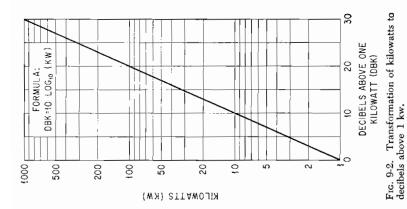
Section 9 CHARTS AND GRAPHS

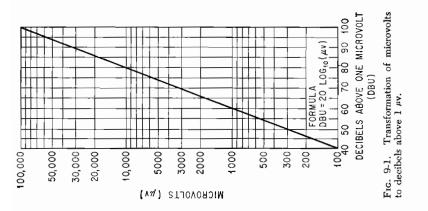
Table 9-1. Decibels

Power ratio	Voltage or current ratio	Db+	Voltage or current ratio	Power ratio	Power ratio	Voltage or current ratio	Db+	Voltage or current ratio	Power ratio
10 ⁻¹ 10 ⁻² 10 ⁻³ 10 ⁻⁴ 10 ⁻⁶ 10 ⁻⁶ 10 ⁻⁷ 10 ⁻⁸ 10 ⁻⁹	10 ⁻¹ 10 ⁻² 10 ⁻³ 10 ⁻⁴ 10 ⁻⁵	10 20 30 40 50 60 70 80 90 100	10 10 ² 10 ³ 10 ⁴ 10 ⁵	10 10 ² 10 ³ 10 ¹ 10 ⁵ 10 ⁶ 10 ⁷ 10 ⁸ 10 ⁹	0.316 0.309 0.302 0.295 0.288 0.282 0.275 0.269 0.263 0.257	0.562 0.556 0.550 0.543 0.537 0.530 0.525 0.519 0.513 0.507	5.0 5.1 5.2 5.3 5.4 5.5 5.6 5.7 5.8 5.9	1.78 1.80 1.82 1.84 1.86 1.88 1.91 1.93 1.95 1.97	3.16 3.24 3.31 3.39 3.47 3.55 3.63 3.72 3.80 3.89
1.000 0.977 0.955 0.933 0.912 0.891 0.871 0.851 0.832 0.813	1.000 0.989 0.977 0.966 0.955 0.944 0.933 0.923 0.912 0.902	0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9	1.00 1.01 1.02 1.04 1.05 1.06 1.07 1.08 1.10	1.00 1.02 1.05 1.07 1.10 1.12 1.15 1.18 1.20 1.23	0.251 0.246 0.240 0.234 0.229 0.224 0.219 0.214 0.209 0.204	0.501 0.496 0.490 0.484 0.479 0.473 0.468 0.462 0.457 0.452	6.0 6.1 6.2 6.3 6.4 6.5 6.6 6.7 6.8 6.9	2.00 2.02 2.04 2.07 2.09 2.11 2.14 2.16 2.19 2.21	3.98 4.07 4.17 4.27 4.37 4.47 4.57 4.68 4.79 4.90
0.794 0.776 0.759 0.741 0.724 0.708 0.692 0.676 0.661 0.646	0.891 0.881 0.871 0.861 0.851 0.841 0.832 0.832 0.813 0.804	1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8	1.12 1.14 1.15 1.16 1.18 1.19 1.20 1.22 1.23 1.25	1.26 1.29 1.32 1.35 1.38 1.41 1.45 1.48 1.51	0.200 0.195 0.191 0.186 0.182 0.178 0.174 0.170 0.166 0.162	0.447 0.442 0.437 0.432 0.427 0.422 0.417 0.412 0.407 0.403	7.0 7.1 7.2 7.3 7.4 7.5 7.6 7.7 7.8 7.9	2.24 2.27 2.29 2.32 2.34 2.37 2.40 2.43 2.46 2.48	5.01 5.13 5.25 5.37 5.50 5.62 5.75 5.89 6.03 6.17
0.631 0.617 0.603 0.589 0.575 0.562 0.550 0.537 0.525 0.513	0.794 0.785 0.776 0.767 0.759 0.750 0.741 0.733 0.724 0.716	2.0 2.1 2.2 2.3 2.4 2.5 2.6 2.7 2.8 2.9	1.26 1.27 1.29 1.30 1.32 1.33 1.35 1.37 1.38 1.40	1.59 1.62 1.66 1.70 1.74 1.78 1.82 1.86 1.91	0.159 0.155 0.151 0.148 0.145 0.141 0.138 0.135 0.132 0.129	0.398 0.394 0.389 0.385 0.380 0.376 0.372 0.367 0.363 0.359	8.0 8.1 8.2 8.3 8.4 8.5 8.6 8.7 8.8	2.51 2.54 2.57 2.60 2.63 2.66 2.69 2.72 2.75 2.79	6.31 6.46 6.61 6.76 6.92 7.08 7.24 7.41 7.59 7.76
0.501 0.490 0.479 0.468 0.457 0.447 0.437 0.427 0.417 0.407	0.708 0.700 0.692 0.684 0.676 0.668 0.661 0.653 0.646 0.638	3.0 3.1 3.2 3.3 3.4 3.5 3.6 3.7 3.8 3.9	1.41 1.43 1.45 1.46 1.48 1.50 1.51 1.53 1.55 1.57	2.00 2.04 2.09 2.14 2.19 2.24 2.29 2.34 2.40 2.46	0.126 0.123 0.120 0.118 0.115 0.112 0.110 0.107 0.105 0.102	0.355 0.351 0.347 0.343 0.339 0.335 0.331 0.327 0.324 0.320	9.0 9.1 9.2 9.3 9.4 9.5 9.6 9.7 9.8 9.9	2.82 2.85 2.88 2.92 2.95 2.99 3.02 3.06 3.09 3.13	7.94 8.13 8.32 8.51 8.71 8.91 9.12 9.33 9.55 9.77
0.398 0.389 0.380 0.372 0.363 0.355 0.347 0.339 0.331	0.631 0.624 0.617 0.610 0.603 0.596 0.589 0.582 0.575 0.569	4.0 4.1 4.2 4.3 4.4 4.5 4.6 4.7 4.8 4.9	1.59 1.60 1.62 1.64 1.66 1.68 1.70 1.72 1.74	2.51 2.57 2.63 2.69 2.75 2.81 2.88 2.95 3.02 3.09	0.1000 0.0977 0.0955 0.0933 0.0912 0.0891 0.0871 0.0851 0.0832 0.0813	0.316 0.313 0.309 0.306 0.302 0.299 0.295 0.292 0.288	10.0 10.1 10.2 10.3 10.4 10.5 10.6 10.7 10.8	3.16 3.20 3.24 3.27 3.31 3.35 3.39 3.43 3.47 3.51	10.00 10.23 10.47 10.72 10.96 11.22 11.48 11.75 12.02 12.30

Table 9-1. Decibels (Continued)

Power ratio	Voltage or current ratio	—Db+	Voltage or current ratio	Power ratio	Power ratio	Voltage or current ratio	Db+	Voltage or current ratio	Power ratio
0.0794 0.0776 0.0759 0.0741 0.0724 0.0708 0.0691 0.0676 0.0661 0.0646	0.282 0.279 0.275 0.275 0.269 0.266 0.263 0.260 0.257 0.254	11.0 11.1 11.2 11.3 11.4 11.5 11.6 11.7 11.8 11.9	3.55 3.59 3.63 3.67 3.72 3.76 3.80 3.85 3.89 3.94	12.59 12.88 13.18 13.49 13.80 14.13 14.45 14.79 15.14 15.49	0.0251 0.0246 0.0240 0.0234 0.0229 0.0224 0.0219 0.0214 0.0209 0.0204	0.159 0.157 0.155 0.153 0.151 0.150 0.148 0.146 0.145 0.143	16.0 16.1 16.2 16.3 16.4 16.5 16.6 16.7 16.8 16.9	6.31 6.38 6.46 6.53 6.61 6.68 6.76 6.84 6.92 7.00	39.81 40.74 41.69 42.66 43.65 44.67 45.71 46.77 47.86 48.98
0.0631 0.0617 0.0603 0.0589 0.0575 0.0562 0.0550 0.0537 0.0525 0.0513	0.251 0.248 0.246 0.243 0.240 0.237 0.234 0.232 0.229 0.227	12.0 12.1 12.2 12.3 12.4 12.5 12.6 12.7 12.8 12.9	3.98 4.03 4.07 4.12 4.17 4.22 4.27 4.32 4.37 4.42	15.85 16.22 16.60 16.98 17.38 17.78 18.20 18.62 19.05 19.50	0.0200 0.0195 0.0191 0.0186 0.0182 0.0178 0.0174 0.0170 0.0166 0.0162	0.141 0.140 0.138 0.137 0.135 0.133 0.132 0.130 0.129 0.127	17.0 17.1 17.2 17.3 17.4 17.5 17.6 17.7 17.8 17.9	7.08 7.16 7.24 7.33 7.41 7.50 7.59 7.67 7.76 7.85	50.12 51.29 52.48 53.70 54.95 56.23 57.54 58.88 60.26 61.66
0.0501 0.0490 0.0479 0.0468 0.0457 0.0447 0.0437 0.0427 0.0417	0.224 0.221 0.219 0.216 0.214 0.211 0.209 0.207 0.204 0.202	13.0 13.1 13.2 13.3 13.4 13.5 13.6 13.7 13.8 13.9	4.47 4.52 4.57 4.62 4.68 4.73 4.79 4.84 4.90 4.96	19.95 20.42 20.89 21.38 21.88 22.39 22.39 22.39 23.44 23.99 24.55	0.0159 0.0155 0.0151 0.0148 0.0145 0.0141 0.0138 0.0135 0.0132 0.0129	0.126 0.125 0.123 0.122 0.120 0.119 0.118 0.116 0.115 0.114	18.0 18.1 18.2 18.3 18.4 18.5 18.6 18.7 18.8 18.9	7.94 8.04 8.13 8.22 8.32 8.41 8.51 8.61 8.71 8.81	63.10 64.57 66.07 67.61 69.18 70.79 72.44 74.13 75.86 77.62
0.0398 0.0389 0.0380 0.0372 0.0363 0.0355 0.0347 0.0339 0.0331 0.0324	0.200 0.197 0.195 0.193 0.191 0.188 0.186 0.184 0.182 0.180	14.0 14.1 14.2 14.3 14.4 14.5 14.6 14.7 14.8 14.9	5.01 5.07 5.13 5.19 5.25 5.31 5.37 5.43 5.50 5.56	25.12 25.70 26.30 26.92 27.54 28.18 28.84 29.51 30.20 30.90	0.0126 0.0123 0.0120 0.0118 0.0115 0.0112 0.0110 0.0107 0.0105 0.0102	0.112 0.111 0.110 0.108 0.107 0.106 0.105 0.104 0.102 0.101 0.100	19.0 19.1 19.2 19.3 19.4 19.5 19.6 19.7 19.8 19.9 20.0	8.91 9.02 9.12 9.23 9.33 9.44 9.55 9.66 9.77 9.89 10.00	79.43 81.28 83.18 85.11 87.10 89.13 91.20 93.33 95.50 97.72
0.0316 0.0309 0.0302 0.0295 0.0288 0.0282 0.0275 0.0269 0.0263 0.0257	0.178 0.176 0.174 0.172 0.170 0.168 0.166 0.164 0.162 0.160	15.0 15.1 15.2 15.3 15.4 15.5 15.6 15.7 15.8 15.9	5.62 5.69 5.75 5.82 5.89 5.96 6.03 6.10 6.17 6.24	31.62 32.36 33.11 33.88 34.67 35.48 36.31 37.15 38.02 38.90	5.0100	3.100	20.0	10.00	130.00





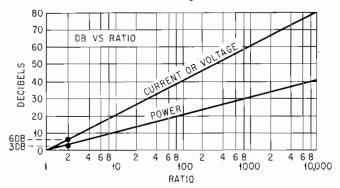


Fig. 9-3. Decibels vs. ratio.

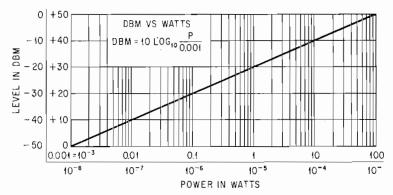


Fig. 9-4. Dbm vs. watts.

Table 9-2. Volume Level to Power and Voltage Conversion

 $\begin{array}{l} {\rm Reference\ Level} \\ {\rm 0\ dbm}\,=\,1\,{\rm mw},\,600\,{\rm ohms} \end{array}$

Milliwatts	Volts	Dbm
0.000001	0.0007746	-60
0.000010	0.002449	- 50
0.000100	0.007746	-40
0.001	0.02449	-30
0.010	0.07746	-20
0.100	0.2449	-10
1.000	0.7746	0
Watts	Volts	Dbm
0.001000	0.7746	0
0.002512	1.228	+4
0.006310	1.946	+8
0.01000	2.449	+10
0.1000	7.746	+20
1.000	24.49	+30
10.00	77.46	+40

RESISTANCE VALUES OF SYMMETRICAL ATTENUATION NETWORKS *

For ready reference and to satisfy most of the practical needs of the various artificial line pads, the following charts have been prepared:

Figures 9-5 to 9-7, inclusive, are curves for determining the three components of pads which are symmetrical but have different input and output impedances. The curves are marked to indicate pad ratios for which it was calculated, and the values of A are for the higher pad series leg resistances shown in Fig. 9-5, while C values for the lower pad series leg resistances are shown in Fig. 9-7. B is for the shunt or transverse resistor shown in Fig. 9-6.

There is a minimum loss for each impedance ratio for which a pad can be designed and for convenience each curve on the figures is terminated by a circle at the lower value of resistance which corresponds to this minimum pad loss. For L networks double the values of A and C.

Figure 9-8 gives the resistance values for the series legs A of symmetrical pads having 1-to-1 impedance ratios. Figure 9-9 gives the transverse resistance values for these pads. For values not shown multiply the value shown for 100 ohms by the ratio of the desired value to 100. Double the series leg values for L networks.

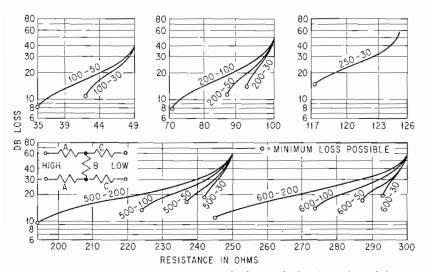


Fig. 9-5. Symmetrical attenuation networks for standard ratios-values of A.

^{*} By Frank H. McIntosh, Consulting Radio Engineer, Washington, D.C.

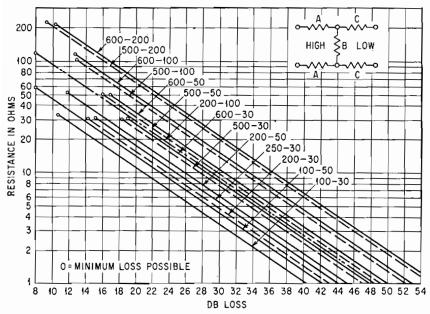


Fig. 9-6. Symmetrical attenuation networks for standard ratios-values of B.

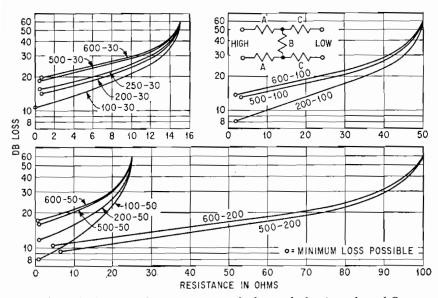


Fig. 9-7. Symmetrical attenuation networks for standard ratios-values of C.

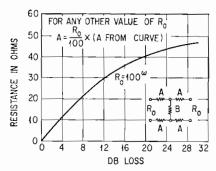


Fig. 9-8. H-type artificial line-value of series resistance A.

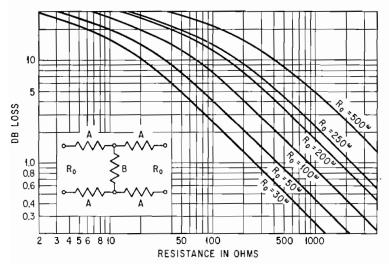


Fig. 9-9. H-type artificial line-value of transverse resistance B.

Table 9-3. Resistive Pads

$$Z_{IN} \rightarrow Z_{IN} \rightarrow Z_{OUT}$$
 $Z_{IN} \rightarrow Z_{OUT}$
 $Z_{IN} \rightarrow Z_{OUT}$

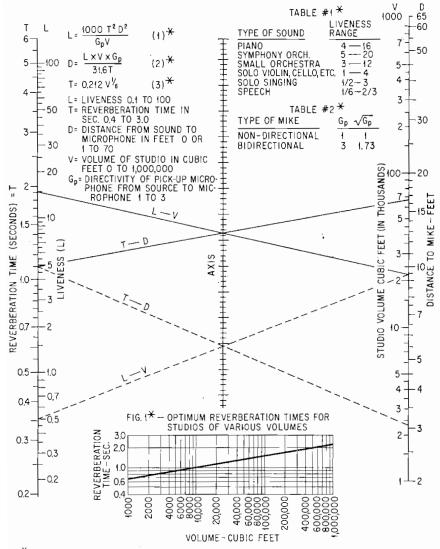
FOR IMPEDANCES OTHER THAN 600 OHMS, MULTIPLY ALL RESISTORS BY FACTOR $\frac{Z_{\rm X}}{600}$

For impedances other than 600 ohms, multiply all resistors by factor Zx/600.

$$Z_{\rm in} = Z_{\rm out} = 600 \; {\rm ohms}$$

	EL	A resistor valu	es *	T	EIA	resistor valu	es *
Loss	R_1	R_2	R_3	Loss	R_1	R_2	R_3
1/2	18	10,000	8.2	16	430	200	220
1	36	5,100	18	17	470	180	220
2	68	2,700	36	18	470	150	240
3	100	1,800	51	19	470	130	240
	130	1,200	68	20	510	120	240
5	160	1,000	82	22	510	100	270
6	200	820	100	24	510	75	270
7	220	680	110	26	560	62	270
8	270	560	130	28	5 6 0	47	270
9	300	470	150	30	560	39	270
10	300	430	160	32	560	30	300
11	330	360	160	34	560	24	300
12	360	330	180	36	560	18	300
13	390	270	200	38	560	15	300
14	390	240	200	40	560	12	300
15	430	220	200				

^{*} EIA resistor values nearest to the exact values are given.



*COURTESY OF WESTERN ELECTRIC CO.

Fig. 9-10. Nomograph for microphone distances in liveness broadcasting. (Reprinted from Tele-Tech.)

Constants V = 22,000 cu ft; T = 1.1 sec.

Example 1 (solid lines): Placement of general microphone. From Table 1 use liveness of 15. Connect 22,000 on V and 15 on L. Mark reference on the axis. Then extend a line from 1.1 on T through reference on axis to 16.5 ft on D. Answer: $16\frac{1}{2}$ ft from mike to sound source.

Example 2 (dash lines): Placement of solo vocal microphone. From Table 1 use liveness of $\frac{1}{2}$. Connect 22,000 on V and $\frac{1}{2}$ on L. Mark reference on the axis. Then extend line from 1.1 on T through this reference to 3 ft on D. For bidirectional mike multiply 3 ft by $\sqrt{3}$, or 1.73. This yields 5 to 6 ft for actual distance.

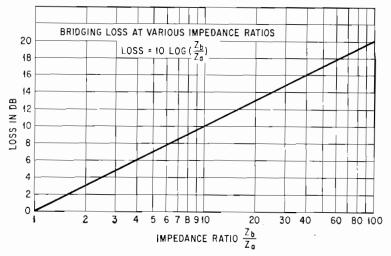


Fig. 9-11. Bridging loss at various impedance ratios. Loss = $10 \log Z_b/Z_a$.

PARALLEL-T NOMOGRAPH °

Summary: Values of five parameters for parallel-T networks are obtained directly with one setting of a straightedge, for frequencies in audio and ultrasonic ranges, to expedite the design of the network used directly in an amplifier chain to eliminate a single frequency. The same network can be used in a negative feedback path to enhance a single frequency.

This nomograph (Fig. 9-12) facilitates calculating parallel-T networks for experimental work in multiplex FM equipment design. The subcarrier frequencies used are in the range from about 20 to 75 kc. With one setting of a straightedge, all parameters of the parallel-T network needed to eliminate the undesired frequency f can be obtained to three significant figures.

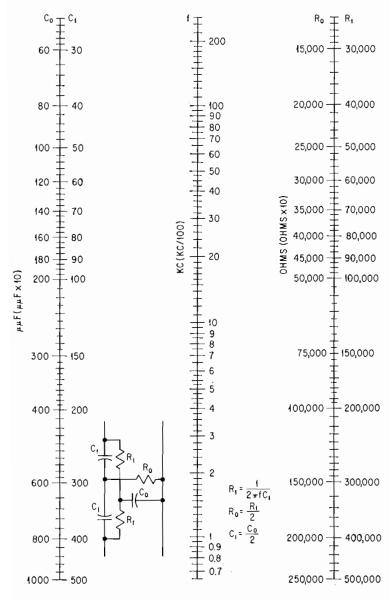
Example. If a specific frequency f of 10 kc is to be eliminated and C_1 is selected by the designer to be 100 $\mu\mu f$, run a straightedge from 100 $\mu\mu f$ on the C_1 scale through 10 kc on the f scale. All other values can now be read directly from the nomograph. Thus, R_1 is 159,000 ohms, R_0 is 79,500 ohms and C_0 is 200 $\mu\mu f$.

Any two of the five parameters can be selected as the initial starting point of design. The other three can then be found with one setting of the straightedge.

If the f scale is divided by 100, the C and R scales must be multiplied by 10. This changes the range of the nomograph to cover from 7 cps at the low end to about 2,000 cps at the high end.

For a 100-cps elimination network and a value of 1,000 $\mu\mu$ f for C_1 , these scale-multiplying factors must be used. The other parameters are then $R_1 = 1.59$ megohms, $R_0 = 795,000$ ohms, and $C_0 = 2,000$ $\mu\mu$ f.

By Donald F. Carter, Chief Electrical Engineer, Harkins and Hershfield, Phoenix, Ariz.
 Reprinted from Electronics, Nov. 1, 1957.



CENTER SCALE GIVES FREQUENCY ATTENUATED BY PARALLEL-T NETWORK Fig. 9-12. Parallel-T nomograph.

MICROPHONE NOMOGRAPH *

Summary: The chart (Fig. 9-13) relates sound pressure level, microphone sensitivity, and output in decibels and volts as an aid in the design of microphone systems and related equipment. Typical sound levels for common sounds are indicated.

Microphone response is usually expressed in decibels referred to 1 volt/dyne/cm². Thus a microphone which produces 1 volt when exposed to a sound pressure of 1 dyne/cm² has a response of 0 db. Most microphones are far less sensitive than this.

Unless otherwise specified, the open-circuit voltage is used in arriving at the response figure.

The nomograph is based on the definition of pressure response in the American Standard Specification for Laboratory Standard Microphones.

Expressed symbolically, this definition becomes

$$\rho = 20 \log \frac{e_o}{p} \tag{9-1}$$

where ρ = pressure response

 e_o = open-circuit output voltage

 $p = \text{pressure, dynes/cm}^2$

Equation (9-1) can be rewritten

$$= 20 \log e_{\mathbf{0}} - 20 \log p \tag{9-2}$$

Sound pressure is commonly expressed in decibels relative to a reference pressure $p_0 = 2 \times 10^{-4}$ dyncs/cm². When so expressed it is called sound pressure level (SPL) and is defined by

$$SPL = 20 \log \frac{p}{p_0} \qquad \text{db} \tag{9-3}$$

Equations (9-2) and (9-3) yield

$$\rho = 20 \log e_{o} - \text{SPL} + 74 \text{ db}$$
 (9-4)

Should absolute sound pressures be required, they can be filled in on the left-hand scale by noting that $100~\rm{db}=20~\rm{dynes/cm^2}$, $80~\rm{db}=2~\rm{dynes/cm^2}$, $60~\rm{db}=0.2~\rm{dync/cm^2}$, and so forth.

A microphone with a response of -50 db is to be used to measure sound levels of 35 db or more. For what minimum input voltage should the amplifier be designed?

A straight line drawn between 35 db on the SPL scale and -50 db on the ρ scale intersects the e_{σ} scale at about 35 μv . This is the open-circuit microphone voltage.

Sound level in a jet-engine test control room is 112 db; a pneumatic chipper at a distance of 5 ft has a sound level of 122 db. At takeoff and 80 ft from the tail, an F-84 has a sound level of 130 db, all typical values.

^o By William B. Conover, Transformer Laboratorics Department, General Electric Company, Pittsfield, Mass. Reprinted from *Electronics*, October, 1955.

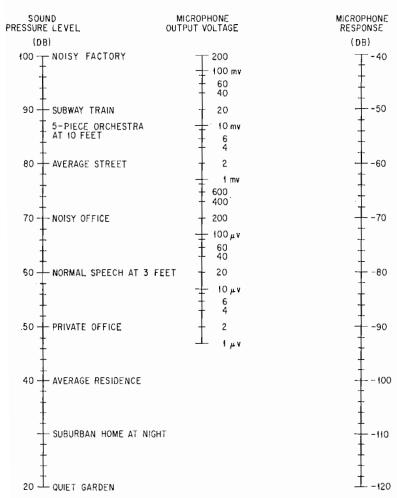


Fig. 9-13

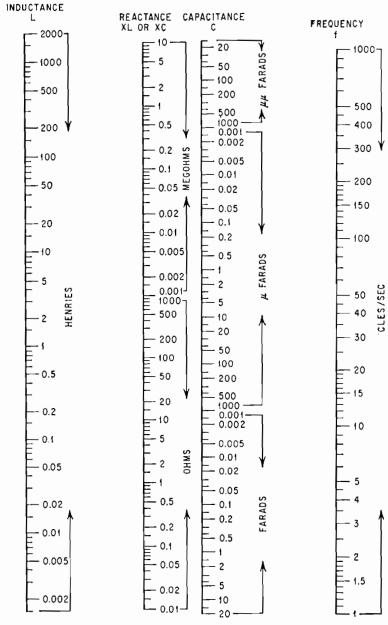
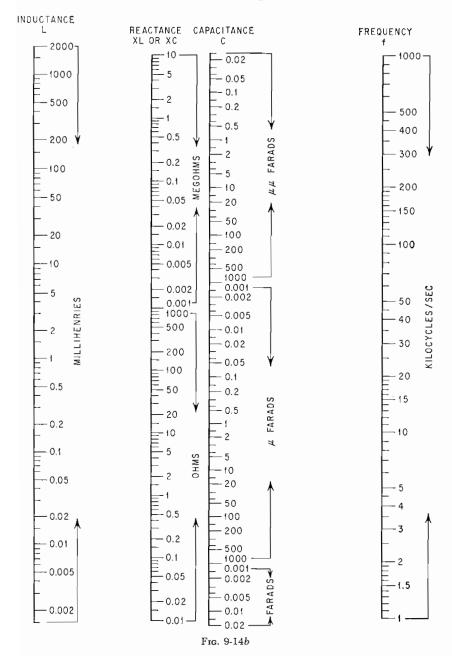
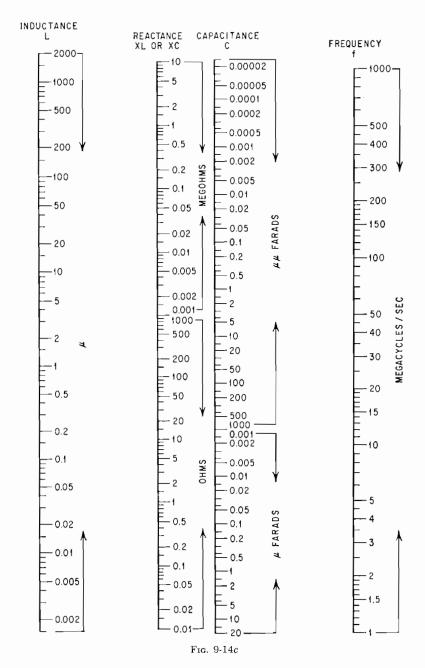


Fig. 9-14a





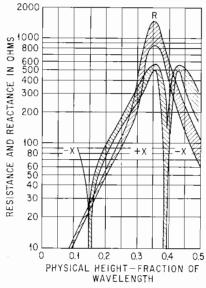


Fig. 9-15. Average characteristics for guyed radiators of uniform cross section. Data compiled from measurements of KNX and KIRO's 4-ft triangular radiators and a large number of 12- to 18-in. triangular radiators. (Prepared by J. B. Hutfield.)

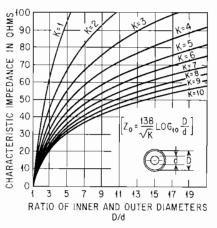


Fig. 9-16. Characteristic impedance of coaxial lines with various dielectrics.

COAXIAL-LINE IMPEDANCE CHART *

Summary: Characteristic impedances of coaxial lines are related graphically to dielectric constants and the ratios of outer to inner conductor diameters. Dielectric constants of common materials are also tabulated.

This chart (Fig. 9-16) simplifies the solution for the characteristic impedance of a single coaxial line.

Example. If a characteristic impedance of 50 ohms is desired and the insulating material is air, then from the chart the D/d ratio is 2.3. If metal tubing with an inside diameter D = 0.250 in. is chosen for the outer conductor, the outside diameter of the metal inner conductor is 0.109 in.

Oby Herbert L. Levin, Electron Tube Laboratory, Federal Telecommunication Laboratories, Nutley, N.J. Reprinted from Electronics, Nov. 1, 1957.

Dielectric Constant K from 1 to 10,000 Mc at 25°C

Ceramics		Plastics	
Alumina 85%	8.3 - 8.0	Bakelite BM 120	3.7
Alumina 95%	8.9-9.3	Epoxy resin	3.1
Alumina 97%	9.0 - 9.6	Formica XX	3.6
Aluminum silicate	5.5 - 5.2	Kel-F	2.3
Fosterite	6.2 - 6.0	Micarta 254	3.4
Magnesium silicate	5.9 - 5.3	Nylon 610	2.8
Steatite	6.5 - 5.3	Plexiglass	2.6
Porcelain, standard elec-		Polystyrene	2.6
trical	5.5	Styrofoam 103.7	1.03
Porcelain, zircon	9.2	Teflon	2.1
		Tenite II	2.9
		Vinylite VG 5901	2.9
Glasses		Miscellaneous	
			1
Corning:	5.1	Air	$1 \\ 2.4$
	5.1 4.0		
Corning: 7052 7070		Air Butyl rubber	2.4
Corning: 7052 7070 7720 nonex	4.0	Air Butyl rubber Mica	$\frac{2.4}{5.4}$
Corning: 7052 7070 7720 nonex 7740 Pyrex	4.0 4.7	Air Butyl rubber Mica Neoprene 38% GN	2.4 5.4 4.0
Corning: 7052 7070 7720 nonex	4.0 4.7	Air Butyl rubber Mica Neoprene 38% GN Silastic 120	2.4 5.4 4.0 5.7
Corning: 7052 7070 7720 nonex 7740 Pyrex 7900 Vycor (96%	4.0 4.7 4.6	Air Butyl rubber Mica Neoprene 38% GN Silastic 120	2.4 5.4 4.0 5.7
Corning: 7052 7070 7720 nonex 7740 Pyrex 7900 Vycor (96% silica)	4.0 4.7 4.6 3.8	Air Butyl rubber Mica Neoprene 38% GN Silastic 120	2.4 5.4 4.0 5.7
Corning: 7052 7070 7720 nonex 7740 Pyrex 7900 Vycor (96% silica) 8871 (lead potash)	4.0 4.7 4.6 3.8 8.4	Air Butyl rubber Mica Neoprene 38% GN Silastic 120	2.4 5.4 4.0 5.7
Corning: 7052 7070 7720 nonex 7740 Pyrex 7900 Vycor (96% silica) 8871 (lead potash) 9010 (lead free)	4.0 4.7 4.6 3.8 8.4 6.5	Air Butyl rubber Mica Neoprene 38% GN Silastic 120	2.4 5.4 4.0 5.7

If a ceramic such as Alumina 95 per cent with K=9 were introduced as the dielectric and the Z_b of 50 ohms were still desired, then from Fig. 9-16 D/d=12.3. If the D of 0.250 were also still desired, then d=0.020 in.

The chart shows that if in this example d were not changed when the ceramic material replaced air, then Z_0 would drop from 50 to 16.5 ohms.

COUPLING AND TUNING CAPACITOR FOR VARIOUS ANTENNAS

Figure 9-17 has been found to be a useful tool for adjusting the transmitter output circuit using capacity coupling to the antenna or transmission line. The values of capacity shown are approximate, but sufficiently close for practical purposes, since stray capacity of leads and components has not been taken into account. The capacity shown is the total capacity required for both the first and second sections of the low-pass filters.

The introduced resistance is the net resistance component when section is adjusted resulting from the effect of the R_a (antenna or line resistance) and the coupling capacity (CC).

The Z is the load impedance for the tubes determined by the dynamic characteristic for the particular tube and its operating voltages.

The value of introduced resistance used generally now lies between 50 and 100 ohms with the upper limit determined by the stray capacity. Formerly with high C ratios, introduced resistances were from 7 to 20 ohms, which resulted generally in higher circuit losses.

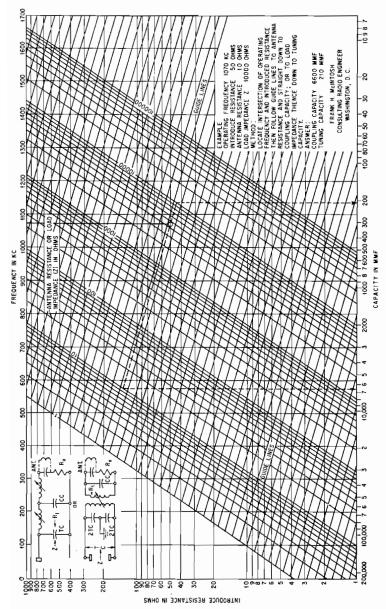


Fig. 9-17. Capacity-coupled circuits. Chart showing coupling and tuning capacities for various antenna resistances, tube load impedances, and introduced resistances for various given frequencies.

APPLICATION OF PROXIMITY-EFFECT CURVE *

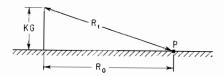
- 1. The curve in Fig. 9-18 shows the amount by which the measured field strength, as measured by a field-strength meter which employs a shielded loop, will depart from an inverse distance function because of induction field or proximity effect due to measuring close to the antenna.
- It is based upon the calculation of the horizontal component of magnetic field close to an antenna, after the manner of George H. Brown.
- It can be used first as a guide determining how close one can measure to a given antenna before the correction due to proximity would be expected to exceed a given percentage.
- 4. It can be used to correct out the error due to proximity before plotting field-strength measurements to determine accurately the inverse distance field. This permits measurements to be made sufficiently close to the tower to eliminate the effects of conductivity.

Derivation

- 1. G. H. Brown, Directional Antennas, IRE, January, 1937, on page 81 and in formula (7) gives the general formula for the magnetic flux density at any point in space from a vertical radiator over a perfectly conducting earth. By restricting this point P to the earth's surface, certain simplifications can be made in Brown's formula. Specifically Z goes to zero and $r_1 = r_2$ and $r_0 = x$.
 - 2. The simplified formula becomes:

$$B_{\phi} = \frac{j2 \times 10^{-9} I_0}{r_0 \sin kG} \left[e^{-jkr_1} - e^{-jkr_0} \times \cos kG \right]$$

where
$$k = \frac{2\pi}{\lambda}$$



3. Now when the distance r_0 becomes so great that $r_0 \approx r_1$

$$B_{\phi}(\text{far field}) = \frac{j2 \times 10^{-9} I_0}{r_0 \sin kG} [1 - \cos kG] \times \epsilon^{-jkr_0}$$

- 4. Now let $57.3kr_1 = r_1$ (degrees); $57.3kr_0 = r_0$ (degrees); 57.3kg = G (degrees).
- 5. Also convert from exponential to trigonometric form.
- 6. The resulting ratio is

$$\frac{B_{\phi}}{B_{\phi} \, (\text{far field})} = K = \frac{\{[\cos r_1 - \cos G \times \cos r_0]^2 + [\sin r_1 - \cos G \times \sin r_0]^2\}^{\frac{1}{2}}}{[1 - \cos G]}$$

7. Therefore:

$$\frac{\text{Field measurement}}{K} = \text{adjusted field}$$

* Silliman, Moffet, and Rohrer.

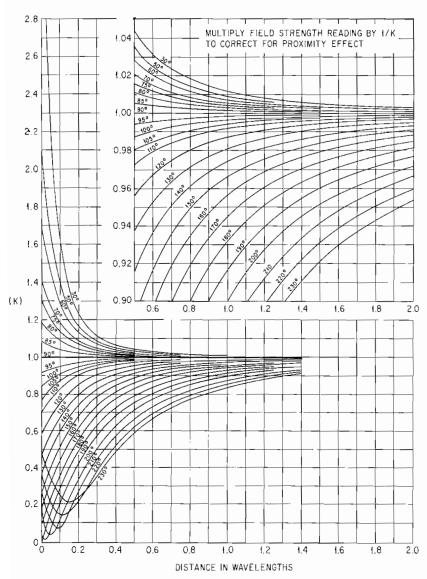


Fig. 9-18. Proximity effect for various tower heights.

WAVEGUIDE LOSS CHARTS *

Summary: Graphical presentation of attenuation values provides data for typical commercial microwave equipment. When effective resistivity is known or estimated, attenuation in decibels per foot can be determined at 1 to 75 kmc. Internal rectangular dimensions are also given.

Attenuation per foot of a particular commercial rectangular waveguide at a given frequency can be computed from published information, but for rapid extrapolation or comparison the accompanying charts (see Fig. 9-19) offer a ready solution.

One must know or be able to estimate the effective resistivity of the conducting surface. This is the product of d-c resistivity and a surface roughness factor K_T , which

Nominal Internal Dimensions for Standard Hollow Rectangular Waveguides

WR No.	Wide	Narrow	WR No.	Wide	Narrow
10	0.100	0.050	112	1.122	0.497
12	0.122	0.061	137	1.372	0.622
15	0.148	0.074	159	1.590	0.795
19	0.188	0.094	187	1.872	0.872
22	0.224	0.112	229	2.290	1.145
28	0.280	0.140	284	2.840	1.340
34	0.340	0.170	340	3.400	1.700
42	0.420	0.170	430	4.300	2.150
51	0.510	0.255	510	5.100	2.550
62	0.622	0.311	650	6.500	3.250
75	0.750	0.375	770	7.700	3.850
90	0.900	0.400	975	9.750	4.875

is unity for an ideal polished surface. Materials having low d-c resistivities require smooth surfaces for low effective resistivity and low loss. In materials having high d-c resistivities the current penetrates deeper into the material and K_T is near unity even for moderately rough surfaces. Thus surface roughness has almost no effect on high-resistivity materials.

Another factor is the size of the hollow waveguide cross section. Lowest losses are obtained by use of the largest possible waveguide. The chart shows the penalty resulting from use of a smaller size.

Measured attenuation of two sizes of rectangular copper waveguides shows that the effective resistivity is about 2.2×10^{-6} ohm-cm from 4 to 6 kmc. This is about 28 per cent above the d-c resistivity of 1.72×10^{-6} ohm-cm. Measurements on WR-229 drawn of 90-10 brass show an effective resistivity of 4.3×10^{-6} ohm-cm at 4 kmc, which is about 7.5 per cent above the d-c resistivity of 4×10^{-6} ohm-cm.

Plotting points on the graph were determined from the equation

$$\alpha = \frac{5.963 (RK_{\rm T}/\lambda)^{\frac{1}{2}} (1/b + \lambda^2/2a^3)}{\sqrt{1 - \lambda^2/4a^2}}$$

where α = attenuation in rectangular waveguide, db/ft

R = d-c resistivity of conducting surface, ohm-cm

a =wide dimension of waveguide, in.

b = narrow dimension of waveguide, in.

 λ = frec-space wavelength, in.

 $K_T = \text{surface roughness factor}$

 RK_T = effective resistivity of conducting surface, ohm-cm

⁹ By A. F. Pomeroy, Bell Telephone Laboratories, Murray Hill, N.J. Reprinted from Electronics, October 1, 1957.

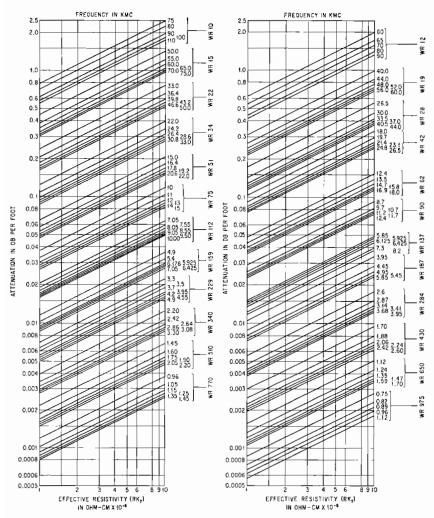


Fig. 9-19. Waveguide loss charts.

Example. Suppose it is necessary to find the attenuation of WR51 made of high-conductivity copper at frequencies from 16.4 to 20.6 kmc. Using 2.5×10^{-6} ohm-cm as an effective resistivity, we read on the chart 0.092 db/ft at 16.4 kmc and 0.078 db/ft at 20.6 kmc. The attenuation of other sizes can be found in a similar manner.

Representative frequencies in the recommended ranges were chosen for each size shown in Fig. 9-19. Interpolation between the characteristics to find the loss for other frequencies is straightforward.

The effective resistivity should be nearly constant over a small frequency interval, which leads to another use of these characteristics. To find an average effective resistivity over a band of frequencies, measured values of decibels per foot can be plotted on the characteristics and an ordinate drawn through the average value of effective resistivity. This result is probably more accurate than any one of the individual determinations.

Thanks are due Miss J. D. Goeltz and Mrs. Dolores G. Hill for their work in computing the attenuations used in plotting the characteristics.

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Benson, F. A.: Waveguide Attenuation and Its Correlation with Surface Roughness, *Proc. IRE*, 100, part III, p. 85, March, 1953.

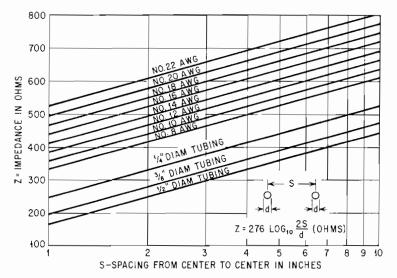


Fig. 9-20. Characteristic impedance of parallel-line wires.

L-NETWORK DESIGN *

Summary: Technique for using Smith chart to speed design of L matching networks for transmission lines and waveguides using lumped parameters. Shaded-area charts show at a glance impedance ranges that can be matched with each type of L network.

The familiar Smith chart for transmission lines is also a useful tool for designing matching networks. As an example, consider the case where it is desired to match an impedance $Z_L = (0.3 - \text{j}1.6)R_\theta$ to R_θ with the L matching network shown in Fig. 9-21. It is assumed that the inductances are lossy so that $R_1 = X_1 \tan \theta = 0.2X_1$ and

* By H. F. Mathis, Goodyear Aircraft Corp., Akron, Ohio. Reprinted from *Electronics*, Feb. 1, 1957.

 $G_2 = -B_2$ tan $\theta = -0.2B_2$. All impedances and admittances are normalized with respect to R_a and $G_a = 1/R_a$, respectively.

Let $Z_A = Z_L + R_1 + jX_1$ and $Y_A = 1/Z_A$. Since $Y_A + G_2 + jB_2 = 1$, Y_A must lie on curve $Y = 1 - k(\tan \theta - j)$, where k is a real variable. This curve is circle OA' with center C. To locate C, lines OC and OD are drawn as indicated in Fig. 9-20. Point D bisects its line. Point C is located as indicated.

Point C is inverted to obtain C' on line OC so that C'O = OC. Since Y_4 must lie on circle OA', Z_4 must lie on circle OH whose center is C'. To determine Z_4 , plot curve $Z = Z_L + p(\tan \theta + j)$, where p is a real variable. Point A, where this curve intersects circle OH, is the desired value of Z_4 . The value of Y_4 is found by inverting point A to obtain A'. Finally, $R_1 + jX_1 = (Z_4 - Z_L)R_0 = (0.498 - j0.610) - (0.3 - j1.6)R_0 = (0.198 + j0.990)R_0$ and $G_2 + jB_2 = (1 - Y_4)G_0 = 1 - (0.803 + j0.985)$ - $G_0 = (0.197 - j0.985)G_0$.

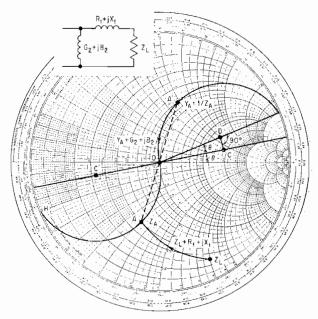


Fig. 9-21. Smith-chart procedure for determining parameters of L matching network.

General Procedure. In general, for L matching networks plot Z_L or Y_L first on the Smith chart. Next, plot the impedance or admittance into which Z_L is to be transformed, and find a suitable path connecting these points.

It is impossible to match all possible values of Z_L with a given type of L network. For example, if $Z_L = 0.5R_o$, the matching network shown in Fig. 9-21 could not be used. Impedances which can be matched with a given type of L network are shown as areas on Smith charts in Fig. 9-22. It is assumed that it is desired to transform Z_L into R_o and that Z_L is normalized with respect to R_o .

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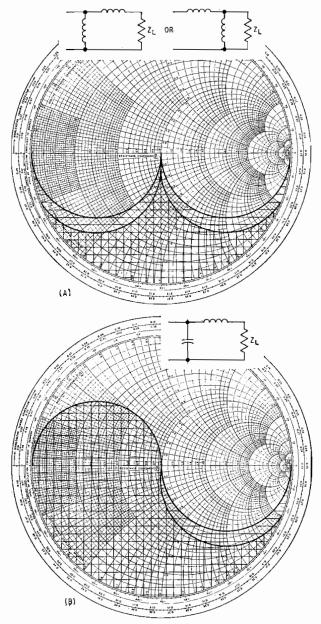
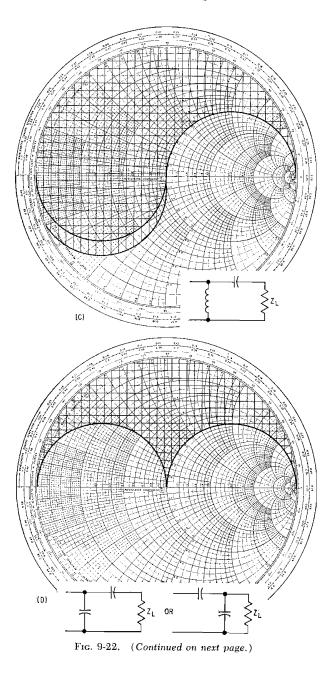


Fig. 9-22. For each network, horizontally shaded areas on the accompanying Smith chart show impedances which can be matched with lossless reactance. Vertically shaded areas can be matched with reactances for which tan $\theta=0.2$.



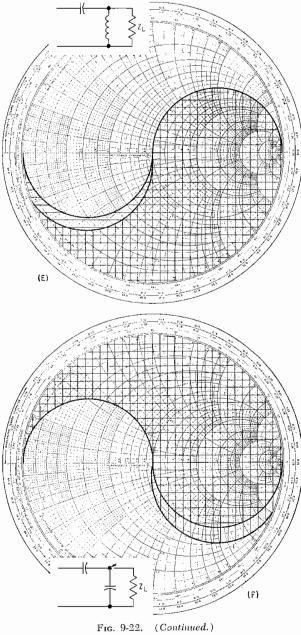


Table 9-4. Comparison of Open-wire Solid-dielectric Lines and Waveguides

Characteristics	Parallel open wires	Brad supported	Stub supported	Solid dielectric (Polyethylene)	Coaxial rubber	Waveguide	Pulse cables
Insulation resistance O	O.K. in dry air, drops in rain	O.K. in dry air or nitrogen	O.K. dry or slightly wet	O.K. dry or wet	O.K. dry, drops when wet. Varies with	O.K.	Same as rubber
Corona voltage and dielectric strength	Depends on dry air and spacing,	Depends on dry nir, depends on	Depends on size, low	Depends on size, high	Depends on dry air, size, medium high	Depends on size, dry air, pres-	Depends on size, dry air,
Dielectrie constant	low Low, air (1)	Low, air plus beads	Low, air (1)	Medium (2.3)	Medium high (3-4)	sure, Iow	nign High (5–6)
Power factor	Low in dry air, goes up in wet	Low in dry air, goes up in wet	O.K. dry or slightly wet	O.K. dry or wet	High dry, higher wet. No good for		Same as rubber
D-c conductor resist- ance	Low, goes down with size	Same	Same	Fligher than con- centries, goes	High, goes down with size	Low, goes down with size	High, goes
Ease of installation	Easy	More difficult	Difficult	Gown with Size Easier than con-	Same as solid di-	Same as bead-	size Same as rubber
Ease of maintenance. Flexible	Easy Somewhat, de-	Very difficult Some, depends on	Not very No	Easy Yes, flexibility goes	do Yes, more than solid	Supported Easy No	Same as rubber
Mechanically strong	Yes, but sepa- rators are weak	Yes, beads are weak points	Yes, but stubs are fragile	Yes, but can be mistreated	Yes	Yes, but can be crushed	Yes
Can be scaled	Yes	Yes, but you have to do the right	Yes	Yes	Yes	Yes	Yes
Self-shielding (electrical)	No	Yes	Yes	Yes, depends on the braid con-	Same as solid di- electric	Yes	Same as solid dielectric
Fire resistive	Yes	Yes	Yes	Yes, except largest	Not completely	Yes	Same as rubbor
High-temperature resistant	Yes. depends on material of	Yes, depends on rubber gaskets or	Yes, same as bead supported	180-200°F for short time	220–250°F for short time	Yes, depends on rubber gasket	Same as rubber
Transmission at high frequency	separators Limited by spacing	Good at low, me- clium frequency losses high at	Good at high fre- quency not at low, need spec	Good, at low and medium not so good at micro-	Poor, loss too high	or solder Best, but each frequency needs spec guide	Poor, loss too high
Stand shock	Good	Fair, beads are	Good, stubs are	wave Very good	Very good	Very good	Very good
Low temperatures	Yes	Yes, but allow for expansion	Same as beaded	Yes	Yes	Yes, but allow for expansion	Yes

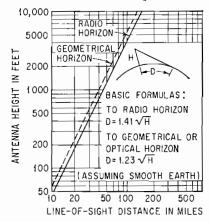


Fig. 9-23. Distance to horizon vs. height of transmitting antenna.

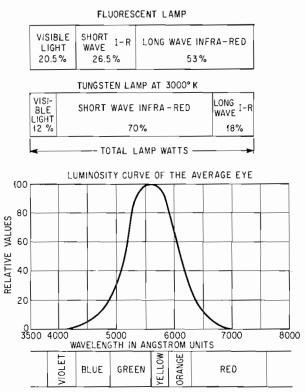


Fig. 9-24. Fluorescent and tungsten lamp spectral distribution and luminosity curve of the average human eye.

HEATER SURGE CHART *

Summary: The effect of heater current surges when voltage is applied to cold tube and efficiency of surge-restricting arrangements can be evaluated with this chart. Hot and cold characteristic curves are typical for most tubes.

To minimize damaging effects of high initial current when heater voltage is applied to a cold tube, starting current surges should be restricted.

The magnitude of heater current surges under various conditions can be calculated by use of the graph (Fig. 9-25), which consists basically of two curves plotted on coordinates of heater current and voltage relative to normal full-voltage conditions. The first curve, a straight line, represents the resistance of a cold heater. It represents a resistance which is 0.15 of the normal operating resistance. This is typical of most receiving tubes. The second curve shows the locus of points at which thermal equilibrium is obtained for steadily applied voltages. Deviations from this curve are relatively small for common receiving-type tubes.

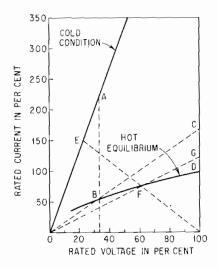


Fig. 9-25. Current-voltage plot for hot and cold tube conditions used to evaluate surge.

The results of applying heater voltage in steps can be shown by simple constructions. If a line is constructed at a chosen value of initial voltage, the magnitude of the initial cold-resistance surge is shown by point A and thermal equilibrium occurs at point B. A line through the origin and point B represents the heater resistance attained in the partially heated equilibrium condition. If 100 per cent voltage is then applied, a current surge of magnitude indicated by point C occurs, and final equilibrium is attained at the normal operating point D.

The effect of applying 100 per cent rated voltage through a series resistor can be shown by the construction of a line having a slope based on the ratio of the series resistance to the normal hot resistance of the tube. The cold-tube surge is indicated by point E, and equilibrium occurs at F. Construction of a line from the origin through point F then represents this equilibrium heater resistance. If the resistor is then shorted out, 100 per cent voltage will be applied and will result in a momentary current indicated by point G. Final equilibrium will occur at the normal operating point D.

^o By M. P. Feyerherm, Defense Electronic Products, Radio Corporation of America, Camden, N.J. Reprinted from *Electronics*, June 1, 1957.

A CONVENIENT SLIDE-RULE SHORT CUT TO CONVERT ELECTRICAL DEGREES TO FEET, OR VICE VERSA WHEN FREQUENCY AND EITHER FEET OR DEGREES IS KNOWN

From the expression

Feet =
$$\frac{\text{degrees}}{360^{\circ}} \times \frac{300}{f(\text{Me})} \times 3.281 = \text{degrees} \times \frac{2.734}{f(\text{Me})}$$

the following ratio may be set up on the slide rule using *C* and *D* scales:

$$\frac{2.734}{f(Mc)} = \frac{\text{feet}}{\text{degrees}}$$

Set 2.734 on scale C over frequency in megacycles on scale D; read feet and degrees on scales C and D, respectively. In some instances it may be convenient to use the folded scales CF and DF.

GREAT-CIRCLE DISTANCE AND BEARING CALCULATIONS

The need often arises in allocations problems for a simple and reliable method of computing the position of one radio station or area with respect to another expressed in degrees clockwise from true north. It is often equally important that the distance between these two points be known.

Bearings and distance can be computed in many ways. The method set forth here utilizes a table developed by Lieutenant Arthur A. Ageton, USN, which permits the simple solution of navigational problems. If the table is properly read and interpolations carefully made, the bearings and distances derived through use of the calculation sheet will be found to be in very close agreement with lengthy mathematical computations.

To use this method one must first obtain Hydrographic Office Publication No. 211, entitled "Dead Reckoning Altitude and Azimuth Table" from the Hydrographic Office, Washington, D.C., or the Superintendent of Documents, Government Printing Office, Washington, D.C.

The calculation sheet can be shortened in some respects if used only for determining bearings and distances between points within a limited area such as the United States or North America. As shown, bearings and distances can be calculated between any two points on the surface of the earth if the latitude and longitude of the two positions are known.

If a considerable number of calculations are to be made, it is suggested that the calculation sheet be duplicated in quantity. Furthermore, it is suggested that until one becomes thoroughly acquainted with the method the various *steps* be checkmarked as they are completed.

Great Circle Distance and Bearing Calculation Sheet

(Based on Ageton, H.O. Publ. 211, Tables)

FROM	Location	(La)	٥	_′	"	(Lo)	•	<i>'</i>	"	
	Location									
		Symbo	ls Use	ed						

- A Numbers in the A columns of the H.O. 211 tables
- B Numbers in the B columns of the H.O. 211 tables
- $t = (Lo \sim Lo')$ The smaller angle between the two meridians, Lo and Lo'
- C Bearing East or West of 0° true
- D Great-circle distance when converted to minutes of arc
- K An arc used in the calculations
- Dn The great-circle distance in nautical miles
- Ds The great-circle distance in statute miles
- $(K \sim La)$ The magnitude of the difference between arc K and La

Rules

- If La and La' are in the same hemisphere:
 (N or S)
- K: Take K from bottom of columns in H.O. No. 211 tables if t is greater than 90°.
- D: Take D from bottom of columns in II.O. No. 211 when t and $(K \sim La)$ are each greater than 90°.
- C: Take C from bottom of columns in II.O. No. 211 when K is less than La.
- $(K \sim La)$: Subtract K and La to find difference.
- If La and La' are in different hemispheres: (N and S)
- K: Take K from bottom of columns in H.O. No. 211 tables if t is greater than 90°.
- D: If t and (K ~ La) are each less than 90°, take D from top of table, otherwise, from bottom.
- C: Take C from bottom of tables in H.O. No. 211 tables unless (K ~ La) is greater than 180°.
- $(K \sim La)$: Add K and La to find magnitude. If $(K \sim La)$ exceeds 180°, subtract 180° before entering H.O. No. 211 table to find B3.

Calculations

[Follow rules closely for K, D, C, and B3—also $(K \sim La)$]

Lo'	ADD A1 B1+ A2 =	8UBTRACT A3 B2- A4 =	B2	4.5
$ \begin{array}{ccc} K &= & & \\ La & & \\ (K \sim La) &= & & \\ \end{array} $	D = D: Dn	° × 60 = miles ×	+'= +'= 1.152 = Ds	Dn miles miles
	C'*	=	, "	$\frac{\mathrm{E}}{\mathrm{W}}$ of 0° true

* Note: When Lo' is west of Lo, C will indicate bearings in degrees west of 0° true. When Lo' is east of Lo, C will indicate bearings in degrees cast of 0° true.

Steps

- 1. List coordinates for locations.
- 2. Subtract Lo and Lo' to find are t.
- 3. Enter H.O. No. 211 with t to find A1.
- 4. Enter table with La' to find B1 and A3.
- 5. Add A1 and B1 for A2.
- 6. Enter table with A2 to find B2.
- Subtract B2 from A3 for A4.
- 8. Enter table with A4 for arc K.

- 9. Determine arc for $(K \sim La)$.
- 10. Enter table with $(K \sim La)$ for B3.
- 11. Add B2 and B3 for B4.
- 12. Enter table with B4 to find A5 and arc D.
- 13. Subtract A5 from A2 for A6.
- 14. Enter table with A6 for bearing C.
- 15. Follow steps shown to find Ds and Dn.

Table 9-5. Temperature-conversion Chart *

SF.	1,292.0	1,235.6	1,297.4	1,299.2	1,301.0	1,302.8	1,304.6	1,306.4	1,308.2	1.310.0	1,311.8	1,313.6	1,315,4	1,317.2	1.319.0	1,320.8	1,322.6	1,324.4	1,326.2	1.328.0	1,329.8	1,331.6	1,333.4	1,335.2	1.337.0	1,338,8	1,340.6	1,342.4	1,344.2	1.346.0	1.347.8	1,349.6	1,351.4	1,353.2
ပ္စ	700	702	703	407	705	200	707	708	200	210	711	715	713	714	715	716	717	718	719	720	721	722	723	724	725	726	7.57	728	729	730	731	732	733	73+
A.	1,112.0	1,115.6	1,117.4	1,119.2	1,121.0	1.122.8	1,124.6	1,126.4	1,128.2	1,130.0	1.131.8	1,133.6	1,135.4	1,137.2	1.139.0	1.140.8	1,142.6	1,141,4	1,146,2	1.148.0	1,140.8	1,151.6	1,153.4	1,155.2	1.157.0	1,158,8	1,160,6	1,162.4	1,164.2	1.166.0	1,167.8	1,169.6	1,171.4	1,173,2
၁့	000	602	603	109	605	909	209	608	609	919	611	612	613	614	615	919	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	55
4°	932.0	935.6	937.4	939.2	941.0	945.8	9.44.6	946.4	948.2	950.0	9:1:8	953.6	955.4	957.2	959.0	9.096	962.6	964.4	966.2	968.0	8.696	971.6	973.4	975.2	977.0	978.8	980.6	985.4	984.2	986.0	87.86	9.686	991.4	993.2
ပ္စ	500	502	503	504	505	506	507	508	509	510	511	513	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	#
P.	752.0	755.6	757.4	759.2	761.0	762.8	264.6	766.4	768.2	770.0	771.8	773.6	775.4	2.777	779.0	780.8	782.6	784.4	786.2	788.0	789.8	791.6	7.83.4	795.2	797.0	798.8	800.6	802,4	804.2	806.0	807.8	9.608	811.4	27212
သ	100	105	403	1 0+	405	400	·107	408	400	410	411	412	413	414	415	416	417	418	419	420	421	422	423	454	425	426	127	428	429	430	431	432	533	15.
J.	572.0	575.6	577.4	579.2	581.0	582.8	584.6	1:980	588.5	290.0	591.8	593.6	595.4	597.2	599.0	8.009	602.6	604,4	606.2	608.0	8.609	611.6	613,4	615.2	617.0	618.8	620.6	622.4	624.2	626.0	627.8	629.6	631.4	053.2
၁့	300	308	303	304	305	300	307	308	308	310	311	312	313	314	315	316	317	318	319	350	321	322	323	324	325	326	327	358	329	330	331	332	333	199
°F.	392.0	395.6	397.4	399.2	401.0	402.8	404.6	406.4	408.3	410.0	411.8	413,6	415.4	417.2	419.0	420.8	422.6	424.4	426.2	428.0	429.8	431.6	433.4	435.2	437.0	438.8	440.6	442,4	444.2	446.0	447.8	449.6	451.4	40.5.2
သ	200	202	203	204	205	206	207	508	500	210	211	212	213	214	215	216	217	218	518	220	221	222	223	224	225	226	227	228	229	230	231	232	233	- KON
°F.	212.0	215.6	217.4	219.2	221.0	222.8	224.6	2.56.4	238.5	230.0	231.8	233.6	235.4	237.2	239.0	240.8	242.6	244.4	246.2	248.0	249.8	251.6	253.4	255.3	257.0	258.8	260.6	262.4	264.2	266.0	267.8	269.6	271.4	27.6.2
ပ္	100	102	103	104	105	106	107	108	109	110	111	112	113	114	113	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	<u> </u>
o.F.	32.0	35.6	37.4	39.2	41.0	45.8	44.6	46.4	48.5	50.0	51.8	53.0	55.4	57.2	59.0	8.09	62.6	64.4	66.2	68.0	8.69	71.6	73.+	75.2	77.0	78.8	90.08	82.4	84.2	86.0	87.8	9.68	91.4	93.2
ွ	0 -	- 24	8	7	100	9		œ	6	10	11	12	13	77	:3	16	17	18	19		21		_	_	<u> </u>	56	_	_	_	8	31	32		Ę.
J.	32.0	28.4	26.6	24.8	23.0	21.2	19.4	17.6	15.8	14.0	12.2	10.4	8.6	6.8	5.0	3.2	1.4	-0.4	-2.2	-4.0	-5.8	9.7-	+.6 –	-11.2	- 13.0	- 14.8	-16.6	-18.4	-20.2	-22.0	-23.8	-25.6	27.4	27.72
သ	0 -	_	_				-1	_			_	-12	_		Ļ		-17	_	_	_	-21	_	_	_		-26	_	_	_	L	_		- 33	_
J.	-148.0	-151.6	-153.4	- 155.2	-157.0	- 158.8	- 160.6	-162.4	-164.2	-166.0	-167.8	-169.6	-171.4	-173.2	-175.0	-176.8	-178.6	-180.4	-182.2	-184.0	-185.8	-187.6	-189.4	-191.2	-193.0	-194.8	-196.6	-198.4	-200.2	-202.0	-203.8	-205.6	-207.4	7.602
သ	- 100	- 102	-103	- 104	- 105	-106	-107	801-	- 109	- 110	-111	-112	-113	-114	- 115	-116	_	- 118		- 120	- 121	$\overline{}$	_	- 124	- 125	1 126	- 127	-128	- 129	- 130	- 131		- 133	
οF	-328.0	-331.6	-333.4	-335.2	-337.0	-338.8	-340.6	-342.4	-344.2	-346.0	-347.8		-351.4		-355.0	-356.8	-358.6	-360.4	-362.2	-364.0	-365.8	-367.6	-369.4	-371.2	-373.0	-374.8	-376.6	-378.4	-380.2	-382.0	-383.8	-385.6	- 387.4	2.020
వి	-200	- 202	-203	204	-205	-206	- 207	-208	- 208	-210	-211	-212	-213	-214	-215	-216	-217	-218	-210	-220	-221	-222	-223	- 224	-225	-226	-227	-258	-229	-230	-231	- 232	- 233	1234

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1,355.0 1,356.8 1,358.6 1,360.4 1,362.2	1,365.8 1,365.8 1,367.6 1,377.2 1,373.0 1,374.8 1,376.6 1,376.1 1,378.4	1,382.0 1,383.8 1,385.6 1,387.4 1,389.2 1,392.8 1,394.6 1,394.6 1,398.2	1,400.0 1,401.8 1,403.6 1,405.4 1,407.2	1,409.0 1,410.8 1,412.6 1,414.4 1,416.2	1,418.0 1,419.8 1,421.6 1,423.4 1,425.2
735 736 737 738 739	740 741 742 743 745 745 746 747 748	750 751 752 753 754 755 756 757 757 758	760 761 762 763 764	765 767 768 768	770 771 773 773
1,175.0 1,176.8 1,178.6 1,180.4 1,182.2	1,184.0 1,185.8 1,187.6 1,191.2 1,193.0 1,194.8 1,196.6 1,198.4	1,202.0 1,203.8 1,205.6 1,205.6 1,207.4 1,209.2 1,212.8 1,212.8 1,212.8 1,214.6 1,214.6	1,220.0 1,221.8 1,223.6 1,225.4 1,225.4	1,229.0 1,230.8 1,232.6 1,234.4 1,236.2	1,238.0 1,239.8 1,241.6 1,243.4 1,245.2
635 636 637 638 639	640 641 642 643 644 645 645 648	650 651 653 653 653 653 656 656 657 658	660 661 662 663 664	665 666 667 668 669	670 671 672 673 673
995.0 996.8 998.6 1,000.4	1,004.0 1,005.8 1,007.6 1,009.4 1,011.2 1,013.0 1,014.8 1,016.6 1,016.6	1,022.0 1,023.8 1,023.6 1,025.4 1,029.2 1,031.0 1,032.8 1,034.6 1,036.4	1,040.0 1,041.8 1,043.6 1,045.4 1,047.2	1,049.0 1,050.8 1,052.6 1,054.4 1,056.2	1,058.0 1,059.8 1,061.6 1,063.4 1,063.2
535 536 537 538 539	540 541 542 543 544 545 545 545 548	550 551 551 552 553 554 555 556 557 558	560 561 562 563 564	565 566 567 568 569	570 571 572 573 574
815.0 816.8 818.6 820.4 822.2	821.0 825.8 825.8 825.4 831.2 833.0 834.8 836.6 838.4	842.0 843.8 845.6 847.4 847.4 851.0 852.8 853.8 854.6 856.4 856.4	860.0 861.8 863.6 865.4 867.2	869.0 870.8 872.6 874.4 876.2	878.0 879.8 881.6 883.4 885.2
435 136 137 438 438	44 44 44 44 44 44 44 44 44 44 44 44 44	455 455 455 455 455 455 456 457 457 458	460 461 462 463 464	465 465 467 468 469	470 471 472 473
635.0 636.8 638.6 640.4 642.2	644.0 645.8 647.6 649.4 651.2 653.0 654.8 656.6 656.6	665.6 665.6 665.6 667.4 669.2 671.0 671.0 674.6 674.6 676.4	680.0 681.8 683.6 685.4 687.2	689.0 690.8 692.6 694.4 696.2	698.0 699.8 701.6 703.4 705.2
335 336 337 338 338	340 341 342 343 344 346 346 346 348	350 351 351 351 351 351 351 351 351 351 351	360 361 362 363 364	363 368 368 368 369	370 371 372 372 373 374
455.0 456.8 458.6 460.4 462.2	464.0 465.8 467.6 471.2 473.0 474.8 476.6 476.6	482.0 183.8 185.6 187.4 189.2 199.2 191.0 491.0 492.8 194.6 196.4	500.0 501.8 503.6 505.4 507.2	509.0 510.8 512.6 514.4 516.2	518.0 519.8 521.6 523.4 525.2
235 236 237 238 239	240 241 242 243 244 245 245 245 245 247	250 251 252 253 254 254 255 257 257 257	260 261 262 263 264	265 266 267 268 269	270 271 272 273 273
275.0 276.8 278.6 280.4 282.2	284.0 285.8 285.8 280.4 291.2 293.0 294.8 296.6 296.6	302.0 303.8 303.8 305.6 307.4 309.2 311.0 311.6 318.4 318.4	320.0 321.8 323.6 325.4 327.2	329.0 330.8 332.6 334.4 336.2	338.0 339.8 341.6 343.4 345.2
135 136 137 138 139	140 141 142 143 144 145 146 146 147	150 151 151 153 154 155 156 156 157 158	162 162 163 163 164	165 166 168 168	171 172 173 173 173
95.0 96.8 98.6 100.4	104.0 105.8 107.6 109.4 111.2 113.0 114.8 116.6 118.4	122.0 123.8 125.6 127.4 129.2 132.8 134.6 134.6 136.4 138.2 138.2	140.0 141.8 143.6 145.4 147.2	149.0 150.8 152.6 154.4 156.2	158.0 159.8 161.6 163.4 165.2
35 37 38 39	\$ 4 \$ \$ \$ \$ \$ \$ \$ \$		82822		13333
-31.0 -32.8 -34.6 -36.4 -38.2	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	-76.0 -77.8 -79.6 -81.4 -83.2	- 85.0 - 86.8 - 88.6 - 90.4 - 92.2	- 94.0 - 95.8 - 97.6 - 99.4 - 101.2
-35 -36 -37 -38	04-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	5 - - - - - - - - -	- 60 - 61 - 62 - 63	- 65 - 66 - 67 - 68 - 69	- 70 - 71 - 72 - 73
-211.0 -212.8 -214.6 -216.4	220.0 - 220.0 - 223.6 - 225.1 - 227.2 - 229.0 - 230.8 - 232.6 - 232.6	2339.8 241.6 241.6 245.4 245.2 252.4 252.4 252.4	- 256.0 - 257.8 - 259.6 - 261.4 - 263.2	-265.0 -266.8 -268.6 -270.4	-274.0 -275.8 -277.6 -279.4 -281.2
-135 -136 -137 -138 -139	- 140 - 141 - 143 - 145 - 145 - 146 - 146	150 151 151 153 153 153 153 153 153	- 160 - 161 - 162 - 163 - 164	- 165 - 167 - 167 - 168 - 169	-170 -171 -172 -173 -173
-391.0 -392.8 -394.6 -396.4 -398.2	-400.0 -400.0 -405.4 -405.2 -409.0 -410.8 -410.8	+ 419.8 + 4119.8 + 421.6 + 425.2 + 425.2 + 425.8 + 432.4 + 432.4 + 432.4	-436.0 -437.8 -439.6 -441.4 -413.2	-445.0 -446.8 -448.6 -450.4 -452.2	-454.0 -455.8 -457.6 -459.4 -459.4
- 235 - 236 - 237 - 238			-260 -261 -262 -263 -263	- 265 - 266 - 267 - 268 - 269	-270 -271 -272 -273 -273

Absolute zero.

Table 9-5. Temperature-conversion Chart (Continued)

°C °F	Ö	Ŧ,	ပွ	Æ	၀	Ą	ွ	Ą.	ွ	°F.	၀	Ą.	ပွ	Ą.	ပွ	°F	သ	भ	ွ	°F
Absolute Zero	-175	-283.0	-75	-103.0	7.5	167.0	17.5	347.0	275	527.0	37.5	0.707	475	0.788	575	1,067.0	675	1,247.0	775	1,427.0
	- 176	- 284.8	92-	-104.8	92	168.8	176	348.8	276	528.8	376	708.8	476	8888	976	1,068.8	929	1,248.8	977	1,428.8
	177	-286.6	12	-106.6	7.7	170.6	177	350.6	277	530.6	377	710.6	477	830.6	577	1,070.6	677	1,250.6	777	1,430.6
	-178	-288.4	8/-	-108.4	28	172.4	178	352.4	278	532.4	378	712.4	478	892.4	578	1.072.4	678	1,252.4	218	1,432.4
	-179	- 290.2	-79	-110.2	79	174.2	179	354.2	279	534.2	379	714.2	479	894.2	579	1,074.2	629	1,254.2	217	1,434.2
	-180	-292.0	-80	-112.0	8	176.0	180	356.0	280	536,0	380	716.0	180	0.968	580	1,076.0	089	1,256.0	280	1,436.0
Formulas:	- 181	- 293.8	-81	-113.8	81	177.8	181	357.8	281	537.8	381	717.8	481	8.768	581	1,077.8	681	1,257.8	781	1,437.8
	-182	-295.6	-85	-115.6	<u>25</u>	179.6	182	359.6	282	539.6	382	719.6	482	9.068	585	1,079.6	682	1,259.6	782	1,439.6
	-183	-297.4	183	-117.4	83	181.4	183	361.4	283	541.4	383	721.4	483	901.4	583	1,081.4	683	1,261.4	783	1,441,4
C = 56(F - 32)	- 184	-299.2	-84	-119.2	₩	183.2	184	363.2	584	543.2	384	723.2	484	903.2	584	1,083.2	684	1,263.2	784	1,443.2
	- 185	-301.0	-85	-121.0	\$€	185.0	185	365.0	285	545.0	385	725.0	485	905.0	585	1,085.0	685	1,265.0	785	1,445.0
F = 95C + 32		-302.8	98-	-122.8	98	186.8	186	366.8	286	546.8	386	726.8	486	8.906	586	1.086.8	989	1,266.8	786	1,446.8
	-187	-304.6	-87	-124.6	87	188.6	187	368.6	282	548.6	387	728.6	487	908.6	587	1,088.6	687	1,268.6	787	1,448.6
	-188	-306.4	- 88	-126.4	88	190,4	188	370.4	288	550.4	388	730,4	488	910.4	288	1,090,4	889	1,270.4	788	1,450.4
	- 189	-308.2	- 89	-128.2	83	192.2	189	372.2	289	552.2	389	732.2	489	912.2	589	1,092.2	689	1,272,2	789	1,452.2
	- 190	-310.0	- 90	-130.0	8	194.0	190	37.4.0	290	554.0	300	734.0	490	914.0	590	1,094.0	069	1,274.0	790	1,454.0
	-191	-311.8	- 91	- 131.8	91	195.8	191	375.8	291	555.8	391	735.8	491	915.8	591	1,095.8	169	1,275.8	791	1,455.8
	-192	-313.6	-95	-133.6	92	197.6	192	377.6	292	557.6	395	737.6	492	917.6	592	1.097.6	692	1,277.6	792	1,457.6
	-193	-815.4	- 93	-135.4	33	199.4	193	379.4	293	559.4	303	739.4	493	919.4	593	1,099.4	693	1,279.4	793	1,459.4
	-194	-317.2	- 94	-137.2	1 6	201.2	194	381.2	294	561.2	394	741.2	494	921.2	594	1,101,2	694	1,281.2	794	1,461.2
		-319.0	-95	-139.0	9.5	203.0	195	383.0	295	563.0	395	743.0	495	923.0	595	1,103.0	695	1,283.0	795	1,463.0
	- 196	-320.8	96-	-140.8	96	204.8	196	384.8	290	564.8	396	744.8	496	924.8	596	1,104.8	969	1,284.8	962	1,464.8
	- 197	-322.6	-97	-142.6	26	206.6	197	386.6	297	566.6	397	746.6	497	956.0	597	1,106.6	697	1,286.6	797	1,466.6
	- 198	-324.4	-98	-144,4	86	208.4	198	388.4	298	568.4	398	748.4	498	928.4	598	1,108.4	869	1,288.4	798	1,468.4
	- 199	-326.2	6	-146.2	66	210.2	199	390.2	900	570.2	300	750 9	499	930.2	590	1.110.2	600	6 006 1	700	1.470.2

* Reprinted from Electronics, May 1, 1957.

MULTIPLY NUMBER OF	ANGSTROMS	MICRONS	MILS	INCHES	FEET	MILES	MILLIMETERS	CENTIMETERS	KILOMETERS
ANGSTROMS	1	104	2.540 X 10 ⁵	2.540 X 10 ⁸	3.048 X 10 ⁹	1.609 X 10 ¹³	107	108	1043
MICRONS	10-4	1	2.540 X 10	2.540 X 10 ⁴	3.048 X 10 ⁵	1.609 X 10 ⁹	103	104	109
MILS	3.937 X 10 ⁻⁶	3.937 X 10 ⁻²	1	103	1.2 X 10 ⁴	6.336 X 10 ⁷	3.937 X (0	3.937 X 10 ²	3.937 X 10 ⁷
INCHES	3.937 X 10 ⁻⁹	3.937 X 10 ⁻⁵	10-3	1	12	6.336 X 10 ⁴	3.937 X 10 ⁻²	3.937 X 10 ⁻¹	3.937 X 10 ⁴
FEET	3.2B1 X 10 ⁻¹⁰	3.281 X 10 ⁻⁶	8.333 X 10 ⁻⁵	B.333 X 10 ⁻²	1	5.280 X 10 ³	3.281 X 10 ⁻³	3.281 X 10 ⁻²	3.281 X 10 ³
MILES	6.214 X 10 ⁻¹⁴	6.214 X 10 ⁻¹⁰	1.578 X 10 ⁻⁸	1.578 x 10 ⁻⁵	1.894 X 10 ⁻⁴	f	6.214 X 10 ⁻⁷	6.214 X 10 ⁻⁶	6.214 X 10 ⁻¹
MILLIMETERS	10-7	10-3	2.540 X 10 ⁻²	2.540 X 10	3.048 X 10 ²	1.609 X 10 ⁶	1	10	106
CENTIMETERS	10 ⁻⁸	10-4	2.540 X 10 ⁻³	2.540	3.048 X 10	1.609 X 10 ⁵	0.1	1	105
KILOMETERS	10-13	10-9	2.540 X 10 ⁻⁸	2.540 X 10 ⁻⁵	3.048 X 10 ⁻⁴	1.609	10-6	10-5	1

Table 9-6. Conversion Table for Units of Length

TRANSISTOR CHARACTERISTICS FOR CIRCUIT DESIGNERS °

Summary: Tables indicate physical properties, maximum electrical ratings, small-signal low-frequency parameters, and average characteristics for grounded-base, grounded-emitter, grounded-collector, and switching circuits for 218 transistor types: 106 junction triodes, 46 high-frequency triodes, 6 tetrodes, 23 high-power units, 25 point-contact, and 12 phototransistors.

Abbreviations Used in Tables

α	Current gain	I_e	Emitter current
β	Base-current amplification factor	I_{eo}	Emitter cutoff current
$_{\mathrm{BW}}$	Bandwidth	NF	Noise figure
C_{c}	Collector capacitance	r_{v}	Base resistance
f_{co}	Alpha cutoff frequency	r_c	Collector resistance
g-b	Grounded base	r_e	Emitter resistance
g-c	Grounded collector	R_{g}	Generator resistance
g-e	Grounded emitter	$R_{\mathfrak{i}}$	Input resistance
I_b	Base current	R_L	Load resistance
I_{b2}	Second base current (tetrode)	R_o	Output resistance
I_c	Collector current	V_c	Collector voltage
I_{co}	Collector cutoff current		

^o By Seymour Schwartz, Lincoln Laboratory, Massachusetts Institute of Technology, Lexington, Mass. Reprinted from *Electronics*, January, 1956.

Successful transistor circuit design requires not only familiarity with transistor equivalent circuits and characteristic curves but also an understanding of the behavior of the parameters describing the transistor and the variation of these parameters with bias and temperature. Tables 9-7 to 9-12 have been compiled as a systematic presentation of data necessary for transistor circuit design.

Each of the charts presents physical properties; maximum electrical ratings; typical small-signal low-frequency parameters; average characteristics for grounded-emitter, grounded-base, and grounded-collector circuits; and switching characteristics. Figure 9-27 illustrates the circuits referenced in Tables 9-8 and 9-9.

Small-signal parameters are expressed as resistances. This permits a familiar physical representation of the transistor in circuit design. The box on page 9-50 enables transformation between h and r parameters.

All the characteristics are for fixed-bias conditions. However, these values vary with operating conditions. Examples of these variations are shown in Fig. 9-26a to c.

Figure 9-26a illustrates how collector capacitance C_c varies with collector voltage V_c . In designing an IF tuned circuit, the tuning capacitor must be large enough to swamp out the effects of the variation of collector capacitance. If the IF stage is a grounded-emitter rather than a grounded-base stage, the collector capacitance is magnified by the base-current amplification factor β .

In IF stages where neutralization is used to maximize gain by balancing out C_c , instability may occur when the battery voltage decreases. This variation of C_c with V_c permits use of the transistor as a reactance element in FM applications.

At low current bias (Fig. 9-26b to d) the noise factor of the transistor decreases and emitter resistance r_e , base resistance r_b , and collector resistance r_e increase, providing increased power gain and larger values of input and output impedance. This is advantageous in hearing aids where low bias currents are used.

Temperature Effects

In the germanium transistor, noticeable chauges in α , β , and I_{co} take place at approximately 60°C as shown in Fig. 9-26e. These changes can lead to instability at high temperatures by α becoming equal to or greater than unity or by I_{co} increasing and causing a collector runaway effect due to self-heating.

Temperature problems are minimized in silicon transistors as seen in Fig. 9-26f. The value I_{ro} becomes almost negligible in design consideration as the upper limit or temperature range is above 100°C. In such special applications as d-c amplifiers, the slightest change in α over the normal temperature operating range can produce a significant change in d-c gain of the grounded-emitter stage.

The low-frequency low-power triode junction transistor, Table 9-7, is most commonly used. The majority are utilized in hearing aids, audio systems, low-power control systems, and low-speed computing circuits. Present units are available in the p-n-p and n-p-n fused germanium, the n-p-n grown silicon types. Of the fused type of transistor, the p-n-p is more available commercially and consequently has found a wider range of applications. The n-p-n fused type is suitable for complementary symmetry circuitry. The grown silicon type is used for high-temperature and low- I_{co} applications.

The germanium and silicon grown transistors are used in almost the same manner as the fused transistor. Frequently, the grown types, owing to their lower value of collector capacitance and higher value of a cutoff, can be employed as high-frequency transistors.

The maximum power ratings on most of the low-power transistors are of the order of 50-mw collector dissipation at room temperature. Some of these units have external heat sinks and are able to dissipate considerably more power.

The rating most commonly employed is the maximum power rating. Maximum current and maximum voltage ratings cannot be achieved simultaneously because the product of these two ratings usually exceeds maximum rating. The maximum voltage rating is set at a value safely below the collector voltage breakdown value while the maximum current is selected where β has not decreased to too low a value.

Table 9-8, high-frequency transistors, includes p-n-p and n-p-n fused junction, n-p-n grown junction, and p-n-p surface-barrier units. Except for the n-p-n grown type, which is of either germanium or silicon, all these units use germanium.

Physically, one of the main distinctions between these units and the low-frequency units is the closer spacing between emitter and collector junctions. Electrical characteristics are higher α cutoff, lower collector voltage breakdown, and in many units lower collector capacitance and lower base resistance. The widest application is in radio receivers and high-speed switching circuits.

In selecting a high-frequency transistor for a grounded-emitter IF amplifier, note that the β -cutoff frequency of the amplifier is equal to a cutoff frequency divided by β .

Table 9-9 lists tetrode junction transistors which are high-frequency triode n-p-n grown junction transistors with an extra base lead and a narrower base region. The electrical characteristics of the grown tetrode transistor are almost identical to the grown triode transistor except for a lower value of base resistance and higher value of α -cutoff frequency. The extra base lead makes the tetrode applicable in specialized control circuits and AVC applications. Bias for the extra base lead is usually obtained from a bleeder across the main supply.

High-power Units

The high-power transistor, Table 9-10, is in most cases the largest of all transistors. One element is attached to the container. In most units the case can be connected to the chassis either directly or through a thin mica spacer. The types used as power transistors are the germanium p-n-p fused and silicon n-p-n grown.

The p-n-p fused transistors are usually the high-power units whose larger physical size provides collector power dissipation up to 20 watts. The larger physical size also contributes a high collector capacitance and lower α -cutoff frequency. Medium-power p-n-p and n-p-n fused units which retain their smaller physical size and most of the electrical characteristics of the low-power transistors are used in applications requiring collector power dissipation below $\frac{1}{2}$ watt.

The characteristics peculiar to the high-power transistor are the lower values of input resistance, output resistance, and α , resulting from the higher values of bias currents employed. Bias stability techniques are used to minimize the effect of runaway due to self-heating of the collector.

The point-contact transistor, Table 9-11, is limited to high-speed switching circuitry. Phototransistor devices, Table 9-12, are divided into two basic types: the two-lead and three-lead devices. In the two-lead unit, one lead is attached to the base and the other to the collector. The three-lead device has leads going to the emitter, base, and collector, respectively.

The two-lead device is used in circuits providing d-c amplification for unmodulated light, while the three-lead device can be used in circuits employing a-c amplification for modulated light.

Acknowledgment is given to Ann M. Field and Elizabeth A. Sewell for their assistance in compiling these data.

Table 9-7. Junction-triode

				ره'	#				Small-sig	nal low-
76			power,	Max coli voltage, volts	curren	ent	Bi	as		
actui	No.		oli p	oli v	coll c	°C				8
Manufacturer	Type]	Type	Max coll I	Inv e	Max c ma	Max ambient temp, °C	V _c , volts	, ma		, ohins
									- a -	
Amperex Electronic Corp. 230 Duffy Ave. Hicksville, N.Y.	OC70 OC71	p-n-p fused a p-n-p fused a	25 (45°C) 25 (45°C)	-10 -10	-10 -10	45 45	$-2 \\ -2$	0.5 3	30 47	39 6.5
CBS-Hytron Danvers, Mass.	2N36 2N37	p-n-p fused p-n-p fused	50 50	$-20 \\ -20$	-8 -8	50 50	-6 -6	1	45 30	30 30
	2N38 HA-1	p-n-p fused p-n-p fused	50 50	$-20 \\ -20$	-8 -8 -8	50 50	-6 -3	1 0.5	15 40	25 24
	HA-2 HA-3	p-n-p fused p-n-p fused	50 50	$-20 \\ -20$	$-8 \\ -8$	50 50	-3 -3	0.5 0.5	30 35	35 30
O Part O	HC-1 NPN-3/	p-n-p fused	50 50 (25°C)	-20 35	-8 -8 10	50 75	-6 4.5	1 -1	45	30 25
Germanium Prod. Corp. 26 Cornelison Ave.	2N103	n-p-n grown		30	10				4	ì
Jersey City, N.J.	RD2517A/ 2N97	n-p-n grown	50 (25°C)			75	4.5	-1	13.3	25
	RD2518A/ 2N97A	n-p-н grown	50 (25°C)	40	10	85	4.5	-1	13.3	25
	RD2521A/ 2N98	n-p-n grown	50 (25°C)	40	10	75	4.5	-1	40	25
	RD2522A/ 2N98A	n-p-n grown	50 (25°C)	40	10	85	4.5	-1	40	25
	RD2523A/ 2N99	n-p-n grown	50 (25°C)	40	10	75	4.5	_I	40	25
	RD2525A/ 2N100	n-p~n grown	25 (2 5 °C)	25	5	50	4.5	-1	140	25
General Electric Co. Electronics Park	2N43 2N44	p-n-p fused p-n-p fused	150 (25°C) 150 (25°C)	-45 e -45 e	$-50 \\ -50$	100 100	$-5 \\ -5$	1 1	49 21.2	32 26.5
Syracuse, N.Y.	2N45 2N43A	p-n-p fused p-n-p fused	150 (25°C) 150 (25°C)	$-45^{e} - 45^{e}$	-50 -50	100 100	-5 -5	Î 1	11.5 43.4	20 15
	2N43A USAF	p-n-p fused	150 (25°C)	-45	-50	100	-š	î	43.4	15
0 15 11 0	2N76 GT-14	p-n-p fused	50 (25°C)	-20 e -25	-10	60	-5	1	19	17
General Transistor Corp. 95-18 Sutphin Blvd.	GT-20	p-n-p fused p-n-p fused	70 (50°C) 70 (50°C)	-25		85 85	-4.5 ·····		28 45	30 30
Jamaica, N.Y.	GT-34 GT-81	p-n-p fused p-n-p fused	70 (50°C) 70 (50°C)	$-25 \\ -25$		85 85			15 65	30 30
	GT-83 GT-87	p-n-p fused p-n-p fused	70 (50°C) 70 (50°C)	-25 -25		85			45 28	30 30
	GT-88 2N34	p-n-p fused p-n-p fused	70 (50°C) 70 (50°C)	-25 -25		85 85	_15	1	65 40	30 30
	2N36	p-n-p fused	70 (50°C)	-25		85	-4.5 -4.5	1	45	30
	2N37 2N38	p-n-p fused p-n-p fused	70 (50°C) 70 (50°C)	-25 -25		85 85	-4.5 -4.5	1	30 15	30 30
	2N39 2N40	p-n-p fused p-n-p fused	70 (50°C) 70 (50°C)	-25 -25		85 85	-4.5 -4.5	1	45 28	30 30
Hughes Aircraft Co.	2N42 HA5001	p-n-p fused n-p-n alloyed	70 (50°C) 500 (25°C)	-25 30	100	85 85	-4.5 5	1	13 65.6	30 16.5
Culver City, Calif.	HA5002	n-p-n alloyed	500 (25°C) 500 (25°C) 500 (25°C)	20 20	100 100	85 85	5	1 1	27.5	16 26
Hydro-Aire Inc.	HA5003 J-1	n-p-n alloyed p-n-p fused	150 (25°C)	-40	-10	50	-6	1	99 34	30
Burbank, Calif.	J-2 J-3	p-n-p fused p-n-p fused	150 (25°C) 150 (25°C)	-40 -40	-10 -10	50 50	-6 -6	1 1	1 5 9	30 30
	HA-1 CQ-1	p-n-p fused p-n-p fused	100 (25°C) 150 (25°C)	-20	-10 -10	50 50	-6 -6	1 1	40 9	30 30
Nat'l Union Electric	2N39 2N40	p-n-piused	47 (25°C) I	-40 -27 -27	-10 -12 -12	60 60	-6 -4.5 -4.5	1	32.4	
350 Scotland Rd. Orange, N.J.	2N42	p-n-p fused p-n-p fused	47 (25°C) 47 (25°C)	-18	-12	60	-4.5	1	15.7-32.4	
	T34D T34E	p-n-p fused a p-n-p fused a	56 (25°C) 56 (25°C)	$^{-27}_{-27}$	-12 -12	70 70	-4.5 -4.5	1 1	32.4 15.7-32.4	20 20
Phileo Corp.	T34F 2N47	p-n-p fused a p-n-p fused a	56 (25°C) 50 (25°C)	-18 -35	$-12 \\ -20$	70	-4.5 -5	1 1	9 39	20 25
4700 Wissahickon Ave. Philadelphia, Pa.	2N49	p-n-p fused a	50 (25°C)	-35	-20		-5	1	39	25
RCA	2N104	p- n - p fused b	110 (25°C)	-30	50	85	-6	1	44	24.5
Harrison, N.J.	2N77	p-n-p fused a	35 (25°C)	-25	15	50	-4	0.7	40	36
Raytheon Mig. Co.	CK721	p-n-p fused c		-15^{f}	-10	70	-6	1	45	25
55 Chapel St. Newton, Mass.	CK722	p-n-p fused c		-22^{f}	-10	70	-6	1	22	25
	CK725	p- n - p [used c		-12^{f}	-10	70	-6	1	90	25
	CK727 2N63	p-n-p fused c p-n-p fused		-6^{f} -22^{f}	-10 -10	70 85	$-1.5 \\ -6$	0.5	35 22	50 25
		r x praced								

Low-power Transistors

freque	ney par	ameters				Grour	nded-e	mitter e	onnect	ion		Grounde	d-bas	se	G	rounded-	eollector	
76, ohus	7c, megohms	faco, Mc	C_c , $\mu\mu^{[-]}$	$I_{co, \mu a}$	NF, db	I_b , ma	Ri, ohms	RL, ohms	Rg, ohms	Gain, db	Ri, ohms	RL, ohms	Rg, ohms	Gain, dl)	Ri, ohms	R_L , ohms	Rg, ohins	Gain, db
1,000	1.43 0.625			-8 -8	10 10													
450 350 350 700 350 450 450	0.95 0.55 0.5 1.7 0.8 0.6 0.95	0.5 0.5 0.5 		-12 -12 -12	12 27		225		1,000 1,000 1,000 1,000 1,000 1,000	40 36 32 30 30 35 40	45	250,00		20	9 500	F00		
100	3.0	0.75	20 19	5 2	20	0.25	400	100, mate 100,	hed	33	35	match 250,00	ed	30	2,500 7,000		atched atched	7
100	10.0	1.0	19	2	15	0.07	400	mate	hed	38	35	match 250,00	ed	32	7,000		atched	11
150	5.0	2,5	14	2	20	0.025	850	100,	hed	47	35	match 250,00	$^{\mathrm{cd}}$	35	20,000		atched	15
	10.0	2.5	14	2	15	0.025	850	mate 100,	hed	47	35	match 250.00	ed	35	20,000		atched	15
150	5.0	3.5	10	2	15	0.025	850	niate 100,	hed	47	35	match 250,00	ed	35	20,000		atched	15
400	5.0	5.0	14	2	20	0.007	3,500	mate 100,	000	53	45	match 250,00	00	35	70,000	l	atched	20
400	1.0	1.0	40	-10	22		1,000	30.000	600	39	60	match 50,000	100	28	30,000	600	30,000	15
300 250 575 575	1.0 1.0 1.43 1.43	1.0 1.0 1.0 1.0	40 40 40 40	10 10 5 5	22 22 10 30		700 450 1,000 1,000	30,000 30,000 30,000 30,000	600 600 600	38 36 39 39	55 50 60 60	50,000 50,000 50,000 50,000	100 100 100 100	28 28 28 28	15,000 7,500 30,000 30,000	600 600 600 600	15,000 7,500 30,000 30,000	12 11 15 15
300 800 800 800 800 800 800 350 600 400 850 400 900 400 900	2.0 2.0 2 1	1.0 0.65 0.65 0.65 0.70 0.50 1.0 	15	-5 -10 -10 -10 -10 -10 -10 -10 -15 -15 -15 -15 -15 -15 -15 -15 -15 -15	18 16 16 16 16 16 16 24 24 24 24 24 24 24		1,000	30,000	600	38	55	50,000	100	28	15,000	600	15,000	12
400 300 300 350 200	1.0 0.7 0.5 0.75 0.5 1-2	1.0 0.5 0.5		-10 -15 -20 -10 -20 -10	11 22 33 20 33 20			30,000	500	40 35 30								
600	$ \begin{array}{c} 1-2 \\ 0.5-2 \\ 1-2 \\ 1-2 \\ 0.5-2 \\ 1.0 \end{array} $	1.0	49	-10 -20 -10 -10 -20 -10	24 28 20 24 28 15		1,000	30,000 30,000 30,000 30,000 30,000 50,0		38 36 39 38 36 42								
600	1.0	1,0	49	-10	12		1,000	50,0 mate	00	42								
750	2.25	0.7	٠	-10	12		1,200	50,0	00	43	140	400,00 matche	ed	32.8	500,000			13.9
560	2.3	0.7	 	-10	9		1,350	50,0 mate	00 hed	42.6	130	400,00 matche	od ed	33.2	10,000		atched	16.2
700	2.0			-6	22		1,500	20,0 mate	hed	41	70	matche	ed	31	600,000	20,000 r		15
250	2.0		'' 	-6	. 25		500	20,0 mate	hed	36	45	100,00 matche	ed	32	200,000	20,000 r		10
1,500	2.0			-6	20		2,700	20,0	hed	42	110	matche	ed {	30	1,000,000	20,000 1		16
350 350	2.0 2.0		··· 	-6 -6	$\begin{vmatrix} 12 \\ 25 \end{vmatrix}$		800	20,000, 20,0 mate	00	36 39	50	200,000 100,00 matehe	0	28 32	540,000 350,000	10,000 20,000	100,000 matched	14 13

Table 9-7. Junction-triode Low-

				, 2,	ŗ,				Small-sig	gnal low-
urer			рожег	coll voltage,	curren	ient	B	as		
Manufacturer	Type No.	Type	Max coll power,	Max coll voits	Max coll current, ma	Max ambient temp, °C	Ve, volts	<i>I_e</i> , ma	В	re, ohms
Raytheon (Continued)	2N64	p-n-p fused		-15^{f}	-10	85	-6	1	45	25
	2N65	p-n-p fused		-12	-10	85	- 6	1	90	25
Sylvania Electric 1740 Broadway New York, N.Y.	2N34 2N35	p-n-p fused n-p-n fused	50 (25°C) 50 (25°C)	-40 -40	-10 -10		-6 6	-1	40 40	26 26
Texas Instruments 6000 Lemmon Ave. Dallas, Tex.	200 201 202 206S 207S 207S 208S 300 301 903 904 905 904 302 302 303 904 905 309 309 309 309 309 309 309 309 309 309	n-p-n grown p-n-p fused p-n-p fused p-n-p n grown n-p-n grown	50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 150 (25°C) 150 (25°C) 150 (25°C) 50 (25°C) 50 (25°C) 50 (25°C)	30 30 30 30 30 30 -30 -30 30 30 30 30 30 30 30 30	5 5 5 5 5 10 -10 -10 10 10 10 10 10	50 50 50 50 50 50 50 150 150 150 150 50	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	-1 -1 -0.5 -0.5 -10 1 -1 -1 -1 -1 -2 1	9 19 49 35 19 19 9 19 9-19 19-39 ▼ 39 ▼ 19	22 22 35 150 150 150
Transitron 407 Main St. Mclruse, Mass. Trans-Sol Electric	2N85 2N86 2N87 2N88 2N89 2N90 2N91 2N91 2N34 2N36 2N37 2N38 2N43 2N43 2N43 2N44 2N63 2N63 2N64 2N64 2N64 2N64 2N64 2N64 2N64 2N64	p-n-p fused	750 750 750 25 25 25 125 125 125 125 125 125 125 375 375 375 125 125 125 125 125 125 50 (25°C)	-45 -60 -30 -12 -12 -12 -15 -25 -25 -25 -45 -45 -25 -25 -25 -25 -25 -25 -25 -25 -25 -45 -25 -25 -25 -25 -25 -25 -25 -25 -25 -2	-100 -100 -100 -100 -10 -10 -10 -10 -500 -200 -20 -20 -20 -50 -50 -50 -20 -20 -20 -20 -20 -20 -20 -20 -20 -2	100 100 100 85 85 85 85 85 100 100 100 100 100 100 100 100 100	-12 -12 -13 -1.3 -3 -6 -6 -6 -6 -6 -6 -6 -1.5	10 10 0.5 0.5 2.5 30 5 1 1 1 1 1 1 1 0.5 5 5 5 1	40 20 25 40 25 40 40 45 30 45 30 16 9 20 30	2.5 2.5 50 50 10 1.5 5 18 20 20 20 20 20 20 20 20
100 Eighth Ave. Newark, N.J. Western Electric 120 Broadway	DR128 DR129 DR130 DR154 2N27 2N28	p-n-p fused d p-n-p fused d p-n-p fused d p-n-p fused d n-p-n grown n-p-n grown	50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 50 (60°C) 50 (60°C)	$ \begin{array}{r} -10^{g} \\ -25^{g} \\ -25^{g} \\ -25^{g} \\ 30 \\ 30 \end{array} $	 5 5	85 85 85 85 85	-1.5 -1.5 -1.5 -1.5 4.5 4.5	0.5 0.5 0.5 0.5 -1 -1	49 32.4 13 124 19–198 5–198	34 26 20.5 55 50 125
New York, N.Y. Westinghouse Box 284 Elinira, N.Y.	2N54 2N55 2N56	p-n-p fused a p-n-p fused a p-n-p fused a	200 (25°C) 200 (25°C) 200 (25°C)	45 45 45	-10 -10 -10	60 60 60	-6 -6 -6	1 1 1	33 20 13	25 20 5

All sockets A to H except where otherwise noted, a Socket type A. Socket types B to H. Socket types A. I, and J. d Socket type not given.

power Transistors (Continued)

freque	ncy pai	ameters		_	Groun	nded-ei	nitter ce	nect	ion		Grounde	d-bas		Gro	ounded-c	ollector	
	sm								I								 i
rb. ohms	r_{c_i} megohms	faco. Mc	Ісо, µз	NF, db	Ib. ma	R _i , ohms	R_L , ohms	Rg, ohms	Gain, db	Ri, ohms	R1., ohnis	Rg, ohms	Gain, db	R_{i} , ohms	R_{L} , ohms	$R_{g_{r}}$ ohms	Gain, dly
700	2.0		-6	22		1,500	20,0		11	70	100,0		31	600,000	20,000	matched	15
1,500	2.0		-6	20		2,700	20,0 nuate	100	42	110	match 100,0	00	30	1,000,000	20,000	matched	16
800 800	$^{2.0}_{2.0}$	0.6 15 0.8 18	$-5 \\ 5$	18	$-0.03 \\ 0.03$	$^{1,200}_{1,200}$	30,000	500 500		 	match			20,090 20,000		atched atched	16 16
150 170 200	0.4 0.4 0.4	0.9 15 1.1 17 1.3 19	10 10 10 3 3.5	26		480 970 1,250	20,000 20,000 20,000 20,000 20,000 300	500 500 1,250 1,000 1,000 1,000	37 40 43 32 29 26	40	100,000 100,000 100,000	60 60 60	30 30 31	9,500 15,500 32,000	500 500 500	15,000 15,000 15,000	12 14.5 17
550 1,000 500 1,250 2,500	0.4	3	- 10 - 10 1 (25°C) 1 (25°C) 1 (25°C) 1 (25°C) 50 (25°C) - 10	$\frac{23}{23}$			10,000										
300 300 300 1,000 1,000 1,000 500	0.125 0.5 2.0 0.5 2.0	0.8 0.8 0.5 0.5	$-10 \\ -15$	20 20 20 10 20 20 20			20,000	500 500 500 1,000 1,000 1,000	26 26 36 36								
500 600 700 500 250 500 300 350 700 1,500 900 1,400 1,200 650 600 700	1.0	0.9 0.9 0.9 0.7 0.5 0.7 2 17 0.95 25	$-10 \\ -9$	20 20 22 24 20 22 25 22 20 14 18 18 30 30	-0.006 -1.5 -0.006 -0.006 -0.006		30,000 30,000 30,000 30,000 30,000 30,000 30,000 30,000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	30 32 40 37 33 38 39 41 33 24 35 27								
400 400 400	1.0 1.0 1.0	0.5	-6 -6 -6	 		550	50,000 67,000 85,000	700 550 450		125	300,000 300,000 300,000	125		35,000 27,000 20,000	1,000 1,000 1,000	35,000 27,000 20,000	15 13 11

Characteristics measured at 25°C unless otherwise noted.
° Characteristics measured at 30°C.
† Characteristics measured at 27°C.
§ Temperature not given.

Table 9-8. High-

				23		ာ့			Ту	pical sma	ll-signal
			H H	, voli	, ma		ro	Bi	as		
Manufacturer	Type No.	Type	Max coll power, mw	Max cell voltage, volts	Max coll current,	Max ambient temp,	Storage temp, °C	V_c , voits	<i>Iе</i> , та	В	re, ohms
General Electric	2N78	n-p-n rate	50 (30°C)	15	20	100	100 max	5	-1	27.5	
Germanium Prod.	2N123 2N135 2N136 2N137 RD2523A (2N99)	grown p-n-p fused p-n-p alloyed p-n-p alloyed p-n-p alloyed n-p-n grown	150 (25°C) 100 (25°C) 100 (25°C) 100 (25°C) 50 (25°C)	-15 -20 -20 -10 40	150 -50 -50 -50 -50 10	75	85 85 85 85	-5 -5 -5 -5	1 1 1 1 -I	30-150 20 40 60 40	25
	RD2525A	n-p-n grown	25 (25°C)	25	5	50		5	-1	100	25
	(2N100) RD2521A (2N98)	n-p-n grown	50 (25°C)	40	10	75		5	-1	40	25
	RD2517A	n-p-n grown	50 (25°C)	30	10	75		5	-1	13	25
Hydro-Aire Philco	HF-1 IF-1 SB-100	p-n-p fused p-n-p fused surface barrier a	35 (25°C) 35 (25°C) 10 (40°C)	-15 -15 -4.5	-5 -5 -5	55 55	-55 to 85	$ \begin{array}{r} -4.5 \\ -4.5 \\ -3 \end{array} $	1 1 0.5	25 20 19	30 30 50
Raytheon	CK-760	p-n-p fused		-6°	-5		55 to 85	-6	1	45	22
Tally viscols	CK-761 CK-762	p-n-p fused p-n-p fused		-6°	-5 -5		-55 to 85	$-6 \\ -6$	1	50 60	22 22
Sylvania	2N94	n-p-n alloyed	50 (25°C)	20	10		-55 to 85	6	-0.5	30	52
	2N94A	n-p-n alloyed	50 (25°C)	20	10		-55 to 85	6	-0.5	30	52
Texas Inst.	220 221 222 223 904A 224-1 2 3 4 5 225-I 2 3 4 5 225-I 2 2 3	n-p-n grown a n-p-n grown	50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 150 (25°C)	30 30 30 30 30	5 5 5 10	50 50 50 50 150		22.5 22.5 22.5 22.5 5 	-1	≥19 	150
	3 4 5 227-1 2										···
	3 4		• •								
Tung-Sol	5 DR-155 2N112 2N113	p-n-p fused b p-n-p fused p-n-p fused p-n-p fused	50 (25°C) 50 (25°C) 50 (25°C)	-10 10 10	-8 -8	85 85 85	-55 to 85 -55 to 85 -55 to 85	-1.5 -6 -6	0.5 1 1	32 32 32 32	3I 31
Western Electric	2N27	n-p-n grown	50 (60°C)	30	5	85		4.5	-1	20-198	50

Socket types A to H unless otherwise noted, ^a Socket type A only. ^b Socket types A and J.

frequency Transistors

E E E E E E E E E E	parameters		HF param- eters	High-frequ	ency ci	reuit cond	itions			h-speed s haracter		g
7.5 14 4.5 14 6.5 14 10 14 150 5.0 3.5 10 400 5.0 5.0 14 100 3.0 1.0 19 500 1.0 5.0 10 500 1.0 5.0 10 500 1.0 2.1 10 0.4 30 2.2 70 1.0 10 10 14 70 1.0 20 14 500 2.0 3.5 10 500 2.0 6.0 10 1,250 0.5 ≥8	faca. Mc Се. µµ[Ico. µа	Ico, µа NF, db	r _b C _c , μμ seα	Application	Ri, ohms	R_o , ohms	Power gain, db	Circuit	Rise time, µsec	Fall time, µscc	Reverse emitter voltage, volts	Great
4.5 14 10 10 10 11 10	5.5 6 1	14		RF amp	1,000	6,000	20					1
150 5.0 3.5 10 400 5.0 5.0 14 150 5.0 2.0 14 100 3.0 1.0 19 500 1.0 5.0 10 500 1.0 5.0 10 0.4 30 2.2 10 0.8cc) 70 1.0 5 14 70 1.0 5 14 70 1.0 20 14 500 2.0 3.5 10 500 2.0 6.0 10 	4.5 14 5 6.5 14 5	5 10		IF amp Switching RF/IF amp RF/IF amp	1,500	10,000	30 29 31		0.1	0.2	5	
150 5.0 2.0 14 100 3.0 1.0 19 500 1.0 5.0 10 500 1.0 2.2 10 0.4 30 2.2 (0ssc) 70 1.0 5 14 70 1.0 10 14 500 2.0 3.5 10 500 2.0 6.0 10 1,250 0.5 ≥8		15		RF/IF amp IF amp unneut	500	10,000	33 22		< 0.2	< 0.3		l
100 3.0 1.0 19 500 1.0 5.0 10 500 1.0 2.9 10 0.4 30 2.2 (osc) 70 1.0 5 14 70 1.0 10 14 70 1.0 20 14 500 2.0 6.0 10 	5.0 14 2	20		IF amp	750	10,000	23		<0.2	< 0.3		
500 1.0 5.0 10 500 1.0 2.1 10 0.4 30 2.2 (osc) 70 1.0 5 14 70 1.0 10 14 500 2.0 3.5 10 500 2.0 6.0 10 1,250 0.5 ≥8	2.0 14 2	20		IF amp	500	10,000	22		< 0.2	< 0.3		
500 1.0 2.0 10 10 30 2.2 (osc) 70 1.0 5 14 70 1.0 10 14 500 2.0 6.0 10 10 14 10 10 14 10 10	1.0 19 2	20		IF amp	350	10,000	20		< 0.2	<0.3		
70 1.0 5 14 70 1.0 10 14 70 1.0 20 14 500 2.0 3.5 10 500 2.0 6.0 10	$ \begin{array}{c cccc} 2.9 & 10 & -10 \\ 30 & 2.2 & -0.5 \end{array} $	0.5	800	,								
1,250 0.5 ≥8 	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 25 2 25 2 25 -3 15	1,000 1,000 1,000 1,000	IF (g-l ₁) IF (g-e)	80 500	100,000 25,000	25 d 32 d	C D	0.15	0.15	≥0	F
1,250 0.5 ≥8	6.0 10 3	-3 15	1,200	IF (g-b) IF (g-e)	80 800	100,000 25,000	$\frac{25}{35} \frac{d}{d}$	C D	0.1	0,1	≥0	l
	50 50 50			RF (g-b) 262-ke (g-e) IF 262-ke (g-e) IF 262-ke (g-e) IF 262-ke conv	750 750 750 750 300	15,000 70,000 70,000 70,000 60,000	20 ^e 31 33 35 20	E A A A B				
	_			Neut 262-kc	600	70,000	26	Н				
				g-e IF			28 30					ł
	1 1 1						32					
				Neut 455-ke	500	50,000	34 24	Н				
				g-e IF			26	"]
							28 30					
							32					ł
				Neut 262-kc	65	120,000	18	Ι				1
	1 1 1			g-b IF			20 22					
	1 1 1						24					
				Nout 455 kg	65	150,000	26 18	1				
				Neut 455-kc g-b IF		150,000	20	1				
							22					
							24					
1.0 1.4		28					26					
110 1.2 5	510	28		IF	600	25,000	32	G				
110 1.2 10 700 2.0 2 17	10 -10	28		IF	600	25,000	33	G				

Characteristics measured at 25 °C unless otherwise noted. $^{\circ}$ Characteristics measured at 27 °C. d Bandwidth 12 kc. $^{\circ}$ Bandwidth 25 kc.

Table 9-9. Grown n-p-n

Manufacturer	Type No.	Max coll power, mw	Max coll voltage, volts	Max coll current, ma	Max base- to-base current, ma	Application
Germanium Prod.	RDX-302/3N23 RDX-301/3N23A RDX-300/3N23B RDX-300A/3N23C	50 (25°C') 50 (25°C) 50 (25°C) 50 (25°C)	30 30 30 30	5 5 5	5 5 5	Video amp, switching 10-Me osc Video amp, switching 20-Me osc Video amp, switching 35-Me osc 20-Me IF Video amp, switching 50-Me osc
Texas Inst. Western Electric	700 3N22	50 (25°C) 50 (25°C) 30 (25°C)	30 12	5 5 5	5 5	20- to 30-Mc IF Low-level, low-freq age Video amp, R-F

All sockets A, F, G, H, and M.

Table 9-10.

		_	Max	power output, v	vatts		Max e			- 1	Small	signal
rer						ower,	voltage.	volts	coll current,		Bia	ıs
Manufacturer	Type No.	Type	('lass A	(push-pull)	D-C switch	Max coll power, watts	Circu	it Î	Max coll et amp	face. ke	Ve, volts	Ie, ma
Amperex	2N115	p-n-p fused *	1.5	2.5		2 (45°C)	-12(B) -6(A)		-1	300		
CBS-Hytron Hydro-Airc Minicapolis-	2-OC72 H D-197 JP-1 H-1	p-n-p fused * p-n-p fused * p-n-p fused * p-n-p fused *	0.45 5	0.9 10	1.5 40	0.045 (45°C) 0.5 (25°C) 0.5 (25°C) 20 (21°C)	-0(A) -13(B) -40 -30	-45	0.045 -0.1 -0.8	150	-10 -22.5 -2	50 20
Honeyweli Regulator Co. 2753 4th Ave. S	2N57	p-n-p fused *	6	12	48	20 (21°(°)	-30	-60	- 1	20	-2	
Minneapolis,	H-2	p-n-p fused *	8.5	18	68	20 (21°C)	-30	-60	-1.4	201	-2	
Minn.	H-3	p-n-p fused *	2	4	16	5 (21°C)	-30	-60	-0.35	20	-2	
	H-4	p-n-p fused †	2	6	16	5 (21°C)	-30	-60	-0.5	20	-2	۱ _۱
Sylvania	2N68	p-n-p alloyed †	0.75	10		4 (25°C)		-25	-1.5		-6	50
	2N95	n-p-n alloyed †	0.75	10	·	4 (25°C)	i	25	1.5	ļ : 	6	-50
Texas Inst.	2N101 2N102 X-2	p-n-p alloyed n-p-n alloyed n-p-n grown	١	Electrically ide Electrically ide				35	0.075	225	5	-1.
	951	n-p-n growu Silicon		0.45 (25°C) 0.3 (100°C)		1 (25°C) 0.5 (100°C)	50		0.06	! ! !		
	952	n-p-n grown Silicon		'0.35 (150°C) 0.6 (25°C) 0.1 (100°C) 0.15 (150°C)		0.15 (150°C) 1 (25°C) 0.5 (100°C) 0.15 (150°C)	80	j ::::	0.05			
	953	n-p-n grown Silicon	· 	1 (25°C) 0.5 (100°C)	: : :	i (25°C) 0.5 (100°C)	120		0.04	 		
Transistor Products 241-251 Crescent Ave.	X-107 X-120	p-n-p fused * p-n-p fused *	1 7.5	0.15 (150°C) 		10.14 (150°C) 12 (25°C) 15 (25°C)	-30 -30	-60 -60	-1 -4		$-24 \\ -28$	80 360
Waltham, Mass. Transitron	! 2N83 2N84	p-n-p fused ‡ p-n-p fused ‡	5 5	15 10	40 30	10 (25°C) 10 (25°C)	$-30 \\ -22$	-45 -30	$-1 \\ -1$	$ ^{200}_{200}$	$-20 \\ -20$	100 100
Tung-Sol Western Electric	DR-150 2N66	p-n-p fused p-n-p fused *		1	3.5	5 (25°C) 5 (25°C)	$-\dot{10}$	$-25 \\ -60$	$\begin{bmatrix} -1 \\ -0.8 \end{bmatrix}$	$\frac{250}{500}$	$-15 \\ -4.5 \\ -40$	10 100 0

^{*} Type A sockets. † Socket types A to II.

Junction-tetrode Transistors

		Typical operation							
V _c .	I _e ,	I_{h2} , ma	α	r _e , ohms	tb. ohms	r _c , megohins	I_{cv} , μa	Freq. Me Circuit J	Power-gain at 5 Mc Circuit K
4. ŏ 4. 5 4. 5	1 1 1	0 0 0	0.95 0.97 0.98	30 30 30	70 100 200	2 2 2	10 10 10	10-20 20-35 35-50	12 14 15
4.5	1	0	0.99	30	300	2	10	50-80	17
5 9 9	$ \begin{array}{c} -1 \\ -2 \\ -2 \end{array} $	$-\frac{0}{4.5}$	0.95 0.90 0.975	30 25 25	1,000 100 1,000	1 1 i	10 10	15	

Characteristics measured at 25°C.

Power Transistors

ow-l	requen	су рага	uneters							T	ypical	operating condi	tions				_
β	r _c , ohms	r ₆ , ohms	re, ohms	C_c , $\mu\mu$	Rise time, assec	Іса, да	Class and circuit	Supply voltage, volts	Coll current,	Base current,	Zero signal current, ma	Power output, watts	Power gain, db	Driving ромег, пъ	R_c , ohus	RL, ohms	Re, ohms
							B(g-e)	- G	-1,280		-5	5 ¶	27				
iö 9 	2	70 150	5,000		1.5 1.2 0.5 1.2	-500 -8,000 -8,000 -8,000 -1,000	B(g-e) A B(g-b) A(g-e) B(g-e) A(g-e) B(g-e) A(g-e) A(g-e) B(g-e) A(g-e) B(g-e)	-6 -22.5 -28 -28 -28 -28 -28 -28 -28 -28 -28	-50 -40 400 510 500 640 690 150 220	50 45 30	4 4 4		27 30 120 15 12 16 13 20 16 16 16 12	158 630 156 625 75 440 48 278	20 100 35 140 40 100 100 240	5,000 70 140 56 128 47 80 187	100
40	1 1	30	100,000		0.6	- 1,000 - 100	A(g-e) B(g-e) A(g-b) B(g-e) B(g-b) A(g-b) B(g-e) B(g-e) B(g-b)	$egin{array}{c} -28 \\ -28 \\ -12 \\ -12 \\ -12 \\ -12 \\ 12 \\ 12 \\ 12 $	150 318 - 150 550 - 550 - 950 150 550 950		0.5 -1 -1 -1 1 1	1.9 6.25 6	21 14 23 15 10 10 23 15 10 10 10	15 250 	60 200 75 50 250 250 75 50 250 250 2	187 224 100 12 12 12 100 12 100 12 12 12	5 5 10
9	25	0.75	200,000	· ;	 	25 5	B(g-b) B(g-b) B(g-e)	22.5 22.5 28	40 40 30	i	· · · · · · · · · · · · · · · · · · ·	0.5 ° 0.5 0.45 (25°C) ° 0.15 (150°C)	9.5 22.7 20			1,000 1,000 1,500	 1,00
	İ			ļ	! : • •	6	B(g-e)	15	25			0.6 (25°C) ¶ 0.15 (150°C)	21			4,000	1,00
	!			l		8	B(g-e)	67.5	20			1 (25°C) € 0.15 (150°C)	23		.,.	! 8,000	1,000
$\frac{22}{20}$	0.85 0.65	12 1	50,000 10,000			-120 -200	A(g-b) A(g-b)	-28 -28	$-80 \\ -360$: 	l :::	l 5	24 20	1 50	1.5 0.8	375 100	
8 12	0.3	15 15	20,000 20,000			100 100	Big-et Big-et	-30 -20	- 160 - 160	l		2.5 ¶	24 22			600 400	100 100
33 45			30,000	400	[<u></u>	75 300											

[‡] Socket types A and K. ¶ Push-pull connection.

Table 9-11. Point-

Manufacturer	Type No.	Application	Max coll power, mw	Max coll voitage, volts	Max coll current, ma	Max reverse emitter voltage, volts	Max emitter current, ma	Max emitter power, mw
Hydro-Airc Sprague Electric Transistor Prod.	A-0 A-1 A-2 A-3 S-0 S-1 S-2 S-2 A 2A 2A 2C 2D 2E 2C 2H 2L 2N32 2N32 2N53 2N51 2N53	Amp, osc Amp, osc Amp, osc Amp, osc Amp, osc Switching Switching Switching Switching Amp, osc, sw Switching Amp, osc Amplifier Amplifier Switching	0 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 50 (25°C) 120 (25°C) 120 (25°C) 100 (25°C)	-20 -20 -20 -20 -20 -40 -40 -30 -50 -50 -50 -50 -50 -50 -50 -50 -50 -5	-8 -8 -8 -8 -8 -10 -8 -8 -8 -8 -8 -8 -8 -8 -8 -8 -8 -8 -8		:::	::: ::: ::: ::: :::
Western Electric	2N21 2N21A 2N110 2N67	Switching Amp, osc, sw Switching High-speed sw	120 (25°C) 120 (25°C) 200 (25°C) 100 (25°C)	-100 -100 -100 -100	-60 -60 -75 -60	-100 -100 -100 -100	60 60 75 60	80 (25°C) ^b 80 (25°C) ^b 100 (25°C) ^b 60 (25°C) ^b

Socket types A to H unless otherwise noted.

^a Socket types A and L
Maximum ambient temperature 50°C unless otherwise noted.

^b Maximum abient temperature 85°C.

Characteristics of A-0, A-1, A-2, A-3, 2N21, 2N21A, 2N110 and 2N67 measured at 25°C.

PARAMETER CONVERSION FORMULAS

$H_{21} = \frac{R_{21}}{R_{22}} = -\alpha$ $H_{11} = R_{11} - \frac{R_{21}R_{12}}{R_{22}}$ $r_b = r_c H_{12}$ $|\alpha| = |H_{21}|$ $r_e = H_{11} - r_b(1 - \alpha)$

TRANSISTOR SOCKETS

	Code Manufacturer	Type
A	Solder connections	
В	Elco Corp.	3-pin polarized
		3-pin printed-circuit
C	Cinch Mfg. Corp.	3-pin polarized
D	Super-Ear Prod. Co.	3-pin polarized
E	Mycalex Tube Socket Corp.	3-pin polarized
F	Eleo Corp.	4-pin polarized
		4-pin printed-circuit
G	Super-Ear Prod. Co.	5-pin
Н	Eleo Corp.	5-pin
	•	5-pin printed-circuit
I	Super-Ear Prod. Co.	3-pin equal spacing
J	Cinch Mfg. Corp.	5-pin
K	Amphenol Co.	
L	Cinch Mfg. Corp.	
М	Cinch Mfg. Corp.	4-pin polarized

contact Transistors

		St	nall-sig	mal lo	w-frequenc	ey para	mete	rs			La	rge-sign:	al param	eters	
Ve. volts	Ie, ma	-α	re, ohms	rb, ohms	re, ohms	faco, Mc	Се, им	NF, db	Ісо, на	Rise time, µsec	Тиглоff time двес	Off Ic, ma	On V _c , volts	Fmitter rev resist., ohms	α (at max rise time)
-8 -8 -8 -8 	0.3 0.3 0.3 0.3 0.3	2 2 2 2 2 2 2 3	425 425 375 350	200 200 175 150	13,000 13,000 13,000 13,000	3 2 1 0.3 5		43	-1,200 -1,500 -2,000 -2,000	0.2 ° d 0.5 d 1 ° 0.12	0.5	-1 -1 -1	-2 -2 -2 -2	50,000 50,000 50,000	
10 10 10 10	1 1 1 1	2.5 f 2.5 f 2.5 f	200 200 200 900	90 90 90 500	10,000 10,000 15,000 20,000	2 2 1.5 20		45 45	$ \begin{array}{c} -1.1 \\ -1.1 \\ -0.9 \\ -0.9 \end{array} $	0.2 0.2 0.3 0.02	1.3 1.3 1.3 0.9	-1.1 -1.1 -0.9 -0.9	-1 -1 -1 -0.8	200,000 200,000 200,000 2,000,000	5 5 4 7

Table 9-12. Phototransistors

Manu- facturer	Type No.	Туре	Max coll volt- age, volts	Max coll cur- rent, ma	Max coll power, mw	Max dark current, μa	Max am- bient temp., °C	Cut- off freq., ke	Noise, ft-c	Sensitivity, µa/ft-c
General									_	
Transistor	GT-66	Fused, 3 lead *	12	20	50 (25°C)	15		750	6×10^{-5}	25
Texas Inst.	800	Grown, 2 lead †	20	20	50 (25°C)	250	40	20		35
Transistor	1N188	Grown, 2 lead	100		40 (25°C)		50		3-10 µv	10 μa/millitumen
Prod.	1N189	Nonrect, 2 lead			30 (25°C)	20	50			0.08%/ft-c
	10A	Grown, 2 lead	15		100 (25°C)	500	50		15-100 μv	4 ma for 300 ft-c
	10B	Grown, 2 lead	15		100 (25°C)	50	50		15-100 μv	50% for 10 ft-c
	5B	Grown, 2 lead	50		100 (25°C)	20	50		3-10 µv	1 ma for 300 ft-c
	5C	Grown, 2 lead	50	ł	100 (25°C)	5	50		3-10 µv	50% for 40 ft-c
	11A	Nonrect, 2 lead	15		50 (25°C)	4,000 nhms	50			2,000 ohms for 300 ft-c
	11B	Nonrect, 2 lead	15		50 (25°C)	4,000 ohms	50			3,000 ohms for 300 ft-c
	17A	Grown, 2 lead							Be ow 1 µv	
Western Electric	1N85	Grown, 2 lead *	90	1	50	20	85	25	$2 \times 10^{-6} \mu a$	0.35 μa/μw

 $[^]c$ Fall time = 1 μ sec. d Fall time = 2 μ sec. e Fall time = 6 μ sec. f Large-signal α = 2.4.

^{*} Socket type A. † Socket type A to H.

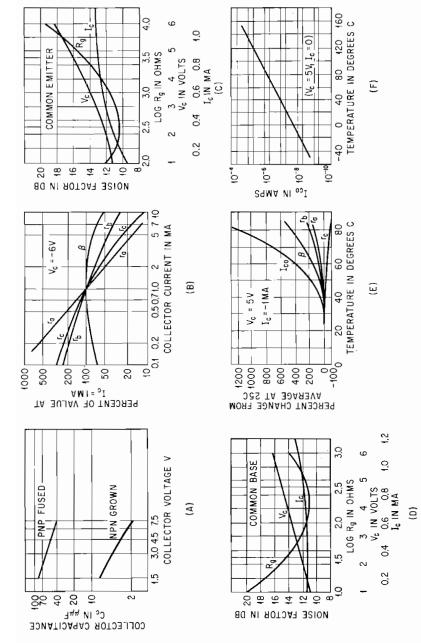


Fig. 9-26. Variation of transistor parameters with operating point (A to D) and ambient temperature (E, F).

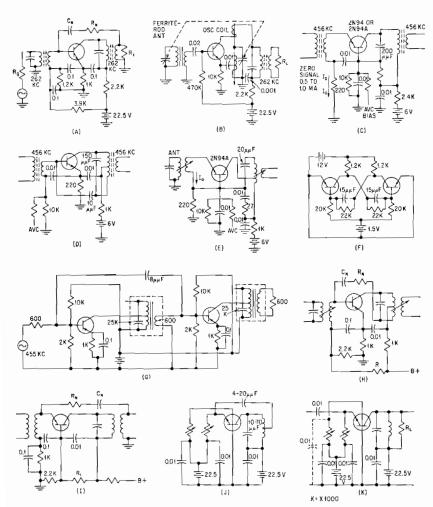


Fig. 9-27. Typical circuits for high-frequency transistors (A to I) and junction tetrode transistors (J,K) referred to in Tables 9-8 and 9-9.

Table 9-13. NAB Data Concerning Tower Failures

Information obtained from 298 television stations during 1958 indicated that 11 towers failed for various reasons. Briefly, 6 towers failed because of high winds, 2 fell during construction, and 3 failed because of structural weakness or faulty design. The following is a detailed breakdown of these 11 failures:

Height, ft	Type	Weather conditions	Cause and comments
826	SS	High wind	Broke in half during high wind
487	SS	97-inph wind	Failed at 125 ft above ground in wind
370	SS	Est. wind 190 knots	Due to gusty turbulence
570	SS	Hurricane "Carol"	Broke off TV tower at 200-ft level, Aug. 31, 1954
1250	G	50- to 60-mph winds	"Tower was completed to the 1,250 point. However, the top set of guys were not completely installed and in the process of tensioning these guys, high winds came up (50 to 60 m.p.h.), the unguyed portion of the tower began to oscillate, finally broke off at the 1150' point and in falling, cut a permaneut guy at the 1000' level which in turn caused the entire structure to fail."
100	G	High winds	During process of erecting, 100 ft had been erected and temporary guy lines attached. Under high winds the temporary lines failed
450	SS	40-mile squall	Faulty design of tower
500	G	High level winds	Structural weakness
1262	G		Fell during erection, Feb. 4, 1957
649	Ğ		Due to excessive strain during the process of attempting to lower a 12-bay antenna from it all at once. Actual cause of collapse not known, but it is not believed to have been caused by tower weakness
550	G		Collapsed during construction. Cause not fully determined, but accident was during guy tensioning

Table 9-14. Decimal Equivalents

1/82	0.03125	17/32	0.53125
1∕16	0.0625	%16	0.5625
3/32	0.09375	19/32	0.59375
1/8	0.125	5/8	0.625
5/32	0.15625	²¹ /32	0.65625
346	0.1875	11/16	0.6875
7/32	0.21875	23/32	0.71875
1/4	0.25	3⁄4	0.75
9⁄32	0.28125	25/32	0.78125
5/16	0.3125	13/16	0.8125
11/32	0.34375	²⁷ /32	0.84375
3/8	0.375	7 ∕8	0.875
13/32	0.40625	29/32	0.90625
7/16	0.4375	15/1 ₆	0.9375
15/32	0.46875	31/32	0.96875
1/2	0.5	1.0	1.0

Table 9-15. Standard Metal Gauges

No.	American or B & S *	U.S. Standard †	Birmingham or Stubs ‡
1	0.2893	0.28125	0.300
2	0.2576	0.265625	0.284
3	0.2294	0.250	0.259
4.	0.2043	0.234375	0.238
5	0.1819	0.21875	0.220
5 6	0.1620	0.203125	0.203
7	0.1443	0.1875	0.180
8	0.1285	0.171875	0.165
9	0.1144	0.15625	0.148
10	0.1019	0.140625	0.134
11	0.09074	0.1250	0.120
12	0.08081	0.109375	0.109
13	0.07196	0.09375	0.095
14	0.06408	0.078125	0.083
15	0.05707	0.0703125	0.072
16	0.05082	0.0625	0.065
17	0.04526	0.05625	0.058
18	0.04030	0.050	0.049
19	0.03589	0.04375	0.042
20	0.03196	0.0375	0.035
21	0.02846	0.034375	0.032
22	0.02535	0.03125	0.028
23	0.02257	0.028125	0.025
24	0.02010	0.025	0.022
25	0.01790	0.021875	0.020
26	0.01594	0.01875	0.018
27	0.01420	0.0171875	0.016
28	0.01264	0.015625	0.014
29	0.01126	0.0140625	0.013
30	0.01003	0.0125	0.012
31	0.008928	0.0109375	0.010
32	0.007950	0.01015625	0.009
33	0.007080	0.009375	0.008
34	0.006350	0.00859375	0.007
35	0.005615	0.0078125	0.005
3 6	0.005000	0.00703125	0.004
37	0.004453	0.006640626	
38	0.003965	0.00625	
39	0.003531		
40	0.003145		

Used for copper, brass, aluminum, etc.; nonferrous alloy sheets, rods, and wire. Used for iron, steel, nickel, and ferrous alloy materials.

Used for seamless tubes and by some manufacturers for brass and copper materials.

Charts and Graphs

Table 9-16. Drill Sizes

Number	Will clear screw	Brass, iron, steel tapping *
$\frac{1}{2}$	12-24	
3	12–20	14-24
4	12-20	
5 6		
7		
8		
9	10.02	
$\begin{array}{c} 10 \\ 11 \end{array}$	10-32 $10-24$	
12	10-24	
13		
14		
15 16		12-24
17		12-24
18	8-32	
19		12-20
20 21		10-32
22	• • • • •	10-32
23		
24		
25 26		10-24
27		
28	6-32	
29		8 - 32
30 31		
32		
33	4-36, 4-40	
34		0.00
35 36		6-32
37		
38		
39 40	3–48	
41		
42		4-36, 4-40
43	2–56	
$\begin{array}{c} 44 \\ 45 \end{array}$		2.49
46		3-48
47		
48		
49		2-56
50 51		
52		
53		
54		

[•] For tapping plastic, bakelite, lucite, hard rubber, micalex, etc., use one size larger drill.

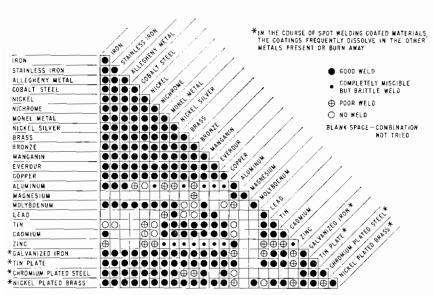
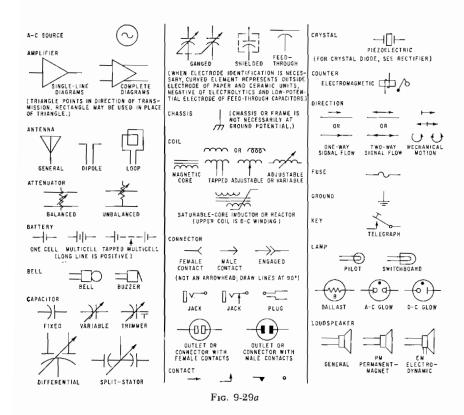


Fig. 9-28. The welding characteristics of some 250 combinations of metals.

STANDARD SYMBOLS FOR ELECTRONICS

The most-used schematic symbols for electronic components are collected here for convenient reference, as abstracted from the 54-page American Standards Association publication Y32.2-1954, "Graphical Symbols for Electrical Diagrams" and (for transistors) from MIL-STD-15A, "Military Standard Electrical and Electronic Symbols." (See Figs. 9-29a, 9-29b, and 9-29c.)

Symbols may have any orientation, size, and line weight. The open-circle terminal symbol can be added to leads if desired. Arrowheads can be either filled or open unless otherwise noted. Electrically actuated devices are normally shown in the power-off position. One-line symbolism has been adopted for waveguide diagrams, as indicated for microwave symbols.



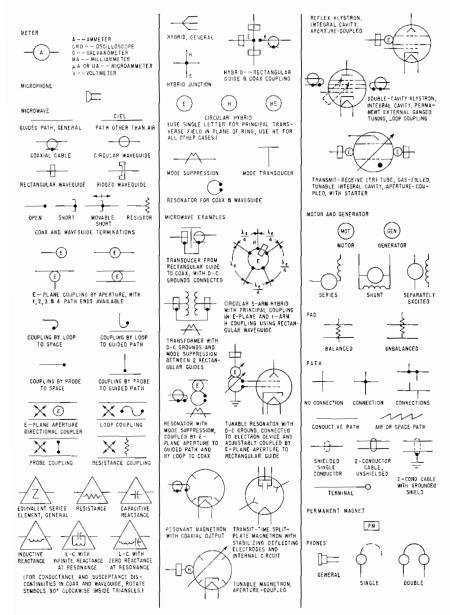


Fig. 9-29b

Charts and Graphs

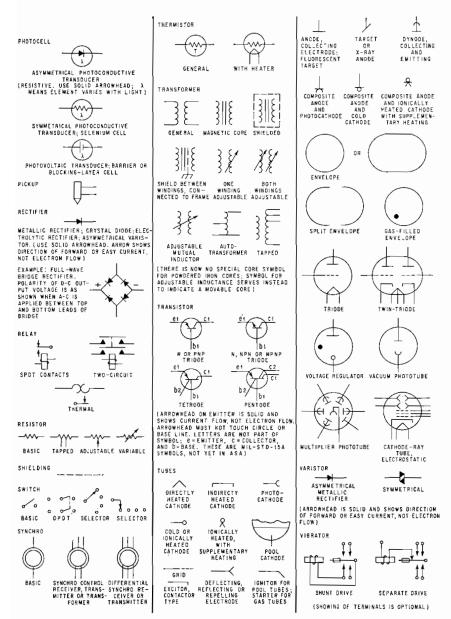


Fig. 9-29c

Table 9-17. Standard Telephone-cable Color Code

Pair No.	Color	Mate	Pair No.	Color	Mate
1	Blue	White	26	Blue White	Red
2	Orange	White	27	Blue Orange	Red
3	Green	White	28	Bluc Green	Red
4	Brown	White	29	Blue Brown	Red
5	Slate	White	30	Blue Slate	Red
6	Blue White	\mathbf{W} hite	31	Orange White	Red
7	Blue Orange	White	32	Orange Green	Red
8	Blue Green	White	33	Orange Brown	Red
9	Blue Brown	White	34	Orange Slate	Red
10	Blue Slate	\mathbf{W} hite	35	Green White	Red
11	Orange White	White	36	Green Brown	Red
12	Orange Green	White	37	Green Slate	Red
13	Orange Brown	White	38	Brown White	Red
14	Orange Slate	\mathbf{W} hite	39	Brown Slate	\mathbf{Red}
15	Green White	White	40	Slate White	Red
16	Green Brown	White	41	Blue	Black
17	Green Slate	White	42	Orange	Black
18	Brown White	White	43	Green	Black
19	Brown Slate	White	44	Brown	Black
20	Slate White	White	45	Slate	Black
21	Blue	Red	46	Blue White	Black
22	Orange	Red	47	Blue Orange	Black
23	Green	Red	48	Blue Green	Black
24	Brown	Red	49	Blue Brown	Black
25	Slate	Red	50	Blue Slate	Black

Note: The last pair in all cables is a red with white mate, viz.,

6-pair cable	6th pair	\mathbf{Red}	White
11-pair cable	11th pair	Red	White
16-pair cable	16th pair	Red	White
26-pair cable	26th pair	Red	White
51-pair cable	51st pair	Red	White

RESISTOR COLOR CODE

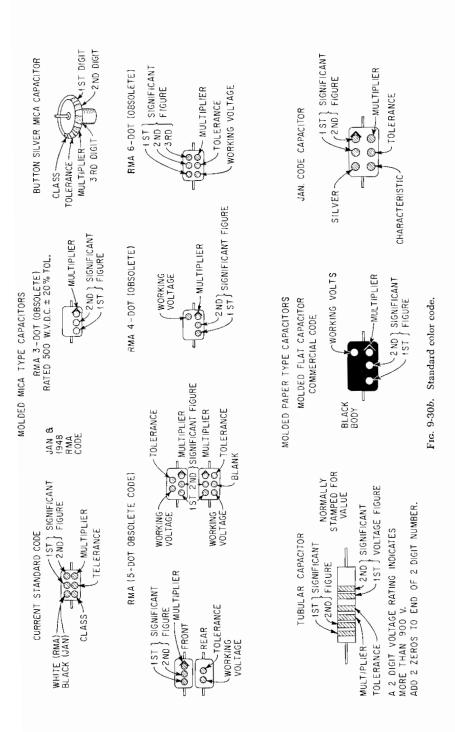
The chart shown in Fig. 9-30a indicates the appropriate significant figure of resistance and the multiplier. The fourth colored band, if any, indicates the tolerance. If none is shown, the tolerance is 20 per cent, with other tolerances as follows: gold, 5 per cent; silver, 10 per cent.

CAPACITOR COLOR CODE

The value of capacitors is similarly shown by colored bands or dots as indicated in Figs. 9-30a and 9-30b. Note that the bands and dots (for disc ceramics) apply for the ceramic-type capacitors, while the various dot systems are applicable to mica-and paper-type condensers. The various systems that have been used in recent years are included, even though some of them are obsolete. The tolerances are indicated by the appropriate colored dot, and the voltage rating is obtained by multiplying the value of the appropriate dot by 100.

RING OLOR PLIER	NONE 0 0 0,000 0,000 0,000,000 0,000,000	BY-PASS COUPLING CERAMIC CAPACITOR CAPACITY CAPACITY (OPT.)	LTOLERANCE LMULTIPLIER DISC CERAMIC RMA CODE	5-DOT 3-DOT WALTIPLIER TOLERANCE TEMP. COEFE
ORS AND CAPACITORS SECOND RING END COLOR SECOND FIGURE MULTIPLIER	NONE 1 2 3 4 4 6,000 5 7 00,000 7 00,000 8 00,000,000	AXIAL LEAD RESISTOR BROWN-INSULATED BLACK-NON-INSULATED MULTIPLIER TOLERANCE	WIRE WOUND RESISTORS HAVE IST DIGIT BAND DOUBLE WIDTH AXIAL LEAD CERAMIC CAPACITOR	TEMP. COEFF COEFF MULTIPLIER TOLERANCE resistors and capacitors.
STANDARD COLOR CODE — RESISTORS AND CAPACITORS FIRST RING BODY COLOR FIRST FIGURE SECOND FIGURE	O01m41091-80	RADIAL LEAD (BAND) RESISTOR MULTIPLIER MULTIPLIER	CTOLERANCE CIST FIGURE EXTENDED RANGE TC CERAMIC HICAP	CAPACITY CAPACITY CAPACITY CAPACITY CAPACITY CAPACITY CAPACITY CAPACITY Tro. 9-30a. Standard color code—resistors and capacitors.
INSULÁTED UNINSULATED COLOR	BLACK BROWN RED ORANGE YELLOW GREEN BLUE VIOLET GRAY	RADIAL LEAD DOT RESISTOR RAMULTIPLIER	CTOLERANCE CIST FIGURE 5-DOT RADIAL LEAD CERAMIC CAFACITOR	TEMP. CAPACITY TELECOSEFE. TOLERANCE CA

Frg. 9-30a. Standard color code-resistors and capacitors.



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