transistorized test instruments with the development of the model 1307-A audio oscillator shown in the photo and diagram.

The pocket-size instrument (6 x 3⅛ x 2½ inches) delivers 400- and 1,000-cycle signals at up to 2 volts across a 600-ohm load for checking continuity of audio systems, setting operating levels, preliminary calibration of audio equipment, and many other applications where these standard test frequencies are used. The output cable terminates in a type 274-MB double plug.

The circuit is a Hartley oscillator using a CK721 transistor. Instead of the usual tapped coil, its coil is wound in two parts to simplify the application of proper operating voltages. The coils are connected in series for oscillatory currents by the 100-μf capacitor. The emitter, corresponding to the cathode of a vacuum tube, connects to the junction of the two coils. The ends of the coils are connected between collector and base (plate and grid in a vacuum tube). The circuit is tuned by the 1- and .075-μf capacitors in parallel across the entire coil. For 1-kc operation, the inductance of the coil is reduced by tapping down from the ends.

The 27,000-ohm resistor in the emitter circuit provides degeneration needed to improve the output waveform. The output voltage, taken from a tap on the coil, is measured by a 3-volt rectifier type a.c. meter across the output terminals. The level is adjusted by varying the resistor in series with the battery. The germanium diode sets the operating bias on the base and provides more reliable operation under different battery voltages, temperatures, and transistors. Further details appeared in the August, 1954, issue of *The General Radio Experimenter*. END

Radio Thirty-Five Years Ago

In Gernsback Publications

HUGO GERNSBACK
Founder

Modern Electrics	1908
Wireless Association of America	1908
Electrical Experimenter	1913
Radio News	1919
Science & Invention	1920
Television	1927
Radio-Craft	1929
Short-Wave Craft	1930
Television News	1931

Some of the larger libraries still have copies of ELECTRICAL EXPERIMENTER on file for interested readers.

In February, 1921 *Science and Invention* (formerly *Electrical Experimenter*)

Hall Jet Relay for Recording Radio Signals, by Prof. Ralph D. Doner
Grand Opera by Radio, by Nellie Gardner
Messages at 100 Words per Minute by Radio
Stock Brokers Find Radio Useful
New Loud Speaking Telephone
Radio Weather Report

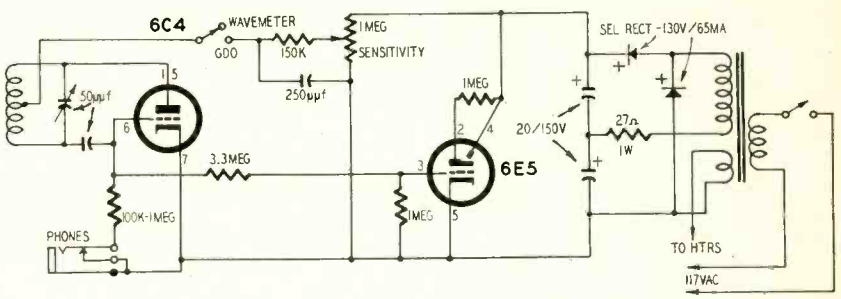
Question Box

G.D.O. MODIFICATION

The grid-dip oscillator described in the June, 1954, issue works swell. Can you show how I can add a 6C4 as a separate oscillator with a switch for disabling the circuit so it can be used as an absorption wavemeter?—R. F., Truro, Nova Scotia

Here is the diagram. In it the 6E5 is used as a vacuum-tube voltmeter to measure the voltage on the grid of the 6C4 oscillator. When the switch is closed, the 6C4 oscillates. Opening the switch removes the oscillator plate voltage. The grid-cathode circuit of the 6C4 acts as a diode rectifier with the grid resistor as the load. The 6E5 indicates this voltage when the unit is used as a wavemeter. Try different values for the grid resistor and use the value giving highest sensitivity.

The phone jack permits the instrument to be used as a diode monitor or as an oscillating (regenerative) detector.



YAGI ANTENNA QUERY

I am having trouble matching a 10-element home-made Yagi antenna to a 300-ohm transmission line, using ¼- and 1-inch tubing in a 2-conductor folded dipole. Please tell me what spacing to use between the dipole conductors when the antenna resistance is 20, 15, 10 and 5 ohms.—G. A., Uniontown, Pa.

The impedance-transformation nomograms in *The Radio Amateur's Handbook* and *Sylvania News* show that the conductors you have selected are not practical for the stepup ratios you desire. Your conductors have a diameter ratio of 4 to 1 so the center-to-center spacing is 0.775 inch for an antenna resistance of 10 ohms, 0.85 inch for 15 ohms and 1.075 inches for a 20-ohm antenna. Subtract the sum of the conductor radii from the spacings indicated and you will see that they will be difficult to attain.

The best bet is to increase the ratio of the conductor diameters to at least 7. Higher ratios increase the conductor spacing and make it easier to attain and hold. If you substitute No. 8 aluminum ground wire (approximately 0.13-inch diameter) for the smaller conductor, the ratio is 7:7 and the spacings are 0.865, 1.105 and 1.43 inches for antennas of 10, 15 and 20 ohms, respectively.

You can obtain the same results by increasing the diameter of the larger conductor to 2 inches. The center-to-center spacings are 7, 9 and 12 times the diameter of the smaller conductor for impedance stepups of 30, 20 and 15 times, respectively.

The nomograms do not provide for impedance stepups higher than 30 so for a 5-ohm antenna you can use dipole conductors to step up the impedance to 150 ohms and then use a quarter-wavelength transformer to double the resulting impedance to match a 300-ohm lead-in.

A.F.C. FOR FM TUNER

The November, 1954, issue carried an article describing how a.f.c. can be added to FM tuners. The reactance tube for this circuit is a 6K4—a subminiature type that is expensive and difficult to locate. Please show how I can substitute a more common and less expensive tube.—J. L. J., Highland Falls, N. Y.

The 6K4 was listed in more than one 1954 parts catalog, but appears to have been dropped in 1955 issues. The diagrams at *a* and *b* show typical reactance-tube circuits using a 6J6 and a 6AB4 or half of a 12AT7. In some sets a small amount of fixed bias is applied to the cathode of the circuit at *b* through a

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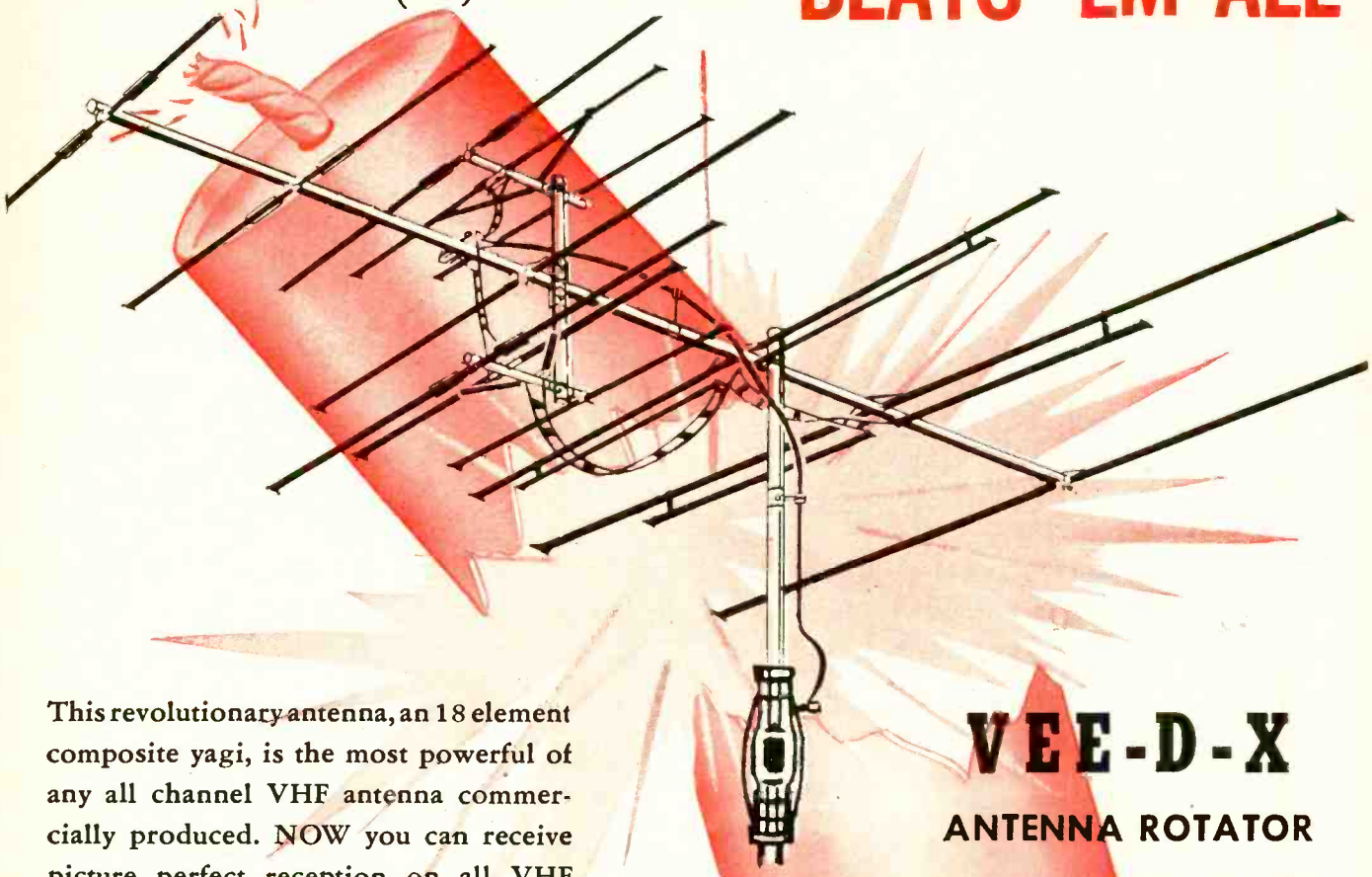

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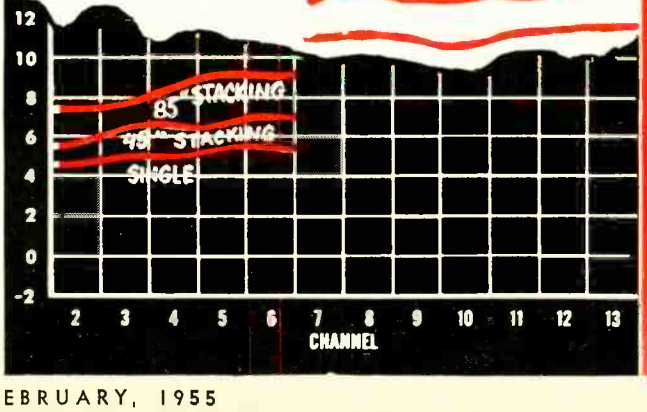

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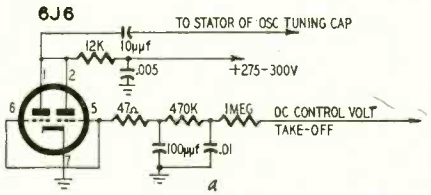
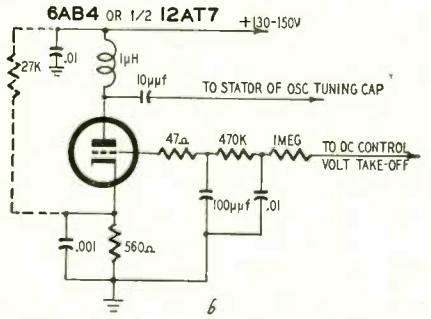
QUESTION BOX *(Continued)*

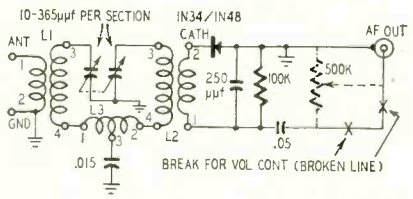
27,000-ohm resistor from the 130-volt B plus line as shown by the dashed lines.





HI-FI CRYSTAL TUNER

While thumbing through back issues of RADIO-ELECTRONICS *I came across an ad describing the Miller bandpass t.r.f. AM tuner kit. The description sounds so interesting I'd like to construct one of these tuners if you will print the circuit.—J. J. M., St. John's, Newfoundland*



This unit was designed for high-quality reception of local broadcast stations. The double-tuned bandpass circuit uses negative mutual coupling to provide adequate selectivity. Bandwidth is approximately 25 kc at 2-db points when measured at 900 kc.

The crystal diode develops between .05 and 0.5 volt on stations within a radius of 20–25 miles when used with a good outside antenna 75–100 feet long. L1 and L2 are Miller 242-A antenna coils and L3 is a type EL-55 negative mutual coupling coil. A volume control can be connected as shown by the dashed lines. Break circuit at X when installing volume control.

END

Response to our query on continuing the Question Box has swamped our staff with questions. If you don't get your answer in a month or so, don't worry—we'll get to it in time. Incidentally, the Question Box will continue.

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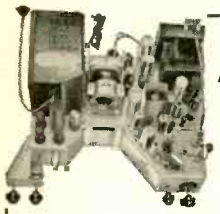

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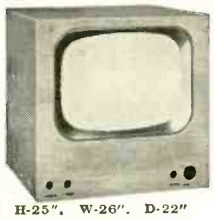

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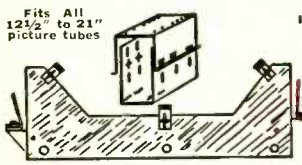

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SOUND DISCRIMINATOR TRANS.	203K1	.94
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2nd PIX I.F. TRANSFORMER,	202K3	.88
1st or 2nd SOUND I.F. TRANS.	201K1	.69
HORIZONTAL DISCRIM. TRANS.	208T8	.98
FILTER CHOKE, 62 ohms		1.15
CATHODE TRAP COIL,	202K4	.88
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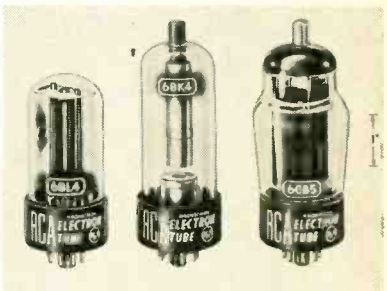
new Tubes & Transistors

6CB5, 6BK4, 6BL4

The first of a new line of receiving tubes designed for use with the RCA 21-inch color receiver has been announced by that company. The new tube types (see photo) are designed to have operating characteristics that match the circuit requirements of the



RCA 21-inch picture tube, the 21AXP22.

The 6CB5 is a high-perveance, beam-power tube designed especially for use as a horizontal deflection amplifier. Its maximum plate dissipation is 23 watts, maximum grid-2 input 3.6 watts, maximum peak positive-pulse plate voltage rating 6,800, and maximum negative-pulse voltage rating 1,500.

The 6BK4 is a sharp-cutoff beam triode designed for regulating the high-voltage supply. It has a maximum d.c. plate voltage rating of 25,000, maximum d.c. plate current rating of 1.5 ma, and maximum plate dissipation rating of 25 watts.

The 6BL4 is a half-wave vacuum-tube rectifier designed for use as a damper diode. Rated to withstand a maximum peak inverse plate voltage of 4,500, it can supply maximum peak plate current of 1,200 ma and maximum d.c. plate current of 200 ma. When the heater is operated negative with respect to the cathode, negative peak pulses between the heater and cathode of as much as 4,500, including a d.c. component of up to 900 volts, may be used.

7AU7

Another release by RCA is the 7AU7, a medium-mu twin triode of the nine-pin miniature type. It is intended for use as a vertical deflection oscillator and horizontal deflection oscillator in TV receivers having a single 600-ma series-connected heater string. Except for changes in the heater design, the 7AU7 is like the 12AU7.

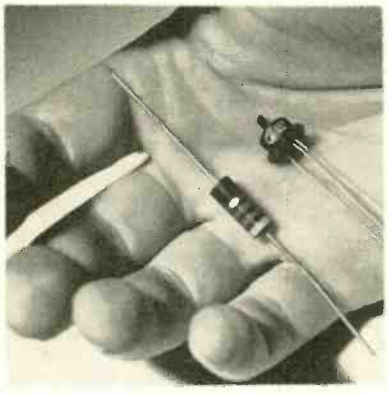
This tube may also be use as an audio mixer, phase inverter, multi-

vibrator, sync separator and amplifier, and resistance-coupled amplifier.

The design features of the 7AU7 include a strengthened mount structure to minimize microphonic effects, a terminal for each cathode and a mid-tapped heater which will permit operation from either a 7-volt or a 3.5-volt supply.

2N76

GE has announced development of a new, low-cost (suggested list price, $7.95), fused-junction transistor, the 2N76. The transistor (see photo) was



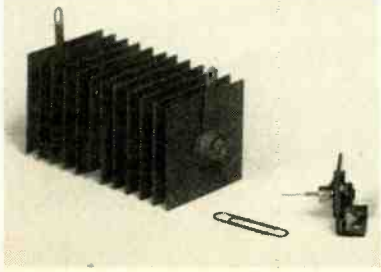
designed to cover a broad specification range. Designers and hobbyists interested in developing and experimenting with transistor circuits now have available a stable, relatively inexpensive component. The unit is hermetically sealed.

The 2N76 was developed for use in audio and ultrasonic-frequency stages. It has a maximum cutoff frequency at 2.5 mc, with a design center at 1 mc. The alpha design center of the transistor is 0.95. Maximum ratings are: collector voltage, −20; collector current, −10 ma; emitter current, 10 ma. The 2N76 is capable of dissipating 50 milliwatts at an ambient temperature of 77° F.

Silicon power rectifier

The Transitron Electronic Co., Melrose, Mass., has announced development of experimental silicon power rectifiers. Dr. Bakalar, company president, said that theoretically these units should have infinite life as they do not exhibit a continuous aging effect as do selenium rectifiers. And because of their extremely low losses, operating efficiencies of as high as 98% are possible.

Silicon rectifiers are capable of



operating efficiently between an extremely wide range of temperatures (150° C to −60° C) and possess large power-handling ability. They can be extremely compact (see photo).

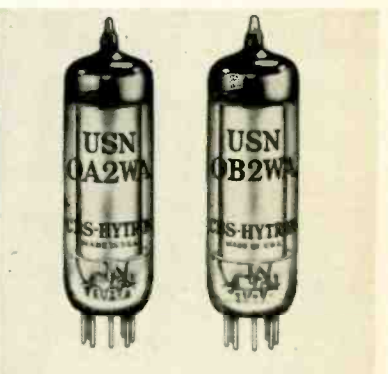
6570

RCA has announced a vacuum phototube for use in industrial applications critical as to microphonics and sensitivity. The 6570 phototube is particularly useful in beverage-inspection and ampule-inspection equipment.

The 6570 is extremely sensitive to red and near-infra-red energy, making it especially suitable for use with an incandescent light source. The tube has a maximum anode-supply voltage rating of 500, a maximum average cathode-current rating of 5 microamperes, and an average luminous sensitivity of 30 microamperes per lumen.

USN-0A2WA, USN-0B2WA

Heralded as the new VR tubes without "pips" (sudden discrete voltage shifts), CBS-Hytron has announced the USN-0A2WA and the USN-0B2WA.



These tubes are of the seven-pin miniature type.

The gaseous VR tubes are designed to provide reliable, stable operation as voltage regulators and, under specific conditions, as voltage-reference tubes. They provide flat, smooth voltage-current characteristics between 5 and 30 ma of tube current and are interchangeable with the 0A2 and0B2. END

COLOR TV

By JULIA R. SEITZ

The purple cow is not a myth
Pink elephants parade
And blue bananas by the bunch
Are garishly displayed.

You doubt my word? You think me daft?
I swear I'm no deceiver.
The proof I'll show you any day
On my TV receiver.

Patents

TV RECORDING

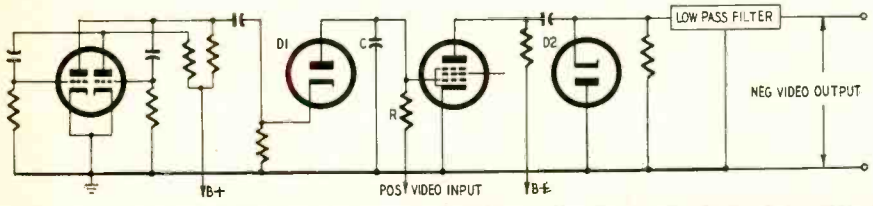
Patent No. 2,688,693
Harold E. Haynes, Haddonfield, N. J.
(Assigned to Radio Corp. of America)

TV programs are recorded on movie film for filing and rebroadcasting. The usual method is to make a negative and then make prints for distribution. Time and expense could be saved by scanning a negative image and photographing directly on positive film. This circuit converts a conventional video voltage so that it corresponds to a *negative* image.

A negative film is one whose light transmission is inversely proportional to its exposure. For example, if its exposure were increased three times, it would transmit only one-third the light. The diagram shows a circuit whose output voltage varies inversely as the input. Therefore if a conventional video signal is fed in, the output will correspond to a negative.

The double-triode multivibrator is followed by a differentiating network and diode D1. Negative pulses flow through the diode, while the positive ones block the tube. Thus C charges periodically and discharges (through R) when the diode blocks. The pentode is a sharp-cutoff tube that conducts only when C is almost completely discharged. In such a circuit, cutoff time varies inversely with the amplitude of the input signal. Thus the tube's output voltage (which is proportional to the cutoff time) also varies inversely with the input voltage.

The output of the pentode is controlled by d.c. restorer D2 and an averaging (low-pass filter) network.

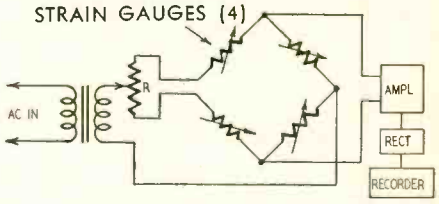


AUDIENCE REACTION

Patent No. 2,688,873
Harold Burris-Meyer, Madison, N. J.
(Assigned to Control, Inc., Jersey City, N. J.)

Psychologists know that the mental state of a person is reflected in his physical attitude and movements. For example, a bored viewer may become fidgety and restless while watching a film or listening to a speech but an interested one leans forward in his seat. This invention measures the movements and positions of a sitting person without his becoming aware of it.

Strain gauges are placed beneath the seat of the person to be tested. In one system four such



gauges are used. Two of them measure changes in the vertical stress (right and left). The others detect changes fore and aft. Each gauge is made of a grid of wire imbedded in a plastic sheet. Its resistance varies when the sheet is bent, stretched or otherwise deformed.

The gauges are used as arms of a bridge network, fed by an a.c. source. The bridge is initially balanced by R. Resistance changes cause unbalance, indicated by the recorder.

The output of the strain gauges is fed to an amplifier to raise the signal level.

PATENTS *(Continued)*

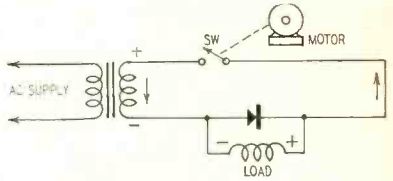
MECHANICAL RECTIFIER

Patent No. 2,673,947

Jerrold B. Winther, Kenosha, Wis.

(Assigned to Eaton Mfg. Co., Cleveland, Ohio)

Mechanical rectifiers handle greater power than other types. This rotating device, for example, delivers more than 100 volts at 2 amps. Fig. 1 shows the rectifier as a switch, controlled by a motor. The switch is closed during most of the positive half-wave (polarity is as shown in Fig. 1). It is opened during the negative half-cycle.



The transformer primary is connected to a 220-volt a.c. line. The switch closes near the peak of the positive half-wave. Electron flow is in the direction of the arrows. It feeds the load, which may be a motor field, for example. The selenium diode is blocked during this time. As the voltage wave tapers off to zero, the conductivity of the switch increases to maintain uniform output.

Just before the voltage polarity reverses, the switch opens. Due to the high inductance of the load, the current is maintained through the load in the same direction. Normally this inductive effect would cause sparking across the open switch contacts. It is eliminated here by the selenium diode which conducts the induced current through the load.

Mechanical details of the switch are shown in Fig. 2. Two brush contacts touch a conducting surface (shaded in Fig. 2) on a rotating cylinder. As it rotates, the conducting surface

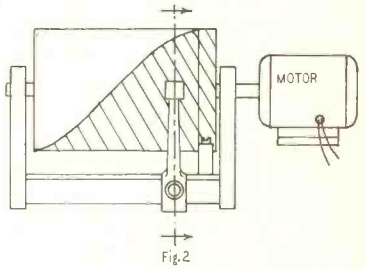


Fig. 2

increases from zero to maximum. This compensates for the drop in voltage as the a.c. wave falls off from its peak value. At the end of the positive half-wave the conducting path is broken.

One of the contacts is mounted on a sliding member so it can be adjusted. Its position controls the phasing of the switch relative to the positive half-wave. END

Technotes

HOFFMAN 301-302 CHASSIS

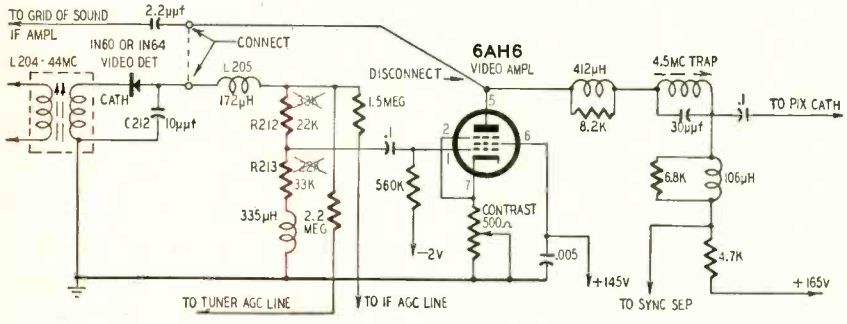
In some areas a buzz problem has been encountered due to modulation at the transmitter. This has been cured by shifting the sound take-off point from the plate of the 6AH6 video amplifier to the junction of L205 and C212 immediately after the video detector, as shown in the diagram. Note also that the values of R212 and R213 have been interchanged.

In areas where greater horizontal and vertical sync stability is needed add a .005-μf, 500-volt capacitor across the horizontal hold control and change the value of C602 (the capacitor between ground and the junction of the 47,000- and 10,000-ohm resistors between the blue lead on the vertical output transformer and pin 1 of the 12AU7 sync separator) from .001 μf to a .0047-μf, 400-volt unit.

• To increase the range of the vertical hold control, add a 680,000-ohm, ½-watt resistor between the center tap and the ungrounded side of the control. Also, add a 470,000-ohm, ½-watt resistor from the ungrounded side of the vertical hold control to the blue lead of the blocking oscillator transformer.

The changes described have been made in later production runs of these chassis.

If feedback occurs on channel 7, redress the speaker leads away from the antenna lead-in.—*Hoffman Service Bulletin*

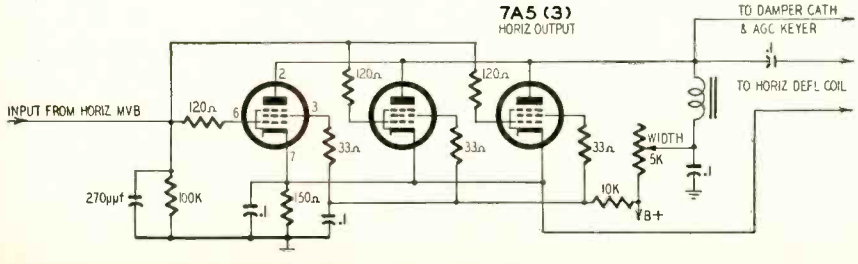


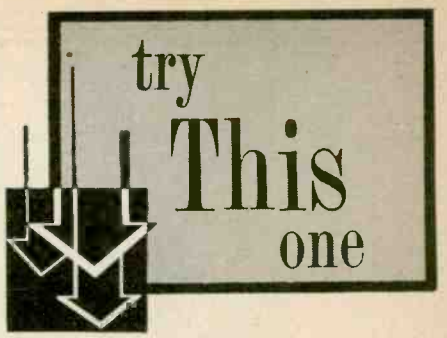
ZENITH G510

After a few weeks of operation the 35W4 rectifier in these models burns out. The heater string on these sets starts at the pilot light tap. This causes excess voltage to be applied to the heater string, reducing the normal life of the tubes. Connecting the line to pin 4 instead of 6 reduces the heater voltage and will result in longer tube life.—*Wayne Miller*

WESTINGHOUSE 600T16

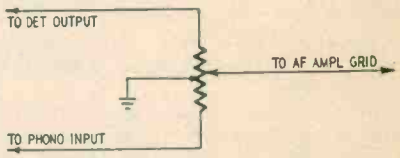
In this set, lack of horizontal deflection can be assumed to be caused by a defective yoke. However, before replacing the yoke, replace the 0.1-μf capacitor between ground and the junction of the width control and the horizontal output choke. It is good practice also to replace the 0.1-μf capacitor between the deflection amplifier plates and the horizontal yoke winding. Position of this capacitor can be seen in the partial schematic.—*Wilbur Hantz* END





SIMPLE PHONO CONNECTION

Frequently radio technicians are called in to add a phono connection to a radio or TV set. Conventional adaptations require the installation of a phono-radio switch. However, when the set owner does not want an extra control knob or is afraid that drilling the mounting hole will mar the set, you can



use a simple trick that will prove satisfactory.

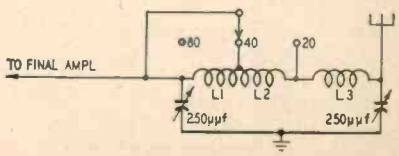
Replace the present volume control with a center-tapped type having twice the resistance of the original. Wire the arm, tap and counterclockwise end of the new control to the leads removed from the arm, ground and hot end, respectively, of the old control. Connect the phono input jack or terminal to the remaining contact on the control.

The revised circuit appears as in the diagram. The center position of the control produces zero volume. Turning the knob clockwise brings up the radio volume and turning it counterclockwise from center brings in the phonograph. —*J. Sareda*

NOVEL PI NETWORK

Pi networks are widely used as antenna couplers and as final tank circuits to minimize harmonic radiation and to simplify matching the rig to single-wire and unbalanced antennas. Separate plug-in coils or expensive variable inductors are used when the rig is operated on several bands.

The diagram shows how I modified a standard center-tapped tank coil to cover the 80-, 40- and 20-meter bands. L1 and L2 are halves of an 80-meter coil with the link removed. We removed three turns from L2 to hit 40 meters. L3, used alone for 20 meters, is a 10-turn section of B & W type 3015 Miniductor (1 inch in diameter, 16 turns per inch). This coil is supported by its leads and is positioned alongside the larger



coil and about ¼ inch from it. One lead is soldered to the base pin connected to the 20-meter terminal on the switch and the other goes to one of the pins formerly used for the link winding. The switch is a transmitting type with ceramic insulation.

With this arrangement the 3-band coil can be removed from its socket whenever necessary. We are not able to detect any loss of efficiency when using this tapped coil in place of separate plug in coils for each band.—*I. Queen, W2OUX*

TV SWEEP OSCILLATORS

A broadcast receiver can be used to determine whether the vertical and horizontal oscillators are functioning in a defective TV receiver. Tune the broadcast receiver to a vacant spot on the dial between about 1490 and 1550 kc. Turn the volume up full. Rotate the horizontal hold control through its range. If the circuit is oscillating, you will hear the horizontal oscillator as it changes frequency. If a picture carrier is coming in and sync pulses are reaching the a.f.c. tube, you will hear a high pitched whistle as the oscillator is brought into sync and a steady hum when it locks in.

When the vertical oscillator is functioning, it produces a buzz that changes frequency as the vertical hold control is rotated. A small battery-operated portable receiver is handy for making these tests on home calls.—*John Mayo*

USING PLASTIC SPRAYS

Exposure to air causes oxidation that decreases the holding power of friction and electricians' rubber tapes and causes them to peel, fray and crumble. When using these tapes for a more or less permanent connection, try spraying the completed wrap with plastic spray. This prevents oxidation and protects against moisture penetration.—*Charles Erwin Cohn*

SOLDERING LUGS

It is a good idea to put a lock washer under a soldering lug before fastening it down with a screw or a nut. This makes it easier to position the lug because the washer keeps it from turning as the screw or nut is tightened.—*J. Sareda*

SHAFT COUPLING HINT

I have found standard shaft couplings a source of irritation and costly callbacks because the setscrews often loosen with ordinary use. I licked the problem with a stick of ferrule cement available at any fishing tackle shop.

Remove the setscrews from the coupling and melt some of the cement into the tapped holes. Heat the coupling to make the cement flow. Replace the screws and screw in tight while the coupling is still hot. When the coupling cools, the screws are locked tight and cannot shift. They cannot be removed without first warming the coupling.—*Alan M. Palmer* END

Business

Merchandising and Promotion

Jensen Industries, Forest Park, Ill., is now merchandising its phono needles in white leatherette-covered boxes. The

company is shipping assortments of ten diamond needles in a metal strong box which the dealer may keep for storage or as a cash box.

ORRadio Industries, Opelika, Ala., is under way on the largest consumer advertising campaign in its history on its line of Irish Brand magnetic sound recording tape. The company is also holding a special promotion during the months of January and February during which six 1,200-foot reels of home recording tape are offered for the price of five.

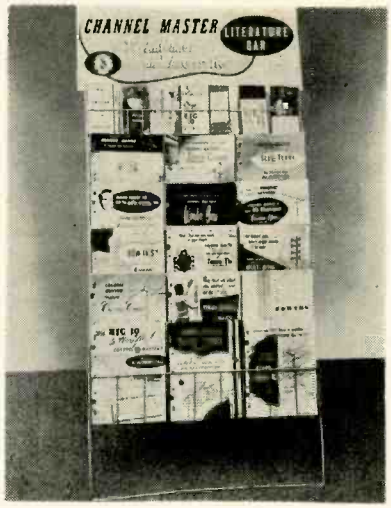
Simpson Electric Co., Chicago, is continuing its series of color and black-and-white TV service meetings. Demonstrations were recently held in California and Arizona.

Cornish Wire Co., New York City, designed a series of counter display cartons for its products.

JFD Manufacturing Co., Brooklyn, N. Y., which celebrates its 25th anni-

BUSINESS *(Continued)*

versary this month, is planning a year-long advertising and promotion program to celebrate the event.



Channel Master Corp., Ellenville, N. Y., designed a literature display rack for its distributors. It will accommodate 22 different pieces of literature.

Electrovox Co., Inc., East Orange, N. J., created a new package for its Walco replacement needles.

General Electric, Syracuse, N. Y., is now packaging its replacement germanium diodes in plastic envelopes mounted on colorful counter display cards. The company also designed a counter shadow-box dealer aid for its TV receiving tube line.

CBC Electronics Co., Philadelphia, is merchandising its high-fidelity interconnecting cables on a rotating display merchandiser.

Calendar of Events

Audio Fair. Los Angeles, February 11-13, Alexandria Hotel, Los Angeles.

National Conference on Transistor Circuits, February 17 and 18, Irvine Auditorium, University of Pennsylvania, Philadelphia, Pa.

1955 Joint Western Computer Conference And Exhibit, March 1-3, Statler Hotel, Los Angeles.

1955 IRE Show, March 21-24, Kingsbridge Armory, Bronx, N. Y.

Fourth Regional Seminar for Parts Distributors, April 1-2, Paxton Hotel, Omaha, Neb.

Ninth Annual Spring Technical Conference of the Cincinnati Section of the IRE, April 15-16, Engineering Society of Cincinnati Building, Cincinnati, Ohio.

1955 High-Fidelity Show, September 30-October 2, Palmer House, Chicago.

Production and Sales

RETMA reported production of 5,654,791 TV sets and 8,040,230 radios for the first ten months of 1954 as against 6,204,803 and 11,201,656 for the 1953 period. The association noted that average weekly production of TV sets for October, 1954, was at the highest level on record. Retail sale of TV sets for the first nine months of 1954 reached 4,645,063 compared to 4,300,360 for the 1953 period. Radio sales for the 1954 period were 4,032,704 as against 4,526,186 for the 1953 period.

BUSINESS *(Continued)*

RETMA announced that manufacturers had sold 6,476,566 cathode-ray tubes worth $134,922,387 during the first nine months of 1954 compared with 7,552,862 tubes valued at $179,133,671 for the 1953 period. Receiving tubes sold during the period totaled 266,050,907 compared with 347,152,450 for the 1953 period.

New Plants and Expansions

Raytheon Manufacturing Co., Waltham, Mass., is constructing a large electronics engineering and research laboratory in Wayland, Mass.

Shure Bros., Chicago, manufacturer of acoustic devices, announced plans to begin construction on a new 80,000-square-foot plant in Evanston, Ill., which it hopes to finish by spring, 1956.

Sprague Electric Co., North Adams, Mass., has begun construction of a 13,000-square-foot building in Venice, Calif., to house all its Southern California operations. It is expected to be completed by spring.

Precision Apparatus Co. and its meter manufacturing subsidiary, Pace Electrical Instrument Co., are now located in a new plant in Glendale, L. I., N. Y.

Davis Electronics, Burbank, Calif., purchased the Vaaro Electronics Engineering Co. which it will operate as a division.

Daystrom Inc., Elizabeth, N. J., which owns about half the capital stock of Weston Electrical Instrument Corp., purchased the assets of the American Gyro Corp., Santa Monica, Calif., which it will operate as a subsidiary.

Motorola Inc., Chicago, purchased the car radio tuner manufacturing facilities of Lee J. Drennan, Inc., Arcade, N. Y.

James B. Lansing Sound Inc., Los Angeles, added a 10,000-square-foot cabinet plant adjacent to its main office. The company also opened a warehouse in Atlanta, Ga.

Aerovox Corp., New Bedford, Mass., acquired the outstanding stock of Henry L. Crowley & Co., West Orange, N. J., manufacturer of powder-irons and steatite products.

General Electric, Syracuse, N. Y., plans to enter complete engineering and manufacturing of germanium rectifiers and diodes in its Clyde, N. Y., plant, transferring engineering design and development of rectifiers and diodes from its Syracuse headquarters.

Kay Lab, San Diego, Calif., electronics firm, plans to begin construction of a new building as the first step in its expansion program.

Show Notes

RADIO-ELECTRONICS will exhibit at the Audio Fair, Los Angeles, in February. M. Harvey Gernsback, Editorial Director of the magazine, will be present. END

NOW a complete, practical, how-to-do-it book on radio control!

RADIO-CONTROL HANDBOOK—

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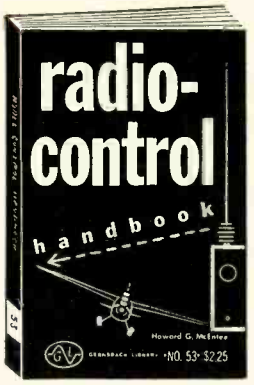

Here's a book that skips theory and gets right down to the business of putting radio-control systems together so they will operate your model planes, boats, trucks, etc.

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RADIO-CONTROL HANDBOOK concentrates on construction details of a number of practical radio-control units which will actually work and work well. It also covers the hitherto neglected field of trouble shooting radio-control systems. Whether or not you know radio, this is a book for anyone and everyone interested in R/C. For the first time, it combines the necessary practical information on radio with detailed instructions on mechanical construction of control units.

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Howard G. McEntee's experience in radio goes back some 25 years. And he has been hailed as a leader in the model field for just as long. Probably no man living knows more about the practical application of electronics in model control, than the author. Certainly no one writes about it better. Here's a book slated to become a classic on model control by radio. Be the first in your area to profit from the ideas it gives you.

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Some of the contents

Here's the perfect companion volume to Radio-Control Handbook! It covers theory as well as construction details for control units and complete systems for the beginner and more advanced fans. The author is a guided missiles instructor and winner of many awards in model-airplane meets.

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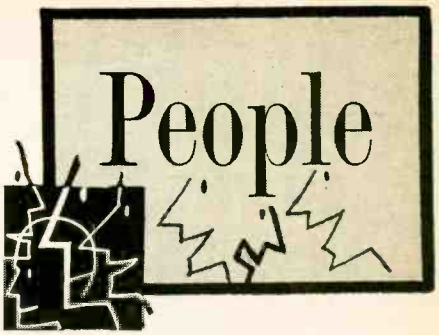


Robert G. Marchisio was promoted to vice president of CBS-Hytron, Danvers, Mass. He joined the company in 1951 as assistant to C. F. Strohmeyer, then vice president.

Adm. J. J. (Jocko) Clark joined Radio Receptor Co., of Brooklyn, N. Y., as a vice president. He was commander of the Seventh Fleet during the Korean war.

Daniel F. Shea, Jr. joined Hallicrafters, Chicago, as engineering liaison executive of the Government contract division. He came to the company from Hazeltine.

Richards W. Cotton, who has joined National Co., Malden, Mass., as assistant to the president, served in a similar capacity with Philco.

Everett E. Leedom was named advertising manager of Electro-Voice, Inc., Buchanan, Mich., and George R. Riley was appointed assistant manager of the Distributor Sales Division. Leedom was formerly with Acme Steel and Riley was a sales engineer with Electro-Voice. The company also announced the appointment of Cullen Macpherson as assistant manager of the Reproducing Components Division and Lloyd W. Loring as sales engineer. Macpherson was formerly a research assistant at the University of Minnesota, and Loring sales manager of Audio House, Inc. Lawrence L. LeKashman, vice president

E. Leedom

G. Riley

PEOPLE *(Continued)*

of sales for Electro-Voice, said the appointments were part of an expansion of the company's Sales Division.

Irving P. Wolfe joined Walsco Electronics Corp., Los Angeles, as Eastern sales manager. He was formerly with Chief Electronics.

Frank G. Mullins, Jr. joined Fairchild Recording Equipment Co., Whitestone, N. Y., as manager of engineering and as special counsel.

Robert J. Marshall was promoted from chief engineer to head of the recently established New Product Development group. Mullins was formerly with Westinghouse.

F. Mullins, Jr.

R. Marshall

Obituaries

Richard A. Graver, vice president and director of marketing for Hallicrafters Co., Chicago, died suddenly of a heart attack while in New York for a business conference. He was 58 years old.

George B. Flood, former treasurer of Sprague Electric Co., North Adams, Mass., pased away at the age of 74 after a long illness.

Albert Brand, secretary-treasurer of Radio Merchandise Sales, New York City, died suddenly in Mount Vernon, N. Y., at the age of 46.

Leo R. Mead, technical assistant to the chief engineer of Hallicrafters, Chicago, died suddenly at the age of 51.

Personnel Notes

. . . **Gen. Walter Bedell Smith**, elected to the Board of Directors of RCA, served as Under Secretary of State from February, 1953, to October, 1954. He is vice chairman of the Board of Directors of American Machine and Foundry Co. RCA also announced the appointment of **Maj. Gen. William L. Richardson**, U.S.A.F. (Ret.), to the new post of manager, Defense Projects Coordination, Engineering Products Division. General Richardson retired from military service last July.

. . . **Carl E. Mosley**, president and treasurer of Mosley Electronics, St. Louis, Mo., was appointed general manager of the company. **George E. Mobus**, advertising manager, assumes additional responsibilities as sales manager. **Jewel Hawkins** will act as purchasing agent and production manager. **Mrs. Janet E. Lloyd** is now assistant secretary.

. . . **Charles A. Hansen,** widely known sales executive, established his own manufacturers' rep firm in Los Angeles, Calif. He was formerly distributor sales manager of Gramer Halldorson Transformer Co., where he inaugurated the company's distributor sales organization, according to James M. Blacklidge, president.

. . . **L. Arthur Hoyt** was appointed advertising manager of Allen B. Du Mont Laboratories' Cathode-Ray Tube Division, Clifton, N. J. He has been with the company since 1952 as technical writer, copywriter and editor of a house organ. Du Mont also announced the appointment of **Robert E. Kessler** as manager of its Communication Products Division. He was formerly assistant manager of the division.

. . . **Lieut. Gen. Lewis A. Pick,** former Chief of Engineers of the United States Army, was elected a director of OR-Radio Industries, Opelika, Ala.

. . . **E. Gordon Burlingham** is the new sales service manager of CBS-Hytron, Danvers, Mass. He was formerly a sales service manager of another company in the electronics field.

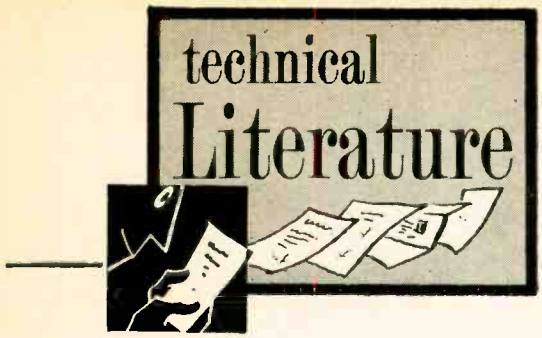
. . . **Jack Whiteside** was promoted to general manager of Simpson Electric Co., Chicago, Ill. He was formerly assistant general manager. **Larry Patterson,** former purchasing agent, was named director of material. **Al Arbeiter,** former assistant chief meter engineer, was named chief meter engineer and **Bill Coon,** former chief engineer, is now director of engineering.

. . . **George E. Bottjer,** chief pilot and manager of flight test for Raytheon Manufacturing Co., Waltham, Mass., was appointed to the Naval Aviation Advisory Committee. The company also announced that **Leslie E. Woods,** its director of industrial relations and personnel, was appointed a member of the Massachusetts Council for Employment of the Aging, for a 3-year term.

. . . **John H. Skehan** was named Southwestern sales representative for Sylvania Electric, with headquarters in Dallas, Tex. He was formerly with the General Engineering Department in Emporium, Pa.

. . . **George Mena** and **Robert Burns** were appointed district managers of the Southeast and East Central districts, respectively, of Belden Manufacturing Co., Chicago, Ill. Mena, who was formerly in the Atlanta-Richmond territory, succeeds Burns.

. . . **Richard M. Thompson** was appointed district sales manager for General Electric Tube Department distributor sales with headquarters in Schenectady, N. Y. He will cover New York State, exclusive of the New York City and Poughkeepsie areas. He was formerly a member of the distributor sales headquarters staff. END



CRYSTAL DIODES

CBS-Hytron's *Reference Guide for Crystal Diodes* lists 185 types of diodes and gives all basic data concerning them, with 18 dimensional diagrams.

CBS-Hytron, a Division of Columbia Broadcasting System, Inc., Danvers, Mass.

TEST EQUIPMENT

RCP's 8-page brochure describes and illustrates their test equipment: the a.c.-d.c. multitester, portable tube tester, wide-range signal generator, v.t.v.m., Midgetscope, Signaligner and Servishop as well as others.

Radio City Products Co., Inc., Easton, Pa.

VOLTAGE STABILIZERS

A 16-page *Catalog No. 4-260* describes voltage stabilizers and their performance. Applications for voltage stabilizers are also discussed in the catalog.

Raytheon Manufacturing Co., Dept. 6120-PR, Waltham 54, Mass.

INSTRUMENT TYPE SWITCHES

No. 17-SC, an 8-page catalog, gives data on instrument type switches and includes a simplified system for use in ordering items. Complete descriptions are given for CES rotary, shorting and nonshorting types, 1, 2 and 3 to 4 poles per deck.

Cinema Engineering Co., Division of Aerovox, Burbank, Calif.

SPEAKER ENCLOSURES

A 32-page booklet, *The Karlson Enclosure*, opens with the basic problem of what speaker baffle to use and describes the discovery of the Karlson principle. Data on the various applications best suited for the Karlson and a discussion of recommended loudspeakers.

Karlson Associates, Inc., 1483 Coney Island Ave., Brooklyn 30, N. Y.

BROADBAND AMPLIFIER

RCA's folder *3R2468* describes the new MI 5185 broadband amplifier, listing the amplifier's features and what it does. It outlines advantages of multiple distribution systems.

Radio Corp. of America, Engineering Products Division, Building 15-1, Camden, N. J.

ALLIGATOR CLIPS

Mueller's circular describes and illustrates the numerous applications in compact equipment of insulated alligator test clips. Shows how lip action of slotted insulator permits clip to bite terminal without exposing metal clip.

Mueller Electric Co., 1567 E. 31st St., Cleveland 14, Ohio.

AUDIO RECORDING SERVICES

A 12-page *Bulletin C* for 1954-55 describes the complete range of tape and disc recording services offered by Dubbings' audio laboratory for broadcast stations, sound studios, businesses, record companies, prerecorded tape firms and hi-fi enthusiasts. It covers the various types of Dubbings in use.

Dubbings Sales Corp., 41-10 45th St., Long Island City 4, N. Y.

HI-FI CATALOG

A 12-page *Altec* catalog provides

When answering advertisements please mention RADIO-ELECTRONICS

TECHNICAL LITERATURE *(Continued)*

detailed information on more than 20 high-fidelity products. Among them are AM-FM tuners, preamplifiers, amplifiers, speakers, speaker systems, horns, networks and cabinets.

Altec Lansing Corp., 8356 Santa Monica Blvd., Beverly Hills, Calif.; or 161 6th Ave., New York 13, N. Y.

HI-FI UNITS

Sightmaster's 16-page catalog on high-fidelity units includes: diamond needles, hi-fi amplifier, baffle board, cabinets, record changer, speaker accessories, speaker enclosures, AM-FM tuner, TV chassis, etc.

Sightmaster Corp., New Rochelle, N. Y.

HEATHKITS

Heath's 1955 catalog features seven new kits and describes more than 55 kits, including test instruments, amateur equipment, high-fidelity audio equipment, etc. The 48-page catalog contains technical specifications and schematics.

Heath Co., Benton Harbor 20, Mich.

Any or all of these catalogs, bulletins, or periodicals are available to you on request direct to the manufacturers, whose addresses are listed at the end of each item. Use your letterhead—do not use postcards. To facilitate identification, mention the issue and page of RADIO-ELECTRONICS on which the item appears. UNLESS OTHERWISE STATED, ALL ITEMS ARE GRATIS. ALL LITERATURE OFFERS ARE VOID AFTER SIX MONTHS.

TV ACCESSORIES

An 8-page catalog, *Mosley TV Antenna Accessories*, gives data on roof and wall insulators, TV conduit, antenna switches, couplers, sockets, etc.

Mosley Electronics, Inc., 8622 St. Charles Rock Rd., St. Louis, Mo.

COIL REPLACEMENT GUIDE

TV Technician's Coil Replacement Guide 155 cross-references all set manufacturers' coil numbers with Miller replacement numbers. Among the things listed in this 20-page guide are radio replacement coils, TV components and TV replacement components.

J. W. Miller Co., 5917 S. Main St., Los Angeles 3, Calif.

TV BULLETIN

A 4-page bulletin describes the book *Most-Often-Needed 1955 Television Servicing Information* and other books.

Supreme Publications, 1760 Balsam Rd., Highland Park, Ill.

NEEDLE CATALOG

Fidelitone, Jensen, Permo, Miller, Recoton, Walco and Duotone brands are cross-referenced to cartridges and cartridge-needle numbers in a 12-page catalog.

Permo, Inc., 6415 Ravenswood Ave., Chicago 26, Ill.

CAPACITORS

Dual-capacitor units, electrolytic capacitors, small-base oil-paper capacitors, etc., are described and illustrated in a 24-page catalog.

Pyramid Electric Co., 1445 Hudson Blvd., N. Bergen, N. J. END

RADIO SCHOOL DIRECTORY

GET INTO ELECTRONICS

You can enter this uncrowded, interesting field. Defense expansion, new developments demand trained specialists. Study all phases radio & electronics theory and practice: TV; FM; broadcasting; servicing; aviation, marine, police radio. 18-month course. Graduates in demand by major companies. H.S. or equivalent required. Begin Jan., March, June, Sept. Campus life. Write for catalog.

VALPARAISO TECHNICAL INSTITUTE
Dept. C Valparaiso, Ind.

Get Your F.C.C. LICENSE Quickly!

Correspondence or residence preparation for F.C.C. examinations. Results guaranteed.

An FCC commercial operator license means greater opportunities and higher pay. We are specialists in preparing you, in a MINIMUM OF TIME, to pass FCC examinations for all classes of licenses. Beginners get 2nd class license in 5 weeks and 1st class in 3 additional weeks. Write for free booklet.

GRANTHAM School of Electronics
Dept. 101E, 6064 Hollywood Blvd., Hollywood 28, Calif.

TV REPAIRMEN EARN TOP MONEY!

IN JUST 12 MONTHS, COMPLETE TV SERVICE TRAINING, INCLUDING COLOR TV. Streamlined course gives you all essentials for a good job as service technician. Graduates in great demand; jobs are plentiful in this growing field. Other electronic courses in radio operation and maintenance. Day or evening classes. Opportunity for employment in local industry. Approved for Korean veterans.

Write for Catalog 111 Today

INDIANAPOLIS ELECTRONIC SCHOOL
312 E. Washington, Indianapolis 4, Ind.

RADIO ENGINEERING DEGREE IN 27 MONTHS

Intensive, specialized course including strong basis in mathematics and electrical engineering, advanced radio theory and design, television. Modern lab. Low tuition. Self-help opportunities. Also B.S. degree in 27 months in Aeronautical, Chemical, Civil, Electrical, and Mechanical Engineering. G.I. Gov't approved. Enter March, June, September, December. Catalog.

INDIANA TECHNICAL COLLEGE
1525 E. Washington Blvd., Fort Wayne 2, Indiana

CODE SENDING RECEIVING SPEED

Be a "key" man. Learn how to send and receive messages in code by telegraph and radio. Commerce needs thousands of men for jobs. Good pay, adventure. Interesting work. Learn at home quickly through famous Candler System. Qualify for Amateur or Commercial License. Write for FREE BOOK.

CANDLER SYSTEM CO.
Dept. 3B, Box 928, Denver 1, Colo., U.S.A.

RCA INSTITUTES, INC.

A service of Radio Corporation of America
350 West 4th St., New York 14, N. Y.

OFFERS COURSES IN ALL TECHNICAL PHASES OF RADIO, TELEVISION, ELECTRONICS

Approved for Veterans
Write Dept. RE-55 for Catalog

ENJOY 3 COLOR TELEVISION FILTER SCREEN NOW

Changes dull eye-straining black and white pictures into beautiful color tones. Seconds to attach. No tools used. Helps eliminate glare and snow in fringe areas. Order direct. Send $1 for screen size up to 16", $1.25 size 17", $1.50 size 20", $2 size 21", $2.50 size 24", $3 size 27". We pay postage except on C.O.D. orders. Satisfaction guaranteed. Inquiries from dealers also welcomed.

Zingo Products, Johnstown 13, New York

MORE JOBS *than graduates*

Electronic Engineers
Excellent opportunity for pro[fes]sional growth and advanc[e]
Interesting and [va]

Demand for our engineering graduates exceeds supply. *Effective placement.* Study in this world-famed college established 1884. Quarters start March, June, September, January.

Bach. Sc. degree in 27 months

Complete Radio Eng. courses . . . TV, UHF and FM. Also Mech., Civil, Elec., Chem., Aero. and Adm. Eng.; Bus. Adm., Acct. Small classes. Well-equipped labs. Modest costs. Prep. courses. *Write Jean McCarthy, Director of Admissions, for Catalog and Campus View Book.*

TRI-STATE COLLEGE
2425 College Avenue, Angola, Indiana

TELEVISION

PREPARE FOR A GOOD JOB!

BROADCAST ENGINEER
ELECTRONICS
RADIO SERVICING

Television Servicing

(Approved for Veterans)
SEND FOR FREE LITERATURE

BALTIMORE TECHNICAL INSTITUTE
1425 EUTAW PLACE, BALTIMORE 17, MD.

RADIO-TV ELECTRONICS

CREI graduates in big demand. ECPD-Accredited Technical Institute Curricula. New classes start monthly. Free placement service for grads. Courses: Radio Engineering, Broadcast or TV Engineering; TV, FM, AM Servicing; resident studies leading to "Associate in Applied Science" degree. Write for free catalog. Approved for vets.

CAPITOL RADIO ENGINEERING INSTITUTE
Dept. RE, 3224—16th St., N.W., Washington 10, D. C.

EARN MORE MONEY— BE A PROFESSIONAL TELEVISION SERVICE TECHNICIAN

GET DOWN-TO-EARTH PRACTICAL TV TRAINING WITH WTI EXPERTS FOR THE TOP PAYING $5,000-$10,000 PER YEAR JOBS.

UHF—COLOR—VHF

Master the latest, up-to-the-minute TV and Color TV developments QUICKLY.

SEND FOR FREE BOOK TODAY!

WESTERN TV offers real experience on live equipment in our BIG SHOPS AND LABORATORIES in the shortest practical time under expert instructors. Graduates are in big demand because they have the "field experience" necessary for immediate "bench" or supervisory positions. You learn every phase of Radio and TV servicing (AM, FM, VHF, UHF). WTI men win fast promotion . . . can demand better pay . . . develop highly profitable businesses of their own with the latest and most PRACTICAL PERSONALIZED TRAINING BEHIND THEM. You concentrate all your time on being a PROFESSIONAL TV SERVICE TECHNICIAN — non-essential math and engineering theory omitted. YOU CAN EARN WHILE YOU LEARN. Special Finance Plan.

APPROVED FOR VETERANS. Find out how you can get into the TOP PAY GROUP — Send for this fact-packed book NOW!

WESTERN TELEVISION INSTITUTE

America's Leading Television Servicing School

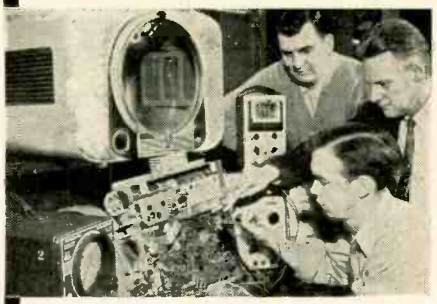
Western Television Institute Dept. E-2-55
341 W. 18th St., Los Angeles 15, Calif.
Without obligation, please send FREE fully illustrated booklet. (No salesman will call.)

NAME_____ AGE____

ADDRESS_____

CITY_____ ZONE____ STATE_____

Become an ELECTRICAL ENGINEER



Major in Electronics or Power BS Degree in 36 months

Prepare now for a career as an electrical engineer or engineering technician — and take advantage of the many opportunities in these expanding fields.

You can save a year by optional year 'round study. Previous military, academic, or practical training may be evaluated for advanced credit.

Enter Radio and Television — courses 12 to 18 months

You can be a radio technician in 12 months. In an additional 6-months you can become a radio-television technician with Associate in Applied Science degree. Color television instruction is included in this program.

These technician courses may form the first third of the program leading to a degree in Electrical Engineering. Twenty-one subjects in electronics, electronic engineering and electronic design are included in these courses.

Courses also offered: radio-television service (12 mos.); electrical service (6 mos.); general preparatory (3 mos.).

Terms — April, July, September, January

Faculty of specialists. 50,000 former students—annual enrolment from 48 states, 23 foreign countries. Non-profit institution. 52nd year. Courses approved for veterans. Residence courses only.

MS-6A

MILWAUKEE SCHOOL OF ENGINEERING

MILWAUKEE SCHOOL OF ENGINEERING
Dept. RE-255, 1025 N. Milwaukee Street
Milwaukee 1, Wisconsin
Send FREE illustrated booklets
☐ Career in Electrical Engineering,
☐ Career in Radio-Television.

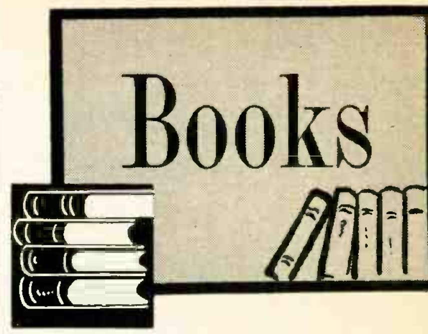
I am interested in_____
(name of course)

Name_____ Age__

Address_____

City_____ Zone____ State_____

If veteran, indicate date of discharge_____



ELECTRONICS FOR EVERYONE, by Monroe Upton. The Devin-Adair Co., 23 E. 26th St., New York, N. Y. 5¾ x 8½ inches, 370 pages. $6.

Here is a thoroughly absorbing book on the evolution of electronics. Partly biographical, partly historic and completely fascinating, Monroe Upton strikes an unusual level of presentation. *Electronics for Everyone* is a quasi-technical story, one that the novice will marvel at and the engineer will read with complete satisfaction.

Starting in ancient Greece with Thales and the discovery of amber's electrical properties and ending with Zworykin and television, the scientific achievements of titans like Faraday, Volta, Tesla, Ohm, Edison and Ampere are woven into a "human" story.

No mathematics beyond simple arithmetic is used. Every technical expression is introduced only after the necessary groundwork for understanding it is laid—there are no abstract terms.

Typical chapter titles are: Georg Ohm Writes a Law; The Marvelous Magnets of Henry; de Forest's Magic Lamp, and Superhet by Armstrong. The experiments and inventions of the famous and lesser knowns are explained.—*JK*

AUDIO AMPLIFIERS AND ASSOCIATED EQUIPMENT (Volume 5). Compiled and published by Howard W. Sams & Co., Indianapolis 5, Ind. Pages not numbered. $3.95.

Fifth of a series, this volume is a compilation of Photofact folders giving complete servicing information and technical details on audio amplifiers, preamplifiers and tuners produced in 1953 and 1954. The service technician will quickly realize the value of the voltage and resistance tables and the photos showing the location of all parts down to the smallest resistor and capacitor. The audio fan and circuit fanatic can study and compare equalizers and tone controls using R-C and L-C networks or various versions of the Williamson, Ultra-Linear and other amplifiers.

LINEAR TRANSIENT ANALYSIS (Volume 1—Lumped-Parameter Two-Terminal Networks), by Ernst Weber. John Wiley & Sons, New York. 348 pages, $7.50.

A comprehensive work giving equal emphasis to all the classical and operational methods of transient analysis. Each fundamental method is illustrated by mathematical examples.

BOOKS *(Continued)*

INTRODUCTION TO ULTRA-HIGH-FREQUENCY RADIO ENGINEERING, by Stephen A. Knight. Pitman Publishing Corp., New York. 256 pages, $4.50.

A guide to the theory, applications and techniques of u.h.f. radio, written for students, engineers and other interested readers wishing to obtain a working knowledge of u.h.f. without mathematical theory and unnecessary details. A good middle-of-the-road text filling the gap between purely engineering texts and books prepared for the radio beginner. Covers such subjects as waveguides, antennas, resonant cavities, propagation and special u.h.f. tubes.

MOST-OFTEN-NEEDED 1955 TELEVISION SERVICING INFORMATION (Volume TV-9). Compiled by M. N. Beitman. Supreme Publications, Highland Park, Ill. 192 pages, $3.

Contains schematic diagrams, drawings, photographs, waveforms, voltage and resistance tables, alignment points and frequencies and other pertinent servicing information on approximately 600 television receiver models and chassis of 26 brands. All information is as supplied by the set manufacturer.

AUDELS HOME APPLIANCE SERVICE GUIDE, by Edwin P. Anderson. Theo. Audel & Co., New York. 842 pages, $4.

Beginning with a 124-page section on electrical fundamentals, appliance testers and house wiring, the author then devotes the remaining 27 of 34 chapters to detailed servicing information including wiring diagrams and disassembly instructions on almost every type of electrical and electrically controlled appliance used in the home. The only appliances conspicuously excluded are shavers, sewing machines and water pumps. The usefulness of the book would be even greater if the author had included a chapter or two on eliminating the radio interference frequently caused by motors and thermostatic controls. END

CORRECTION

There is an error in the review of M. N. Beitman's book *Most-Often-Needed 1954 Radio Diagrams and Servicing Information* on page 153 of the November, 1954, issue. The review should read as follows: "This is the latest addition in the continued series of volumes of diagrams and service data on modern home, auto and portable radios.

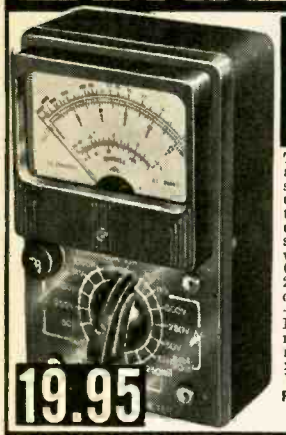
"The volume consists of reprints of data and diagrams on approximately 560 models made by 32 receiver manufacturers."

The last paragraph of this review as it was published is actually the second and concluding paragraph in the review of the NBS publication in the same column.

ADVERTISING INDEX

Radio-Electronics does not assume responsibility for any errors appearing in the index below.

LAFAYETTE'S SPECTACULAR MULTITESTER VALUES



HIGH SENSITIVITY AC-DC MULTITESTER
20,000 ohms per Volt

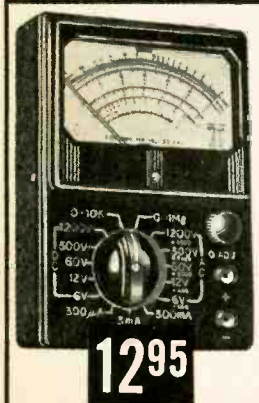
The new Lafayette High Sensitivity Multitester is a complete instrument (not a kit). Here is an instrument packed with every desirable feature found only in instruments costing twice as much. One of the most sensitive multitesters ever offered. **20,000 ohms per volt DC; 8,000 ohms AC,** having a high sensitivity 45 microamps meter. Full scale AC-DC voltage ranges are 0-10V, 0-50V, 0-250V, 0-500V, 0-1 000V; DC current ranges 50 microamps, 2.5 ma, 25 ma, 250 ma. Resistance: 0-5K ohms, 0-50K ohms, 0-500K and 0-5 megohms. Decibel range: —20 +5 db; +5 +22 db (0 db - 0.775V - 600 ohms). Extreme versatility and accuracy. 1% precision resistors; 3" meter; beautiful plastic front, with metal bottom for ruggedness. Size: 3¾" x 5¾" x 2⅝". Complete with batteries and leads. Shpg. Wt. 4 lbs.

RW-30G ..... NET **19.95**
In lots of 3 **19.25**

NEW POCKET AC-DC VOM MULTITESTER
1,000 ohms per Volt

This instrument is one of the best buys that Lafayette has ever offered in a Wide Range **AC-DC MULTITESTER.** An ideal portable unit that meets the need for a compact, yet rugged test instrument. Has ease of operation usually **FOUND ONLY IN MORE EXPENSIVE INSTRUMENTS.** Has 1000 ohms/volt sensitivity on both AC or DC. Uses full 3" rectangular meter with large easy to read scale. Uses 1% precision resistors, jeweled D'Arsonval microamp meter movement. Ranges: AC-DC and output volts 0-5, 0-25, 0-250, 0-1000V; DC current 0-1, 0-10, 0-100 MA: Resistance 0-10K and 0-100K ohms. In handsome sturdy bakelite case. Size: 4¾" x 3¼" x 1⅝". Supplied Complete with test leads and batteries. A Must for every serviceman, shop, Laboratory or experimenter—and at Lafayette's Price you can afford to own one. Shpg. Wt. 2½ lbs.

MODEL RW-27C—Complete In Lots of 3 **9.45** Single, ea. **9.95**



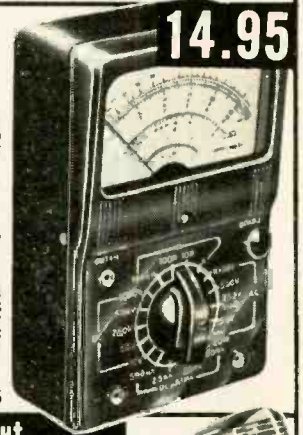
SENSITIVE AND ACCURATE AC - DC MULTITESTER
2000 OHMS PER VOLT ON BOTH DC AND AC

An unusual buy in a very accurate and sensitive VOM. Features single selector switch for all ranges. Has 3 ", sensitive 110 microamp meter, 2000 ohms per volt on both AC and DC, 21 full scale ranges, consisting of AC-DC Voltage Ranges: 0-6; 0-12; 0-60; 0-300; 0-1200 Volts; **DC Current Ranges:** 0-300 ua; 0-3 MA; 0-300 MA; **Resistance Ranges:** 0-20 K ohms; 0-2 Megohms; **Decibels:** 0 db +6 db; +20 db; +34 db; +46 db (0 db - 0.774V);

Extreme versatility and accuracy. 1% precision resistors; beautiful plastic front with metal bottom for ruggedness and shielding. Size 3⅝" x 5¼" x 1½". Shpg. Wt. 3 lbs.

MODEL RW-360 Complete
In lots of 3 **12.45**
Singly, ea. **12.95**

NEW! SLOPING PANEL MULTITESTER
2,000 Ohm per Volt Sensitivity on both DC and AC



- **High Sensitivity 3¼", 160 Microamp Meter Insures Accuracy**
- **25 Full Scale Ranges**
- **Sloping Panel for Easy Reading**
- **4 Resistance Ranges on Two Separate Scales**
- **5 Output Ranges to Measure AC with DC present**
- **Convenient Pocket SIZE 3¾"x 5¾"x 2-2/5."**

This unusual Multitester is a complete instrument (not a kit) with high quality and sensitive 160 microamp meter. Features extreme versatility, accuracy and ruggedness. In an attractive bakelite front panel, with metal bottom for ruggedness and shielding. Single switch selects all ranges; 1% precision resistors used throughout. An outstanding instrument, for the professional, serviceman or Laboratory. **FULL SCALE RANGES: DC Volts:** 0-10; 0-50; 0-250; 0-500; 0-1000. **AC Volts:** 0-10; 0-50; 0-250; 0-500; 0-1000. **Output Volts:** 0-10; 0-50; 0-250; 0-500; 0-1000. **DC Current:** 0-500 microamps; 0-2.5 MA; 0-25 MA; 0-250 MA; **Resistance:** 0-1K; 0-10K; 0-100K; 0-1 Meg; **Decibels:** +22 and +50 db (0 db - 0.755V - 600 ohm). COMPLETE with test leads and BATTERIES shpg. wt. 4 lbs.

RW-29Y ...NET **14.95** ..... In lots of 3, ea. **14.25**

Collaro
THE WORLD'S FINEST 3 SPEED AUTOMATIC RECORD CHANGER

SPECIAL **29.50** LIST PRICE ~~54.50~~

Lafayette scores again with an almost unbelievable price on the Collaro 3-speed Automatic record changer. We made a spectacular buy and we are passing the savings on to you. Here's the finest changer made. Manufactured in England—with a world-wide reputation. It plays all sizes and all speeds automatically. It's packed with quality features that the Hi-Fidelity enthusiast will appreciate: Jam-proof ball bearing mounted tone arm; automatic shut-off after last record; powerful fan cooled hum-shielded 4-pole motor with self-aligning oilite bearings; automatic muting switch; weighted ball-bearing mounted constant speed turntable; rubber drive couplings—and more! Base size 14¾" x 12¼". Depth below base 2½". Shpg. Wt. 19 lbs. Available either less cartridge with plug-in shell or with famous Turnover Ceramic or G.E. Triple-Play cartridge.

COLLARO Model 3/531 changer ..... Net **29.50**
COLLARO Model 3/531 with Turnover Ceramic cartridge ..... Net **33.50**
COLLARO Model 3/531 with G.E. Triple Play RPX-050 cartridge installed ..... Net **34.50**

45 RPM SPINDLE

Slips on in place of regular spindle, eliminating use of center inserts on 45 RPM records.

GSA Spindle ..... Net **3.23**

High Output Dynamic Microphone
Worth Many Times Its Price

At Last! A Hi-Fi Dynamic Mike for tape recorders, etc.—at a price you'd expect to pay for a good crystal mike! **14.95**

Lafayette went abroad to obtain a high quality **DYNAMIC MICROPHONE** at a price that is 70% less than any comparable dynamic microphone on the market today. Exceptionally fine for public address, recording and other general purpose use. Substantially flat response, 60-10,000 cps, assures faithful reproduction of speech and music. Impedance 40,000 ohms ±15% at 1000 cps. Output Level —55 db. Die cast metal case finished in light grey and fine chromium. Compact and light weight. Net Wt. 1 lb. Head at fixed tilt of 15°, equipped with 6 ft. well shielded low-loss special vinyl-jacketed cord. Standard ⅝"-27 thread. Dimensions 1-23/32" high, 2" wide, 3⅝" deep. Shpg. Wt. 3 lbs.

PA-19...Singly, ea. **14.95**... In lots of 3 **14.45**

RCA 807 TUBES
QUANTITY LIMITED
BRAND NEW JAN. SPECS.
STOCK NO. SP-70 **1.29**

CARDWELL UHF CONVERTER SALE!

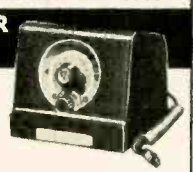
List ~~42.50~~
Net **13.95** ea. Lots of 3
Singly **14.45** ea.

Outstanding Value! The Cardwell ES-1 UHF converter covers the entire UHF spectrum—channels 14-83. Has 6AF4 oscillator, 6CB6 IF amplifier and 1N72 crystal diode. Features printed circuit oscillator, high overall gain (3 to 4 times), high sensitivity, constant L/C ratio tuner, 25-1 gear drive. Has AC cord and plug, 3-pos. switch for UHF, VHF and OFF. Handsome wood cabinet 8⅛ x 6½ x 3½" with easy reading dial. Shpg. Wt. 4½ lbs.

CARDWELL ES-1 Converter— Singly each..... Lots of 3 each..... **13.95** **14.45**

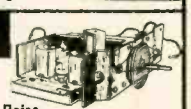
RADIART TV BOOSTER
QUANTITY LIMITED

List 29.95
6.45 ea. in lots of 3
Singly, ea. 6.95



A special purchase enables Lafayette to offer **Radiart Model TVB-1** at a fraction of their original cost. High signal-to-noise ratio greatly minimizes ghosts, snow and interference. Wide Band Amplification insures sharp pictures, free from smear. Attractive styled polished Mahogany cabinet. For 115 Volts, 60 cycles. Shpg. Wt. 4 lbs.

CROSLEY UHF FRONT END



- **Mallory 3 Gang Inductuner**
- **6AF4 — 6BZ7 and 1N72**
- **Parts Alone Worth Twice the Price**

UHF front end covers all channels 14 through 82, using the famous Mallory continuous tuning inductuner. Original replacement for Crosley part 154698-1-1 used in Crosley series EU chassis 393 and 394. Ideal for building UHF converters, etc. Output feeds into channel 5 I.F. Concentric shaft includes fine tuning. Built-in antenna switch operates off tuning shaft. Comes complete with 1N72 diode, 6BZ7 and shock mounted 6AF4 tubes. Size: 8 x 5 x 3½. Shpg. Wt. 5 lbs. Quantity limited.

TL-25.....Lots of 3, ea. **4.45**
Singly, ca. **4.95**

TIMER-SWITCH SALE

Automatically turns on radios, television sets, toasters, coffeemakers, etc.—at any pre-set time within 12 hour period; also tells time. Built-in single-pole switch handles up to 15 amps, 115 volt. Requires 3½" diameter round hole. Depth behind dial face 2¼". Shpg. Wt. 1½ lbs. **MS-62, for 110V/60 Cy AC**

BINOCULARS NEVER BEFORE AT THIS PRICE

IMPORTED DIRECT
Prism-Coated Lenses

- **All-Metal Construction**
- **Individual Focus**
- **Leather Case & Straps**

F-105, 8 x 30 with case....NET **19.95**
F-15, 7 x 35 with case....NET **22.50**
F-103, 7 x 50 with case....NET **24.95**
F-104, 12 x 50 with case....NET **32.50**

with order, Add 10% Fed. Tax

Lafayette Radio

NEW YORK, N.Y.	100 Sixth Ave.
BRONX, N.Y.	542 E. Fordham Rd
NEWARK, N.J.	24 Central Ave.
PLAINFIELD, N.J.	139 West 2nd St.
DEPT. J.B. BOSTON, MASS.	110 Federal St.

Include postage with order.
Write for FREE Bargain-Packed Catalog!

"TAB" THAT'S A BUY

METER BARGAINS

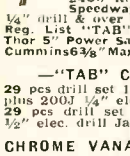
0-1 MADC/3½ Rnd $3.95
0-5 MADC/3½ Rnd 3.70
0-100 MADC/3½ " 3.50
0-1 MADC 3½ Sq. 7.00
800 VDC/3½ Sq. 8.95
1500 VDC/3½ Rnd 4.95
150 VAC 3½ Sq..... 4.95
5 MA/DC Tuning Meter/AN $1.39; 3 for.....$4.00
Weston 120 MA/RF/3" Rnd/301.....10.95

OIL CONDENSERS FRESH STOCK

1.3 MFD/2400WVDC $1; 12/$8
25 MFD/1000WVDC $8; 2/$14
26 MFD/1000WVDC $8; 2/$14
48 MFD/1000WVDC $11; 2/$18
0.25 MFD/1200WVDC* (tubular oil 30c; 5 for.....$1
0.38 MFD/2400WVDC* 29c; 6 for.....$1
1.4 & 0.3 MFD/1800WVDC $2; 3 for....$5
2X0.31 MFD/3200WVDC* 29c; 12 for...$2
2X0.44 MFD/2800WVDC* 49c; 6 for $2.50
2X.76 MFD/2400WVDC* 29c; 6 for.....$1
*Kit one each all six $1.50

HQS. FOR ALL TOOLS

CUMMINS BALLRITE 44 ¼" Elec. Drill



Perm-Align gears. All Ball-bearings. Jacobs chuck. 1800 RPM/115 VAC. Ind. Quality.....$22.50
Speedway 200J ¼" drill w/ chuck 2400 RPM.....$14.25
Speedway 400J ½" drill w/ chuck 2400 RPM.....$29.95
Speedway 200J Kit, incls. 200J ¼" drill & over 30 pieces.....$25.50
Reg. List "TAB".....$18.95
Thor 5" Power Saw (90°+45° cut)....$22.35
Cumminș63⅜" Maxsaw (90°+45°cut)..$39.95

—"TAB" COMBO SPECIALS—

29 pcs drill set 1/16" to ½" w/¼" shank plus 200J ¼" elec. drill.....$23.95
29 pcs drill set 1/16" to ½" plus 400J ½" elec. drill Jacobs Chuck.....$37.50

CHROME VANADIUM SPEED DRILLS

60 pcs set #1 to 60 C.V. $5.95
29 pcs set 1/16" to ½" by 64ths, ¼" shank, wood case $9.95
5 pcs Wood Bit set ¼" shank ¼"to½"....$1.98
13 pcs set 1/16" to ¼" w/index $1.98
Hand Saw, Swedish steel cross cut.....$3.98

¼" DRILL ATTACHMENTS

ROTO Sabre Saw..$8.05 lots of 3; $8.95 ea
ROTO Hacksaw.....4.04 lots of 3; 4.50 ea
Roto Hcksw Snder $6.74 lots of 3; $7.50 ea
ROTO Buzzsaw ..... 9.67 lots of 3; 10.75 ea

CUMMINS "DO IT" SHOP

Home Workshop, 7 power tools in 1. Powered by Ball-Rite 4¼" elec. drill. Reg. $79.95; "TAB" special.....$64.98
Write for Complete Details

REPAIR KITS

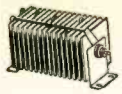
#873 Utility Kit: Incls. (4) interchangeable screwdriver blades & handle, electrician's pliers, adj. wrench, long nose pliers & wrap around case $2.69
#874 Buddy Kit: Incls (5) interchangeable screwdriver blades & handle, 3 ft. steel tape rule, diagonal cutter & case.....$1.79

Swiss Moly Wrench, 10 way wrench w/1001 uses. Fits 95% all sizes. Sq. & hex head nuts & bolts ¼" to 9/16". Rustproof. Spec. (postpaid U.S.A.) 98c; 6 for.....$5

FAMOUS SOLDERING GUNS

TA S-4 Soldering Gun 135W.....$7.89
TA 10 Soldering Gun 180 W at tip.... 5.83
TA D-4 Dual Heat 100-150W..... 9.65
Lenk Soldering Gun, the best..... 7.45

"TABTRON" SELENIUM RECTIFIERS



We mfg. Power Rectifiers to your specs. From 1 amp. up to and above 1000 amps. Following List. Full Wave Bridge. Dated 1 Yr. GTD.

Curr.	18/14.	36/28.	72/56.	130/100
Cont.	Volts	Volts	Volts	Volts
1AMP	1.35	2.35	4.60	7.50
2AMP	2.00	2.75	6.00	9.25
3AMP	2.95	4.15	7.90	12.90
4AMP	3.50	6.50	14.50	22.00
6AMP	4.10	8.00	17.50	29.95
10AMP	5.95	11.50	25.00	41.50
12AMP	7.50	14.50	30.00	44.50
20AMP	12.00	23.00	49.00	72.00
24AMP	14.50	29.00	58.00	81.50
30AMP	18.00	34.50	72.00	110.00
36AMP	22.50	42.50	88.00	135.00
50AMP	29.75	54.50	105.75	175.00

Rectifiers to Convert 6-Volt Trickle & Reg. Battery Chgrs to 12V & 6V

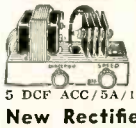
BA14/1A/$1.35; BE14/2A/$2; BF14/3A/$3
BG14/4A/$3.50; BJ14/6A/$3.50; BK14/10A/$6
Includes Data for Conversion BCT 2/2A, 12 & 6V Battery Charger.....$5.98

—100% SATISFACTION GTD—

HEAVY DUTY BATTERY "Fast" Charger Rectifier

13-0-13V (CT) 100 Amp Fan Cooled or 34 Amp Air Cooled. Replmt's 6V Booster Charger. Model CR16 ..$10 @ 3 for $27
16-0-16V (CT) Fan Cooled. For 12V/60A and 6V/100A Booster Chargers. Model CR30.....$11 @ 3 for $30

VARIABLE DC POWER SUPPLY



Full Wave rectification, 6000Mfd filter Condenser, fused. 6.3V or 12.6V @ 2 amp, operates 115V/60cy.
Model 2DCF.....$12.98
As above except 5 Amp Model 5DCF $22.98
5 DCF ACC/5A/1% Ripple.....$32.00

New Rectifier & Transformers

115V/60 cy inputs.

up to 14VDC at 12 Amps.	$ 19.98
up to 28VDC at 4 amps.	14.98
up to 28VDC at 12 amps.	29.98
up to 28VDC at 24 amps*	59.98
up to 28VDC at 50 amps*	117.98
up to 28VDC at 100 amps*	199.00

*Transformer has 115&230V PRI

NEW RECTIFIER CHOKES

CH07/4AMP/.07HY/.6R/10 # $7.95
CH01/12AMP/.01HY/.1R/12 # $14.95
CH004/24A/.004HY/.025R/20 # $29.95
CH001/50A Hipersil Core.....$54.00
CH0035/70A/.0035Hys/.0096R $66.00

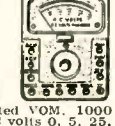
NEW RECTIFIER XFMRS

Primary 115V 60 Cyc

Sec	18-15-9-0-9-15-18 Volts
4 Amp	$8.65; 2/$15.75
12 Amp	$16.65; 2/29.95
24 Amp*	$35.75; 2/69.95
50 Amp*	$59.00/ 2/$112
100 Amp*	$108.00; 2/$210
18 Volt, 2 Amps	$1.98

*Dual primary 115 & 230V 60cy

POCKET AC-DC MULTITESTER MODEL 12C



$9.35 ea.
Lots of 3
Sold Singly $9.89
(plus 40c ship. in U.S.A.)

Hi-accuracy precision imported VOM. 1000 Ohms per/V. Reads AC & DC volts 0, 5, 25, 250, 1000V. DCMA: 0, 1, 10, 100MA. Ohms: 0, 10, 100K. Size 1¼"D, 4⅜"L, 3¼"W. Test Leads.

Model TS-52. Smallest precision built VOM, jeweled 3" D'Arsonval meter. 1000 Ohms per/V. Reads AC & DC volts 0, 10 250, 500V. DCMA: 0, 1, 250MA Ohms; 0-100K. Only 1½"D. 4"L. 3⅛"W .Test Leads. $6.89 ea. (plus 40c ship. in U.S.A.)
GTD to SATISFY or your MONEY BACK!!
Special MODEL TS-52 & 12C @ $15

NEW HIGH CURRENT PWR SUPPLIES GTD*

Variable 0-28VDC. Completely Built. Ready to Go. Full Wave Selenium Rectifier, Transformer, Variac, Volt & Amp Meters, Switch, Terminals & Fuse. In Hvy Dty Steel Cabinet. Std. 115V 60Cy Input. 110&220V†, 3 phase to order.

Stock Number	Continuous Rating	With Meters
T28V/5A	0-28 WVDC at 5 Amp	$45.00
T28V5ACC	5 Amp (1% Ripple)	$60.00
T28V12A	0-28 VDC at 12 Amp	$99.00
T28V/12ACC	12Amp (1% Ripple)	$139.00
T28V24A†	0-28 VDC at 24 Amp	$135.00
T28V/24ACC†	24 Amp (1% Ripple)	$195.00
T28V50A†	0-28 VDC at 50 Amp	$260.00
T28V/50ACC†	50 Amp (1% Ripple)	$370.00
T28V100A†	0-28 VDC at 100 Amps	$469.00
T28V/100ACC†	100 Amp(1% Ripple)	$650.00

NEW! LOW PRICED HIGH CURRENT BASIC SUPPLIES

Consisting of Transformer & Full Wave Bridge, Rectifier mtd & wired with no frills, ready to deliver DC power.

Stock Number	Continuous Rating	Basic
B28V/5A	0-28WVDC at 5 Amp	$35.00
B28V/5ACC	5 Amp (1% Ripple)	49.00
B28V/12A	0-28WVDC at 12 Amp	75.00
B28V/12ACC	12 Amp (1% Ripple)	109.00
B28V/24A	0-28WVDC at 24 Amp	110.00
B28V/24ACC	24 Amp (1% Ripple)	159.00
B28V/50A	0-28WVDC at 50 Amp	205.00
B28V/50ACC	50 Amp (1% Ripple)	319.00
B28V/100A	0-28WVDCat100Amps	395.00
B28V/100ACC	100 Amp(1% Ripple)	499.00

Now Power Your Gov't Surplus Rec'r & Transmitters from the Set Dynamoter

B28V/5A for ARC5, BC312, 342, 348 .....$ 35.00
B28V/24A for BC654 or BC375.....$149.00
B28V/100A for ARC 13.....$395.00
B12V/50A for BC191.....$110.00

"TAB" FEBRUARY BUYS

C.D. Condenser BT14/.012/25000WVDC.....$4.98; 3/$12
HS30 Cord CD622R..... 49c @ 12 for $5
IF Transformer 456KC.....49c @ 6 for $2
Pentode Output Transformer to V.C. 3 for $1
Brach MCD4 Neon Arrester.....3 for $1.00
Var. Condsr. 10 to 360 mmf Vernier 3/$2
Planetary Drive 5:1 & 1 .....spec. $2.49
Isol. Transf. vs 110 to 220 or 440/150 watt .....$4 @ 2/$7
Globar T2FD/350 ohm/500 w RF Ant. Resistor & Clips.....$2

TRANSFORMERS

All 115 V 60 Cyc Input TV, & CR pwr Xmfr up to 20" tubes. Hi VOLTS to 20KV (w/quadrupler ckt.) ALL tubes, PL & FIL wndgs. 5000 VDC/5MA. 300 VDC/275 Ma Full-Wave; 6.4V/10.3A,5.4V/8A,2.5V/3A Hypersil Core, Oil Fill 2 lbs. 2 for $22.00
2500V/20MA, 6.3V/.6A. 2.5V/1.75A for BC412 Scope Replmt.....$7.98
1600VCT/5MA, 6.3VCT/3A, 6.3VCT/10A, 2.5VCT/5A SPECIAL $7.95; 2 for $14.00
900V/35MA 2X2.5V/3A, EXCLENT 1800V DBLR TWO 2X2 FIL WNDGS.....$1.98
778VCT/200MA, 5V/3A, 6.3VCT/5A $4.98
770V/2.5MA, 2.5V/3A. HVINS HMSLD Includes FILTER PARTS. 4 scope.....$3.98
700VCT/70MA, 6.3VCT/3A.6.3VCT/2.5A, $4
550VCT/250MA, 5V/2A, 6.3VCT/2.5A, 12.6V/3.5A. CSD RCA.....$4.50; 2/$8.00
500VCT/60MA, 6.3V/4A Hmsld. $2.98
420VCT/90MA, 6.3V/1A W/INPUTS 6, 12, 24 115VDC 115 & 230 VAC @ $1.49
2X330VCT/10MA, EACH WNDG.....1.39
42V/1A/6.3V/6A.....$2.98 @ 2/$5

PRECISION LAB POTENTIOMETERS

Helipot 100 ohm/0.5% $6.49
Helipot 2000 ohm/0.5% $6.49
Micropot 20,000 ohm/0.1%.....$6.49
Helipot 30,000 ohm/0.5%/$15 Reg.$6.49
Helipot 50,000 ohm/0.5%/$15 Reg.$6.49
Wire Wound 20,000 ohm 2¾" Dia./¼" shaft, ...$1.98 ea; 2 for $3.50
Buy in Quantity.....6 for $24

SLIM-JIM HI-GAIN DYNAMIC MIKE & TILT HAND

Postpaid U.S.A. Only $3.49
Lots of 3
Hand, chest or table use. Compact width 1⅜", lght. 6" wt. only 7 ozs. W.E. Head UTC-Xfmr—50 DB/80-7500 cps. All purpose. Gtd. to Satisfy. Mobile Clamp .25c Singly.....$3.79 ea.

OIL CONDENSER BUY

4MFD 1200VDC $1.65 ea.
lots of 3
Case dimensions, not including insulators. 3½"H. 1 5/16D. 3¾"L. Sold Singly $1.79
10 MFD/600VDC.....$1.98 ea; 3/$5.25

HI-FI SPEAKERS

Inbuilt Network, 2 wires needed for HF & LF Response Famous Hi-Fi Speakers Mfgrs.
15" Coaxial Pm & 5" Tweeter. 25 watt/20-17500 cy. Model P25CO.....$19.85
12" Coaxial TM & 3½" Tweeter. 12 watt/45-15KC Spec. $12.75; 3 for $35
8" Coaxial PM & 2½" Tweeter, 8 watt/70-15000 cy Model P8CO ....$7.98; 2/$15
12" Hi-Fi PM 10 watt/35-14kc $10; 2/$18
8" Hi-Fi PM 7 watt 45-14kc $7.25; 2/$13
Tweeter 5"/12W2-15kc/16ohm $4.45
Tweeter 3½"/5w/2-15kc/8ohm $3.25
8 ohm, V.C., Alnico V, Magnets.
5-1201-A 12" P.M.E. (Demo) 25w/50-13000 cy $33.95 Reg. .....Special $17.95
12/CL/AL 12" Warfedale (Demo) 30/18000 cy $74.63 Reg.....Special $67.17
10/CS/B 10" Warfedale (Demo) 30/18000 cy $39.50 Reg.....Special $34.95
Stentorian 10" Hi-Fi Woofer & Tweeter 10w/40-20000 cy $44.50 "TAB" $23.95
"TAB" for ALL make SPEAKERS

AUDIO COMPONENTS

Electrovoice triplay cart. $1.98
GE RPX040/78 Goldtone $5.25
GE RPX041/MG Goldtone $5.25
RPX050/Dual.001&.003 $6.69
GE RPX052/Dual (DES) $17.75
GE RPX053/.001 & .003 diamonds $25.98
"TAB" GTD Phono Needle Replacements
RPJ010 Dual .001 & .003 sapphire $1.69
RPJ012 Dual .001 & .003 diamonds $20.89
RPJ001/78 or RPJ005 .001 sapphire $1.35
RPJ003/78 or RPJ004/LP diamond $10.89
RPJ013 Dual diamond & sapphire $12.89
Repl'mt needles for all phonos, specify mdl. MG or 78 Single Sapphire styli $1.15
MG and 78 Dual Sapphire $1.98, 4/$7.50
MG or 78 Sngl Diamond "Tetrad"..$10.89
MG and 78 Dual Diamond "Tetrad"..$20.89

230 TO 115V AUTOFORMERS

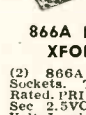
For 220-240V/50-60 cy In. To 110-120V or step-up. W/cord, Plug & Receptacle.

TPA050/50W	$2.55
TPA075/75W	$3.65
TPA100/100W	$4.00
TPA200/200W	$5.75
TPA250/250W	$6.75
TPA300/300W	$7.25
TPA500/500W	$8.25
TPA750/750W	$11.75
Model TPA1000/1000 W/1KW	$16.95
Model TPA1500/1500W/1.5KW	$22.50
Model TPA2000/2000W/2KW	$28.95
Model TPA3000/3000W/3KW	$49.95

$100 Order Take 10% Disc.

"TAB" MONEY BACK GUARANTEE

KITS* IN PLASTIC BOXES

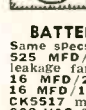


Resistors 100 ½ & 1W/95c
Tube Sockets 20 Asst'd/85c
Ceramicon Cond. 25 Asst'd85c
Controls 10 Asst'd/$1.98
Vit WW Res. 15 Asst'd/$1.45
Rotary Sw. 12 Asst'd/95c
Knobs 10 Asst'd/98c;
Buy Six Deduct 10%

866A KIT and XFORMER

(2) 866A Tubes & Sockets. Transformer Rated. PRI 115V/60cy Sec 2.5VCT/10A Hi. Volt Insulation $4.98

106 WATT SEC PHOTOFLASH KIT—AC



Includes (transf condensers two/525MFD/450V/Total 1050W/Secs. Resistors, rectifier, flash tube in indicating flash gun. guide #40 on Kodachrome. Special $33.98

BATTERY 106 WATT/SCDS KIT

Same specs, only batteries.....$32.98
525 MFD/450V/53W/Scds conds. new low leakage famous mfgr. .....$9; 2/$16
16 MFD/2500VDC/60WS/OIL $6; 2/$10
16 MFD/1.8 to 2.8KV/60WS $5; 2/$8
CK5517 mini gas rectifier.....$2.88
600 VAC Selenium Rectifier.....$4.25
1600VDC Selenium Rectifier.....$2.98
Electronic Flash Handbook ckt. data 50c

"TAB" PHOTOFLASH AND STROBE LAMPS

"Tab" No.	Replaces	W-Sec. Max	Each
TLW	FA 104/FT118	150	$ 5.98
THI	AMGLO 5804X	100	10.98
23ST	GE FT 210	200	9.98
THVA	SYLV 4330	200	9.98
V4X4	X400	200	10.98
TLX	DX & FA10Q	150	9.00
TDX	DXC/250-350	150	10.00
353GTQ	FT 503	2000	49.98
FT 105	GE FT105	150	4.29

Trigger Coil for LO&HI Volt Flash $1.47
Write for "TAB" Flash Tube Data 50c

TRANSFORMER BUY 6.3 Volt 3¾ Amp.

Continuous 115VAC input Size 2-5/16" H/2" L/11/8" W, MTG CNTR 2⅜". SPEC. Ea. 98c; lots of 12, 89c

TUBES

*From This Special List We Ship $10.00 and Up Tube Orders At Our Expense (Postpaid) Within Continental Limits of U.S.A.

90 Day Gtd. When ordering mention 2RE.

0A2	.88	6AQ6	.81	6K6	.54	7H7	.72
0A3/VR75	1.04	6AQ7GT	1.29	6K7	.58	7N7	.92
0B2	1.37	6AS7G	3.48	6K8GT	1.08	7V7	1.06
0B3/VR90	.54	6AT6	.54	6L6	1.48	7Y4	.68
0C3/VR105	.92	6AU5GT	1.10	6L6G	1.08	12A6	.48
0D3/VR150	.92	6AU6	.49	6L6GC	1.08	12AH7GT	1.45
1B3/8010	.79	6AV5GT	.98	6SA7GT	.66	12AT6	.54
1L4	.48	6AV6	.49	6SC7	.58	12AU6	.72
1L6	1.35	6AX4/6U4	.74	6SF5	.78	12AV6	.52
1P5	.78	6BA6	.49	6SF7	.73	12AU7	.59
1T4	.79	6BA7	1.09	6SG7	.64	12AV7	.98
1R4	1.29	6BC5	.63	6SH7	.61	12AW6	1.18
1R5	.59	6BC7	1.23	6SJ7	.58	12AX7	.98
1U4	.52	6BD6	.83	6SK7GT	.56	12BA6	.59
1U5	.54	6BE6	.54	6SL7GT	.64	12BA7	.94
2A4G	1.18	6BG6G	1.58	6SN7GT	.59	12BD6	.59
2X2	.42	6BJ6	.69	6SQ7GT	.62	12BE6	.59
5R4GY	1.20	6BK7	1.58	6T8	.96	12BF6	.85
5T4	1.48	6BL7GT	1.19	6U4	.74	12BH7	1.29
5U4G	.54	6BN7	2.69	6U8	.99	1208	.62
5X4G	.79	6BQ6GT	.99	6V6	1.39	12H6	.64
6AC7	.80	6BQ7	1.65	6V6GT	.59	12J5	.52
6AG5	.71	6C4	.52	6W4GT	.39	12K8	.68
6AG7	1.14	6C5	.68	6X4	.49	12Q7GT	.55
6AH6	1.21	6CB6	.59	6X5	.54	12SA7GT	.68
6AJ5	1.40	6H6	.60	6Y6G	.88	12SC7GT	.84
6AK5	.87	6J4	6.66	7A8	.68	12SF7GT	.80
6AK6	.92	6J5	.54	7C7	.66	12SG7	.54
6AL5	.48	6J6	.58	7F7	.82	12SH7	.63
6AL7GT	.98	6J7	.72	7F8	1.24	12SJ7GT	.54

12SK7	.66	CK539DX	2.19
12SL7GT	.62	CK543DX	.99
12SN7GT	.68	CK544DX	.99
12SQ7GT	.54	CK546DX	1.39
19BG6	1.98	CK571AX	2.49
19V8	1.98	CK1005	.68
25BQ6GT	.98	2050	1.48
25L6GT	.67	CK5672	1.20
25Z5	.78	CK5678	1.28
25Z6GT	.58	5687	3.74
28D7	1.94	CK5702	2.90
35B5	.52	CK5703	1.29
35L6	.67	Xtal Diodes	
35Z5GT	.54	1N21A	1.55
35Y4	.68	1N21B	2.10
45Z3	.88	1N22	1.22
50A5	.76	1N23	1.35
50B5	.54	1N23A	1.89
50C5	.54	1N23B	2.00
50L6GT	.62	1N25	4.98
RK61/XFG1	2.65	1N26	8.75
80	.58	1N27	1.55
81	1.38	1N34	.40
83	1.12	1N34A	.88
83V	1.22	1N35	1.65
84/6Z4	.62	1N38A	1.29
117L/M7GT	1.98	1N41	8.95
117Z6GT	.96	1N42	16.95
CK502AX	1.49	1N45	1.45
CK503AX	1.49	1N46	.69
CK505AX	1.79	1N47	4.00
CK512AX	1.45	1N48	.47
CK531DX	1.89	1N51	.45
CK533AX	1.89	1N54	.78
CK533DX	1.89	1N60	.40
CK536AX	.99	1N63/K63	2.49
CK538DX	.98	1N69	.98

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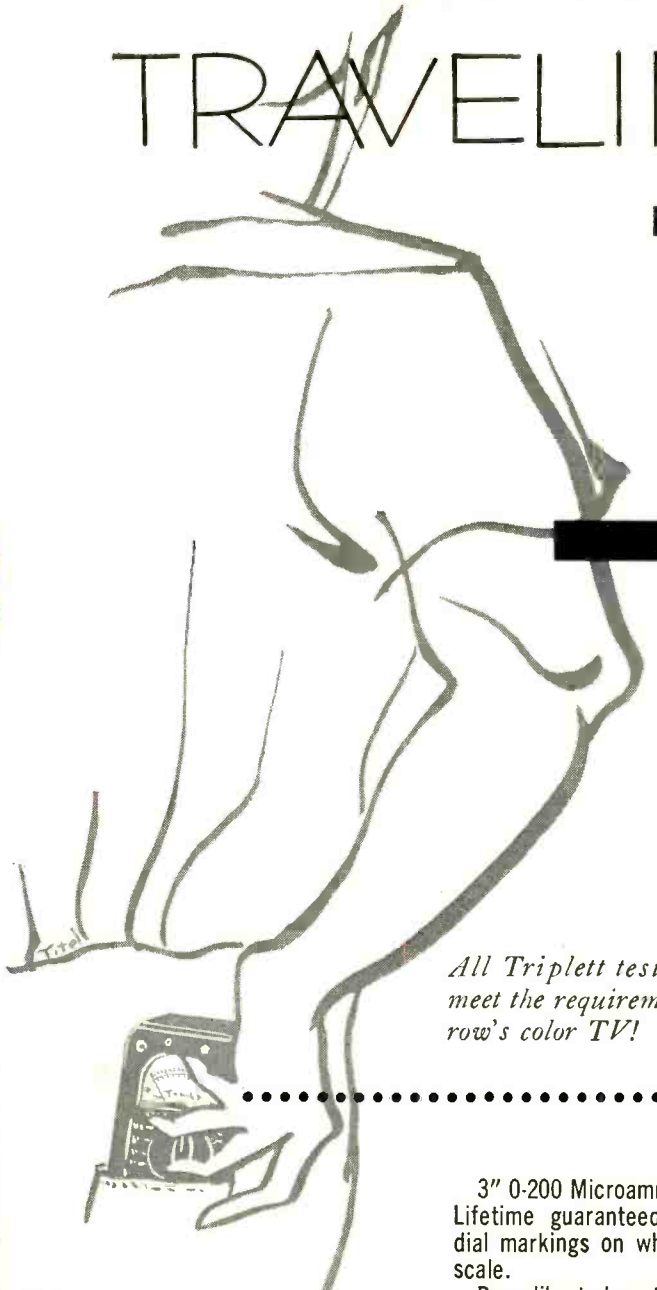

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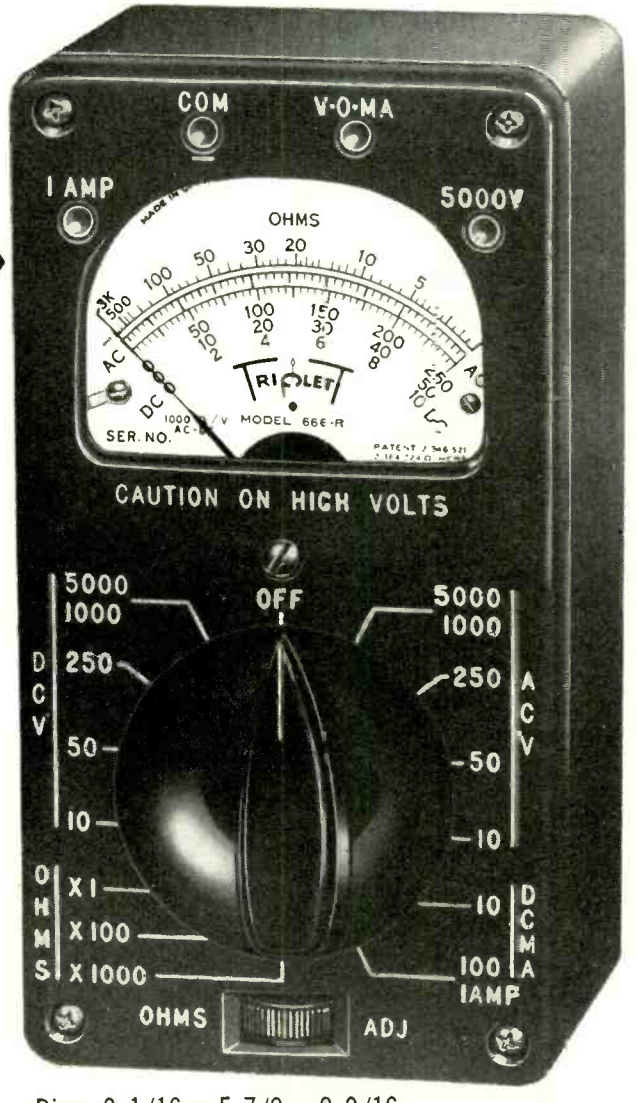

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