TALK

EDITORIAL office of ELECTRONICS in New York partially shown above includes eleven modular offices for editors at right, men working and not visible, with some overflow into the in-line arrangement at center. Through these doors pass the editors pictured last month

special Sears, Roebuck-size ones that have to be delivered by truck, yet.

"But now you blithely announce that you're going to begin publishing not one, but THREE of these sacred tomes monthly, and Sirs, that puts you 'way at the top of my hate list. Gee, there's a limit to what any woman should have to put up with. A few months of this and the kids and I will have to move out to the garage.

"Housewives, unite!"

▶ **SAVES FACE** . . . Mailing of the first issue of the ELECTRONICS Business Edition solved a problem for some of the editorial staff.

In planning the layout of the new edition, dummy copies were prepared consisting of headlines set in type, black boxes for photographs, and wiggly lines to represent text.

Quite often on the way home one of the editors would look up from studying his dummy copy to find his fellow commuters trying to figure out what a sane man could possibly find to study in articles with interesting headlines but with no printed text and black gobs instead of photographs.

With editions now out, an editor can face his friends once more without having them suspect mental degeneration.

▶ **STRANGE PLACES** . . . Twice in the past year we have seen a copy of ELECTRONICS play a minor role in television dramas presented over New York stations.

The first time, one of the leading characters seemed to be reading an issue, as part of the plot, but we didn't learn what his special interest was.

In the second instance, the issue was lying on top of a table in a harrassed businessman's home. The cover was upside down and caused us to engage in some physical and optical gymnastics in front of the set and family to identify the issue.

We assume that the prop men didn't bother to buy a newsstand magazine, just borrowed a copy of ELECTRONICS from a studio engineer.

Which reminds us that for the past two and a half years the NBC "Home" show has been subtitled "the electronic magazine for women."

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Subscriptions: Address correspondence to Electronics—Subscription Service, 330 W. 42nd St., New York 36, N. Y. Allow one month for change of address. Subscriptions are solicited only from persons engaged in theory, research, design, production, maintenance and use of electronic and industrial control components, parts and products. Position and company connection must be indicated on subscription orders.

Single copies 75¢ for Technical Edition and 50¢ for Business Edition in United States and possessions, and Canada; $1.50 and $1 for Latin America; $2.00 and $1.50 for all other foreign countries. Buyers' Guide $3.00. Subscription rates—United States and possessions, $6.00 a year; $9.00 for two years. Canada, $10.00 a year; $16.00 for two years. Other western hemisphere countries and the Philippines, $15.00 a year; $25 for two years. All other countries $20.00 a year; $30.00 for two years. Three-year rates accepted on renewals only, are double the one-year rate. Entered as second-class matter August 29, 1936, at the Post Office at Albany, N. Y., under act of Mar. 3, 1879. Printed in U.S.A.

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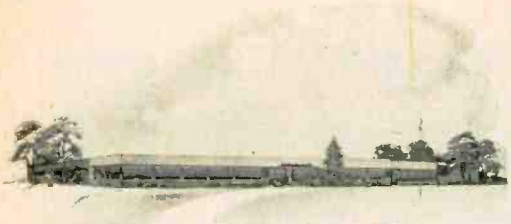

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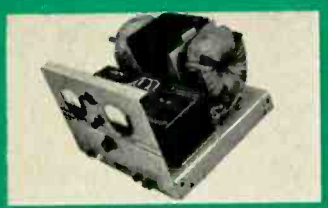

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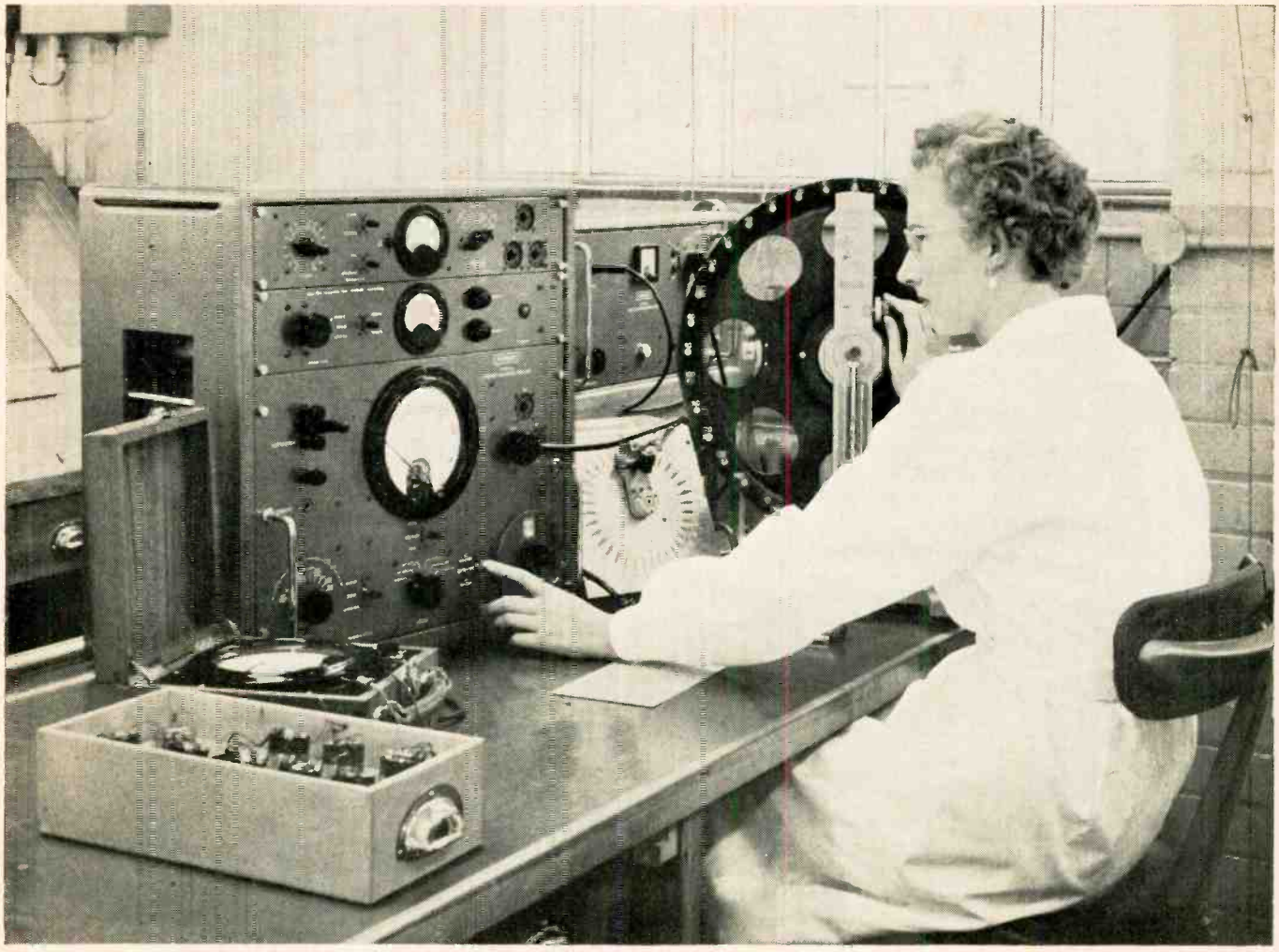

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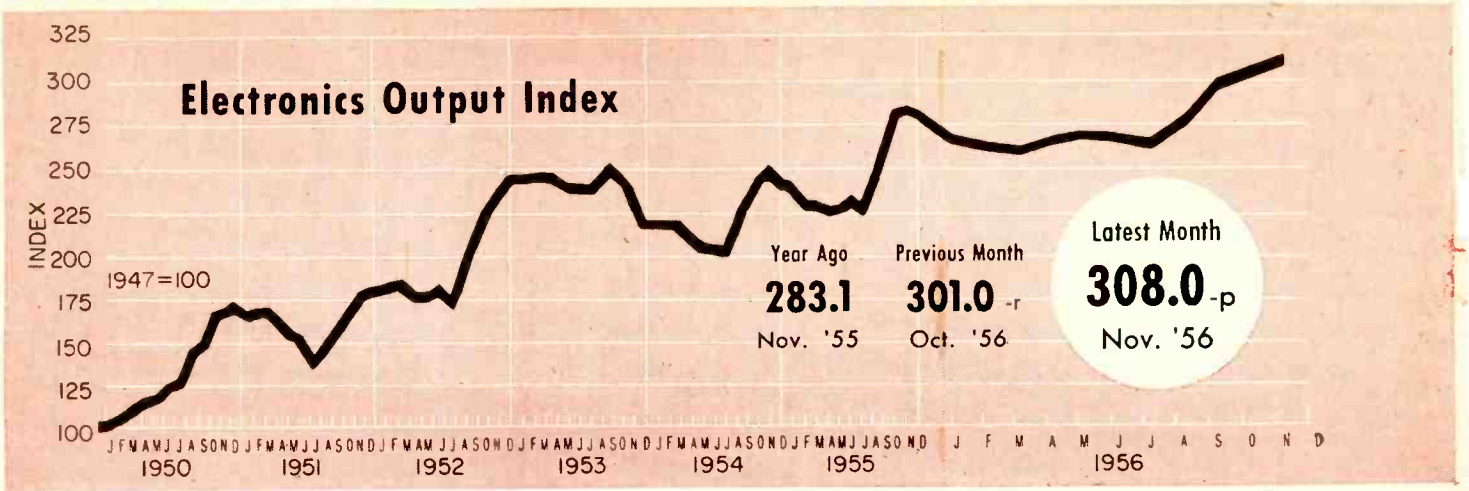


FIGURES OF THE MONTH

RECEIVER PRODUCTION

(Source: RETMA)	Latest Month	Previous Month	Year Ago
Television sets, total	Nov. '56	Oct. '56	Nov. '55
With UHF	679,993	820,781	631,654
Color sets	116,183	131,243	114,645
Radio sets, total	nr	nr	nr
With F-M	1,381,831	1,348,864	1,580,797
Auto sets	2,326	nr	44,357
	609,139	547,818	733,859

RECEIVER SALES

(Source: RETMA)	Nov. '56	Oct. '56	Nov. '55
Television sets, units	560,391	683,573	591,366
Radio sets (except auto)	689,409	585,666	865,602

RECEIVING TUBE SALES

(Source: RETMA)	Nov. '56	Oct. '56	Nov. '55
Receiv. tubes, total units	39,489,000	42,921,000	45,965,000
Receiv. tubes, value	$31,476,000	$34,362,000	$34,788,000
Picture tubes, total units	957,765	1,146,428	1,086,998
Picture tubes, value	$16,014,839	$19,786,764	$20,894,647

INDUSTRIAL TUBE SALES

(Source: NEMA)	Quarterly Figures: Latest Quarter	Previous Quarter	Year Ago
Vacuum	2nd '56	1st '56	2nd '55
Gas or vapor	$7,680,250	$8,754,054	$9,832,751
Magnetrons and velocity modulation tubes	$2,983,488	$3,394,059	$3,365,008
Gaps and T/R boxes	$16,254,025	$15,136,522	$13,193,395
	$1,238,469	$1,455,558	$1,677,574

MILITARY PROCUREMENT

(Source: Defense Dept.)	3rd '56	2nd '56	3rd '55
Army	$23,107,000	$44,882,000	$19,477,000
Navy	$22,273,000	$34,132,000	$20,054,000
Air Force	$84,952,000	$128,781,000	$128,023,000
Total—Electronics	$130,332,000	$207,795,000	$167,554,000

BROADCAST STATIONS

(Source: FCC)	Latest Month: Dec. '56	Previous Month: Nov. '56	Year Ago: Dec. '55
TV stations on air	511	511	482
TV stations CPs—not on air	120	117	108
TV stations—new requests	59	55	29
A-M stations on air	3,008	2,987	2,824
A-M stations CPs—not on air	117	121	111
A-M stations—new requests	291	288	229
F-M stations on air	530	528	540
F-M stations CPs—not on air	24	22	17
F-M stations—new requests	5	7	3

COMMUNICATION AUTHORIZATIONS

(Source: FCC)	Nov. '56	Oct. '56	Nov. '55
Aeronautical	53,192	51,826	43,939
Marine	60,153	59,073	53,622
Police, fire, etc.	21,829	21,539	19,637
Industrial	32,788	32,434	27,427
Land transportation	9,287	9,227	8,381
Amateur	154,839	154,311	142,408
Citizens radio	22,036	21,356	14,147
Disaster	330	330	319
Experimental	775	744	666
Common carrier	2,559	2,358	2,056

EMPLOYMENT AND PAYROLLS

(Source: Bur. Labor Statistics)	Oct. '56	Sept. '56	Oct. '55
Prod. workers, comm. equip.	419,500-p	403,100	408,600
Av. wkly. earnings, comm.	$78.12-p	$77.33-r	$75.12
Av. wkly. earnings, radio	$76.07-p	$74.74-r	$71.40
Av. wkly. hours, comm.	40.9 -p	40.7	41.5
Av. wkly. hours, radio	40.9 -p	40.4-r	40.8

SEMICONDUCTOR SALES ESTIMATES

	Oct. '56	Sept. '56	Aug. '56*
Transistors, Units	1,290,000	1,155,000	1,315,000

STOCK PRICE AVERAGES

(Source: Standard and Poor's)	Dec. '56	Nov. '56	Dec. '55
Radio-tv & electronics	345.2	353.9	451.5
Radio broadcasters	454.1	446.9	519.1

p—provisional r—revised nr—not reported
*1955 not available

FIGURES OF THE YEAR

TOTALS FOR FIRST ELEVEN MONTHS			1955
1956	1955	Percent Change	Total
6,730,045	7,151,895	— 5.8	7,756,521
12,266,591	13,108,365	— 6.4	14,894,695
5,847,563	6,487,617	— 9.9	7,421,084
6,680,127	5,532,583	+20.7	6,921,384
429,846,000	441,753,000	— 2.7	479,802,000
10,191,545	9,992,769	+ 2.0	10,874,234

Television set production
Radio set production
Television set sales
Radio set sales (except auto)
Receiving tube sales
Cathode-ray tube sales

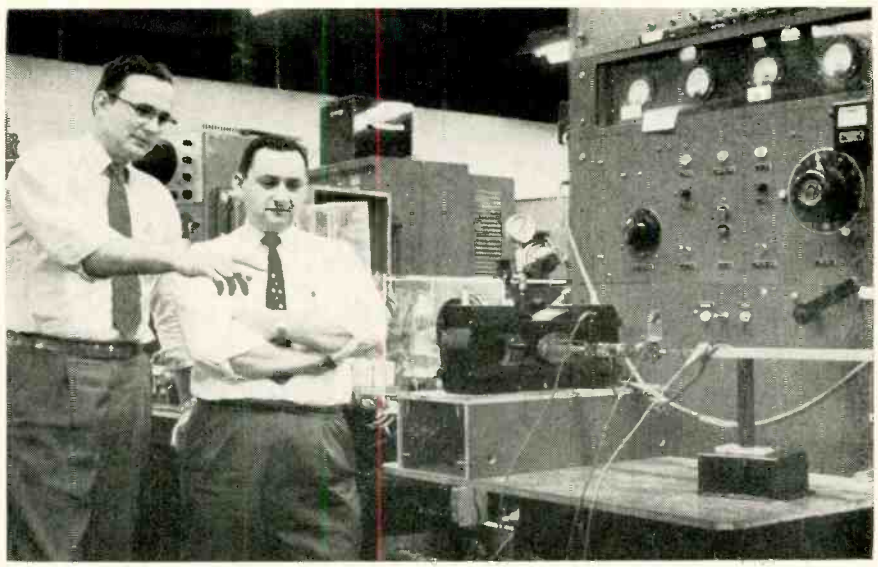
Sonar Sales Register Five-Fold Growth

Increasing military and commercial sales lift volume beyond $35 million

UNDERWATER electronics in the form of all types of sonar equipment has grown into a sizable business for marine equipment manufacturers. Sales hit a volume of nearly $35 million in 1954, according to the Census Bureau, and probably exceed $40 million now if the past growth trend has held its course. Since 1947, when volume was estimated at less than $7.5 million, sonar sales have increased five-fold.

► **Market**—It has been estimated that the military market for sonar accounts for 90 percent of the total business with the commercial and pleasure boat field taking the remaining 10 percent. Today, many of the nation's 450,000 commercial fishing boats have the equipment. Not only has it helped to spot obstructions but has also saved expensive nets from being ripped and ruined. Sonar has also helped to improve the catch. It enables the fisherman to know at what depth to keep his nets. For the commercial fishing and pleasure boat field, an annual sonar business volume of $2.5 million has been estimated. The remainder of the business goes to the larger commercial ships with 30 to 40 sales a year and to the military.

► **Makers**—According to the Census Bureau there are between 20 and 30 manufacturers of sonar.



ENGINEERS at Sylvania test out a magnetron as new contracts . . .

Spur Microwave Tube Output

Contracts for magnetrons and klystrons boost plant expansion and sales volume

INCREASING activity in the $ multimillion microwave tube field has been marked by new business and defense contracts and sizable plant expansion plans by firms in the field.

► **Business**—Sylvania will start development and production operations under a $1.4-million defense contract for four types of magnetrons in the next few months. Raytheon was awarded a $1.4-million magnetron contract and Westinghouse also began production on the tubes. GE announced that its line of voltage-tunable magnetrons will be in volume production this year.

In the klystron field, Sperry announced plans to double production at its Florida plant. Varian Associates has built and installed $500,000 worth of tube processing equipment to go into production on a $4-million order for their V-87 million-watt pulsed klystron.

► **Expansion**—Increasing business, both military and civilian, has forced the microwave tube maker to expand plant and facilities. Sylvania's microwave tube lab in Mountain View, Calif., plans to add 18,000 sq ft of space for its engineering research and development work. Varian, which began operations in a 1,200 sq ft plant, is completing a 126,000 ft vacuum-tube factory in Stanford Industrial Park. The new tube plant is designed to be enlarged to 252,000 sq ft if necessary.

GE announced that facilities at

the firm's microwave lab at Stanford University are being increased to provide more efficient and higher power microwave developments particularly for defense systems.

► **Klystrons**—Sperry, in planning to double production, will expand its 18-month old Gainesville, Florida plant. The addition to be completed by next summer will produce multi-million watt klystrons for high-power missile guidance systems.

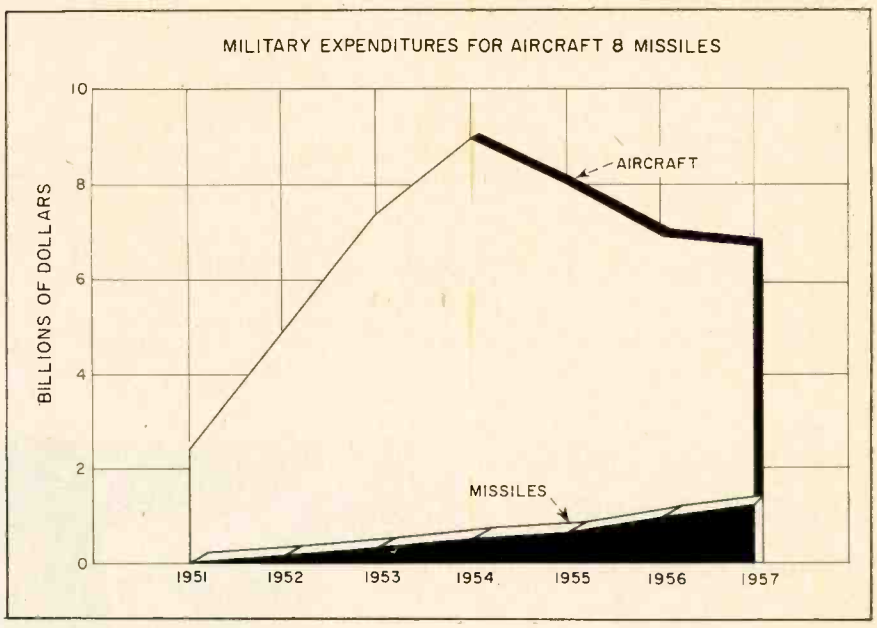
The expanded plant is expected to employ 600 and will contain over $3.5 million of scientific instruments, automated devices and special machine equipment. Production lines of the division are currently producing 17 types of microwave tubes for industry and the military.

► **Future**—Varian expects that microwave tube sales, which account for about 55 percent of its total dollar volume, will increase by as much as 100 percent over the next five years. GE, which lumps magnetrons and klystrons in with other power tubes, sees a 10 percent increase in the power tube market in 1957 and a 100 percent increase during the next ten years.

Census figures show that the magnetron field alone has had a ten-fold sales increase since 1947.

One Radar Coupler —Well Done

Chassis that connects a firecontrol system to the automatic pilot control system, to automatically zero an airplane in on its target, goes into an oven for tests at Westinghouse. It's designed for operation at 400 F



Aircraft Electronics Levels Off

Planes still account for the king-sized share of airborne business despite missile growth

ALTHOUGH military expenditures for guided missiles have risen at a rapid rate, the missile electronics business has a long way to go before it becomes the market that aircraft represents.

► **Comparison**—Right now defense expenditures for manned aircraft are about six times greater than those for missiles, as shown in the chart. Although production of military airplanes has been tapering off since 1953, according to Aircraft Industries Association of America, funds for procurement have held relatively steady due to the heavier and more expensive craft. Some 7,000 military planes were produced in 1956. In 1955 the total was about 8,000 units. A further tapering off is expected this year.

Despite the decline in plane unit production, military aircraft takes about 85 percent of Defense department procurement expenditures for aircraft and guided missiles. The AIA predicts that beginning in fiscal 1958 military orders will probably be in a ratio of 65 percent to 35 percent in favor of manned aircraft and that it will be 1961 before the ratio evens out at 50-50.

► **Electronics** — The modern jet bomber uses more than 1,000 vacuum tubes that range in cost from 56 cents to $681 each while a missile may require no more than eight tubes.

Some modern fighter planes use more electron tubes or transistors than 80 home radios. The Sidewinder missile, on the other hand, uses no more tubes than one average home radio and is said to be no more complex.

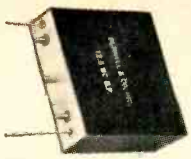
Paper Types Lead Capacitor Sales

Shipments have tripled in ten years and now account for 43 percent of sales

CAPACITOR manufacturing has grown into a kingsize business in the past ten years. This is revealed in the latest census report that shows volume grew from $50 million in 1947 to $158 million in 1954.

► **Breakdown** — Paper capacitors account for 43 percent of the industry's dollar volume. They rank next to ceramic capacitors in unit volume with some 443 million produced in 1954 compared to 227 mil-

(Continued on page 14)



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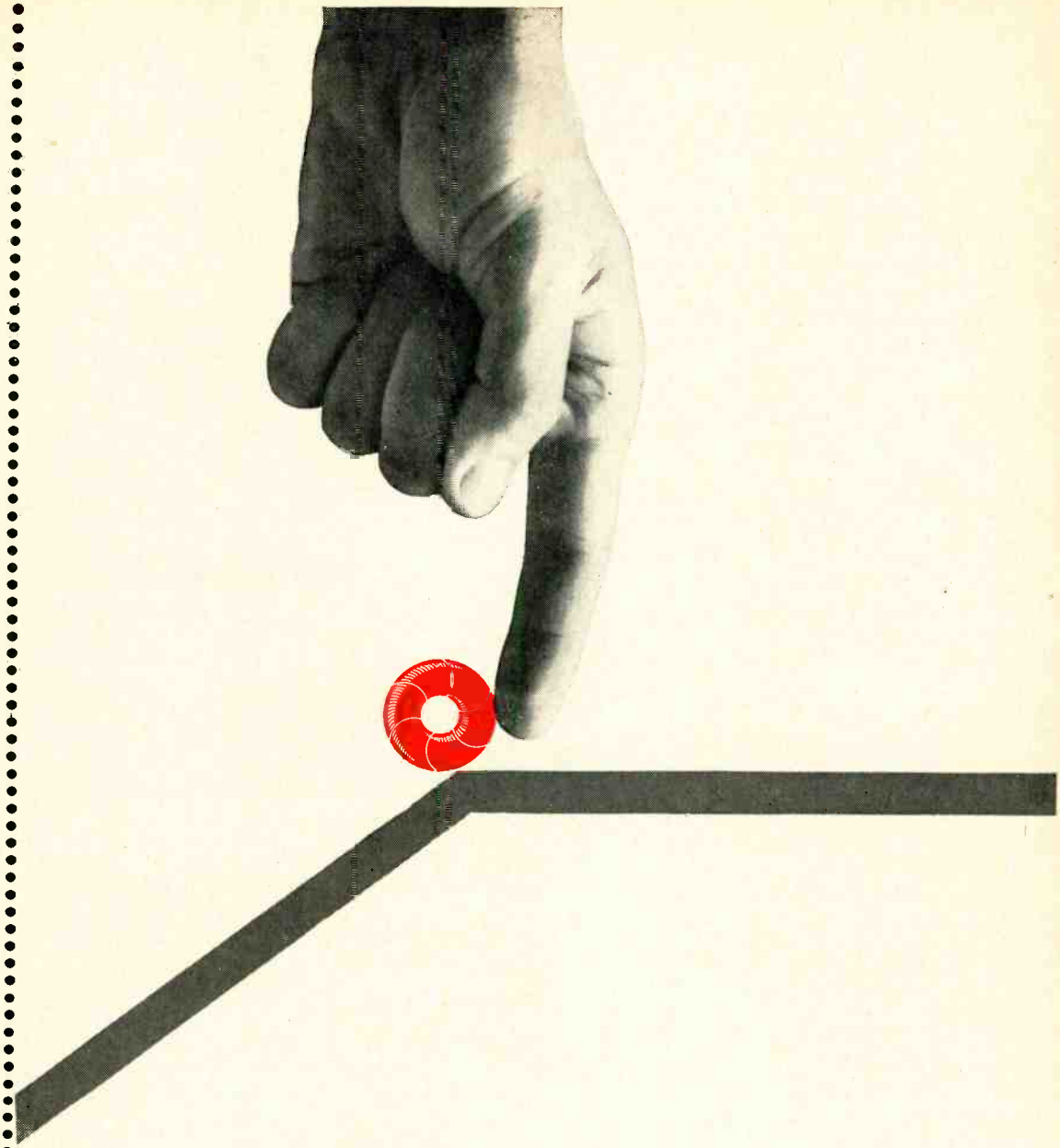

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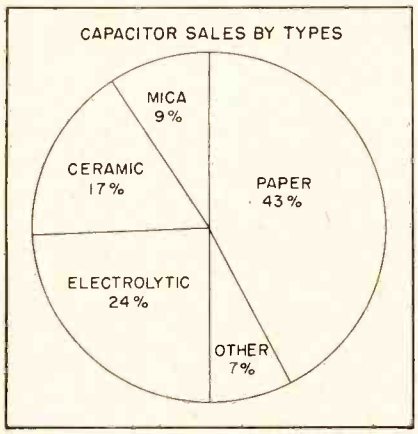
lion in 1947. Electrolytics, with 75 million produced in 1954, ranked second in sales and accounted for 24 percent of total dollar volume. Ceramic capacitors led in units with 560 million but accounted for only 17 percent of total dollar shipments volume. Mica capacitors with shipments of 105 million units and other types with unit shipments of 79 million followed. In 1947 mica capacitors led ceramic types in dollar shipments but even then were behind in unit volume.

► **Companies** — Today there are probably over 90 companies producing capacitors for the electronics industry, according to figures from the Electronic Production Resources Agency. EPRA estimates that about 25 of the companies produce the bulk of U. S. output. The number of companies in the field has grown with its volume. In 1952 there were about 60 companies manufacturing the components.

► **Need** — The electronics division of the Business and Defense Services Administration with the EPRA recently reviewed with 14 capacitor makers the ability of the capacitor industry to meet mobilization requirements. Deficiencies due to shortages of tantalum and other materials were found. As a result the government is to be asked to look into the tantalum situation. Capacitor manufacturers also expressed concern over their supplier's capacity to come up with needed quantities of sub-components in case of emergency, such as pressure seals, small metal cases, capacitor grade paper and very thin aluminum foil. More than 60 categories of capacitors were studied in the review.



On the whole, however, the meetings indicated that U. S. capacitor manufacturers have sufficient capacity to produce most types in the quantities needed to meet an emergency. Manufacturers indicated, however, that the exacting specifications for missile capacitors will substantially reduce the industry's ability to meet emergency needs.

FURNACE at Hughes Aircraft converts coarse nuggets into silicon ingots as . . .

Silicon Output Increases

New company enters field. Consumption grows and production increases as prices drop

WITH demand for pure silicon growing fast, there are only a handful of commercial sources for the material in the United States, although a score of companies produce it experimentally or for their own use.

Latest company to enter the supply field is Flight Research of Richmond, Va. which recently established a division for the manufacture of single-crystal silicon. The firm's plans include growing silicon crystals to specification for rectifier and transistor manufacturers. The company is now in production and has 50 gram boules available. They measure 2.5 inches high and 1.5 inches in diameter.

► **Source**—Sylvania has stepped up its silicon production. It has been operating a production unit since last year that is yielding commercial quantities of pure silicon on a regular basis. Through plant expansion, production quantities are being increased. The firm's tungsten and chemical division is being expanded by 48,000 sq. ft.

► **Price**—As silicon production has increased, prices have dropped. DuPont recently dropped prices on pure silicon for a third time, reducing them from $350 to $320 a pound. Solar-cell-grade silicon was cut from $180 to $150 a pound. Sylvania presently offers transistor grade silicon at $704 a killogram and solar grade at $330.

► **Market**—Texas Instruments has announced quantity price reductions up to 10 percent on production-type silicon transistors and rectifiers.

There are some 19 types of silicon transistors available from the company.

Hughes Aircraft, which estimates that it does 20 percent of the total semiconductor business, says that its silicon sales are to a point where they now approach in dollar volume the sales of its germanium products. This could place its present silicon sales at $4 to $6 million. The company has indicated that technical problems in developing

(Continued on page 12)

new method solves **DIFFICULT R-F NOISE** *problem*

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Faced with a new version of the same old r-f interference vs. space-weight problem, he came upon a solution that sidestepped the usual time, trouble, and expense . . . by calling on Sprague.

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see SPRAGUE® for filters

Top engineers of Hoffman Electronics look over firm's new silicon solar cell portable radio

advanced silicon diodes and transistors are rapidly being overcome.

► **Solar Cell** — Use of solar-cell-grade silicon is also increasing. At least two companies now have solar portable radios on the market. Hoffman Electronics introduced a transistorized model last month that has the silicon solar battery pack encased in the carrying handle. The cells are produced by the company's semiconductor division in Evanston, Ill.

Manufacturers Forecast Business For 1957

Firms see overall good year ahead but with specialized problems for some segments

YEAR-END reviews by associations and major manufacturers in the electronics field also contain some crystal gazing on what 1957 may hold in store for the industry. Here is a rundown of some of the forecasts:

► **RETMA** — President W. R. G. Baker predicts that 1957 will bring an added 10-percent growth to the electronics industry. He sees sales of closed-circuit tv exceeding $6 million in 1957 and the percentage of defense spending for electronics increasing by 100 percent in the next 10 years. Hi-fi is expected to remain in good demand and transistor output for 1957 is estimated at 22 million units.

► **NICB** — Economists at a forum held by the National Industrial Conference Board gave an overall view of what businessmen, electronic and otherwise, might expect this year. Consensus of the forum is that 1957 will be a record year for total business but only moderately above the record set in 1956. Rising national output and rising prices during the first-half of 1957, and a tapering off or plateau in business growth during the following six months was forseen by 14 economists at the forum.

► **Admiral** — President Ross D. Siragusa made the forecast that tv output for the industry this year might reach 9-million units with nearly half in 10, 14 and 17-inch portable models. Color sales are estimated at nearly 500,000 units for the year and radio may increase 5 percent.

► **GE**—President Ralph J. Cordiner predicted that shipments of the electrical manufacturing industry, which includes electronics, will rise 4 to 5 percent to a record $21 billion. The company is sticking to its plans for a $500-million capital expenditure in the 1956-58 period despite a cutback in three planned

(Continued on page 14)

Business Briefs

► **Sale** of $8 million in debentures this year is planned by Daystrom. Proceeds will be added to general funds and used, among other things, for plant additions and working capital

► **Sharp** rise in tv and hi-fi sales will boost Magnavox sales to nearly $50 million for the first six months of its fiscal year compared to $34 million during the period last year. Annual sales will approach $95 million this year compared to $70 million in fiscal 1955. A $6-million loan from two insurance companies will be used to retire a $2.8-million loan and bring working capital to approximately $19 million

► **Parent** company to 13 major divisions including several in electronics, Thompson Products, anticipates total sales for 1956 in the range of $300 million. It sees sales in 1957 exceeding by a substantial margin the previous record of $326 million set in 1953. Its sales currently run at annual rate in excess of $350 million

► **Business** developed more favorably than expected during 1956, according to Philips. Sales for the Netherlands electronics manufacturer totaled $466.5 million in the first 9 months of 1956 compared to $399.8 million for the period in 1955, a 16.7-percent increase. The company now employes 150,000 workers compared to 137,000 a year ago

► **Year-old** Pacific Automation Products had gross sales of $1.1 million for the first 11 months of 1956. It currently serves 150 accounts

► **Producer** of patented cable and panel equipment and triaxial connectors, Mutual Electronic Industries, was acquired by Sightmaster Corp., manufacturer of fuses and hi-fi equipment

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plant expansions. It was predicted that within the next ten years GE will go substantially all the way electronically with many of the jobs now done electrically taken over by electronics.

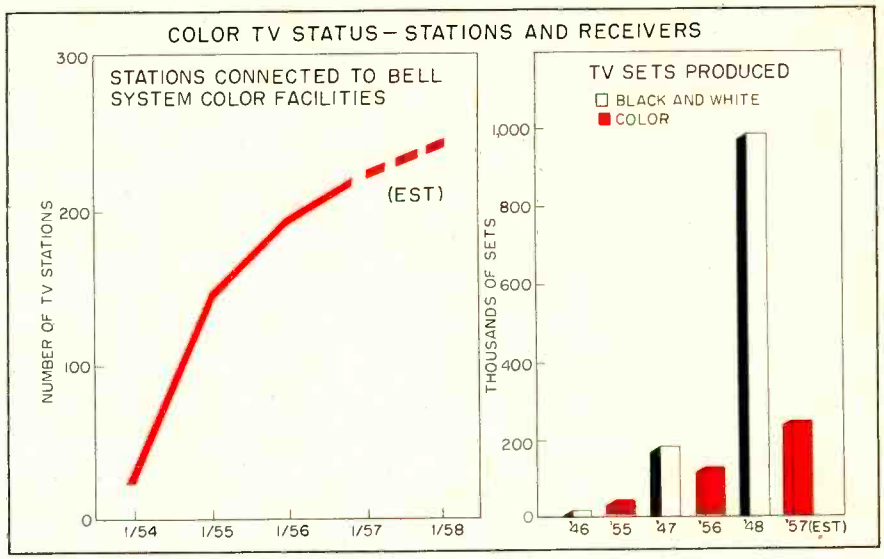
▶**Motorola**—President Robert W. Galvin saw industry tv sales possibly reduced to the area of 6.8 million in 1957 with portables accounting for 2.5 million of the total. Color tv sales were expected to exceed 300,000 and consumer radio were seen rising by five to ten percent in the first half of the year. For the first half of 1957, Galvin predicted an industry increase of 20 percent in hi-fi record player sales. In the first half of 1956, over 920,000 units were sold, according to the company.

▶**Philco** — President James M. Skinner sees production and sales of tv sets leveling off at about 7 million in 1957. He said that the largest gains in 1957 will be made in the fields of military and industrial electronics with a gain of 10 percent over a 1956 volume of almost $3 billion.

Hot Air Powers Thermopile Radio

Metal tube and thermopile, mounted on glass chimney of paraffin lamp, utilizes wasted heat to operate transistorized radio. (ELECTRONICS, p 196, May, 1946) Receiver, developed by The Philips Industries, uses 7 transistors

Color Television Shows Progress



Although its growth did not meet expectations in 1956, it moved ahead significantly

DESPITE the fact that color television did not turn out to be the whiz kid of the electronics industry during 1956, it nevertheless made substantial progress both in number of color tv stations and in color set production.

▶**Service**—Number of tv stations that have color tv service available over Bell System routes increased from 190 at the beginning of 1956 to 219 at the beginning of 1957, an increase of 29 stations. This is a smaller increase than took place during 1955 when 51 stations were added for color network service and 1954 when 118 stations had network color service available. However, over half of the 428 tv stations in the U. S. are now on color network routes.

▶**Networks**—American Broadcasting does not as yet have any of its stations or studios equipped for color but has funds set aside so that it can convert to color at any time. It's new facilities being built in Chicago, New York and Hollywood will be able to handle color equipment. AB-PT has obtained a $60-million loan to finance further growth of the network.

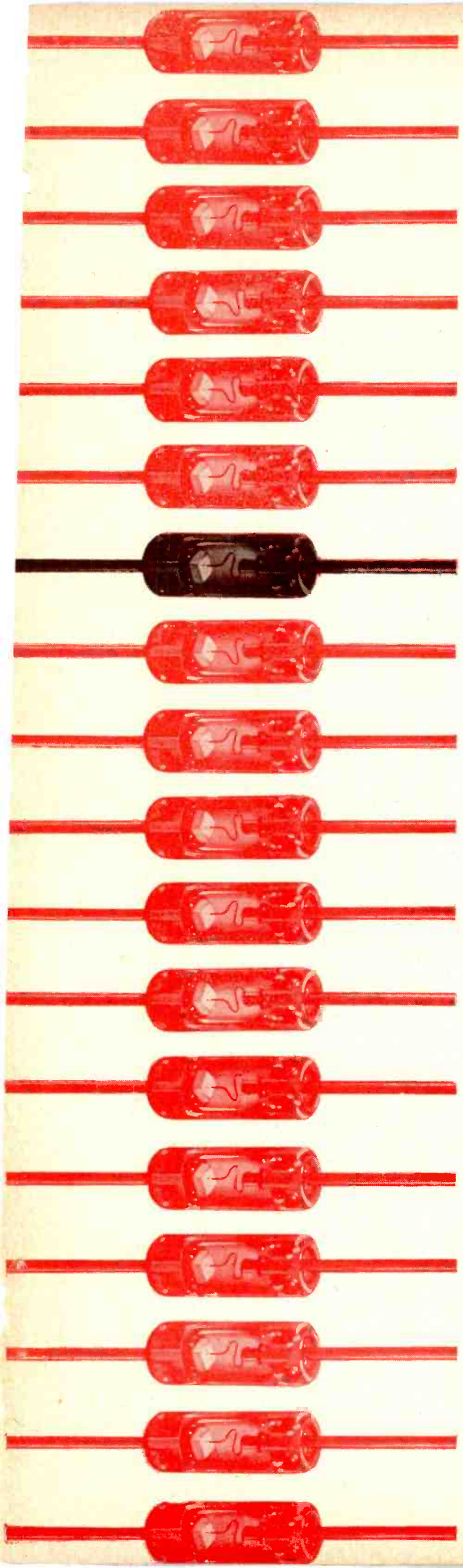
Total of 146 of CBS's 216 tv affiliates are equipped for network color. Of these 22 have color slide and film equipment and another 11 have color studio equipment including color cameras as well as slide and film equipment.

This represents a substantial increase for the network. A year ago 110 of its affiliates were equipped for network color including six with color studio, film and slide gear.

At the end of 1956, 132 of NBC's 201 affiliated tv stations were able to rebroadcast network color shows. Forty-nine of the stations were equipped for some form of local color broadcasting and 21 had color cameras for live programs. A year ago 106 of the network's stations were set for network color, 32 had slide and film equipment and 11 could originate live color shows.

▶**Sets**—The chart shows the relative rate of growth of color tv set production compared to black-and-white during its beginning years. It shows that although color is not growing as fast as black and white, production of the sets has more than tripled in the past three years. This year with production of some 300,000 color sets forecast, color tv will fall further behind the growth rate of black and white sets but will still represent plus business.

(Continued on page 16)



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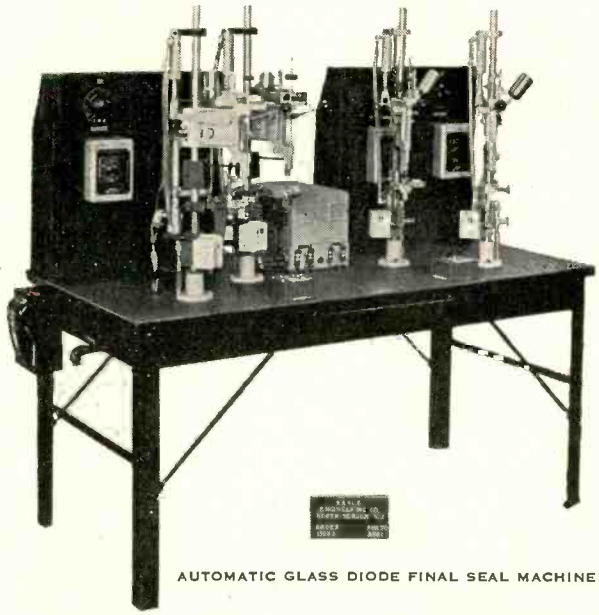

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CONT

SUBMICROSCOPIC iron particles are collected from a pool of liquid metal with a conventional magnet (left). These are later pressed to form a superpower magnet that can be drilled and tapped as . . .

Magnets Make New Advances

Continuing magnet research brings new developments that will open broad markets

SIGNIFICANT advances in magnets were made by government and industry researchers last year. Purified magnese-bismuth was developed by Westinghouse for the Air Research and Development Command to yield permanent magnets with high resistance to demagnetization. At Naval Ordnance Laboratory, flakenol was developed as a magnetic core material for electronic filter and communications systems.

As 1957 gets underway, further advances show promise. General Electric has announced an experimental magnet made from invisible iron "dust" that is equal to the strongest commercial magnets now available and which the company believes can be made ten times stronger.

▶ **How**—Fine single-domain iron particles several times longer than their cross-section are being successfully produced at the Lynn labs. The long particles resist demagnetization as well as such high-coercivity materials as the ferrites and Alnicos.

The elongated particles are dispersed in a binder, which can be glass, plastic, rubber or another metal. The dispersion is aligned in the binder by a strong magnetic field. Once made, such a magnet must be placed in an opposite field strong enough to reverse its polarity before it can be demagnetized.

The magnets can be machined drilled, tapped and molded into any desired shape.

▶ **Uses**—The new magnet will allow smaller, lighter more accurate and more rugged instruments to be made. They are expected to make possible the application of magnets in nuclear reactors, something now limited because of the potential radioactivity of the cobalt in alnico.

The already important permanent magnet market today consumes about 150-million magnets annually. The electronics industry alone accounts for more than 50 percent of this amount.

▶ **Future**—Research will continue at a high rate. GE, for example, is keeping more than 20 scientists at its research laboratory working on the basic physics of magnets and metallurgical development of magnetic material.

Westinghouse has developed a technique for taking pictures of the atomic insides of magnetic materials. Using it, neutron diffraction is made visible to photographic film. Heretofore neutrons were invisible to film. The new technique will expedite the analysis of crystals of magnetic materials which cannot be done with x-rays.

College Recruiters Get Set For 1957 Market

More colleges will be contacted and company representatives will offer engineers more money

ELECTRONIC manufacturers are once again getting set for annual engineer recruitment drives at the nation's colleges. A recent survey of the policy and practice of 200 companies in the employment of college and university graduates, by Northwestern University, gives some indication of what's ahead in recruiting.

Trends in almost all aspects of engineer recruiting are up. In 1957, more companies will visit more campuses to hire more engineers at more money than last year.

▶ **Contacts** — Companies reporting in the survey almost without exception send representatives to various campuses. The firms include 145 with recruiters who visit 10 or more campuses. These companies used a total of 923 recruiters. In all, 8,989 campus contacts were made last year, an average of 45 schools per company.

This year, plans are to contact an average of 52 schools per company. Only 25 firms will contact less than 10 schools while 34 will contact more than 100 colleges and universities. One company will contact over 300 colleges and universities in 1957.

▶ **Number**—According to the survey, in 1957 some 63 companies will hire approximately 1,627 electrical engineers or an average of 26 men per company. Last year 51 companies hired 862 men for an average of 17 men per company.

In physics, 27 firms hired 186 men last year while this year 33 firms expect to recruit 269 men. For total engineering, chemistry and physics graduates, employment demand from the companies surveyed will be up 35 percent this year over last.

▶ **Salaries** — Starting salaries in 1957 for college engineering grad-

(Continued on page 20)

How to Make Manual Instruments Automatic

PHOTO COURTESY PHILCO CORPORATION

SWEEP DRIVE operates the G-R Type 1304-B Beat-Frequency Oscillator at the Philco Corporation. This setup is designed to check frequency response of encapsulated R.C. printed networks. The limit curves penciled on the scope faces permit various characteristics of each printed circuit to be checked rapidly and in a form that is easily interpreted by unskilled personnel.

Philco engineers specified this mechanical sweeping technique because the response at the low end of the audio spectrum of certain networks under test was of prime importance. The poor frequency distribution of electronic audio sweeps ruled this type of equipment out for this application.

G-R Type 1750-A Sweep Drive . . . $460

The G-R Sweep Drive attaches to knobs, dials and shafts for the automatic sweeping of a wide variety of equipment. This Drive can be used to turn shafts automatically for many purposes . . . to sweep a receiver or analyzer to obtain panoramic response . . . to open or close a switch or shutter . . . to modulate light, heat, or sound . . . and, most important, to convert manually-operated signal sources to sweep devices.

Many mechanical or electronic integral sweep oscillators are available, but here is a new concept — a drive that can be attached to any oscillator or signal generator to fit it for a specific measuring job. Oscillators can be taken off the shelf for conversion to sweep devices as the need arises. There is a choice of as many sweep generators as there are hand-operated oscillators available.

Speed Range: adjustable 0.5 — 5 cps, reciprocating motion

Sweep Arc: adjustable 30° — 300°

Sweep Arc Center-Position: on reduction drives, may be set to any point within eight full turns.

Coupling System: four spider-like arms attach to knobs and dials 1" to 4" in diameter and to ¼" and ⅜" shafts.

Limit Switch Circuit: disconnects and brakes the motor if preset limits of shaft travel are accidentally exceeded.

CRO Deflection Circuit: voltage proportional to shaft angle is provided for application to oscilloscope horizontal deflection plates.

Blanking Circuit: eliminates the return CRO trace and produces a reference base line.

Rated Maximum Torque: 24 oz.-in.

Used in combination with G-R's popular line of Unit Oscillators, the Sweep Drive makes available sweep generators for the frequency ranges: 500 kc-to-50 Mc, 50 Mc-to-250 Mc, 65 Mc-to-500 Mc, 250 Mc-to-920 Mc, and 900 Mc-to-2000 Mc. The Drive can be coupled to either the oscillator's slow-motion drive for sweeping over small ranges or coupled directly to the main shaft to take advantage of the extremely wide frequency ranges offered by G-R Unit Oscillators.

The Type 1263-A Regulating Power Supply has been especially designed to hold oscillator output constant for sweep-type presentation. Regulation is held to within ±2% of the preset output level, independent of frequency.

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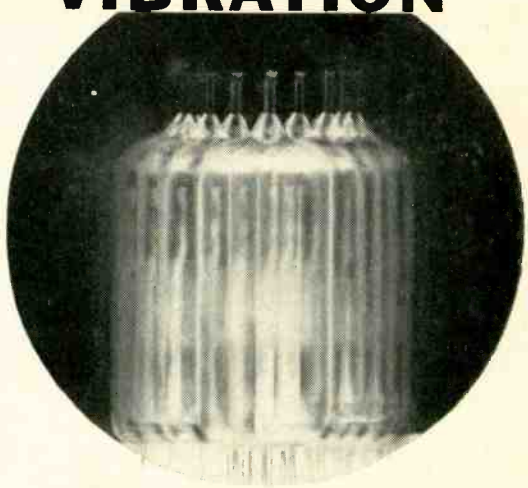

Conventional rectifiers are destroyed by this same vibration test in less than five hours.

The NEW RAYTHEON CK6763 Cold Cathode Medium Voltage Rectifier

(a ruggedized version of the popular CK5517)

The improved structure of this Raytheon CK6763 makes it almost impervious to fatigue from high level vibration.

What's more it requires *no heater power* • *no warm-up time* • and it permits a wider ambient temperature range.

Some of the characteristics of this and other Raytheon Cold Cathode Rectifiers are shown in the chart.

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Type	Max. Dimensions Inches		Max. Peak Inverse Voltage	Max. Peak Plate Current Per Plate	Max. DC Output Current
	Height	Diam.			
*CK5517	2.25	0.75	2800	100 ma.	12 ma.
CK6174	2.25	0.75	2800	30 ma.	3 ma.
CK6436	1.82	0.40	1500	10 ma.	100 μa.
CK6659	2.13	0.40	2800	40 ma.	8 ma.
CK6763	2.25	0.75	2800	100 ma.	12 ma.

*MIL Specification

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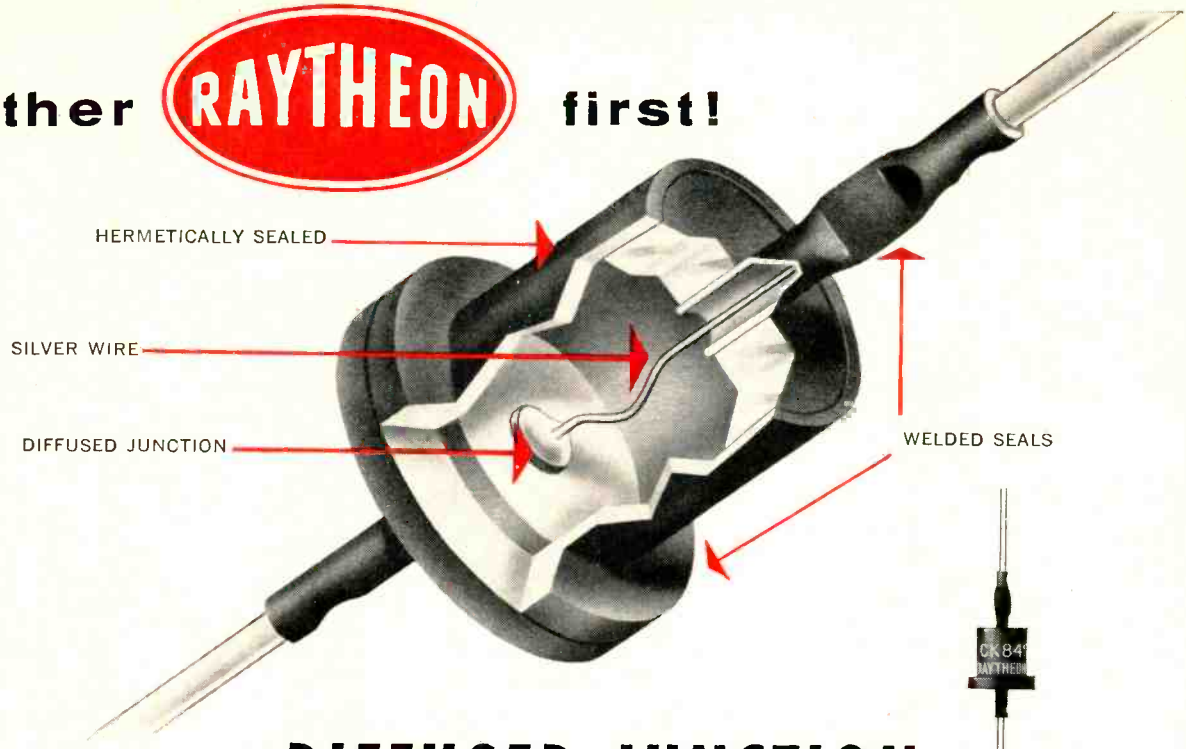

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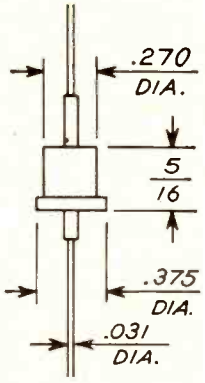

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2. Precise junction gradient for specific rectifier applications.
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CK840(1N537)	100	500	250	1 0	0.002
CK841(1N538)	200	500	250	1 0	0.002
CK842(1N539)	300	500	250	1 0	0.002
CK843(1N540)	400	500	250	1.0	0.002
CK844	500	500	250	1.0	0.002
CK845	600	500	250	1 0	0.002

*PIV ratings apply from −65°C to +165°C

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uates, as reported by 144 of the companies, indicate that they will average $433 per month compared to $415 last year. Seventy-seven of the firms, the largest single group, will pay between $426 and $450.

Total of 139 of the companies hiring engineers reported a salary spread of $56, the gap between $405 and $461, the bottom and top average starting salaries.

▶ **Raise**—Of the companies hiring engineers last year, 81 raised rates after the interviewing season began and 62 did not raise rates. Of those who raised rates, 10 met their needs and 71 did not. For the 62 firms that did not raise rates, 20 met their needs and 42 did not. It is considered likely that companies will again raise rates after recruiting has started this year.

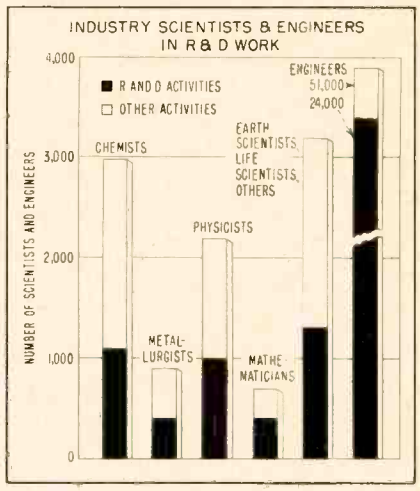
▶ **Time**—The survey also shows earnings of engineers from previous graduating classes. Engineers with 3 years of experience earn an average of $527 per month; 5 years, $592 per month; 7 years, $650 per month and 10 years, $740 per month.

▶ **Factors**—Recruiters listed what they considered to be the most important factors limiting a companies effectiveness in recruiting. The five most important factors, according to the survey were: The number of college graduates available is too small; College professors need a better understanding of our type of business; The quality of many applicants is below our standard; Company not well known on college campuses; Too many graduates have not decided what to do.

Video Tape Goes To Work

Every weekday evening since Nov. 10, 1956, CBS has been recording in Hollywood, Calif. a 15-minute news program which originates in New York, and playing it back later the same evening to west coast affiliates. In addition, one half-hour show and a one-hour program have been regularly taped since the beginning of the year for the same purpose. The video tape recorder shown is one of two units delivered last spring to CBS by Ampex Corp. Since mid-January, NBC has been recording a half-hour daily program on video tape for West Coast playback

R & D Take Half of Industry's Engineers



Increasing importance of research and development boosts costs and manpower needs

RESEARCH and development in the electronics industry is big in both dollars and manpower. Today, annual research costs approach $1 billion and nearly 50 percent of the scientists and engineers in the industry are engaged in research and development work. Figures are from the final report of the National Science Foundation study of science and engineering in American industry.

▶ **Cost**—Estimated cost of research and development in the electronics, electrical industry in 1953 was $743.3 million and rose to $823.0 million in 1954, a 10.7 percent increase. The industry accounts for 20.3 percent of total r&d costs for U. S. industry. Only the aircraft industry accounts for more, 20.7 percent.

▶ **Personnel**—Of the 61,000 engineers and scientists working in the electronics-electrical field, 28,800 are in research and development work. Here is r&d's take in manpower from the industry's various individual occupational groups: engineers, 24,600 out of 51,000; chemists, 1,100 out of 3,000; metallurgists, 400 out of 900; physicists, 1,000 out of the 2,200; mathematicians, 400 out of the 700; and 1,300

(Continued on page 22)

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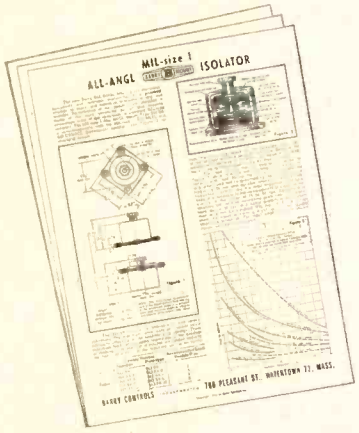

you load-deflection curves, transmissibility curves, and load-versus-natural-frequency curves that show how these isolators perform under various loads and vibration inputs and for different directions of applied acceleration. They explain how these curves can be used to evaluate isolator performance. And they contain detailed drawings that show all necessary dimensions and clearances.

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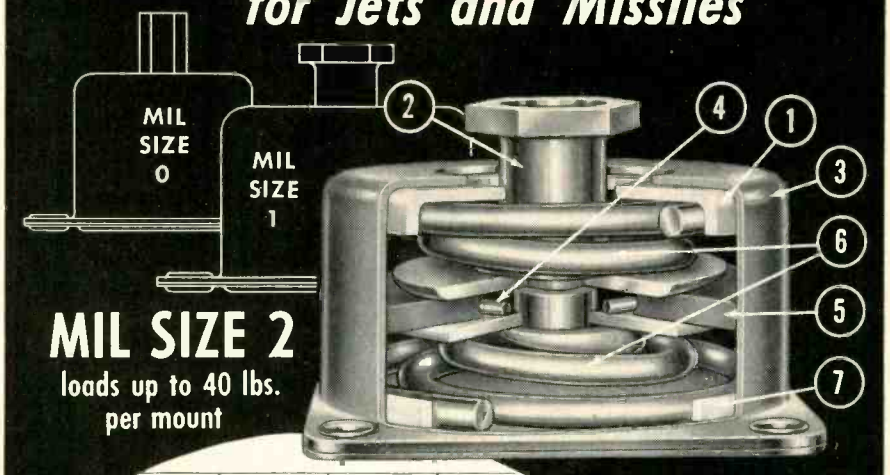

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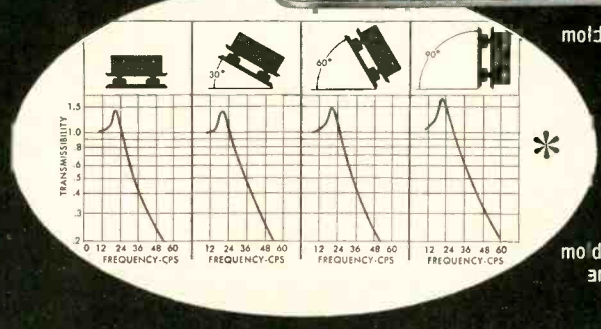

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of the 3,200 remaining scientists and engineers in other occupations.

▶ **Assistants** — The survey also shows that for each 100 of the 28,800 r&d scientists and engineers in the industry, there were 150 supporting personnel, or statistically, 1.5 men per engineer or scientist. Of the 150, 90 are technicians, 10 are craftsmen and the remaining 50 are in various other classifications.

At least three other industries use more supporting personnel per man than the electronics, electrical field. Tops is aircraft where there are 270 supporting personnel per 100 r&d engineers and scientists. Next is machinery with 170 per 100, followed by fabricated metal products with 160 per 100.

▶ **Definition** — Research and development as defined in the study includes activities carried on by persons trained in the physical sciences including related engineering if the purpose of such activity is to pursue a planned search for new knowledge; apply existing knowledge to problems of creating a new product or process or apply existing knowledge to problems involved in the improvement of a present product or process.

If the primary objective is to make further improvements on the product or process, then the work comes within the definition of research-development. If the product or process is substantially "set" and the primary objective is to develop markets or to do preproduction planning, or to get the production process going smoothly, then the work is not research-development.

BOMARC-NOSED B-57 Canberra jet bomber, modified by Temco Aircraft, tests guidance system as . . .

Missile Gets Ready For Production

ELECTRONIC guidance system for the Bomarc long-range supersonic missile will soon be in use as the Air Force gets ready to go into quantity production of the missile. Produced by Boeing Airplane Co. in Seattle, Wash., the missile is believed to be in the 200-mile range class.

▶ **Navigation** — Its guidance system has been under test at Temco Aircraft using the modified B-57 shown. The modification included attaching the 17-foot nose which involved weight and stress and design changes in the bomber itself. Temco's work was done under contract to Boeing.

▶ **TV** — Industrial tv applied to guided missiles allows tv in a missiles nose to transmit back to the pilot in a control plane a picture of what's ahead. Pilot could select target and aim missile via remote control while a video tape recorder "cans" the operation.

Computers Solve Aircraft Problems

Flight test data reduction requires more special large-scale computers

MULTIMILLION - DOLLAR airplanes must be tested thoroughly and quickly to keep up with the ever-increasing race for air superiority. Data-processing time and costs are important factors here.

▶ **Latest**—A system that automatically takes care of data reduction of flight test information obtained from airborne magnetic tape recorders is now in use at Boeing Aircraft. The system, engineered by Boeing and other firms, simultaneously records 14 tracks of data on a single inch-wide magnetic tape using pulse-width modulation techniques.

▶ **How It Works** — In processing, the first step is to scan the data at high-speed using a tv display. The equipment operator can tag important data for immediate attention. This tagged tape is fed to the digitor for conversion from pulses to numbers which are recorded on a second tape. This second tape is run through the computer which scales and calibrates the data and presents it in the desired form.

▶ **Other** — Research and development work in the fields of supersonic aircraft, missiles and rocket engine design at North American Aviation, is being accelerated through the use of three IBM 704's now in operation.

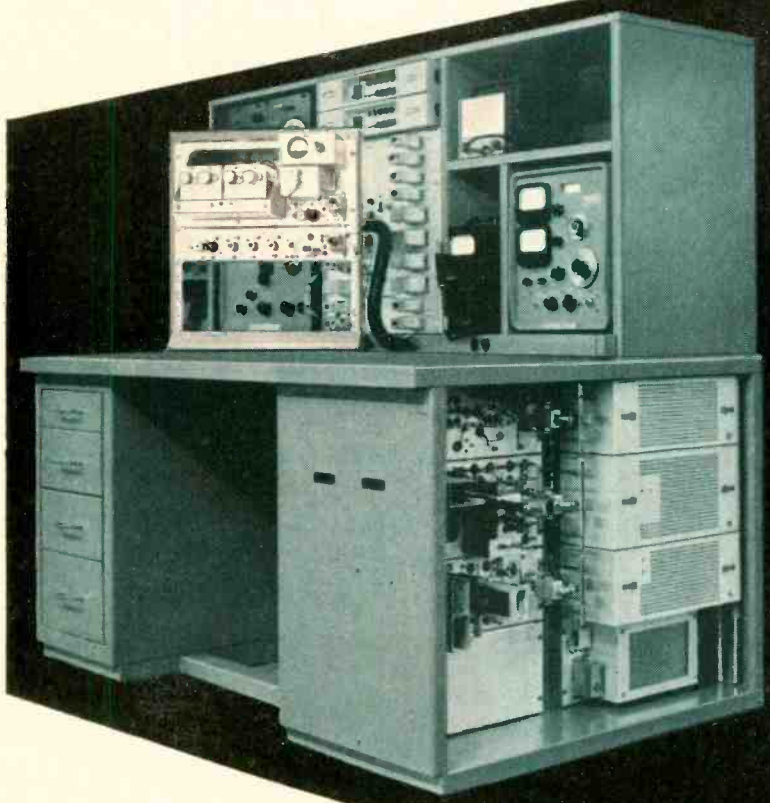
Ammunition Pack May Replace Parts Reels

Boxes for belted components require less space and give smoother feed to machines

ADVANTAGES OF boxes for storing, handling and feeding machine-gun bullets may bring about an industry-wide transition to this type of

(Continued on page 24)

Accelerated testing



A vital link in our national defense is White Alice—largest Tropospheric Scatter system yet conceived—which is to provide military communications and civilian telephone service throughout Alaska.

With the system now in partial operation, reliability of the equipment becomes essential. This is assured both by the choice of REL for the development and manufacture of the Tropo Scatter radio equipment, and by the remarkable test bench pictured, also designed and built by REL.

Any panel of the White Alice driver exciters or dual diversity receivers can be slipped into the test rack *(left)* and instantly plugged into the bench for immediate testing. This eliminates the bother and delay of cumbersome conventional test procedures, and is an important addition to the overall operating reliability of White Alice.

REL's unique facilities and thirty-five-year experience are available for the solution of your specialized radio problem.

Radio Engineering Laboratories·Inc.

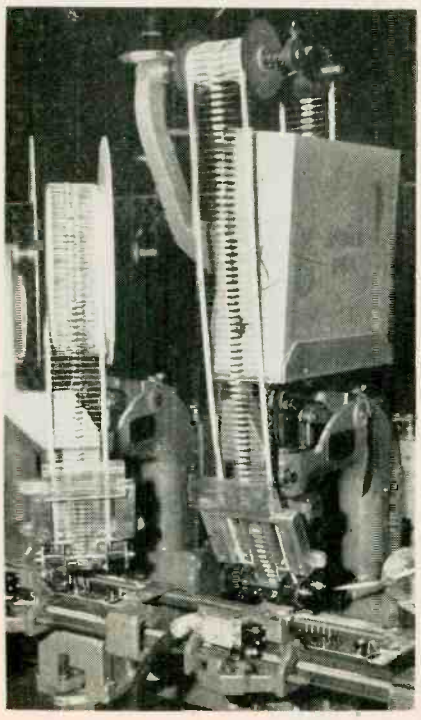
36-40 37th St · Long Island City 1, N Y

STillwell 6-2100 · Teletype: NY 4-2816

Canadian representative: AHEARN & SOPER CO ·BOX 715 · OTTAWA

Creative careers at REL await a few exceptional engineers. Address resumes to James W. Kelly, Personnel Director.

Experimental ammunition pack for video peaking coils having lead belting. Components stack automatically as belt is lowered



New box pack on coil insertion head of United Shoe machine in Philco plant, with reel pack on adjacent head for comparison

pack for belted electronic components as well.

Tests by Philco Corp. and others have shown that up to about 60 percent more components can be put into a box than on a reel requiring the same shipping space. With boxes, loading onto the insertion head of an automatic assembly machine is much easier; the box is simply placed on a shelf, whereas a reel must be placed on a shaft and locked in position. From boxes the feed tension is essentially constant; with reels the tension increases as the reel runs down, causing occasional jams. Finally, boxes are considerably cheaper than reels.

▶ **Size**—Component vendors, manufacturers of automatic assembly machines and users of the machines now seek agreement on standard sizes for the boxes. This standardization can mean added cost savings in making the throw-away boxes, particularly if component manufacturers use the same type of pack for all. The box pack works for both body taping and lead taping, and insertion heads of United Shoe and other machines are easily modified to take the boxes. Small axial-lead coils such as television peaking coils can be handled equally as well as axial-lead resistors and capacitors in the boxes.

▶ **Trend** — Practically all component manufacturers are now pro-

(Continued on page 26)

Military Electronics

▶ Navy awarded Convair division of General Dynamics a $29-million contract for production at Pomona, Calif. of guidance and control units for the Terrier guided missile. Convair operates the 1.2-million sq ft government-owned Naval Industrial Reserve Ordnance plant at Pomona for the Bureau of Ordnance

▶ **Government** backlog totaling $245 million at the end of 1956 for Raytheon is the largest in the firm's history and almost two and a half times the backlog of a year ago

▶ **Test** and launching equipment for the Thor intermediate range ballistic missile will be built by Packard-Bell for Douglas Aircraft under a $3-million contract. Production test equipment, check-out equipment and launching equipment, including closed-circuit tv gear to monitor the projectile before and during flight and observation of the firing site, will be designed and developed

▶ **More** Doppler navigation systems for the Air Force will be built under a $17-million contract awarded to GPL by the Air Material Command. The systems provide direct and continuous readings of a plane's ground speed and drift angle independent of ground or celestial guidance

▶ **Volume** of military electronics for the industry will run about $3 billion in 1957, an increase of 10 percent over last year, according to G. L. Haller of GE

▶ **Electronic** controls and instrument sales for U.S. planes and guided missiles will total $1.5 billion in 1957, up $100 million over 1956, according to Minneapolis-Honeywell estimates

There's a standard PERKIN model for your every need!

In addition to the 28 volt models featured at the right, the following units are also available:

OTHER 28 VOLT MODELS

Mode	Volts	Amps	Reg.	AC Input (60 cps)	Ripple rms
28-5VFM	0-32 V	5	20% (24-32 V range)	115 V 1 phase	2%
28-10WX	24-32 V	10	±½%	100-125 V 1 phase	1%
28-15VFM	0-32 V	15	20% (24-32 V range)	115 V 1 phase	5%
28-50WX	24-32 V	50	±½%	230 V* 3 phase	1%
MR2432-200	24-32 V	200	±½%	230 V* 3 phase	1%
MR2432-300	24-32 V	300	±½%	230 V* 3 phase	1%
MR2432-500	24-32 V	500	±½%	230 V* 3 phase	1%

*±10%. Also available in 460 V ±10% AC input. Will be supplied with 230 V input unless otherwise specified.

6, 12, 115 VOLT (NOMINAL) MODELS

	Model	Volts	Amps	Reg.	AC Input (60 cps)	Ripple rms
6 Volt	6-5WX	6 ±10%	5	±1%	95-130 V 1 phase	1%
6 Volt	6-15WX	6 ±10%	15	±1%	95-130 V 1 phase	1%
6 Volt	6-40WX	6 ±10%	40	±1%	95-130 V 1 phase	1%
12 Volt	12-15WX	12 ±10%	15	±1%	95-130 V 1 phase	1%
115 Volt	115-5WX	115 ±10%	5	±½%	95-130 V 1 phase	1%
115 Volt	MR15125-5	15-125	5	±1%†	95-130 V 1 phase	1%†
115 Volt	G125-25**	115-125	25	1½-4%	230/460 V 3 phase	5%

**Germanium Rectifier Unit †Increases to 2% @ 15 V.

PERKIN SALES OFFICES:

New York area N.J. Newark — MAkt 3-1454
Philadelphia BR 5-2600
Chicago PA 5-6824
St. Louis PA 5-7701
Kansas City, Mo. VA 1-5330
Dallas FO 8-8306
Denver MA 3-0343
San Francisco area (Palo Alto) DAvnpt 5-6136
Los Angeles RY 1-8810
Pittsburgh WA 1-2959
Minneapolis MI 4-7884
Seattle MO 4895
Albuquerque 5-9632
Atlanta EL 3020
Miami MO 5-1563
Charlotte ED 2-7356
Winston-Salem 4-0750
Boston MI 8-0756
Canada Agincourt, Ontario AX 3-7011

PERKIN...THE LEADER

IMMEDIATE DELIVERY FROM STOCK

in tubeless magnetic amplifier regulated

DC POWER SUPPLIES

No Moving Parts • No Vibrating Contacts

Model MR532-15A

2-36 VOLTS @ 15 AMPS SPECIFICATIONS

Regulation:	5-32 Volt Range: —½% 2-5 Volt and 32 36 Volt Range: ±2%
AC Input:	105-125 Volts, for 2-32 V.DC), 110-125 V, (for 32-36 V.DC), 1 phase, 60 cps (8 amps)
Ripple:	1% rms max. (@ 36 volts and full load. Increases to 2% @ 2 volts and full load).

Remote Sensing • Vernier Control

Model M60V

0-32 VOLTS @ 25 AMPS SPECIFICATIONS

Regulation:	±1% @ 28 Volts (Regulation increases to 2% over range of 24-32 volts; does not exceed 2 volts over 4-24 volt range. Not stabilized for AC line changes.)
AC Input:	115 Volts, 1 phase, 60 cps (12 amps).
Ripple:	1% rms (@ 32 volts and full load—2% rms max. @ any voltage above 4 volts).

Model MR1040-30A

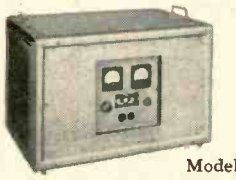
5-40 VOLTS @ 30 AMPS SPECIFICATIONS

Regulation:	±1% (over entire 5-40 volt range)
AC Input:	100-130 Volts 1 phase, 60 cps
Ripple:	1% rms

Model 28-30 WXM

24-32 VOLTS @ 30 AMPS SPECIFICATIONS

Regulation:	±½%
AC Input:	100-125 Volts, 1 phase, 60 cps (20 amps). (Unit rated for DC output of 28 volts ±10% for 95-130 volt input.)
Ripple:	1% rms



Model MR2432-100XA

24-32 VOLTS @ 100 AMPS SPECIFICATIONS

Regulation:	±½%
AC Input:	208, 230 or 460 Volts, ±10%, 3 phase, 60 cps (14, 12 and 6 amps respectively). 230 volt input will be supplied unless otherwise specified.
Ripple:	1% rms

Wire factory collect for prices . . . Write for catalog.

PERKIN

LEADER IN TUBELESS MAGNETIC AMPLIFIER REGULATION

Representatives in Principal Cities

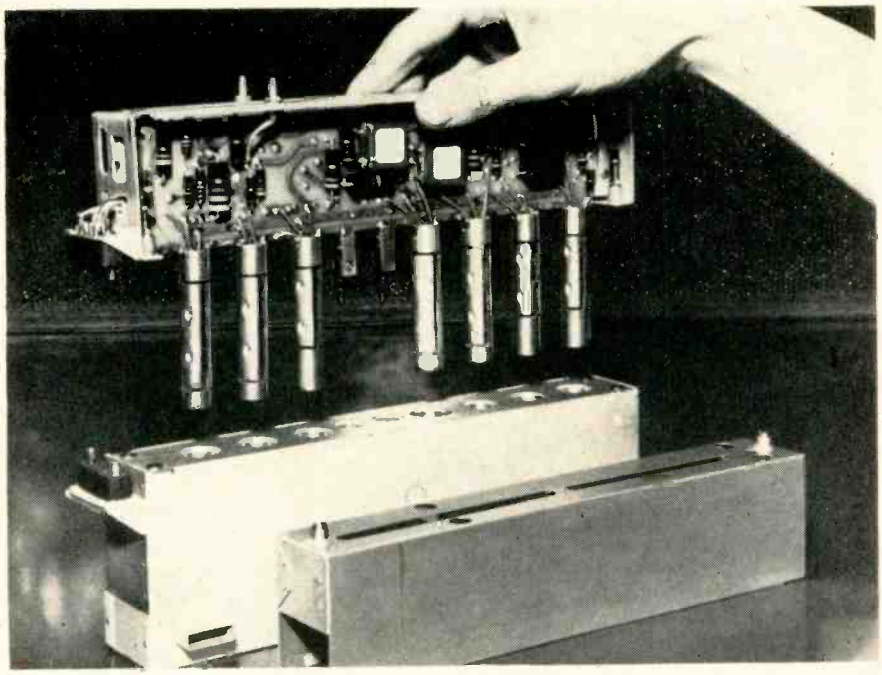
PERKIN ENGINEERING CORPORATION

345 KANSAS ST. • EL SEGUNDO, CALIFORNIA • PHONE: ORegon 8-7215

viding belted components to meet the demands of their high-volume customers, despite early reluctance to give up bulk packaging.

The change in packaging is hinged to the success of these assembly machines in most of the large assembly plants; here it is not at all unusual to run every single printed wiring board through an assembly machine, even though additional parts are inserted by hand later to complete the assembly.

Natural evolution is thus bringing about now a packaging standardization for mechanization that was impossible to achieve during the first year of transition.



NEW packaging for airborne assemblies insulates and cools vacuum tubes as . . .

Electronics Adds Air Conditioning

More tubes, higher speeds, boost cooling requirements for electronic equipment

ALTHOUGH only a drop in the bucket to the billion-dollar air-conditioning market, the growing amount of cooling equipment required by increasingly complex electronic equipment is adding up to sizable business.

In terms of household unit ratings, some computers require 25-ton equipment. In military aircraft, the modern jet bomber has sufficient air conditioning capacity to air condition five five-room houses.

▶ **Market**—It has been estimated that by 1960 there will be some 5,000 computers in use in the U. S. This could mean a total air-cooling requirement of about 5,000 20-ton units. This estimate could be revised sharply downward depending on the speed with which semiconductors come into the computer picture. Up to now, air conditioning requirements of computers have almost doubled in the past two or three years as each model becomes more complex.

▶ **Military** — Cooling of military electronic equipment has become highly important especially with the advent of supersonic flight. Not only does it have important effects on the performance and reliability of the electronic equipment but also upon the operation of the aircraft itself. The advantage of the equipment must be balanced against the penalties that the added weight will have on flying performance.

Above the speed of sound, the metal skin of jet aircraft heats up to several hundred degrees. Garrett Corp.'s AiResearch division has developed a aircraft refrigeration system with a two-pound turbine that cools the air entering the cabin to 40 degrees in 2/10 of a second.

▶ **Packaging**—One method of reducing the amount of aircraft air cooling equipment is with special packing. Sylvania has a method in which vacuum tubes are mounted in carefully sized holes in light foam plastic material of the desired thermal properties. Controlled air flow gives optimum cooling while exhausting the air at high temperature. The method gives cooling efficiencies of about 90 percent and reduces the amount of air cooling equipment required.

▶ **Coolers**—Production of weather simulators, which are devices that prevent electronic equipment in jet aircraft from being damaged by heat when operated on the ground during run up and maintenance operations, is also becoming kingsize business, according to American Electronics of Los Angeles. The company, in the past year, has received almost $10 million in orders for the equipment. Output of the units has climbed from 25 units a month to 82 units. Average cost of a weather simulator is about $11,000.

Manufacturers Cash-In On Hustler

About 35 companies in electronics contribute to the new jet's complex subsystems

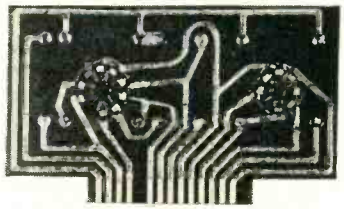
AIR FORCE'S new delta-winged supersonic bomber is loaded with electronics equipment and some 35 companies in the industry are supplying equipment for the Hustler.

▶ **Makers**—To indicate the importance of electronics in modern aircraft and the types of firms sharing in the business here are the 16 major system vendors for the B-58: Bell Aircraft, Fairchild, Sperry, Melpar, Bendix Eclipse-Pioneer,

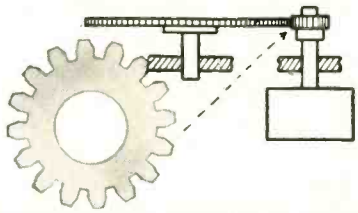
(Continued on page 28)

glass-base laminates?

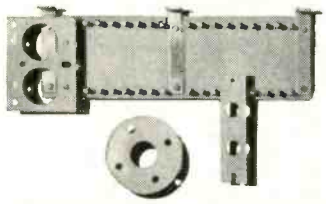
C-D-F DILECTO®
is the answer!



SPEED AUTOMATIC PRODUCTION of printed circuits with warp-resistant C-D-F metal-clad Teflon* and epoxy laminates. Other advantages: high bond strength of copper to laminate, superior blister-resistance in solder immersion.



HIGH-VOLTAGE (1800v.) RF ISOLATION is achieved by miniature C-D-F Dilecto gears in an aircraft receiver-transmitter switch. They also had to exhibit dimensional stability through a wide temperature range, resistance to fungus growth and thermal shock.



PRECISE MACHINING AND FABRICATION are standard benefits of Dilecto laminated plastics. These silicone glass-base parts (coil mountings, aircraft terminal board) were sawed, drilled, punched, and milled in production quantities by C-D-F and customer.

Teflon*, silicone, epoxy, melamine, phenolic, polyester resins laminated with glass-fiber cloth

You can improve design, speed production, and save money by specifying one of the many C-D-F Dilecto grades. Whatever your application for these laminates — with fine- or medium-weave glass-cloth base — you'll find a better answer to your problem at C-D-F. (Melamine and polyester can also be made with glass-mat base.) And C-D-F offers modern machining and fabrication facilities to deliver production quantities of finished Dilecto parts to your specifications.

See our catalog in Sweet's Product Design File, where the phone number of your nearby C-D-F sales engineer is listed. For free trial samples of glass-base Dilecto, or of any other C-D-F plastics, mica, or fibre product, send us your print or your problem! Write for your free copy of C-D-F Technical Bulletin 64.

PROPERTIES OF SOME TYPICAL C-D-F DILECTO GLASS-BASE GRADES

Grade	Equivalent NEMA or ASTM grade	Flexural Strength Lengthwise (PSI)	Dissipation Factor at 10^{6} ~ Cond. D24/23	Dielectric Strength Parallel Step x step	Insulation Resistance Cond. C96/35/90	Arc Resistance (seconds)	Maximum Operating Temp. (°C.)
GB-116T (Teflon*)	None	14,000	0.001	65	100,000	180+	250
GB-12S (Silicone)	G-7	30,000	0.008	60	100,000	245	200
GB-181E (Epoxy)	G-10	75,000	0.020	75	20,000	120	165
GB-28M (Melamine)	G-5	48,000	0.025	50	100	185	150
GB-261D (Phenolic)	G-1 and G-2	22,000	0.060	55	10,000	5	150
GM-PE (Polyester)	GPO-1	35,000	0.060	60	5,000	145	150

These are typical grades for typical applications. To meet special requirements, C-D-F makes many other Dilecto grades, one of which may serve your purpose better than any of these listed here. Consult the C-D-F Technical Department for expert assistance with your design problem involving laminated plastics products.

*DUPONT TRADEMARK FOR TETRAFLUORDETHYLENE RESIN

CONTINENTAL DIAMOND FIBRE

CONTINENTAL-DIAMOND FIBRE DIVISION OF THE BUDD COMPANY, INC.

NEWARK 16, DELAWARE

Emerson Electric, Sylvania, Magnavox, Motorola, Westinghouse, Hamilton Standard, Ultrasonic Corp., Minneapolis-Honeywell, Airojet, Federal Electric and Bendix Radio. Total of about 55 companies, electronic and otherwise, are involved in the production of the newest jet bomber.

Some of the types of equipment that electronics manufacturers are making for the bomber include transistorized fuel gauges and autopilots, passive defense systems, armament systems, bombing and navigation systems, photo-reconnaissance systems and closed-circuit tv systems.

► **Operation**—The new plane is designed to operate at altitudes above 50,000 feet. It measures 95 feet in length and has a wingspan of 55 feet. Its crew consists of a pilot, navigator-bombardier, and electronics defense systems operator.

Solid State Gains New Transistor

Symmetrical units acts as switch in prototype board produced for Navy

A NEW addition to the family of transistors apparently has been at work for some time. Known as a symmetrical transistor, the device passes signals in either direction under proper base-biasing conditions. Its most recent application is in a 100-line electronic switchboard built for the Navy by Stromberg-Carlson and now undergoing evaluation. Approximately 4,500 transistors and 5,000 diodes are used in the switchboard which is purported to save a third the power and weight of its predecessors.

► **Device**—The new transistor can provide gain in either direction by changing bias conditions or may be used as a fast relay by accepting a loss. The latter operating condition is employed in the 100-line switchboard. A voltage of one polarity applied to the base allows signals to pass whereas an opposite polarity voltage switches the unit off.

Meetings Ahead

Feb. 7: Annual Mid-Winter Symposium Aircraft Instrumentation, New York ISA, Garden City Hotel, New York.

Feb. 7: IRE Operations Research Symposium, University of Penn. Museum Lecture Hall, Philadelphia, Pa.

Feb. 7-8: 1957 West Coast Convention of the Audio Engineering Society, Ambassador Hotel, Los Angeles, Calif.

Feb. 14: Symposium On Recording Of Heart Sounds. IRE. University Of Buffalo Medical School, Buffalo, N. Y.

Feb. 14-15: 1957 Transistor & Solid State Circuits Conference, IRE, AIEE, U. of Pa., Philadelphia, Pa.

Feb. 15-16: Cleveland Electronics Conference, IRE, Masonic Auditorium, Cleveland, Ohio.

Feb. 26-27: Third Conference on Radio-Interference Reduction, Armour Research Foundation, Chicago, Ill.

Feb. 26-28: Western Joint Computer Conference, IRE, AIEE, ACM. Statler Hotel, Los Angeles, Calif.

Feb. 26-28: Joint Military-Industrial Guided Missile Electronic Test Instrument Symposium, Redstone Arsenal, Huntsville, Ala.

March 11-15: 1957 Nuclear Congress, EJC, Convention Hall, Phila., Pa.

March 18-21: IRE National Convention, Waldorf-Astoria Hotel, New York Coliseum, New York, N. Y.

March 18-21: Military Automation Show, New York Trade Show Bldg., New York, N. Y.

Apr. 8-11: British Radio And Electronic Component Show, Grosvernor House and Park Lake House, London, England.

Apr. 9-10: Annual Industrial Electronics Educational Conf., IRE, Armour Research, Ill. Institute of Technology, Chicago, Ill.

Apr. 11-13: Southwest IRE Regional Conference & Electronics Show, Shamrock Hilton Hotel, Houston, Texas.

Apr. 14-16: National Symposium On Telemetering, IRE, Sheraton Hotel, Phila., Pa.

May 13-15: National Aero & Navigational Electronics Conference, IRE, Dayton, Ohio.

May 14-16: Industrial Nuclear Technology Conference, ARF, Ill. Tech, Nucleonics Magazine, Museum of Science and Industry, Chicago, Ill.

May 20-23: 1957 Electronic Parts Distributors Show, Conrad Hilton Hotel, Chicago, Ill.

May 27-29: 1957 National Telemetering Conference, AIEE, ISA, IAS, Hotel Cortez, El Paso, Texas.

Aug. 20-23: 1957 WESCON, IRE, WCEMA, Cow Palace, San Francisco, Calif.

Industry Shorts

► **All** 12-volt models in Motorola's new car radio line are transistor powered. Printed circuits and a form of the module concept of condensed circuitry has been added to some models.

► **Public** information office has been established by the Army Ballistic Missile Agency in Huntville, Ala.

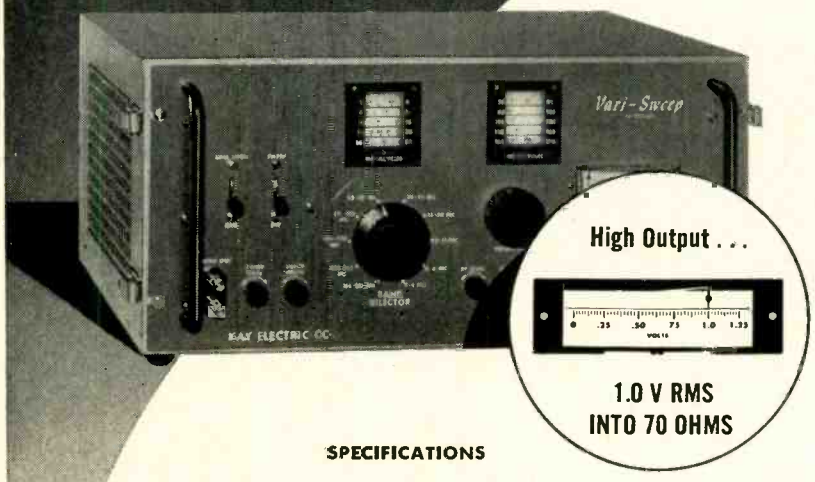
► **West** German radio and tv industry sold about 3.3 million radios in 1956, about the same as in 1955, and produced 600,000 tv sets compared to 350,000 in 1955.

► **Chicago area** (50 mile radius) bought 292,389 tv sets during the past year, according to the city's electric association.

► **Attendance** of at least 50,000 is expected for the IRE National Convention and Radio Engineering Show, to be held at the Waldorf-Astoria Hotel and the New York Coliseum, March 18-21, 1957.

► **Third** in a series of ARDC-sponsored symposia on the Use of Computers in Medicine, designed to bring together leaders in the computer and medical research fields, was held in Chicago.

HIGH Output (1.0 v. RMS into 70 ohms)
WIDE Range (2-220 Megacycles. All At Fundamental)
and
CONSTANT OUTPUT
(Fast Acting AGC)



NEW KAY *Vari-Sweep*

ALL-ELECTRONIC HIGH LEVEL SWEEPING OSCILLATOR OR, (with sweep off) CONTINUOUSLY TUNED CW SIGNAL SOURCE

- **Operates On Fundamental Frequency, Therefore Stable Narrow-Band Sweeps**
- **1.0 v. RMS (into 70 ohms) Output Flat to ±0.5 db Over Widest Sweep**
- **Output Automatically Held Constant (AGC) Over Complete Range**
- **Variable Sweep Width (to 30 mc. PLUS) — Variable Center Frequency**
- **Direct Reading Frequency Dial Accurate To ±2.0%**
- **Sweep Repetition Rates Down to 10 cps**

Price: **$695.** FOB Plant

SPECIFICATIONS

Range: Fundamental frequency 2 to 220 mc., continuously variable in 10 switched overlapping bands. Direct reading frequency dial calibrated to ±2.0%.

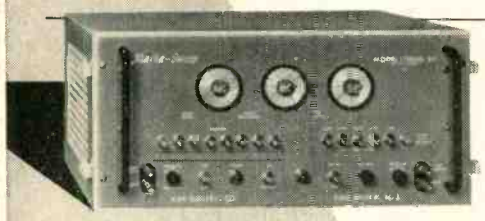
RF Output: 1.0 v. RMS into 70 ohms, metered. Flat within ±0.5 db over widest sweep and frequency band.

Sweep Width: Continuously variable to ± 30% of center frequency to maximum of at least 30mc.

Sweep Rate: Continuously variable 10 to 40 cps.; also locks at line frequency.

Attenuator: Switched 20, 20, 10, 6, and 3 db plus continuously variable 6 db.

Power Supply: Electronically regulated 105 to 125 v. A. C. 50 - 60 cycles



NEW KAY *Marka-Sweep* MODEL VIDEO 50

Combined Video and IF Sweeping Oscillator with Marks

SPECIFICATIONS

Frequency Range: Continuously variable, 50 kc to 50 mc.
Sweep Width: Linear, continuously variable, 4.0 mc to 50 mc.
Sweep Rate: Variable around 60 cps; locks to line frequency.
Amplitude: 1.0 v, peak-to-peak, into nom. 70 ohms. Flat within ±0.5 db over widest sweep.
Attenuators: Switched 20, 20, 10, 6 and 3 db, plus continuously variable 3 db.
Markers: Eight sharp, pulse-type, crystal-positioned, internal and external markers.
Price: $695.00 F.O.B. Factory. Substitute markers, $10.00. Additional markers, $20.00 each.

See us at the IRE Show Booths 2608-09-10

KAY ELECTRIC COMPANY
14 MAPLE AVENUE PINE BROOK, N. J. CAldwell 6-4000 Dept. E-2

Kennard and V. C. McIntosh of WRIGHT AIR DEVELOPMENT CENTER Install Magnetic Tape Recorder in F-101 Aircraft.

Dynamics Section, Engineering Support Branch at Wright Air Development Center's Equipment Laboratory is primarily responsible for evaluating aircraft equipment under conditions of actual use . . . particularly vibration, shock, and acceleration. Under Section Chief D. C. Kennard, it records these phenomena as they actually exist in aircraft and missiles under all conceivable service conditions.

Prior to 1952, 12-channel recording oscillographs were used. But weight and size limited their use, as did the need for an operator to set attenuators for optimum sensitivity on each channel. Furthermore, the Dynamics Section is particularly interested in the frequency content of vibration, and the relative amplitude of each component frequency. But getting this information from oscillograph traces proved something of a problem. Visual examination was neither accurate nor complete. The Section resigned itself to using the 24-point method of Fourier Analysis in conjunction with punched card equipment, but was far from satisfied.

Searching for an entirely new approach, the Dynamics Section settled on magnetic tape recording, despite the fact that no suitable equipment was in existence. On November 2, 1949, in Exhibit MCREXE84-2, The Air Force called for the development of airborne magnetic tape data recording, reproduction and analysis equipment.

Among the responses to the exhibit was a proposal from the Davies Laboratories, Inc. Though the company had no previous experience with tape or recording, the ideas which Gomer L. Davies set forth in that proposal were interesting enough to gain his company the contract. Let on April 7, 1950, it called for three 14-channel airborne recorders, a 14-channel ground playback unit, and a dual channel automatic wave analyzer.

The combined efforts of Davies and his staff, and the Dynamics Section overcame obstacles that for years had chained magnetic tape to the broadcasting studio. The first system delivered to the Dynamics Section included such refinements as servo speed control for correcting low-frequency tape speed variations and a unique, completely elec-

MAGNETIC TAPE data recording Born: April 7, 1950

Today, magnetic tape is an accepted tool for data acquisition, processing, and storage. It has proved its worth in laboratories, industrial plants, even missile test centers. But a decade ago magnetic tape data recording did not exist. And without the inspired cooperation of a government agency and a private enterprise, it might not exist yet.

tronic compensation system for eliminating the effects of wow and flutter.

By 1952 magnetic tape data recording was a reality, with the delivery and acceptance of the first complete system for airborne use in November.

Substantially all the requirements set forth in the 1949 exhibit had been met. And several had been exceeded. The completely self-contained recorders were even smaller than specified. The three recorders so speeded up data acquisition that The Air Force immediately placed an order with Davies for four additional channels of analysis equipment.

With the introduction of magnetic tape data recording in November, 1952 as a full grown art, the technique was quickly adopted in laboratories, manufacturing plants, and government installations across the country . . . an amazing growth. But the record set by Davies equipment at Wright Air Development Center is impressive enough in itself. Davies recorders have been used there in testing every conceivable kind of aircraft, including:

F-86A F-86D B-36 B-45 B-47 B-50 B-52 B-57 B-66 C-47 C-54 C-123 C-124 C-130 H-19 KC-97 Q-2A RB-50

They have been used for ground testing at least ten different power plants. They have been taken to other military installations so that data recorded there could be analyzed on Davies equipment at the Dynamics Section. Most important, data made available by Davies equipment assisted in causing revisions in basic Air Force Specifications. It has been possible to prove, for example, the importance of high frequency vibration as a vital design consideration, and thereby eliminate an arbitrary upper limit of 55 cps on vibration testing.

Surely, magnetic tape data recording has been proved a development of vital importance. But it has even greater significance as an outstanding example of the benefits of a country in which government and industry can work hand-in-hand . . . cooperating on every level for the eventual betterment of all mankind.

COLORED SILICONE THAT LASTS— BH "1151" SLEEVING

BLUE • RED • GREEN
BROWN • YELLOW • NATURAL

When you want the indentification possibilities of color, and need the extra protection of a silicone insulation, your first choice should be BH "1151" Silicone-Fiberglas Sleeving.

For all their beneficial properties, silicone insulations do have an enemy . . . it's COLOR! Unless the coloring pigments used are compatible with the basic silicone sleeving, insulation effectiveness can be lost. But . . . you can use BH "1151" with complete confidence of product protection. A superior Class "H" insulation, it loses none of its strength, or resistive properties, through the incorporation of color.

Take your choice of red, yellow, blue, green, brown, or natural (off white). With these five colors, and with the addition of tracer stripes in any of these colors, the identification range becomes a wide one when you use BH "1151" Silicone-Fiberglas Sleeving. Or, you may have special colors made up, provided compatible pigments are available.

And here's another advantage! The minimum order for special colors, or those not in stock, is only 500 feet. Write today for samples and data sheets and make your own tests.

BENTLEY, HARRIS MANUFACTURING CO.
1302 BARCLAY ST., CONSHOHOCKEN, PA.
Telephone: TAylor 8-0634

BENTLEY, HARRIS *Fiberglas** **SLEEVINGS**

*BH Non-Fraying Fiberglas Sleevings are made by an exclusive Bentley, Harris process (U.S. Pat. Nos. 2393530; 2647296 and 2647288). "Fiberglas" is Reg. TM of Owens-Corning Fiberglas Corp.

solve many difficult control problems...use

OHMITE®

RHEOSTATS

with special features

Ohmite offers not only a line of *standard* rheostats but also rheostats with a wide variety of *special features*. Illustrated are only a few. All have the distinctive Ohmite design features: smoothly gliding metal-graphite brush; all-ceramic construction; insulated shaft and mounting; windings permanently locked in place by vitreous enamel. You will find the special rheostat feature you need in the dependable Ohmite line.

BUSHINGS FOR SPECIAL THICKNESS
Extra-long bushings and shafts for panels up to 2" in thickness. Seven bushing lengths.

SCREW DRIVER SLOT SHAFT
Shaft ends slotted for operation with a screw driver where few adjustments are needed.

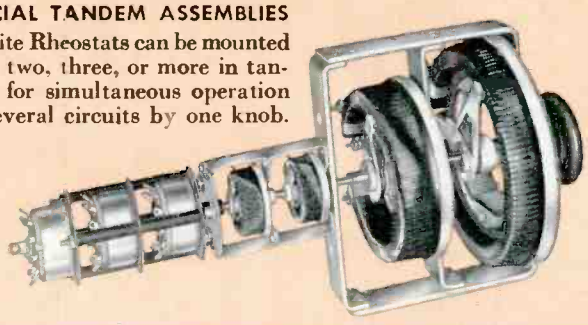
VENTILATED CAGES
Prevents mechanical injury to rheostat or human contact with electrically "live" parts.

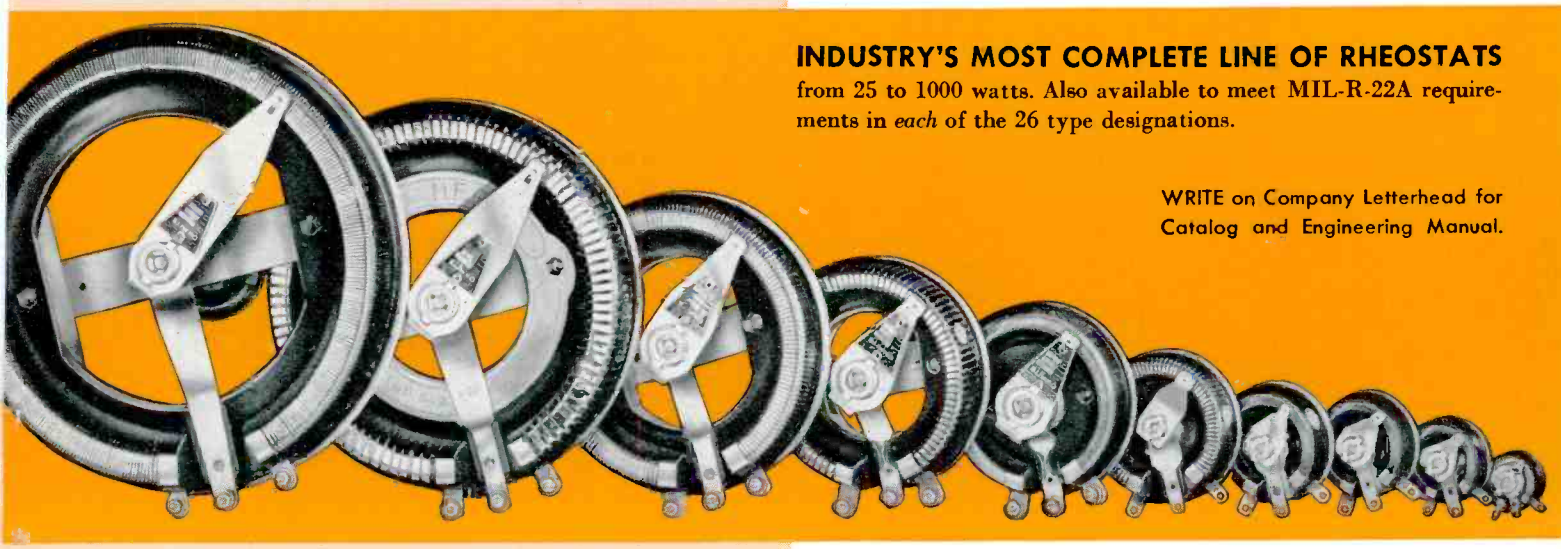
SENSITIVE SWITCH
Opens or closes circuit with minimum movement of control knob shaft. Extremely dependable long life switches.

TOGGLE SWITCH
Is operated with a positive snap by the rheostat arm at either end position. Used for heavy-duty applications.

WITH OFF POSITION FEATURES
Opens circuit at high or low resistance position with *snap-action* (illus.); opens circuit at high resistance position with *dead lug* off position; or has *dead section* off position.

SPECIAL TANDEM ASSEMBLIES
Ohmite Rheostats can be mounted with two, three, or more in tandem for simultaneous operation of several circuits by one knob.





INDUSTRY'S MOST COMPLETE LINE OF RHEOSTATS
from 25 to 1000 watts. Also available to meet MIL-R-22A requirements in *each* of the 26 type designations.

WRITE on Company Letterhead for Catalog and Engineering Manual.

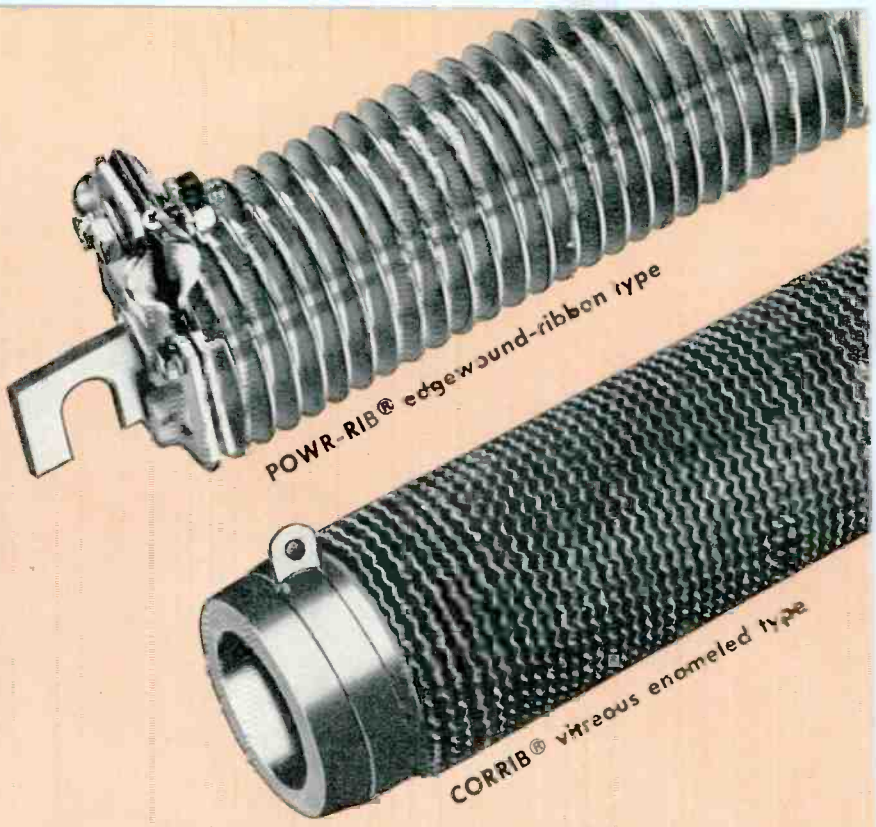
BE RIGHT WITH

RHEOSTATS · RESISTORS · RELAYS
TAP SWITCHES · TANTALUM CAPACITORS

OHMITE®

OHMITE MANUFACTURING COMPANY, 3610 Howard Street, Skokie, Illinois

specify OHMITE® *Power Type* RESISTORS for high current low resistance applications—



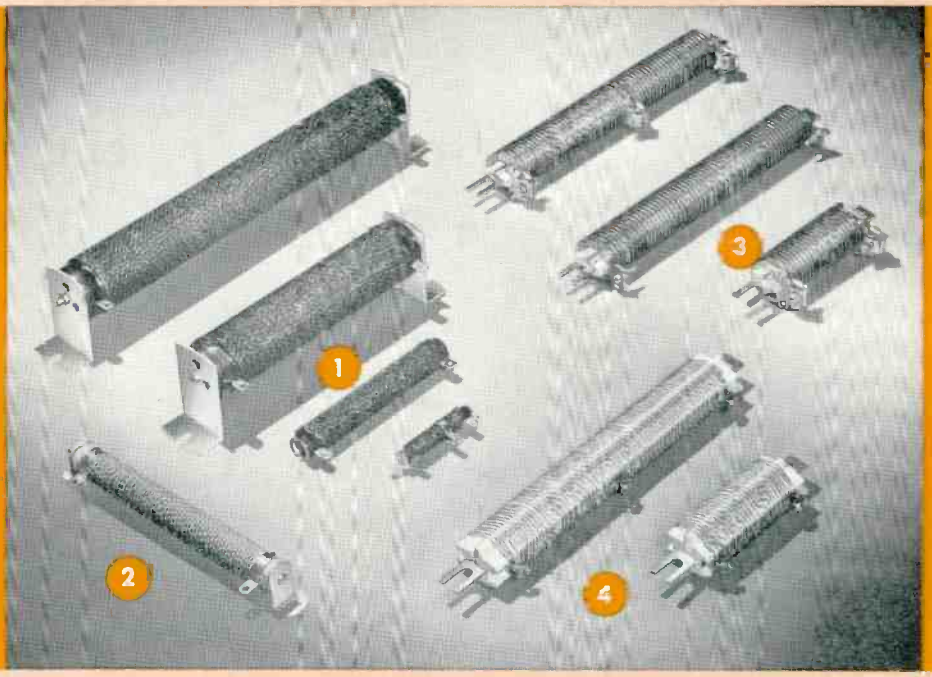
The Ohmite line of specialized CORRIB and POWR-RIB resistors solves your high-current, low-resistance problems. The four basic types of Ohmite units (shown below) handle a wide range of special power resistor needs. They are designed for continuous or intermittent duty and provide dependability for heavy-duty applications. Available in Fixed or Adjustable "DIVIDOHM®" Types.

IN STOCK—22 Corrib Resistance Values in 300 Watt Size (Core 8½" x 1⅛").

IN STOCK—26 Powr-Rib Resistance Values in 5 Section Size (17⅞" long).

Write for Bulletin 144

1. **CORRIB®**
   vitreous-enameled corrugated-ribbon type
   Fixed, tapped, and adjustable types in 25 sizes, 90 to 1500 watts. Resistances from .04 to 110 ohms.
2. **CORRIB®**
   bare threaded tube type
   For continuous or intermittent operation at higher than normal 375°C temperature rise. In two sizes, from 0.36 to 4.25 ohms.
3. **POWR-RIB®**
   edgewound-ribbon type
   Has ceramic core, sectionalized to resist shock. Four sizes. Values .043 to 1.6 ohms; 24 to 95 amps.
4. **POWR-RIB®**
   round-wire type
   Has sectionalized core similar to ribbon type. Four sizes. Values from .69 to 25 ohms; 5.1 to 18.4 amps.



Be Right with OHMITE®

RHEOSTATS
RESISTORS
RELAYS
TAP SWITCHES
TANTALUM CAPACITORS

OHMITE MANUFACTURING COMPANY, 3610 Howard Street, Skokie, Illinois (Suburb of Chicago)

Here's why Electronic Equipment is Safeguarded Best — when Protected by BUSS Fuses

To make sure BUSS fuses will give dependable electrical protection under all service conditions . . . BUSS fuses are tested in a sensitive electronic device. Any fuse not correctly calibrated, properly constructed and right in all physical dimensions is automatically rejected.

That's why BUSS fuses blow only to protect—and not needlessly. Equipment receives maximum protection against damage due to electrical faults —yet, it is not put out of operation by needless fuse blows.

Most important, the reputation of your equipment for service and quality is not harmed by the faulty operation of poor quality fuses.

Why settle for anything less than BUSS quality fuses? To meet your needs, a complete line of BUSS fuses is available, plus a companion line of fuse clips, blocks and holders.

For more information on BUSS and FUSETRON Small Dimension fuses and fuseholders . . . Write for bulletin SFB. Bussmann Mfg. Co. (Div. of McGraw Electric Co.), University at Jefferson, St. Louis 7, Mo.

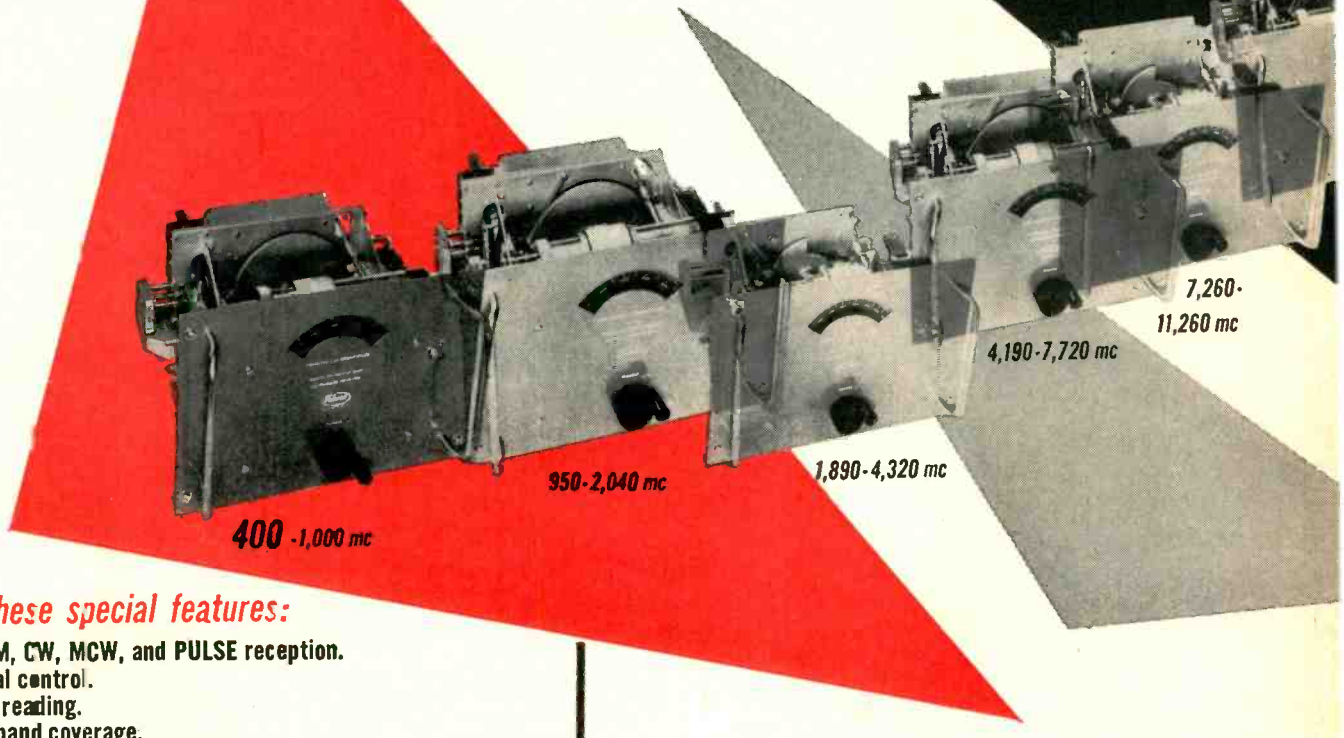
BUSS fuses are made to protect —not to blow, needlessly

FUSETRON
TRUSTWORTHY NAMES IN ELECTRICAL PROTECTION
BUSS

Makers of a complete line of fuses for home, farm, commercial, electronic, automotive and industrial use.

NEW

Model R



Note these special features:

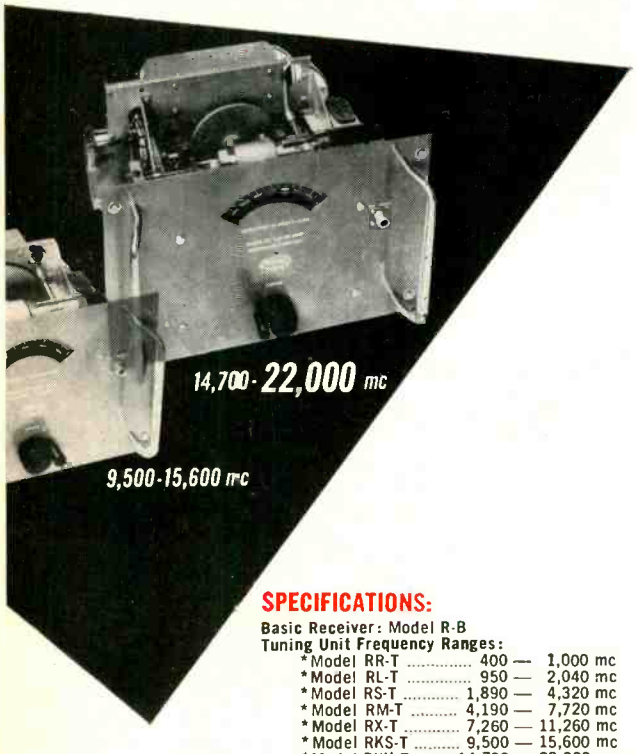
- AM, FM, CW, MCW, and PULSE reception.
- Uni-dial control.
- Direct reading.
- Broadband coverage.
- Output level reading directly in db.
- High sensitivity.
- Seven interchangeable plug-in r-f tuning units cover the entire frequency range.
- Low noise figure; excellent gain stability.
- Microwave preselection, tracked and double-tuned, used in the plug-in tuning units covering the range 400 to 11,260 mc.
- Audio, video, and trigger outputs.
- Special recorder output.
- High video output—low impedance.
- AGC and AFC circuits.

For these applications:

- General communications.
- Field intensity meter.
- Frequency meter.
- Measurement of radiation and leakage of microwave devices.
- Measurement of bandwidth of microwave cavities.
- Measurement of relative power of fundamental and harmonic signal frequencies.
- Measurement of noise figure.
- Antenna field patterns.

EXTENDED RANGE MICROWAVE RECEIVER!

400 to 22,000 mc



Three new r-f tuning units double the frequency range of the well-known Polarad Microwave Receiver. Now more than ever the Model R becomes a basic multi-purpose instrument for microwave research and production in the field, in the laboratory, and in the factory.

This receiver is designed for quantitative analysis of microwave signals and is ideal for the reception and monitoring of all types of radio and radar communications within the broadband 400 to 22,000 mc. It permits comparative power and frequency measurements, by means of its panel-mounted meter, of virtually every type of signal encountered in microwave work.

It is compact and functional, featuring 7 integrally designed plug-in, interchangeable RF microwave tuning units to cover 400 to 22,000 mc; non-contacting chokes in pre-selector and microwave oscillator to assure long life and reliability; and large scale indicating meter for fine tuning control.

Call any Polarad representative or direct to the factory for detailed specifications.

SPECIFICATIONS:

Basic Receiver: Model R-B

Tuning Unit Frequency Ranges:

*Model RR-T	400 — 1,000 mc
*Model RL-T	950 — 2,040 mc
*Model RS-T	1,890 — 4,320 mc
*Model RM-T	4,190 — 7,720 mc
*Model RX-T	7,260 — 11,260 mc
*Model RKS-T	9,500 — 15,600 mc
*Model RKU-T	14,700 — 22,000 mc

Signal Capabilities: AM, FM, CW, MCW, pulse

Sensitivity:
(a) For Model RR-T: Minus 85 dbm
(b) For Models RL-T, RS-T, RM-T, and RX-T: Minus 80 dbm
(c) For Models RKS-T and RKU-T: Minus 65 dbm

Frequency Accuracy: ±1%

IF Bandwidth: 3 mc

Video Bandwidth: 2 mc

Image Rejection:
(a) For Models RR-T thru RX-T: Greater than 60 db
(b) For Models RKS-T and RKU-T: Spurious response rejection obtained through the use of a bandpass filter

Gain Stability with AFC: ±2 db

Automatic Frequency Control: Pull-out range 10 mc off center

Recorder Output: 1 ma. full scale (1,500 ohms)

Trigger Output: Positive 10-volt pulse across 100 ohms

Audio Output: 5 volts undistorted, across 500 ohms

FM Discriminator: Deviation Sensitivity: .7 v./mc

Skirt Selectivity: 60 db — 6 db bandwidth ratio less than 5:1

IF Rejection: 60 db

Input AC Power: 115, 230 V ac, 60 cps, 440 watts

Input Impedance: Models RR-T through RX-T: 50 ohms Models RKS-T & RKU-T: waveguide

VSWR: Less than 4:1 over the band

Range of Linearity: 60 db

Receiver Type: Superheterodyne

Maximum Acceptable Input Signal Amplitude: 0.1 volt rms, without external attenuation

Video Response: 30 cps to 2 mc

Size: 17" w x 23" d x 19" h

Weight: 180 lbs. for basic unit with one tuning unit.

For private demonstration without obligation ask for the

to stop at your plant

maintenance available by field service specialists

AVAILABLE ON EQUIPMENT LEASE PLAN

*U. S. PATENT NO. 2,774,243

POLARAD PROVEN RELIABILITY

ELECTRONICS CORPORATION

43-20 34th Street · Long Island City 1, New York

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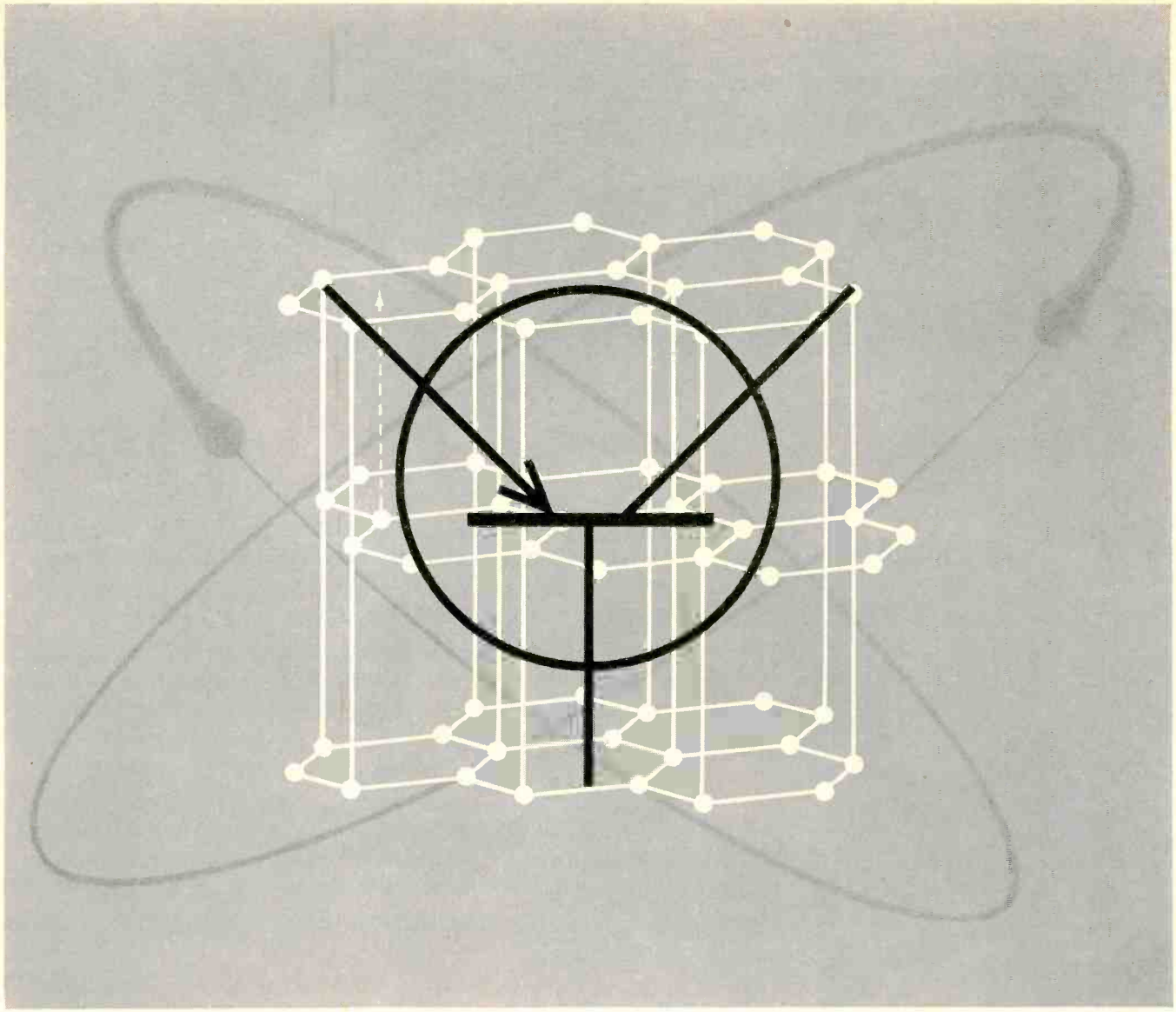


GRAPHITE

. . . ultra pure for the electronic industry

If you wish competent technical help concerning the use of graphites in the electronics field . . . combined with graphite products of the maximum density and purity . . . we invite you to UNITED CARBON PRODUCTS CO., INC.

Your electronic graphite problem—whether it be on production material or parts—can probably find fast solution in the technical service division at UNITED.

We have been privileged, over the years, to have worked out successful solutions to innumerable graphite problems for many world-famous organizations.

A simple, brief letter concerning your problem will put our technical service division at your confidential service—immediately. Or, if you wish, telephone or wire.

UNITED

CARBON PRODUCTS CO. INC.

P.O. BOX 269, BAY CITY, MICH.

CMC *model 226A*

UNIVERSAL COUNTER-TIMER

FEATURES:

- ★ Three independent, adjustable trigger-level controls permitting full rated sensitivity at any voltage level between −300 and +300 volts.
- ★ Simplified color-coded controls and direct read-out in kc, mc, sec or millisec with automatic decimal point indication.
- ★ Small voltage increments ordinarily masked by attenuators are easily selected.
- ★ Oscilloscope marker signals facilitate start and stop trigger-level adjustment for time interval measurement of complex waveforms.

APPLICATIONS:

Multi-purpose instrument designed for precise measurement of Frequency, Frequency Ratio, Period (1/frequency) and Time Interval. Pressure, Velocity, Acceleration, Displacement, Flow, RPS, RPM, etc., may also be measured with suitable transducers. May be used as a secondary frequency standard.

BRIEF SPECIFICATIONS

Frequency Range	0-1,000,000 cycles per second
Period Range	0.000001 cps to 100 kc
Time Interval Range	3 microseconds to 1,000,000 seconds
Time Bases	0.00001, 0.0001, 0.001, 0.01, 0.1, 1 and 10 seconds; external 1 and 10 cycles of unknown (period)
Secondary Frequency Standard	1 mc; 100, 10, 1 kc; 100, 10, 1 cps
External Standard Input	0 to 1 mc

Price $1,100.00

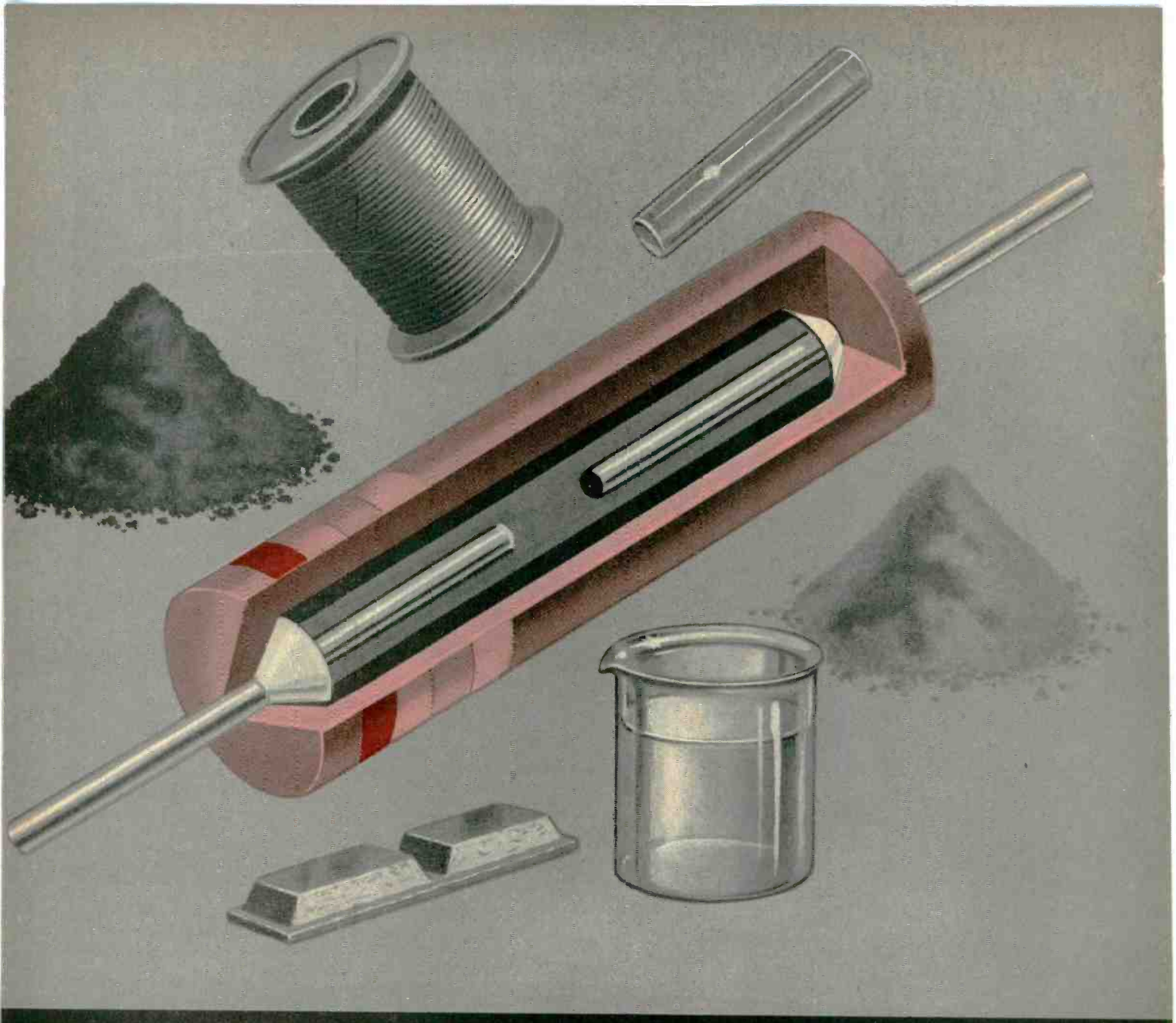
Model 225A —0 cps to 100 kc also available. Price $840.

Complete specifications available from representative in your area or direct from factory . . .

Computer Measurements Corporation

5528 Vineland Ave. • No. Hollywood, Calif.

Want more information? Use post card on last page.



They're made from standard materials—

WHY DO IRC® RESISTORS OFFER HIGHEST REPRODUCIBILITY?

Carbon, glass, coating resins, molding powder, copper wire, and a metal alloy—they're the only materials you'd need to make a resistor such as IRC's famous Type BT fixed composition resistor. But the real problem, you'd soon discover, is to make every resistor just like the ones before it and just like those following it. That's where IRC's exclusive processes pay off. They give you resistors that "test out" more alike in mechanical and electrical characteristics than any other resistors of their type. That's why only IRC resistors make possible unvarying performance of your own equipment.

The outstanding thing about IRC production processes is that they provide this uniformity at economical mass-production rates. For example, over 5 miles of carbon filament are drawn every day for film type resistors. And for maximum efficiency and uniformity, this filament is measured and cut while it's being produced. It's this kind of know-how that makes every type of IRC resistor your best buy. Send the coupon today for more facts.

How IRC provides unique reproducibility

FILM RESISTORS

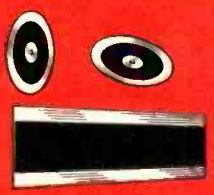
Type BT Fixed Composition Resistors

Type DC Deposited and Type BO Boron Carbon Resistors

Molded Type MD Deposited and Type MB Boron Carbon Resistors

Type HFR High Frequency Resistors

Type MV High Voltage Resistors

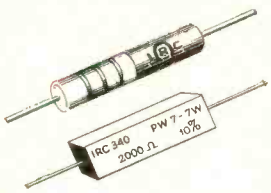


Resistance Strips and Discs

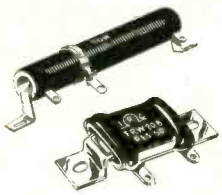
IRC film resistors exceed military specifications but the really outstanding thing is that they do it with unusual lot-to-lot uniformity in characteristics. What's the reason for this reproducibility? IRC's secret production processes!

You'll find this kind of production know-how in the making of Type DC Deposited Carbon Resistors, for example. The carbon used and the way the carbon film is formed both assure complete dispersion for better resistor performance. In IRC Boron Carbon Resistors, too, the urique method used to combine gases results in greater uniformity at low cost.

WIRE WOUND RESISTORS



Types BW and PW Low Power Wire Wound Resistors



Types PWW and FRW Power Wire Wound Resistors

Type WWJ Precision Wire Wound Resistors

"PH" Series Encapsulated Precision Resistors

Type CL Insulated Wire Wound Chokes

Type MW Bracket Mounted Resistors

IRC wire wound resistors are exceptionally uniform in their accuracy of adjustment and in characteristics making for long-term stability. The main reason is that they are all automatically machine wound under uniform tension and constant temperature and humidity conditions.

You can see the result of this superior winding skill in the element of the Type CL Insulated Choke, for example. Extremely fine wire is wound so expertly that the element appears to be one smooth, uninterrupted surface! This same winding skill also makes the element of all other IRC wire wound resistors a study in perfection—free from shorted turns or winding strains.

Insulated Composition Resistors • Deposited and Boron Carbon Precistors • Power Resistors • Voltmeter Multipliers • Ultra HF and Hi-Voltage Resistors.

Wherever the Circuit Says

Low Wattage Wire Wounds • Resistance Strips and Discs • Selenium Rectifiers and Diodes • Hermetic Sealing Terminals • Insulated Chokes • Precision Wire Wounds.

IRC®

HYCOR, Division of International Resistance Co., Sylmar, Los Angeles County, California

Subsidiaries:
Circuit Instruments Inc., St. Petersburg, Florida
Hycor Company, Inc., Vega Baja, Puerto Rico

INTERNATIONAL RESISTANCE COMPANY

Dept. 234, 401 N. Broad St., Philadelphia 8, Pa.
In Canada: *International Resistance Co., Ltd., Toronto, Licensee*

Please send technical bulletins describing ☐ Fixed Compositions ☐ Deposited and Boron Carbons ☐ High Frequency Types ☐ High Voltage Types ☐ Low Power Wire Wounds ☐ Power Wire Wounds ☐ Precision Wire Wounds ☐ Insulated Chokes ☐ Resistance Strips and Discs.

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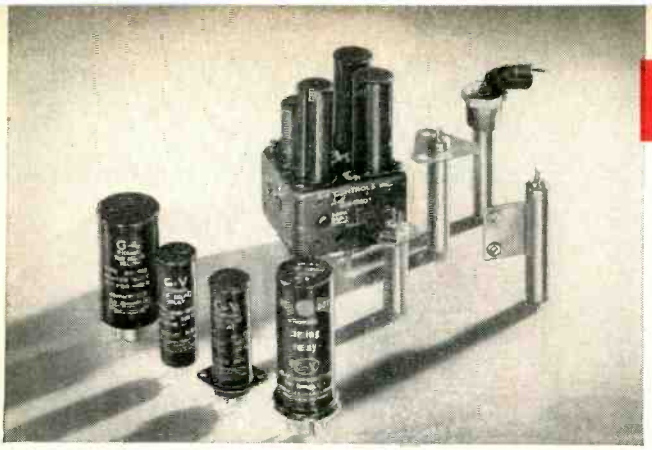
ADDRESS_____

CITY_____ **STATE**_____



THE G-V LINE—(l. to r.) Thermal Relays, a Thermal Relay Assembly, Sealed Thermostats. The complete G-V line, incorporating over 1,000 variations, covers more than 98% of all application requirements.

No. 1 of a series

Research and Engineering

What Makes G-V Controls

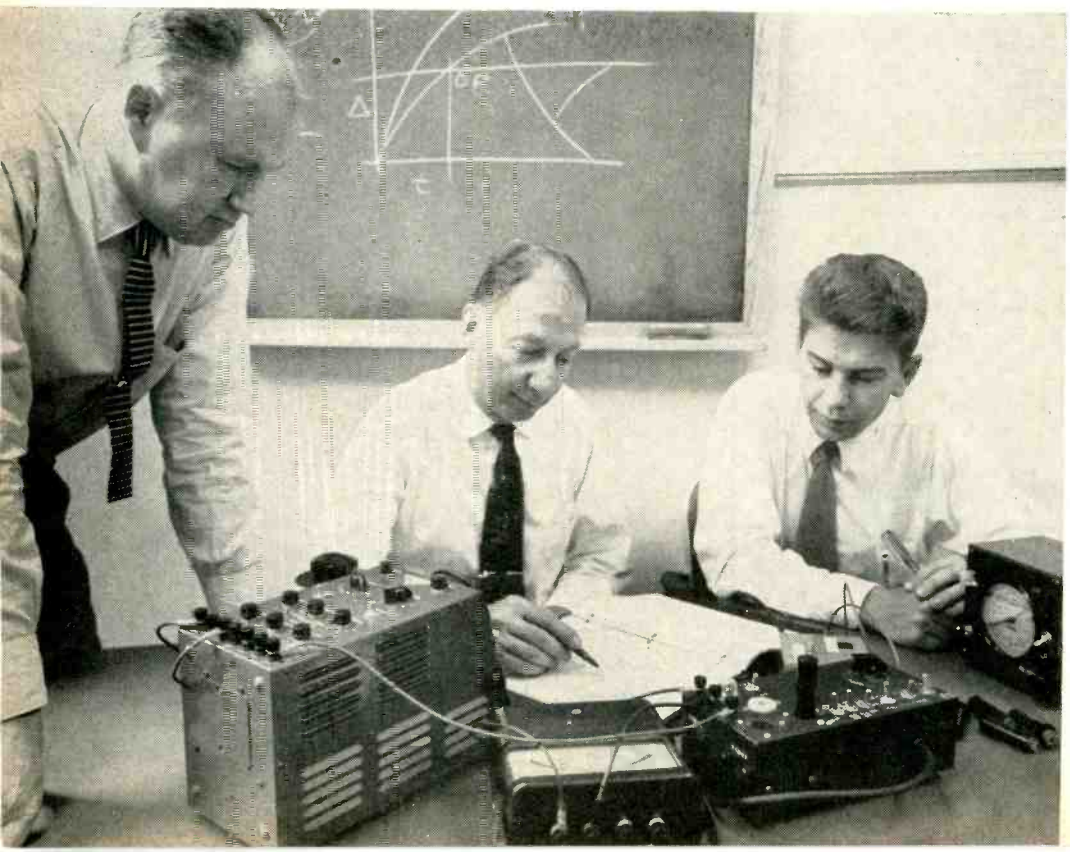
G-V TOPS IN THERMAL RELAY FIELD

In business as a producer of thermal relays and thermostats for less than 6 years, G-V Controls has already achieved the enviable position of undisputed leader in the design, development and manufacture of thermal relays. In the vast, competitive electronic industry, this can be considered an outstanding accomplishment.

G-V OFFERS UNIQUE FACILITIES

G-V Controls' rapid progress has been due in large measure to the highly competent personnel and modern equipment which it has devoted to the field of thermal relays. Its Engineering Staff has produced most of the recent technical advances in this field. Its Manufacturing Department has built a reputation for high quality and dependable deliveries. Its Field and Sales Engineering Organization is known throughout the country for helpful and intelligent cooperation. All of these facilities are freely available to our present and prospective customers. They can help you to make your products better.

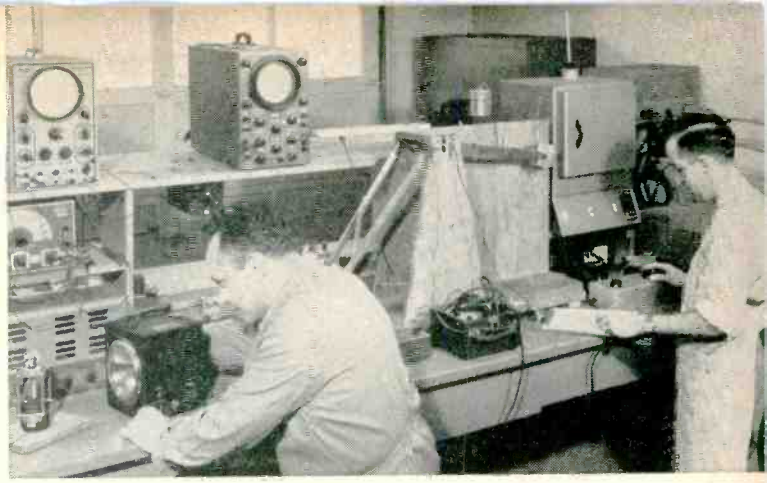
We give you on these pages a view of some of our Research and Engineering activities. Later in this series, we will feature Production and Sales and Field Engineering.



APPLICATION ENGINEERING

Every new relay application is studied by the Application Engineering Group. Complete operating data on over 1000 types and variations of thermal relays permits these men to recommend the best type and to predict its behavior.

Key spots open for engineers interested in going places with a young progressive organization.



RESEARCH and DEVELOPMENT—G-V Controls developed the first 7-pin miniature thermal relay, the first adjustable hermetically sealed thermal relay, the first hermetically sealed hot-wire relay. The precision and uniform characteristics of G-V's relays have qualified them for many uses new to relays of this type.

The Leader In Thermal Relays?

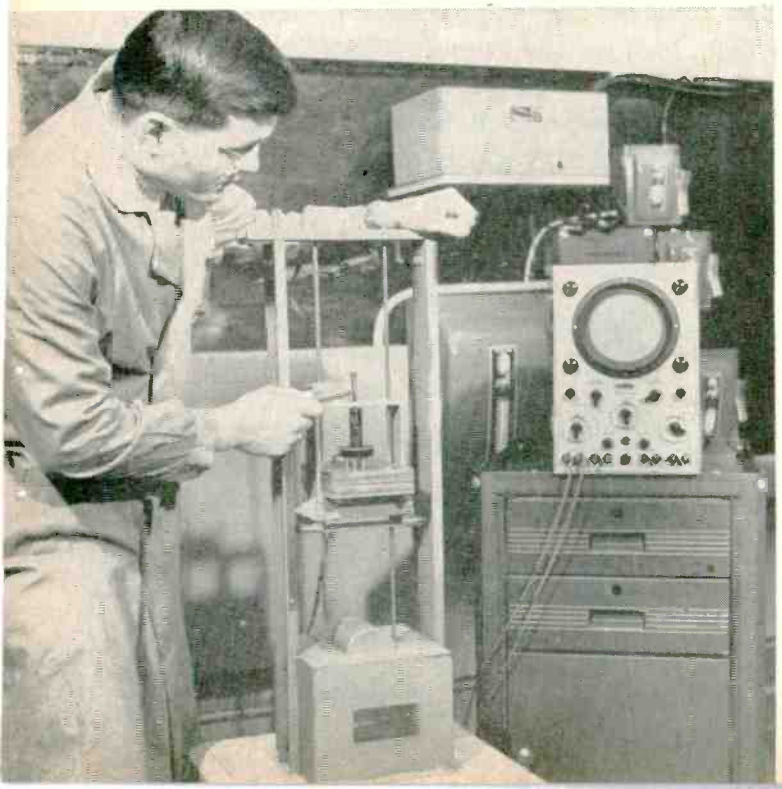
UNUSUAL APPLICATIONS are "bread-boarded" to duplicate conditions in users' equipment.

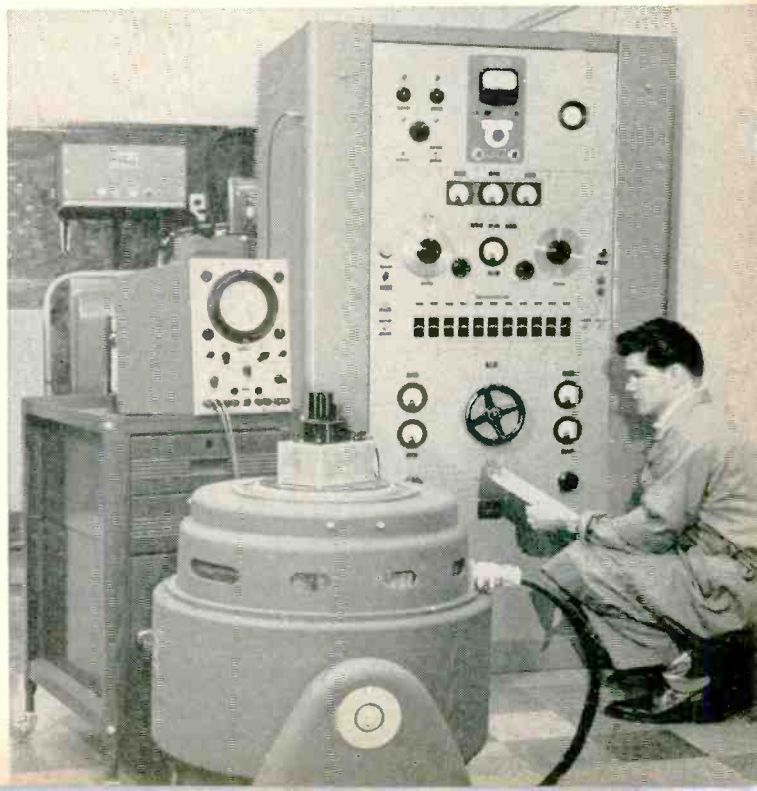
Complete catalog data is available.

G-V CONTROLS INC.

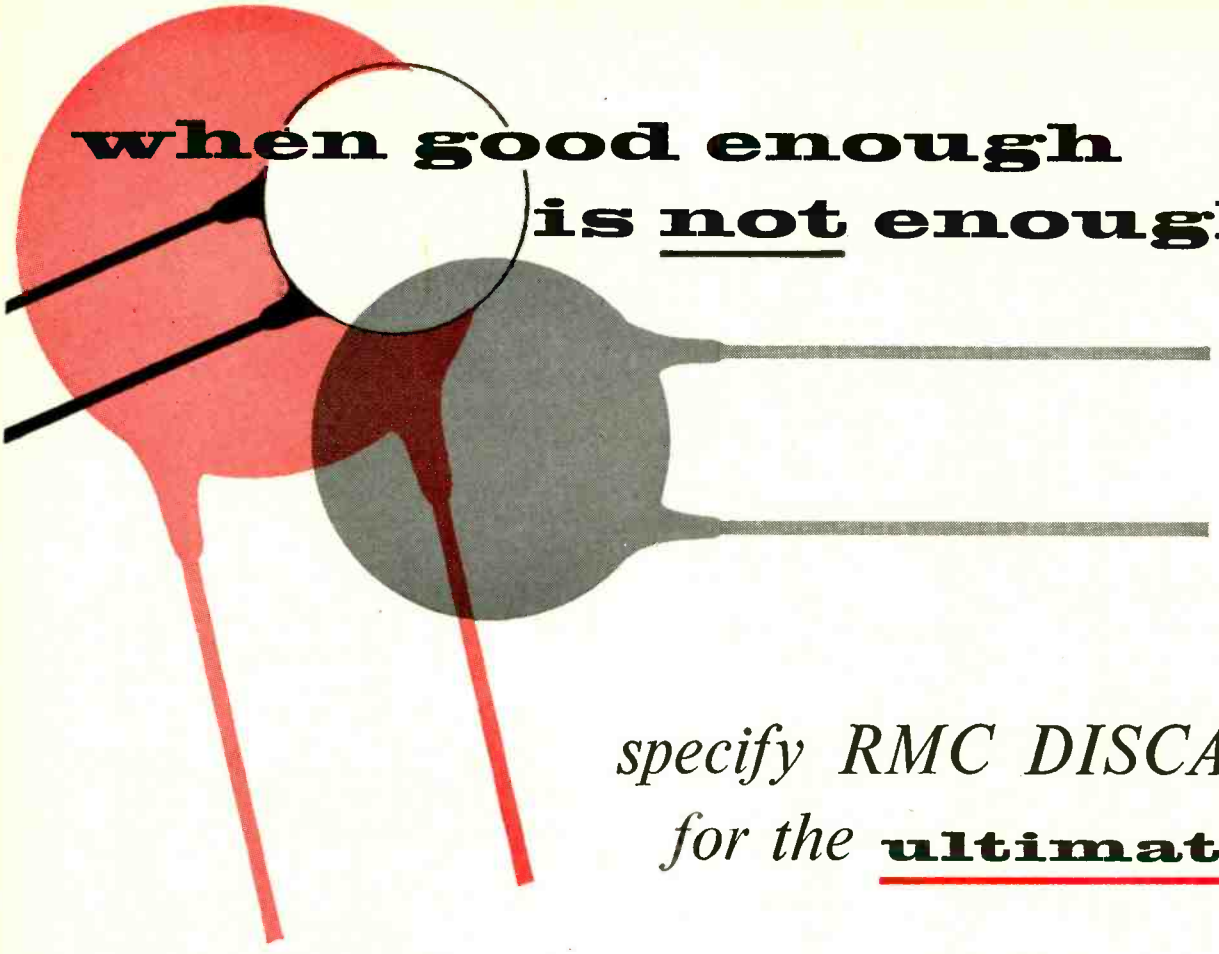
24 Hollywood Plaza, East Orange, N. J.

G-V ENVIRONMENTAL TEST LABORATORY—This modern laboratory, with all the newest testing equipment, assures the user of maximum reliability. Qualification tests to military requirements, followed by periodic quality control testing, guarantees continued reliability under extreme environmental conditions.

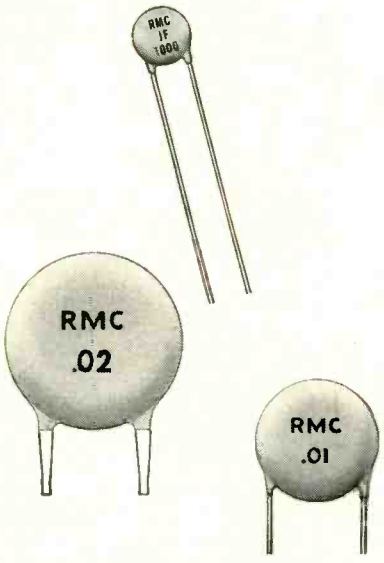




when good enough is not enough...



specify RMC DISCAPS for the **ultimate**



If you want to improve the quality of your electrical or electronic product you will do well to investigate the advantages of RMC DISCAPS. Modern research methods and strict quality controls have made DISCAPS the outstanding ceramic capacitors for a wide range of applications.

RMC offers standard temperature compensating, heavy duty, high voltage frequency stable, and temperature stable as well as special types. If you use ceramic capacitors look to RMC, DISCAPS are our only business.

Write for complete information on your company letterhead.

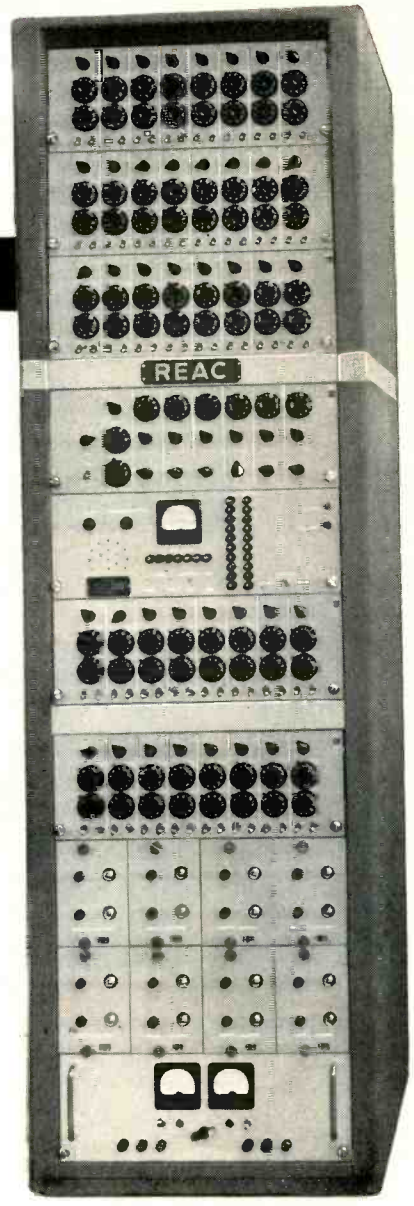
DISCAP CERAMIC CAPACITORS

RMC

RADIO MATERIALS CORPORATION
GENERAL OFFICE: 3325 N. California Ave., Chicago 18, Ill.
Two RMC Plants Devoted Exclusively to Ceramic Capacitors
FACTORIES AT CHICAGO, ILL. AND ATTICA, IND.

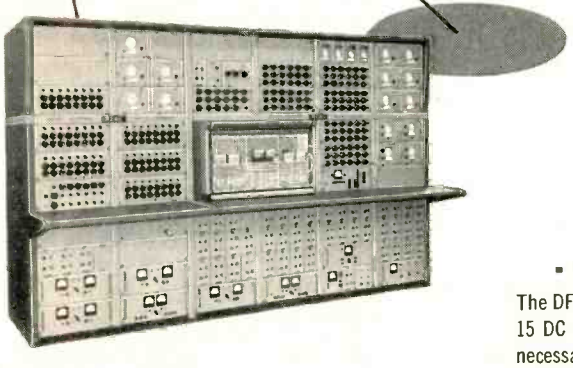
Generation of Functions of ***Two or More*** Variables

with the 400 series REAC®



DIODE FUNCTION GENERATOR

- Allows direct generation of slopes up to 12 volts/volt without paralleling diode segments.
- 10-turn potentiometers for both "slope" and "break point" give excellent resolution. Still further improvement in resolution is obtained by splitting slope adjustment into two ranges.
- 1000-division direct read-out 10-turn dials permit logging of function for fast reproduction later.
- Flexible switching system allows number of segments per channel to be varied from 2 to 30.
- Built-in calibration circuit permits functions to be set up quickly and easily without use of external plotting board.



. . . a complete self-contained unit

The DFG-401 is a completely self-contained unit consisting of 5 channels of function generation, 15 DC amplifiers (with VTVM and all control circuits for monitoring and balancing), and all necessary power supplies (except relay and reference voltages). In the event that any amplifiers supplied are not needed in the problem, they can be made available in groups at the patchbay as inverters with one gain of one.

This unit is ideal for the addition of up-to-date diode function generation equipment to an existing analog computer installation.

Electronic generation of functions of two or more variables is another outstanding Reeves contribution to the flexibility and efficiency of the electronic analog computer. Before installing new equipment, it will pay you to consult us. A comprehensive new REAC "400" series computer technical brochure will be sent upon request.

2RV57

Reeves INSTRUMENT CORPORATION

REEVES INSTRUMENT CORPORATION

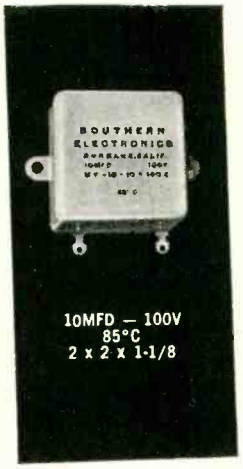
A Subsidiary of Dynamics Corp. of America, 201 East 91st St., New York 28, New York

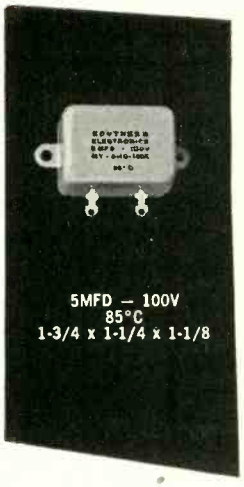
REAC Analog Computers

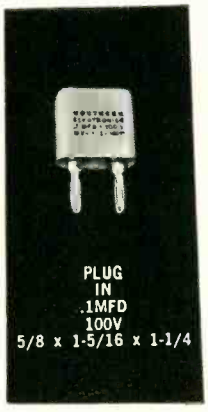
Precision Floated Gyros

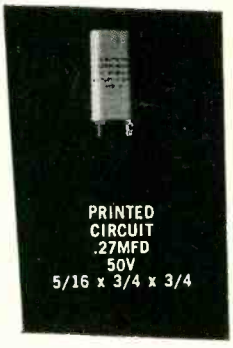
Precision Resolvers and Phase Shifters

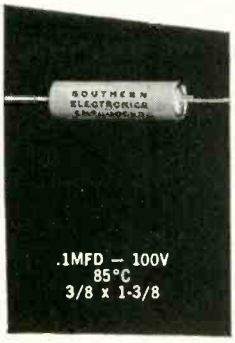
Servo Mechanical Parts











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- *Rated for infinite long life*
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Derated at 125°C as follows:
100 volts — 50%
200 volts — 50%
300 volts — 33⅓%
400 volts — 33⅓%
500 volts — 20%
600 volts — 16%

Tested and proved! Only Southern Electronics Corporation has developed a test procedure which insures built-in reliability! For your most exacting requirements—be sure—always specify S.E.C.

SUPER MYCON CAPACITORS

Tolerance to 1%—lowest temperature coefficient. Superior insulation resistance at high ambient temp. Good stability compatible with material.

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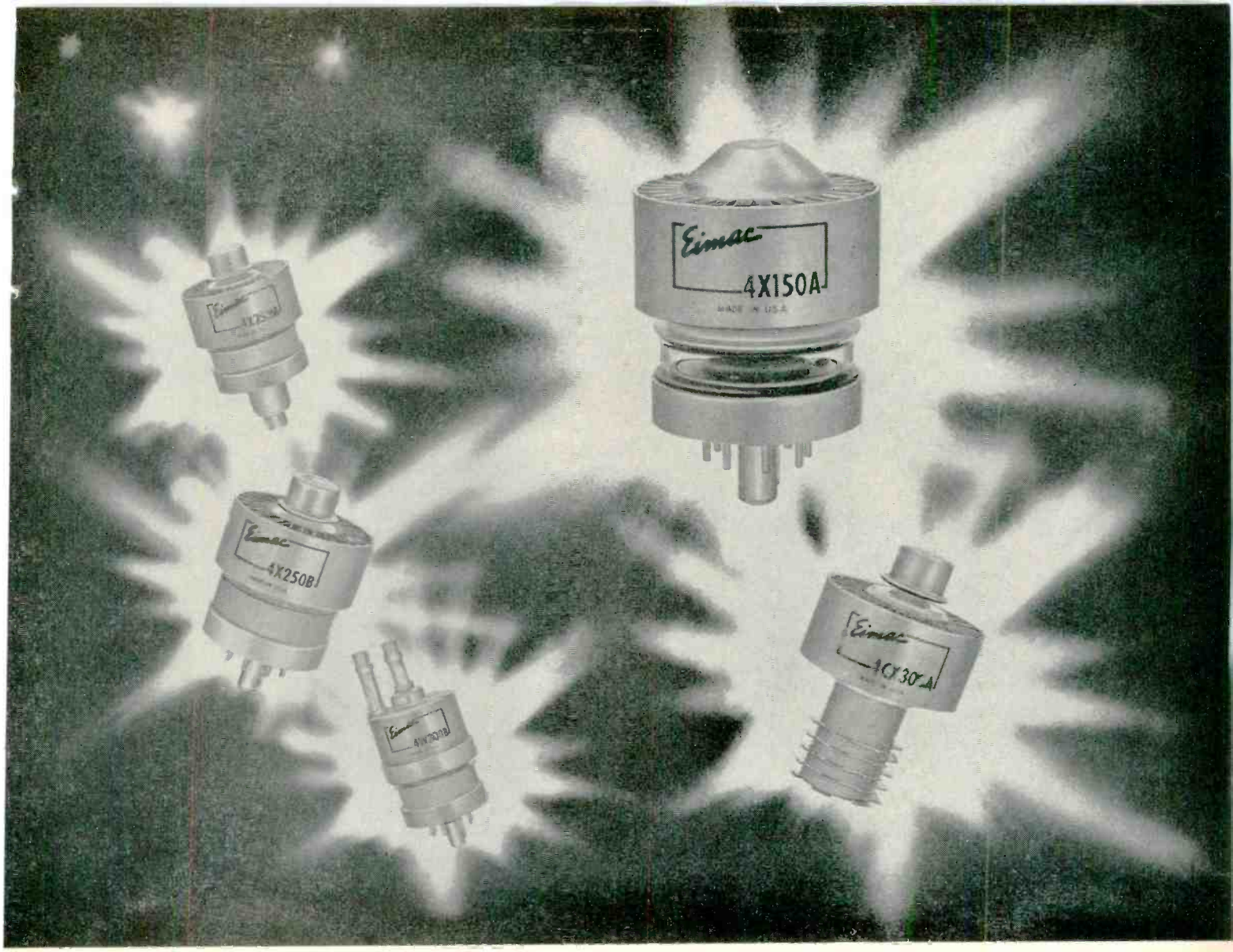
Wire, write or phone for complete catalog today!

SOUTHERN ELECTRONICS
Corporation

239 West Orange Grove Ave., Burbank, California

PIONEERS IN CUSTOM CAPACITOR ENGINEERING



Evolution at Eimac

Back in 1946 Eimac developed and produced the 4X150A—a new concept in power tetrodes. Its immediate acceptance by the industry then, has led to even more popularity now.

But today at Eimac the glass 4X150A is virtually obsolete.

Since 1946 Eimac has constantly improved the 4X150A to the point where it has evolved into a family of superior quality 250w and 300w tubes for operation to 500Mc. Small, compact structure has been retained. In fact, the 4X250 series is interchangeable with 4X150 tubes. Ceramic envelopes make possible greater mechanical strength, better production techniques, and higher temperature processing.

Because "good enough" has never been accepted at Eimac, however, this family of air cooled or water cooled, co-axial or conventional socketed tubes (2.5v, 6v, and 26.5v) is again accelerating the pace in quality, design, and performance, exactly as the 4X150A did a decade ago.

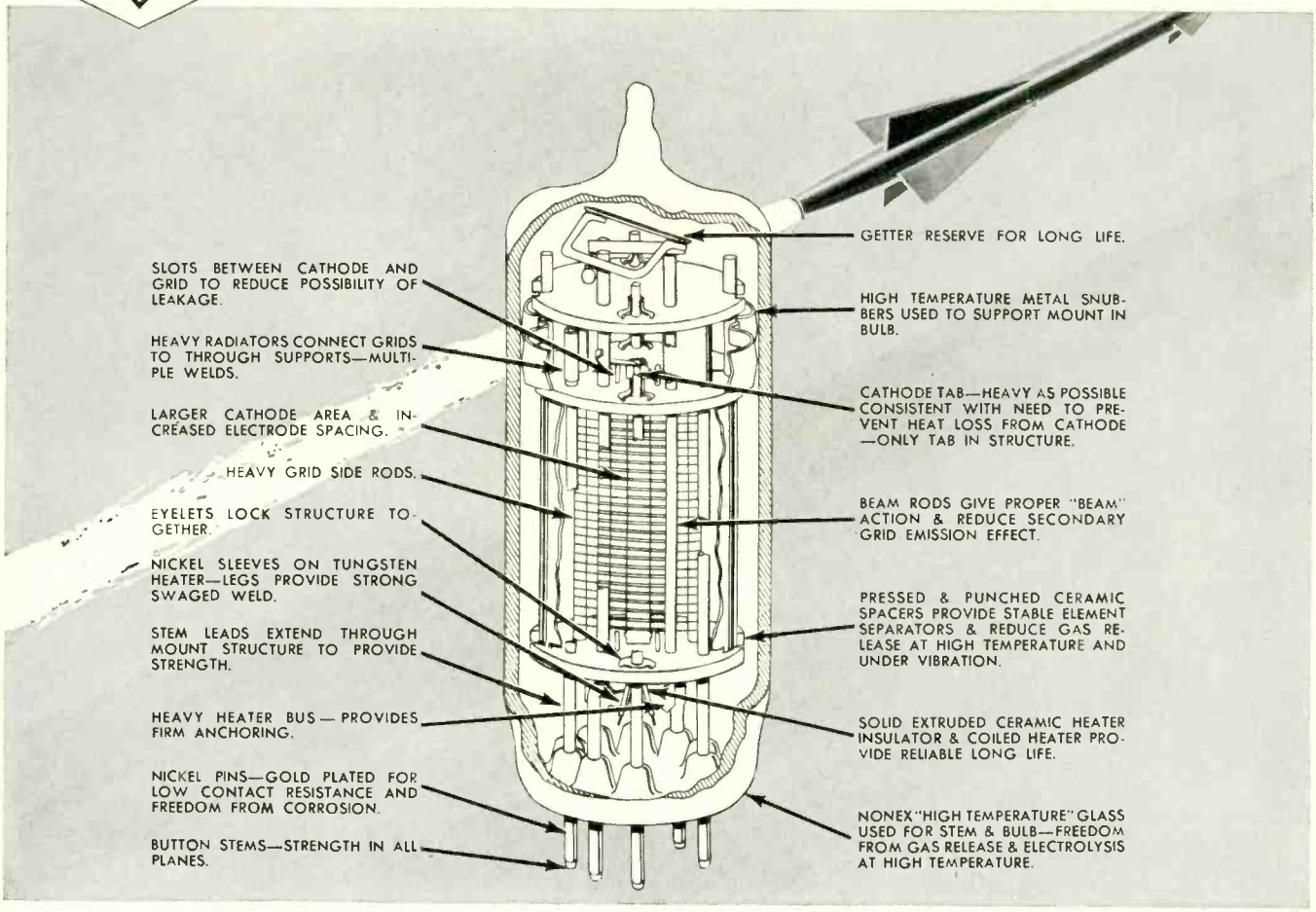
EITEL-McCULLOUGH, INC.
SAN BRUNO · CALIFORNIA
The World's Largest Manufacturer of Transmitting Tubes

Eimac

4X150A

4X150 Series	4W300 Series	4X250 Series	4CX300 Series
4X150A-1946	4W300B-1953	4X250B-1955	4CX300A-1956
4X150G-1949		4X250F-1955	
4X150D-1952		4X250M-1955	
		4CX250K-1956	

HY-G-300 **ELECTRON TUBES FOR SURVIVAL**



WHY BENDIX* HY-G-300 ELECTRON TUBES ARE BEST FOR EXTREME SHOCK, VIBRATION AND TEMPERATURES!

From the standpoint of design features (see above), these reliable hard glass tubes offer the superior quality needed to survive today's severe environmental demands.

Specifically, Bendix HY-G-300's are designed to withstand the following environmental conditions—bulb temperatures up to 300° C; vibration up to 20G's over the range of 5-2000 cycles; and shock of 200G's having 20-millisecond duration.

For full information about the HY-G-300 line . . . the surest answer to electron tube applications in jet aircraft, missiles and rockets . . . write RED BANK DIVISION, BENDIX AVIATION CORPORATION, EATONTOWN, NEW JERSEY. *TRADEMARK

West Coast Sales and Service: 117 E. Providencia, Burbank, Calif. • Export Sales and Service: Bendix International Division, 205 E. 42nd St., New York 17, N. Y. • Canadian Affiliate: Aviation Electric, Ltd., P. O. Box 6102, Montreal, Que.

HY-G-300 **TUBES ARE AVAILABLE FROM STOCK**

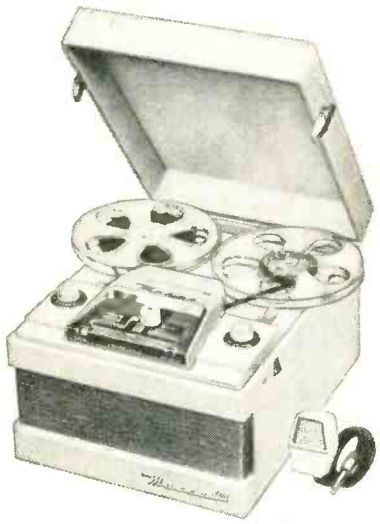
Bulb Size	Dbl. Triodes Volt Amp.	R. F. Pentodes	Gate Pentodes	Rectifiers FullWave	Beam Power	Power Triodes Passing
T-12	—	—	—	—	—	6080WB 6082A
T-11	—	—	—	—	6384 6889	—
T-9	—	—	—	6853	—	—
T-6½	6851 6854 6900	6582A	6486A	6754	6094	6877 6900

Retma Type No.	Retrofit For	Generic Type	E_f	I_f	Bulb	Bendix Type No.
6080WB	6080 6080WA	6080	6.3	2.5	T-12	TE-46
6094	—	6AQ5-6005	6.3	0.6	T-6½	TE-18
6853	6106 5Y3	5Y3	5.0	1.7	T-9	TE-45
6384	6AR6 6098	6AR6	6.3	0.9	T-11	TE-27
6854	6385	2C51 5670	6.3	0.5	T-6½	TE-47
6486A	6486	6AS6	6.3	0.25	T-6½	TE-43
6582A	6582	6AK5	6.3	0.25	T-6½	TE-44
6754	412A	—	6.3	1.0	T-6½	TE-36
6851	5751	—	6.3	0.5	T-6½	TE-42
6877	—	Half of 6080	6.3	0.8	T-6½	TE-48
6900	5687	5687	6.3	0.9	T-6½	TE-54
6889	—	—	6.3	0.9	T-11	TE-52
6082A	6082	6082	26.5	0.6	T-12	TE-55

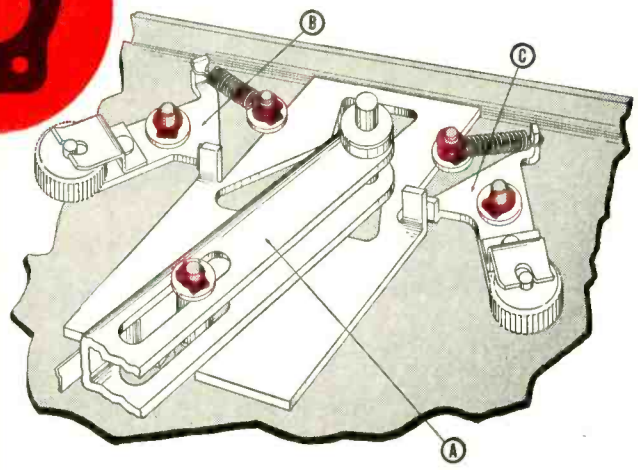
Red Bank Division

Bendix AVIATION CORPORATION

Waldes Truarc grip rings used on die-cast studs eliminate threading, tapping, other costly machining



Mark Simpson Manufacturing Co., Long Island City, N. Y., uses Waldes Truarc series 5555 Grip Rings to secure parts to studs of the zinc die-cast base of its "Masco 500" portable tape recorder.
The rings—which need no grooves—replace nuts, screws, cotter pins and other types of fastening devices which require threading, tapping, drilling and other expensive machining operations. Because a single cracked or broken stud would render the entire cast base useless—and with it, all assembly completed to that point—the rings also eliminate extremely costly rejects.



Pivot Assembly of shift lever (A) is secured by a single Waldes Truarc Grip Ring and washer. Because the washer must be installed over the shift level in a sliding fit, critical tolerances would have to be maintained if a screw or cotter pin were used. The Truarc Grip Ring eliminates that problem: it requires no groove and may be seated over the washer at any point on the stud, automatically compensating for accumulated tolerances in the parts. BRAKE ASSEMBLIES (B and C) use Grip Rings to secure the brake wheel and spring subassemblies. Here again problems of critical tolerances are avoided and expensive rejects eliminated.

Whatever you make, there's a Waldes Truarc Retaining Ring designed to improve your product... to save you material, machining and labor costs. They're quick and easy to assemble and disassemble, and they do a better job of holding parts together. Truarc rings are precision engineered and precision made, quality controlled from raw material to finished ring.

36 functionally different types... as many as 97 different sizes within a type... 5 metal specifications and 14 different finishes. Truarc rings are available from 90 stocking points throughout the U. S. A. and Canada.

More than 30 engineering-minded factory representatives and 700 field men are available to you on call. Send us your blueprints today... let our Truarc engineers help you solve design, assembly and production problems... without obligation.

For precision internal grooving and undercutting... Waldes Truarc Grooving Tool!

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Please send the new supplement No. 1 which brings Truarc Catalog RR 9-52 up to date.
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City..... Zone..... State..... EO29

WALDES TRUARC Retaining Rings, Grooving Tools, Pliers, Applicators and Dispensers are protected by one or more of the following U. S. Patents: 2,382,948; 2,411,426; 2,411,761; 2,416,852; 2,420,921; 2,428,341; 2,439,785; 2,441,846; 2,455,165; 2,483,379; 2,483,380; 2,483,383; 2,487,802; 2,487,803; 2,491,306; 2,491,310; 2,509,081; 2,544,631; 2,546,616; 2,547,263; 2,558,704; 2,574,034; 2,577,319; 2,595,787, and other U. S. Patents pending. Equal patent protection established in foreign countries.

need quick service on TIMERS for automatic control?

Time Delay Timers

The more automatic control problems we get, the better we like it. For while it's true each automatic control job is a bit different from the rest, the record shows that our 19 years of timer experience has given us the special knowledge it takes to give you the right answers, and in near-record time.

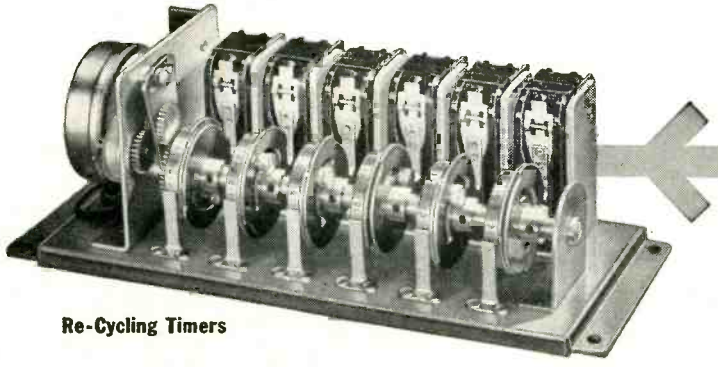
If one of our standard timers won't do your job — or one of the 721 combinations we have thus far developed from our 17 basic units — our engineers will go right to work to develop a new combination that's the one for you. That's the way we grow — and we like it.

We manufacture a complete line of timers in these 4 broad classifications:

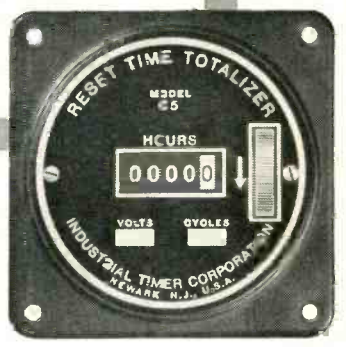
TIME DELAY TIMERS • INTERVAL TIMERS
RE-CYCLING TIMERS • RUNNING TIME METERS

And since we maintain large stocks of our 17 basic units, we can assure you of rapid deliveries — of excellent deliveries even on special orders. So whatever your automatic control problem, you have everything to gain by submitting it to our timer specialists. They'll give you a profitable answer — almost with the speed of automatic control itself.

Interval Timers



Re-Cycling Timers



Running Time Meters

Timers that Control the Pulse Beat of Industry

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The most important announcement

in modern oscillograph history...

the dramatic new Honeywell direct-recording

VISICORDER®

All at once you can *record* and *read the record* of the Visicorder. Using a completely new direct-recording principle, the Visicorder puts six channels on a direct-reading record at sensitivities comparable to photographic oscillographs, and at frequencies from DC to 2000 cps!

H
HONEYWELL

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THE **NEW** *VISICORDER,* perfected after years of research by the Heiland Division of Honeywell, combines the high frequency and high sensitivity characteristics of photographic oscillographs with the convenience of a direct-recording instrument.

By means of a completely new type of recording paper, light source, and optical system, the Visicorder makes use of mirror-type galvanometers to record phenomena from DC through 2000 cps *without* peaked amplifiers or other external compensation.

The record requires no liquids, vapors, powder magazines, or other processing materials. Development is accomplished by external light only as the record emerges from the oscillograph.

The Visicorder records are stable and require no further processing under normal conditions. They may be subjected to room light for extended periods without fading, and are permanent indefinitely when protected from light. Should it be necessary to subject the records to direct sunlight, they may be chemically "fixed" (in room light) using conventional photographic practices.

Visicorder records are reproducible by several methods using commercially available equipment.

Since the Visicorder operates on light-beam galvanometers, traces may deflect the full 6″ width of the chart, peak to peak, and their deflection is not limited by adjacent channels.

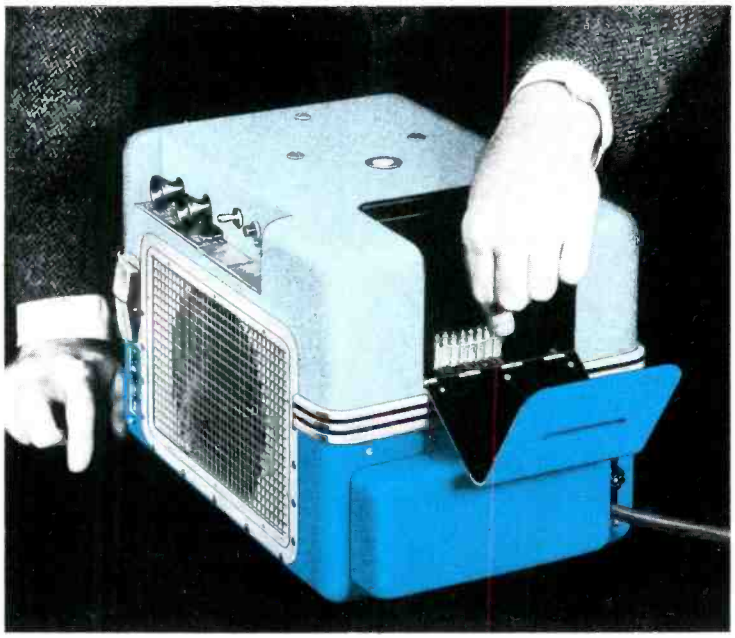
The remarkable exclusive features of the Visicorder make it the ideal recording oscillograph for applications where readable, permanent analog records are required and for additional uses where the measured phenomena need to be monitored or where immediate recorded results are desirable.

GENERAL FEATURES

FREQUENCIES	From DC to 2000 cps without peaked amplifiers or other compensation of any kind.
SENSITIVITIES	Comparable to photographic-type oscillographs.
RECORDING METHODS	Records directly on paper which requires no powder magazines, liquids, vapors, or other processing. Records are immediately visible and usable. Daylight loading. Accommodates recording paper 100 feet in length. Indicator shows unused recording paper available.
NO. OF CHANNELS	6 channels on 6″ wide paper plus provisions for two timing traces.
DEFLECTION	Full 6″ peak to peak. Traces may overlap; not limited by adjacent channels.
RECORD SPEEDS	0.2, 1, 5, and 25 inches per second, minute, or hour.
GALVANOMETERS	D'Arsonval-movement mirror galvanometers with choice of natural frequencies to suit individual requirements.
AMPLIFICATION	None required for most applications.
POWER	115 volt 60 cycle AC operation. 4 amperes.
DIMENSIONS	10″ height; 15″ depth; 10″ width.
WEIGHT	37 pounds, complete and ready to operate.
PRICE	$2,500.00, less galvanometers. Galvanometers $150.00 each.

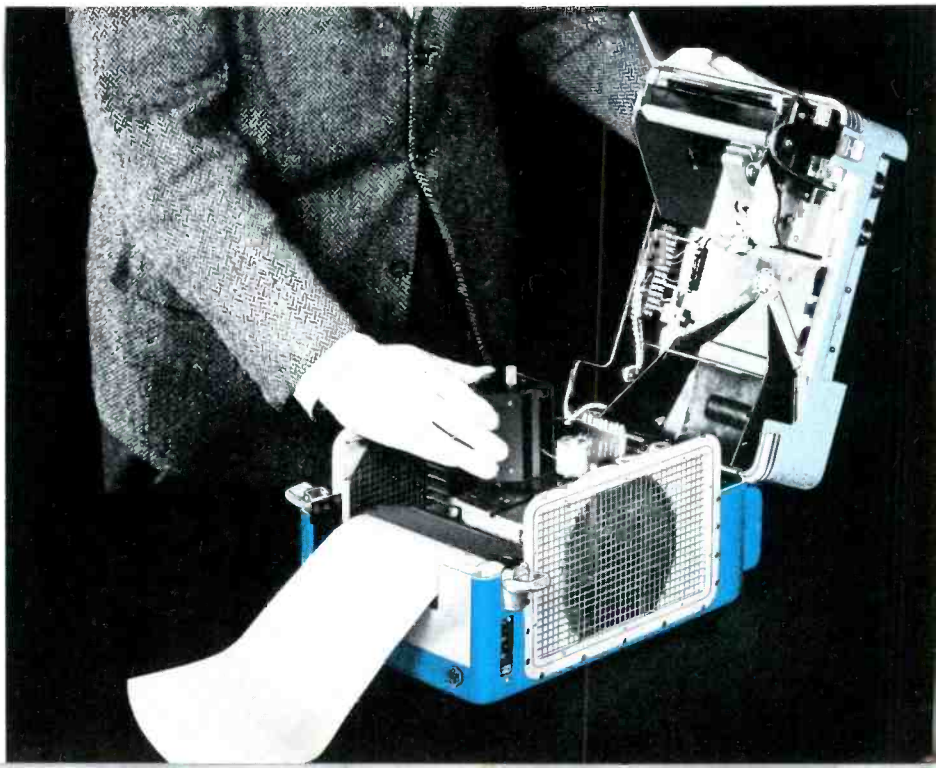
Deliveries starting January, 1957

1 *THE VISICORDER* is the first and only photographic-type oscillograph that can be loaded with recording paper in daylight. The paper speeds can be selected while the instrument is in operation. The light spots from the galvanometers are *visible from the exterior* at their point of contact with the paper; thus phenomena can be monitored simultaneously with their recording.



2 *GALVANOMETER ADJUSTMENTS* may be made through a panel-covered opening in the back of the instrument. Other operating controls —power on-off, lamp switch, paper drive and paper speed—are located on one convenient panel. Galvanometers are of the familiar Heiland solid-frame type: high sensitivity, accurate balance, high stability, low drift, in a versatile range of frequencies and sensitivities.

3 *SERVICE* on the Visicorder is extremely easy, since the instrument opens completely as shown. All components—galvanometers, recording lamp, transmission—are completely accessible.



VISICORDER® APPLICATIONS

The versatile Visicorder will fit almost unlimited applications because of its high frequency and sensitivity characteristics, and because of its ease of operation.

In any application where instantaneous monitoring is needed, whether or not a record is desired, the Visicorder is ideal.

★ **In CONTROL** applications the Visicorder will continually monitor and record reference and error signals, and present an immediately available recording of information.

★ **In NUCLEAR** applications, the Visicorder will monitor and record temperatures, pressures, and all other phenomena needed.

★ **In PRODUCTION TEST** applications, the Visicorder will provide a final dynamic inspection of electrical and mechanical devices such as motors, relays, generators, governors, solenoid valves, etc., where high frequency response has been required, but unavailable in the past.

★ **In COMPUTING** applications, the Visicorder will provide immediately-readable analog recordings representing dynamic solutions at much higher frequencies than have ever been available via pen—and-ink-type recorders previously used for this work.

★ **In PILOT and COMPONENT TESTING,** the Visicorder will accomplish more rapid evaluation of design and prototypes than any other direct-writing oscillograph available.

★ **In MEDICAL** applications the Visicorder is useful for dynamic blood pressures, electrocardiograms, EEG, and other physiological measurements.

★ **In all TEST** applications the direct-recording features of the Visicorder are invaluable. Where complex tests involve the assembly of considerable equipment and the gathering of personnel, the immediate Visicorder record will prove the success of the test at once before the test equipment is dispersed.

For further information about the Visicorder, contact the Minneapolis-Honeywell Industrial Division Sales Office nearest you. Sales-service facilities in over 130 principal cities throughout the world.

700-C Series Recording Oscillographs
Galvanometers
Bridge Balance Units
Amplifier Systems
HEILAND Photo-Flash Equipment

MINNEAPOLIS **Honeywell**

HEILAND INSTRUMENTS

5200 E. EVANS AVENUE • DENVER 22, COLORADO

in color tv, too

CRUCIBLE PERMANENT MAGNETS

for beam correctors, color purifiers and color equalizers give maximum energy . . . minimum size

Designers of electronic and control equipment can count on a *consistently higher* energy product with Crucible alnico magnets. *It means greater power from a minimum size magnet!*

And they're available in practically any size you want—from a fraction of an ounce to several hundred pounds. What's more, Crucible alnico permanent magnets can be sand cast, shell molded, or investment cast to your exact size, shape, or tolerance requirements.

Crucible has been a leading producer of these permanent magnets ever since alnico alloys were developed. And their manufacture is backed by over a half century of fine steelmaking experience. That's why so many magnet applications begin at Crucible.

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The Oliver Building, Mellon Square,
Pittsburgh 22, Pa.

CRUCIBLE first name in special purpose steels

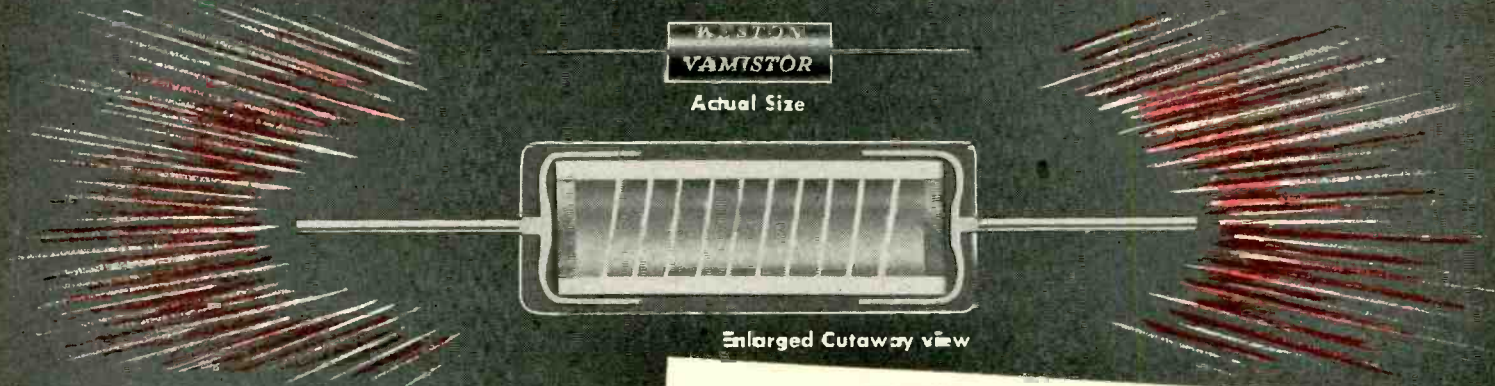
Crucible Steel Company of America

FOR HIGHEST STABILITY...

WESTON precision in a metal film resistor...

PRACTICALLY ZERO T.C.

FULL ½ WATT AT 125 C



Actual Size

Enlarged Cutaway view

The Weston VAMISTOR offers you many advantages over wire wound or conventional film resistors, in critical applications. It is a sealed, metal-film resistor that provides greater stability than all previous types. Following are a few of its outstanding characteristics:

- Stable under temperature, moisture and load life
- Stable under vibration, acceleration
- Non-inductive
- Noise free
- Excellent HF performance

As shown on table at right, VAMISTORS meet or surpass MIL specifications. They are now available in the following types:

	INITIAL TOLERANCE	TEMP. COEFF.
Model 9851 — ½ watt at 85C	1% or .5%	± 50 or ± 25 ppm
Model 9852 — ½ watt at 125C	1% or .5%	± 50 or ± 25 ppm
Model 9853 — 1 watt at 70C	1% or .5%	± 50 or ± 25 ppm

all models available in resistance values from 1000 to 100,000 ohms

For complete information on VAMISTORS, return the coupon today.

WESTON VAMISTOR PERFORMANCE DATA
COMPARED WITH SPECIFICATIONS FOR OTHER PRECISION TYPE RESISTORS

Characteristic	Vamistor production units	MIL-R-19074A (ships) Style RI-94	Wirewound MIL-R-93A Style RE-52 Char. A	Film MIL-R-10509B Style RN-70 Char. A
Short Time Overload 2.5 Times—10 sec	Average + .01% Low .00% High − .06%	.5% max.	.5% max.	.75% max.*
Load Life 1000 hrs—85 C	Average + .15% Low + .10% High + .20%	.5% max.	.5% max	1.0% max.**
Low Temperature −65 C—24 hours	Average .00% Low .00% High + .02%	.5% max.	(no test)	1.0% max.
Moisture Resistance MIL-STD-202, Method 106	Average − .03% Low − .15% High + .36%	.5% max.	1.0% max.	3.0% max.
Salt Water Immersion 0 to 85 C—5 cycles	Average − .04% Low + .02% High − .10%	.5% max.	.5% max.***	(no test)
Temperature Cycle −55 to 85 C—5 cycles	Average + .04% Low + .02% High + .07%	.2% max.	.2% max.	1.0% max.
Insulation Resistance 100 v d-c	Greater than 10,000 megohms	10⁶ megohms min.	50 megohms min	10,000 megohms min.
Dielectric Strength 900 v rms—1 minute	Below measurable value—all samples	.05% max.	.05% max.	.5% max
Terminal Strength		.5% max.	(no limit)	.5% max
Effect of Solder		.5% max.	(no test)	.5% max.

*MIL-R-10509B test 2.5 times—5 seconds **MIL-R-10509B test at 70 C ambient
***MIL-R-93A test not cycled, 25 C—24 hours

Weston Electrical Instrument Corp.
617 Frelinghuysen Ave., Newark 2, N.J.

Rush me full particulars on WESTON precision metal film resistors.

Name _____

Company _____

Address _____

_____

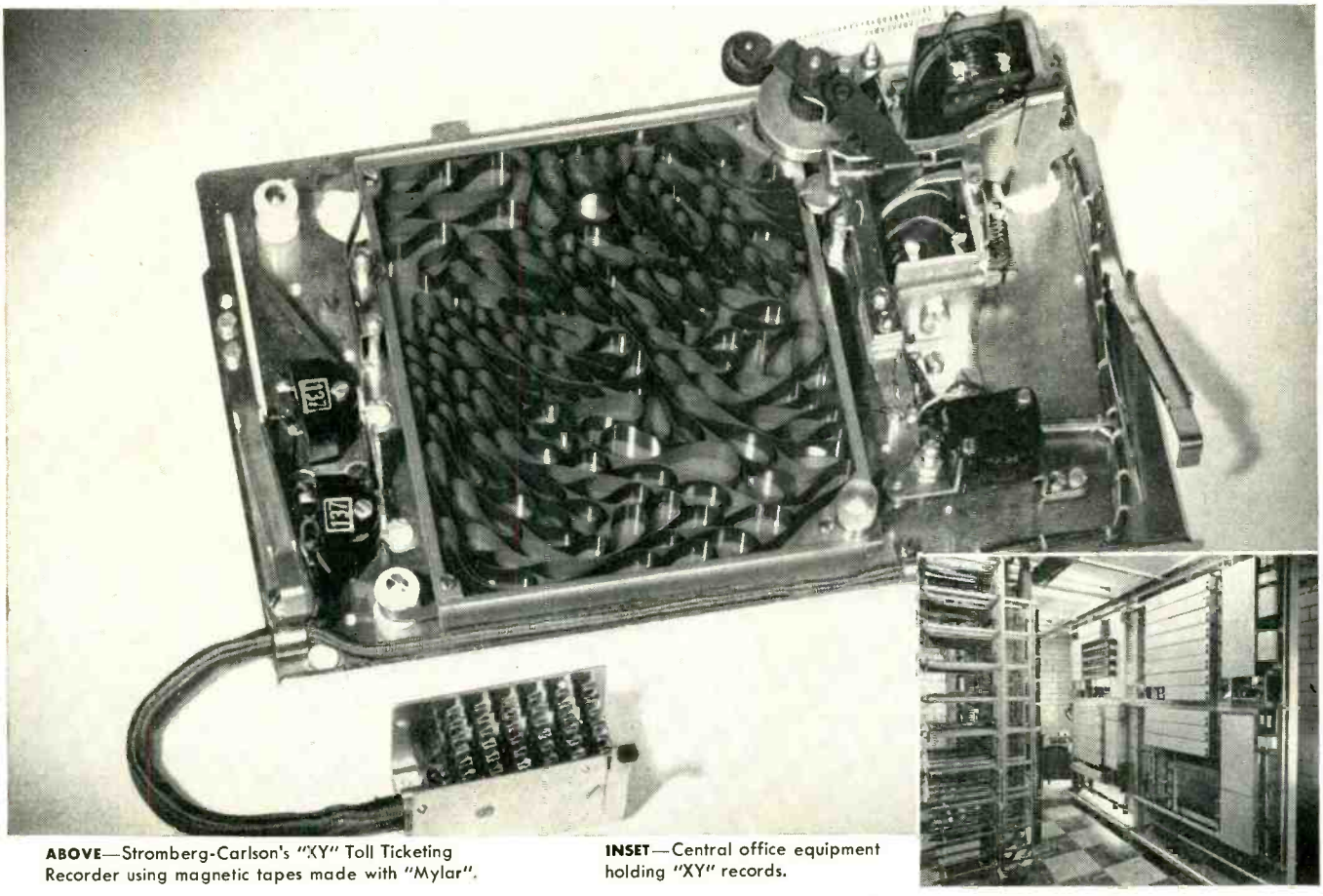
WESTON VAMISTORS

precision metal film resistors

A DAYSTROM UNIT

New Stromberg-Carlson equipment speeds up telephone service...cuts cost!

Heart of system is automatic recorder using tape made of Du Pont "Mylar"



ABOVE—Stromberg-Carlson's "XY" Toll Ticketing Recorder using magnetic tapes made with "Mylar".

INSET—Central office equipment holding "XY" records.

Thanks to Stromberg-Carlson's new "XY" Toll Ticketing system, independent telephone companies are now able to speed up service while cutting equipment and operational costs.

The system works like this: When a customer dials, all pertinent data—such as numbers involved, rate and duration of call—is recorded on magnetic tape formed into an endless loop in its own magazine. The tape, 35 feet long, holds up to 50 completed calls. When the "read-out" equipment is ready, the recorded information is translated into impulses that actuate billing equipment.

Why tape made with "Mylar"?

"We selected magnetic recording tape made with 'Mylar'* polyester film after a long period of testing," reports Mr. J. D. McKay, design engineer of Stromberg-Carlson, division of General Dynamics Corporation. "We had to be sure the tape was tough enough to withstand the grueling stops and starts of the recorder. We had to be sure the tape was dimensionally stable—not be affected by humidity. But, most important, the tape had to be economical—it had to provide long-lasting service with a minimum number of magazine changes."

This is but one of the hundreds of new uses industry has found for magnetic recording tape made with "Mylar". Computer manufacturers, geologists, audio and video engineers for TV broadcasting, archivists, and guided missile manufacturers are switching to recording tapes made with "Mylar" because of thinner tape, better performance and longer life. If you're interested in more information on "Mylar"—or how tapes made with "Mylar" can help you speed up service while cutting costs—send in coupon below.

**Du Pont manufactures the base material "Mylar"—not finished magnetic recording tape.*
"Mylar" is a registered trademark for Du Pont's brand of polyester film.

DU PONT
REG. U. S. PAT. OFF.

BETTER THINGS FOR BETTER LIVING
... THROUGH CHEMISTRY

DU PONT MYLAR® POLYESTER FILM

E. I. du Pont de Nemours & Co. (Inc.), Film Dept.
Room E-2, Nemours Bldg., Wilmington 98, Delaware

☐ Please send your booklet outlining advantages of magnetic recording tape made with "Mylar".

☐ Please send your booklet listing properties, applications and types of "Mylar" available.

Name _____

Firm _____

Address _____

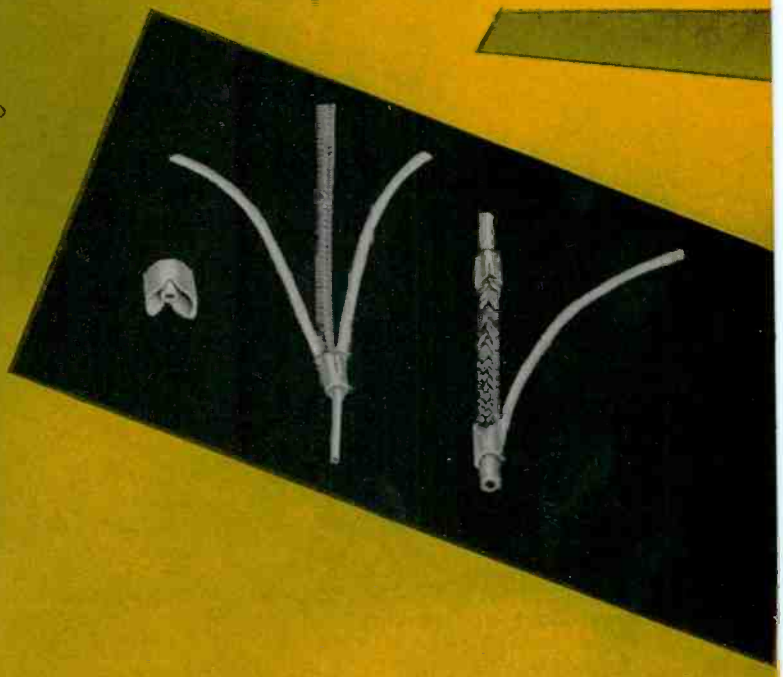
City _____ State _____

Want more information? Use post card on last page.

application time cut to a

SHIELDED WIRE SPLICES and

for the aircraft and

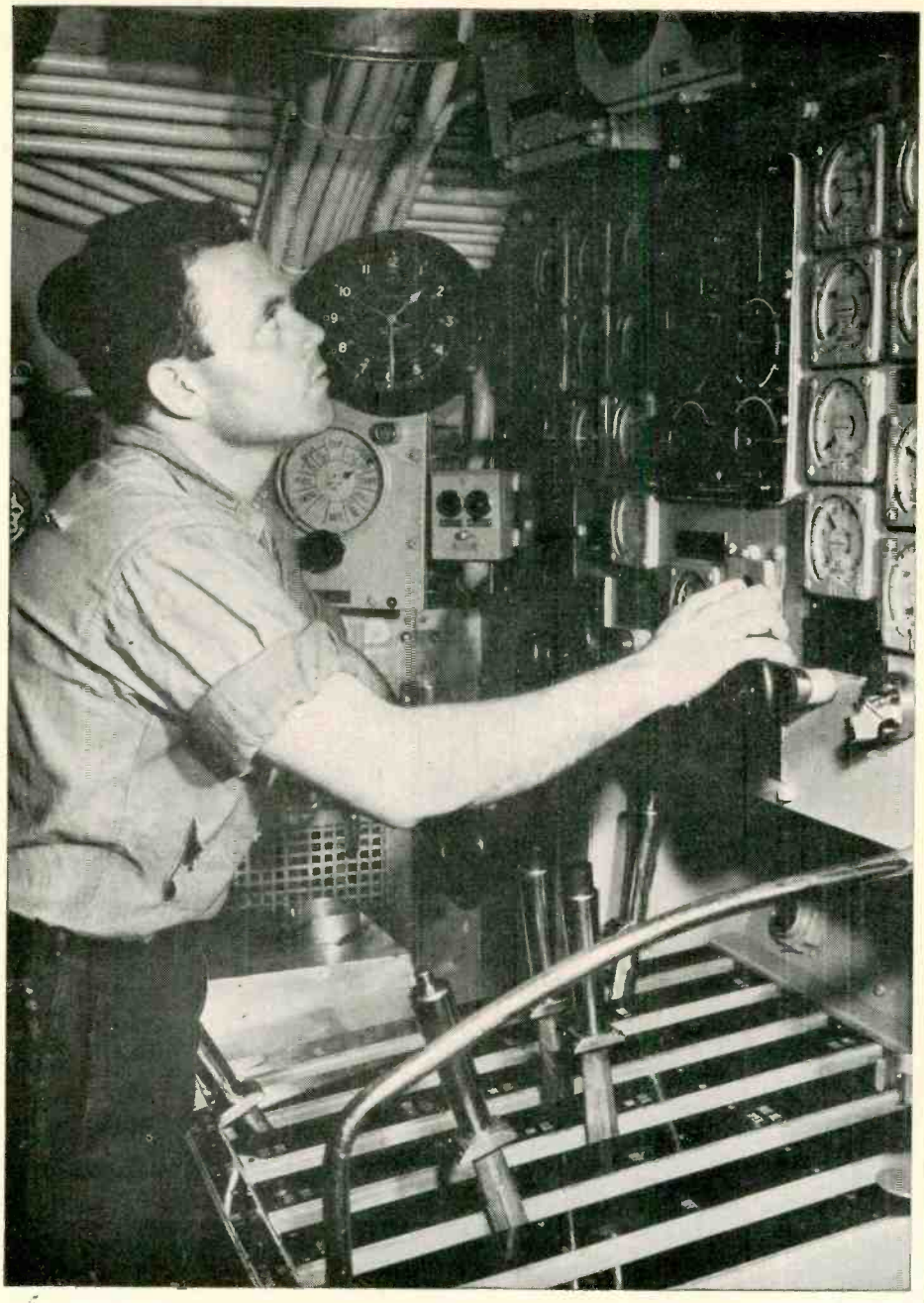


This newest team of A-MP connectors is crimped onto shielded wires making permanent mechanical and electrical connections. More than three and one-half years of engineering and development have gone into these new A-MP shielded wire parts, with advantages that minimize application time and costs. There are no loose pieces required to make connections. A splice between two shielded wires is completed by crimping the connector on each end with a recommended A-MP hand crimping tool or appropriate power tooling. Grounding connections are made with the Shielded Wire Ferrule and similar tooling.

The new A-MP Shielded Wire Connectors and Shielded Wire Ferrules incorporate several new features which facilitate inspection and selection of the proper connector and ferrule. These are: color coding to identify wire sizes and inspection ports to establish definitely and positively the depth of the braid which is enclosed after crimping.

A rectangular window in the center of the Shielded Wire Splice enables the operator or inspector to see at a glance if the ends of the inner conductors are properly placed.

The new A-MP Shielded Wire team proves to be the answer to faster, more compact splicing with resultant superior performance.



Meters tell the tale but SPECIAL ELECTRICAL ALLOYS do the work

"Steelmaker to the Electrical Industry" is a title we have earned the hard way . . . by the sweat of research and pioneering development. In this modern world of gauges and instruments, of automation, electronics and atomics, the heart of the design is so often some silicon steel, high-permeability alloy, or other special electrical material that we produce. ● When *you* need a steel to do what ordinary steels cannot do—whether electrically or in resisting corrosion, heat, wear or great stress, call on us. *Allegheny Ludlum Steel Corporation, Oliver Bldg., Pittsburgh 22, Pa.*

STEELMAKERS to the Electrical Industry

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Warehouse stocks of AL Stainless Steels carried by all Ryerson plants

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STEELS FOR THE ELECTRONIC AGE

Write for **"MAGNETIC MATERIALS"**

This 32-page book contains valuable data on all Allegheny Ludlum magnetic materials, silicon steels and special electrical alloys. Illustrated in full color, includes essential information on properties, characteristics, applications, etc. Your copy gladly sent free.

ADDRESS DEPT. E-86

POWER TRANSISTORS

Clevite Power Transistors are used in leading auto radios.

- High power ratings
- High power gain
- Rugged, compact mechanical design
- Welded, hermetically sealed package for stability and long life
- Excellent heat dissipation characteristics

Now Clevite can supply you with power transistors that fit your needs for audio applications, portable power supplies, etc., from a full line of six types. All are available in production quantities. All are rated at 25 watts continuous operation with infinite heat sink — 15 watts with 36 sq. in. heat sink.

Clevite Power Transistor packaging is compact. Vacuum baking and hermetic sealing of the package insure stability and long life. Low thermal resistance between collector junction and large copper flange insures excellent heat conduction from the package to the heat sink.

OUTLINE SPECIFICATIONS

TYPE	2N268	CTP 1111	2N257	CTP 1104	CTP 1109	CTP 1108	Units
Instantaneous Collector-to-Base Voltage (absolute maximum)	−80	−80	−40	−40	−20	−20	Volts
Junction Temperature (absolute maximum)	85	85	85	85	85	85	°C
Average Total Power Dissipation (with inf. heat sink @ 25°C)	25	25	25	25	25	25	Watts
Average Total Power Dissipation (with 36 sq. in. heat sink @ 25°C)	15	15	15	15	15	15	Watts
Power Gain	28[a]	23[a]	30[a]	23[a]	27[b]	20[b]	db
Frequency Cutoff	6	4	7	4	6	4	kc/s

a V_{cc} = −14V; I_c = 500 ma; R_L = 30 Ω (choke coupled); R_g = 10 Ω

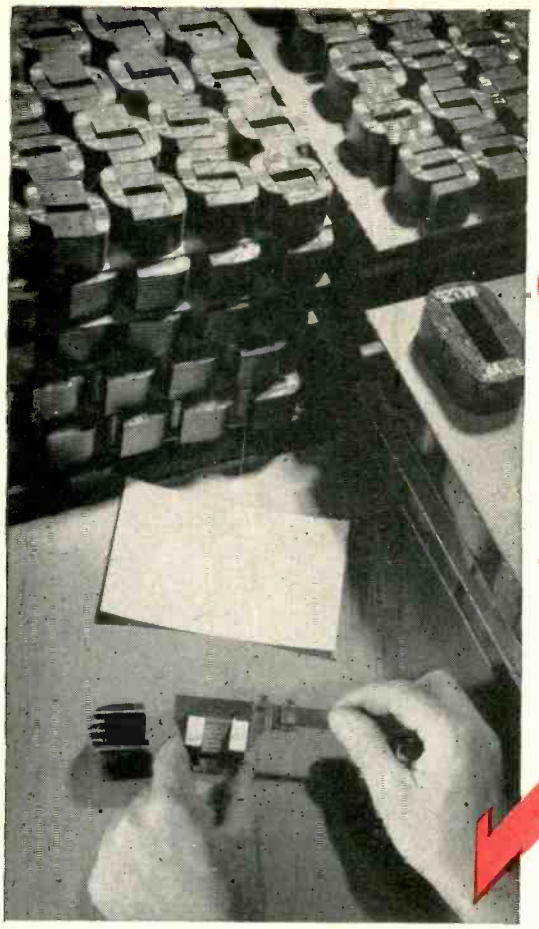
b V_{cc} = −7V; I_c = 500 ma; R_L = 15 Ω (choke coupled); R_g = 10 Ω

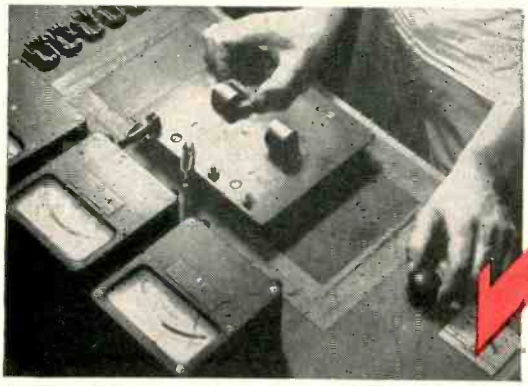
CLEVITE TRANSISTOR PRODUCTS

241 Crescent St., Waltham 54, Mass. TWinbrook 4-9330

Write for Data Sheet B-211

Clevite Divisions: Brush Electronics Co. • Cleveland Graphite Bronze Co. • Clevite Harris Products Inc. • Clevite Research Center • Clevite Ltd.





MOLONEY HyperCore ELECTRONIC CORES

Check and double Check

HyperCore Electronic Cores measure up to the highest standards of quality and performance. One check is not enough . . . each core undergoes at least two rigid inspections. The first makes certain that it is of the specified size . . . and the second determines that finished cores have the desired electrical qualities. All HyperCore electronic cores *must* test well within industry tolerances. Special tests for specific operating conditions can be made also if desired.

These tests are the real proof of the superior fabrication which combines the finest materials with superior "know how". Result; electronic cores that give better performance . . . have greater flux carrying capacity and lower losses. And since Moloney HyperCore Electronic Cores are wound cores of cold-rolled oriented silicon steel, they are smaller and lighter.

ME86-17

Specify HyperCore Cores for smaller, low loss transformers

Write for Catalog SR 206 "HyperCores for Magnetic Components" and Catalog ST 3506 "Magnetic Components for Electronic Applications."

MOLONEY ELECTRIC COMPANY

Plate and Filament Transformers • Chokes • Unit Rectifiers • Modulation Transformers and Reactors • Pulse Transformers and Charging Chokes • HyperCores for Magnetic Components Developmental Magnetic Components • Power and Distribution Transformers

SALES OFFICES IN ALL PRINCIPAL CITIES • FACTORIES AT ST. LOUIS 20, MO. AND TORONTO, ONT., CANADA

DESIGN PROBLEM:

MORE RECTIFIER POWER PER INCH OF SPACE...

SOLVED AT LOWER COST—

with greater reliability—by this new General Electric High Current Silicon Rectifier

Packing *greater* rectifying capacity into *less* space—with maximum reliability and efficiency—is becoming standard practice with General Electric Silicon Rectifiers. And the cost of these G-E High Current Silicon Rectifiers, with their unmatched performance, is now actually less than that of comparable rectifying devices.

REQUIRE MINIMUM SPACE

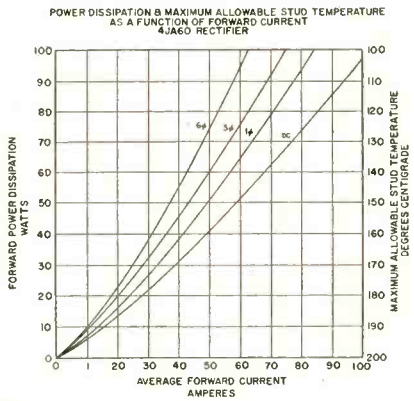
The Silicon Rectifier pictured here in full size has ratings up to 85 amps... yet measures less than 1⅝ inches in diameter. It operates, or can be stored, safely at temperatures from 200° to −65° centigrade and checks out above 99% in efficiency. Maximum peak inverse voltage is 300. Silicon rectifiers of higher ratings are on the way.

Produced by the alloy technique developed in General Electric laboratories, these high-capacity rectifiers show no deterioration in rectifier characteristics during extended life tests at full rated condition. The silicon element is hermetically sealed in a steel housing for protection against moisture, fumes, dust, vibration, and corrosion. Effective cooling is assured by the tapered thread "plumbing type" stud that screws tight into heat sink or cooling fin.

WORK ANYWHERE... ON ANY APPLICATION

General Electric Silicon Rectifiers are installed in any position or location, and work in any rectifier operation. They are now serving in many applications such as arc furnaces, welding, and protection against cathodic erosion.

They are available now in different voltage ranges, and meet rigid military specifications. For detailed information, consult your local General Electric representative, or write to *General Electric Company, Semiconductor Products, Section S2527, Electronics Park, Syracuse, New York.*



TYPICAL APPLICATION GENERAL ELECTRIC HIGH CURRENT SILICON RECTIFIER

CIRCUIT	Three Phase Bridge Rectifier, Resistive Load.
DC OUTPUT	280 Volts, 215 amperes, 60 kilowatts.
RECTIFIER LOSSES	Approximately one percent (½ kilowatt).
COOLING REQUIRED	One 6½-inch square, ⅛" thick copper fin for each of six rectifying units when used with 2000 fpm 30°C forced air. Free convection cooling may be utilized by increasing the fin area.
VOLUME	Total volume of rectifiers and fins—less than ⅓ of a cubic foot.

CUSTOMER CONFIDENCE 10th ANNIVERSARY SEMICONDUCTOR PROGRESS

Progress Is Our Most Important Product

GENERAL ELECTRIC

FROM DATA TO DIGITS...

Today Hughes is developing systems which convert radar data and other information to digital form and process it for use in performing control functions.

These systems will be able to receive and store vast quantities of data from many different sources and distribute it, after processing, over large and complex ground nets.

Special-purpose digital computers are employed, utilizing magnetic drum memory and novel programming techniques. The systems will also include visual displays and employ the latest concepts of human engineering to simplify equipment operation and minimize the possibility of human error. Vacuum tubes are being replaced by transistors or ferrite cores in flip-flops, registers, and amplifiers; and diode matrices are being replaced by ferro-magnetic circuitry.

These and other features of the new systems promise to maintain and extend Hughes leadership in the fields of digital computers and processing systems. In order to design and build these and future systems, Hughes requires engineers with experience in electronic circuit design, logical design, electronic packaging, radar systems, and many others.

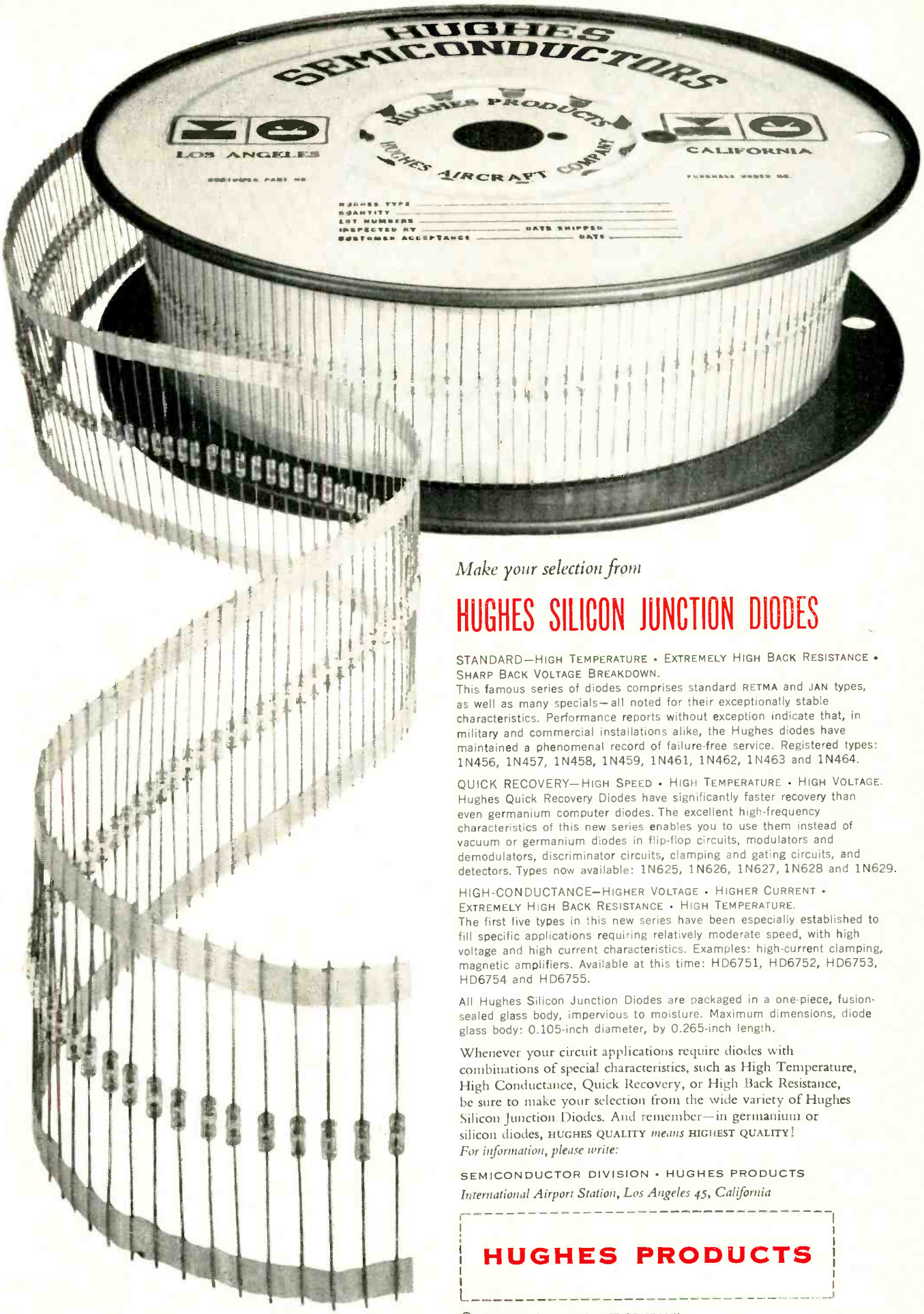
For further information write us at the address below.

HUGHES

RESEARCH AND DEVELOPMENT LABORATORIES

SCIENTIFIC STAFF RELATIONS

Hughes Aircraft Company, Culver City, Calif.



Make your selection from

HUGHES SILICON JUNCTION DIODES

STANDARD—HIGH TEMPERATURE • EXTREMELY HIGH BACK RESISTANCE • SHARP BACK VOLTAGE BREAKDOWN.
This famous series of diodes comprises standard RETMA and JAN types, as well as many specials—all noted for their exceptionally stable characteristics. Performance reports without exception indicate that, in military and commercial installations alike, the Hughes diodes have maintained a phenomenal record of failure-free service. Registered types: 1N456, 1N457, 1N458, 1N459, 1N461, 1N462, 1N463 and 1N464.

QUICK RECOVERY—HIGH SPEED • HIGH TEMPERATURE • HIGH VOLTAGE.
Hughes Quick Recovery Diodes have significantly faster recovery than even germanium computer diodes. The excellent high-frequency characteristics of this new series enables you to use them instead of vacuum or germanium diodes in flip-flop circuits, modulators and demodulators, discriminator circuits, clamping and gating circuits, and detectors. Types now available: 1N625, 1N626, 1N627, 1N628 and 1N629.

HIGH-CONDUCTANCE—HIGHER VOLTAGE • HIGHER CURRENT • EXTREMELY HIGH BACK RESISTANCE • HIGH TEMPERATURE.
The first five types in this new series have been especially established to fill specific applications requiring relatively moderate speed, with high voltage and high current characteristics. Examples: high-current clamping, magnetic amplifiers. Available at this time: HD6751, HD6752, HD6753, HD6754 and HD6755.

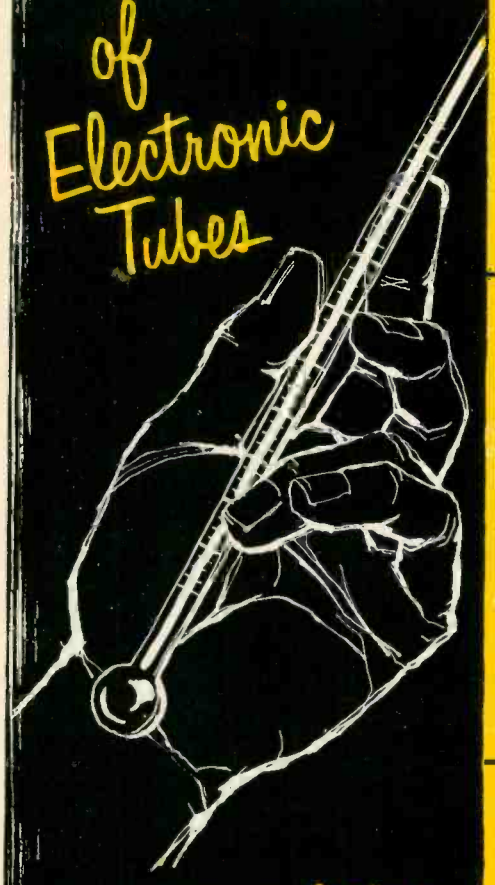
All Hughes Silicon Junction Diodes are packaged in a one-piece, fusion-sealed glass body, impervious to moisture. Maximum dimensions, diode glass body: 0.105-inch diameter, by 0.265-inch length.

Whenever your circuit applications require diodes with combinations of special characteristics, such as High Temperature, High Conductance, Quick Recovery, or High Back Resistance, be sure to make your selection from the wide variety of Hughes Silicon Junction Diodes. And remember—in germanium or silicon diodes, HUGHES QUALITY *means* HIGHEST QUALITY!
For information, please write:

SEMICONDUCTOR DIVISION • HUGHES PRODUCTS
International Airport Station, Los Angeles 45, California

HUGHES PRODUCTS

LIQUID COOLING of Electronic Tubes



WITH Eastern COOLING UNITS

By a sustained program of research, Eastern continuously extends the uses of the latest units in electronic tube cooling, pressurizing electronic equipment, and pumping fuels and hydraulic fluids. Research and testing laboratories, a model shop, and three manufacturing plants provide the specialized equipment and manpower to turn out fully qualified units to meet appropriate government specifications.

From our extensive line of existing units, adaptations of these units, or completely new designs, Eastern can provide equipment to handle your project well. Your inquiry is welcomed.

EASTERN INDUSTRIES, INC.
100 SKIFF STREET
HAMDEN 14, CONNECTICUT

Eastern Cooling Units provide coolant liquid for maintaining within safe operating temperature limits liquid cooled electronic tubes or similar devices. The units are completely self-contained and usually comprise such components as heat exchangers, fans or blowers, liquid pumps, reservoirs, flow switch, thermostat, etc.

Cooling units can be modified as required for varying conditions encountered in land or sea as well as aircraft service. Almost all units are designed to meet such specification as MIL-E-5400 and MIL-E-5272.

The units shown below are intended only to illustrate the varying requirements which can be satisfied. By utilizing fairly standard components and designs based on broad experience in this field, Eastern is able to provide at minimum cost equipment exactly suiting a specific requirement.

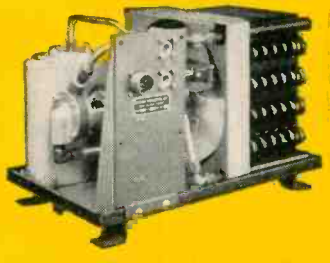
Eastern welcomes your consultation on liquid cooling problems ranging from 200 to 20,000 watts dissipation.

Write for Aviation Products Bulletin 330.

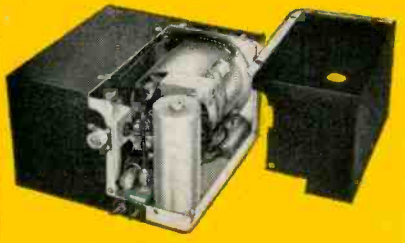
MODEL MB-175, TYPE 200 DISSIPATION: 2,000 watts. ALTITUDE RANGE: sea level to 50,000 feet. POWER REQUIRED: 28 volts D.C. WEIGHT: 25 pounds. SIZE: 10" x 15-15/16" x 10¾" high.

MODEL E/HT-205, TYPE 200A DISSIPATION: 1600 watts. ALTITUDE RANGE: sea level to 5,000 feet. POWER REQUIRED: 28 volts D.C. WEIGHT: 25 pounds. SIZE: 10" x 21" x 10" high.

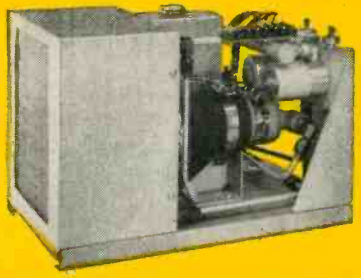
MODEL MB-177, TYPE 202 DISSIPATION: 1700 watts. ALTITUDE RANGE: sea level to 50,000 feet. POWER REQUIRED: 110 volt, 400 cycle, 3 phase. WEIGHT: 27 pounds. SIZE: 10" x 19 15/32" x 7⅝" high, per JAN-C-1720A, size B1-D1.



MODEL E/HT-210, TYPE 200 DISSIPATION: 1500 watts. ALTITUDE RANGE: sea level to 10,000 feet. POWER REQUIRED: 208 volts, 400 cycle, 3 phase. WEIGHT: 35 pounds. SIZE: 11¼" x 19½" x 12½" high.



MODEL E/HT-200, TYPE 201 DISSIPATION: 1,000 watts. ALTITUDE RANGE: sea level to 50,000 feet. POWER REQUIRED: 28 volts D.C. WEIGHT: 14½ pounds. SIZE: 10" x 10" x 6" high.



MODEL NO. 5-A DISSIPATION: 1,000 watts. ALTITUDE RANGE: sea level to 5,000 feet. POWER REQUIRED: 100 to 110 volts D.C. WEIGHT: 10 pounds. SIZE: 7⅞" x 13½" x 9-1/16" high.

ANDREW HIGH GAIN ANTENNA IS

RUGGED, DEPENDABLE

Says William E. Whiting,
Director of Communications,
Kern County, California

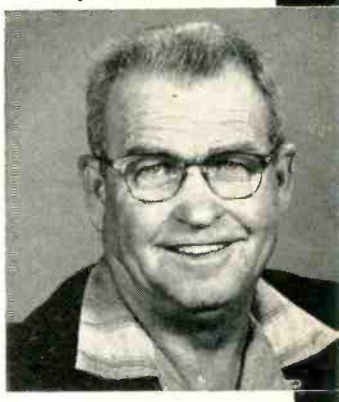
RADIO COMMUNICATIONS DEPARTMENT

Telephone 3-1788 or
3-7671 — Ext. 2300

William E. Whiting
Director of Communications
Mailing Address
P. O. Box 643
Bakersfield

COUNTY OF KERN · STATE OF CALIFORNIA

BAKERSFIELD, CALIFORNIA



Andrew Corporation
363 East 75th Street
Chicago 19, Ill.

Gentlemen:

The County of Kern has, for the past 27 months, had two of your type 3000 Antennas installed on a mountain top at an elevation of 4,853 feet. At this location, during the winter months, there is a great amount of ice and sleet and, at times, the wind reaches velocities approaching 100 m.p.h.

There have been times when there was a build-up of ice on these antennas to such a degree that the elements were entirely enclosed in the ice formation and the total thickness of the antenna was approximately 30". Even under these conditions there was little noticeable signal attenuation. In periodic physical checks of these antennas, we have been unable to find any broken or damaged elements, loose connections or clamps—something that might be expected from the strain of expansion and contraction together with action of high wind velocities at this location.

These antennas have given such complete satisfaction that we are ordering two additional for our new installation which will be at 7,500 feet elevation on Breckenridge Mountain, where snow, ice and wind conditions will be as severe as any encountered in California. We are confident that they will give as good service as they have at the lower elevation.

Yours very truly,

William E Whiting

William E. Whiting, Director of Communications
County of Kern

ANDREW

Type 3000A antenna for 148-174 mc range has 6.3 db gain. Omnidirectional with vertical polarization—eliminates high angle (wasted) radiation . . . Multiplies the effective power of base and mobile transmitters.

Other high gain antennas with db gains up to 7.6 are available for 400-420 and 450-470 mc ranges.

For complete information on Andrew Antenna systems, write for Communication Antenna Folder — No. 15C.

Andrew
CORPORATION
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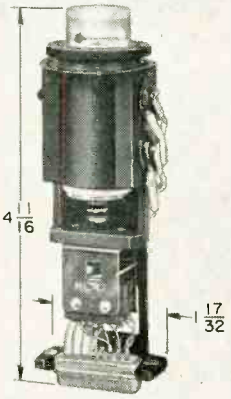
Offices: New York · Boston · Los Angeles · Toronto

Switches have uses unlimited

H HONEYWELL

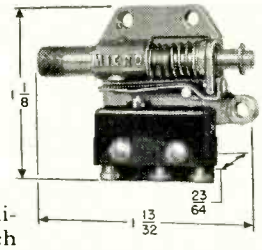
3-LIGHT PUSH BUTTON SWITCH FOR COMPLEX CONTROL PANELS



Here is a new, unique indicating push button switch which lights in three different colors. It is the latest MICRO SWITCH development for use in complex console panels. This compact assembly is ideal for applications where absolute dependability is required. It has a reliable operating life through hundreds of thousands of operations. Use is simplified by a pre-wired connector plug.

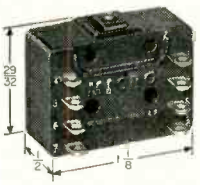
(Send for Data Sheet 110)

SUBMINIATURE SAFETY SWITCH DEVICE FOR HAZARDOUS EQUIPMENT



This MICRO SWITCH Subminiature door interlock switch assembly is designed for use as a safety device on such hazardous equipment as radio, radar, and X-ray cabinets. Installed on the cabinet door the switch automatically cuts off the power circuit when the service door is opened. Assembly shown uses a MICRO SWITCH Subminiature basic switch with single-pole, double-throw contact arrangement.

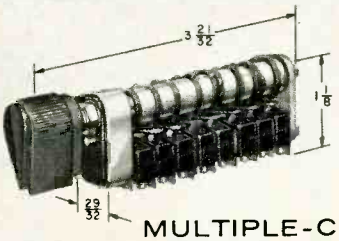
(Write for Data Sheet 108)



FOUR-CIRCUIT SWITCH FOR CONTROL OF COMPLEX CIRCUIT

Here is a four-circuit double-break switch for simultaneous control of four isolated circuits. This small switch is ideal in complex circuit applications where space and weight are prime factors in switch selection. Two snap-action springs are operated with each actuation of the plunger. This provides quick make and break of the contacts in each of the four double-break circuits. Electrical rating is 10 amperes 115-230 volts a-c; 10 amperes 30 volts d-c.

(Write for Catalog 78)

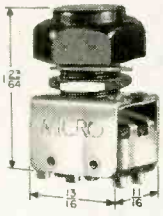


SUBMINIATURE ROTARY SELECTOR SWITCH FOR MULTIPLE-CIRCUIT CONTROL

This assembly is an 8-gang, 8-position rotary selector switch. It consists of 8 single-pole, double-throw Subminiature basic switching units operated by cams on a common shaft. Any combination of the 8 basic switching units may be actuated in any of the 8 positions if cams are set to specifications at the factory. Variations with from 2 to 8 single-pole, double-throw basic switches are available.

(Write for Catalog 75 "Subminiature Switches")

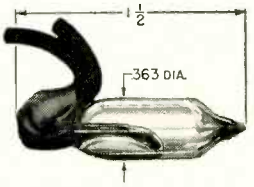
SEALED PUSH BUTTON SWITCH FOR PANEL MOUNTING APPLICATIONS



This MICRO SWITCH push button switch for panel mounting is outstanding because of its very small size and ease of installation. After the push button is mounted on a panel, the switching unit can be wired and then easily snapped into place on the end of the button assembly behind the panel. In addition, the push button is sealed to keep dirt and moisture from penetrating to the back of the panel. Switch has operating force of 3 lbs., weighs but .05 lbs.

(Write for Catalog 75 "Subminiature Switches")

SMALL HONEYWELL MERCURY SWITCH MEETS SMALL LOAD CIRCUIT DEMANDS



The small Honeywell Mercury Switch shown here is especially designed for reliable service in low-energy circuits. This switch meets the requirements of applications where space and economy are critical factors. Mercury switches are widely used in animated displays, control and indicating devices, home freezer units, alarms and hundreds of other tilt-motion, low-force applications. Ratings available down to micro-volt, milli-ampere ranges.

(Write for Catalog 90 on "Mercury Switches")

MICRO SWITCH, a division of Honeywell, is the pioneer in the manufacture of precision snap-action switches.

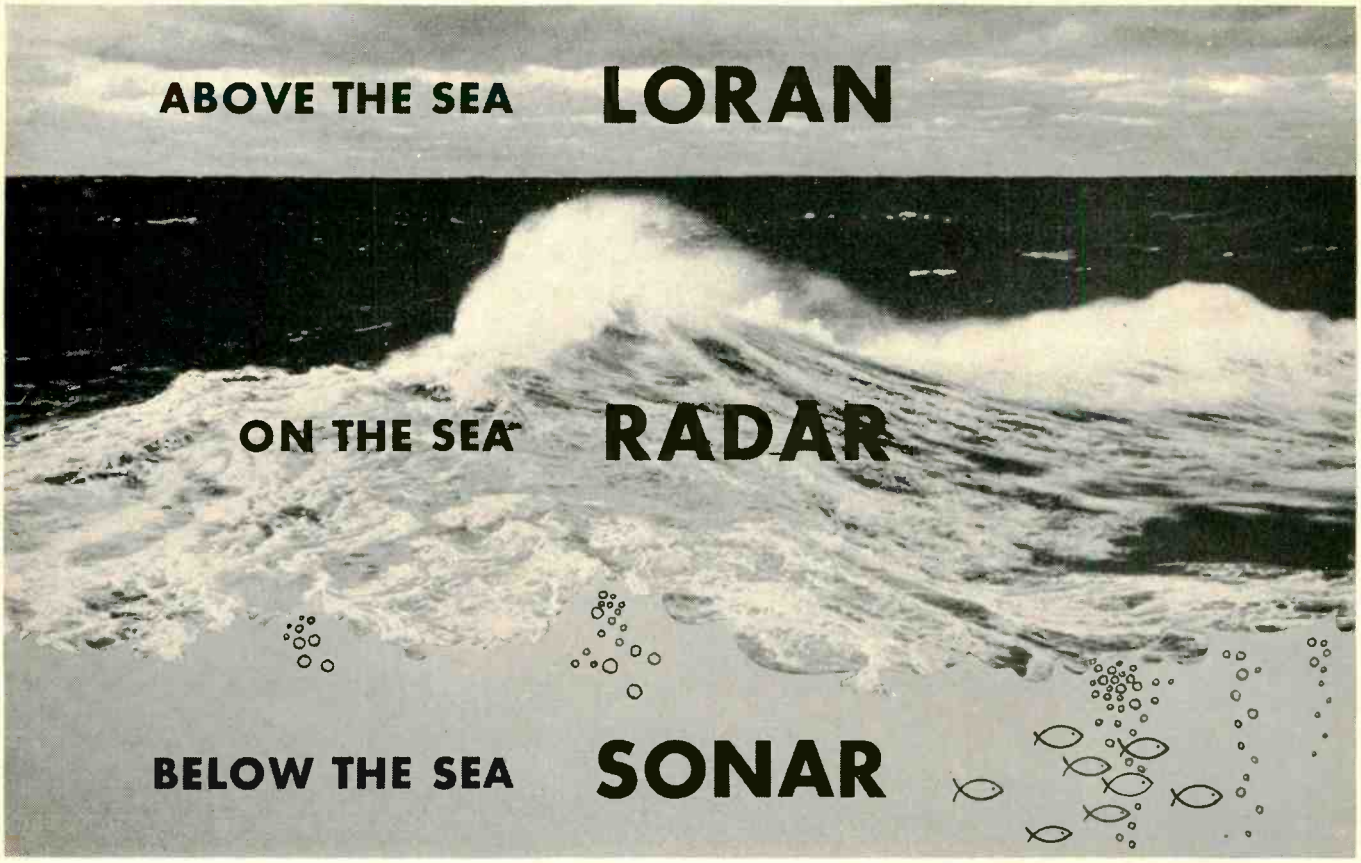
MICRO SWITCH

A DIVISION OF MINNEAPOLIS-HONEYWELL REGULATOR COMPANY

H HONEYWELL

In Canada, Leaside, Toronto 17, Ontario • FREEPORT, ILLINOIS

Want more information? Use post card on last page.



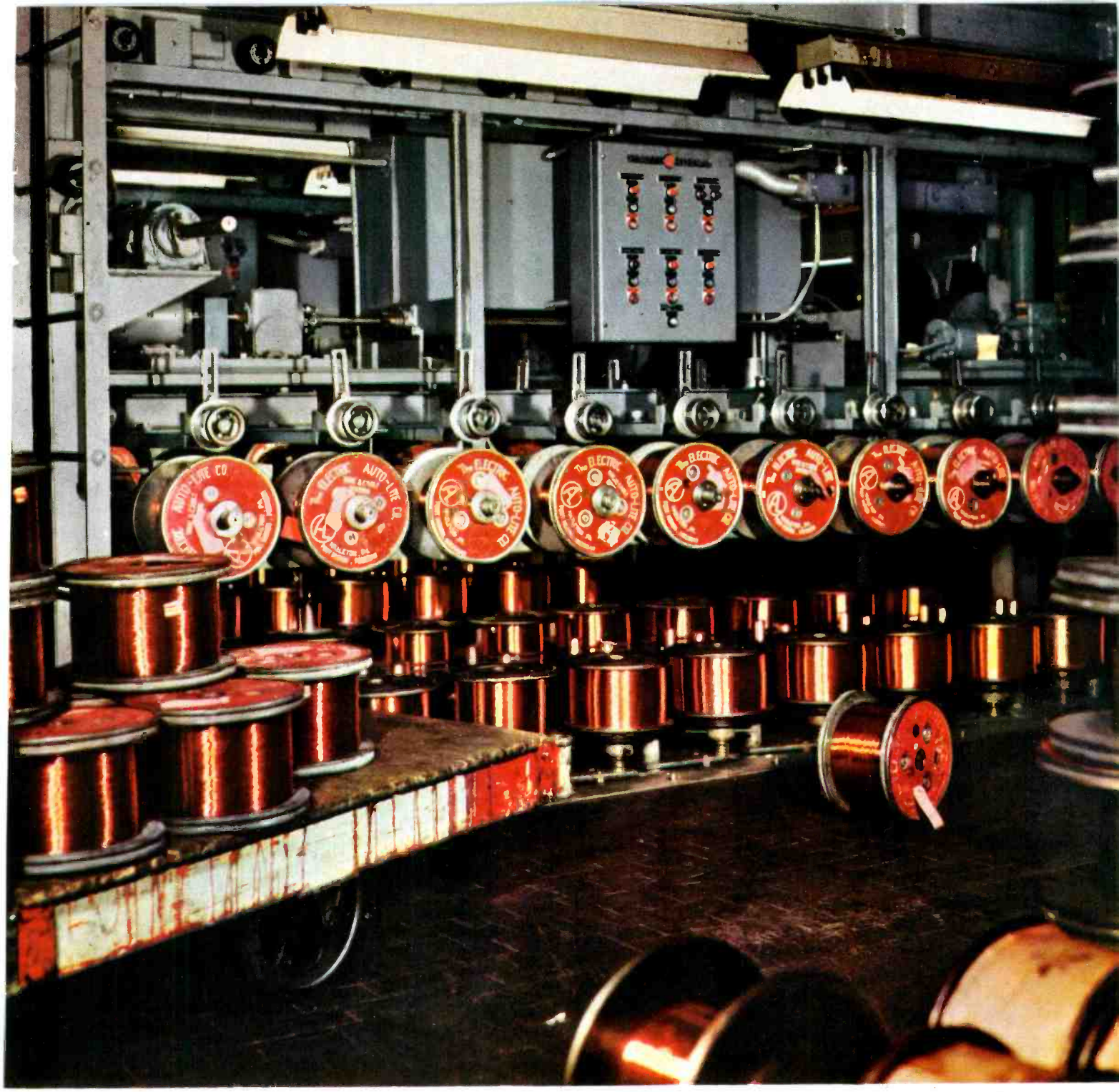
HIGH-PERFORMANCE EQUIPMENT BY Edo

SONAR, RADAR, LORAN and other related equipment designed and built by Edo serves commerce and national defense below the sea, on the sea, above the sea.

- Newly introduced Edo airborne LORAN puts this over-ocean navigation aid in the pilot's cockpit, so compact is its design, so simple its direct-reading capability.
- Edo RADAR, with close-in definition heretofore unheard of, provides safe, accurate navigation in the thickest weather for vessels, large and small, in open sea or the narrow confines of river, harbor or channel.
- Edo SONAR—active or passive—is in production for a wide range of commercial and naval applications from fish finding to long range submarine detection.

Whether it involves equipment for use below the sea, on the sea or above the sea, Edo's unique 33 years of work in aerodynamics, hydrodynamics and electronics gives the company a unique background of experience that is reflected in the superior performance of equipment bearing Edo's famed flying fish emblem.

Edo CORPORATION College Point, L.I., N.Y. SINCE 1925



Modern specialized plants assure prompt delivery of Magnet Wire.

Auto-Lite Expands Productive Capacity to Assure Quick Delivery of Finest Quality Magnet Wire

New facilities including filtered air conditioning, latest equipment, and rigid production controls have been installed in Auto-Lite Wire Plants to give customers a new high in production, quality, and service.

MAGNET WIRE

PLANTS and WAREHOUSES . . .

Port Huron, Mich.
YUkon 5-6131 •
Hazleton, Pa.
GLadstone 5-4781 •
Yonkers, N. Y.
Murray Hill 9-1842 •
Chicago, Ill.
WEbster 9-3144 •
Cincinnati, O.
POplar 1-3600

LECTALITE

Newest Enameled Magnet Wire by Auto-Lite!

LectALite magnet wire has been tested in accordance with AIEE 57 and MIL-W-19583 thermal aging test and found to be acceptable for Class B applications. LectALite can be applied to copper, aluminum, steel or silver magnet wires. Ideal for small electric motors, transformers, and TV yoke coils. Extreme resistance to Freon 12 and 22 and low extractables make it an outstanding wire insulation for hermetic refrigeration motors.

LectALite opens new magnet wire fields throughout the electrical industry.

This new insulation offers more heat resistance, higher thermoplastic flow, higher dielectric strength, greater flexibility and lower extractables than vinyl acetal insulation—with no increase in cost! Now available in sizes from 13 AWG through 30 AWG.

Tests indicate LectALite is the superior insulation for use in hermetic refrigeration motors due to its outstanding Freon 12 and 22 resistance plus low extractables. LectALite insulation has been found to have 30°C margin over vinyl acetal insulation by test performed under AIEE No. 57, Oct. 1955, "Proposed Test Procedure for Evaluation of the Thermal Stability of Enameled Wires" and MIL-W-19583 (NAVY) "Military Specification Wire, Electrical, Magnet, High Temperature, Film Insulated", July 15, 1955. Impregnation of LectALite wound coils can be done by any phenolic-alkyd type or suitable temperature rated impregnation varnishes.

The Auto-Lite magnet wire line is complete in classes O, A, B, and H to meet your design requirements.

ELECTRICAL, PHYSICAL AND CHEMICAL PROPERTIES

Description of Test	LectALite Insulation	Vinyl Acetal Insulation
Build	.0021	.0023
Heat Aging—hrs. 125°C	1500 hrs.	288 hrs.
Heat Aging Twist AIEE 200°C	506 hrs.	165 hrs.
Heat Aging Twist AIEE 225°C	110 hrs.	59 hrs.
Heat Aging Twist AIEE 250°C	20 hrs.	17 hrs.
Dry Dielectric Breakdown—KV/mil	2.5 to 3.5 KV/mil	1.5-2.0 KV/mil
Wet Dielectric Breakdown—KV/mil	1.1 KV/mil	1.1 KV /mil
Wet Insulation Resistance	1-2 months	1-3 weeks
G.E. Scrape Abrasion	45	41
Cut-Through Temperature—°C	300-320°	170-180°C
Heat Shock	(IX at 175°C 1 hr. O.K.	(IX at 125°C 1 hr. O.K.
Solderability	Good—900°F	Very Poor
Extractables—%	0.5-2.5%	3.0-6.0%
Solvent Resistance	Good	Good
Freon 22 Resistance	Excellent	Fails
Freon 12 Resistance	Excellent	Fair
Chemical Resistance 5% Sulfuric Acid	Very Good	Very Good
5% Hydrochloric Acid	Very Good	Very Good
1% Potassium Hydroxide	Very Good	Very Good
Xylene	Very Good	Very Good
Cresylic Acid	Good	Poor
Carbon Tetrachloride	Very Good	Very Good
Naphtha	Very Good	Very Good
Acetone	Poor	Poor
Alcohol	Very Good	Fair
Pyridine	Failed (Softens)	Failed (Softens)
Solvent Crazing (Stretched 5%—Dipped in Toluene)	Very Slight Crazing	Crazes
Annealed 15 Min. at 105°C Dipped in Toluene	No Crazing	Borderline Failure
Crazed Sample Heated 10 Min. at 150°C	Heals Completely	Heals Completely
Adherence Twist Test—4 in sample twisted on its own axis until coating twist cracks	120 to wire break	57

Auto-Lite Magnet Wire Line Is Complete In All Classes

CLASS O (90°C)

COTTON—Unbleached, long-staple white cotton protects primary insulation from damage caused by sharp bends and mechanical handling. Even wrapping forms a close, firm, continuous covering for increased dielectric. Additional layers, when required, are wound in opposite directions. When impregnated or immersed in a liquid dielectric, cotton is Class A insulation; when used alone, it is Class O. Available with colored tracers for coding. Manufactured to latest NEMA specifications. Available in a variety of combinations with other insulations. Double or triple conductors, individually cotton or paper covered, formed into a unit by an over-all cotton or paper covering supplied to meet requirements.

PAPER—A thin paper ribbon, wrapped spirally with overlap, is bonded to wire with adhesive. When impregnated or immersed in a liquid dielectric, paper is Class A insulation; when used alone, it is Class O. Similar to cotton in protective qualities, occupies less space because of uniformity of size, and increases dielectric. Paper insulation is available with one cotton wrap applied over two wraps of paper wound in opposite directions. Available with wax coating. Manufactured with multiple or single paper with a ¾ ″ lap, on round, square, or rectangular wire to the latest NEMA specifications.

Availability: **Round,** AWG #4 through #26;
Square, AWG #4 through #12;
Rectangular, width plus thickness not to exceed 0.650″.

CLASS A (105°C)

COTTON—When impregnated or immersed in a liquid dielectric, cotton is Class A insulation.

PAPER—When impregnated or immersed in a liquid dielectric, paper is Class A insulation.

CONVENTIONAL ENAMEL—A smooth uniform insulation with the basic electrical, physical and chemical properties for limited use as Class A insulation. Manufactured in single and heavy grades to latest NEMA specifications.

Availability: **Round,** AWG #9 through #40.

FORMVAR—A synthetic insulation of vinyl acetal, Formvar has better dielectric qualities, higher heat resistance, better flexibility and adherence, lower power factor and better solvent resistance than conventional enamel. Formvar is manufactured in single and heavy grades to the latest NEMA specifications.

Availability: **Round,** AWG #4 through #40;
Square, AWG #4 through #12;
Rectangular, width plus thickness not to exceed 0.650″.

NyALite—Moisture resisting quality of a Formvar base coat is coupled with an overcoating of nylon, for its excellent craze resistance, to produce NyALite. The high dielectric qualities of each insulation combine to provide an excellent magnet wire both in single and heavy grades for winding difficult coils.

Availability: **Round,** AWG #8 through #40.

BondALite—A combination of a Formvar insulation plus a thermoplastic overcoat. BondALite can be quickly and easily bonded wire-to-wire without damaging basic insulation. BondALite can be bonded in three ways: oven heat, electrical resistance, and solvents. Ease of bonding simplifies manufacturing of coils of the most complex forms.

BondALite No. 1 consists of Single Formvar with the addition of a bond coating to bring it up to the approximate dimension of Heavy Formvar.

BondALite No. 2 consists of Heavy Formvar with a bond coating to bring it up to the approximate dimensions of Triple Formvar.

BondALite No. 3 consists of Triple Formvar with a bond coating to bring it up to the approximate dimensions of Quadruple Formvar.

Availability: AWG #20 to #30.

SodALite—A new polyurethane insulation designed for ease of solderability at low temperatures (650-700°F) without scratch brushing or chemical stripping. SodALite has excellent over-all electrical and physical properties, approaching vinyl acetal insulation. It is manufactured under exacting conditions for ease of solderability.

Availability: AWG #8 through #40.

CLASS B (125° C)

LectALite—(*See page 2*)

IsALite—A new high temperature magnet wire for use up to 150° C as tested by Underwriter's Laboratories and Auto-Lite tests performed under AIEE No. 57. This magnet wire is manufactured with a polyester type enamel (Isonel) and found to have outstanding physical, electrical and chemical properties.

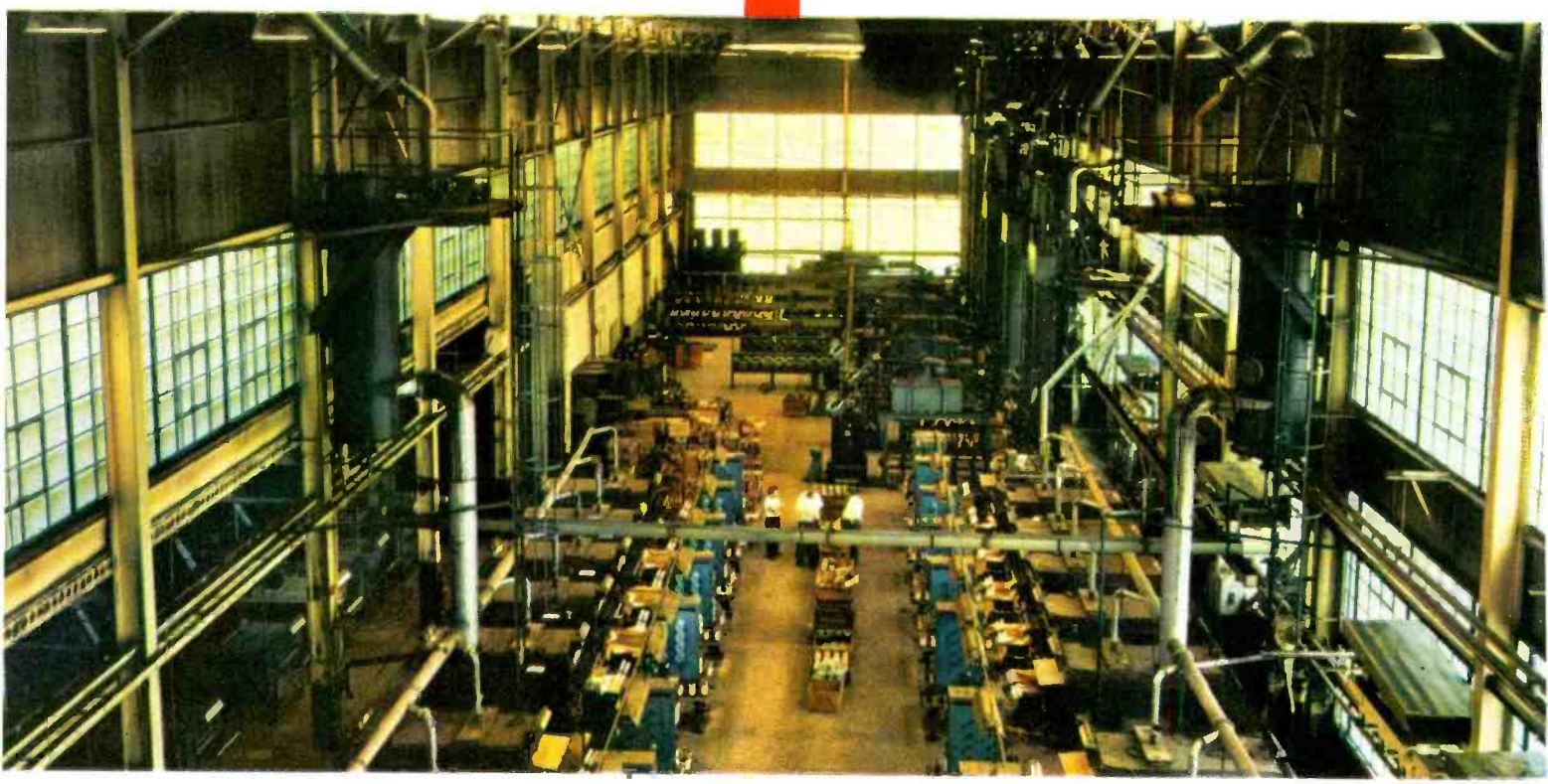
Availability: **Round,** AWG #8 through #40.

CLASS H (180°C)

GLASS-DACRON—An inorganic insulation bonded with suitable organic-inorganic binders for use at Class H ratings. Good electrical and mechanical properties are incorporated in this product to give improved flexibility and abrasion. It is wrapped in an even spiral, forming close, firm, continuous covering with single or double glass-dacron for increased dielectric strength.

Availability: **Round,** AWG #4 through #26; **Square,** AWG #4 through #12; **Rectangular,** width plus thickness not to exceed 0.650".

Latest equipment and controls assure consistent quality.



SEND FOR THESE FREE WIRE AIDS . . .

WIRE-O-METER—This convenient slide-rule type of pocket reference gives you complete specifications on all common sizes of wire. At a glance it tells you area in circumference, feet to a pound and pounds per thousand feet, turns per lineal inch and per square inch, and ohms per foot and ohms per pound.

MAGNET WIRE CATALOG—This quick reference is full of facts covering many different types of wire. It's complete with physical, chemical, electrical and military specifications.

AIRCRAFT WIRE AND CABLE KIT—This handy kit gives you complete military specifications for Auto-Lite Aircraft Wire including samples of famous Auto-Lite 350 General Purpose High Temperature Aircraft Wire.

WIRE GUIDE OF ELECTRICAL AND CHEMICAL PROPERTIES—Here's a handy reference that gives you a complete run-down on 9 basic kinds of insulation.

MAIL TODAY

THE ELECTRIC AUTO-LITE COMPANY
WIRE AND CABLE DIVISION
PORT HURON, MICHIGAN

- ☐ MAGNET WIRE CATALOG
- ☐ WIRE-O-METER
- ☐ AIRCRAFT WIRE AND CABLE KIT
- ☐ WIRE GUIDE OF ELECTRICAL & CHEMICAL PROPERTIES

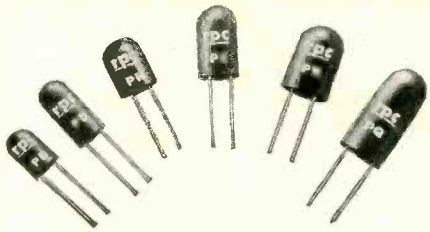
NAME_____

FIRM_____

ADDRESS_____

CITY_____

ZONE_____ STATE_____



Precision Resistors Printed Circuit

To meet the requirements for printed circuitry, RPC has developed Type P Encapsulated Wire Wound Precision Resistors Miniature, single ended units designed for easy rapid mounting on printed circuit panels with no support other than the wire leads. Many newly developed techniques are employed in the manufacture of Type P Resistors. These units can be operated in ambient temperatures up to 125°C. and will withstand all applicable tests of MIL-R-93A, Amdt. 3. Available in 6 sizes, rated from 1/10 watt to .4 watt. ¼" diameter by 5/16" long to ⅜" diameter by ¾" long. Resistance values to 3 megohms. Tolerances from 1% to 0.05%.

rpc

HIGH QUALITY RESISTORS FOR ELECTRONICS

RPC is a widely recognized supplier of high quality resistors to industry, Government Agencies and the Armed Forces. Advanced production methods, modern equipment and scientific skill enables RPC to manufacture resistors of *highest quality* in *large quantities* at *reasonable cost*. Modern manufacturing plant is completely air conditioned and equipped with electronic dust precipitators to insure highest production accuracy. RPC resistors are specified for use in instruments, electronic computers, radiation equipment, aircraft equipment and scientific instruments.

Test equipment and standards for checking and calibrating are equalled by only a few of this country's outstanding laboratories. Our ability to produce resistors of highest quality coupled with prompt delivery have established RPC as a leading manufacturer of resistors. Small or large orders are promptly filled.

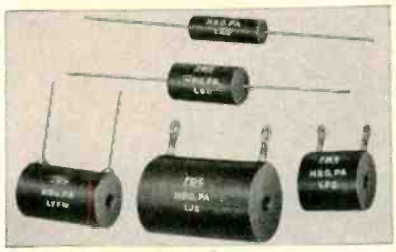
Representatives in principal cities. For full information send for latest catalog.

High Frequency Resistors

Used where requirements call for very low inductance, capacitance and skin effect in circuits involving pulses and steep wave fronts. Depending on size and resistance value, these resistors are usable at frequencies to over 400 mc. Resistance values range from 20 ohms to 100 megohms with tolerance of 20% to 5%. 2 types available.

TYPE G resistors (shown) are tubular, in 6 sizes from 4½" long x ¾" diameter to 18½" long x 2" diameter. With band terminals or ferrules. Power rating 10 to 100 watts.

TYPE F resistors (not shown) in 8 sizes from 9/16" long x 0.10" diameter to 6½" long x 9/16" diameter. Lugs or wire leads. Power rating ¼ to 10 watts.

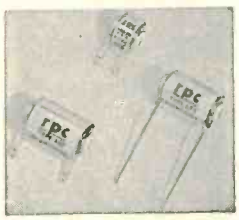


Encapsulated Precision Wire Wound Resistors

RPC Type L Encapsulated Resistors will withstand temperature and humidity cycling, salt water immersion and extremes of altitude, humidity, corrosion and shock without electrical or mechanical deterioration. Type L resistors are available in many sizes and styles ranging from sub-miniature to standard with lug terminals, axial or radial wire leads. Available for operation at 105° C. or 125° C. ambient temperatures. These resistors will meet all applicable requirements of MIL-R-93A, Amdt. 3. Type L can be furnished with all resistance alloys and resistance tolerances from 1% to .02%.

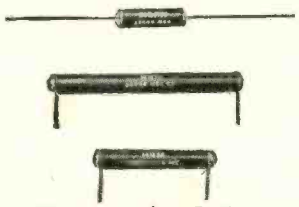
High Voltage Resistors

Type B Resistors are stable compact units for use up to 40 KV. These resistors are used for VT voltmeter multipliers, high resistance voltage dividers, bleeders, high resistance standards and in radiation equipment. They can be furnished in resistance to 100,000 megohms. Available as tapped resistors and matched pairs. Sizes range from a 1 watt resistor 1 inch long x 5/16 inch diameter rated at 3500 volts, to a 10 watt resistor 6½ inches long x 5/8 inch diameter rated at 40 KV. Low temperature and voltage coefficients. Standard resistance tolerance 15%. Tolerances of 10%, 5% and 3% available. Tolerance of 2% available in matched pairs.



Wire Wound Precision Resistors

Type A Precision Resistors are widely used for all general requirements. They are available in a wide variety of sizes, styles and terminal types. They can be furnished with all resistance alloys in tolerances from 1% to .02%. Type A will meet the requirements of MIL-R-93A, Amdt. 2, Characteristic B. Special winding techniques, impregnation and thermal aging result in resistors of exceptional stability. Matched resistors, networks and special assemblies can be supplied.

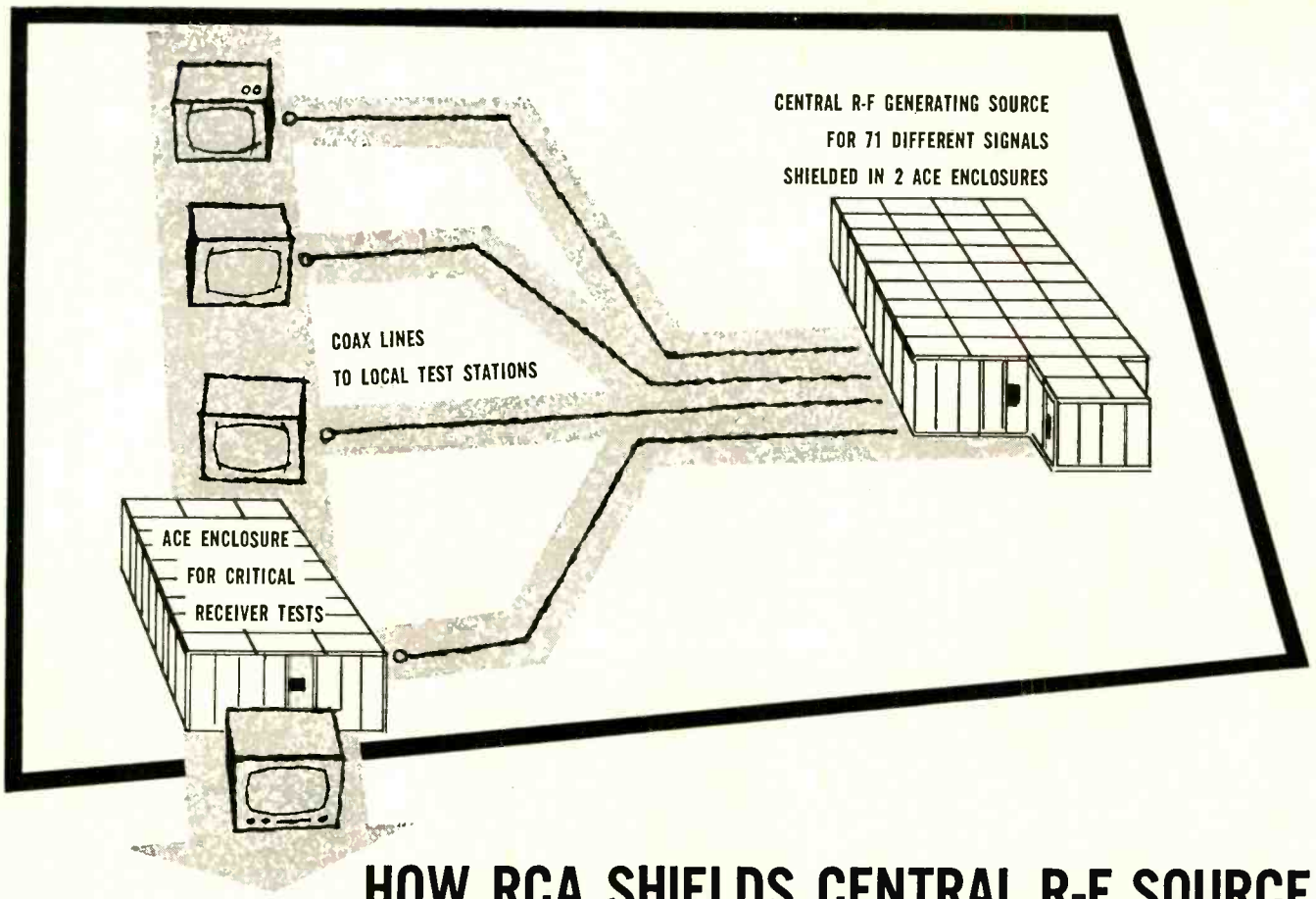


High Megohm Resistors

Type H Resistors are used in electrometer circuits, radiotion equipment and as high resistance standards. Resistance available to 100 million megohms, (10^{14} ohms). For utmost stability under adverse conditions Type HSD and HSK Hermetically Sealed are recommended. Eight sizes from ⅞ inch to 3 inches long are available. Voltage rating to 15,000 volts. Low temperature and voltage coefficients. Standard resistance tolerance 10%. Tolerance of 5% and 3% available. Also matched pairs 2% tolerance.

RESISTANCE PRODUCTS CO.

914 S. 13th Street
HARRISBURG, PA.



HOW RCA SHIELDS CENTRAL R-F SOURCE FOR INTERFERENCE-FREE LOCAL TESTING

Almost all of the 70-odd r-f signals needed to test receivers in RCA's modern plant at Indianapolis, Indiana, are generated at a central location. These signals are then piped via coaxial cables to testing sites throughout the plant. This novel approach to production line testing and aligning decreases r-f interference . . . allows more precise adjustment of the receivers.

For this system to work, however, the central r-f generators must be shielded properly. Otherwise, direct radiation of the oscillators would interfere with the receiver tests. In addition, certain critical tests require that the receivers themselves be shielded from all sorts of miscellaneous electrical interference associated with a large manufacturing plant.

To achieve its testing needs, RCA installed three Ace solid sheet metal enclosures (RFI Design)*. Two measure over 30 feet by 16 feet, stand ten feet high, and house the powerful signal generators. The third is used for analyzing the television receivers.

All of the rooms are equipped with air-conditioning, and two personnel access doors. Coaxial and electrical cables enter the enclosures through special filter traps designed to eliminate any possible stray radiations.

In addition to supplying a guaranteed 100 db attenuation from 14 kc to 1000 mc. (they have been known to hit 128 db), these rooms offer RCA several distinct advantages:

*Lindsay Structure

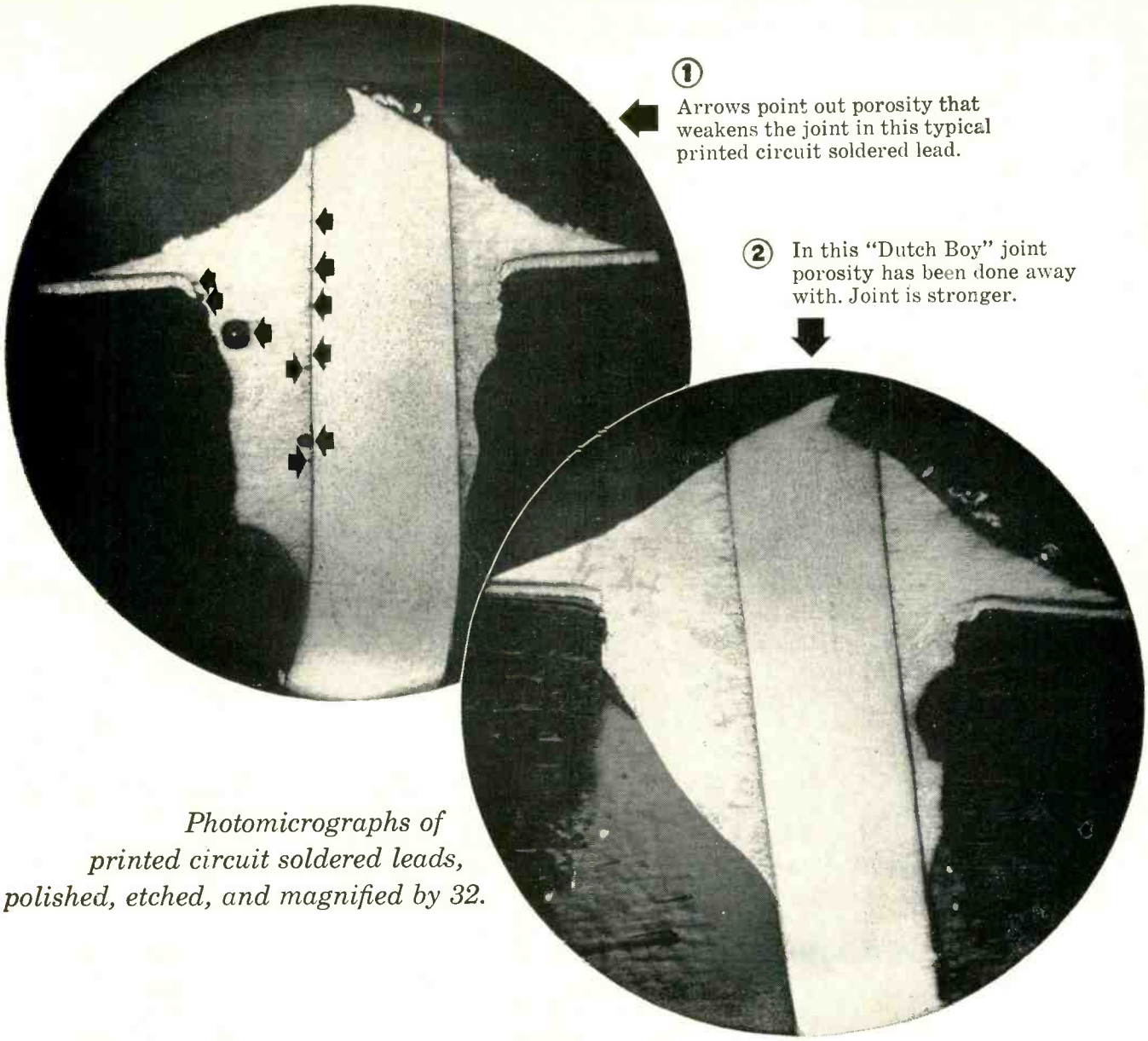
1. They may be easily moved in the assembled state if the plant should be rearranged.
2. Their dimensions may be altered, if necessary, by adding or removing interchangeable panels.
3. They are designed for exceptionally long life with no decrease in attenuation due to aging.

The Indianapolis installation shows just one of the ways in which Ace enclosures are being used today in industrial, military, and medical applications. An Ace Sales Engineer would be glad to show you how you can solve your interference problems with comparable success. Write for further information—a free catalog on standard enclosures is yours for the asking.

ACE

First and Finest in Shielded Enclosures

ACE ENGINEERING & MACHINE CO., INC. 3644 N. Lawrence St. • Phila. 40, Pa.



① Arrows point out porosity that weakens the joint in this typical printed circuit soldered lead.

② In this "Dutch Boy" joint porosity has been done away with. Joint is stronger.

Photomicrographs of printed circuit soldered leads, polished, etched, and magnified by 32.

"Dutch Boy" gets inside story on printed circuit soldering

...develops solders and fluxes that give stronger joints, coat more uniformly, show higher conductivity

"Dutch Boy" researchers keep a close eye on printed circuit soldering.

For example, they cross-section soldered leads, polish, and examine the polished sections under the microscope.

Most such joints prove too weak

The photomicrograph above left shows why. Notice this typical joint is honeycombed with porosity. Arrows point to holes.

Now look at the photomicrograph on the right. This joint is strong. Non-porous.

How was joint on the right made stronger?

No great trick. A "Dutch Boy" Solder Specialist simply worked out slight improvements in flux and solder formulae and operating conditions.

Maybe this would help improve *your* printed circuits.

"Dutch Boy" solders develop maximum surface tension. They don't form "tear drops" when coated boards are lifted from the bath...they improve coating uniformity. The residual flux is both non-corrosive and non-conductive, and can be left on the soldered board.

So, if you feel there is room for improvement in your printed circuit soldering, look first to "Dutch Boy". Write, giving details if possible, to National Lead Company, 111 Broadway, New York 6, N. Y.

Dutch Boy®
SOLDER AND FLUXES

HOW TO TEST CORES

With the growing realization that cores are here to stay, more companies every day are expressing an interest in their application. But as Burroughs discovered some six years ago, a core investigation program must be a core *testing* program as well. And since the special equipment and procedures needed for core testing were not available at the time, Burroughs had to develop them.

These tools and techniques, born of a practical need are available now for your core testing needs. The tool is the Burroughs BCT-301, a complete and flexible system for accurately measuring the operating characteristics of tape wound cores. Allowing precise control over frequency, pattern, amplitude, and rise time of the core driving signal, the BCT-301 gives you extremely accurate measurements of the switching time of the core as well as the amplitude of the output pulse. And since it is constructed of unitized sections, the BCT-301 can be expanded and modified to meet new testing requirements as they arise.

But the BCT-301 is more than just a tool. With it you get the benefit of techniques and procedures which are now in everyday use at Burroughs, and are accepted practice among major core manufacturers. If you're interested in designing tape wound cores into your products, we'll be glad to send you additional detailed information on the BCT-301. Or, if you wish, have a Burroughs Sales Engineer demonstrate how the BCT-301 can get your core testing program off the ground . . . NOW.

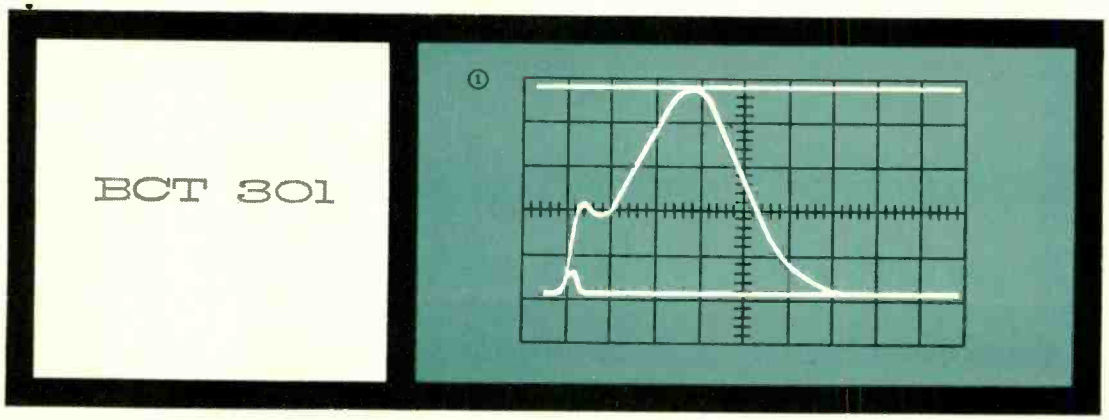


Figure ① shows the peak voltage amplitude of the output pulse being measured with the calibrating voltage. For amplitudes less than one volt, measurements can be made in millivolts.
Figure ② shows the calibrating voltage being used to measure pulse width at 10% of the amplitude.

tools for engineers

Burroughs

Burroughs Corporation • ELECTRONIC INSTRUMENTS DIVISION
DEPARTMENT C • 1209 VINE STREET • PHILADELPHIA 7, PENNSYLVANIA

. . . with the BCT-301

A Complete and Flexible Core Testing System

The BCT-301 has been designed expressly for the individual testing of square loop cores. It provides precise control over the frequency, pattern, amplitude and rise time of the core driving signal, and allows extremely accurate measurements of the switching time of the core, as well as the amplitude of the output pulse. The unit is composed of five basic sections, each of which can be replaced or expanded for other types of core testing.

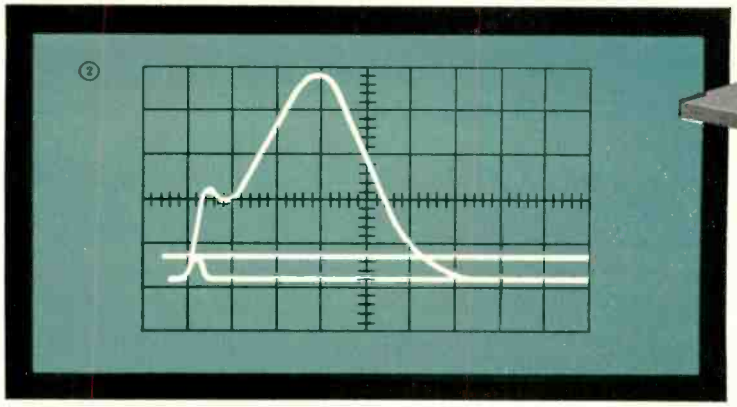
Core Mounting Jig This low-noise test mounting jig applies tight single turn loops around the core for input and output windings. It has been designed to minimize not only pickup by the secondary, but also other disturbances caused by air flux. Adjustable pins accommodate a wide range of bobbin sizes with equal precision.

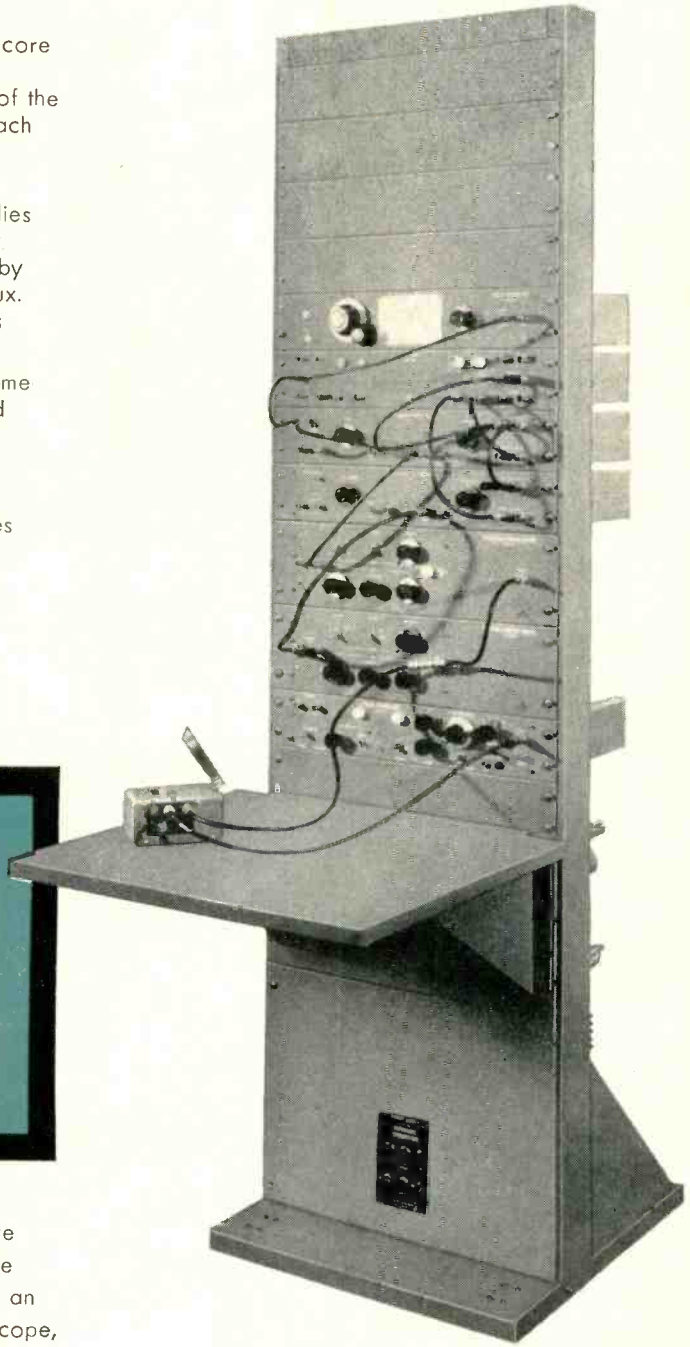
Pattern Generator The Pattern Generator provides extreme flexibility in generating the pulse patterns which are applied to the core. This section of the system controls the pulse spacing, repetition rate of the cycle, and the number of pulses in the pattern.

Current Drivers Two Current drivers convert the voltages from the pattern generator into the positive and negative constant current pulses used for driving the core.

Front panel controls provide:

Variable current amplitude from 0 to 1.0 ampere
Variable rise time from 0.2 μsec. to 1.0 μsec.
Variable pulse duration from 1.0 μsec. to 10.0 μsec.



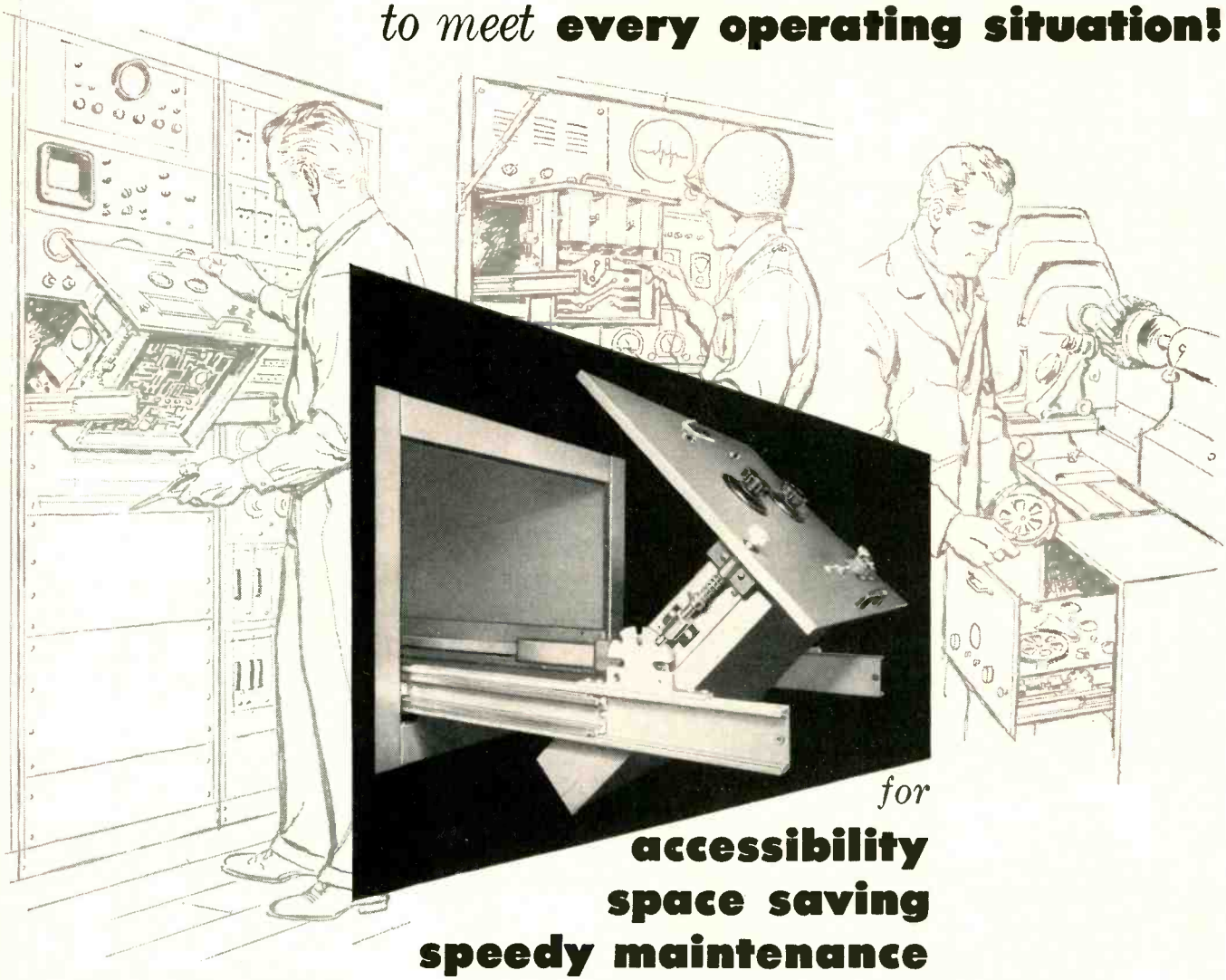


Calibrator The calibrator is designed to accurately measure currents and voltages. It permits the measurement of both the driving current and the amplitude of the output voltage with an error of less than 1%. When used with a calibrated oscilloscope, it makes possible highly accurate readings of switching time.

Power Supply The power supply provides seven regulated d-c voltages.

over **100** *designs of* **Grant INDUSTRIAL SLIDES**

to meet **every operating situation!**

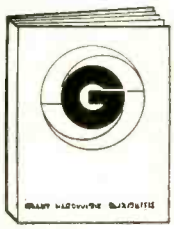


for

accessibility
space saving
speedy maintenance

Grant Industrial Slides afford substantial, practical mountings for nearly all types of assemblies—electronic, hydraulic, pneumatic, mechanical. They allow quick access... the pivoting types permit testing or work on underside as well as top of chassis... also provide for quick release of chassis for bench servicing. Slide mounting usually eliminates need for rear access doors and rear aisles—a very important saving of space. Grant slides are soundly engineered, durable and dependable. Load capacities range up to 500 lbs. and more.

Grant engineers and representatives in all important industrial areas offer specialized experience—will aid in working out custom variations to adapt standard slides to especially exacting requirements.



Ask For This Important Working Data

The Grant Industrial Slide Catalogue is a working manual on built-in accessibility. Ask us to mail your free copy.

Grant INDUSTRIAL SLIDES

Grant Pulley and Hardware Corporation
31-73 Whitestone Parkway, Flushing 54, N.Y.
944 Long Beach Avenue, Los Angeles 21, Calif.

Want more information? Use post card on last page.

NEW GRID-CONTROLLED KLYSTRON NOW IN QUANTITY PRODUCTION

SAL-89 HIGH-POWER PULSE AMPLIFIER FOR AIR NAVIGATION SYSTEMS

In introducing the SAL-89, Sperry is offering the first production tube featuring grid-controlled pulse operation for ease of modulation. This tube, with its unique technological advances, was designed specifically for air navigation and traffic control service.

With grid control, Sperry has greatly eased the problem of modulating high-power klystrons. For example, only 575-volt pulses are now required to modulate the tube where previously 10,000-volt pulses were necessary. Specially shaped pulses are also easily applied to the tube.

SAL-89 incorporates space-charge focusing, another Sperry development, which eliminates large, heavy magnetic structures and simplifies cooling. Integral resonant cavities make external microwave circuits with their associated sliding contacts unnecessary.

For further information on this new tube, write our Electronic Tube Division.

GENERAL CHARACTERISTICS

Frequency Range	960 to 1215 mc
Peak Output Power	30 kw
Grid Bias (Negative)	1% of Beam Voltage
Grid Drive (Positive)	2.2% of Beam Voltage

TYPICAL PULSE OPERATION

Frequency	1100 mc
Grid Bias	170 v
Grid Drive	575 v
R-f Input Peak Power	30 w
R-f Output Peak Power	25 kw
Duty Cycle	2.5%
Beam Voltage	17 kv

SPERRY **ELECTRONIC TUBE DIVISION**
GYROSCOPE COMPANY
Great Neck, New York
DIVISION OF SPERRY RAND CORPORATION

CLEVELAND • NEW ORLEANS • BROOKLYN
LOS ANGELES • SAN FRANCISCO • SEATTLE
IN CANADA: SPERRY GYROSCOPE COMPANY OF CANADA, LIMITED, MONTREAL, QUEBEC

all new

hp precision

18 KMC

The revolutionary new waveguide equipment shown here represents a practical, efficient adaptation of an ultra-modern concept of waveguide instrumentation. Emphasis throughout is on functional simplicity, rugged dependability, highest accuracy, and low cost. The instruments are offered as individual basic test components, yet all are integrated electronically and mechanically with the *-hp-* waveguide line.

There has been no compromise with traditional *-hp-* quality in extending *-hp-* waveguide instrument coverage to the 40 KMC region. Yet there is present the same ingenious design simplicity which make possible mass-production economy—low cost to you.

Today, more than ever, *-hp-* offers you the best value in waveguide instrumentation ever available.

each covers full waveguide band
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easy set-up, simple operation

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◀ *-hp-* 752 Directional Couplers. Available with coupling factors of 3, 10 and 20 db ± 0.7 db full range. SWR better than 1.05. Directivity 40 db or better over entire range. *-hp-* K752, $100.00. *-hp-* R752, $120.00.

◀ *-hp-* 910A Waveguide Terminations. Matched load for use where waveguide must be terminated in its characteristic impedance. Residual reflection approx. 1.0%. Average power 0.5 watts. *-hp-* K910A, $30.00. *-hp-* R910A, $35.00.

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26.5 to 40.0 KMC
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Covering frequencies 12.4 to 40.0 KMC, the new, convenient -hp- 814A mounts -hp- 815A Waveguide Slotted Sections in P, K and R bands. Waveguides may be interchanged instantly with positive-accuracy alignment. For use with the new -hp- 446A Broadband Probe ($145.00), the 814A Carriage provides direct readings to 0.1 mm and interpolation to 0.01 mm (approximately 0.001 wavelength). Dial adjusts quickly for differential readings; accuracy is assured by a precision-threaded drive free of backlash. SWR to 1.02 is easily read, and slope error can be eliminated. $225.00.

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-hp- 487A Thermistor Mounts. Broadband mounts for fast, accurate power measurements. Negative-temperature coefficient thermistors provide burnout protection. SWR approx. 2.0. -hp- K487A, $85.00.

-hp- 870A Slide Screw Tuners. For flattening waveguide systems. Probe sets up SWR which cancels existing SWR. No back lash in adjustments. Accuracy SWR 1.02. -hp- K870A, $140.00. -hp- R870A, $140.00.

-hp- E80A E-H Tuners. For tuning high power systems or setups where low leakage is essential. Consists of hybrid tee, with movable choke shorts in shunt and series arm. -hp- K380A, $155.00. -hp- R880A, $170.00.

-hp- 914A Moving Loads. Low reflectance load (1.0%). Load position variable at least ¾ wavelength, permitting reversing phase of residual reflection. -hp- K914A, $65.00. -hp- R914A, $75.00.

-hp- 920A Adjustable Shorts. Choke type adjustable shorts for introducing reactance in combination with detecting sections, series, shunt or hybrid tees. -hp- K920A, $75.00. -hp- R920A, $85.00.

Remember

-hp- also offers complete waveguide instrumentation 3 through 18 KMC for S, G, J, H, X and P bands!

waveguide instrumentation 3 through 40 KMC!

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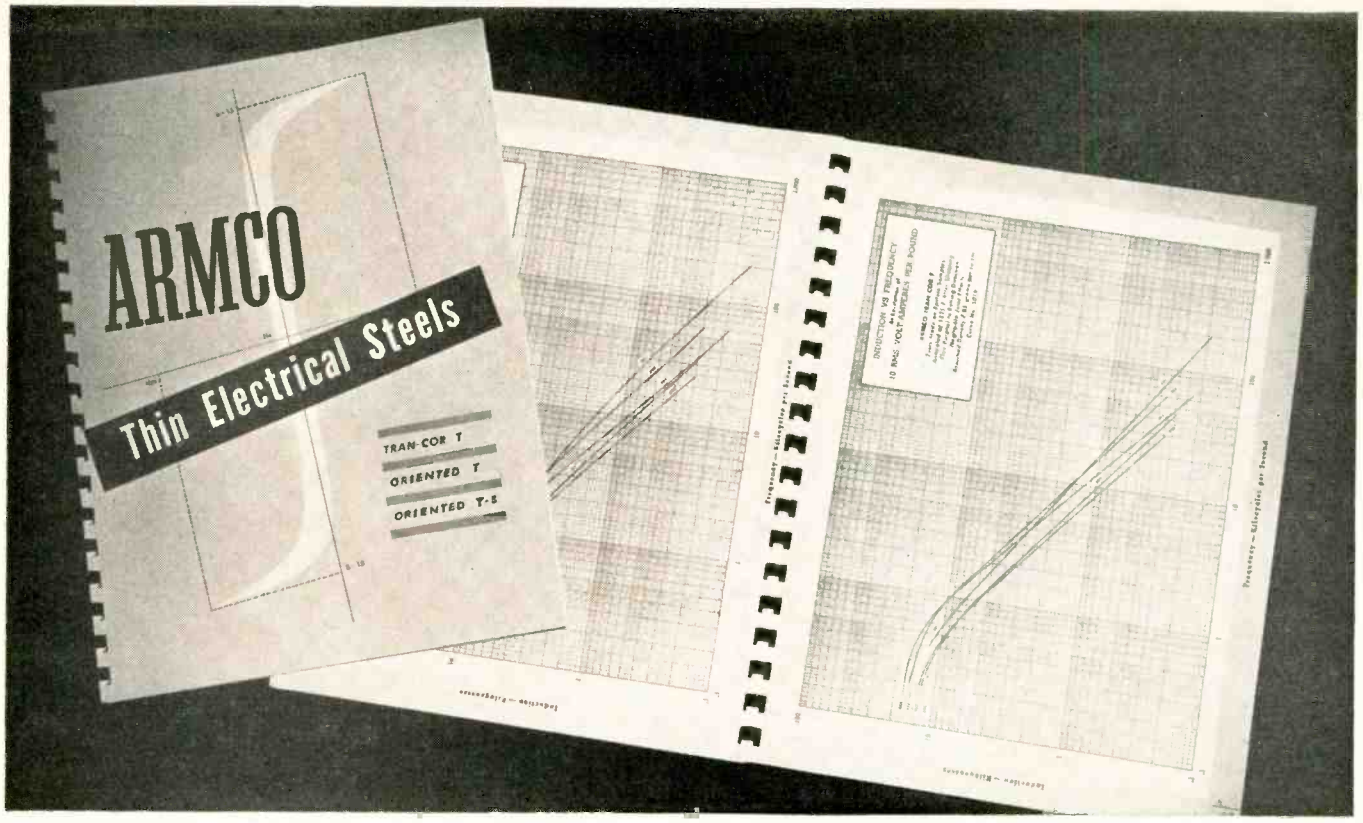

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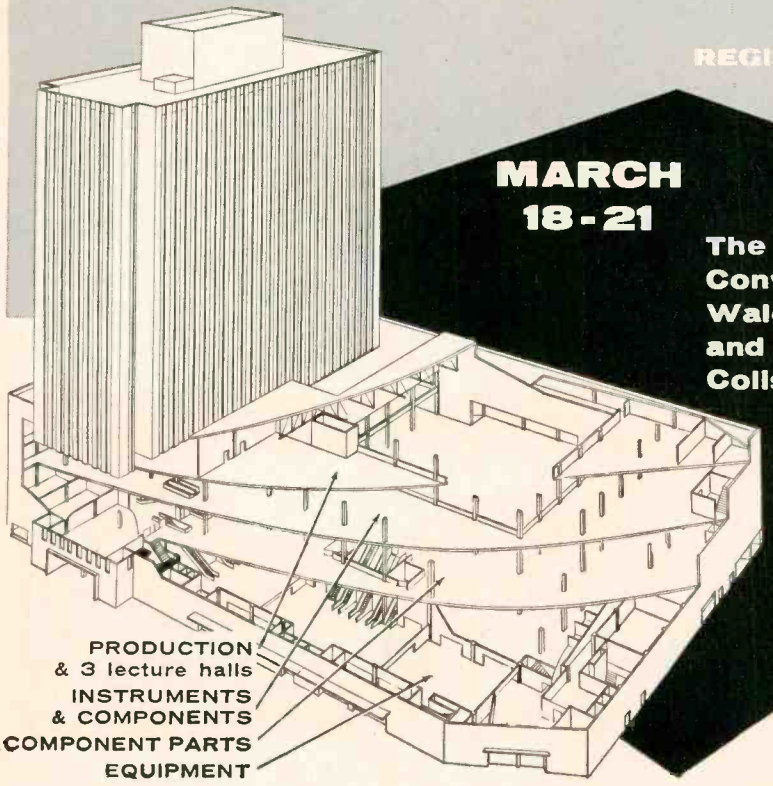

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One of the most widely used materials for electrical contacts, SILVER provides high resistance to atmospheric corrosion. Silver Alloys—which contain base metals to achieve specific properties—provide other modified characteristics, such as increased resistance to arc erosion, sticking and metal transfer.

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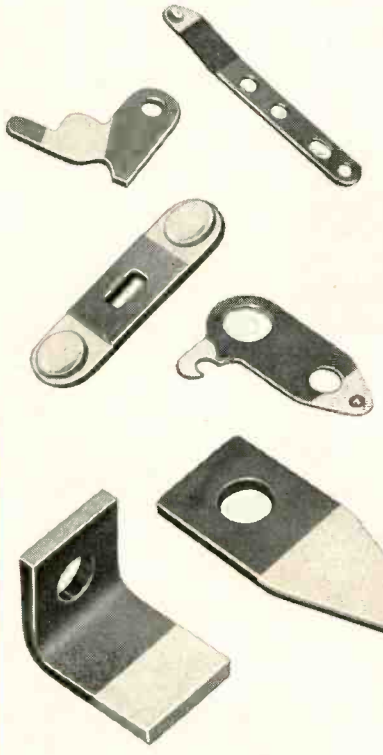

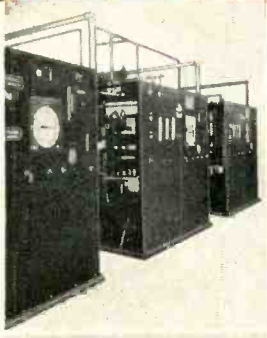

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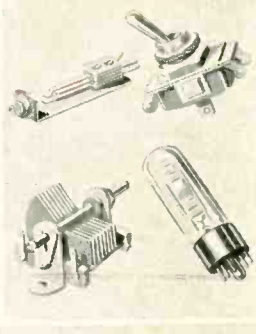

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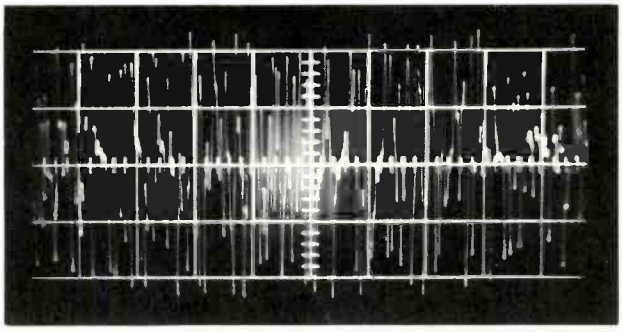
Electron Tube News
–from Sylvania

–contributing to equipment performance everywhere in electronics

Sylvania adds its newest reliability factor to premium subminiature tubes

– **"White noise" vibration test** is worthy measure of the superior construction of the button-header subminiature.

A full line of Sylvania "gold brand" subminiature tubes is now being "white noise" tested on a pro-

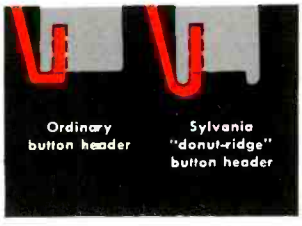


This unretouched oscillogram demonstrates the wide spectrum of frequencies inherent in the "white noise" vibration test, which is applied to the tube.

duction basis. Thus a new measure of reliability has been added to the tubes already acknowledged as the world's most reliable.

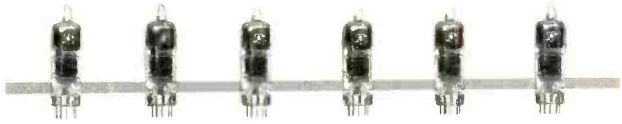
The "white noise" test presents a full range of frequencies over a broad spectrum at peak g-levels of 15 and provides a closer approximation of vibrational environment encountered in guided missile and other vehicular applications.

The ability of Sylvania subminiatures to submit to this more exacting test is dramatic proof of the superior construction of the button-header design. Stronger leads, vertical support in three rather than a single vertical plane, wider spacings – these and other features of the button-header have added considerable impetus to the accepted use of Sylvania "Gold Brand" subminiatures in guided missiles.



Here's a simple comparison of the advantage of Sylvania's "donut ridge" button-header over ordinary types. When the leads are bent sharply as shown, ordinary headers will flake, chip, or crack; but leads bend cleanly around the "donut ridge" in Sylvania "Gold Brand" subminiatures.

– in military equipment



For the first time by any manufacturer, subminiature tubes are being given the "white noise" vibration test in addition to the currently used static-vibration tests at 40 cps and 15 g. Types listed are now being tested for "white noise."

Type 5636 . . . . . UHF pentode
Type 5639 . . . . . Video pentode
Type 5718 . . . . . UHF medium Mu triode
Type 5719 . . . . . High Mu triode
Type 5840 . . . . . UHF sharp cutoff pentode
Type 5899 . . UHF semi-remote cutoff pentode
Type 5902 . . . . . Audio Beam Power Pentode
Type 5977 . . . . . Medium Mu Triode
Type 6021 . . . . . Medium Mu Double Triode
Type 6111 . . . . . Medium Mu Double Triode
Type 6112 . . . . . High Mu Double Triode
Type 6205 . . . . . UHF sharp cutoff pentode
Type 6206 . . UHF semi-remote cutoff pentode
Type 6788 . . . . . RF Pentode

New Subminiature RF Pentode is Tailor-made for Guided Missiles

The new Sylvania Type 6788 features high gain in the audio region and has exceptionally low vibrational noise, making it ideally suited for guided-missile application.

It is the first subminiature tube released from Sylvania's guided-missile development program and is the only tube specifically designed for use as an amplifier where conditions of severe mechanical vibration are encountered.

—contributing to equipment performance,

—in television

New Dual Triode developed for Vertical Deflection in 110° Systems

Anticipating the need for a new vertical deflection tube to complete the designer's needs in 110° deflection circuits, Sylvania developed the type 10DE7. The 10DE7 is a T6½ double triode with dissimilar sections — one triode for vertical deflection and the other suitable for vertical oscillator use. The type utilizes a 600 ma heater with warm-up time control for series string operation.

The high perveance type 10DE7 will deliver 80 ma peak plate current at lower supply voltages and at a plate dissipation up to 7 watts in the vertical deflection amplifier section.

The grid of the output section is connected to two external pins providing for additional cooling and greater circuit flexibility. The miniature construction of the type 10DE7 also makes it particularly adaptable to printed circuits and automation techniques.

The types 6DE7 and 13DE7 are also available for use in transformer circuits and 450 ma series string operations respectively.

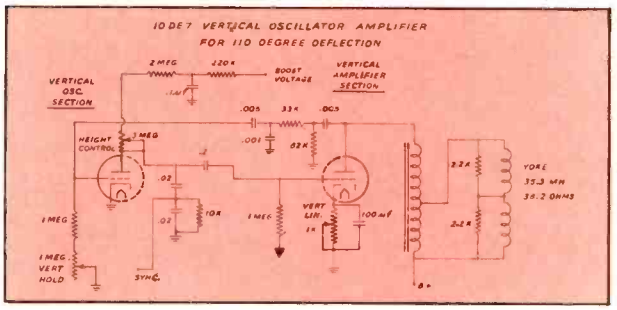
Average characteristics of the 10DE7 in a typical 110° deflection circuit

Amplifier Section

Cathode Current	29 ma
Peak Cathode Current	80 ma
Peak-to-Peak Grid Drive	103 V
Grid Bias	−11.5 V
Cathode Bias D.C.	21 V
Plate Voltage—Peak-to-Peak	577 V
Filament Voltage	10 V
High Voltage	16 KV @ 100 ma
B+ Voltage	250 V

Oscillator Section

Plate Voltage	65 V
Cathode Current—Peak	47 ma
Grid Voltage	−55 V
Grid Voltage—Peak-to-Peak	235 V



Design and performance capabilities of the 10DE7 have been checked out thoroughly in the typical 110° circuit shown. Characteristics reflect average characteristics measured.

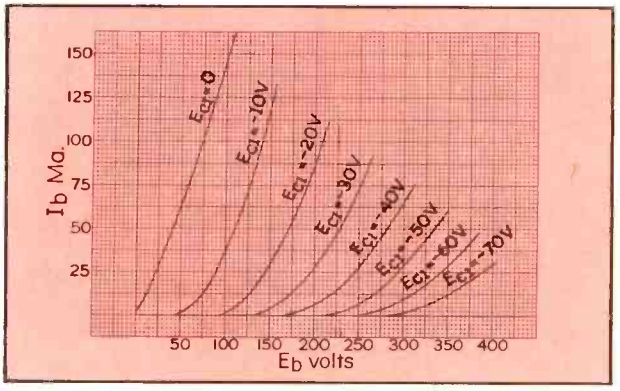


Plate family characteristic curves for the Type 10DE7

Beam Power Pentodes for 110° vertical deflection

For systems using pentodes for vertical deflection amplifier use Sylvania provides two basic important types, the type 6CM6 and type 6CZ5. Both are suited for 110° deflection—the 6CM6 for up to 17" picture sizes and the 6CZ5 for larger.

Characteristics — pentode connections

Type 6CM6	pentode conn.
Plate V	315 V Max.
Peak Pos. Plate Volt	2000 V Max.
Plate Diss.	8 Watts Max.
Grid 2 V	285 Volts Max.
Grid 2 Diss.	1.75 Watts Max.
Type 6CZ5 —	
Plate V	315 V Max.
P.P.P. V.	2200 V absolute Max.
Plate Diss.	10 Watts Max.
Grid 2	285 volts Max.
Grid 2 Diss.	2 watts Max.

The types 6DQ6A and 6DN6 will meet horizontal deflection needs in 110° circuits and the proved type 6AU4GTA or 6AX4GTA will provide adequate damper service.

Completing the tube needs in 110° deflection systems, Sylvania offers the types 1B3GT and 1X2B for high voltage rectifier use.

everywhere in electronics

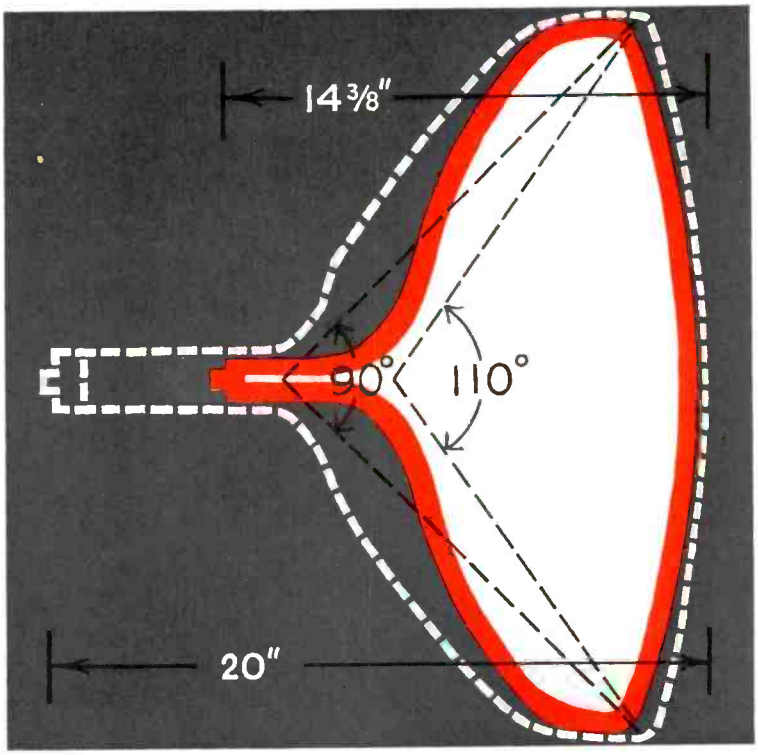
New 110-Degree Picture Tube offers more picture per cubic inch of TV set

— other new tubes offered include 90° short-neck, non-ion trap types and a dramatic new development scheduled for early production.

New, shorter, lightweight, 110° deflection picture tubes will save as much as 20% in picture tube weight and will make it possible to design more compact, lighter TV consoles, as well as more portable TV sets.

Light weight and structural strength of the picture tube have been achieved in a new faceplate design. New trim set styling made possible by shorter lengths should provide new stimulus for the sale of black-and-white TV sets.

As a leading picture tube manufacturer, Sylvania is working closely with TV set makers to supply the industry's requirements for both 110° deflection types and 90° short-neck non-ion trap types. New developments will be made available early this year.



Compare a 21" bulb in 90° and the new 110° versions. New 110° offers considerable savings in depth per square inch of picture. ▶

Sylvania offers new types in a complete line of 12-volt tubes for hybrid auto radio

—in Radio

Type 12CY6 — New T5½ IF Pentode

Heater Voltage	— 12.6 volts
Heater Current	— 200 ma.
Transconductance	— 3250 umhos
Plate Resistance	— 140K ohms
Plate Current	— 1.6 ma.
Grid to Plate Capacitance	— .18 uuf max.

Type 12CX6 — New T5½ RF-IF Pentode

Heater Voltage	— 12.6 volts
Heater Current	— 150 ma.
Transconductance	— 3100 uhmos
Plate Resistance	— 40K ohms
Plate Current	— 3.0 ma.
Grid to Plate Capacitance	— .05 uuf max.

Type 12J8 — New T6½ Transistor Driver

Heater Voltage	— 12.6 volts
Heater Current	— 350 ma.
Transconductance	— 5400 uhmos
Plate Resistance	— 4000 ohms
Power Output	— 20 mw.
Total Harmonic Distortion	— 5%

Sylvania's line of 12-volt tubes for hybrid auto radio features an RF pentode with high transconductance, an IF pentode with high gain and a transistor driver designed to match the input characteristics of single-ended or push-pull transistor output stages.

These developments reflect the specific design requirements which have been brought about by the hybrid radio design, particularly the need for high performance with fluctuations in voltage-supply conditions.

All auto-radio types are produced under Sylvania's well-known "noise-free" tube program which exerts tighter limits and more rigid controls on all factors influencing microphonism.

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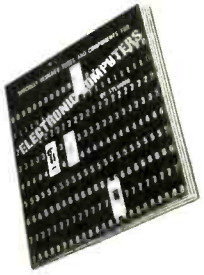
—in computers

The Type 6888 is a dual control computer pentode designed for long life and low failure rate. It is especially designed for pulse amplifier use, core driver and coincidence circuits.

It is built to the highest standards of reliability established for commercially available tubes and is dynamically tested for pulse characteristics under pulse test conditions.

The type 6888 is just one of a full line of Sylvania tubes especially designed for computer applications.

Write for this complete brochure of Sylvania's line of computer products



What every computer designer should know about Sylvania components is completely outlined in this 64-page book. Between these two covers is the complete story of Sylvania's stake in the computer field: its philosophy of reliability, its testing procedures, and its ability to develop the tube parameters required for computer applications.

—in test equipment

Type 6D4 is specified for noise output

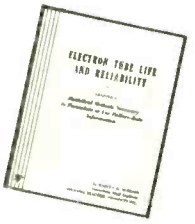
The type 6D4 has been redesigned to meet the requirements of test-equipment manufacturers and is specified to produce, in its output, a wide range of random noise frequencies.

It's the first commercial tube ever to be so specified and typifies the co-operation between Sylvania and equipment manufacturers to produce tubes for special applications.

—Advanced Engineering Series

Series on Electron Tube Life and Reliability is published by Sylvania

As a service to the industry and in an attempt to explore the factors of design and application of reliable tubes, Sylvania is currently publishing a high-level technical discussion on tube reliability in chapter form.



This series is available to electronic engineering staffs through their chief engineer who may request it directly on company letterhead.

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- ☐ premium subminiature tubes
- ☐ type 6788
- ☐ miniature deflection package
- ☐ 110° deflection tubes
- ☐ hybrid auto-radio tubes
- ☐ type 6888
- ☐ computer book
- ☐ 6D4

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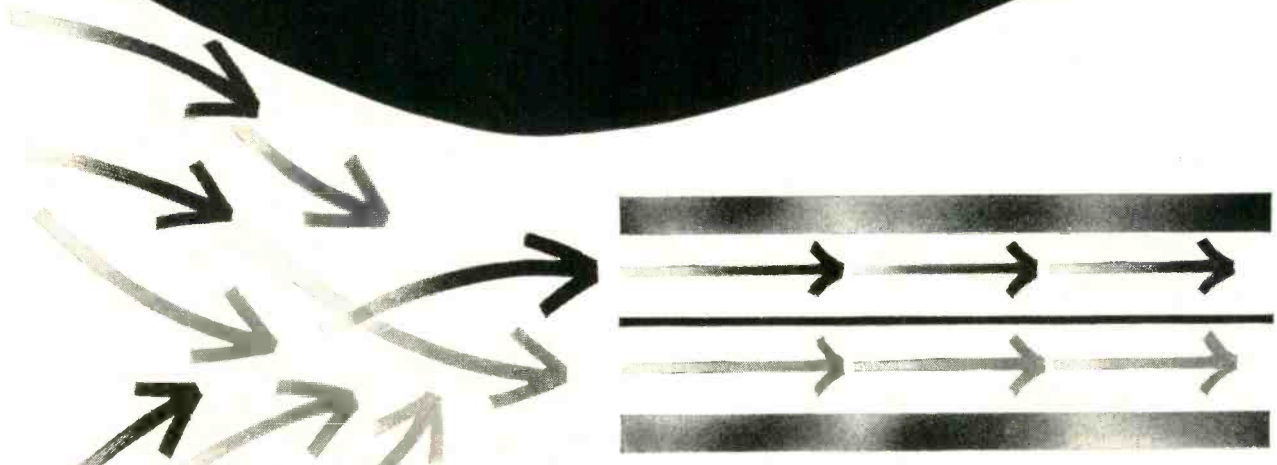

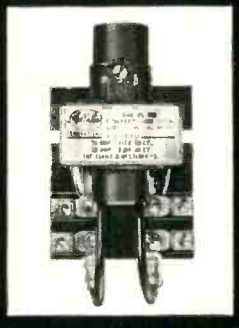

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Oil Circuit Breaker Leads are Insulated and Protected with NATVAR Varnished Seamless Bias

This Federal Pacific Electric Type AJ-54 heavy duty oil circuit breaker, 69 kv, 2000 amp, has a 5000 mva interrupting rating. Interrupting time is 5 cycles with 20 cycle reclosing. Natvar seamless bias cut varnished cambric is used to insulate the current transformers located around each bushing, and the leads from the transformers to the operating control mechanism. Natvar 400 extruded vinyl tubing is also used to protect the conductor between the expulsion chamber and the resistors.

The Pacific Switchgear Division of the Federal Pacific Electric Co., San Francisco, now celebrating its 50th anniversary, manufactures oil circuit breakers to provide protection for large high voltage systems so they may keep pace with rapid load growth, and yet retain the advantages of simplified bus schemes and minimum use of current limiting devices.

Both design and materials play an important part in reliability of performance. Natvar flexible insulating materials are used because of their excellent physical and electrical properties—particularly their resistance to oil—and their exceptional uniformity.

Where performance of electrical apparatus and equipment is important, it pays to specify Natvar flexible insulations. They are always of uniformly high quality, whether supplied from your wholesaler's stock or direct from our own.

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- Varnished cambric—cloth and tape
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- Varnished silk and special rayon
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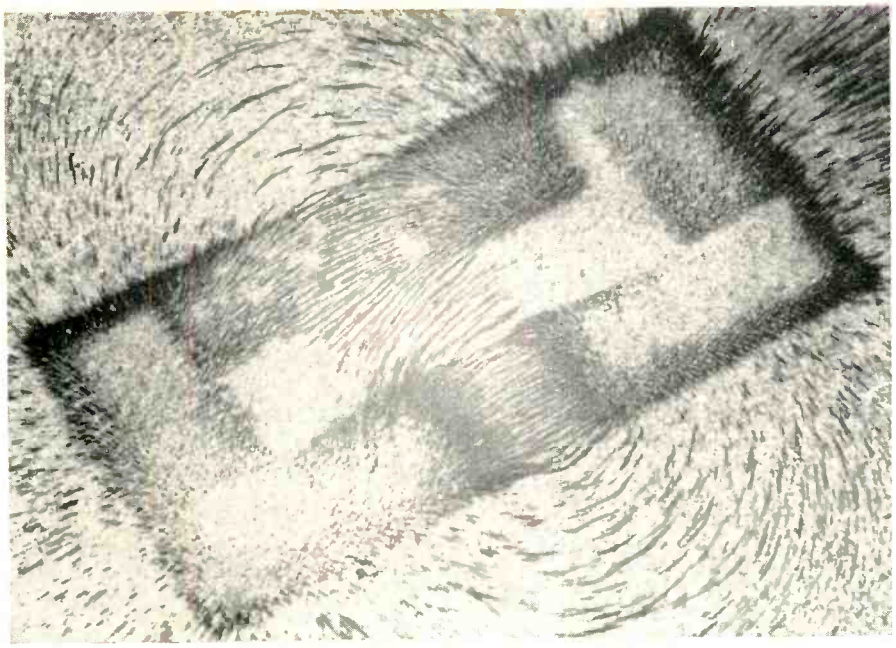


Flux pattern of experimental magnetic circuits

How location of magnets affects magnetic circuits

Adapted from an article by Charles A. Maynard, vice president, Research and Engineering, The Indiana Steel Products Company

The LOCATION of permanent magnets in a magnetic circuit is a definite factor in design. To determine the extent to which this is true, involved calculations are necessary.

A comparatively simple experiment, however, which shows the nature of the changes that take place when permanent magnets are placed in different positions in a magnetic circuit, was devised by Mr. Maynard. The material on which the following questions and answers are based was taken from a report, "An Experiment in Magnet Location," published in Vol. 3, No. 5, of Applied Magnetics. *A copy of this issue is available on request to The Indiana Steel Products Co., Dept. A-2, Valparaiso, Ind.*

Question: What effect does the location of permanent magnets have on a magnetic circuit?

Answer: It has a marked influence on the flux density in the various portions of the magnetic circuit.

Question: Is there a preferred location for magnets?

Answer: Yes, it is important to place the magnets as close to the air gap as possible.

Question: What is the benefit of their location?

Answer: The leakage flux is reduced, and the useful flux in the air gap is increased.

Question: How is this an important factor in design?

Answer: It minimizes the amount of magnet material required to produce a given flux in the air gap.

Question: Does this mean lower magnet costs?

Answer: Generally, this is true. However, structural considerations may prevent the placement of permanent magnets at preferred positions.

Question: Are there available quantitative data which indicate the degree to which magnet position influences the efficiency of a circuit?

Answer: A brief experiment was conducted on the nature and magnitude of the changes that occur when magnets are placed in various positions in a simple magnetic circuit. The results are discussed in *Applied Magnetics*, Vol. 3, No. 5.

World's largest permanent magnet separates electron particles

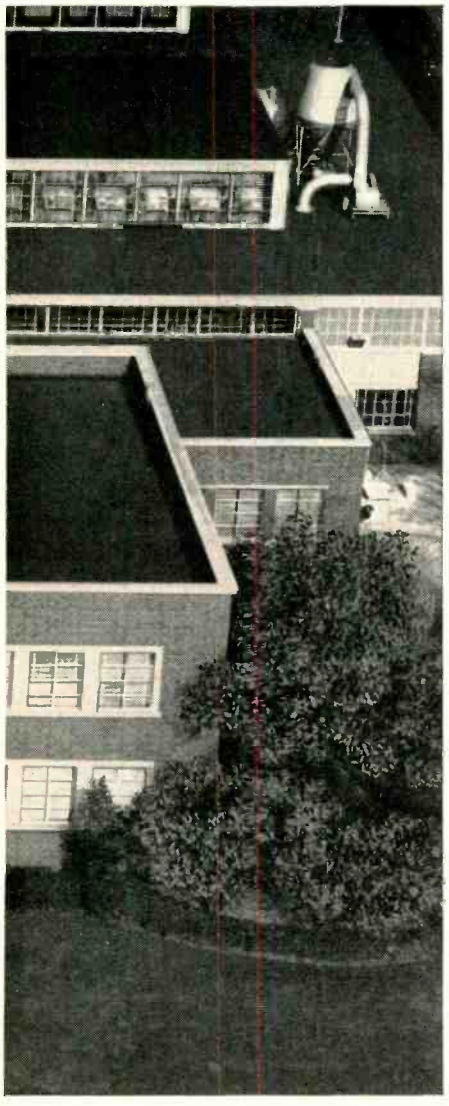
The largest and most powerful permanent magnet ever designed is an important part of a new Mass Spectrometer to be used for high molecular weight hydrocarbon analysis at the Whiting, Indiana, research and development laboratories of a large Midwestern oil company. Function of the spectrometer is to establish a strong magnetic field that separates electron particles.

Indiana's C. A. Maynard inspects air gap of giant Alnico V magnet assembly

The Alnico V permanent magnet used in the assembly has a maximum field strength of 6,000 gauss . . . equal to 10 tons of magnetic holding force . . . and weighs 1,300 pounds. The complete assembly, which weighs approximately 4,700 pounds, was designed and fabricated by The Indiana Steel Products Company, Valparaiso, Indiana.

Headquarters of the Metallurgical Products Department of General Electric Company, 11137 E. 8 Mile. Ave., Detroit 32, Michigan. Carbides, vacuum-melted alloys, and hevimet are made here. G-E permanent magnets and specialty resistors are manufactured in the Edmore, Mich., plant.

CAN LOOK FORWARD TO FROM ELECTRIC'S PRODUCTS DEPARTMENT



The new G-E Metallurgical Products Department is the successor to the Carboloy Department. Here's what this change will mean to you.

Since 1928, the General Electric trademark "Carboloy" has been identified with a brand of cemented carbide. First used solely as a cutting tool material because of their strength and toughness, carbides have more recently become one of the designer's most effective wear-proofing materials.

Carboloy® cemented carbides are manufactured by the new Metallurgical Products Department—successor to the Carboloy Department, which G-E organized to produce this metal for industry. But today carbides are just one of a broad range of products and materials this Department manufactures—many of which do not carry the famous Carboloy trademark.

These include G-E Alnico permanent magnets, thermistors, and Thyrite® varistors which have helped solve many basic design problems in the electrical and electronics industries. And G-E vacuum-melted alloys, and hevimet, which are now making important contributions to advanced aircraft, automotive, and atomic energy programs.

Thus, the new departmental name symbolizes the broadened scope of this Department's activities . . . a scope which will have far-reaching effects for design engineers in every phase of industry.

For General Electric – through its Metallurgical Products Department and the G-E Research Laboratory – is carrying on fundamental investigations which are extending the frontiers of metallurgy.

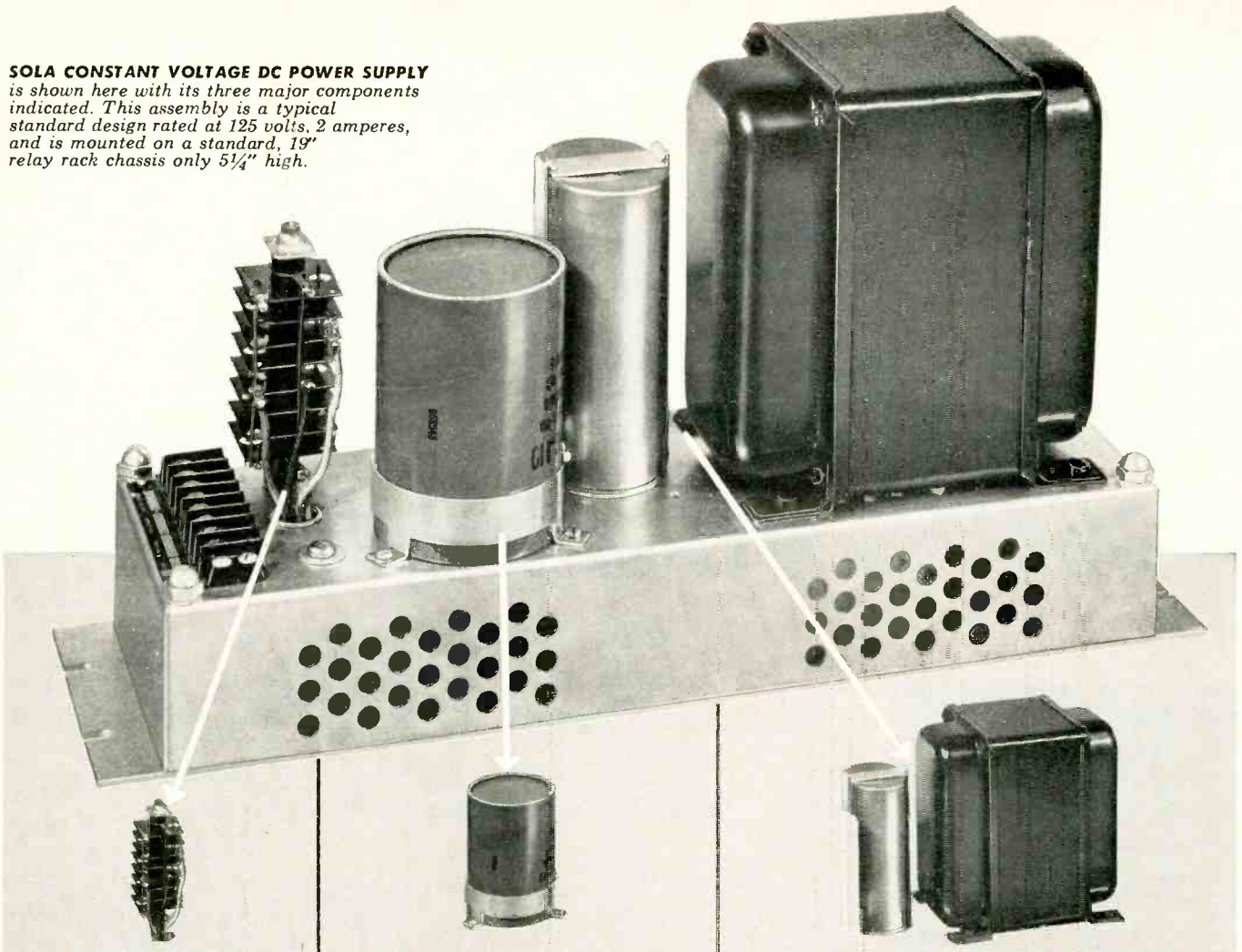
For example, the process which created G-E man-made diamonds may yield new structural and design materials which do not even exist in nature. And General Electric's work in powder metallurgy, metallic oxides, and semiconductors – which produced many of the products mentioned above – has a fascinating future all its own.

New products, and new methods of utilizing these products, are on their way. And when they are developed, they, too, will come to you from the new G-E Metallurgical Products Department.

Progress Is Our Most Important Product

GENERAL ELECTRIC

SOLA CONSTANT VOLTAGE DC POWER SUPPLY *is shown here with its three major components indicated. This assembly is a typical standard design rated at 125 volts, 2 amperes, and is mounted on a standard, 19" relay rack chassis only 5¼" high.*



GERMANIUM RECTIFIER *has unusually-low voltage drop per junction, and high efficiency in proportion to size and cost.*

HIGH-CAPACITANCE FILTER *section constitutes "energy reservoir" for meeting short transient loads; eliminates need for bulky, expensive chokes; reduces ripple voltage to less than 1%.*

CONSTANT VOLTAGE TRANSFORMER *corrects line voltage variations, provides nearly square-wave input to rectifier, limits maximum current delivered through rectifier to filter capacitors and load, permitting economical use of the efficient germanium rectifier.*

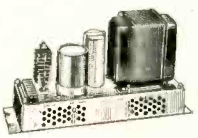
2 amps of 125v regulated dc power in only 5¼" of relay-rack height

Exceptional performance under intermittent, variable, pulse, or high-amperage loads is a prime advantage of the new static-magnetic, Sola Constant Voltage DC Power Supply. Its design simplicity — possible because of the mutual support and protection provided by the combination of its three basic components — provides compact size, low weight, and moderate price in proportion to power output and performance.

Output of these power supplies is regulated within ±1% for line voltage variations of up to ±10%. They are available in six stock models, in ratings ranging from 24 volts at six amperes to 250 volts at one ampere. Also, design-and-assembly service for special ratings is offered to meet the specific requirements of equipment manufacturers.

Your area representative, listed below, is part of a nationwide organization maintained to provide you with prompt service. He'll be happy to supply further information on stock or special Sola Constant Voltage DC Power Supplies.

SOLA *Constant Voltage* **DC POWER SUPPLIES**



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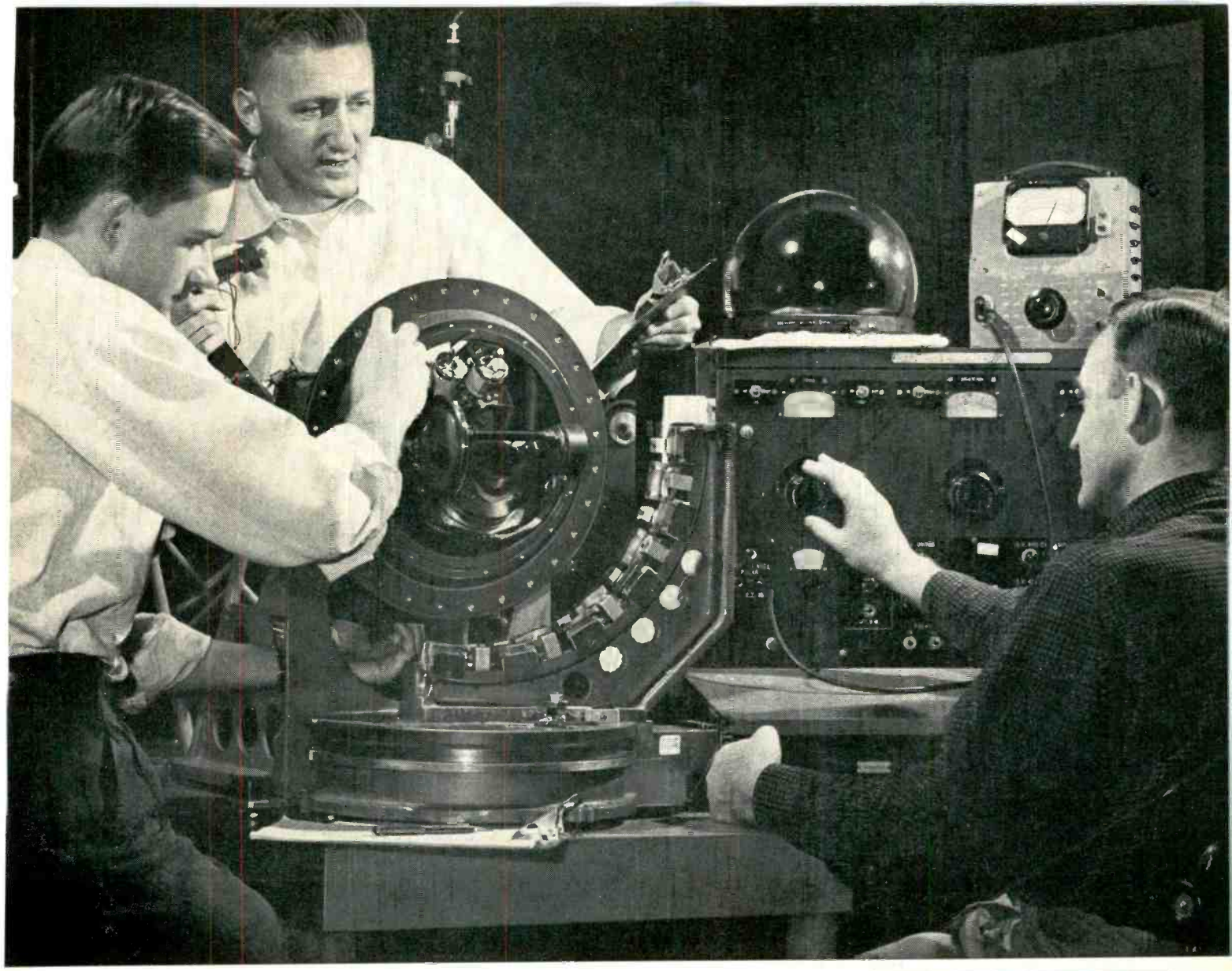

Can you use the talent that built 1,500 Y-4 bombsights on schedule?

These General Mills technicians are representative of the production talent that built more than 1,500 Y-4 bombsights, 1,500 coordinate converters, 1,400 azimuth and sighting angle indicators and 1,400 amplifier and power supply units—and, delivered them to the Air Force on *time*. Here the men inspect a bombsight before it progresses to the next stage of production.

Because we have the highly skilled men—and the men have the specialized tools and machines—we produce precision piece parts or complete, complex assemblies to meet the most exacting requirements.

While building the Y-4 bombsight, we improved original design, exceeded USAF specifications. In addition, our thorough testing facilities assured delivery of only perfect instruments.

Such performance has come to be expected of us and has benefited many other customers. We'd like to help with your production problems too.

Booklet Tells More, explains mechanical and electro-mechanical production facilities. Send to Dept. EL-1, Mechanical Division, General Mills, 1620 Central Ave. N.E., Minneapolis, Minn.

No slow-downs for the B-47—Bombsights ready in advance! During production of the B-47 Stratojet, not a one was kept from the ready-line for lack of a bombsight. The same developmental, engineering and production skills that gave the Air Force on-time delivery are available to speed production of your products.

MECHANICAL DIVISION

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another example of exciting work at los alamos...

PREPARATION OF RaLa SOURCES

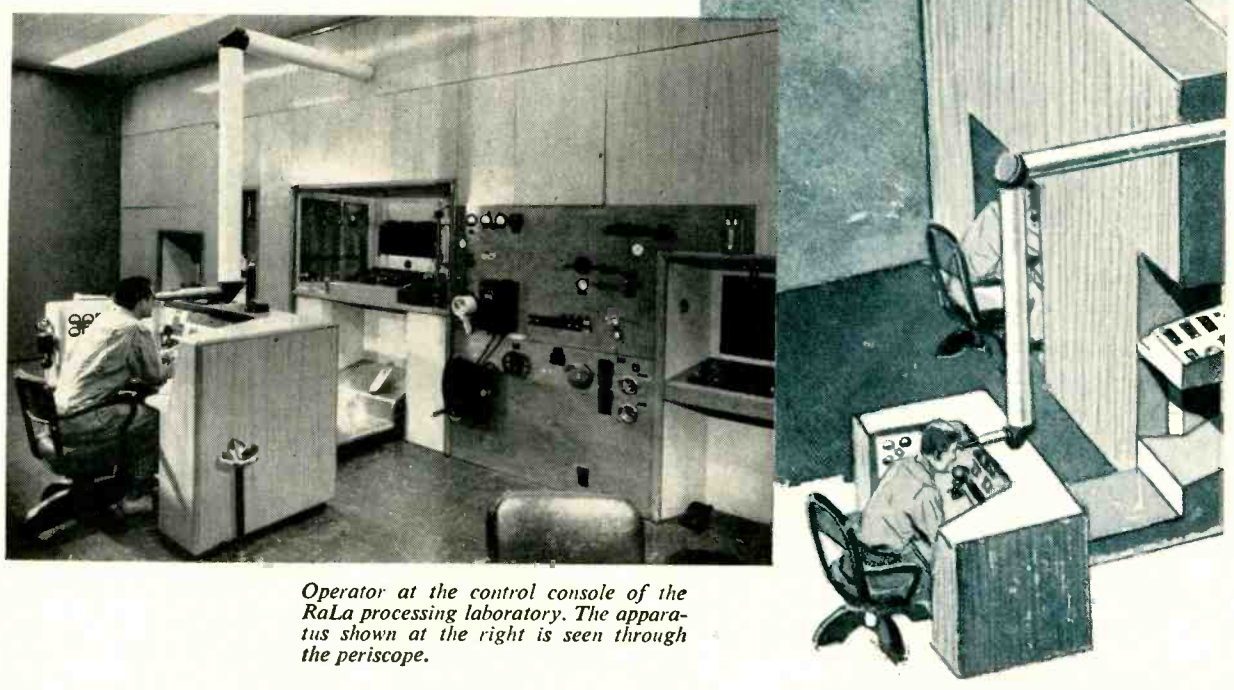
Since 1944 the Los Alamos Scientific Laboratory has pioneered in the study of the effects of intense radiation on chemical, biological and radiographic systems. Among energy sources for such experimentation are extremely small, high-intensity gamma ray emitters containing radioactive lanthanum-140. Known as RaLa, these sources range up to 10,000 curies (370 million million disintegrations per second, equivalent to several times the known amount of the world's extracted radium).

Obviously, preparation of RaLa sources is done entirely with remote-handling equipment largely controlled with pushbuttons and actuated through servo-mechanisms. Design and much of the fabrication of the handling apparatus are also Los Alamos accomplishments and the Laboratory facility is one of the most highly developed in the United States.

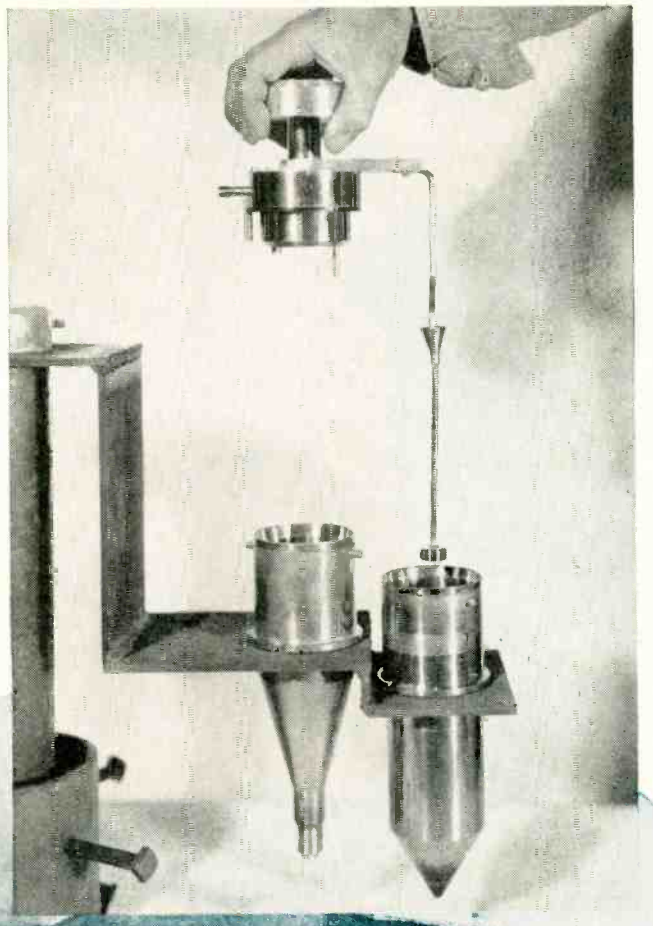
Scientists and engineers interested in these or other projects at Los Alamos Scientific Laboratory are invited to write to:

Director of Scientific Personnel
Division 1703

los alamos
scientific laboratory
OF THE UNIVERSITY OF CALIFORNIA
LOS ALAMOS, NEW MEXICO

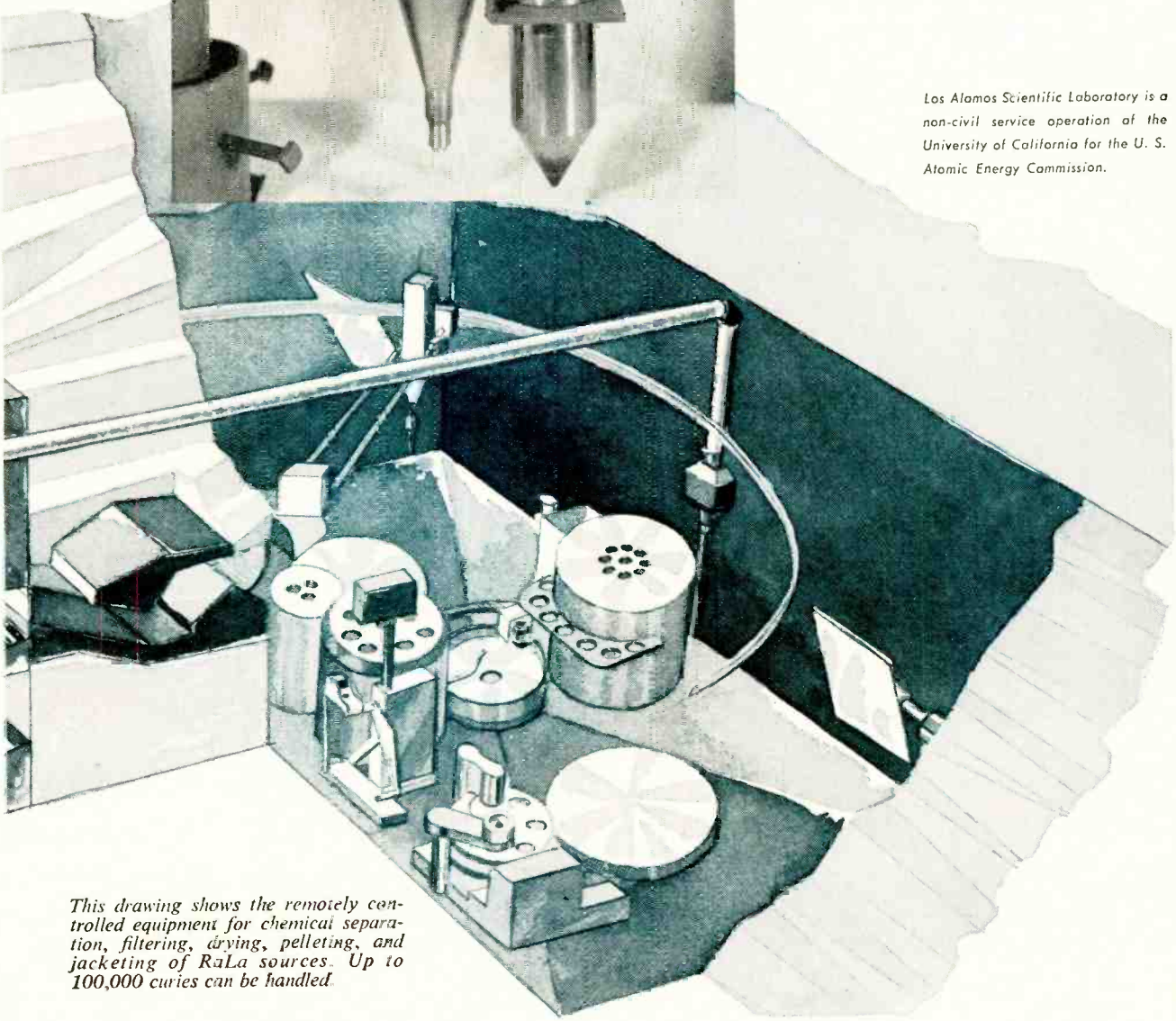


Operator at the control console of the RaLa processing laboratory. The apparatus shown at the right is seen through the periscope.



The apparatus to the left is used for precise alignment of the filtering assembly used in hot cells for RaLa processing. When in actual use it is operated by remote control.

Los Alamos Scientific Laboratory is a non-civil service operation of the University of California for the U. S. Atomic Energy Commission.



This drawing shows the remotely controlled equipment for chemical separation, filtering, drying, pelleting, and jacketing of RaLa sources. Up to 100,000 curies can be handled.

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1. **Uniform over-all size—for uniform windings.**
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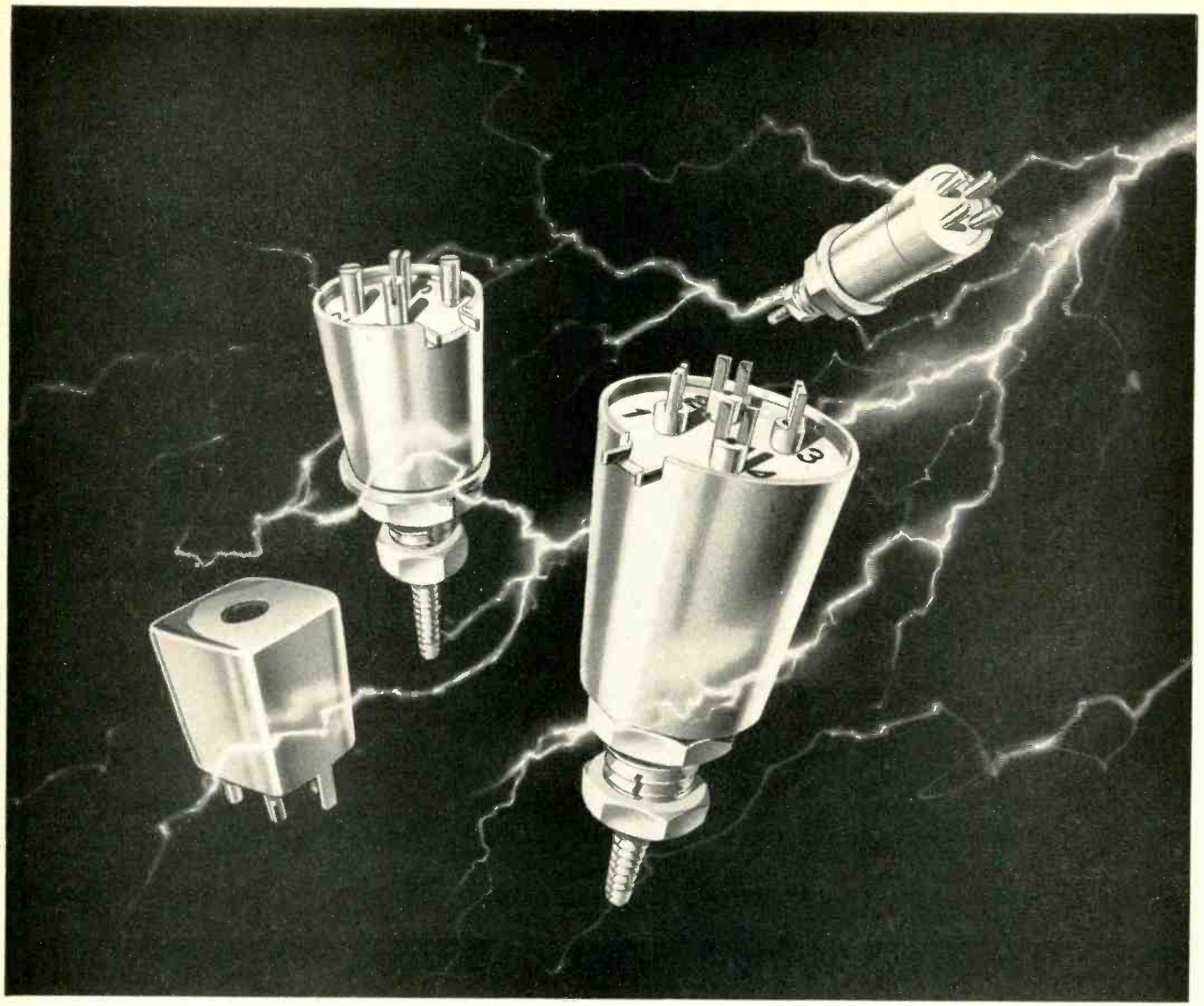


These shielded coil forms offer the utmost in reliability due to their unique design and construction. Dimensions when mounted, including terminals, are: LS-9, 7/16" diameter x 1/2" high; LS-10, 5/8" x 15/16"; LS-11, 15/16" x 17/32". Each form mounts by a single stud. The LS-12 is a square type for printed circuits and measures 1/2" x 1/2" x 1/2". Single layer or pie-type windings to your specifications.

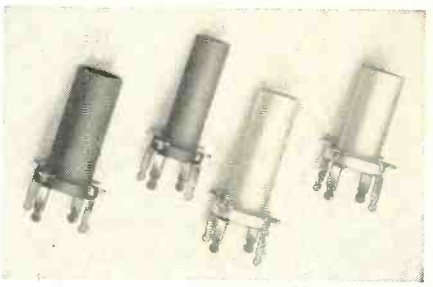
Reliability — under any condition!

CTC miniaturized shielded coil forms are highly shock resistant. With mechanically enclosed, completely shielded coil windings, they bring all the ruggedness and dependable performance you require for your "tight spot" applications — IF strips, RF coils, oscillator coils, etc.

CTC combines *quality control* with *quantity production* to supply exactly the components you need, in any amount. CTC *quality control* includes material certification, checking each step of production, and each finished product. And CTC *quantity production* means CTC can fill your orders for any volume, from smallest to largest.

For samples, specifications and prices, write to Sales Engineering Dept., Cambridge Thermionic Corporation, 437 Concord Ave., Cambridge 38, Mass. On the West Coast contact E. V. Roberts and Associates, Inc., 5068 West Washington Blvd., Los Angeles 16, and 61 Renato Court, Redwood City, Cal.

TYPE SPC phenolic and ceramic printed circuit coil forms can be soldered after mounting. Phenolic forms: 3/4" high when mounted, in diameters of .219" and .285". Ceramic forms: 1/4" diameter, in mounted heights of 5/8" and 15/16", with 19/32" powdered iron core, and collars of silicone fibreglas. Forms come with threaded slug and terminal collar. Units mount through two to four holes, as required. Available as forms alone or wound as specified.



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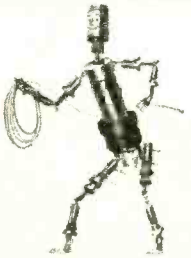
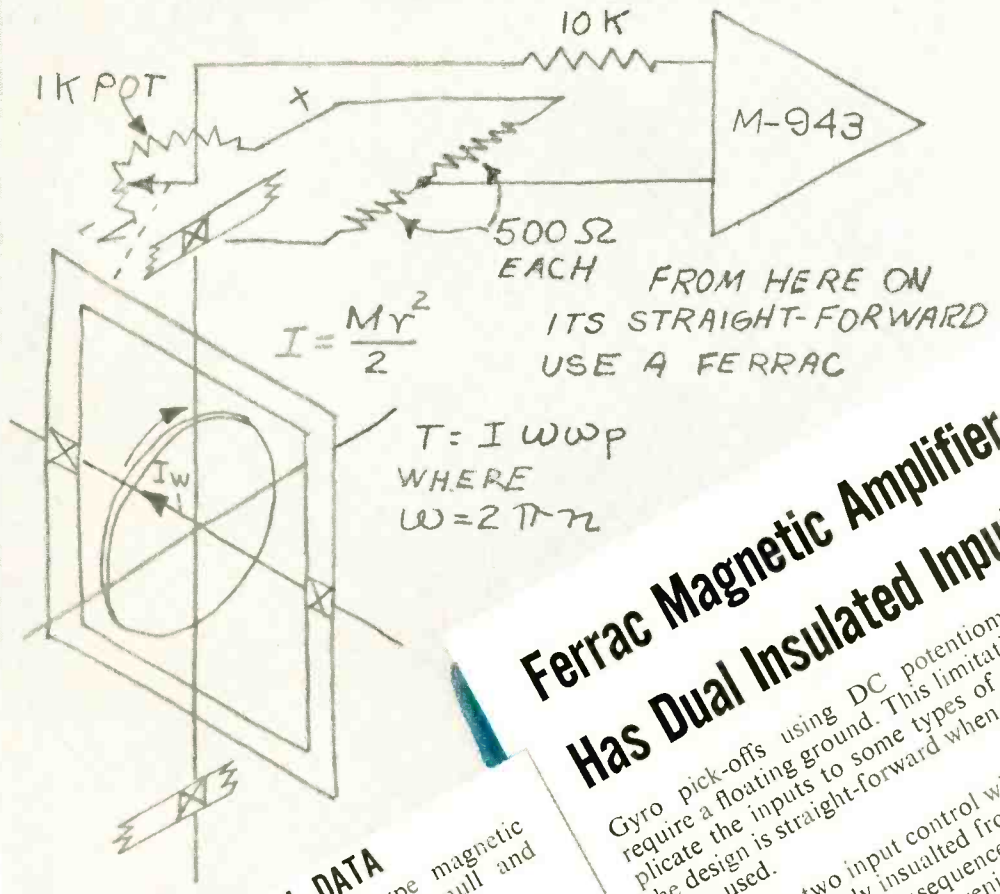


MAGNETIC AMPLIFIER SIMPLIFIES GYRO PICK-OFF



Ferrac Magnetic Amplifier Has Dual Insulated Inputs

Gyro pick-offs using DC potentiometers often require a floating ground. This limitation can complicate the inputs to some types of amplifiers but the design is straight-forward when a Ferrac amplifier is used.

Each of the two input control windings of a Ferrac unit is completely insualted from ground and from each other. As a consequence, the ground connection can be at any convenient point of the input circuit. If another signal, such as a course command, is to be mixed with the gyro signal, it can be fed to the other Ferrac input, again with the ground wherever most convenient.

This flexibility of Ferrac type magnetic amplifiers makes them useful in a variety of guidance equipments. They are sufficiently stable to be used in analog computing portions of such equipments, and are so rugged as to withstand most environmental conditions.

TECHNICAL DATA

Ferrac units are instrument-type magnetic amplifiers having unusually low null and standoff errors.

Input: Two independent control windings for reversible DC.

Output: Unfiltered DC linear over the range ±7.5 volts into 1000-ohm load.

Power Requirements: Less than 3 W at 115±10 RMS volts and 400±40 CPS; no bias supply is needed.

Gain: Gains of typical standard Ferrac amplifiers for each of their two control windings are:

Type	Control B	Control A
M-943	2.5v/100ua	2.5v/100ua
M-1039	0.5v/100ua	10.0v/100ua
M-1057	5.0v/100ua	5.0v/100ua

These gains are expressed as output volts per 100 microamperes of input. Gains are stable within ±1 db.

Environment: Units are rated for operation −55 C to +85 C, withstand vibrations of 10 G at 10 to 2000 CPS, shocks of 100 G for 11 ±1 milliseconds along each principal axis, and are hermetically sealed.

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Large area, thinness and intimacy of collector contact with large copper base provide the efficient thermal transfer.

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Furthermore, these transistors are normalized to retain their performance characteristics regardless of age. Write for engineering data. Delco Radio transistors are produced by the thousands every day.

TYPICAL CHARACTERISTICS

	2N173	2N174	
Properties (25°C)	12 Volts	28 Volts	
Maximum current	12	12	amps
Maximum collector voltage	60	80	volts
Saturation voltage (12 amp.)	0.7	0.7	volts
Power gain (Class A, 10 watts)	38	38	db
Alpha cutoff frequency	0.4	0.4	Mc
Power dissipation	55	55	watts
Thermal gradient from junction to mounting base	1.2°	1.2°	°C/watt
Distortion (Class A, 10 watts)	5%	5%	

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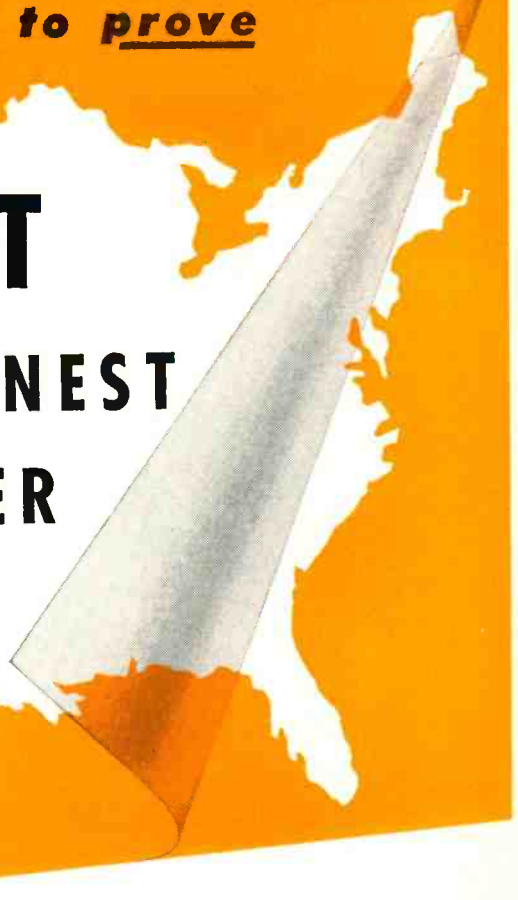

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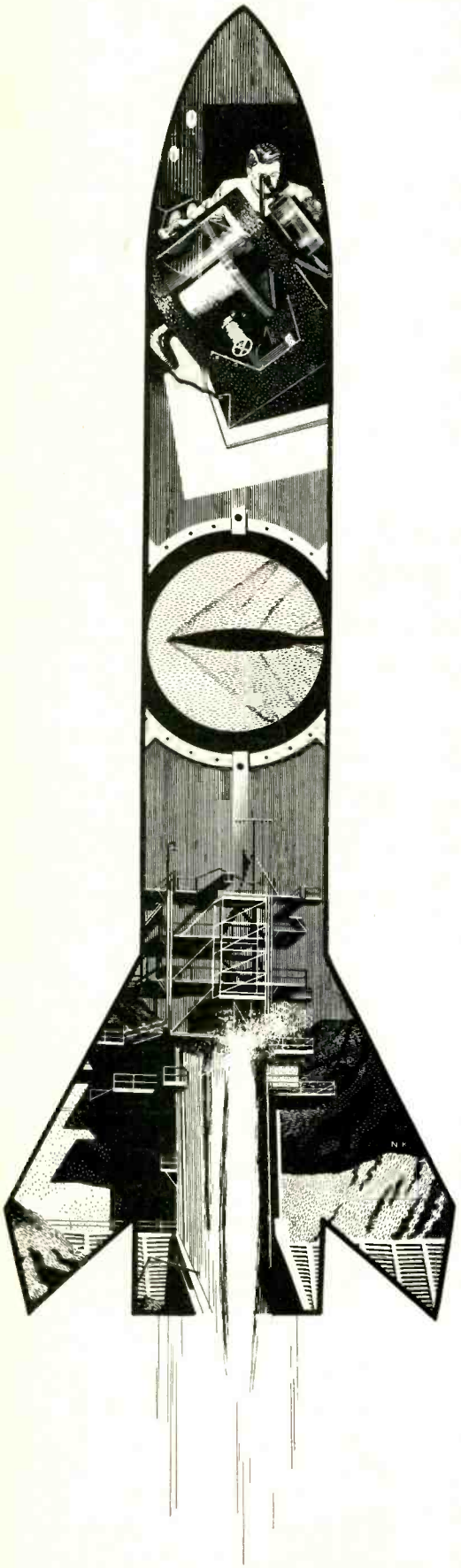


When project engineers at North American Aviation, Inc., needed a special telemetering cable for their advanced guided missile work at various missile test centers, Rome Cable Corporation was asked to make it.

The cable was a tough one to manufacture. The specifications called for exacting dielectric requirements, low-loss characteristics, adequate service life—and a total of 111 conductors—all contained by one heavy-duty jacket.

Because Rome Cable engineers are accustomed to solving tough cable problems like this, they readily produced the cable which met North American's rigid specifications. Rome RoLene—a polyethylene compound—proved perfect for insulating the 37 triplets inside the jacket, and it easily met the specification requirements calling for controlled capacitance and uniform wall thickness. Rome Synthinol, a tough polyvinyl chloride compound, proved to be an excellent jacket material.

Rome Cable can also help you

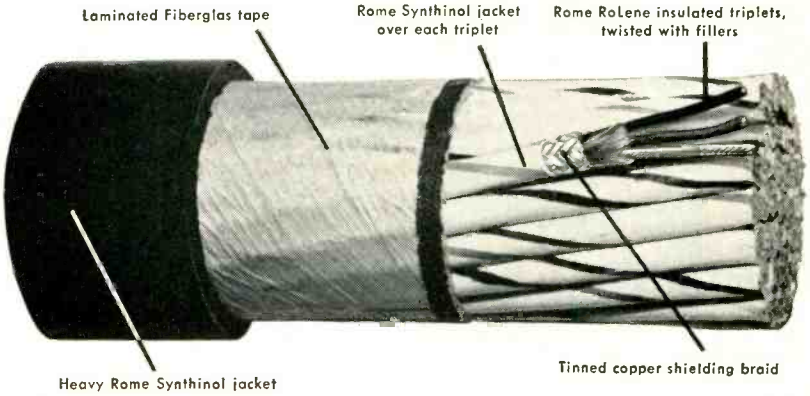
You can turn to Rome Cable with confidence for the right solution to *your* special cabling problems. Rome's competence in its field is, in part, a function of the following factors:

1. Engineering experience. Rome engineers regularly handle complicated specification problems. They've had years of experience dealing with electronic circuit problems.

2. Complete production facilities. The completeness of Rome Cable's manufacturing facilities is unique.

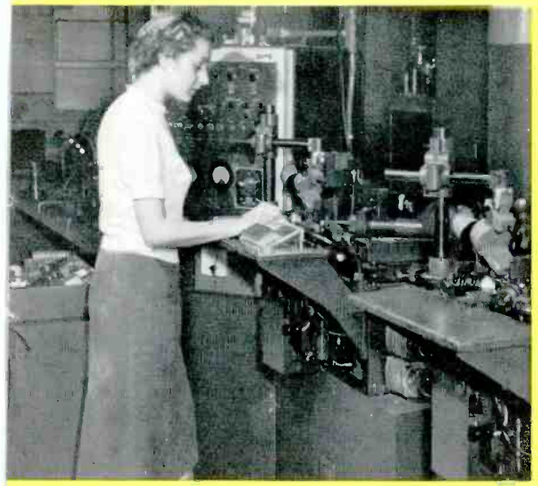
3. Uncompromising quality control. Latest devices, like the photoelectric gauge, are regularly used to assure highest quality. This particular gauge enabled Rome to maintain an exacting control on the diameter limits of insulations and jacket for this special cable.

Rome Cable's engineers can probably be of real help to you on your next cable problem, especially if it is a really tough one. For more information as to what we can do to help you, simply contact your nearest Rome Cable representative—or write to Department 850, Rome Cable Corporation, Rome, N. Y.

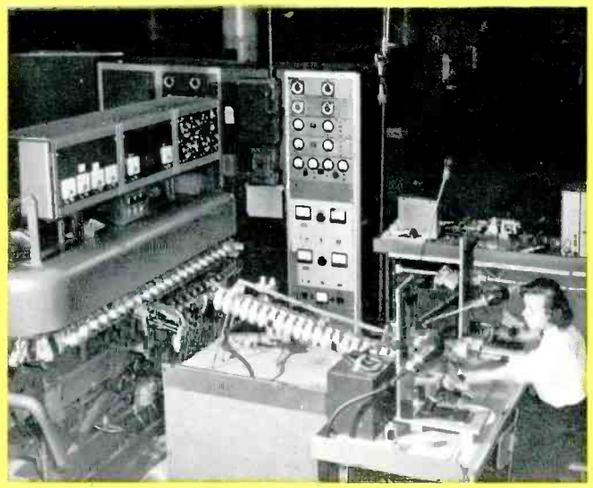


ROME CABLE

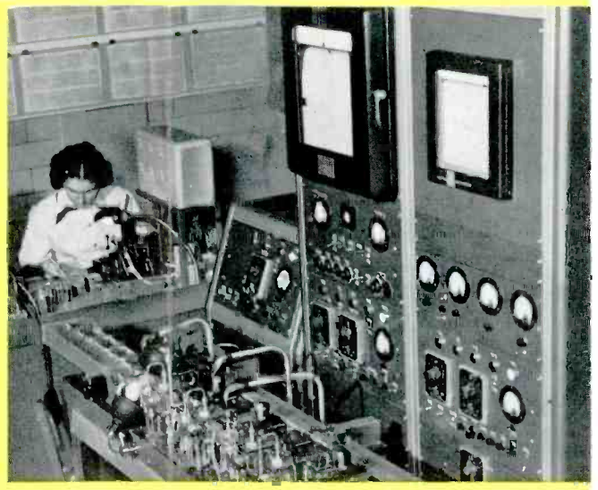
CORPORATION



An exclusive machine, designed by Philco engineers. It's a Surface Barrier Transistor Lead Attacher which feeds, cuts, plates, precisely positions and automatically solders the whisker wire to the transistor emitter and collector.



New Philco automatic "Carousel" assembles and processes alloy junction type transistors. It prepares stems by localized plating, solders stems to transistors, solders leads to emitters and collectors, and follows with electrolytic clean-up etching, dip rinsing and ultra sonic rinsing to remove contaminants.



This exclusive Philco Automatic Transfer Machine performs nine operations in the manufacture of surface barrier transistors. Following each step is a rinsing operation, and finally—hot nitrogen drying. Critical operations are automatically monitored and recorded for quality control.

WITH THIS GREAT NEW AUTOMATED PLANT

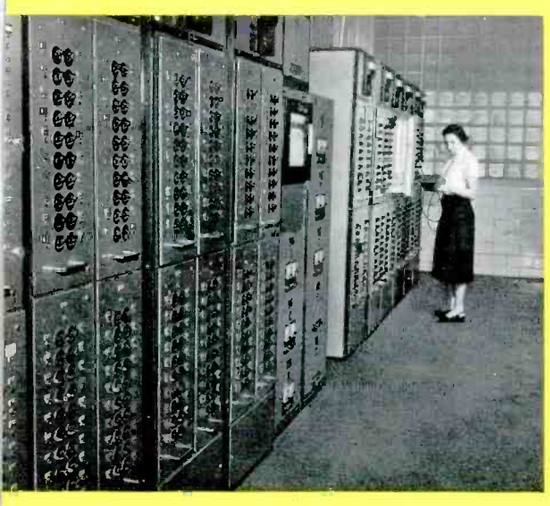
PHILCO

revolutionizes production methods and sets new quality standards in the transistor field

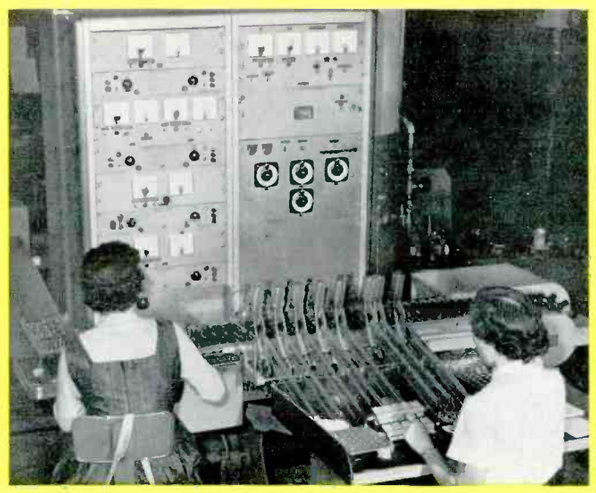
It's the greatest development in transistor history. A complete plant, housing the most advanced transistor manufacturing equipment and utilizing entirely new production methods, is now in mass production at Spring City, Pa. We call it Philco Transistor Center, U.S.A.—and, that's exactly what it is. From this plant come the world's finest transistors—unmatched in quality and reliability.

100,000 square feet of area devoted exclusively to semi conductor production. This plant is equipped with centralized supplies of de-ionized water, vacuum, disassociated ammonia, hydrogen, nitrogen and high purity compressed air, plus complete air conditioning with dust and humidity control.

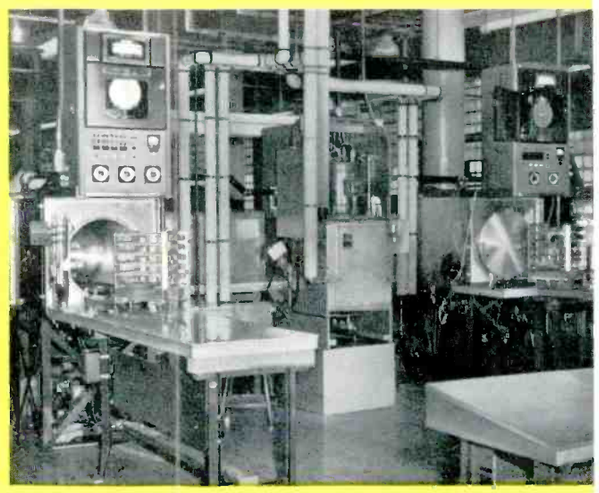
Shown below is a portion of the Life Test Section where all types of Philco transistors are tested under a variety of storage and operational conditions. Individual test positions are provided for over 10,000 units.



The new Spring City Transistor Plant is unmatched for advanced testing methods. Below is a Philco designed high speed Automatic Test Facility for testing seven parameters of power transistors.



Unsealed power transistors in large batches go into vacuum oven (shown below at left) for baking, while simultaneously caps go into vacuum oven (shown at right). After baking cycle the transistors roll on carriers into dry box for cold weld sealing.



NEW METHODS Extensive research, design and planning by Philco engineers has resulted in completely new and far superior transistor production methods. Mass production is now a reality, and special equipment results in closer devise tolerances.

NEW MACHINES Designed specifically for the new mass production methods at Spring City, Pa., machinery completely new in concept is now in operation, with the finest precision control in the industry. These new machines have been designed with the flexibility to accommodate future advances in the transistor field.

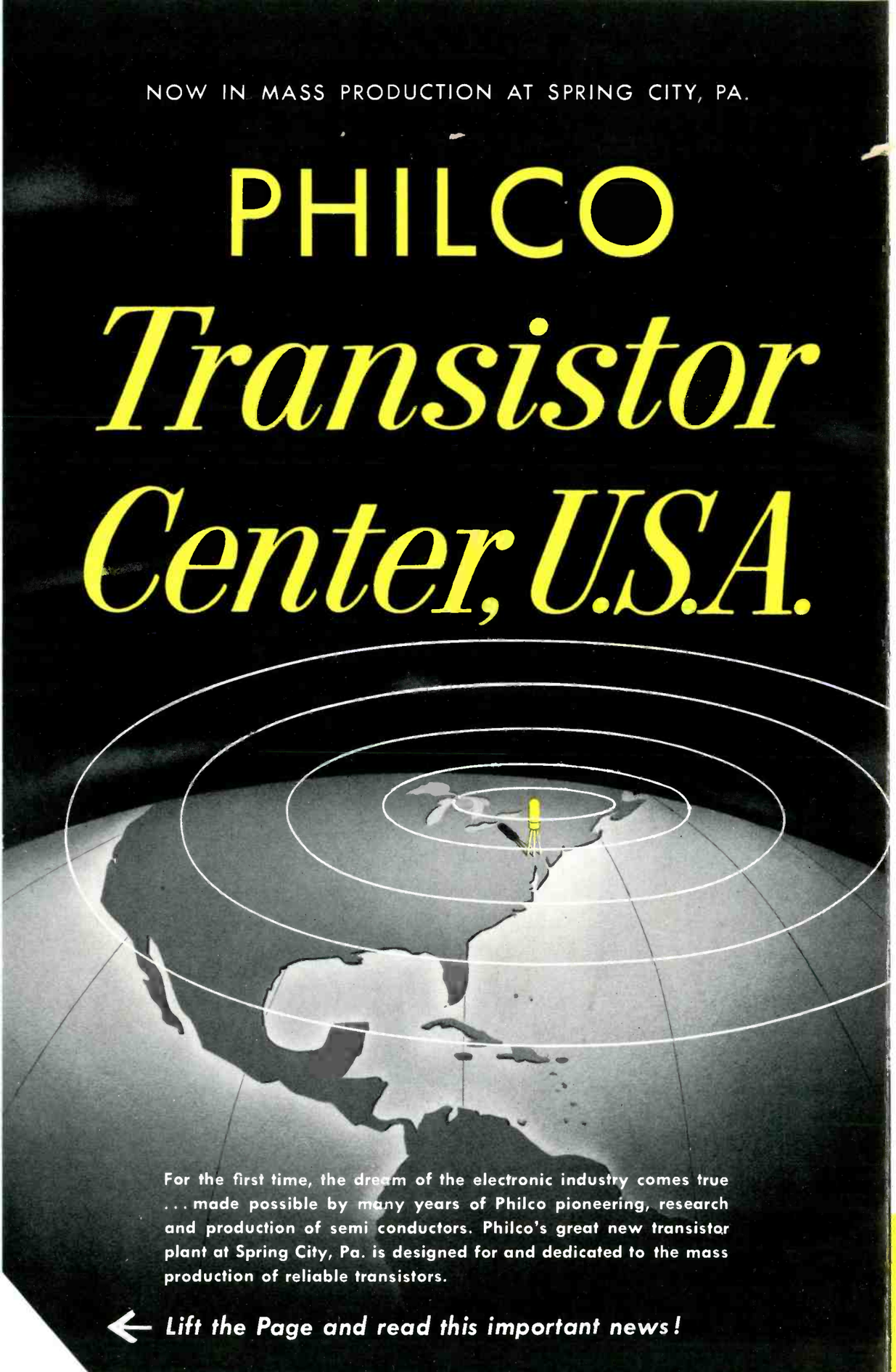
NEW AUTOMATION The result of this new production machinery is automation—more automation than ever before in the transistor field. This automatic equipment eliminates human error, increases production capacity and minimizes contamination.

NEW TEST CONTROLS Automatic test equipment, designed by Philco engineers, tests each transistor at every stage of fabrication. Each vital performance parameter is accurately tested. Environmental and life tests assure utmost reliability.

See Back Page FOR DETAILS ON PHILCO TRANSISTORS

NOW IN MASS PRODUCTION AT SPRING CITY, PA.

PHILCO *Transistor Center, U.S.A.*



For the first time, the dream of the electronic industry comes true . . . made possible by many years of Philco pioneering, research and production of semi conductors. Philco's great new transistor plant at Spring City, Pa. is designed for and dedicated to the mass production of reliable transistors.

Lift the Page and read this important news!

FOR RELIABLE PERFORMANCE, STABILITY OF OPERATION AND LONG LIFE

. . . base your designs on

PHILCO *Transistors*

Proven performance of Philco Hermetically Sealed Transistors has made them the basis for design in commercial and military applications where reliability is the major consideration. Philco transistors range from the world's smallest germanium transistors now in production to silicon transistors with excellent performance at temperatures from —60°C to +150°C. The following are some of the available Philco transistor types:

ACTUAL SIZE

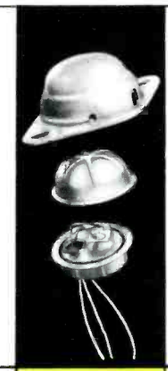
Low Level Transistors

2N207, 2N207A and 2N207B—Germanium PNP Alloy Junction Transistor . . . world's smallest transistor in production. Useful in any low level audio application such as hearing aids where size is an important consideration.

ACTUAL SIZE

Medium Power Transistors

2N223, 2N224, 2N225, 2N226, 2N227 — Germanium PNP Alloy Junction Transistor for portable radio output stages, medium power switching, servo-amplifiers and other applications where medium power must be handled at low frequencies.



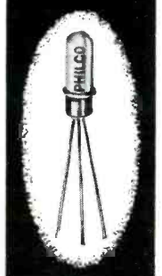
Power Transistors

T1040, T1041—Germanium PNP Alloy Junction Power Transistor with low thermal drop designed for audio output stages, power switching, servo-amplifier output stages and other applications where high power must be handled.

ACTUAL SIZE

High Frequency Transistors

Surface Barrier Types 2N128 and 2N129 —Surface Barrier Transistors for critical military applications, produced to meet MIL-T-12679A (SigC) military requirements.



ACTUAL SIZE

High Speed Switching Transistors

2N240 —Germanium Surface Barrier. High Speed switching transistor with response time in the low millimicrosecond range. Made the basis for design of both military and commercial computers where speed and reliability are essential.

ACTUAL SIZE

Silicon Transistors

T1025, T1159—PNP High Speed Silicon Transistors for computers and amplifiers operating at high ambient temperatures. These transistors feature low saturation voltage.

All Philco transistors are hermetically sealed to insure long life. In addition to the above types, Philco produces a wide range of transistors designed for special applications in accordance with customer requirements. The Philco Micro Alloy Transistor is already in pilot production and tentative specifications and design quantities are available. New and exciting transistor types, such as the Philco Micro-Alloy Diffused Base Transistor, are now in development. In keeping with our policy, specifications will be made available as soon as these units reach pilot production and are available in design quantities.

Make Philco your prime source for complete transistor application information . . . write to Lansdale Tube Company, Dept. I-2, Lansdale, Penna.

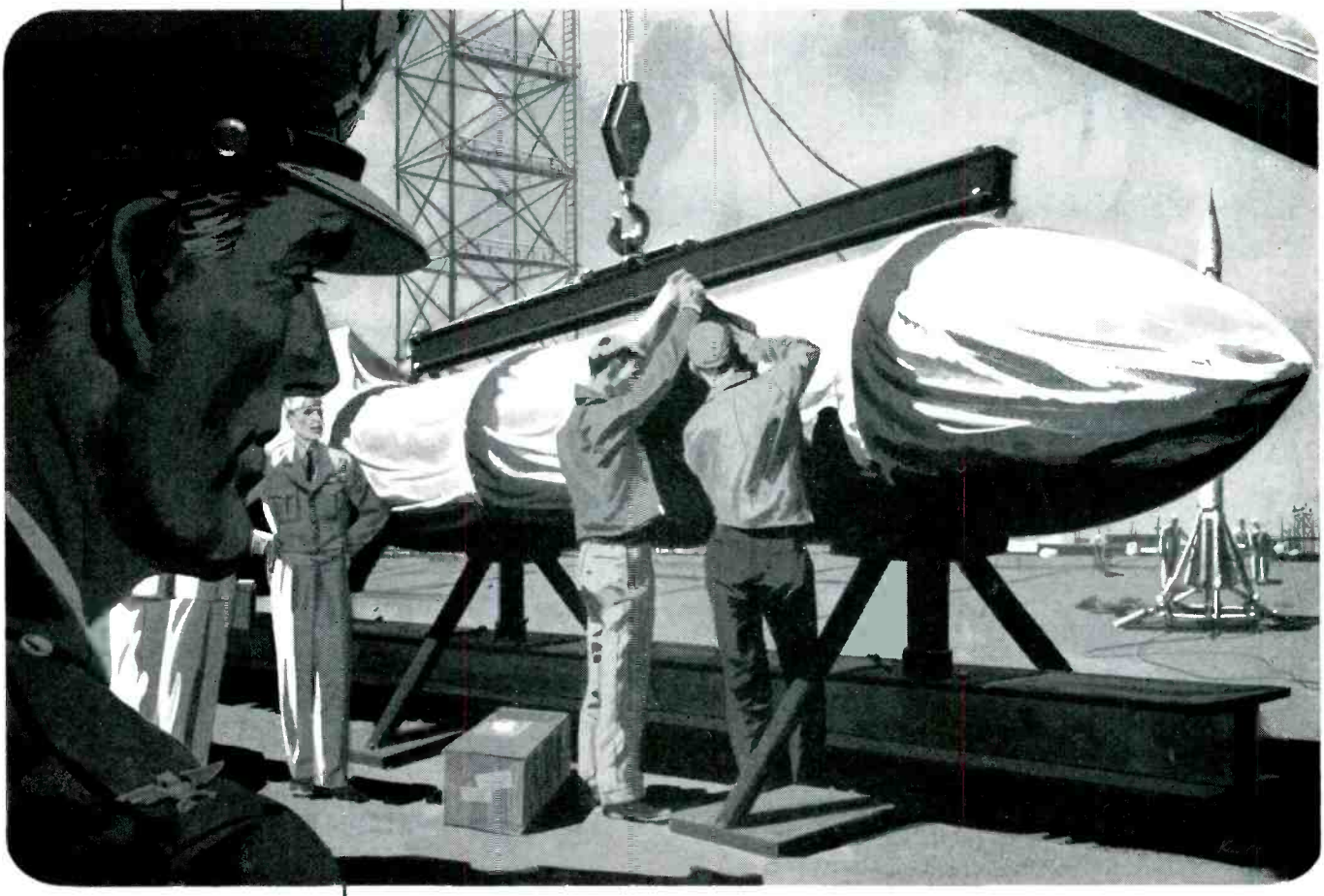
Regional offices—Merchandise Mart Plaza, Chicago 54, Ill.—10589 Santa Monica Blvd., Los Angeles 25, Calif.

PHILCO CORPORATION

LANSDALE TUBE COMPANY DIVISION

LANSDALE, PENNSYLVANIA

IMPORTANT ACHIEVEMENTS AT JPL



Development of the Sergeant

The Jet Propulsion Laboratory is a stable research and development center located north of Pasadena in the foothills of the San Gabriel mountains. Covering an 80 acre area and employing 1600 people, it is close to attractive residential areas.

The Laboratory is staffed by the California Institute of Technology and develops its many projects in basic research under contract with the U.S. Government.

Opportunities open to qualified engineers of U.S. citizenship. Inquiries now invited.

Announced as a successor to the Corporal is another highly accurate surface-to-surface ballistic missile named "The Sergeant." This weapon will continue the United States Army's advance in the development of mobile firepower.

The latest techniques in guidance, airframe design and rocket propulsion are being applied to the development of this rugged weapon which is capable of operating in any area.

The Jet Propulsion Laboratory, designer of this new missile, has the same prime technical responsibility to provide the development of the complete Sergeant system as it had for the Corporal weapon system.

In addition to weapon development the "Lab" carries on supporting research in all areas related to guided missile work. These supporting research and weapon development activities complement and extend each other to produce superior end results.

This fact, coupled with ideal facilities and working conditions at JPL, is a prime attraction for scientists and engineers of unusual ability because of their close integration with such vital programs. At the same time, other varied and interesting activities in weapon development are providing new challenges and openings for qualified people.

JOB OPPORTUNITIES ARE NOW AVAILABLE

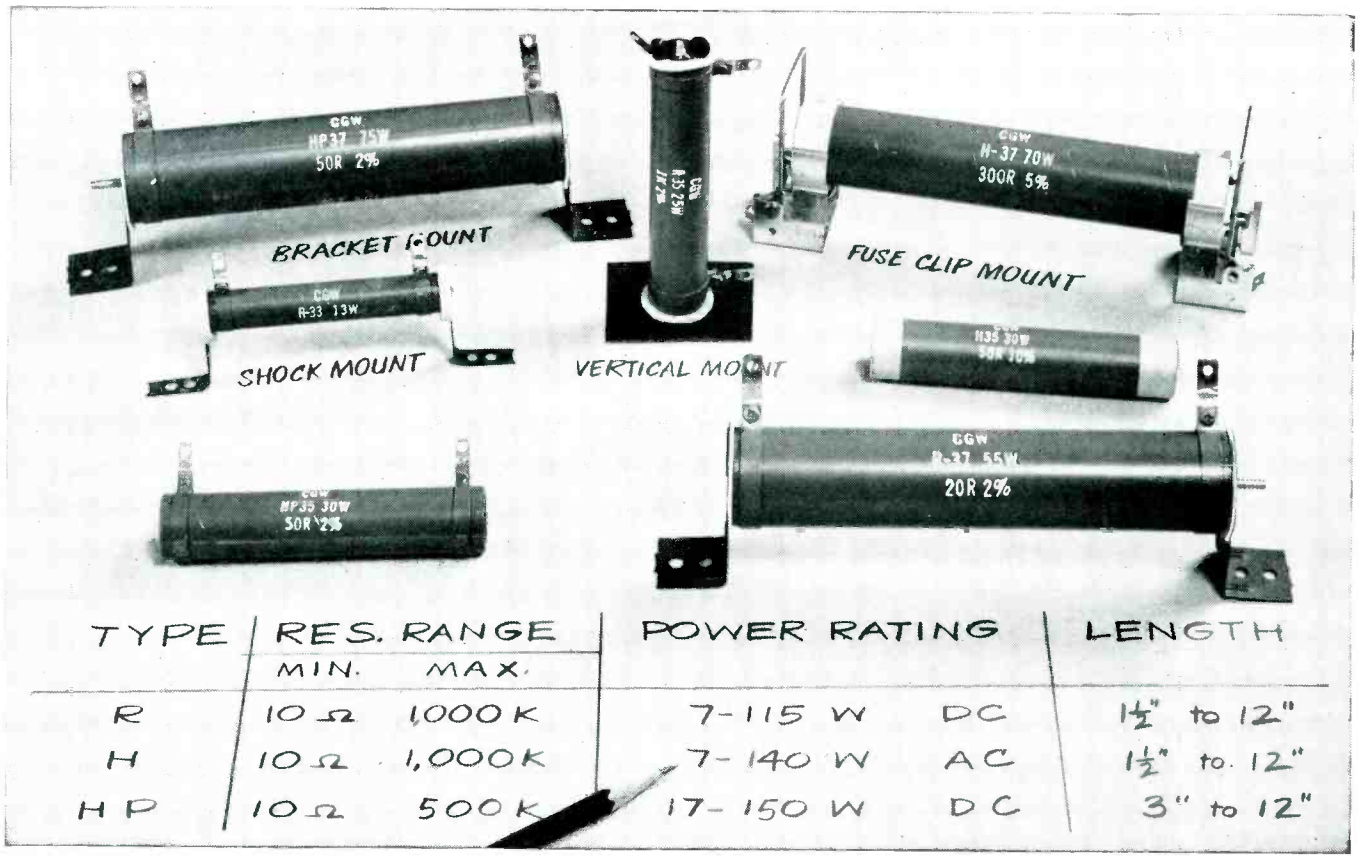
jpl

IN ALL FIELDS OF ENGINEERING AND THE PHYSICAL SCIENCES

COMPUTERS • APPLIED MATHEMATICS • DATA HANDLING • INSTRUMENTATION
APPLIED PHYSICS • TELEMETERING • RADIO AND INERTIAL GUIDANCE • GUIDANCE ANALYSIS
SYSTEMS ANALYSIS • ELECTRO-MECHANICAL • MICROWAVES • PACKAGING
MECHANICAL ENGINEERING • AERONAUTICS • MECHANICAL • STRUCTURES • DYNAMICS
PROPULSION • APPLIED MECHANICS • INERTIAL ELEMENTS • METALLURGY
CERAMICS • SOLID STATE PHYSICS • OPERATIONS RESEARCH

JET PROPULSION LABORATORY

A DIVISION OF CALIFORNIA INSTITUTE OF TECHNOLOGY
PASADENA • CALIFORNIA



TYPE	RES. RANGE MIN.	RES. RANGE MAX.	POWER RATING		LENGTH
R	10 Ω	1,000 K	7-115 W	DC	1½" to 12"
H	10 Ω	1,000 K	7-140 W	AC	1½" to 12"
HP	10 Ω	500 K	17-150 W	DC	3" to 12"

Why Corning High-Power, High-Frequency Resistors meet your most exacting circuit requirements

You'll find Corning High-Power and High-Frequency Resistors designed for stable, long-life service—even under the most difficult operating conditions.

With Corning Resistors you get the highest resistance range for a given physical size compared to wire-wound resistors.

Their thin-film construction makes them inherently non-inductive. The noise level of these resistors is so low it's difficult to measure. The resistive film is a metallic oxide, fused to the PYREX glass core at red heat to form a permanent bond. This special glass insures highest core resistivity even at elevated temperatures, great resistance to chemical attack and to mechanical and thermal shock.

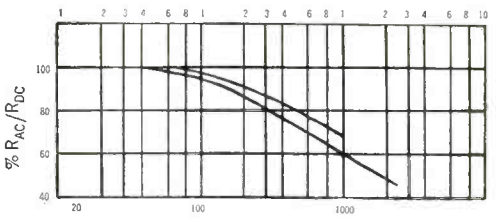
These Corning Resistors are remarkably stable regardless of moisture and humidity.

The chart in the next column gives you a quick idea of their exceptional frequency characteristics.

The ranges and ratings shown in the illustration are for our standard lines, but we can design and build resistors to match your own requirements for all usable frequencies. We've made specials with ratings up to 150 kw. and we can go higher.

Within the standard range of these resistors, we can give you wide variations in mounting hardware. You can get hardware for vertical or horizontal mountings and mountings to absorb mechanical shock and severe vibration. Ferrule-type terminals are available for use with standard fuse clips.

Our catalog sheets give far more complete details than we are able to here. We'll be glad to send you copies with current price lists.



Ask for information on these other Corning Resistors:

Low-Power—3-, 4-, 5-, and 7-watt sizes. Highest resistance range of any low-power resistor.

Type S—Stable performance to 200° C. Meet MIL-R-11804A specs. Values to 1 Megohm.

Type WC-5—5 KW water-cooled. Range, 35 to 300 ohms. Versatile, adaptable.

Type N—Accurate grade. Made to meet all requirements of MIL-R-10509A. Characteristics X and R.

Specials—To your specifications—Co-axial Line Elements, Dummy Loads, HF Elements, Peak Pulse Loads, High-Voltage Resistors.

Other products for Electronics by Corning Components Department: Fixed Glass Capacitors*, Transmitting Capacitors, Canned High-Capacitance Capacitors, Subminiature Tab-Lead Capacitors, Special Combination Capacitors, Direct-Traverse and Midget-Rotary Capacitors*, Metallized Glass Inductances, Attenuator Plates.

**Distributed by Erie Resistor Corporation*

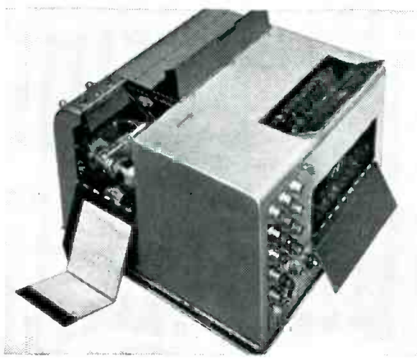
CORNING GLASS WORKS, 94-2 Crystal Street, **CORNING, N. Y.**
Electronic Components Department

Corning means research in Glass

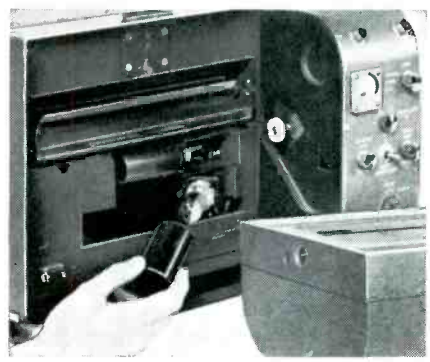
HERE'S HOW GENERAL ELECTRIC'S

New PM-20 Oscillograph Helps Reduce Costs

NEW EASY-ACCESS DESIGN, MANY CONVENIENCE FEATURES MAKE OPERATION AND MAINTENANCE EASIER, SAVE TIME AND MONEY



EASY-ACCESS DESIGN permits reaching all parts easily through hinged doors. For complete access, simply turn 3 fasteners and entire cover may be quickly removed.



SEPARATE VIEWING LAMP permits viewing without disturbing the recording lamp adjustment. Both lamp holders swing out for easy lamp removal and replacement.

NEW G-E FEATURES SAVE TIME

General Electric's new general-purpose oscillograph, the PM-20, is uniquely designed for easier, time-saving operation and convenient maintenance.

UNIQUE 71-GALVANOMETER CAPACITY in two banks gives you new versatility in measuring and recording many variables simultaneously. A wide range of frequencies—from d.c. to 6000 cps—can be recorded at speeds from 0.8 to 100 inches per second with the new oscillograph.

ONLY TWO IDLER GEARS TO CHANGE for entire speed range, and both are always in use, eliminating storage and the chance of loss. No tools are needed for changing idler gears to get new ranges.

MAGNETIC SPOOLS in the record holder reduce loading time. No fumbling—the spools automatically position themselves correctly in the record holder.

AUTOMATIC SHUTTER on record holder closes as the record holder is removed, preventing fogging of records.

AUTOMATIC RECORD NUMBERING, timing lines, the trace interruption for identification, and automatic record-length control are additional features which give you easy, reliable operation.

FOR MORE INFORMATION, contact your nearest G-E Apparatus Sales Office or write for Bulletin GEA-6348 to Section 585-36, General Electric Company, Schenectady 5, New York.

GENERAL ELECTRIC

No blue sky...just to back up our belief that you and Collins

We're going to build a proposition which we believe deserves your most serious consideration, if you are a mechanical or electrical engineer. This proposition is built on pure and simple fact—no high flown promises or broad generalities. Our proposition: you and Collins should get together. We present these facts to support it.

FACT NUMBER 1:

Collins Radio Company's sales have increased 10 fold in each of three successive seven year periods. 1933 sales were $100,000; 1940 sales, $1,000,000; 1947 sales, $10,000,000; 1954 sales, $100,000,000, and 1956 sales, $126,000,000. (Note graph.) This company *has grown, and is growing* at a phenomenal rate. Total employment is 9,000 of which 24% are research and development personnel.

You grow when the company you work for grows.

FACT NUMBER 2:

As shown in the graph at right, the employment of research and development personnel has increased steadily despite fluctuation in sales. Notice that even during periods of national sales regression Collins continued to strengthen its engineering staff.

Collins has based its growth on the solid foundation of stability in the engineering department.

FACT NUMBER 3:

At Collins, the ratio of engineers to total employees is extremely high, far higher than the average among established companies engaged in both development and production. First and foremost, Collins is an engineering company.

Engineering is king at Collins—never takes a back seat to production expediency.

FACT NUMBER 4:

Collins' reputation for quality of product is universally recognized. It has led to Collins' phenomenal sales record. At Collins there is no compromise when quality is at stake.

If you're the man we want, you'll get real satisfaction out of this quality-consciousness.

FACT NUMBER 5:

Electronics is Collins' only interest. In no way is it subsidiary to the manufacture of industrial or consumer products. Collins builds electronic equipment, not airplanes or vacuum cleaners. Every research, development and production facility is devoted to progress in electronics.

If electronics is your interest, you'll like the climate at Collins.

FACT NUMBER 6:

There is a limitless variety of fields and types of work for the Collins engineer. Recent Collins work in air and ground communication, and aviation electronics include developments in transhorizon "scatter" propagation; single sideband; microwave and multiplex systems; aircraft proximity warning indicator; aviation navigation, communication and flight control; broadcast; and amateur equipment.

There is big opportunity for your special talents.

Right now we are prepared to offer you a technical or supervisory assignment in one of many interesting fields. And the sky *is* the limit as far as responsibility and salary are concerned.

You will work in one of Collins' new research and development laboratories located at Cedar Rapids, Iowa; Dallas, Texas; and Burbank, California. Offices and subsidiary companies are located in New York; Washington, D. C.; Miami; Knoxville; Seattle; Hickman Mills, Missouri; Toronto, Canada; London, England; and South America.

All your moving expenses are paid. Company benefits are tops in the industry.

We repeat—if you are a mechanical or electrical engineer, you and Collins should get together. Take the first step now, send your resume today to:

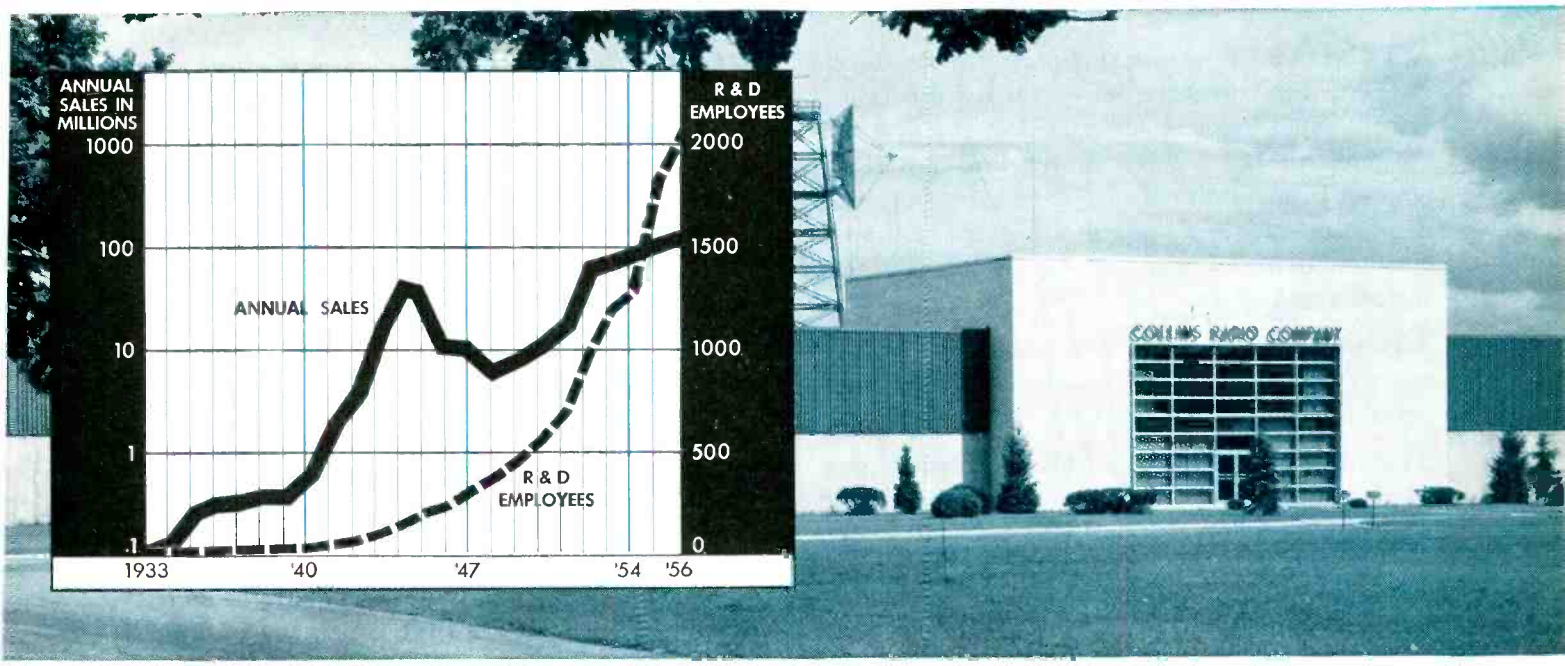
L. R. Nuss
Collins Radio Co.
Cedar Rapids, Iowa

Fred Aiken
Collins Radio Co.
2700 W. Olive Ave.
Burbank, California

Harold McDaniel
Collins Radio Co.
1930 Hi-Line Drive
Dallas, Texas

black and white facts

should get together



This graph shows the relationship between sales and employment of engineering personnel at Collins. Notice the steady increase in research and development employment despite sales fluctuations.

Collins new research laboratory building at Cedar Rapids, Iowa. Air-conditioned, shielded against radio waves, completely equipped.

Collins

CREATIVE LEADER IN ELECTRONICS

COLLINS RADIO COMPANY • CEDAR RAPIDS • BURBANK • DALLAS

COLLINS

MALLORY

Completely new design concept eliminates usual button contact, provides larger contacting area. New units have far longer life, lowest noise level yet . . . but cost no more.

Vibrator life increased 50 to 100% . . . in

newest Mallory design

STANDARDS of vibrator performance never before possible are being set by the latest development in Mallory vibrator engineering. Through the use of new design and materials, contact is made directly between vibrating reed arm and side arm—eliminating conventional contact buttons—providing far greater contacting area and longer life.

And in addition, a further refinement in the mounting of the vibrator establishes a new high standard of quieter operation.

The results of these new design concepts are important to everyone who designs, makes or uses vibrator-powered equipment.

Life is increased 50 to 100% . . . due to greater contacting area and far lower rate of wear.

Sticking of contacts is eliminated.

Complete uniformity of characteristics is made possible by this simplified design, which permits automatic production and adjustment techniques.

Extra-quiet operation. Mechanical hum is held to a new low level, due to the lighter mass of the mechanism, and to noise-squelching Mallory refinements.

Smaller size for equivalent load rating.

The new Mallory 1600 series vibrator is now available for auto radios, headlight dimmers, garage door openers and many other applications. In addition, the new leaf spring contacting concept is available in another new Mallory vibrator—the 1700 series for two-way communications equipment and other heavy duty applications.

Serving Industry with These Products:

Electromechanical—Resistors • Switches • Television Tuners • Vibrators
Electrochemical—Capacitors • Rectifiers • Mercury Batteries
Metallurgical—Contacts • Special Metals and Ceramics • Welding Materials

Parts distributors in all major cities stock Mallory standard components for your convenience.

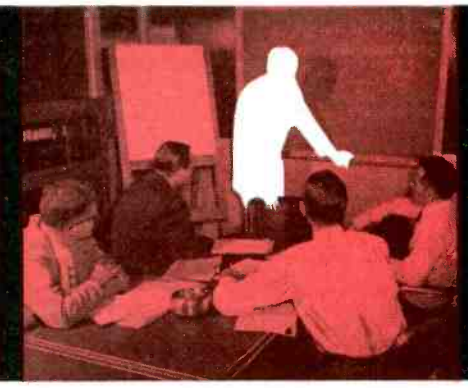
Expect more . . . Get more from

P. R. MALLORY & CO. Inc.
MALLORY

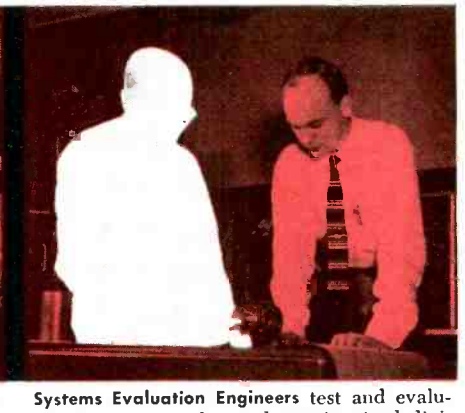
P. R. MALLORY & CO., Inc., INDIANAPOLIS 6, INDIANA

Where do you belong in

Computer Circuit Design Engineers plan electronic circuitry for advanced airborne analog and digital computers . . . design linear and pulse circuits employing transistors, tubes, magnetic devices. Opportunities also exist in airborne power supply design, or to develop new techniques for marginally checking computer performance. *Do you belong on this team?*



Computer Logical Design Engineers determine the systems outline of a computer and its inter-connection with external equipment. Close liaison is maintained with mathematical support, circuit design, packaging and test engineers. Computer speed, memory size, configuration and arithmetic structure are tailored to requirements of weapons systems. *Do you belong on this team?*



Systems Evaluation Engineers test and evaluate electronic analog and transistorized digital computer systems design for aircraft; evaluate new systems and improvements to insure compliance with specifications and Air Force requirements. Other assignments: tie-in testing of peripheral equipment, liaison with design, development and field engineering. *Do you belong on this team?*

Harry Branning (center): B.S.E.E. 1950, Syracuse. Design Engineer in circuit design, 1951; October, 1954, promoted to Associate Engineer; April, 1956, promoted to Staff Engineer, Systems Planning. In June, 1956, appointed Project Engineer and Manager of the 110 Computer Circuit Design Department; discussing the performance and packaging details of a transistorized read amplifier.

William Dunn (standing): M.E. 1950, M.S.E.E. 1952, Stevens Institute. Technical Engineer, 1955; April, 1956, promoted to Associate Engineer; August, 1956, transferred to Development Engineering in charge of Logical Design for digital computers in advanced weapons systems; here discussing Boolean Algebra method of optimizing the logical design of an airborne digital computer.

Eli Wood (left): B.S.E.E. 1950, Connecticut. IBM Customer Engineer, July, 1950; September, 1952, transferred to ACL Field Engineering. February, 1954, in charge of Field Engineering at Hunter AFB; May, 1955, Associate Engineer; appointed Project Engineer, Manager of Systems Evaluation in August, 1956; here investigating a problem in radar data presentation set evaluation testing.

The brief records of the men cited above indicate only a few of the exciting activities right now in IBM Military Products. This division, organized 18 months ago, has grown enormously. A small-company atmosphere prevails. Men work in small teams . . . individual contributions are instantly recognized. Promotions occur frequently.

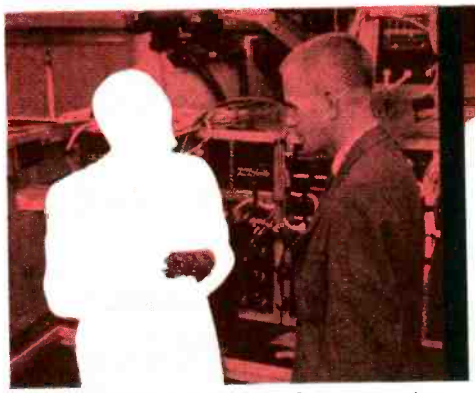
As a member of IBM Military Products, you'll enjoy physical surroundings and equipment second to none. Educational programs at IBM expense lead to advanced degrees. Salaries and benefits are excellent. Stability is guaranteed by IBM's history of consistent achievement—underlined by the fact that the rate of turnover at IBM is only one-sixth the national average.

Throughout the length and breadth of the United States IBM has built modern plants and laboratories. This map points out the various locations where you might live as an IBM em-

DATA PROCESSING
ELECTRIC TYPEWRITERS
TIME EQUIPMENT
MILITARY PRODUCTS

IBM® MILITARY PRODUCTS

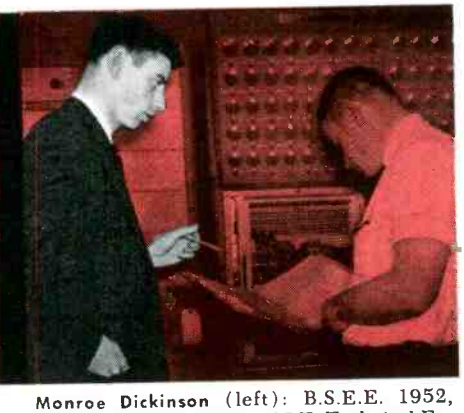
IBM Military Products?



Systems Engineers oversee the engineering support provided by the Systems Coordination and Specification Group to the factory on the AN/ASB-4 Bombing-Navigational System. Air Force requirements are analyzed and the resulting engineering changes evaluated to determine effect on system performance and accuracy. Mathematical error analyses are run. *Do you belong on this team?*

Systems Analysts anticipate performance and recommend design criteria before and during development of equipment. Later, they compare dynamic performance accuracy and reliability characteristics with what has been anticipated. Other assignments include Digital Computer Systems Engineering, Input-Output and Analog-Digital Conversion Engineering. *Do you belong on this team?*

Quentin Marble (left): B.S.M.E. 1951, Syracuse. Joined IBM in 1951; promoted to Design Engineer in 1952; May, 1955, promoted to Associate Engineer, and then to Project Engineer, Manager of the Systems Coordination and Specification Group, Production Engineering Department, in February, 1956; shown here describing a unique cooling design to a new employee in his group.



Monroe Dickinson (left): B.S.E.E. 1952, W.P.I.; M.S.E.E. 1954, M.I.T. Technical Engineer in analog and alternate computer techniques for weapons systems, 1952; Associate Engineer responsible for systems design and analysis, 1954; December, 1955, Staff Engineer, responsible for research planning; here reviewing set-up on laboratory analog computer of a sampled data control problem.

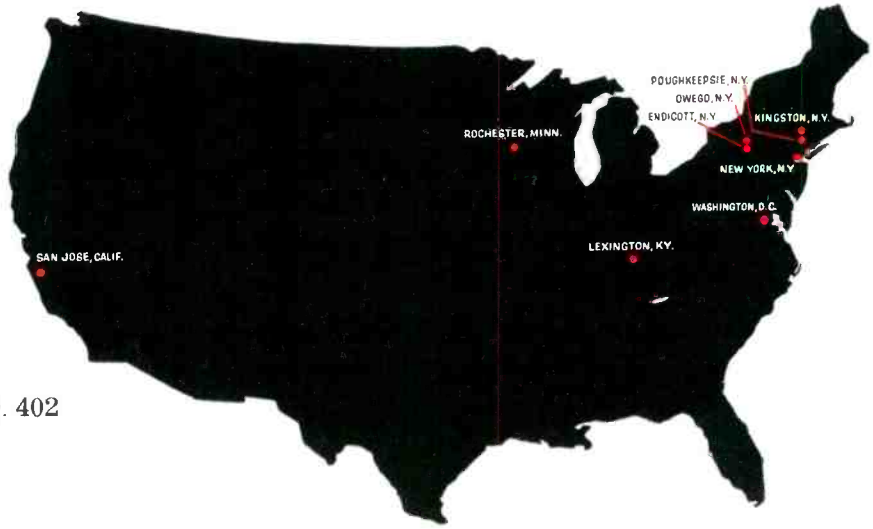
Exceptional career opportunities are now open in IBM Military Products for E.E.'s, M.E.'s, physicists, and mathematicians, in the following fields:

SYSTEMS PLANNING AND ANALYSIS
DIGITAL AND ANALOG SYSTEMS
INERTIAL GUIDANCE
SERVO-MECHANISMS
ELECTRONICS
MECHANICAL DESIGN
ELECTRONIC PACKAGING
PROGRAMMING
FIELD ENGINEERING
RELIABILITY
COMPONENTS
PHYSICS
MATHEMATICS
HUMAN ENGINEERING
INSTALLATION
CIRCUIT DEVELOPMENT
POWER SUPPLIES
TRANSISTORS
HEAT TRANSFER
OPTICS
TEST EQUIPMENT
COST ESTIMATING
TECHNICAL PUBLICATIONS

ployee. IBM Military Products include the Airborne Computer Laboratories located in Owego, N. Y., and the Project SAGE installations directed from Kingston, New York.

Here is a real ground-floor opportunity that you can't afford to overlook. Without exaggeration, your potential in this dynamic young field of electronic computers is virtually unlimited. Get all the facts. Write, outlining your background and interests to:

R. A. Whitehorne
Manager of Engineering Recruitment, Dept. 402
International Business Machines Corp.
590 Madison Ave., New York 22, N. Y.



Financial Aid to Higher Education

A Fine Start, But...

This editorial has two purposes. The first is to salute American business for the fine start it has made in helping to relieve the financial plight of our colleges and universities. The second purpose is to stress the importance of having business provide more financial aid, and soon.

How Business Helps Higher Education

Business contributions to higher education doubled between 1950 and 1955. They jumped from $40 million to $80 million. Preliminary figures indicate they will be even higher this year.

Business firms have also shown a lot of ingenuity in devising different ways of making their contributions. The methods range from a matching of an employee's contribution to his particular alma mater to wide diffusion of the money through state and regional money-raising associations of colleges and universities. Thanks to this ingenuity, business firms now have a wide choice of ways by which to give effective aid. The way most appreciated by college administrators is the making of gifts unrestricted as to the purpose for which the money is used.

Imposing as it is, however, what business has done thus far is only a good start. Only a tiny fraction of the total number of business firms in the country are giving direct financial help to our colleges and universities; and this fraction includes fewer than half of the hundred largest corporations in the country. Also, the amount of financial help being provided by business constitutes only a very small fraction of what is needed.

Why Colleges Need More Aid

Right now our privately endowed colleges and universities need about $350 million more in operating income a year than they are receiving to enable them to pay decent faculty salaries and be in tolerably good working order otherwise. The reasons, including a severe decline in the purchasing power of their endowment income because of price inflation, have been dealt with in the previous editorials in this series.

In addition, these institutions, together with the tax-supported schools, are faced with a tremendous increase in enrollment over the years ahead. With both a rapidly increasing population of young people and an increasing propor-

tion of them going to college, this year's enrollment of 3.2 million students is expected to reach 4.0 million by 1960, and to be doubled by 1970.

For the next ten years our privately supported colleges and universities must have an average of about $400 million a year above what they can be expected to collect from tuition fees, income from endowment funds, etc.

This figure of $400 million does not include what is needed for new buildings and equipment. It also does not include help for tax-supported schools above what they get from taxes, fees, etc. Business has given and will continue to give these schools substantial aid. Indeed, almost 25% of the financial help from business for our colleges and universities went to tax-supported schools in 1955.

If aid from business met their needs for increased operating income, the privately supported colleges and universities would be given a decisive lift in performing successfully their part in our system of higher education. They would still have large needs of capital equipment — buildings, dormitories, laboratories — but help from other sources, such as that provided by devoted alumni, where they are well organized, could be expected to go far toward meeting these needs. Also some companies prefer to concentrate on meeting needs of this type.

What 1% of Profits Would Do

But do business firms have the capacity to fill the gap in adequate operating income for our privately endowed colleges and universities without putting an excessive financial burden on themselves? Those who have studied this capacity carefully say that the answer clearly is yes. If, of its profits before taxes — last year an estimated $43 billion — business were to devote 1% to helping our privately endowed colleges, it would take care of present operating needs of about $350 million a year. And the balance of $80 million would be a big step in meeting their needs for new buildings and equipment, too.

About one half of a 1% contribution of this sort would, in effect, be made by the federal government. Up to a limit of 5%, contributions of this type are exempt from the federal corporate income tax. For corporations with incomes above $25,000 per year this tax is 52%.

It is clear that not all business firms are in shape to devote 1% of their profits to aid to higher education. Even in this year of record-breaking prosperity, many of them will have no profits at all. But if business generally would take 1% of pre-tax profits as a target or benchmark for financial help to our privately endowed colleges and universities these institutions would again have sturdy financial foundations.

Relatively this is a very small price to pay (1) to insure a continuing supply of competently trained young men and women and (2) to buttress our freedom by assuring the successful survival of the privately supported sector of our system of higher education.

This is one of a series of editorials prepared by the McGraw-Hill Department of Economics to help increase public knowledge and understanding of important nationwide developments of particular concern to the business and professional community served by our industrial and technical publications.

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Donald C. McGraw

PRESIDENT

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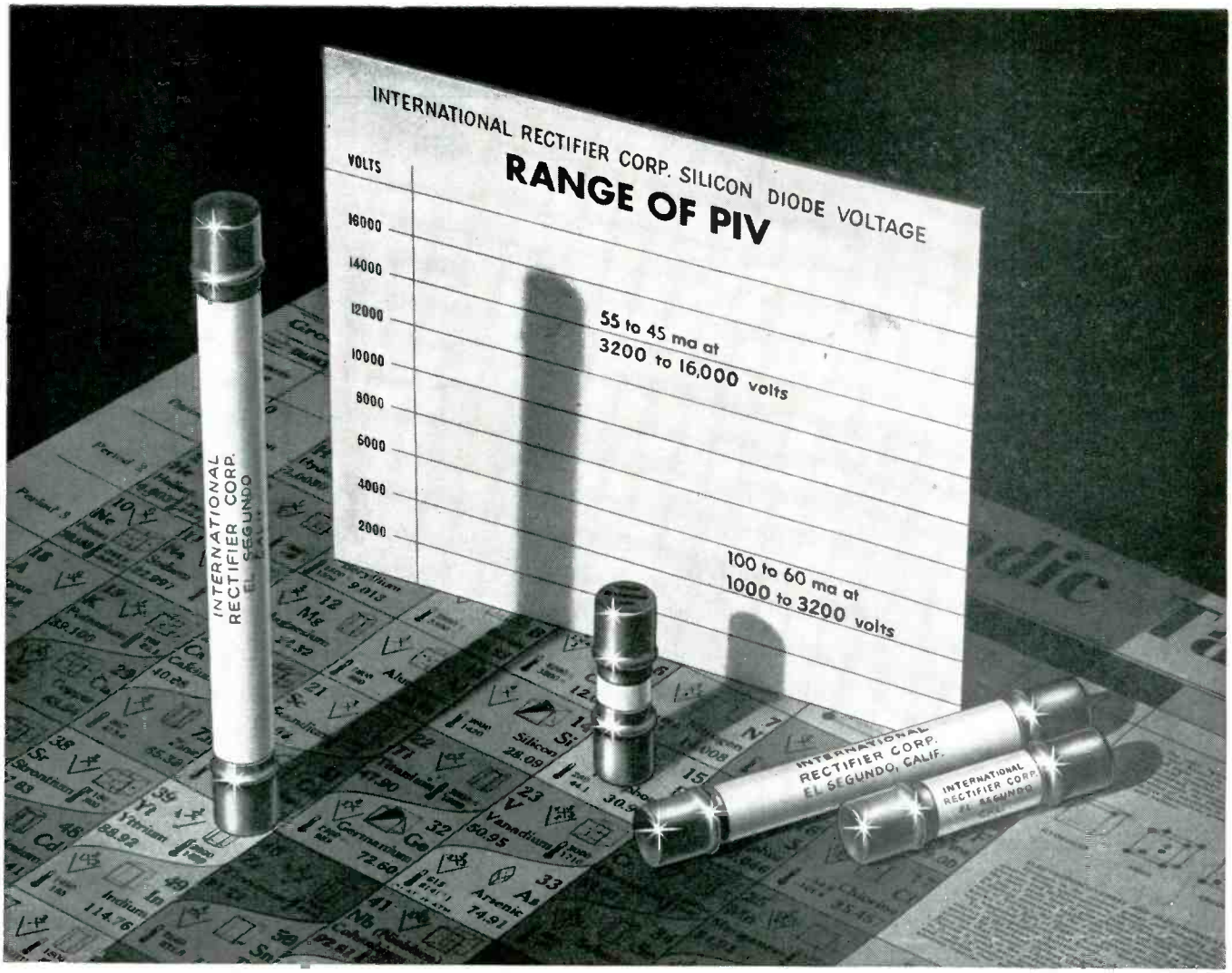
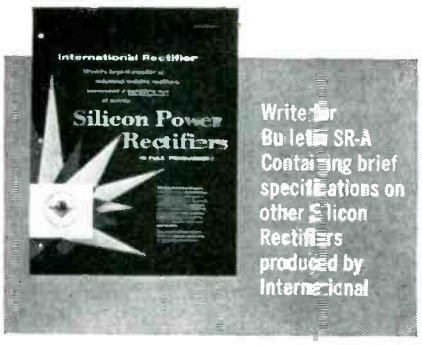


Pictured are the 4 sizes available, ranging in length from 1 13/16" to 6 1/16". Diameter 37/64".

International Silicon Diodes feature ratings to 16,000 volts PIV...require up to 95% less space!



Here is the answer to tough miniaturization problems where high temperature and high efficiency are prime design factors. International's high-voltage silicon diode series, now in full production, offers ratings ranging from 600 volts at 100ma half-wave dc output, to 16,000 volts PIV at 45ma, over a temperature range of −55°C to +150°C. Constructed from selected silicon junction diodes connected in series, hermetically sealed within a metalized ceramic housing, these rectifiers feature ferrule terminals for clip-in applications into standard 30-ampere fuse clips.

This new series is ideal for those "compact-packaging" jobs. For example, the 16,000 volt unit, with a diameter of 37/64", measures only 6 1/16" in length. This represents a size ratio of 20 to 1 over rectifiers of other types. This marked size and weight savings over conventional units of comparable rating cuts engineering time normally spent "designing around" bulky units... can sharply reduce the dimensions and weight of your equipment.

Write, wire or telephone our Application Advisory Department. This group of experienced rectifier engineering specialists will be happy to supply specific information on how these rectifiers can fit into your project.

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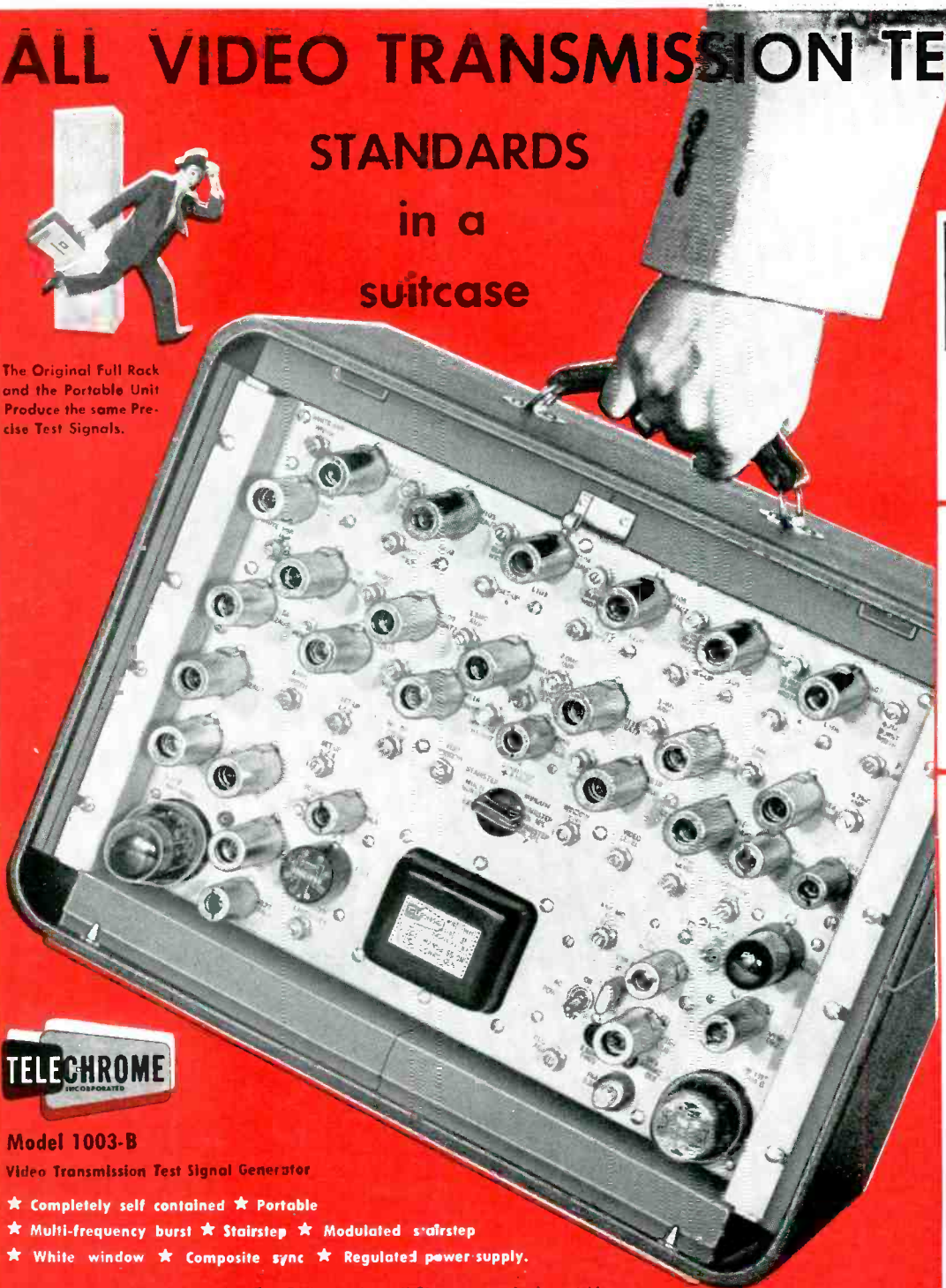

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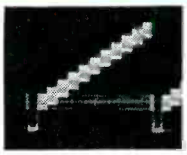
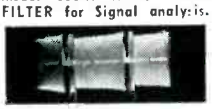
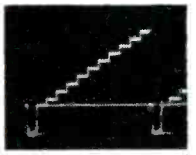


STAIRSTEP SIGNAL modulated by crystal controlled 3.579 mc for differential amplitude and differential phase measurement. Checks amplitude linearity, differential amplitude linearity and differential phase of any unit or system.
Model 1003-C includes variable duty cycle stairstep (0-90% average picture level).

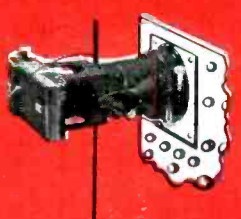
Model 608-A HI-LO CROSS FILTER for Signal analysis.



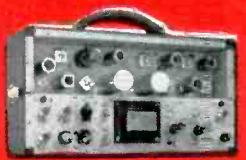
MODULATED STAIRSTEP signal thru high pass filter. Checks differential amplitude.



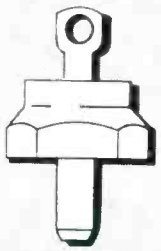
MODULATED STAIRSTEP signal thru low pass filter. Checks linearity.

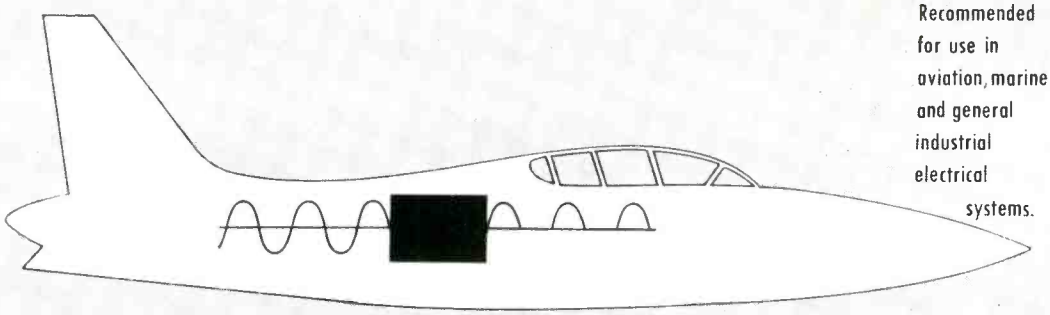


B21-A OSCILLOSCOPE CAMERA—Polaroid type for instantaneous 1 to 1 ratio photo-recording from any 5" oscilloscope.



1004-A VIDEO TRANSMISSION TEST SIGNAL RECEIVER for precise differential phase and gain measurements. Companion for use with 1003-B.

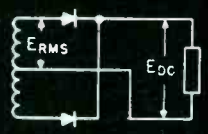




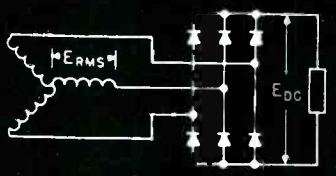
Recommended for use in aviation, marine and general industrial electrical systems.

WN-5051 and WN-5091 with *maximum peak inverse voltage* ratings of 50-350 v. (up to 200 amperes in bridge assemblies).

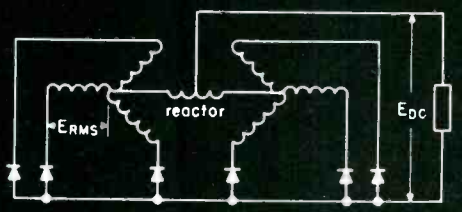
TYPICAL RECTIFIER CIRCUITS



Single phase full wave (center tap)

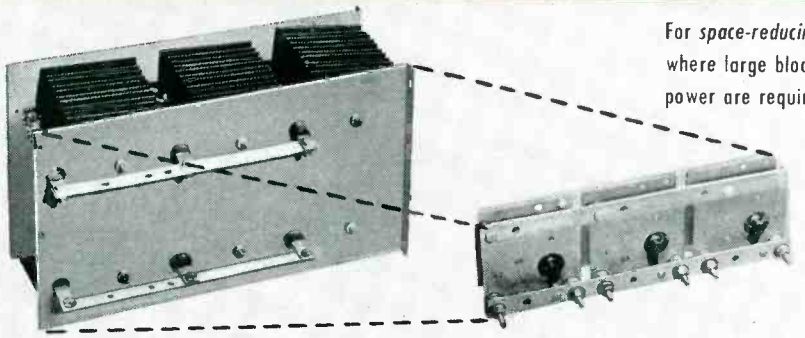


Three phase full wave bridge



Six phase half wave

WN-5082 with *maximum peak inverse voltage* ratings of 50-300v. (300 to 5000 amperes in bridge assemblies.)



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Recommended for greater reliability, highest efficiency and lowest cost

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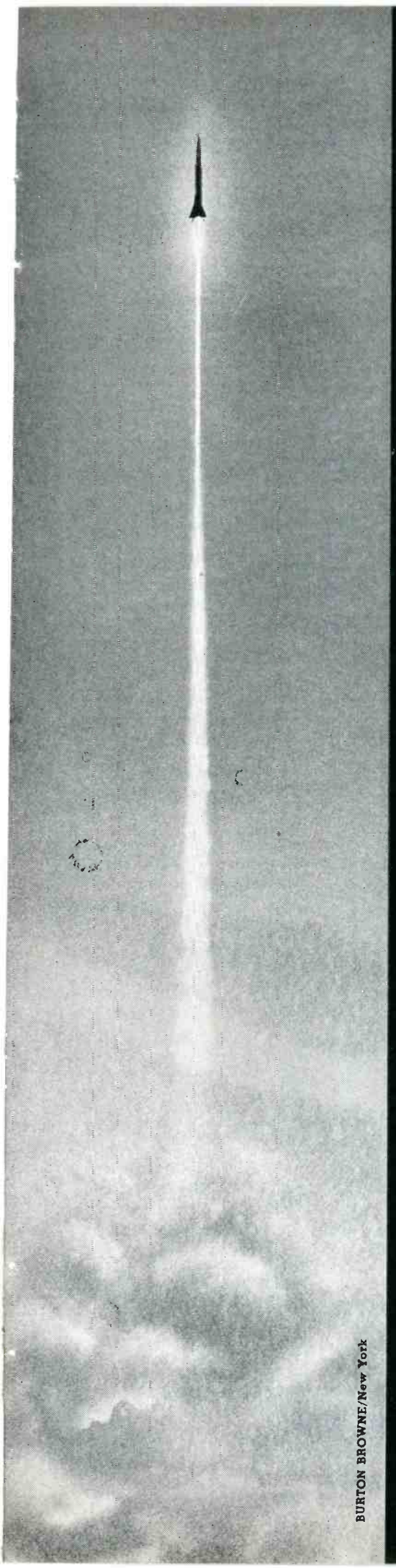

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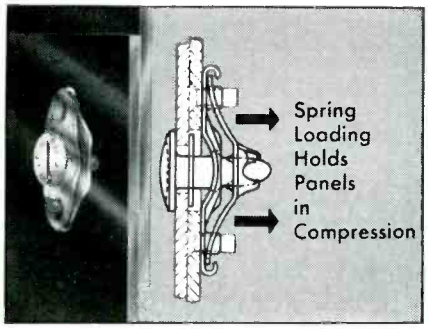
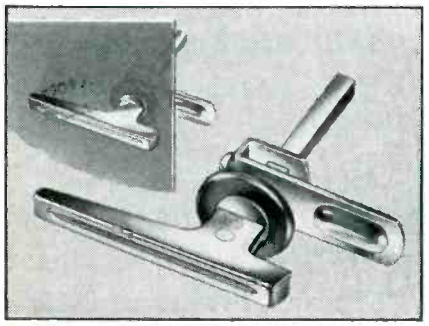
*"Use captive fasteners wherever feasible . . . Avoid the use of loose washers and loose nuts . . . Fasteners on equipment covers should be operable either with no tools or with standard hand tools"**

(John D. Folley, Jr. & James W. Altman, Research Scientists, American Institute for Research)



Quarter-Turn Fastener

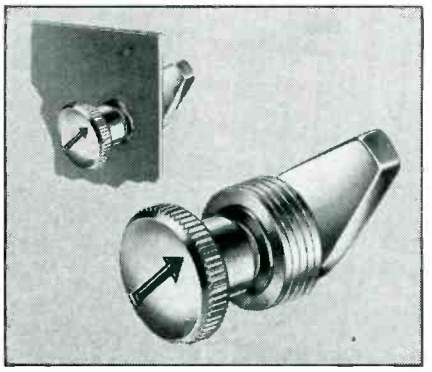
Lion Fasteners open and close with a ¼ turn, hold sheets tightly under the compression of a rugged spring. Quickly operated and fully retained in the outer panel, they are approved under U. S. Government military specifications. Stud and receptacle float for easy alignment and simplified hole preparation. Flush, oval, wing, knurled, ring, and key head styles available. Sizes—No. 2, No. 5, and High Strength for extra heavy duty.



Cabinet Latch

Just drill a hole, push the fastener stem through, and slide the special push-on clip into place. No welds, screws, bolts or rivets: the fastener is permanently installed in seconds!

Adjustable to any grip length or panel thickness, the pawl is fixed in place by a single set screw. The fastener's brightly finished knob is set off by a plated washer. Also furnished with screwdriver operated flush head.

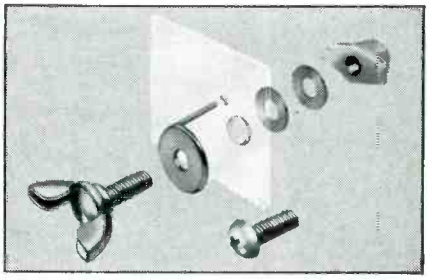


Spring Tension Latch

For fastening slide-out drawers and hinged panels the Southco Arrowhead Latch is recommended. It locks or opens with a quarter turn yet occupies less than ½" inside space.

Doors are held under spring tension—a push against the arrowhead knob relaxes this tension, allows operation with fingertip ease. Drill a single hole for installation—no fastening to the door is necessary. No striker plate is needed.

Pawl stop is eliminated—arrowhead shows at a glance exact position of pawl.



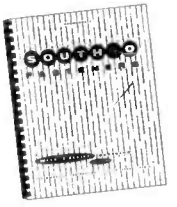
Adjustable Panel Latch

Small doors and panels can be fastened with greatest speed and lowest cost with the Southco Adjustable Latch.

The entire fastener is quickly installed through two holes punched in the door; no bolts or rivets are needed.

It operates with a quarter turn, requires no striker plate. An extra twist after the nylon pawl is engaged pulls up the door to form a seal and eliminate vibration.

Available with wing, knurled, or Phillips head.



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Send for your free copy of Fastener Handbook No. 7, just released. Gives complete engineering data on these and many other special fasteners. Fifty-two pages, in two colors.

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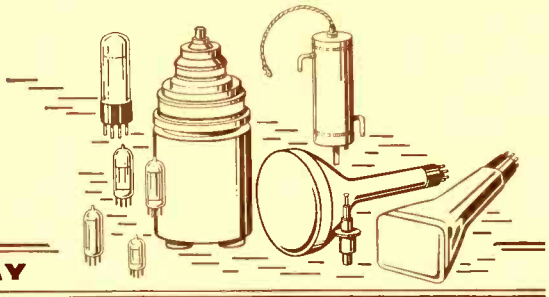
* *Quotation from "Designing Electronic Equipment for Maintainability"; Machine Design, July 12, 1956.*

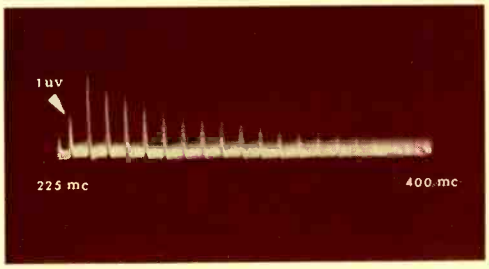
TUBE DESIGN NEWS

GENERAL ELECTRIC

RECEIVING * POWER * CATHODE RAY



Using Low-Noise GL-6299's, Applied Research Analyzer Monitors Republic Fighter Planes for Radio Interference



ABOVE: narrow white band across bottom of the scope portrays low noise level of the GL-6299 triode (less than 5 db) in 225-to-400-mc service. Actual (or simulated) signal impulses 1 microvolt and up show as sharp spikes, easy to detect. RIGHT: monitoring the electrical components of a Republic plane for absence of radio interference or interaction.

Applied Research Inc., Flushing, N. Y. employs 11 GL-6299 tubes in the SPA-224 visual noise-interference analyzer, developed jointly by Applied Research and Republic Aviation Corporation to detect any radio interference from airborne electrical equipment.

Super-sensitive, the SPA-224 analyzer continuously presents 225 mc to 400 mc, making possible identification of any spurious signal in this range from one microvolt up.

While an extremely low noise figure and high tube gain were primary reasons for specifying Type GL-6299 in the SPA-224 analyzer, other features were its small size (1 inch long by ½ inch diameter), planar design, and metal-ceramic construction. The GL-6299 is suited to many advanced instrument and other applications which call for precise, dependable performance and space-saving compactness.

Wide frequency range—from v-h-f to 3,000 mc—plus tube efficiency throughout this range, make for versatility. Extensive tests show life to 2,500 hours.

GL-6299's are in full-scale production, for immediate delivery. Characteristics, ratings, and price available from any General Electric office on the next page.

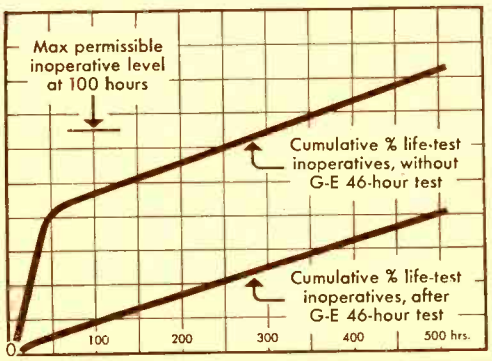
46-Hour Inoperative Control Test of All G-E Five-Star Tubes Cuts Failure Rate Sharply

By operating all 5-Star Tubes for 46 hours as an additional process before life tests begin, General Electric weeds out early-life tube failures.

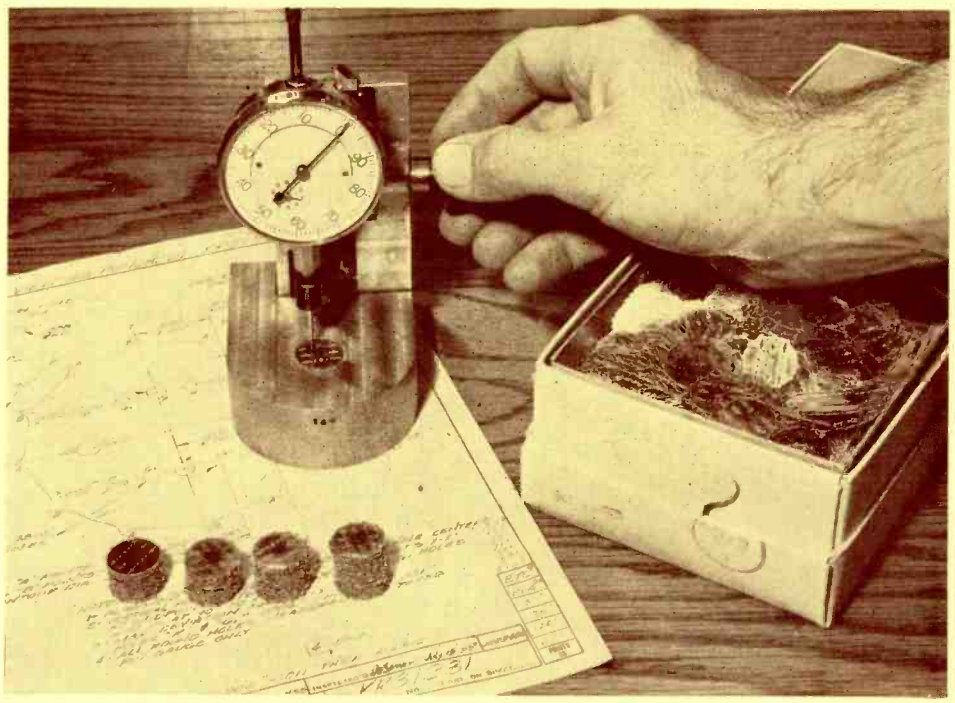
Consequently, as the chart at right shows, the inoperatives in any 5-Star lot on life test are only half as many, at 500 hours, as they would be without G-E inoperative control. Furthermore, at 500 hours, the percentage of G-E 5-Star inoperatives is still far below the permissible figure established for 100 hours.

Employed only by General Electric, this 100% inoperative control process helps assure that 5-Star Tubes installed in critical military and industrial sockets will perform dependably across the board.

(Continued on Page 2, Column 1)



RIGHT: General Electric 5-Star Tubes on 46-hour inoperative control test. Only G.E. conducts this 100% pre-life test process on high-reliability tubes, to weed out early-life failures. ABOVE, the result: curve of General Electric 5-Star inoperatives is far lower throughout regular life test—1 to 2 at 500 hours' operation.

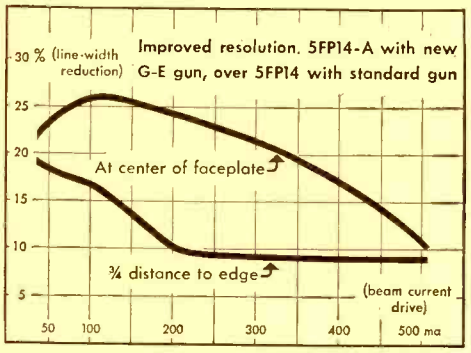


CLOSE G-E TUBE-MICA SPECIFICATIONS MEAN STEADIER TV. With tapered-pin micro-gages like that shown above, the diameter of grid side-rod apertures in G-E vertical sweep-tube micas is checked to an allowable half-mil tolerance, providing tight grid fit and minimum microphonics. By micro-measuring G-E tube micas and holding the grids to precision tolerances, image "jitter" on TV screens is virtually eliminated.

Higher Resolution up to 35% from New G-E Precision C-R Gun

A new General Electric gun for military and industrial cathode-ray tubes makes possible improved image resolution, which with some types reaches the high figure of 35% at center of face-plate.

Three construction features are responsible for the new gun's efficiency: smaller grid apertures . . . less space between Grids 1 and 2 . . . closer tolerances on parts.



Improvement in image resolution in Type 5FP14-A with the new gun is shown by these curves of increased line-width reduction over the 5FP14 at successive beam drives. Better resolution for this tube ranges 8.5 to 26.1%.

G.E.'s high-resolution gun has wide application—can be used in any magnetic focus and deflection tube, with any phosphor.

Six radar tubes with the new gun already are available, ranging from 5 to 12 inches. Their presentations show details that with former types were cloudy or obscure. These types are listed under NEW PRODUCT BRIEFS at left.

46-Hour Inoperative Control Test

(Continued from Page 1)

All 5-Star tests, as well as all product inspection—all manufacture of parts and assembly of tubes—are carried out in a special 5-Star factory set apart for the purpose, which is air-conditioned and pressurized to keep out dust and dirt. Lint-free Nylon and Dacron garments are worn throughout.

The industry's most extensive testing, plus manufacture under "Snow White" conditions, continues the quality theme that was established in the 5-Star Tube design stage, where ruggedness, reliability, and long life were the aims. For a convenient listing of these high-reliability types, ask any General Electric tube office for the 5-Star Selection Chart (ETD-1276-A) described on this page.

NEW PRODUCT BRIEFS

Receiving Tubes:

5DH8. New G-E triode-pentode for TV, especially suited to 600-ma series-string use.

6BW8. New G-E duplex-diode pentode for TV, useful as a horizontal phase detector and sound i-f amplifier, limiter, and AGC keyer.

6CX8, 8CX8. New G-E triode-pentodes for TV. Identical except for heater ratings. Also, 8CX8 is suited to 600-ma series-string circuits.

6919. New G-E twin diode for computer gating and clamping circuits. Has separate cathodes, low heater power, high perveance.

Cathode-Ray Tubes:

New radar types with high-resolution gun. 5FP7-B, 5FP14-A, 7BP7-B, 10KP7-A, 12DP7-C, 12SP7-D. Fully interchangeable with their prototypes.

ASK FOR COMPLETE INFORMATION!

REVISED!

General Electric 5-Star Tube Selection Chart

Up-to-the-minute . . . all types are included, with key ratings. Useful to designers of military and industrial equipment. Ask for ETD-1276-A!

EASTERN REGION

General Electric Company, Tube Sales
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DAPON® resin

superior moisture resistance

Completely protected and locked-in—the excellent electrical properties inherent in cured DAPON resin are protected by the *resistance* of DAPON resin *to moisture in all forms.*

DAPON resin is the *new prepolymer* of diallyl phthalate—a dry white powder with improved properties. It is *easy to handle and store.* Its advent has made possible the use of diallyl phthalate in *all processing methods* for thermosetting resins.

Because the cure of DAPON resin involves addition polymerization, and not condensation, *moisture formation is non-existent* during cure.

Think of an electrical connector with *volume resistivity higher than that of porcelain* with complete protection that guarantees the retention of these properties under the most adverse conditions. This is DAPON resin.

Rid yourself of the moisture problem. Be assured of locked-in initial properties and locked out moisture. *Write now for technical literature containing properties, uses and methods of application for DAPON resin.*

Molding compounds containing DAPON resin are produced by Acme Resin Corporation, Durez Plastics Division, and Mesa Plastics Company.

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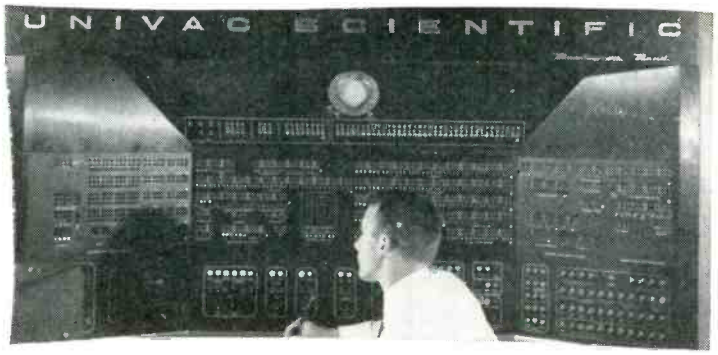

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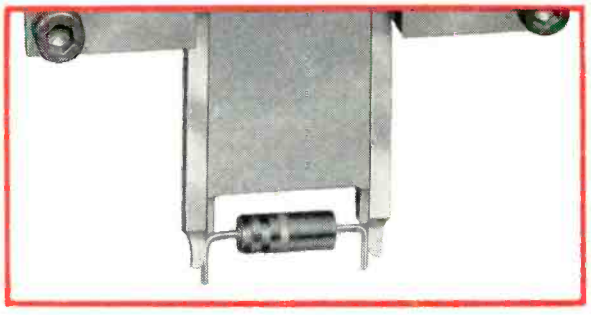

- **Cut component assembly costs**
- **Reliable, uniform assembly to printed wiring**
- **Reduce operator fatigue**

For large volume or limited production of printed wiring assemblies there is Dynasert equipment that will help make your assembly work more efficient. Write today for full information and literature on DYNASERT.

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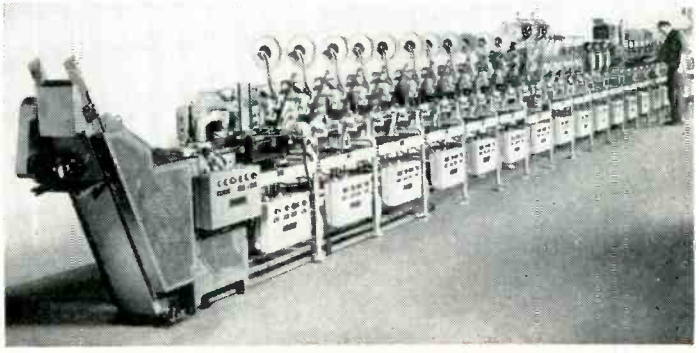
PRODUCTION EQUIPMENT FOR ELECTRONICS

Individual Dynasert Component assembly machines let you realize maximum speed and lower costs in placing components in printed wiring assemblies.

This Dynasert machine feeds, trims leads, forms, inserts and clinches leads in a single stroke. Up to 800 components can be inserted per hour on a single set-up. Rejects are low. Other Dynasert machines handle jumper wires or a variety of electronic components as received from your supplier.



DYNASERT single-head assembly machines are closely related to fully automatic DYNASERT conveyor assembly systems. In fact, your individual bench machines can be easily converted for use on assembly lines as your production increases.

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THE MAN WE MEAN IS A COMPOSITE of the editorial staff of this magazine. For, obviously, no one individual could ever accomplish such a vast business news job. It's the result of many qualified men of diversified and specialized talents.

AND, THERE'S ANOTHER SIDE TO THIS "COMPOSITE MAN," another complete news service which complements the editorial section of this magazine — the advertising pages. It's been said that in a business publication the editorial pages tell "how they do it"—"they" being all the industry's front line of innovators and improvers — and the advertising pages tell "with what." Each issue unfolds an industrial exposition before you—giving a ready panorama of up-to-date tools, materials, equipment.

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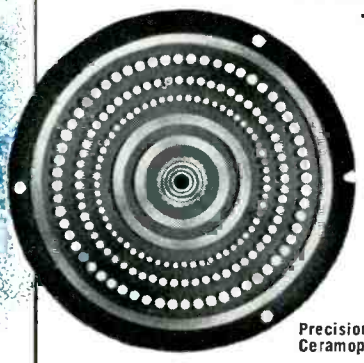
At 10 feet or 100,000 feet, test teams rely upon telemetering for flight performance data. When signals fail vital information is lost forever.

Perfect commutation of these microsecond signals is an important job of MYCALEX TM55 switches, whose specially engineered design is setting new standards of dependable, low-noise-level performance — less than 1 millivolt peak-to-peak under most conditions. Their extreme durability (more than 5,000 hrs. continuous operation at 600 rpm) significantly reduces down time.

Individually designed to your specifications. Write to Dept. 448 for complete information.



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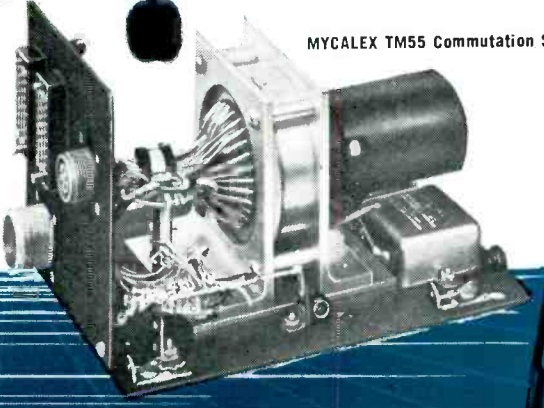

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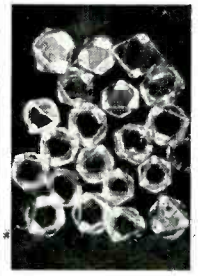
The engineering test reports as well as extended field use of Sensitive Research have graphically demonstrated the great improvements in electrical testing equipment made possible by the Tetrad Diamond pivot.

Here are some findings of Sensitive Research:

- Drop Test: Pivot in ruggedized instrument survived *300* falls of 3 ft. onto concrete floor, with no alteration of sensitivity or accuracy of instrument.
- Durability: No discernible wear of diamond pivot or sapphire jewel after 5,184,000 oscillations over a period of 3 months.
- Friction Free: Highly polished riding surface and small radius of pivot eliminates tapping. Reduction of friction coefficient by better than 18 to 1 ratio.
- No Hysteresis Effect: Tetrad diamond pivot and mounting are completely non-magnetic.
- Reduces Servicing: Very economical when compared to servicing of instrument which exhibits pivot or jewel deformation.

Expert with loupe selecting stones from large quantity of original diamond parcel. Only a small percentage pass this phase of rigid quality control. These are not chips, but small individual diamond crystals.



Perfect diamonds make perfect pivots. Diamonds which pass loupe inspection are then carefully and individually examined through a binocular stereoscopic microscope. Only perfect diamonds — free from flaws, inclusions and cleavages are kept for fabrication of diamond pivots.

Skilled lapidary performing one of several diamond cutting and polishing operations. Final finish of the radiused tip of the diamond pivot is made with an 0 to 2 micron diamond powder. This results in a highly polished surface with an extremely low coefficient of friction.

Shadowgraph inspection of diamond pivot. Shape and included angle are important for perfect pivot design. Each completed diamond pivot is enlarged on contour projector and rotated 360°. Tolerances are kept to within ±.0001″ on radius and ±1° on included angle.

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Highly magnified photomicrograph of diamond pivot. Before diamond pivots are put into final instrument assembly they are given another microscopic check. Only one pivot is made from one diamond crystal. This permits the best orientation for strength and wear resistance.

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Do you have an engineering application where durability, minimal friction and maintenance of shape is important? Consider Tetrad Diamond Products. Please submit specifications or drawings. Samples furnished upon request. Write to:

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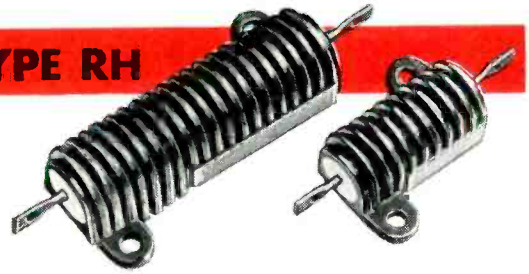
These Dalohm resistors combine high power rating with sub-miniature design. High heat dissipation and protective covering are achieved with vertical-finned black anodized aluminum housings. Vertical single hole panel mounting is provided by integral threaded base and lock nut. Ruggedized construction assures dependability under the most extreme conditions.

- Completely welded construction from terminal to terminal
- Silicone sealed for absolute protection against moisture, shock and salt spray
- Three wattages and sizes: PH-25, 25 watts; PH-50, 50 watts; PH-100, 100 watts
- Resistance values from 0.1 ohm to 60K ohms, depending on type
- Tolerances from 0.05% to 3%

Ask for Bulletin R-33

TYPE RH



Another Dalohm resistor that resolves power and space problems in tight specifications. Black anodized finned housing provides protection and maximum heat dissipation. Mounting lugs provided for horizontal mounting.

- Completely welded construction from terminal to terminal
- Silicone sealed for absolute protection against moisture, shock and salt spray
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New miniature diode construction for cool operation

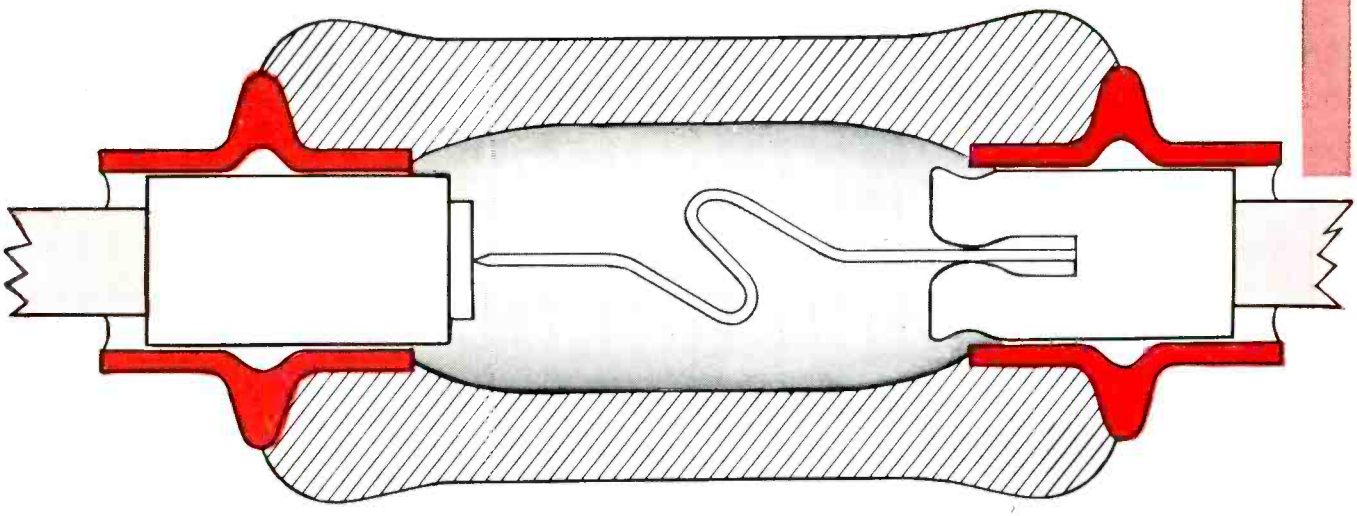
Shown actual size

Now, designers can incorporate Sylvania's new miniaturized diode in equipment where space is at a premium. It meets the standard Retma outline of .105″ maximum diameter and .265″ maximum over-all length and meets requirements for automatic production methods. Its construction inherently assures greater reliability and superior performance.

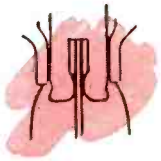
Metal eyelet—fused to glass tubing—provides strong construction and builds in provision for cooler operation. In Sylvania's metal to-glass package, heat is dissipated by the eyelets and leads.

Preassembled cartridge—By preassembly of the diode cartridge, the metal-to-glass design affords another advantage. The whisker and die of the diode are not subjected to excessive sealing heats. There is no danger of breaking down the conductive characteristics of the diode.

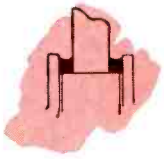
features metal-to-glass ruggedness and



Nickel-plated Steel pin—butt-welded to copper lead adds structural strength and provides coupling between the internal diode structure and the metal eyelet for greater heat dissipation. Nickel plating insures strong welds, and good solder sealing.



New whisker mounting—The use of a crimp hold rather than impulse weld to mount the whisker eliminates the possibility in production of overheating the tungsten whisker. Thus, the conductive properties remain undisturbed, assuring more reliable performance over longer life.



Smooth Solder Seal—is possible only with glass-to-metal construction. It adds reliability by preventing cracks and chips when leads are bent at right angles for mounting in printed circuit boards.

Write for complete details on this important new diode development. Address Dept. B20R

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1740 Broadway, New York 19, N. Y.
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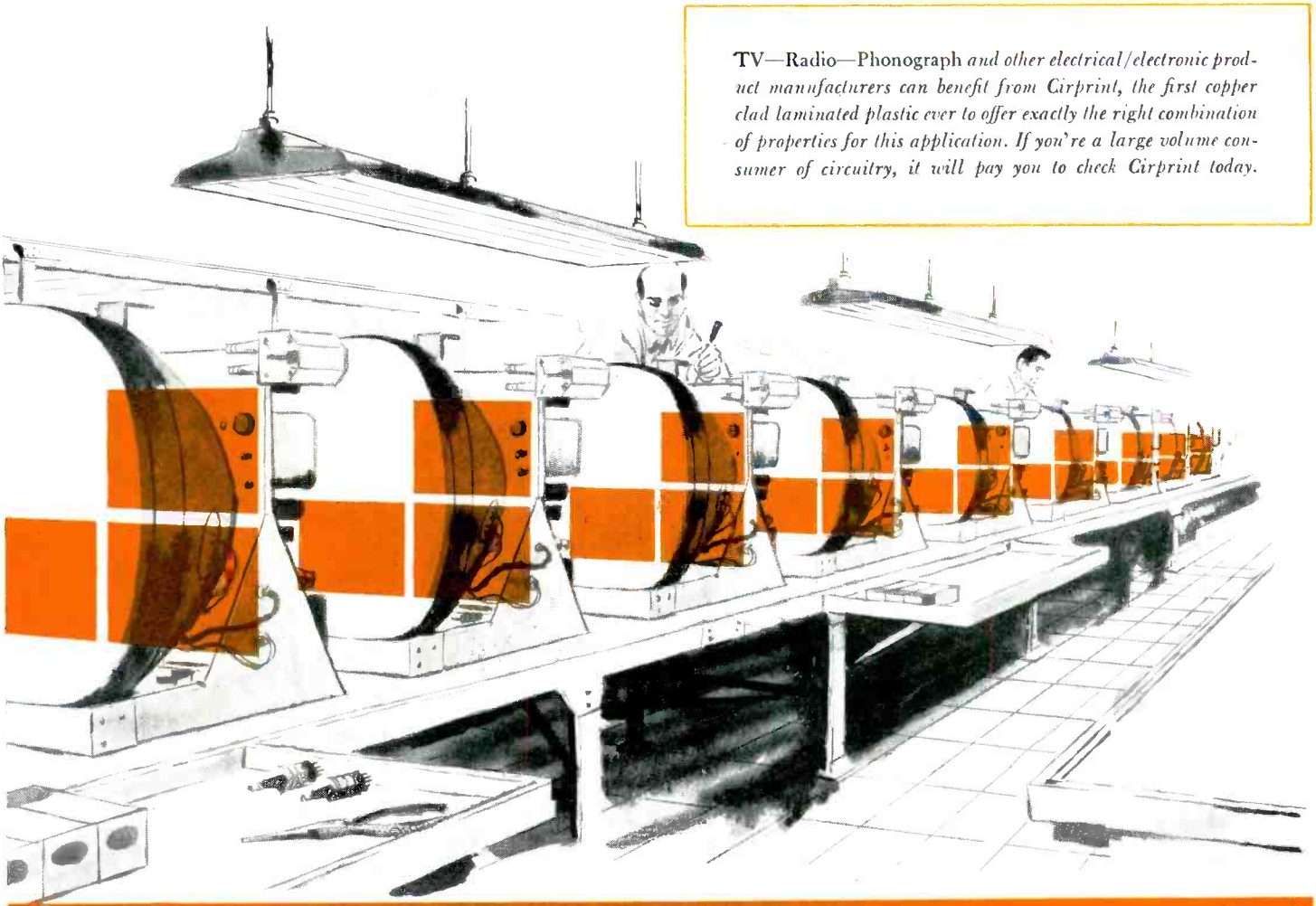

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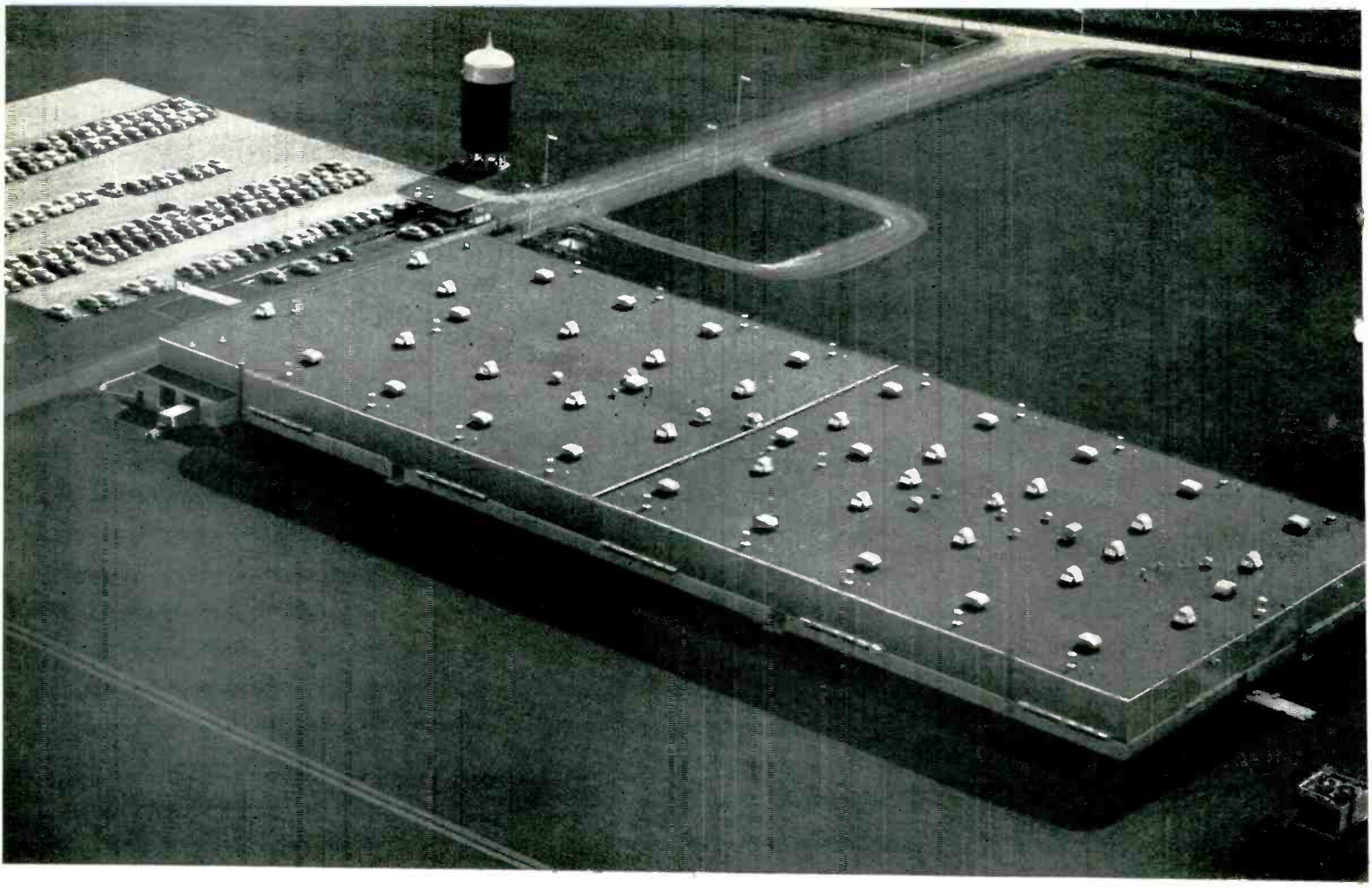

New 2½-acre Owensboro plant is fourth General Electric receiving-tube facility for serving TV manufacturers!

WELL over a million dollars in building costs have gone into General Electric's new receiving-tube factory on the outskirts of Owensboro, Ky. Another large investment is for advanced automatic machinery. Located on a 90-acre site, the plant itself is 500 feet long and 200 feet wide, with special ventilation and air-filtering to keep out dust and lint.

Here the tube needs of TV designers and builders are being met by new facilities unmatched in the industry. Here the prime targets are: still more dependable tube performance . . . even longer tube life . . . even greater values that help to keep down the curve of TV manufacturing costs.

Now, more than ever—from circuit stage through mock-up to receiver assembly—it will profit you to keep in touch with General Electric on *all* your tube requirements! *Electronic Components Division, General Electric Co., Schenectady 5, N. Y.*

Progress Is Our Most Important Product

GENERAL ELECTRIC

162-1A1

Irvine D. Daniels (seated), general manager, General Electric receiving tube department, points out to three members of the G-E field commercial engineering staff—from central, western, and eastern regions—how facilities in the new plant are being systematically brought up to full production. ▼

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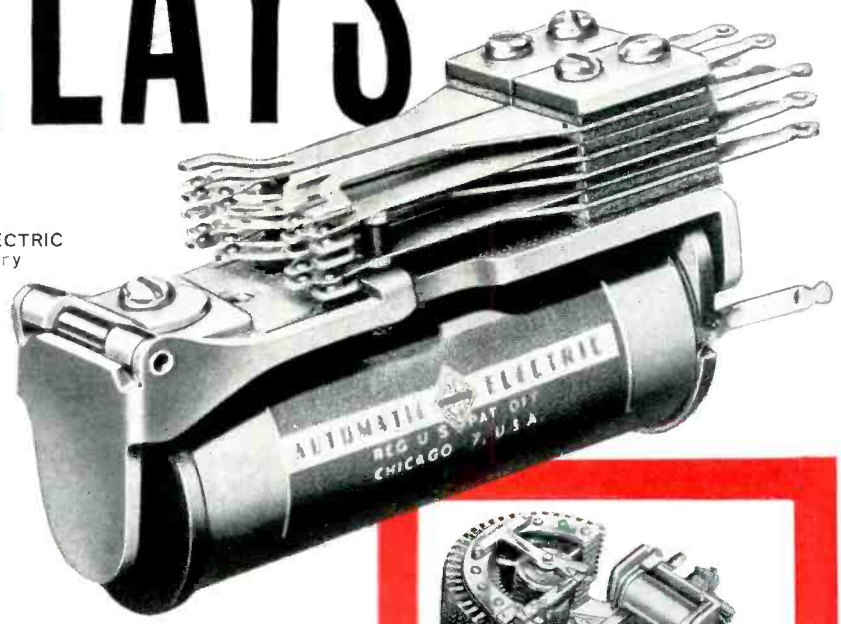

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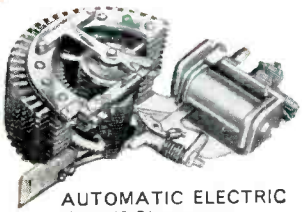

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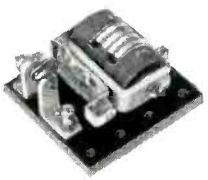

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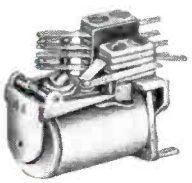

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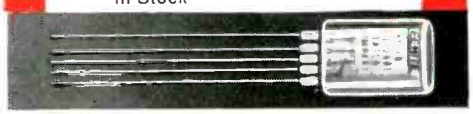

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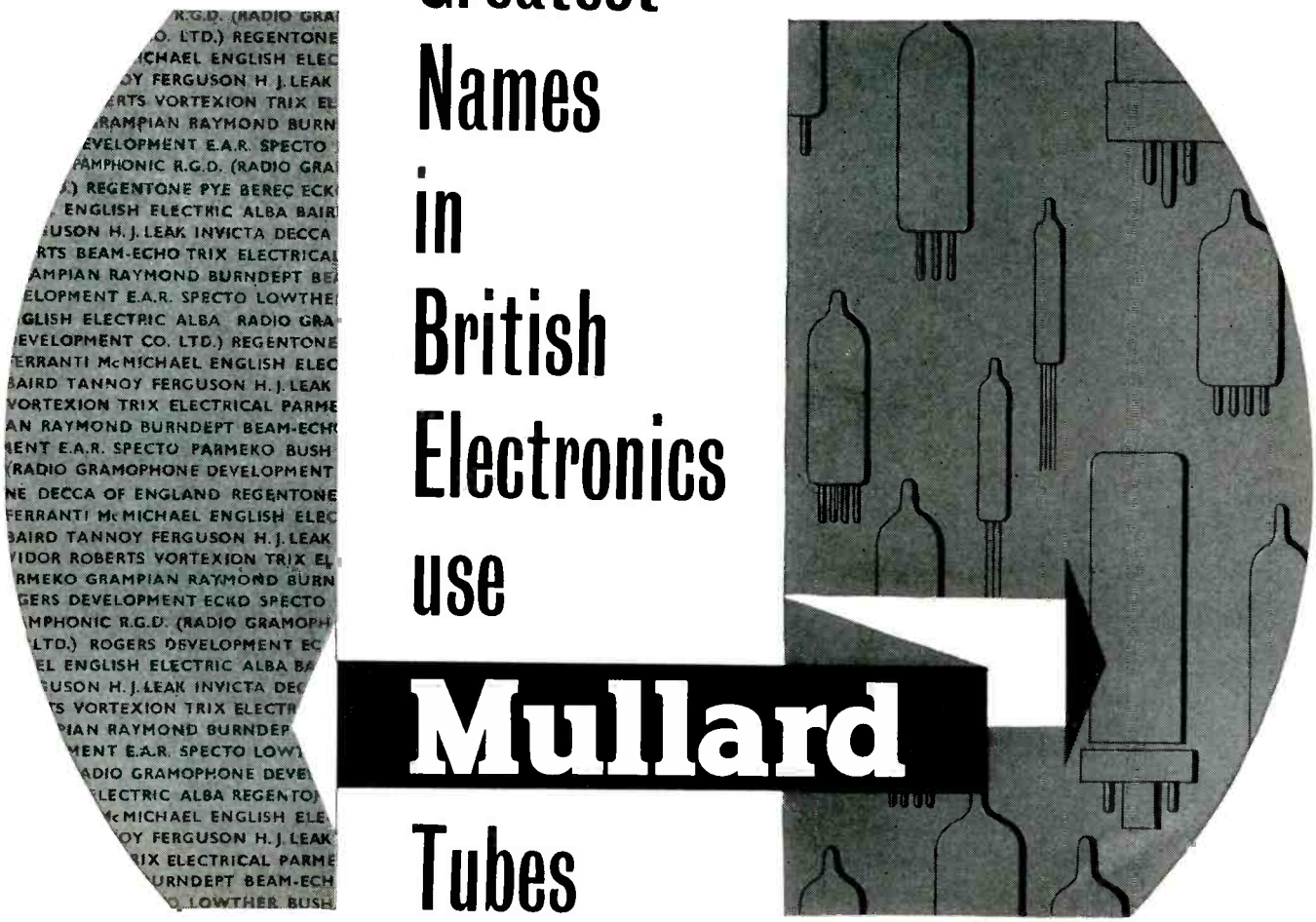

British equipment manufacturers are making a vital contribution to the development of electronics in all fields of application.

Their products are being exported to every corner of the world, earning a universal reputation for advanced techniques and excellent performance.

The majority of these electronic equipment manufacturers consistently use Mullard tubes. This choice is decided upon because they prefer the greater assurance of efficiency and dependability, and because the vast manufacturing resources of the Mullard organisation guarantee ready availability of Mullard tubes wherever they are needed.

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Electronic Tubes — used throughout the world

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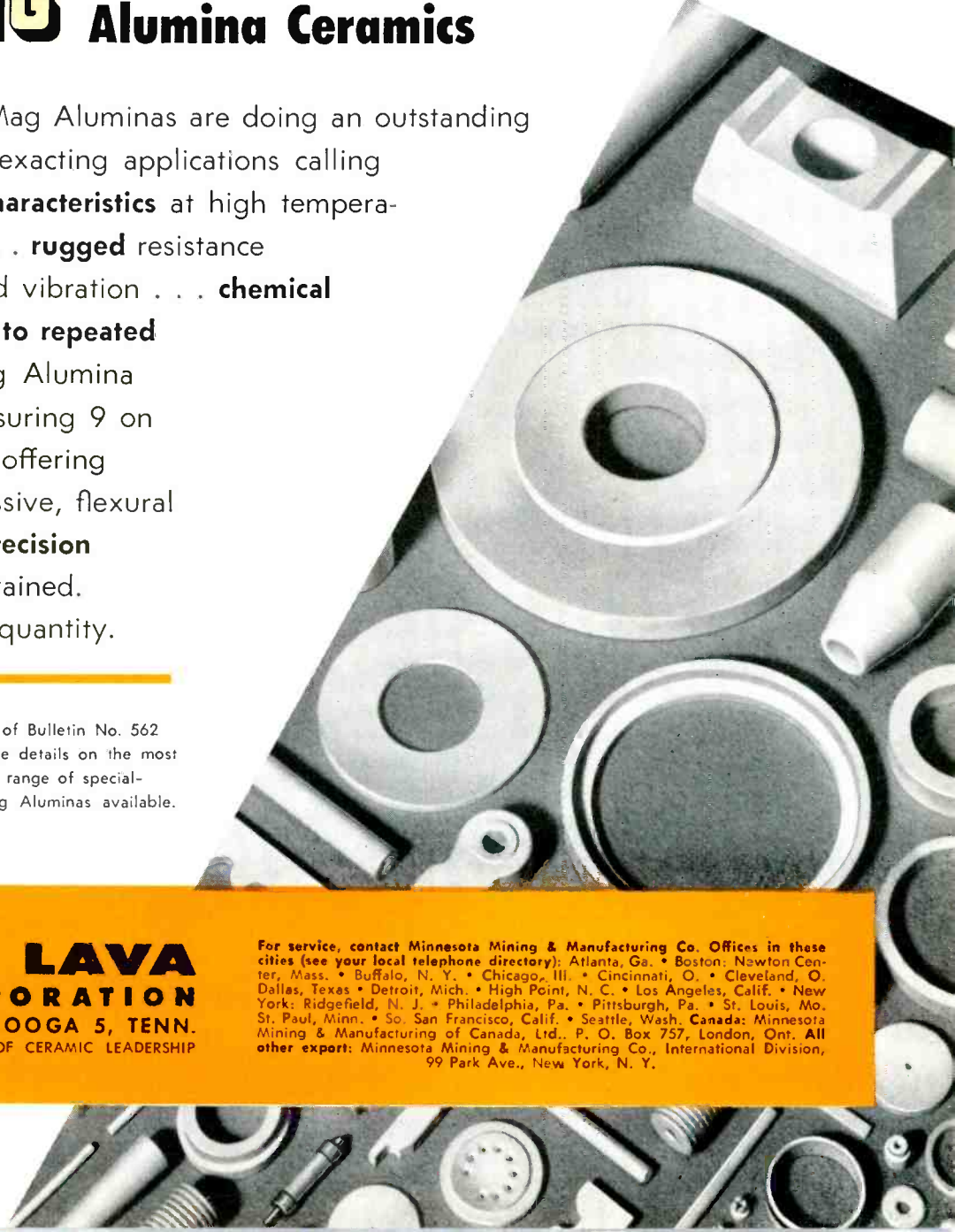
Write for free copy of Bulletin No. 562 which gives complete details on the most popular of the wide range of special-characteristic AlSiMag Aluminas available.



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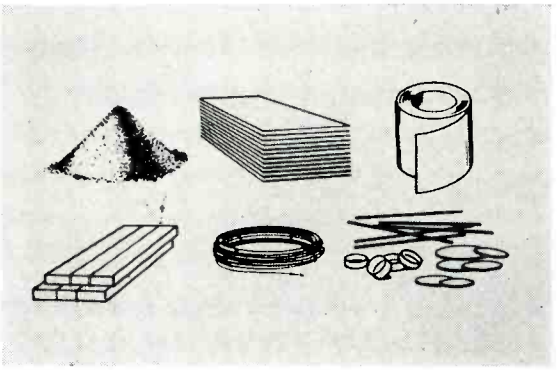

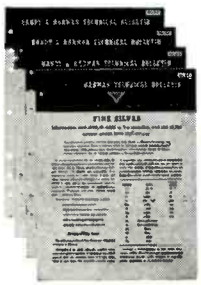

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TUNG-SOL®

12AL8

TRIODE / SPACE CHARGE TETRODE

another successful application

of the space charge grid principle of tube design

for hybrid auto radios

see other side for additional information

TUNG-SOL®

12AL8

TRIODE / SPACE CHARGE TETRODE

The widespread use of hybrid car radios today is proof of Tung-Sol's long-held conviction that tubes could be made to operate directly off a 12-volt power supply—an accomplishment made possible by the advent of the transistor. Vacuum tubes can now be designed to perform at the same low voltages for which transistors are most suitable.

The 12AL8 is a further utilization of the space charge grid principle . . . and Tung-Sol's engineering of this tube has resulted in circuit simplification and reduction of costs.

The 12AL8 is an electrically smaller version of the 12K5, plus an independent triode. It is designed to drive the relay that controls the motors of signal-seeking mechanisms. This combination tube can also provide the additional versatility needed in automotive receivers, such as in the audio amplifier portions of the circuitry.

MECHANICAL DATA

Coated unipotential cathode

Outline drawing	RETMA 6—3	Bulb	T—6½
Base	RETMA E9—1	Miniature button	9 pin
Maximum diameter			⅞"
Maximum overall length			2⅝"
Maximum seated height			2⅜"
Base pin connections:		RETMA	9GS

Pin 1—triode plate
Pin 2—tetrode grid #2
Pin 3—tetrode grid #1
Pin 4—heater
Pin 5—heater
Pin 6—tetrode plate
Pin 7—tetrode cathode
Pin 8—triode grid
Pin 9—triode cathode

Mounting position — ANY

ELECTRICAL DATA

*Heater Characteristics**

Heater voltage—nominal	12.6	VOLTS
Heater current—nominal	0.45	AMP.

Direct Interelectrode Capacitances

Triode input: (G to K+H)	1.5	μμf
Triode output: (P to K+H)	.3	μμf
Triode grid to plate	12	μμf
Tetrode input: (G_2 to G_1+K+H)	8.0	μμf
Tetrode output: (P to G_1+K+H)	1.1	μμf
Tetrode grid to plate	.7	μμf
Coupling: (tetrode grid #2 to triode grid #1)	.013	μμf

*This tube is intended to be used in automotive service from a nominal 12-volt battery source. The heater is therefore designed to operate over the 10.0 to 15.9 voltage range encountered in this service. The maximum ratings of the tube provide for an adequate safety factor such that the tube will withstand the wide variation in supply voltages.

ELECTRICAL DATA

Ratings—Interpreted According to Design Center System

Maximum tetrode plate voltage	30	VOLTS
Absolute maximum positive tetrode grid #1 voltage	16	VOLTS
Maximum negative tetrode grid #2 voltage	20	VOLTS
Maximum tetrode grid #2 circuit resistance	10	MEGOHMS
Maximum triode plate voltage	30	VOLTS
Maximum triode cathode current	20	MA.
Maximum triode grid circuit resistance	10	MEGOHMS
Maximum heater—cathode voltage	±30	VOLTS

Operating Conditions and Characteristics

Class A_1 Amplifier—single tube	Triode	Tetrode	
Heater voltage	12.6		VOLTS
Plate voltage	12.6	12.6	VOLTS
Grid #1 (space-charge grid) voltage	——	12.6	VOLTS
Control grid voltage	−0.9[A]	−0.8[A,B]	VOLTS
Plate current	0.25	25	MA.
Grid #1 (space-charge grid) current	——	50	MA.
Plate resistance	27000	1000	OHMS
Amplification factor	15	8.0	
Transconductance	550	8000[C]	μMHOS

Resistance-coupled amplifier—single tube		
Plate (space-charge grid & heater) supply voltage	12.6	VOLTS
AF signal voltage	.13	VOLTS
Plate current (tetrode)	13	MA.
Grid #1 (space-charge grid) current	50	MA.
Load resistance (tetrode)	800	OHMS
Total harmonic distortion (max.)	10	PERCENT
Power output	20	MW.

A—Average bias developed across a 2.2 megohm grid resistor.
B—Grid #2. C—From grid #2 to plate.

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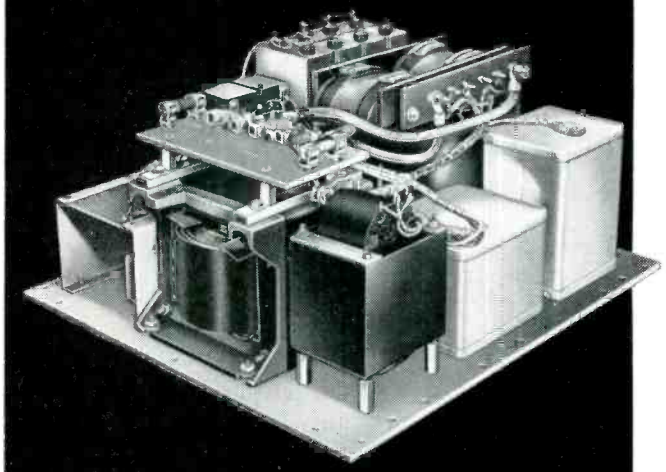
(Tubeless Magnetic)



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TYPE TM7105 (with cabinet as mounted on wall)

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INPUT: 95-135 volts, single phase on nominal 115 volt types
195-255 volts, single phase on naminal 230 volt types

OUTPUT: Adjustable 110-120 volts on nominal 115 volt types
Adjustable 220-240 volts on nominal 230 volt types

ACCURACY: 1 volt band for line voltage variations and/or load magnitude and power factor changes

FREQUENCY: 60 cycles ±5%

WAVEFORM DISTORTION: 4% maximum

RESPONSE TIME: Less than ½ second for ordinary line and/or load changes. For extreme conditions of line and load changes, maximum response time is 2.0 seconds. (Response time is measured from the time of initiation of transient to the time when output voltage is within and remains within rated limits)

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POWER FACTOR: 0.5 lagging to 1.0

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THE MARCONI S.H.F. WAVEMETER

Type TF 1059

SPECIFICATION

FREQUENCY RANGE
4 to 10 KMC

ACCURACY
0.05%

DISCRIMINATION
0.02 to 0.03%

SENSITIVITY
A meter reading of greater than 15% f.s.d. is obtained for 1 mw input.

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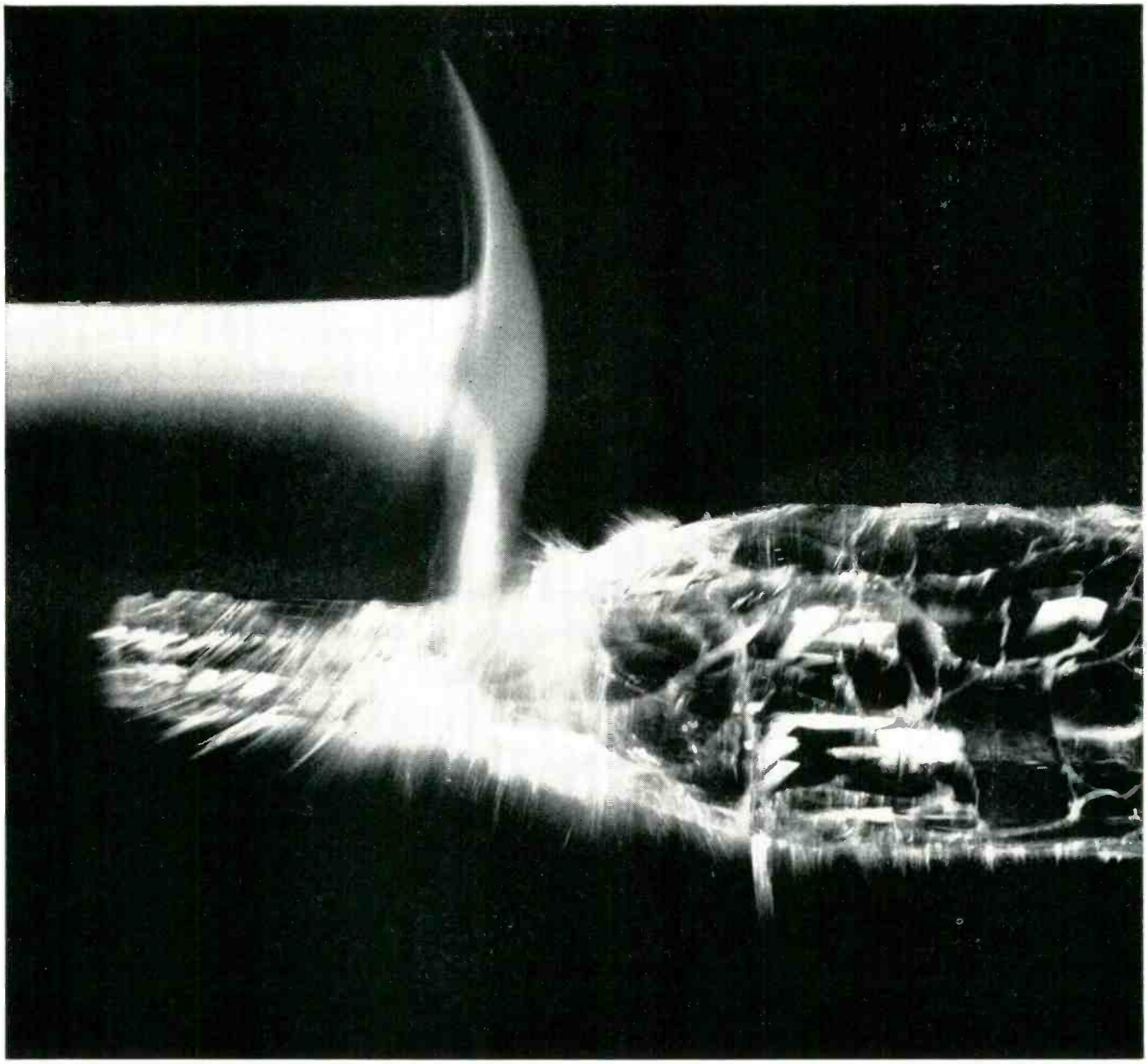

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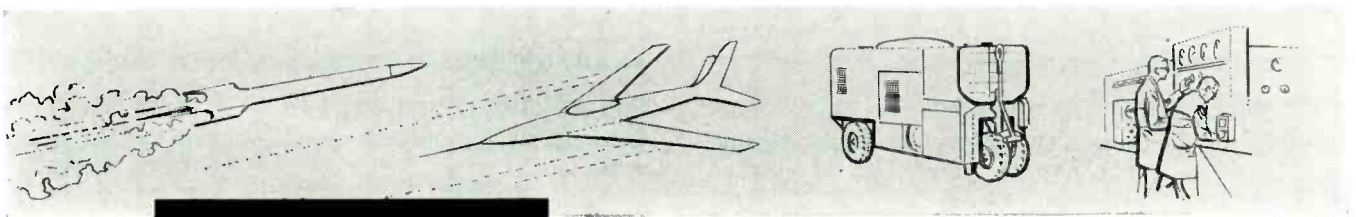

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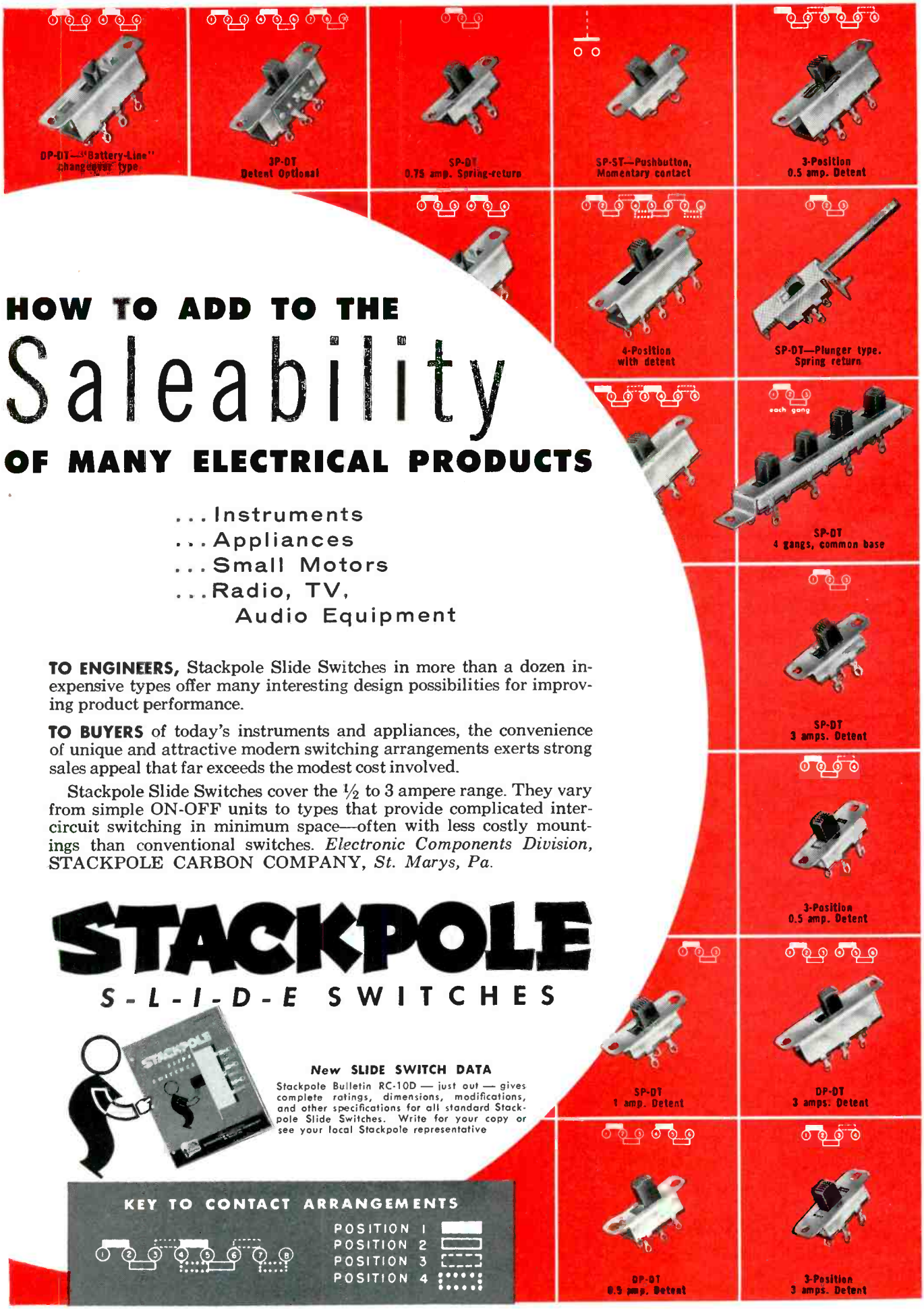

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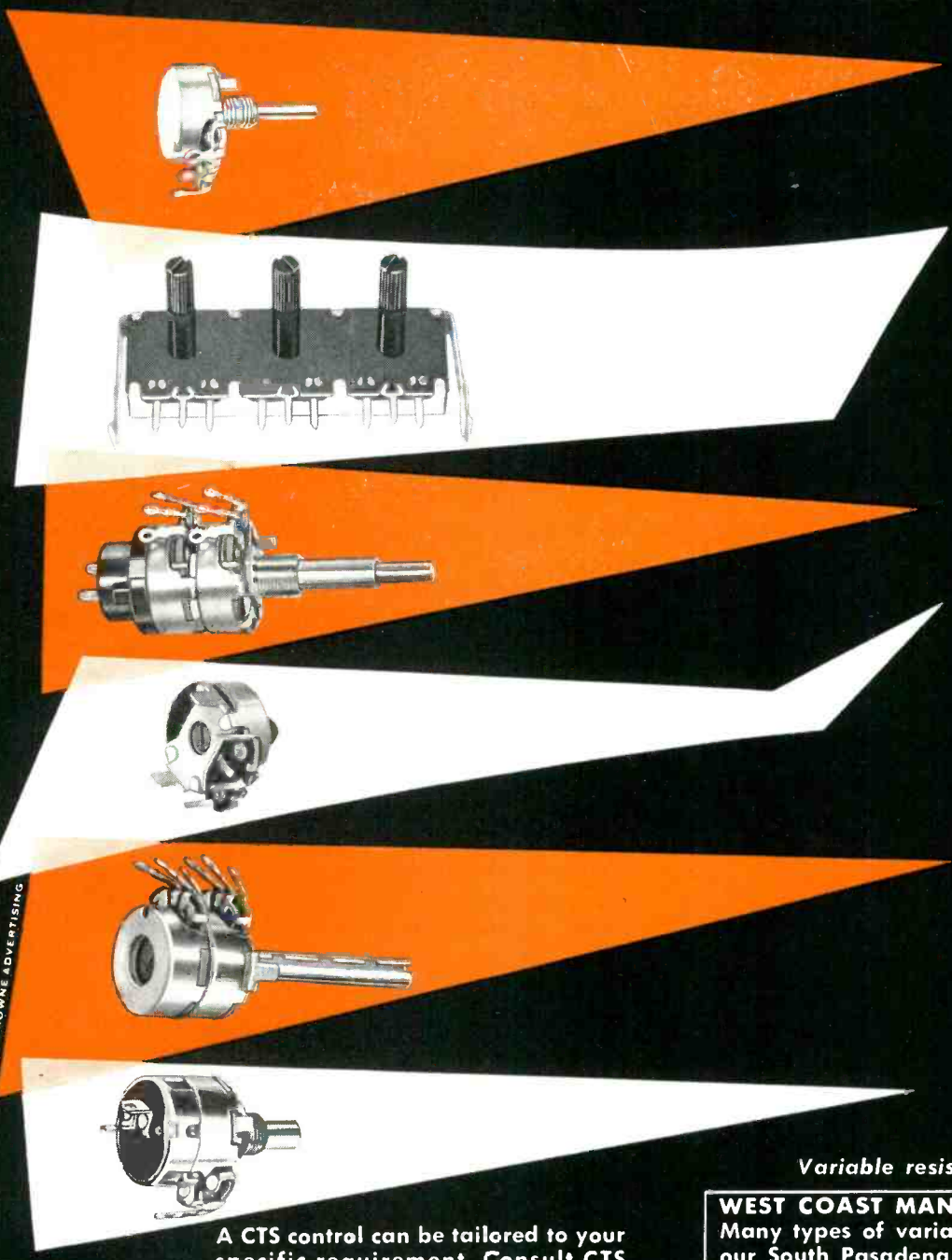

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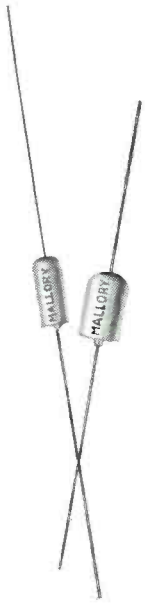

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W. W. MacDONALD, Editor

FEBRUARY 1 • 1957

CROSS TALK

► **CONSOLIDATION** . . . Technical progress has a habit of occurring in spurts. In between spurts there are lulls, or what appear to be lulls. Actually, these are often periods in which progress is being made on seemingly little things, too little to make the headlines in themselves. But these little things, in combination, are often the stuff of which important commercial developments are eventually made.

We seem to be momentarily in such a period. Many interesting technical developments are being reported to us but few of them appear to warrant page-one handling. Similarly, there is much commercial news but little of it is sufficiently different from the news of the past six months to have long-range significance. Rather, the industry appears to be gathering ideas and strength for the next big push, whatever and whenever this may be.

The key to 1957 may be consolidation of past gains.

► **MACHINE OF PARTS** . . . Designers of electronic equipment frequently use computers to predict the performance of new circuits. Usually, the values of the component parts to be initially used in the circuit are more or less arbitrarily chosen on the basis of past experience. If circuit performance is not what is desired new component values are substituted and the computer tries again.

Now comes a computer that eliminates still more cut-and-try. The design engineer feeds in information about the proposed circuit itself. He also feeds in the conditions to be satisfied by the circuit. The machine then tries various values of component parts in critical positions and delivers a complete answer so that the first prototype does the required job.

What comes next? Maybe a computer that designed itself.

► **BULLS** . . . Bearish attitude exhibited by many potential manufacturers of color-television receivers is not shared by technical personnel of non-color television stations.

Station engineers are itching for color, wait impatiently for their front offices to give the go ahead, wish the public would stir up the situation.

► **GRASSROOTS** . . . No shift in educational emphasis can do more than help reduce the shortage of engineers in the immediate future but more and more people are agreeing that the key to tomorrow is the phrase "Catch 'em young."

One way to interest promising youngsters in electronic engineering as a career is to invite grade-school and high-school pupils to tour plants, and particularly research laboratories. Teachers are a good point of contact.

If the electronics industry had started on this tack when the shortage first became apparent during the war, instead of scrambling each year since then for college graduates, the situation would be easier.

► **D.O.A.** . . . We haven't harped on the need for more careful assembly, inspection and packaging of electronic equipment for over a year but a recent experience causes us to pluck this string once again.

One unit of a pair of transceivers carried home for a tryout through the New York rush-hour proved to be dead on arrival. Inspection of the jangling innards disclosed that a vibrator had jumped its socket.

The particular point of this story is the fact that the equipment was designed for use in the Citizens' Radio band. The user is not supposed to open the little black box for any reason whatsoever.

► **HEADACHE, UNDERWATER** . . . One particular type of acoustical torpedo homes on the noise made by exploding air bubbles, and such bubbles are made by cavitation around a submarine's propellers.

Sub's countermeasure is to release a king-size Alka-Seltzer tablet, which makes bigger and better bubbles, luring the torpedo into an area where the sub ain't.

Typical studio setup uses conventional tv camera housing as flying spot source. Strobe units provide general lighting during blanking

Color TV System Uses

By HAROLD MATE

Technical Products Division
Allen B. Du Mont Laboratories, Inc.
Clifton, New Jersey

THERE has been a need in color-tv broadcasting for a high-quality live pickup device which is low cost and relatively simple to maintain and operate. To meet this need, the Vitascan system was developed. Although it can not replace the image-orthicon color camera, the system has features which can be used advantageously in commercial broadcasting.

System Operation

The system, shown in Fig. 1, is based on an extension of the flying-spot scanner principle.

The light from an unmodulated scanned raster is focused on the scene to be televised. The flying spot of light, which is reflected from the scene, is intercepted by eight pickup scoops, each of which contains four photocells; two of the phototubes in each pickup scoop are connected to the red-processing amplifier, one phototube is connected to the green-processing amplifier and the fourth phototube is connected to the blue-processing amplifier. A filter of appropriate spectral transmission is placed in front of each phototube so the electrical output from the tube is a measure of the intensity and color of the reflected light from the scene.

In the processing amplifier, each signal is properly clipped, phosphor corrected, gamma corrected and has the proper amount of pedestal added. The final output consists of three simultaneous color signals which can be applied to an encoder or simultaneous color monitor.

The system can be thought of as the reverse of a conventional studio camera setup. The phototube pickup scoops replace studio lighting fixtures and the cathode-ray-tube light source replaces the image-orthicon camera.

No light other than that created by the scanning beam can be allowed to fall on the photocells during scanning time. Any extraneous light would produce noise in the picture. The studio must, therefore, be constructed so that it is light tight.

To provide light for studio per-

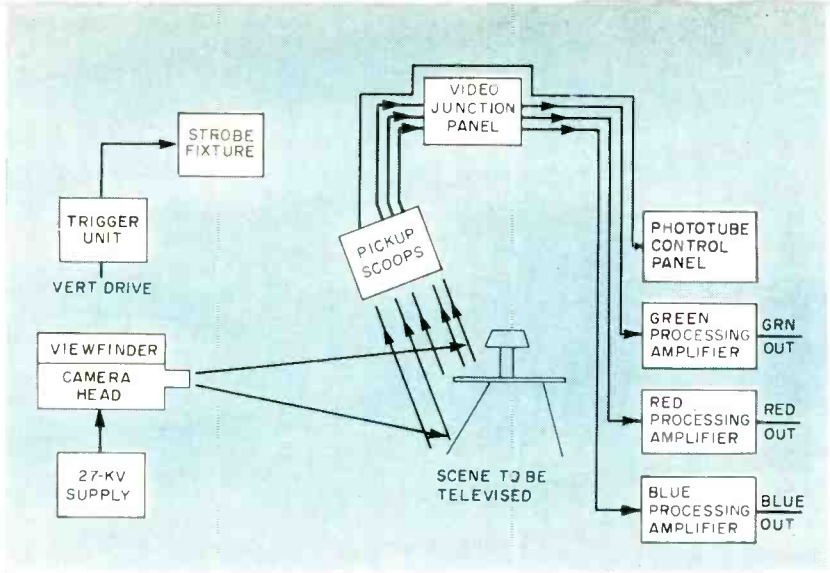


FIG. 1—Vitascan system for live color-tv pickup shown in block form

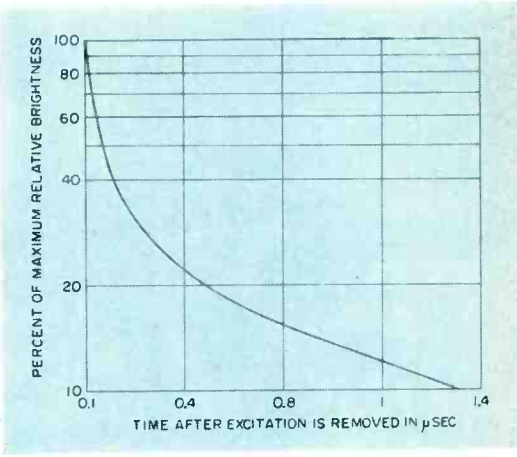


FIG. 2—Persistence characteristic of P24 phosphor

SUMMARY — Flying-spot scanner in camera head illuminates scene in darkened room. Reflected light is picked up by red, green and blue-sensitive phototube banks to form luminance and chroma signals. Strobe lights provide general studio illumination during blanking periods. System is applicable to live pickup for commercial broadcasting and for industrial applications

FLYING-SPOT SCAN

sonnel to see by, a bank of xenon lamps is ionized and deionized during vertical blanking time.

Camera Light Source

The mobile camera utilizes a 5AUP24 tube as the light source. The tube is mounted within the camera housing on a rack assembly that can be moved back and forth for best optical focus.

The tube is operated at 27-kv final anode potential, is electrostatically focused and draws approximately 300-μa cathode current. About 30 percent of the cathode current is utilized by the focusing electrode and the remainder is the final anode current.

The P24 phosphor is specifically used for flying-spot scanner tubes because of its short decay characteristic, which is shown in Fig. 2. The gun structure and small grain size of the phosphor in the 5AUP24 permit the scanning raster to be reduced in size and still maintain adequate picture resolution.

The reduced raster size allows shorter focal length lenses to be used for the same viewing angle. Table I shows the depth of field of these lenses. The short focal lengths considerably increase the depth of field of the system.

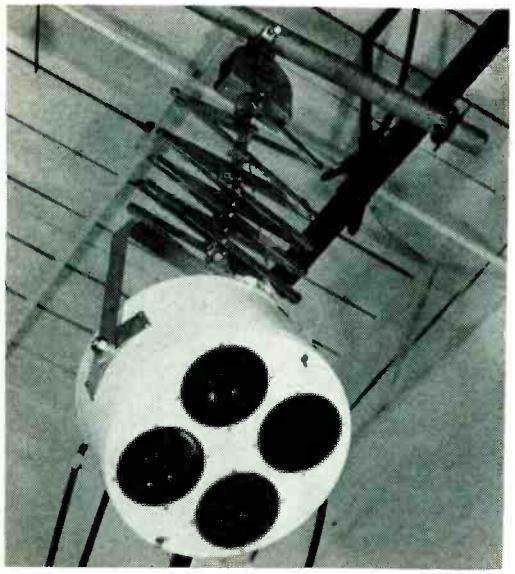
The standard complement of lenses for the camera is 101 mm, 150 mm and 210 mm, which corresponds to the 50 to 150-mm complement for an image-orthicon camera.

The camera sweep circuits are conventional. Both horizontal and vertical sweep can be adjusted to within 2-percent linearity over the entire raster.

Sweep Loss Protection

To protect the crt against loss of sweep, the protection circuit shown in Fig. 3 is provided. The vertical flyback pulse is applied to the plate of V_{1A} and rectified, charging C_1 to 165 volts.

The negative pulse from the horizontal output transformer is applied to the cathode of V_{1B}, which restores the tip of the horizontal pulse; the total of the charge on C_1 and the average horizontal pulse voltage appears across R_1 and R_2. A portion of this voltage is then applied to the grids of V_2 so that the tube conducts as long as horizontal and vertical pulses from their respective output transform-



Phototube scoops are hung from studio ceiling with pantographs

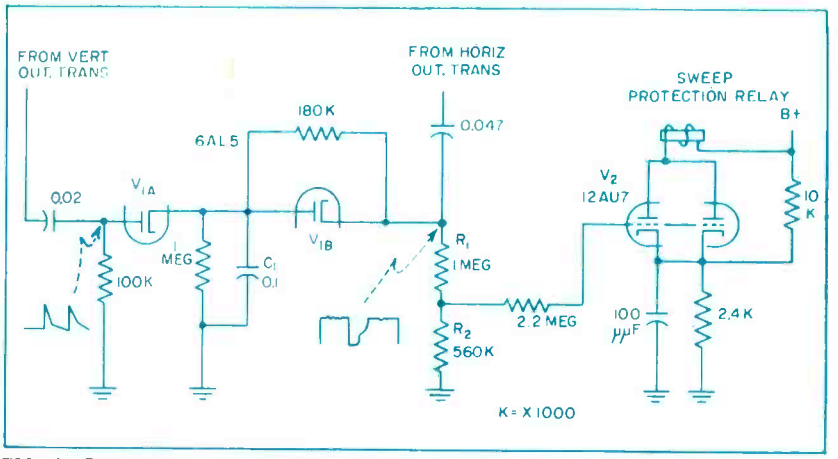


FIG. 3—Protection circuit prevents damage to crt in case of sweep loss

ers are present. If one or both pulses fail, V_2 cuts off and deenergizes the relay which biases the crt to cutoff.

Focus voltage for the crt is obtained from a bleeder placed between the high-voltage input and ground, as shown in Fig. 4. Resistor R_1 adjusts the bias on the 6BD4A which varies the plate-to-ground impedance and determines the focus voltage.

High-Voltage Supply

High voltage for the crt is supplied by a Du Mont 5313-B high-voltage power supply. This unit supplies 27 kv at 600 μa. The output of a blocking oscillator is coupled to a pair of 6CD6 tubes driving an autotransformer which supplies a 24-kv peak-to-peak pulse. The pulse is applied to a ladder-arranged high-voltage rectifier-quadrupler circuit in a lucite container. This container is filled with Dow Corning 200 Silicone fluid which eliminates corona and breakdown.

High-voltage regulation is accomplished by sampling a portion of the high voltage and feeding it through a d-c amplifier. The amplifier output determines the voltage on the screens of the 6CD6 drivers.

A standard image-orthicon viewfinder is placed on top of the camera head to permit framing and focusing. The video signal for the viewfinder is obtained from the monitor output of one of the video-processing amplifiers.

The photocells used to pick up the reflected light from the scene are K1416 red pickup cells and K1420 blue-green pickup cells. The cells are of the end-window type with 10-stage box-type dynode multipliers.

Average cathode sensitvity is 60 μa per lumen, optimum photoelectron collection is accomplished by adjustment of the potential between the separate shield and the photocathode. The box-type dynode results in low leakage currents because of the long leakage paths in the tube.

To properly shape the red, green and blue channel sensitivities for color tv, color filters are placed in front of the phototubes. Figure 5 shows the spectral output of the crt and the spectral response of the color filters and the photocell. The normalized resultant R, B, G sensitivities are obtained by taking the product of the three spectral responses and multiplying by a factor which will make the area under all three curves equal.

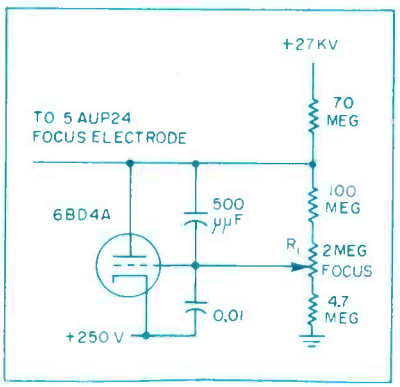


FIG. 4—Focus voltage-regulator circuit

Red Boosted

The most serious loss of signal is in the red channel because of poor red response in both the crt and the photocell. The red output is doubled by using two red phototubes for every green and blue tube. To obtain equal R, G, and B signals for equal-energy white balance, it is necessary to adjust the negative voltage applied to the cathodes of the photocells. A photocell voltage control panel is available for this purpose.

The video output of each pickup-scoop color channel terminates at a video junction panel located within the studio; from the junction panel the video is coupled to the proper processing amplifier.

Since the cable is not terminated at the junction panel, connecting cable from the pickup scoop must be kept short to minimize the capacitance at the junction point. For long video cables, a mixing amplifier would properly terminate the output of each photocell.

Processing Amplifiers

The video signals developed at the junction box are applied to the processing amplifiers (Fig. 6) through 185-ohm coaxial cable. To limit the high positive white peak on the grid of the second stage caused by the pulsed light source

required for illumination of the studio, a white clipper is added between the plate of V_1 and the grid of V_2.

This clipper takes the form of a crystal diode so biased that conduction will not occur when the positive pulse exceeds a prescribed level. The clipper is set so the pulse is not positive enough to drive the second video stage into grid current and yet is not clipped so low that compression of the video signal occurs.

Because of the finite decay time of the P24 phosphor (Fig. 2), it is necessary to insert peaking into the video amplifiers to correct the transient response of the system.

It might be assumed that a different frequency compensation would be needed for the transition from black to white than for the change from white to black since the phosphor excitation is practically instantaneous while the phosphor decay is exponential. If the spot were to scan from black to white, the photocell pickup would at first see a maximum brightness; then, as the spot moved, it would still provide the maximum instantaneous brightness plus the decaying brightness.

The light input to the photocell is, therefore, proportional to the integral of the original light decay

Table I—Depth of Field of Vitascan Camera Lenses

Focal Length (mm)	Subject Distance (feet)	Depth of Focus (inches)	Scanned Area
101 *f*2.8	5	10.7	28.4″ x 37.8″
	10	42.8	58.5″ x 78.5″
	20	171	9.98′ x 13.3′
150 *f*2.8	5	3.24	19.2″ x 25.6″
	10	19.3	40.6″ x 54.1″
	20	77	6.93′ x 9.24′
210 *f*3.5	5	3.0	13.1″ x 16.5″
	10	12.0	28.4″ x 37.8″
	20	49.0	4.9′ x 6.5′

characteristic. Since the decay characteristics is an e^{-t} function, its integral is of the same form.

Assuming that the light output as a function of time rises instantaneously and decays according to the function $L(t) = Ae^{-at} + Be^{-bt}$, the black to white signal is

$$S = \int_0^t L(T)dT = \int_0^t (Ae^{-aT} + Be^{-bT})dT$$

and

$$S = \frac{A}{a} + \frac{B}{b} - \left(\frac{A}{a}\right)e^{-at} - \left(\frac{B}{b}\right)e^{-bt}$$

At t infinity, $S = A/a + B/b$.

Starting from this level of signal, when the spot goes behind a mask

$$S = A/a + B/b - \int_0^t L(t)dt$$

$$= \left(\frac{A}{a}\right)e^{-at} + \left(\frac{B}{b}\right)e^{-bt}$$

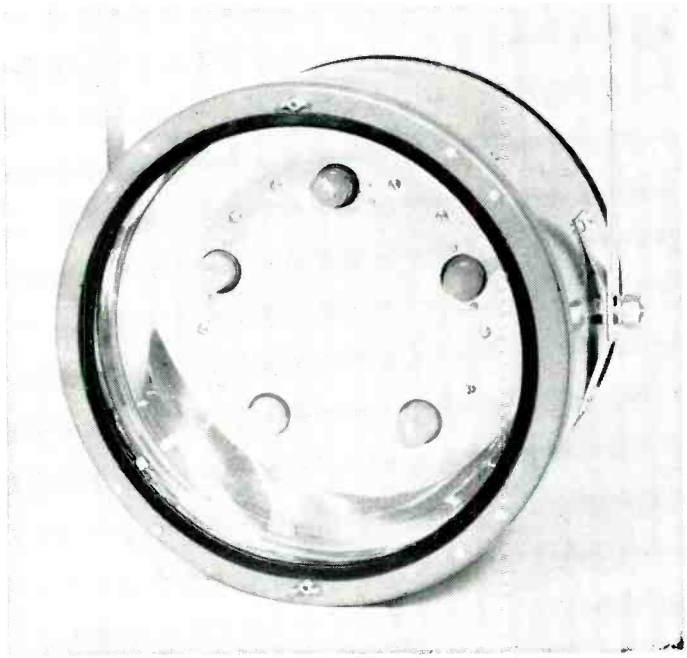
The shape is typical of the square-wave response of a circuit in which high frequencies are deficient.

Peaking

Peaking is accomplished in the first four stages of the amplifier by placing R-C time constants in the cathodes of these stages. The time constants can be adjusted so they peak at low, medium and high frequencies.

After phosphor correction, the black positive waveform at the grid of V_6 is clamped to blanking level by V_{11} during each horizontal blanking period.

The circuit in the cathode of clamped amplifier V_6 allows the gamma characteristics of the video amplifier to be adjusted as desired. At peak white, minimum signal to the grid of V_6, the three crystal diodes which shunt the cathode resistor are nonconducting and the stage gain is set by the 1,800-ohm resistor in the cathode. When the signal changes progressively from white to black, the three diodes



Strobe lighting fixture contains five xenon-gas lamps which are triggered by negative vertical drive pulses

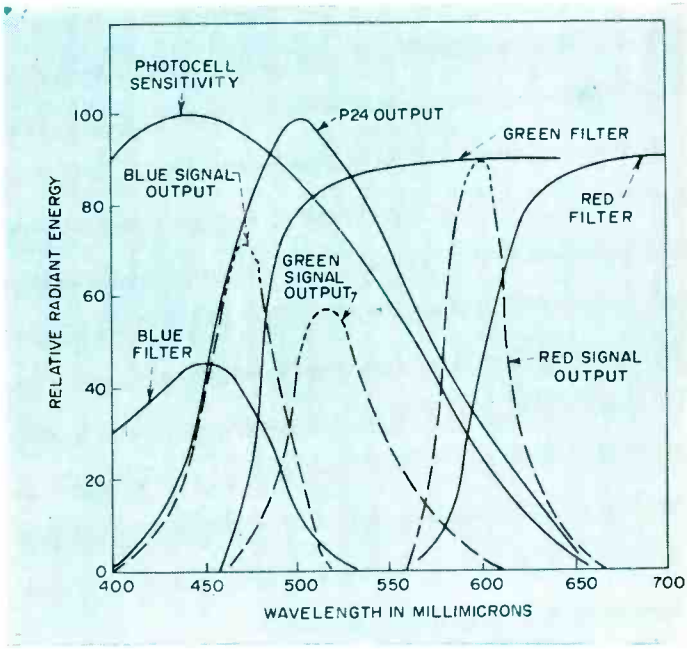


FIG. 5—Spectral response characteristics of crt, filters, phototubes and R, B, G outputs

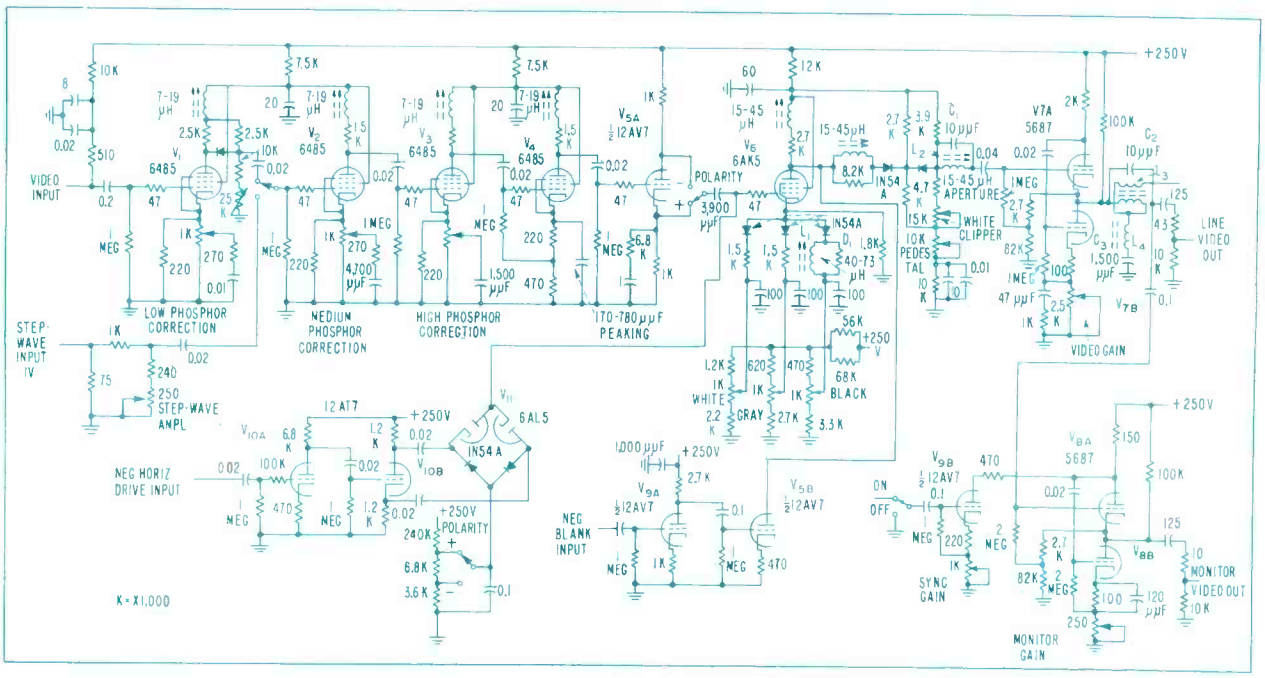


FIG. 6—Processing amplifier provides phosphor, aperture, gamma and other corrections for video signals from phototube banks

conduct in turn to lower the cathode impedance of V_6.

As each diode conducts, the lower cathode resistance causes increased gain in the stage; reaching maximum with a black picture. The three controls permit adjustment of the resulting characteristic curve of the amplifier stage in the separate portions designated by the titles White, Grey and Black.

Since stage gain is maximum at black level, the noise may become objectionable. To minimize the effect of the higher noise content of the black video, coil L_1 is inserted in series with black-stretch diode D_1 to cause high-frequency degeneration above 2.5 mc.

Addition of a large blanking pulse permits control of pedestal setup. The pedestal control consists of a crystal diode inserted between the plate of V_6 and the grid of V_{7A}.

During the time of normal video, the anode of the diode is more positive than the cathode. When the negative blanking is added, its voltage drives the diode plate less positive than the cathode and so cuts off the signal. Changing the diode cathode voltage with the pedestal control changes the point of cutoff and so sets the pedestal level.

Aperture Correction

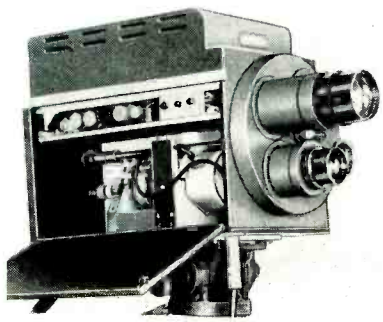
Network L_2C_1 is used to improve the high-frequency detail lost by the system optics; L_2 permits the peaking to be adjusted from 7 to 12.5 mc.

Since the relative phase shift of the aperture correction network is positive, a lagging phase shift network, C_2, L_3, L_4 and C_3, is inserted so that the total phase shift will be zero.

The output stages, V_7 and V_8, used in the processing amplifier are essentially double cathode followers, each capable of producing a 1½-v signal with good linearity and frequency response along with low power consumption.

Assuming a g_m of 5,000 micromhos for each half of the 5687, the midfrequency gain from the grid of V_{7A} to the video output termination, with the video gain control at maximum, is 0.475. Under these conditions, the output impedance is 32 ohms. To match the impedance of the 75-ohm coaxial cable, a 43-ohm resistor is inserted in series with the output.

The stage response is about 1 db down at 10 mc.



Camera head contains crt light source

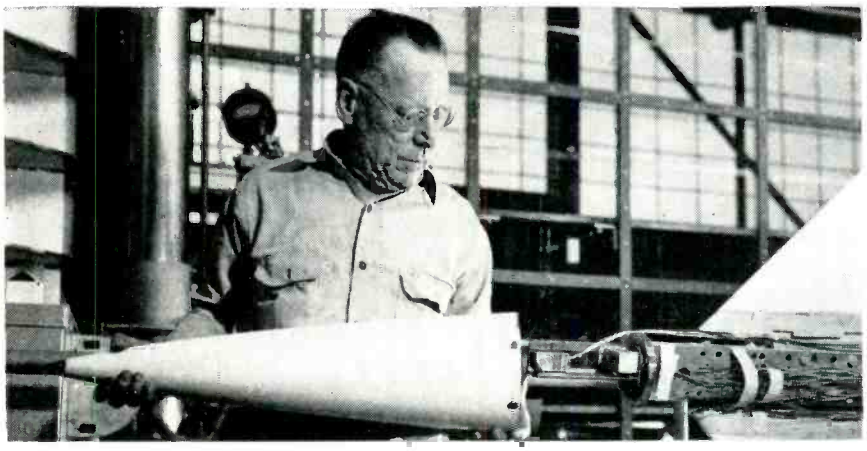
Sync Light System

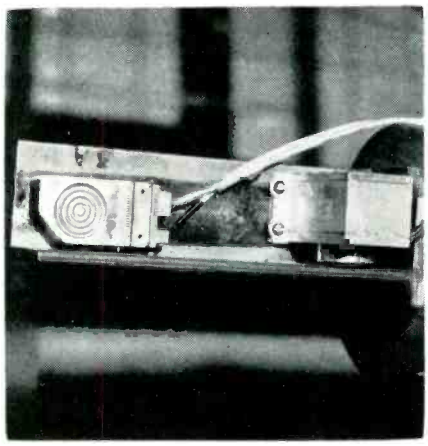
To produce the pulsed light for studio illumination, an Amglo U-35K lamp is used in the sync light equipment. This lamp is a U-shaped tube containing xenon gas with electrodes located at each end of the tube. The high voltage trigger potential is applied to bands wrapped around the outside of the tube. When the trigger voltage is applied, the gas is ionized and the d-c potential applied between the ends of the tube causes gas current flow; the gas produces blue-white light output.

To provide a suitable light level, five xenon lamps are used in each light fixture and four fixtures are used with each system.

The light trigger unit consists of a negative vertical drive pulse amplifier and a thyratron which develop the trigger pulse applied to the high voltage transformer in the light fixture.

When the high-voltage trigger pulse ionizes the xenon gas, a capacitor connected across the xenon lamp discharges through the lamp producing the blue-white glow used for lighting.





Capacitance-pickup gage in body of model is checked before nose assembly is installed. Close-up (right) shows installation

Capacitance Pickup Measures Small Forces

By JOHN DIMEFF and THOMAS B. FRYER

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SUMMARY — Noncontacting arm on angle-of-attack potentiometer reduces friction to permit measurement of very small forces acting on airplane models in wind tunnel. Accuracy and repeatability of unit is within ±0.02 degree of rotation over temperature range from 0 to 150 F at pressures from 0 to 70 psi

WIND-TUNNEL testing requires a small device that can be mounted inside a test model to measure angle of attack, or the rotation of the model about a horizontal axis. Accuracy must be maintained while the model is subjected to large excursions of ambient pressure and temperature and to rotations of ±40 deg about the two axes perpendicular to this horizontal axis.

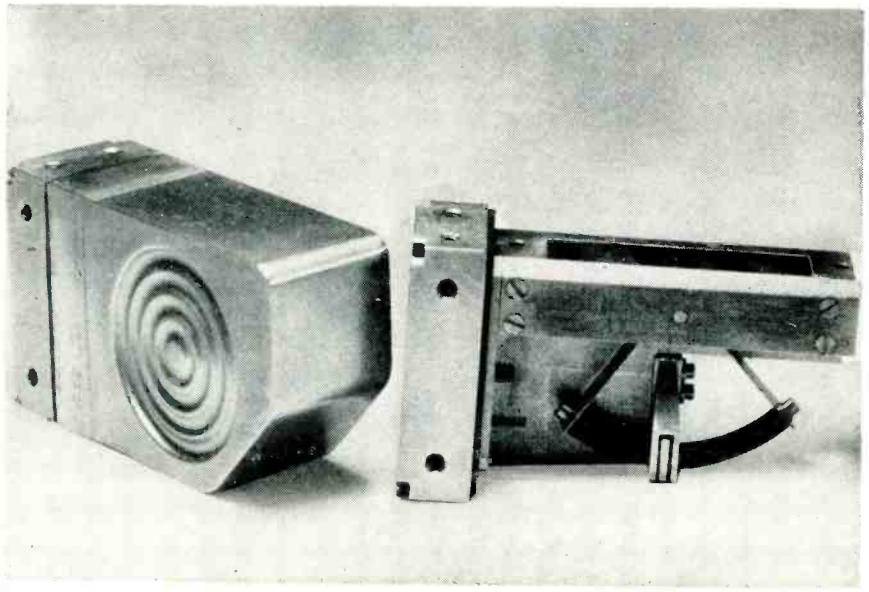
A resistance-potentiometer element suspended as a pendulum and moving past a wiper is the simplest system usable in the tunnel environment. A method devised to overcome the restrictions of friction associated with the potentiometer wiper has also provided improvements in problems of resolution, linearity and hysteresis.

Contactor

Undesirable effects of wiper friction are eliminated by moving the contactor slightly away from the resistance element, so that direct mechanical connection is removed. Electrical connection is maintained by electrostatic coupling. The contactor, or coupling plate, thus becomes a capacitance plate in close proximity to certain portions of the resistance element and greatly removed from others.

The arrangement of the contactor is shown in Fig. 1A. The equivalent circuit of this frictionless contactor is shown in Fig. 1B. An alternating potential, applied across the resistance R, causes the flow of current through the capacitance formed between the coupling plate and those elements of resistance in close proximity to the coupling plate.

The magnitude of current flow



Angle-of-attack transducer uses resistance element pivoted as pendulum on jeweled bearings passing through capacitance pickup arm

is determined by the position of the coupling plate, the effective capacitance between resistance element and the coupling plate, and the impedance of the circuit between the lead to the detector unit and the return to the alternating potential source.

The operation of the normal slidewire-type potentiometer element is thus altered in several important respects. Frictional restraint and wear are eliminated. Since the modified device depends on electrostatic coupling which gradually shifts from one wire to the other, greater resolution is obtained. Electrostatic effects of the various elements of the resistance wire within the region of influence of the coupling plate are effectively averaged by the plate. Local nonlinearities are averaged over the length of the coupling plate and the effective linearity of the transducer is thereby increased.

Bridge Circuit

Since the magnitude of the coupling capacitance could be greatly altered by small physical shifts of the resistance element in a direction perpendicular to the direction of motion and since electrical leads to remote indicators might present large and nonconstant-impedance loads, an indicating circuit must be utilized which allows accurate detection of the angular position of the coupling plate in the presence of these variable electrical quantities.

The basic circuit shown in Fig. 1C is satisfactorily insensitive to impedance in the detector circuit. The resistance element of the basic transducer is divided into two parts, R_1 and R_2, formed between the electrical center of the coupling plate and the two ends of the resistance element. These two parts are connected in a resistance bridge, the remaining two parts of the bridge, R_3 and R_4, being formed by a remote resistance potentiometer of conventional type.

The movable contact of the remote potentiometer is grounded. Under balance conditions, the electrical lead to the capacitance coupling plate is, therefore, at ground potential. Since the shield of the coaxial cable connecting the transducer to the remote detector is also at ground potential, no current flows in the circuit at bridge balance, and therefore, the circuit is insensitive to coupling, cable and detector impedances.

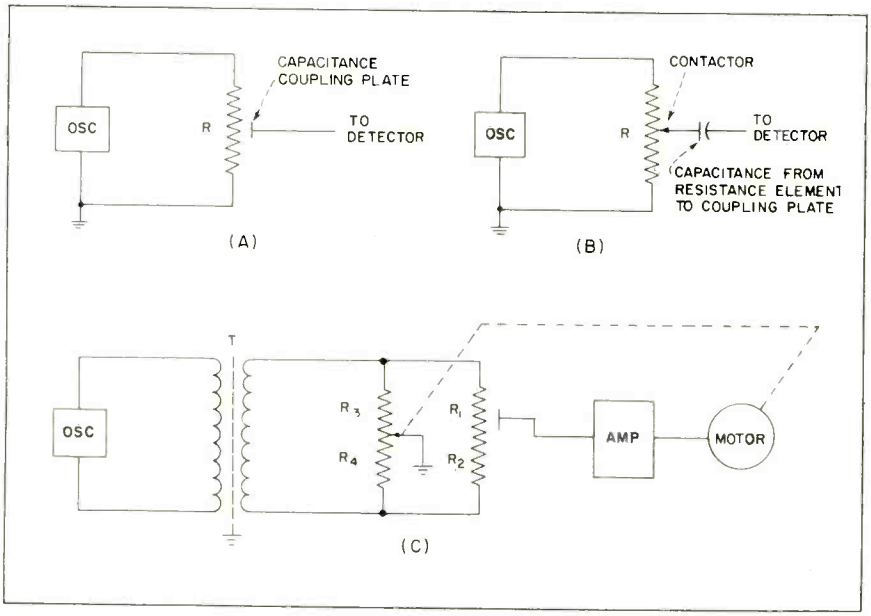


FIG. 1—Capacitance-coupled potentiometer (A) and its equivalent circuit (B). Bridge arrangement (C) permits balancing out cable capacitances

Construction

The angle-of-attack transducer utilizing this technique is shown in the photographs. The pendulum formed by the resistance element moves past a stationary coupling plate by rotating on an axle supported at its two ends by jeweled pivot bearings.

All elements of the coupling plate circuit are shielded to prevent coupling to extraneous elements of the resistor or its leads. Accuracy and repeatability of the unit are limited predominantly by the friction of the jeweled bearings and have been found to be within ±0.02 degree of rotation. Overall rotational range of the instrument as designed is ±30 deg.

Effects of temperature from 0 to 150 F and pressure from 0 to 70 psi are negligible. Rotation of ±40 deg about axes perpendicular

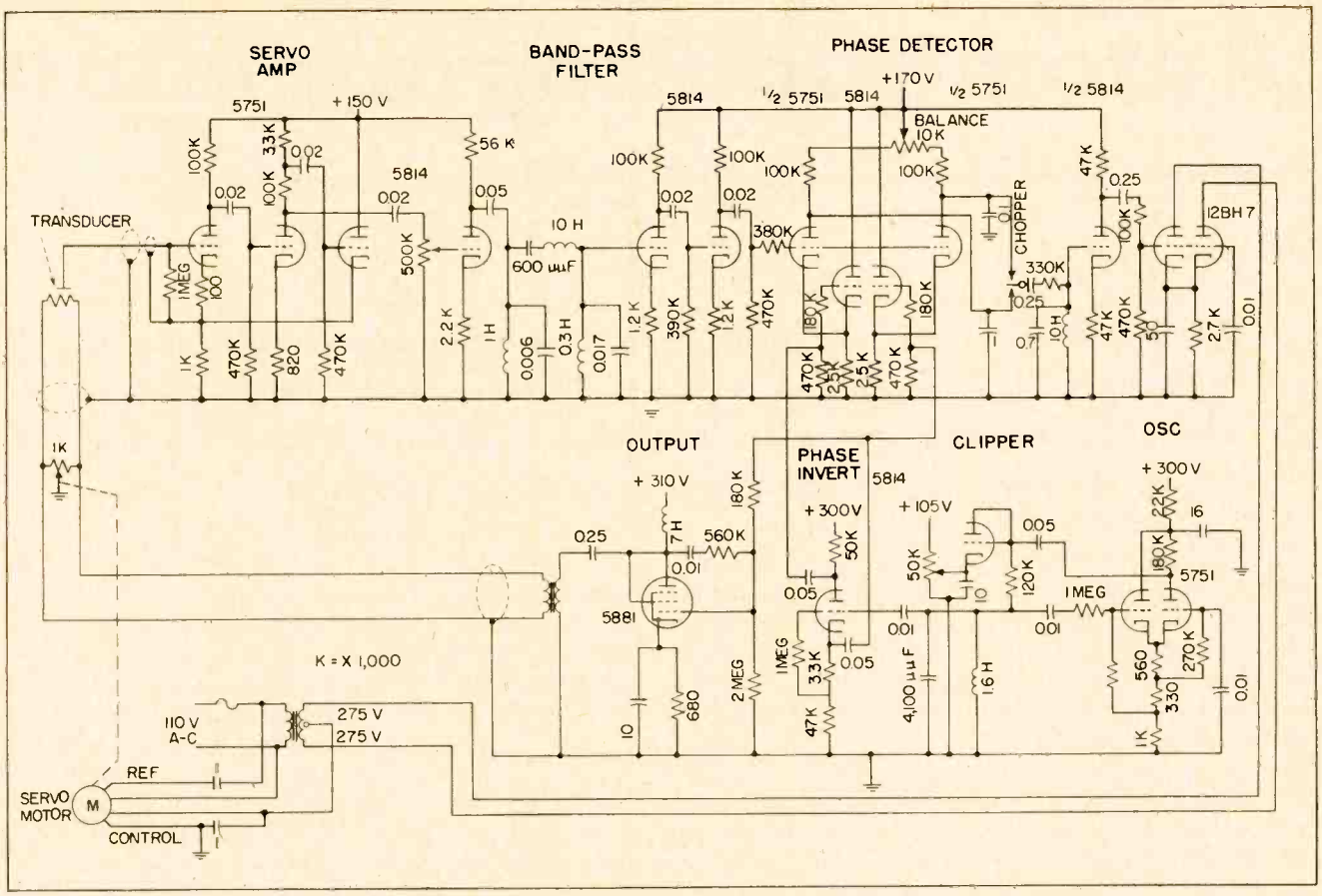


FIG. 2—Complete self-balancing system uses 2-kc oscillator to drive transducer bridge. Error signal is balanced out by servo-driven potentiometer fed from output of servo amplifier through phase detector

to the sensitive axis produced no change in calibration of the unit.

The circuit used in the final installation is shown in Fig. 2. The servo-balancing bridge of this circuit is supplied with a 10-volt rms, 2-kc signal. Choice of the operating frequency is not critical.

A 5751 tube is used as a 2-kc oscillator with one section of a 5814 connected as a diode clipper to regulate amplitude. The other half of the 5814 is used as a buffer amplifier and a phase inverter to drive a 5881 output tube. To avoid capacitance unbalance in the bridge, a well-shielded power transformer is used to couple the 5881 to the resistance bridge.

The first two tubes of the servo amplifier amplify the error signal between the servo potentiometer and the capacitance-coupled potentiometer, and provide a low-impedance source for driving the inner-shield of the triaxial cable. If the inner shield of this cable is maintained at the same potential as the center wire the value of effective cable capacitance is reduced to zero.

The circuit has a gain of approximately 0.99 from the center wire to inner shield giving an effective reduction in capacitance by a factor of 100. Since the coupling capacitance in the potentiometer is only 3 to 10 $\mu\mu$F, a reduction by a factor of 100 in the cable capacitance makes possible the use of long cables without excessive reduction in the error signal.

The 5814 tube is followed by a pi-section bandpass filter that has a fairly broad characteristic ($\pm$100 cps at 2-kc) but which effectively reduces signal harmonics and extraneous noise. The signal is further amplified and applied to a phase-sensitive demodulator.

Demodulator

The phase-sensitive demodulator is a full-wave cathode-switched circuit. The input signal is connected to the grids and the detected signal appears between the plates of the 5751 tube. This signal is modulated by a 60-cps chopper and amplified to drive a servo motor. The motor is in turn coupled to the servo-potentiometer and rotates that potentiometer in such a direction as to reduce the error signal sensed by the amplifier.

Although the capacitance between the coupling plate and potentiometer resistance element in the angle-of-attack unit is of the order of 2 $\mu\mu$F, the circuit shown in Fig. 2 has allowed use of one-hundred feet of cable between transducer and servo.

The substitution of a capacitance coupling plate for the direct contacting wiper of the normal resistance potentiometer provides considerably increased resolution and linearity. The elimination of contactor friction resulting from use of such a device allows measurement of displacement where forces are so small that hysteresis introduced by wiping friction of the normal contactor would be prohibitive. By proper design of electronic circuits used with the capacitance contactor, the undesirable effects resulting from high contactor impedance can be greatly reduced.

Automatic Programming

By ED C. MILLER

Technical Director
Inland Broadcast Co.
Weiser, Idaho

SUMMARY —— Subsonic tones control operation of automatic record player and tape recorder to permit small station to prearrange one-hour program of records and commentary in 3 to 10 minutes recording time. Control console can be operated by nontechnical personnel

AUTOMATIC control systems have been used for years in the radio broadcast field for frequency control of transmitters, lightning arc suppression and overload reset. Larger stations and network feed points have used many more automatic devices. Small stations have just now begun to exploit automatic control in programming, logging and filing. The system described here handles microphone and turntable switching and fading that takes up much of the time of a disc jockey at a small station, and concentrates his time for introduction of records and reading of spot announcements into a continuous period of talk.

Operation

This control unit works in conjunction with an Ampex tape recorder and Seeburg automatic music system. Switching is accomplished in each case by making and breaking the motor leads to both units and is controlled by a 20-cps tone and 1.8-sec time delay. The 20-cps tone is superimposed on the tape when it is recorded. This tone trips the music system to set up the next record. The end of the tone stops the tape transport and switches the faders, fading the tape output and increasing the music level. The 1.8-sec time delay occurring at the end of a musical selection reverses the fader operation, starting the tape and stopping the music system. A 35-cycle tone can be superimposed on the tape when it is recorded to switch to an alternate tape machine at its release. Then, whichever tape machine is operating continues to operate until a 35-cps tone appears at which time it switches to the other tape.

Automatic programming system uses portable tape recorder and automatic record selector-player mounted on wall

Figure 1A shows the basic circuit of the tape-phono control. With no signal input from tape or phono, V_1 and V_2 are conducting. When a 20-cps tone passes the selective amplifier into the tape input, it is rectified by V_3, and filtered by C_1, R_1 and C_2 only enough to prevent the V_1 relay from chattering. This negative d-c cuts off the grid of V_1 and deenergizes its relay, closing the contacts to the music-system motor. The other contacts of the relay open the grid of V_2, it continues to conduct and RE_2 remains closed.

This condition exists until the tone stops, at which time the fast discharge of C_1 causes V_1 to conduct again, closing V_1 relay, opening the phono motor circuit. The phono unit continues to operate since the motor in the music system is locked on during the playing of a record,

in Small A-M Stations

and is released after the record trips at the end of play. The other relay contacts return the grid of V_2 to V_5 so the charge which has been slowly acquired by C_3 through R_2, appears on the grid of V_2, cutting this tube off.

The opening of RE_2 stops the tape motor, switches the faders and also applies a positive voltage through R_3 to the grid of V_1 to assure that it continues to conduct while the tape is stopping. This prevents any extraneous noises on the tape after the end of the tone from reactivating the two relays.

The slow discharge of C_3 through R_4 and R_5 keeps V_2 cut off for about seven seconds. During this time, relay RE_2 is open and its contacts have opened the motor lead to the tape recorder transport and switched the faders in favor of the music system input. This time is ample to cover any dead grooves at the beginning of the record and as soon as the music level is rectified by V_6, it is filtered by R_6 and C_4 and applied to the grid of V_2 to keep it cut off.

Thus, relay RE_2 remains deenergized during the playing of the record and for a period of time after the record has ended, determined by the discharge rate of C_4 and R_5 (in this instance, 1.8 seconds), at which time V_2 conducts, starting the tape transport and switching the faders. To prevent tripping RE_2 by noise from the music system, the cathode of the phono-isolation amplifier is made positive when RE_2 is energized.

Small recording console controls tape recorder, inserts tones and indicates elapsed time during recording of announcements

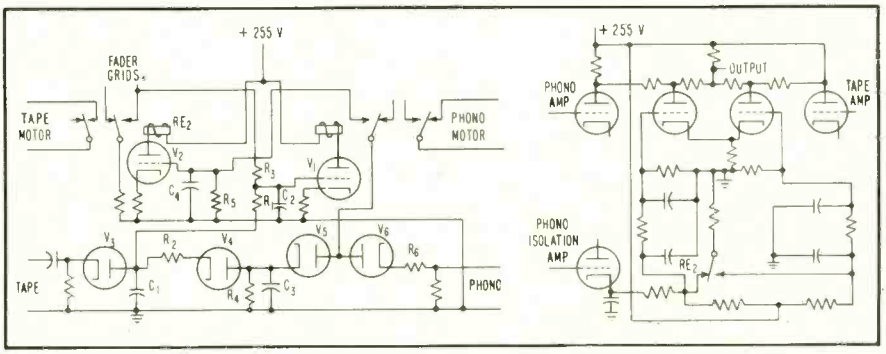


FIG. 1—Tape and phono-motor control section (A) and fader section (B) of automatic programming control system

Fading

The basic fader circuits are shown in Fig. 1B. As can be seen from the circuit, T-pad electronic attenuators are used, with control provided by positive voltage applied to alternate grids. Because grid current flows during times when the grid of either fader is positive, large electrolytic capacitors are used to provide the time constants for attack and release. By using the switching arrangement shown, the actual switched voltage is about 10 volts. Resistors are placed from each grid to ground to limit the voltage across the capacitors in the event of tube failure, or if the B+ voltage should be present before tube heaters have reached operating temperature.

The cathode of the phono-isolation amplifier is connected to the switch contact of the phono fader. When that contact is opened and its voltage goes positive, it cuts off the phono isolation amplifier and fades the phono input.

It is not considered advisable, from a programming standpoint, to fade the phono more than about 15 db. The 20-cps tone can be placed in advance of the end of the voice on the tape, which will allow the

record to be placed on the turntable and music to start while the announcer's introduction is being presented on the tape. This permits introductions over the musical introduction on the record and allows more versatile operation that more nearly approaches manual programming in results.

Figure 2 shows the complete schematic, including the isolation amplifiers, selective amplifier, delay circuits, control circuits and faders.

The amplifiers are straightforward circuits. The selective amplifier uses a twin-triode with a bridged T in the negative feedback circuit, to provide amplification only at 20 cps. A form of volume limiting is provided by clipping in the first stage of this amplifier. Clipping of the phono level is done in the triode driver of the phono rectifier.

Control Circuit

Because the control unit is used by nontechnical personnel, it is necessary to have a recording consolette that applies the proper tone of correct duration, and records the elapsed talking time in as automatic a manner as practical.

The schematic of the consolette is shown in Fig. 3. In operation, S_1 is switched to the start position when it is desired to start recording. Its contacts close the circuit for relays RE_3 and RE_4 across the 115-volt d-c supply and discharge C_2 through the 200-ohm resistor. The contacts of RE_3 close the motor circuit for the tape recorder. Contacts of RE_4 apply 115-volts a-c to the clock and it begins timing the talk. Light P_1 or P_2 will also operate, indicating the tape transport is moving and indicating also which switching function, tape to music (20 cps), tape to tape (35 cps) or no tone, will be accomplished at the end of the talk period.

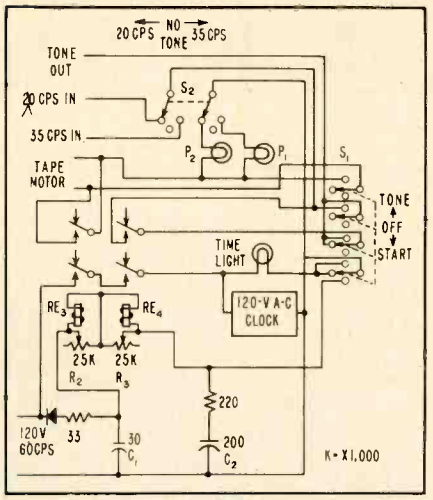


FIG. 3—Dual input control circuit provides automatic switching between record player and tape unit

No tone is used at the end of a break spot, for example, if the next program is a live program, given at the broadcast time. Thus, if the board operator is a little slow in switching off the tape, there will be no tone present to insert the first record of the next program, prematurely.

When S_1 is returned to its neutral position, RE_3, RE_4 remain closed for an additional period of time determined by the combined R-C time constants of C_2, RE_3 and R_2 and RE_4 and R_3. Variable resistances are used across each relay to compensate for minor differences in drop-out current.

If S_1 is moved to the tone position, the tape transport control and tone contacts of RE_3 and RE_4 are shorted out by the contacts of S_1 and the tone and transport continue to operate until S_1 is returned to the off position or for the duration of the time constant whichever is longer. The duration of this time constant is set by R_2 and R_3 to about 6 seconds.

The timing clock starts running when S_1 is switched to the start position and stops 6 seconds after S_1 is switched to the off or tone position. The time light comes on when the tone starts and stays on for 6 seconds. When the time light goes off, it provides a visual indication to the operator that music has started in the background.

The clock runs only when the tape is running and there is no music. This makes it possible for the operator to total his music time, subtract this figure from the actual program time, and arrive at the total talking time available.

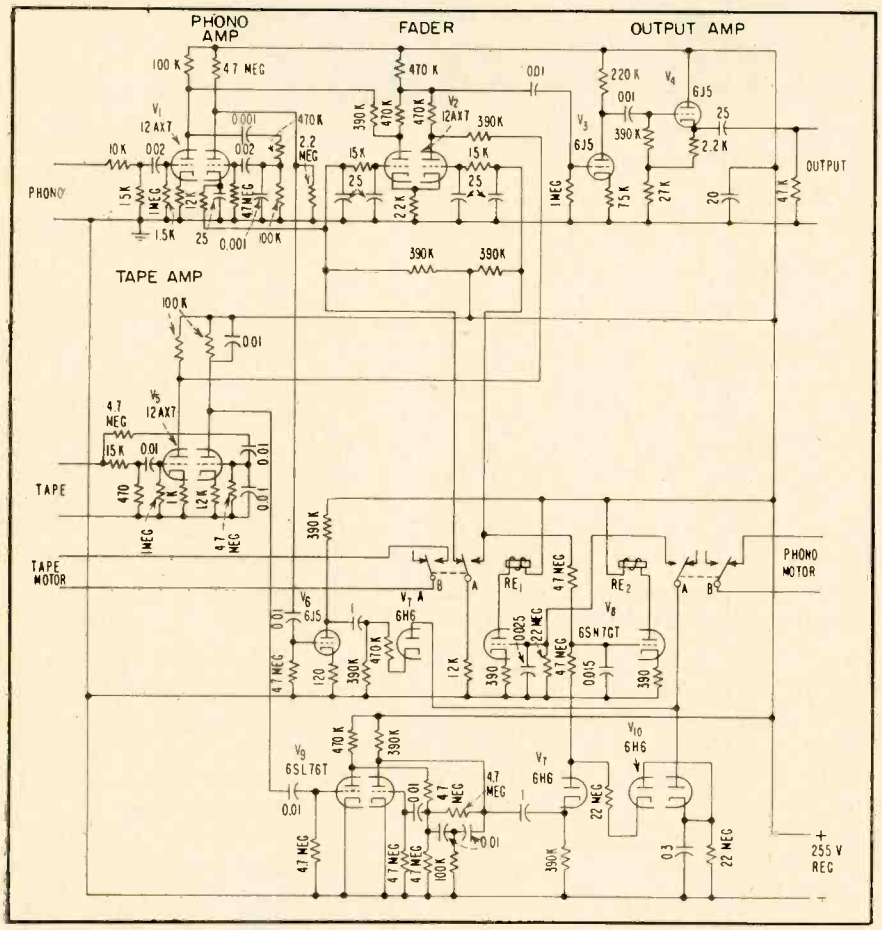
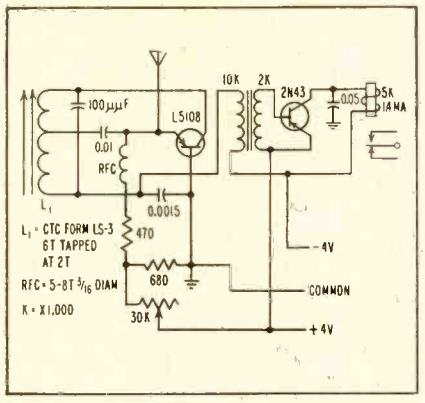
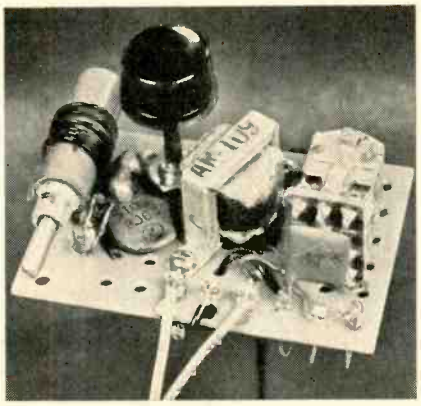
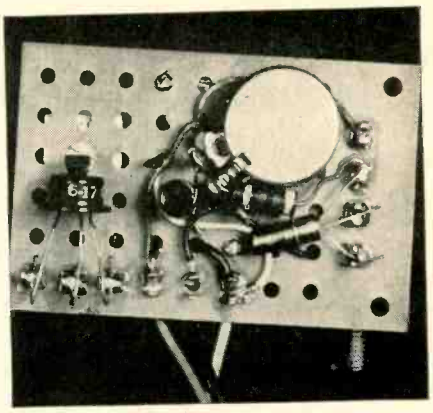


FIG. 2—Recording console places tones on tape and indicates elapsed time during recording of commentary



Circuit uses a Philco surface barrier transistor operating at 27 mc





Tuning coil and fixed capacitor, squelch control, audio transformer and remote control relay above chassis with two transistors beneath (right)

Remote Control Receiver

By EDWIN BOHR

Huntsville, Ala.

SUMMARY —— A lightweight device capable of actuating electrical circuits comprises a two-transistor superregenerative receiver operating on the 27.255-mc Citizen Radio frequency for which formal license is not required

ADVANTAGES of a completely transistorized remote-control receiver are realized in the circuit described below. Superregenerative operation at the license-free frequency of 27.255 mc is obtained through use of the L-5108 surface barrier transistor.

Because the detector functions at a power level insufficient to operate a normal remote-control relay, an additional transistor stage amplifies the quench frequency to drive a conventional plate relay.

The detector operates with a grounded base. Feedback is tapped from the tuned circuit to the emitter through a rather large value of coupling capacitance. This coupling capacitor periodically quenches the detector oscillations. Rectification of the oscillator frequency by the emitter charges this capacitor sufficiently negative to block oscillation.

The Q of the tuned circuit and in general the vigor of the oscillator determines the build-up time of this blocking action. The decay of the blocking depends upon the value of the coupling capacitor and the Thevenin equivalent resistance of the bias supply.

Using a low value of emitter-bias resistance results in much the same action as returning a vacuum-tube superregenerator grid leak to the plate supply.

Quench Frequency

An interruption frequency from 10 kc to 30 kc seems to yield the greatest sensitivity. In addition to the usual quench frequency, there is a lower frequency component available at the detector output. This lower-frequency component is somewhat greater in amplitude than the high-frequency quench. In addition, it is a submultiple of the high-frequency quench, falling somewhere near the resonant frequency of the coupling transformer and collector bypass capacitor. A typical frequency for this low-frequency component is 3 kc.

The received signal from the remote-control transmitter advances the initial oscillator build up, increasing the quench frequency. A reduction in the quench amplitude also accompanies this action.

A strong signal will reduce the quench amplitude by a factor greater than two-to-one. It is this effect that operates the relay.

A 2N43 relay-driving amplifier receives the quench components through the coupling transformer. The low winding resistance of this transformer accounts for the low value of collector leakage current. A representative 2N43 in this circuit with no signal input between base and emitter may have a quiescent collector current of only 20 microamperes at room temperature.

The relay-driving amplifier both rectifies and amplifies the quench components. The resulting current pulses at the collector are smoothed by the 0.05-μf ceramic plate capacitor.

SUMMARY —— Capacitor-discharge unit for extremely thin, highly conductive metals provides up to 10,000 amperes in single millisecond pulse. Voltage regulator tube in simple control circuit stops recharging of capacitor bank at exact voltage level called for by heat control potentiometer. As charging voltage approaches this level, regulator tube current applies increasingly greater negative bias to grids of thyratron rectifiers in power supply. Welder cannot fire until weld pressure is exactly correct, thereby insuring repeatable perfect welds

By W. W. ROBINSON
Chief Engineer
Pacific Welding Co.
Los Angeles, Calif.

Precision Spotwelder

ATTEMPTS to spotweld fine wires or thin foils are often unsatisfactory because the uncontrolled high-energy discharge of conventional welding machines damages the extremely thin, highly conductive metal. The resulting unsightly weld joints often require considerable reworking before the materials can be plated or otherwise finished. Because of this, many fine wires and foils have been considered unweldable.

A solution to this problem was found in the development of a stored-energy spotwelder that delivers controlled high peak current at the electrode tip and repeats the exact discharge for each succeeding weld. The energy is stored in a capacitor bank for intermittent use by welding electrodes. Secondary current at the electrode tips may have a high peak magnitude (up to about 10,000 amperes), completely discharged in 0.0030 to 0.0166 second for each spotweld.

Circuit Description

As indicated by Fig. 1, storage-capacitor bank C_3-C_4 is supplied with energy at a level of approximately 1,500 volts d-c by a full-wave rectifier power supply. The capacitor bank is connected to the primary of the welding transformer through thyratron firing tube V_6, which is normally biased below cutoff so that the tube functions as a switch when the bias is momentarily removed.

When the switching action of the thyratron takes place, the capacitor bank is discharged through welding transformer primary T_3 so that current will flow in the secondary and energize electrodes closed on a workpiece.

Primary power is supplied to transformer T_1 and to all tubes when a heater switch and safety interlock are closed. A six-minute time-delay cycle prevents damage to the tubes before they are adequately warm.

At the end of the warm-up cycle, a relay removes power from a time-delay motor. A high-voltage switch can then be closed to apply primary power to T_2 and energize relay K_2, removing shorting resistors R_2 and R_3 from across the capacitor bank. Rectifiers V_3 and V_4 now charge capacitor bank C_3-C_4.

Charging Control

When the d-c voltage between the cathodes of voltage regulator tube and B + is large enough to cause the voltage regulator tube to pass current, a negative voltage appears at the anode and acts in series with the a-c voltages on the grids of the rectifier tubes. This bias serves to hold off the rectifier tubes for a part of each a-c cycle.

As the capacitor bank becomes more and more fully charged, the bias voltage produced by the regulator tube increases and holds off the rectifier tubes for a correspondingly greater portion of each a-c cycle.

When the capacitor bank is charged to the level corresponding to the setting of the heat control, regulator tube current has increased to the point where the rectifiers are cut off and charging ceases. This insures that the capacitor bank is charged to the same level after each weld, no matter

Operator adjusts spotwelder controls. Welding transformer is in box at right

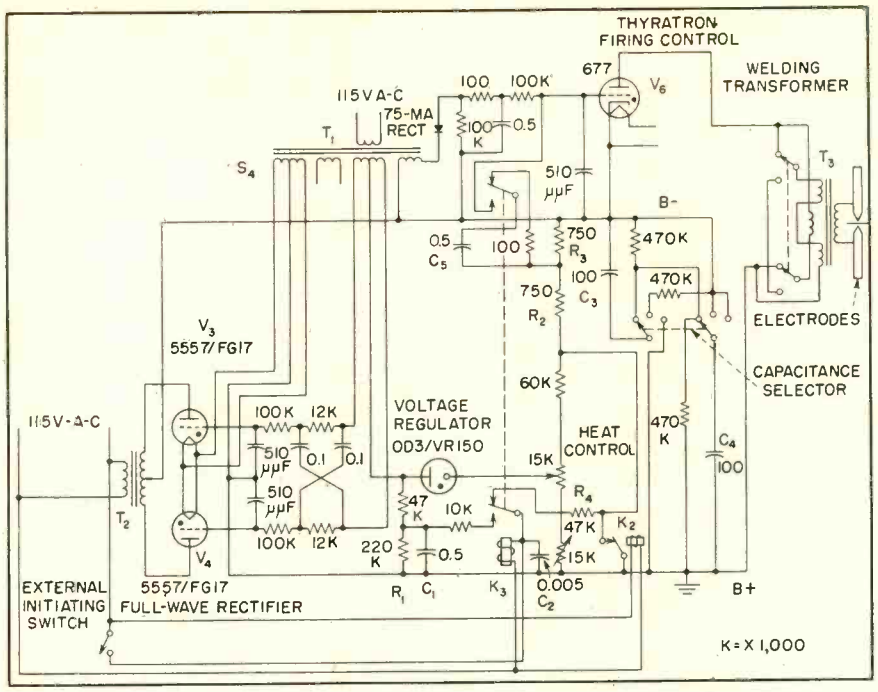


FIG. 1—Heat control and capacitance selector determine energy supplied to welding transformer by capacitor bank

HANDLES METAL FOILS

how long the operator takes to load in a new part.

The voltage to which the capacitor bank is charged depends on the setting of heat control R_4. This voltage is applied to the output circuit by closing the external initiating switch to pull in firing relay K_3.

Welding Cycle

When the firing relay is energized, a negative charge is transferred from C_2 to C_1 so as to make rectifiers V_3 and V_4 nonconductive during the welding period. Relay K_3 also connects capacitor C_5 to the grid of thyratron V_6, driving this grid positive and firing the thyratron for the time required to discharge capacitor bank C_3-C_4 through the primary of the welding transformer. At the end of the welding cycle, relay K_3 is open so that C_1-R_1 cause the rectifiers to become conductive once again and recharge the capacitor bank for the next weld.

The capacitance selector switch gives a choice of 50, 100 and 200 μf for positions 1, 2 and 3 respectively, with 470K across each 100-μf unit for the series connection in position 1. If the capacitance selector switch is set for 100 μf, twice as much energy is applied as in using 50 μf and the heating effect is doubled.

The voltage level at which energy is stored is governed by the heat control, which provides a range of 650 to 1,500 volts.

Primary windings in the welding transformer may be connected in series or parallel by means of a series-parallel switch to give different output voltages.

Weld Pressure

Welding pressures ranging from ½ to 18 psi are obtained by adjusting a metal bellows unit which supports the floating lower electrode. The design of this unit is such that, when the upper electrode is depressed or lowered by pressure applied to a foot pedal, it halts the downward electrode movement and actuates a snap-action switch. This initiates the welding cycle when the parts to be welded are under a predetermined amount of pressure. Where the parts comprise extremely thin sheet or foil materials, this may amount to less than 1 psi.

Applications

Materials that have been welded with the welder include nickel to molybdenum, copper and tantalum-tungsten; brass to brass, bare or tinned copper, platinum, iridium, palladium and phosphor bronze; copper (bare, tinned or plated) to copper, phosphor bronze and bare or plated steel; Kovar to Kovar, carbonized steel, tungsten-platinum, nickel, molybdenum and Dumet; as well as many other materials.

Fusion temperatures and energy requirements were selected on the basis of the same considerations that would apply to the use of any resistance welder with only one exception. Due to the high peak current discharged in a very short time, the spotwelder develops heat so quickly that little energy is dissipated in the metals being welded. Besides keeping the weld area small, this feature avoids the use of power that would normally cause burning.

Reference Generator

By M. I. JACOB

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SUMMARY — Applicable to scatter propagation, equipment uses stable frequency generator employing phase-locked oscillators to provide accurate reference frequencies for ssb generator. Beam-switching tube used in frequency-dividing circuits permits coverage of 2 to 30-mc range in 1-kc steps

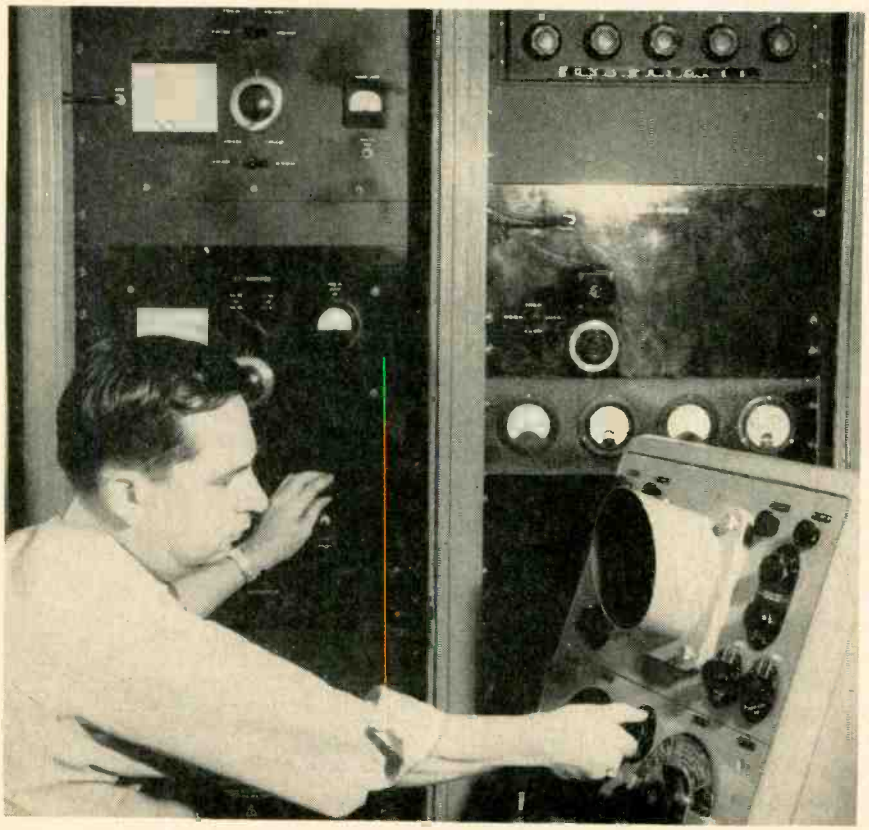
PROPER OPERATION of single sideband system depends upon the ability of the associated transmitters and receivers to be accurately adjusted to assigned frequency channels and upon their ability to remain on these assigned frequencies after initial adjustment. As a result the excitation frequencies of transmitters and the local oscillator frequencies of receivers are frequently derived from a single highly accurate and stable source. The stable frequency generator and ssb generator to be described are designed to fill these requirements.

Generator

Operating from a 5-mc internal or external source, the frequency generator derives frequencies suitable for exciters or receivers operating in the h-f (2 to 30 mc) band. A unique system of phase locking free running oscillators to the stable reference frequency provides, in practically continuous 1-kc steps, spurious-free (80-db attenuation) injection frequencies.

The block diagram of Fig. 1 shows the output frequencies of the stable frequency generator as produced by stabilized oscillators. The stabilizer reference frequencies are produced by synthesis from the single 5-mc source. These synthesized frequencies are not radiated but are used only as stabilizer references.

Since the output frequencies are phase locked to the 5-mc standard,



Intermodulation distortion tests are made on ssb exciter containing stable frequency generator

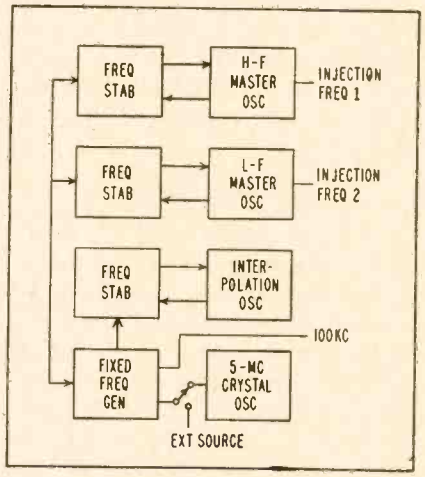


FIG. 1—Stable frequency generator uses either a 5-mc internal source or an external source

for SSB SYSTEMS

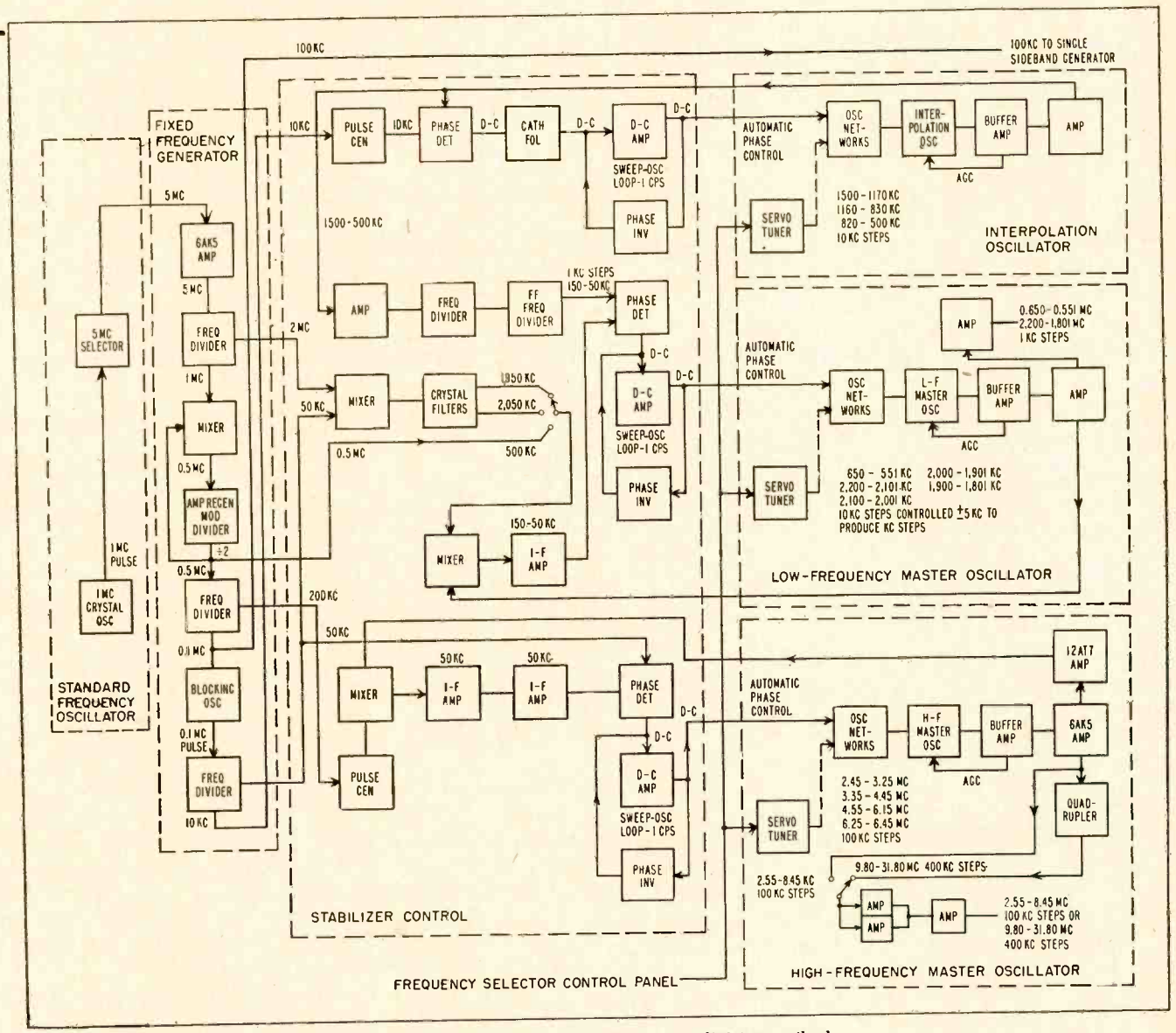


FIG. 2—Detailed block diagram of stable frequency generator shows frequency division method

the accuracy and stability of these frequencies is the same as the standard. Standards having a performance capability of holding 1 part in 10^8 over 24 hours under military conditions are available today.

To promote maximum reliability, the design uses a minimum number of tubes consistent with the high performance requirements. Thirty-four tubes of eight types are employed.

Tuning controls on the stable frequency generator consist of a group of ten-position switches each controlling a dial reading one digit of the desired operating frequency. Since the ssb generator or ssb receiver with which this unit works covers the 2-to-30-mc bank in 1-kc steps, five controls are required. These controls operate switches that provide signals to a servo positioning system that physically tunes the unit's free running oscillators.

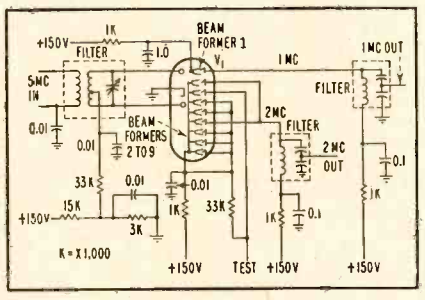


FIG. 3—Beam switching tube frequency divider

This servo is a 60-cps device that provides a frequency setting accuracy of a 0.03 percent, which is well within the pull-in range of the stabilizer circuits.

In Fig. 2, a detailed block diagram shows how injection frequencies are generated with relation to the basic 5-mc standard.

The circuitry employed in the stable frequency generator falls

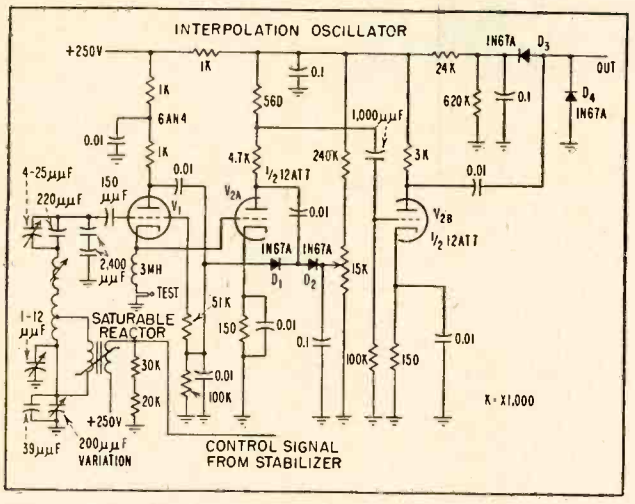


FIG. 4—Saturable reactor is used to stabilize vfo

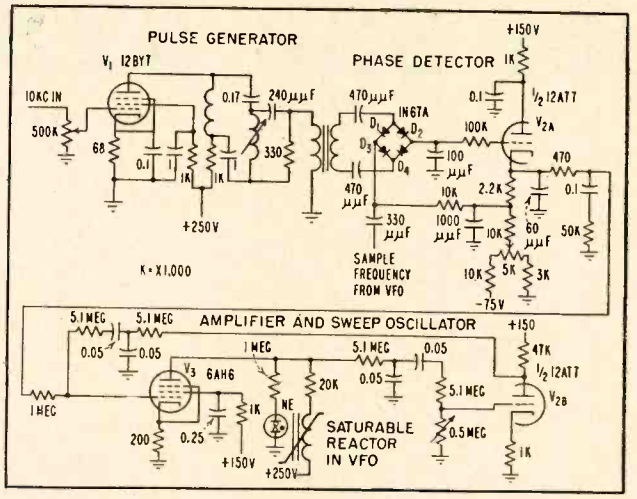


FIG. 5—Frequency stabilizer provides signal for saturable reactor

into four major functional catefories, the reference oscillator, the frequency dividers, the stabilized oscillators and the stabilizers.

The reference oscillator can be one of a number of available types, the selection being dependent on the accuracy and stability required. The particular unit utilized is a Sulzer type[1], 1-megacycle standard oscillator with a frequency stability better than 1 part in 10^9 per 24 hours after six months of continuous operation. The unit is variable over the range of approximately on cycle and is capable of being reset to 5 parts in 10^{10}.

Frequency Dividers

An example of the application of a multielement tube is illustrated in Fig. 3. The tube employs a magnetically focused electron beam that can fall on any one of a total of ten plates in the tube. This state is stable and once it is formed will remain.

However, the beam can be advanced from plate to plate by excitation applied to the control grids of the tube. Thus by application of a signal on the grid to advance the beam and by making connection to one of the plates, it is possible to obtain one pulse for every ten applied to the grid.

As arranged in the circuit of Fig. 3 the input steps are applied in push-pull and therefore are effective at twice the driving frequency and the overall division ratio of the circuit is 5 rather than 10. By tying two of the plates together, pulses can be obtained at twice the revolution rate, which is equivalent to dividing by 2.5.

For frequency generator applications where a number of fixed frequencies are required, providing more than one division ratio simultaneously with one tube is useful.

Oscillator

All frequencies delivered from the stable frequency generator originate in three variable frequency oscillators. Because these oscillators are referenced back to the master standard through stabilizer units, they are not required in themselves to maintain minute frequency tolerances.

Figure 4 illustrates the type circuitry involved in these oscillators. The oscillator covers the range from 500 to 1,500 kc and is tuned in 10-kc steps. The output is later divided by 10 to furnish 50 to 150-kc frequencies in 1-kc intervals to interpolate between the coarser steps of the next oscillator.

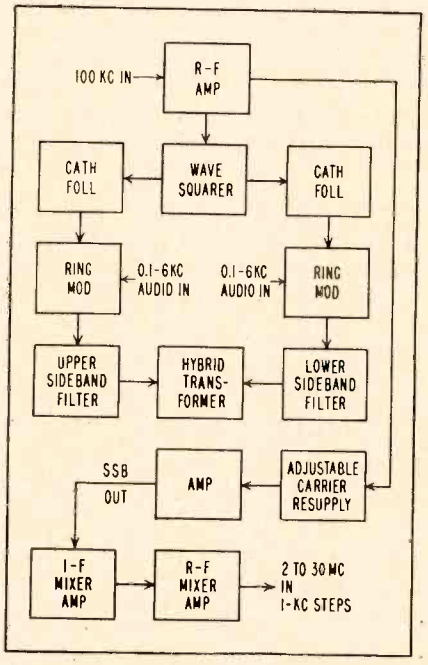


FIG. 6—Block diagram of ssb generator which uses stable reference frequencies

Stabilizing

A variable reactance in the form of a saturable ferrite reactor is included to apply automatic frequency control to the oscillator. The control current for this reactor is produced by the stabilizer unit and is related to the frequency of the standard reference associated with the frequency generating portion of the circuit. Automatic gain control is provided by tube V_2 and related components.

Action of the agc circuit is to produce, by the voltage doubling and rectifying action of diodes D_1 and D_2, a d-c voltage proportional to the amplitude of the oscillations emanating from the tank circuit of V_1. This d-c is then used as bias to maintain a fixed amplitude output from V_1. The oscillation amplitude is set by an adjustable positive bias on diode D_2. The addition of the 0.01-μf capacitor from the plate of V_1 back to the agc control line provides stability for the agc circuit which necessarily has a high loop gain.

This feedback circuit operates by sampling the signal developed across the 1,000-ohm resistor in the plate of V_1. The rate of change of this signal is out of phase with the rate of change of oscillations on the

grid of V_1, resulting in negative rate feedback being applied to the agc line. This is found to be effective in stabilizing the agc circuit. Circuitry associated with V_2 provides conventional amplification and limiting to the gain stabilized oscillator output.

Phase Locking

The absolute frequency output of the three oscillators is determined by the standard reference frequency and is a function of the phase-locking stabilizer servo system. Control signals from the error detecting circuits of the stabilizer are fed back to variable reactance elements tapped across the frequency determining networks of each vfo. The stabilizer circuit controlling the frequency of the 500-to-1,500-kc oscillator is shown schematically in Fig. 5.

The circuit is in three functional sections; a pulse generator, a phase detector and an amplifier and sweep oscillator. Essentially the 10-kc reference signal is converted into a pulse suitable to produce harmonics up to 1,500 kc.

The pulses are generated by passing the circulating current of a tuned circuit in the plate of V_1 through a small saturable reactor. Pulses then appear at each of the current zeros. These pulses are fed into a balanced phase detector and compared with a sample of the vfo output. A d-c error signal is generated and fed through this amplifier to the reactance controlling device in the vfo.

Associated with the amplifier is a sweep oscillator whose purpose is to provide a sweeping control voltage to pull the vfo within the lock-in range of the servo loop. This sweep system will automatically start sweeping when the servo loses control. This happens because the time constant of the frequency-correcting servo loop is much faster when in lock than that of the sweep circuit.

Thus when the sweep circuit tries to oscillate and change the vfo frequency, the servo overrides the error and prevents oscillation. If the servo loop gets out of lock, the sweep oscillator is free to oscillate at its one-cycle rate and will sweep the controlled vfo over a range compatible with the phase detector output.

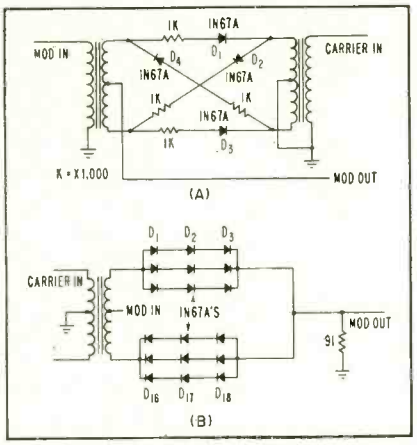


FIG. 7—Balanced ring modulator (A) is used for low-frequency conversions, while unbalanced modulator (B) converts high-frequencies

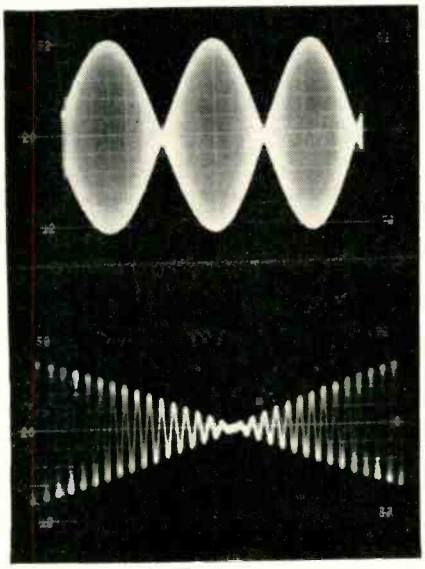


FIG. 8—Conventional two-tone waveforms appearing at first modulator output

When supplied with proper injection frequencies, the single sideband generator provides a source of ssb emission in the h-f 2- to 30-mc band. The unit accepts two separate 6-kc wide modulation signals and converts them to independent sideband signals around a common suppressed carrier. Crystal filters remove unwanted carrier and sidebands after conversion.

The unwanted sideband is attenuated 70 db and out-of-band spurious is rejected 80 db. The carrier is emitted with the minimum level 50 db below the desired sideband level. Intermodulation products are 60 db below the level of one tone on a two-tone test. Operation of the ssb generator is shown in the block diagram of Fig. 6.

Two independent channels of audio each approximately 6-kc wide can be fed simultaneously to the ssb generator. These signals are introduced into balanced modulators where they are heterodyned to 100 kc. Since these are balanced modulators their outputs consist of two sidebands, each containing both channels of audio, with the 100-kc carrier suppressed 35 db. These signals are now fed to crystal-lattice filters at which point the carrier is attenuated an additional 15 db and one sideband is removed.

The independent upper and lower sideband signals are then combined in a hybrid transformer and fed to a series of converter stages where they are heterodyned to the final output frequency. Spurious products generated in the mixing stages are attentuated more than 80 db below the desired signals by the i-f and r-f networks.

Mixers

Crystal diodes were employed as mixing elements in the modulators. In the lower frequency conversions, 100 kc and 2 mc, balanced modulators of the type shown in Fig. 7A were utilized. In the final conversion (2 to 30 mc) it was more practical to use the circuit of Fig. 7B. This circuit requires only one balanced transformer, which is an advantage when such a wide frequency range must be covered.

The series-parallel arrangement of a number of diodes was necessary to keep the power dissipation per diode below rated levels. This combination of modulator circuits produced single sideband signals with intermodulation products — 60 db below the level of the test tones on a standard two-tone test. The classical two-tone test wave forms appearing at the output of the first modulator are shown in Fig. 8. The frequencies involved were 2,200 cps and 600 cps with a 100-kc carrier. The expanded view (approximately 4 to 1 expansion) at the bottom shows in detail the form of the wave at the null or crossover point.

REFERENCE

(1) P. G. Sulzer, High Stability Bridge Balancing Oscillator, *Proc IRE*, 43, p 701, June 1955.

Pickup coils at front wheels guide feeding carts along rows of coops following buried wire layout

Transistorized Guidance

SUMMARY —— Semiautomatic equipment for large chicken farm uses carts following buried wire for distributing feed and collecting eggs along rows of coops. Transistor amplifiers feed position data to steering motors from magnetic pickup coils at front of cart. A third amplifier automatically stops cart if it goes off path

STEERING of a small, slowly moving cart over a desired path is achieved by the method to be described.

The path is marked out by a buried wire carrying approximately one ampere of 60-cps alternating current. The guidance unit senses the position of the cart relative to the wire by the magnetic field surrounding the wire. If the cart is off course, an error signal is sent to the power steering unit to bring about the necessary correction.

Use of transistors allows operation directly from the 12-v storage battery which supplies motive power for the vehicle, and also eliminates the maintenance problems associated with vibrator type high-voltage supplies. Transistors also allow the unit to give reliable operation in spite of the vibration experienced on the moving cart.

The advantages of this type of guidance over a rail system are obvious. The path is simple and inexpensive to lay out or change. Also, switching can be done electrically from a fixed point by energizing the proper branch at a junction.

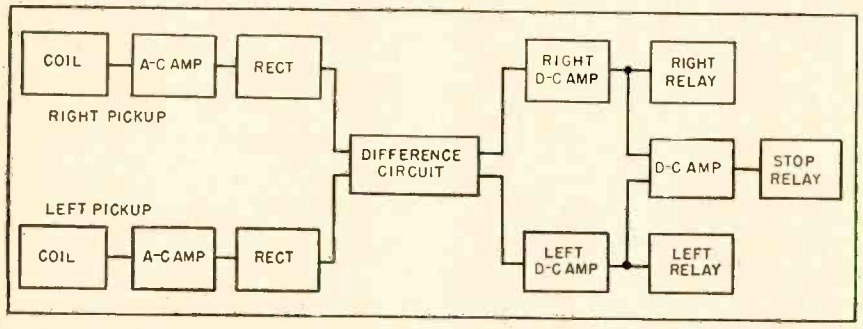


FIG. 1—Block arrangement of circuits used in cart control system

Basic Operation

Two small pickup coils are suspended about six inches over the ground in front of the vehicle, and are placed about one foot apart. As shown in the photograph of the

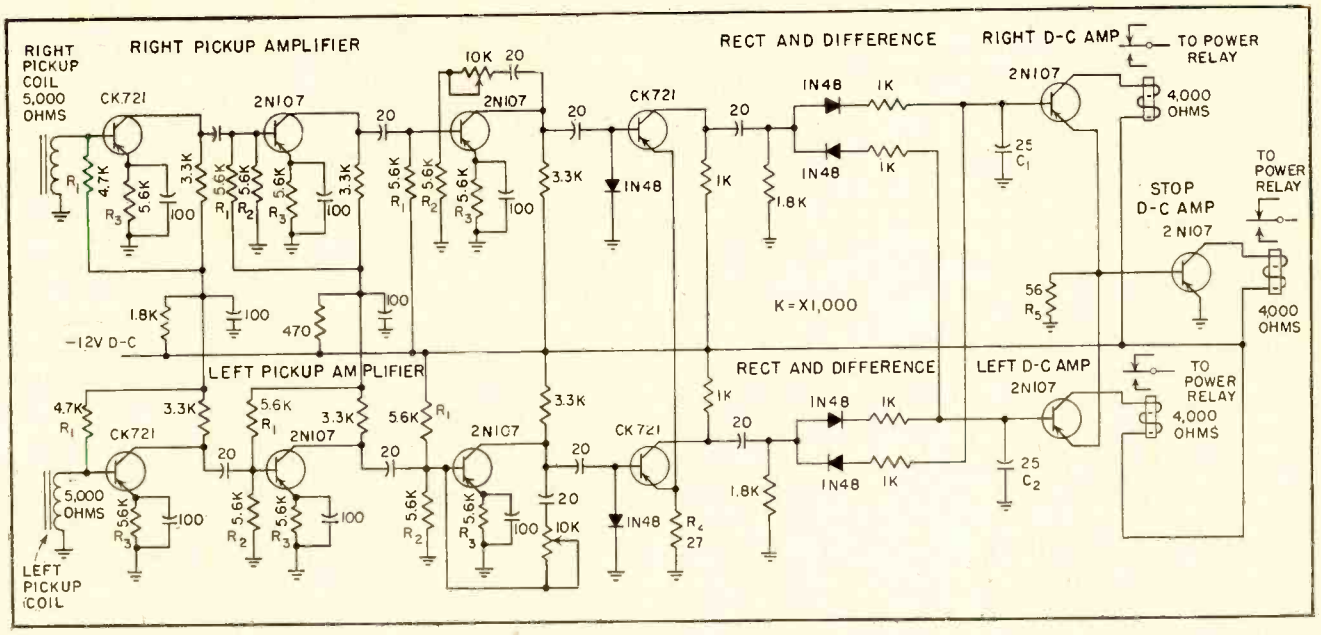
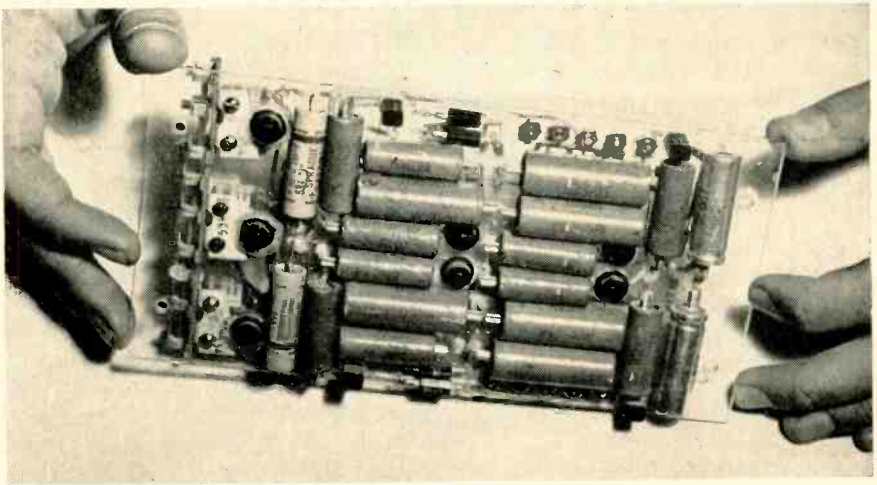


FIG. 2—Four-stage transistor amplifiers boost signals picked up by coils to control steering motors for cart

System Feeds Chickens

By SHELDON KNIGHT
K & R Development Co.
Hughson, California



All control circuit components including relays are mounted on polystyrene board

cart, the two coils are mechanically connected to the front wheels in such a way that they move from side to side as the wheels turn with steering. When the vehicle is on course, the buried wire is midway between the two coils, and so the voltages induced in the coils by the magnetic field surrounding the wire will be equal. If the vehicle drifts off course, one coil will move slightly closer to the wire, producing a difference in the induced voltages.

Each coil feeds a four-stage transistor a-c amplifier as shown in block form in Fig. 1. The output of each amplifier is rectified and the two d-c signals combined to produce a difference output to the d-c amplifiers. The magnitudes of the outputs are proportional to the difference between the rectified outputs of amplifiers. But the polarities are opposite.

As the vehicle moves off course to the left, the rectified output from right-pickup amplifier increases and the output from the left-pickup amplifier decreases, causing a negative d-c voltage to be developed in the right side final output and a positive d-c voltage to be developed in the left channel.

When the vehicle is on course the output of both amplifiers will be equal and the final outputs will be zero.

Each final output drives a single stage d-c amplifier which controls a sensitive relay. The transistors in these d-c amplifiers are connected in the grounded-emitter configuration, and collector current is low in the absence of an input signal to the base. When the base is driven negative the collector current increases and closes the relay.

The relays actuate power-control relays which operate the electric

steering motor to make the proper correction.

Since the pickup coils are moved laterally as the front wheels turn, they will be in a position of balance over the buried wire after the wheels have turned a few degrees towards the course. Thus, the steering motor will be stopped leaving a small correction to intercept the course.

As the vehicle approaches the course again, the coils which are turned with the wheels, give an error indication in the opposite direction. This starts the steering motor to straighten the wheels, moving the coils back to their normal position, restoring balance and completing the correction cycle.

This is far from the ideal error-actuated servo system. However, it has the advantage of simplicity since no error-time derivative signal is required and since the follow up is purely mechanical. At the one to two miles per hour speed at which this cart operates, the system has proved entirely satisfactory.

A third d-c amplifier and relay is connected with the steering control d-c amplifiers in such a way that if the collector current of either steering amplifier exceeds a preset amount it will close and, through a power control relay, cut off the main motive power to the vehicle. This is a safety measure which will automatically stop the cart should it get more than a maximum distance off course due to some malfunction of the guidance system.

Electronic Details

The complete diagram of the electronic unit is shown in Fig. 2. The four-stage a-c amplifiers use conventional grounded-emitter configurations. A high degree of temperature stability in each stage is provided by stabilizing networks R_1 and R_2 together with emitter resistors R_3.

A slight increase in stability is provided by the method of obtaining gain control. A potentiometer does this by providing variable negative-current feedback around the third stage.

There is a considerable excess of gain provided by the four stages, so during normal operation considerable negative feedback is used. Extending the feedback loop to include more stages is not practical because of low-frequency stability problems which arise from the coupling and decoupling capacitors and the low impedances associated with the transistors.

Because the desired final output is the difference between the two amplifier outputs, and also because there is some loss in the difference circuit, the fourth stage must operate at a fairly high power level. To avoid excessive dissipation in this stage, the bias current is developed by rectifying the signal feeding the stage with the diode in the base input circuit. This maintains the bias and hence the collector current at the lowest possible level consistent with the signal level.

At first glance it would appear that the low forward resistance of the base-emitter section of the fourth-stage transistor would serve this purpose; however this proved to be too high to allow adequate charging of the input capacitor and so the diode was added. This variable bias circuit also eliminates the need for the temperature stabilizing resistors used in the first three stages.

A small amount of cross coupling is provided between channels by the common-emitter resistor R_4 in the fourth stage of the two amplifiers. The input coils are connected to the amplifiers so that the amplifiers are excited in phase. Thus the signal developed across R_4 due to either amplifier is of such polarity as to reduce the output of the other amplifier. If the output of either amplifier increases, the output of the other amplifier will decrease even if the input to the other amplifier has not changed. This cross coupling feature further increases the differential in the amplifier outputs. The rectifier and difference circuit is a conventional diode system.

The emitters of both d-c amplifiers are grounded through the common resistor R_5. These emitters are also connected to the base of the stop d-c amplifier. Thus a part of the emitter current of either d-c amplifier must flow through the base input circuit of the stop amplifier. If this base current exceeds a certain maximum, the collector current of the stop amplifier will increase sufficiently to close the relay.

Possible Modifications

This unit was designed and built for one specific application. In this capacity it worked well, so no further development effort has been expended on it. However, usage has pointed out some possible improvements that could be incorporated in subsequent designs.

Bias stabilizing networks, R_1 and R_2, produce more stability than is really necessary, and so introduce an unnecessary loss of gain. These resistors could possibly be increased to as high as 27,000 ohms, depending upon the range of temperature variation expected, and the resulting increase in gain would allow the unit to operate satisfactorily with only three instead of four stages of a-c amplification.

There is a slight lag in the response of the unit due to the time required for charging capacitors C_1 and C_2. This lag places a low limit, in the neighborhood of three miles per hour, on the forward speed of the vehicle. With 60-cps current in the buried wire, the capacitance cannot be reduced below 25 μf and still maintain adequate filtering. For higher forward speeds the wire should be fed from a higher frequency source so that the capacitor values and the resulting lag could be reduced proportionately.

The unit was built on a 4 by 8 inch sheet of $\frac{1}{4}$-inch polystyrene. Holes were drilled in the sheet to allow wire leads to the various components to pass through from the component side of the board to the wiring side.

Components were temporarily mounted with plastic cement. The wiring itself serves to permanently mount the components. This type of construction provides a compact unit in which all parts and wiring are readily available for rapid servicing.

The unit was mounted in a small aluminum box for protection. Gain controls are mounted on the aluminum box, and so do not show in the photograph.

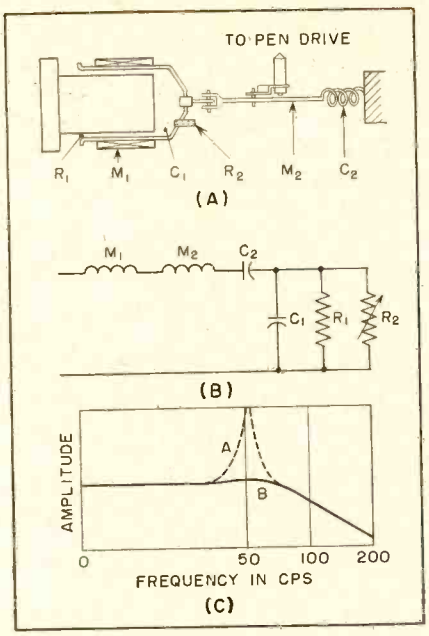
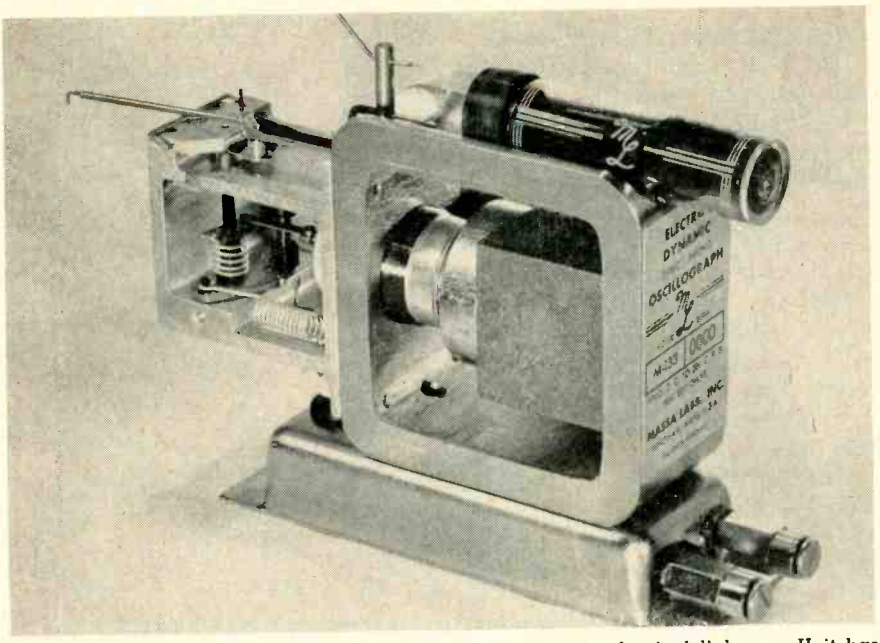


FIG. 1—Schematic of pen motor vibrating system (A), its equivalent circuit (B) and response with and without damping (C)



Dust shields have been removed from pen motor to show mechanical linkage. Unit has application in measuring time intervals among several related events such as receiving ground echoes at various pickup stations used in geophysical exploration

PEN MOTOR For Rectilinear Recording

By FRANK MASSA and ERNEST A. MASSA

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SUMMARY —— High-speed rectilinear recordings are now possible with pen motor having a frequency response from d-c to 60 cps and gradual decrease in sensitivity to 200 cps. Unit is independent of amplifier compensation and can be fed from any impedance. Coaxial body prevents whipping at high frequencies and mechanical filter permits splatter-free writing to 200 cps

DIRECT-WRITING high-speed pen recorders have become popular in spite of several apparently inherent limitations in performance of available instruments. Some of these limitations, as reported, may include ink spattering at high writing speeds, curvilinear distortion of the pen tip, pen-whipping at high frequencies, lack of rectilinear motion and inherent resonance of the pen-motor system resulting in poor transient response. The direct-inking recorder to be described overcomes many of these limitations.

Drive System

The basic drive system for the pen motor consists of an electrodynamic transducer comprising a cylindrical current coil freely supported in an annular magnetic air gap. The coil winding not only occupies the complete air-gap volume, but also projects axially on either side of the air gap by an amount equal to the peak excursion of the coil at full-scale amplitude of operation. This design insures a constant force factor for various positions of the coil and eliminates the nonlinear distortion present with a coil placed entirely within the mechanical air gap.

Since the entire air-gap flux is used, a relatively small magnet is needed as compared to the larger magnets required in conventional

d'Arsonval structures available.

The pen motor is normally protected by dust shields. A disposable hermetically-sealed ink cartridge is easily inserted into the hypodermic ink feed and vent assembly.

Acoustic Damping

The current-carrying coil is wound on an accurately dimensioned cylindrical form which is assembled to glide smoothly over Teflon ribs held rigidly in longitudinal slots on the surface of the pole piece.

The left-hand end of the coil form is closed and the physical spacing between the periphery of the pole piece and the inner surface of the form is adjusted so the viscosity of the resulting air film critically damps the resonance of the vibrating mechanical system.

As a result of this critical air damping the pen motor has a flat frequency response characteristic, making the instrument independent of special compensating amplifiers or source impedances.

Figure 1 illustrates the effect of the various parameters in the design of the acoustic damping for the vibrating system. In the equivalent circuit of the mechanical system, the mass M_1 of the current coil is represented by the inductance M_1. A second inductance M_2 represents the effective mass M_2 of the linkage and pen assembly and appears in series with M_1. A series electrical capacitance C_2 represents the compliance of the control spring C_2 and, in combination with M_1 and M_2 determines the resonant frequency of the pen-motor assembly.

A trapped volume of air, C_1 corresponds to capacitance C_1 in the equivalent circuit. The thin film of air in the annular clearance space between coil form and pole tip introduces mechanical resistance owing to its viscosity and appears as resistance element R_1 in the equivalent circuit.

A tiny capillary tube of adjustable length is shown attached to the closed end of the coil form to establish communication between the trapped volume of air C_1 and the atmosphere. The viscosity of this air film is proportional to the length of the tube and therefore the resistance R_2 is shown as a variable resistance in the equivalent circuit.

In the conventional instrument the current coil is open and therefore capacitance C_1 is infinite. This results in a short-circuit of resistance element R_1. Under this condition a highly-peaked resonant system results as represented by curve A in Fig. 1C.

In the pen motor, the trapped volume of air C_1 is dimensioned so the impedance of equivalent capacitance C_1 does not shunt resistance element R_1 in the frequency range of operation. By adjusting the dimension of the film of air R_1 and tailoring the length of the capillary tubing R_2 it is possible to critically damp the resonance of the pen-motor assembly to result in the flat frequency response characteristic indicated by curve B in Fig. 1C.

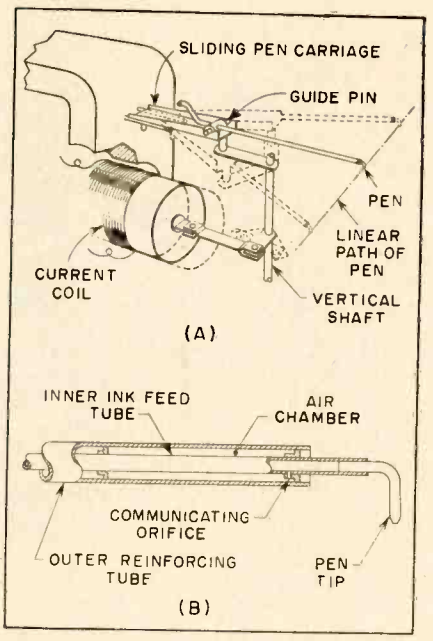


FIG. 2—Pictorial view of mechanical linkage (A) and pen construction (B). Drive coil moves in and out horizontally like loudspeaker voice coil, to move pen through linkage

Rectilinear Motion

Figure 2A shows the linkage system interposed between the closed end of the coil form and the pen carriage. Forces generated when an electric current passes through the coil are imparted to the offset portion of the vertical shaft assembly. The shaft is mounted in jewel bearings and rotates against the stiffness of a calibrated spring around the lower portion of the shaft. This spring establishes the frequency range and sensitivity of the instrument.

The top end of the vertical shaft projects through the top wall surface of the linkage housing and oscillates an offset arm coupled through the lower left-end surface of the pen carriage. The left end of the pen carriage terminates in a vertical guide pin held between parallel, hardened guide surfaces to permit free axial carriage displacement. The linkage system and pen-carriage dimensions are adjusted so as the current coil deflects, the pen carriage moves forward in progressively greater amounts such that the pen tip describes a true straight line instead of a curve.

Pen Zero-Adjustment

A mechanical pen-biasing adjustment is located behind the pen carriage assembly. Zero adjustment is achieved by anchoring the main control spring to a gear-sector plate engaged to a small pinion. The pinion is rotated by a slotted shaft

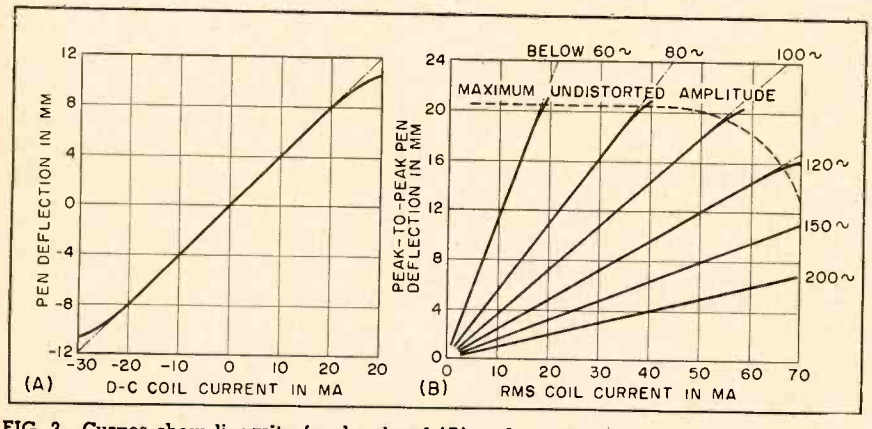


FIG. 3—Curves show linearity for d-c signal (A) and a-c signal (B)

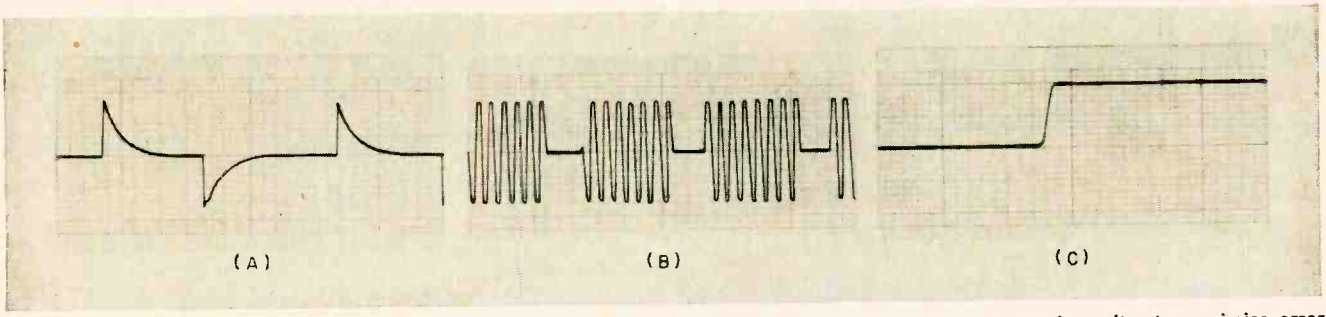


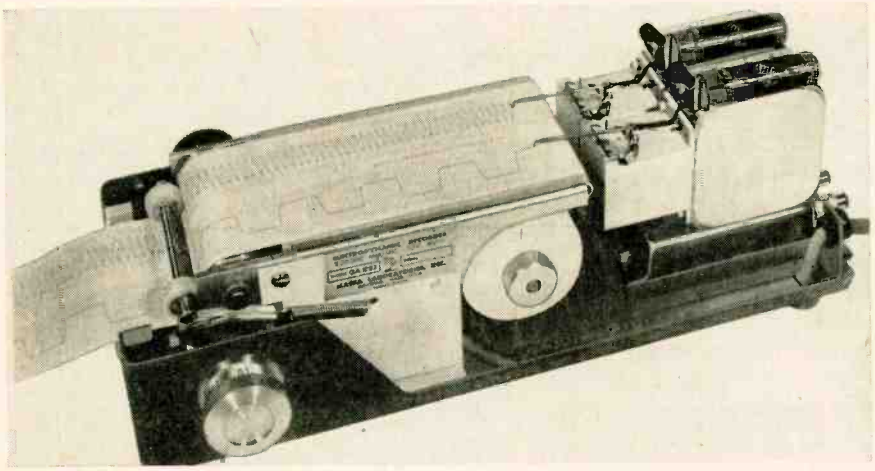
FIG. 4—Recordings show return to zero after application of step function and gradual current reduction thereafter to maximize error (A), return to zero after successive bursts of sinusoidal a-c excitation (B) and step function at high speed (C)

which projects through the top of the linkage housing.

This adjustment permits accurate alignment of the pen tip along the chart center line. The tip may be set to either chart extremity to obtain twice the normal recording amplitude for unidirectional pulses.

A second micrometer set screw adjustment in the pen-motor base permits exact axial positioning of the complete motor unit relative to the base. This set screw is located between the electrical terminals on the base.

The complete assembly weighs 1½ lbs and mounts 1¼ in. on centers in multiple-channel installations.



Ink reservoir cylinder is on top of magnetic frame for drive coil system

Whipping and Ink Splatter

One of the generally unrecognized sources of distortion results from pen whipping. Flexibility can cause bending at high frequencies, resulting in errors in the position of the pen tip. At full high-frequency amplitudes, forces of 1,000 g act on the pen to cause whipping. It was found necessary to increase the stiffness of the pen body to eliminate small amounts of pen whipping which would introduce an instantly visible curvilinear distortion into the rectangular recording.

Increased ink flow resulting from large centrifugal forces developed at high frequencies may cause the writing fluid to splash violently from side to side beyond the limits of the chart. A cross-sectional view of the pen assembly in Fig. 2B, shows the design used to prevent splatter at frequencies up to 200 cps. The inner ink feed tube is surrounded by an outer reinforcing tube which is rigidly secured through annular spacing disks to the inner tube. Thus, the stiffness of the pen assembly is increased with a minimum increase in weight. The concentric air chamber between the two tubes and the two spacers forms the compliance element of a mechanical filter which is coupled by a communicating orifice to the inner tube which carries the ink.

Pressure changes created near the pen tip neutralize the pulsating forces which would otherwise cause high-frequency ink splattering in the absence of the filter, thereby producing continuous unbroken ink lines at all writing speeds up to 200 cps.

The graphs in Fig. 3A and 3B show the relationship between pen deflection and coil current for both d-c and a-c inputs. The linearity is near perfect up to 80 percent of full-scale deflection from d-c to 100 cps and the amplitude at full-scale deflection of ± 10 mm falls off less than about 4 percent below the straight-line value.

A common type of error encountered in direct-ink-writing oscillographs results from the inability of the pen tip to return to the same zero point on the chart every time a signal is removed. A d-c pulse was slowly discharged through a capacitor from opposite polarities to produce the recording shown in Fig. 4A. The maximum hysteresis error was actually less than ± ¼ mm under these most disadvantageous conditions, which amounts to an error of less than ± 3 per-

For a-c signals the hysteresis effects are still lower, as seen from the return to zero of the pen tip in Fig. 4B after successive bursts of sinusoidal excitation.

Response

Rise time is defined as the time required for a step function to rise to approximately ⅔ of its full-scale value after the instant of application. The strip chart reproduced in Fig. 4C shows a step function made at a chart speed of 200 mm per sec. Since each horizontal 2-mm division on the paper represents 10 milliseconds in time, the rise time of the pen motor is about 5 milliseconds.

SENSORY AID DEFINES

SUMMARY — Miniature device using cadmium sulfide photocell, diode and two transistors to actuate a magnetic earphone gives audible indication of printing, meter readings or location of maximum ambient light. Unit, including accessory lamp bulb, is powered by 1.5-volt battery

AN ELECTRONIC device that provides an audible signal with frequency proportional to the intensity of a received light signal is a useful tool for the blind. Such a device has been described[1] by the late Dr. C. E. Witcher of this laboratory. The original device employed a neon-bulb relaxation oscillator and therefore required a 90-volt battery supply.

This supply was physically large and resulted in fairly expensive ($2.50 to $3.00) replacement cost. To eliminate these two disadvantages the optical probe has recently been transistorized and redesigned mechanically. The complete unit including the small pen-light bulb now operates on a single 1.5-volt cell.

Light Sources

The probe provides an audible signal whose frequency is proportional to the intensity of the received light. The received light may originate from ambient sources external to the device or from a tungsten bulb that may be attached to the device.

A photograph shows the disassembled unit, together with a meter-reading attachment. The 4.5-inch cylindrical tube contains an optical lens, an electronic package, a battery and a switch in the screw cap. The V-shaped attachment is secured to the tube by a twist-lock feature and contains a small prefocused penlight bulb. The bulb is contained in a holder that can be secured to either of two attachments by another twist-lock. Overall length of the device is approximately 5.5 inches.

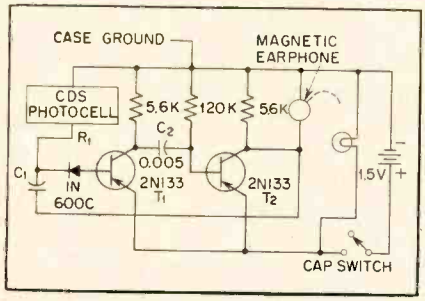
The lens has a diameter of 0.5 inch and a focal length of 0.5 inch. It is mounted in a movable tube. A milled slot shown at the left end of the barrel provides two prefixed focal distances for the lens. Focus at infinity is used with ambient light sources and a focus at 1 inch is for use with attachments.

The circuit is a two-stage, capacitance-coupled, free-running multivibrator. The transistors are low-noise *pnp* junction types. The frequency of oscillation is controlled by the time constant

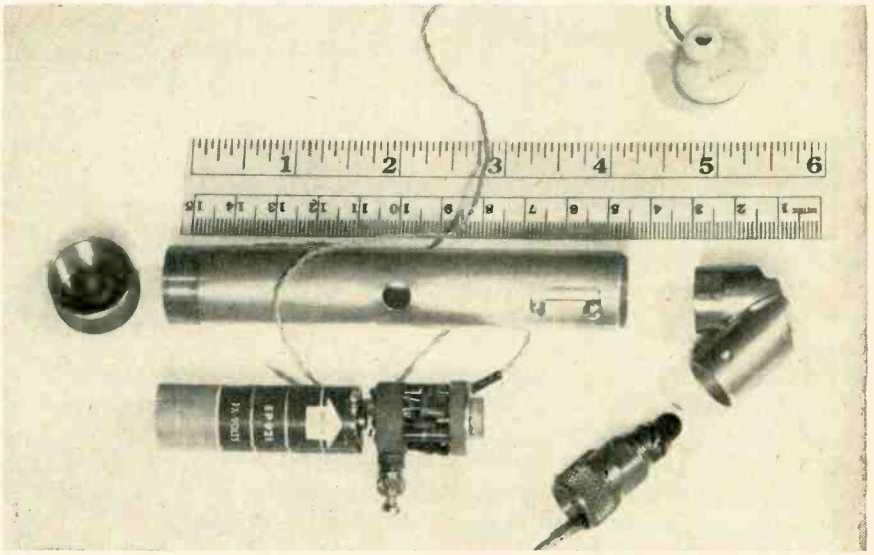
$$T = C_1 \frac{R_1 R_d}{R_1 + R_d}$$

where C_1 is the value of capacitance of the coupling capacitor, R_1 is the equivalent resistance of the photocell and R_d is the sum of the diode and transistor resistances under reverse bias conditions.

Since the effective resistance of the photocell is approximately an inverse function of the intensity of the received light, the frequency will be related linearly to the received light intensity. The silicon diode is employed to make the value of R_d large compared with R_1 in low levels of light intensity. Since the dark resistance of the photocell may easily exceed 10^8 ohms, whereas the input resistance of the transistor with reverse bias applied may be as



Circuit of the transistorized sensory aid is essentially a multivibrator



Elements of the audible reader show lamp (lower right) transistor-photocell-diode assembly (center) battery and case. Hearing-aid type earphone upper right

LIGHTS AND MARKS

By C. R. HURTIG

Research Laboratory of Electronics
Massachusetts Institute of Technology
Cambridge, Mass.

To read a meter the plastic card with embossed indices is placed over the glass face of the meter and the location of the pointer found and related to the raised marks. Any meter can be used without alteration

high as 10^6 ohms, the diode is necessary to extend the frequency range of operation.

Under normal conditions, the waveform of the multivibrator is highly asymmetrical. If the probe is employed in direct sunlight, the photocell resistance becomes very low and the mode of operation becomes more symmetrical, with a final limit of sinusoidal operation. The transistors are not bias-stabilized; however, no difficulty with thermal instability was noted.

Frequency Range

The frequency variation is from a few pulses per second to several thousand pulses per second. At low light levels the nonlinear characteristics of the photocell and diode cause the loop gain to fall below unity; hence the oscillation fails. If operation at low light-intensity is necessary, sustained oscillation can be maintained by the use of a supply voltage of 3 volts or greater.

Current drawn by the transistor circuit varies from 650 to 550 μa as a function of light intensity. Thus, the operating life of the battery is a few hundred hours with the bulb disconnected.

With the bulb connected, the battery life is a few hours, since the bulb current is approximately 200 ma. If the attachments requiring bulb operations are to be used continuously, it is advantageous to employ an external 1.5-volt d-c supply operated from a convenient line source.

The probe is shown in the photograph as it is normally used to read the deflection of a meter needle. A transparent plastic overlay with a series of raised markings is placed on the glass surface. The probe is moved over this overlay until the large change in frequency, indicating the location of the meter needle, is observed. The center of the probe is then measured tactually with respect to the raised markings. The probe is designed to focus at a depth below the overlay of approximately 0.19 inch, which corresponds to the vertical locations of the needle.

The printed numbers and markings on the meter scale cause background noise but the change in frequency caused by these sources is small compared with the change caused by the needle. For some meters—those having a needle width that is small compared with its depth—the location of the needle and the shadow of the needle created by the angular incidence of the light from the bulb are difficult to distinguish. With the present arrangement the location of the needle can be detected within an accuracy of a few percent.

Two other attachments are provided. One is used for detecting the presence of printed matter on paper, second for tracing patterns from ambient sources such as an oscilloscope or detecting the presence of sun-lighted windows.

The work described was supported in part by U. S. Army, U. S. Air Force and U. S. Navy agencies.

CAUTION AGAINST OVEROPTIMISM

THE AMERICAN Foundation for the Blind has appropriated sufficient funds for the construction of fifty of these sensory units by Dunn Engineering Associates, Cambridge, Mass.

These units are to be distributed on a loan basis to determine possible applications that may result in a higher level of employment for the blind.

The difference between a useful tool and an interesting device is that the cost of a tool will be either self-liquidating by a higher employment level or it will open new avenues of information-gathering to the blind.

The usefulness of this device remains to be determined by the American Foundation for the Blind

REFERENCE

(1) Pointer and Line Locator Aids Blind, ELECTRONICS, p 194, Feb. 1954.

PRECISE HEAT for

SUMMARY —— Drawing a large single crystal of silicon from a crucible heated by r-f induction requires control within 0.25 deg C at 1,400 C over the period of an hour. Saturable core-reactors controlling r-f energy receive d-c signals from 100-deg full-scale recorder actuated by thermopile

ROUTINE production of large single crystals of silicon for use in transistor manufacture requires precise control of high temperature. The semiconductor, heated in a crucible by induction from an r-f generator, is controlled to within 0.25 or 0.30 deg C of its crystallization point for about an hour. Such control is needed to produce smooth crystals, as shown in the photograph.

The temperature limit of 0.25 deg is not a limit of error of measurement, but only a limit of drift from a set temperature of about 1,400 C. The problem is severe, because there is so little room for such factors as mechanical error of the recorder-controller, changes in calibration of the temperature detector and development of stray potentials in the circuits.

Temperature Sensing

Either thermocouple or thermopile (Rayotube) can be used as a detector for the electronic potentiometer recorder-controller, as shown in the block diagram, Fig. 1.

A thermopile equipment used by Philco Corp. at the Lansdale, Pa. plant is shown in the photograph. The thermopile in the housing below the crucible has a lens and mirror system that focuses radiation from the crucible bottom onto the pile. A small flow of inert gas in the path from pile to crucible keeps out dust and fumes, preserving the brightness and accuracy of the optical system.

The Le Carbone air cells are used to supply the recorder potentiometer circuit since they have good current output stability for the time required to grow a crystal. The Speedomax recorder-controller's expanded range covers 60 deg C.

Dual Control

Essentially two control loops are shown in Fig. 1 (outer). In the primary loop, an error signal, which is proportional to the deviation of measured crystal temperature from a set point, is developed by the control slidewire in the temperature recorder-controller *B* and delivered to the high-speed current-output controller *C*. Here the error is continuously analyzed to determine the corrective action necessary to restore the melt temperature to set point.

An output signal, ranging from 0 to 5 ma d-c is generated in accordance with this analysis and fed to magnetic amplifier *D* where it is changed to the level required to operate saturable core reactors, which adjust the power supply to a 300-kc induction furnace. This in turn controls the energy transfer to the melt and thus regulates its temperature.

In the secondary loop, the primary measuring element, its associated recording equipment and the process itself, together with their intrinsic time delays, are bypassed through the use of a pick-up coil that detects the energy level delivered to the melt and develops a proportional d-c signal that is fed back directly to the controller.

It is by this circuit that the con-

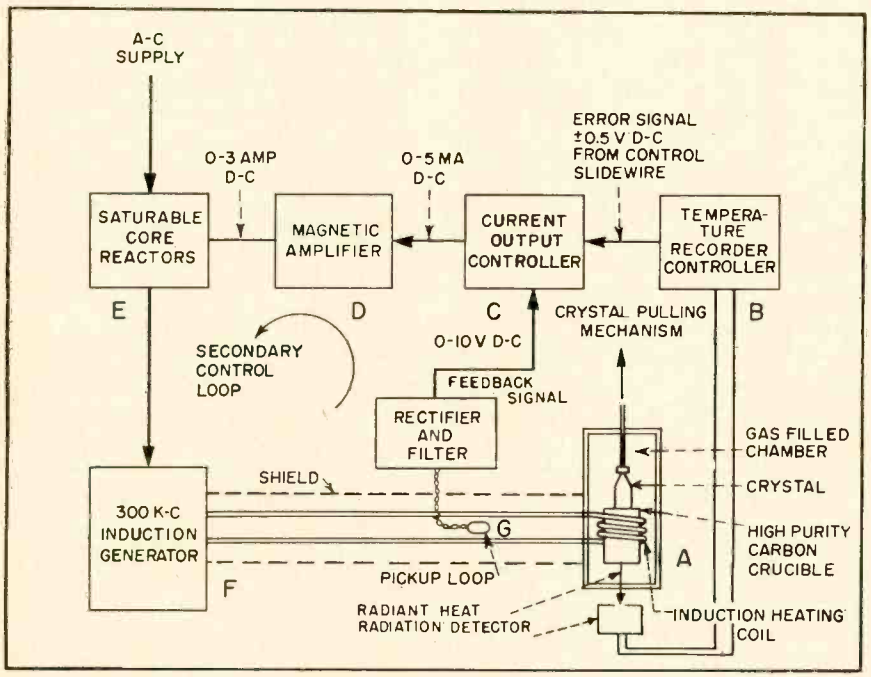
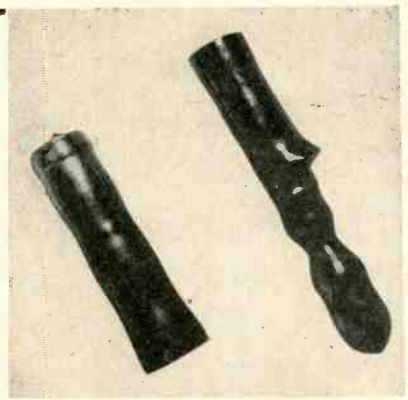


FIG. 1—Block diagram shows elements of the temperature control equipment including primary and secondary control loops

Growing Silicon Crystals

By E. T. DAVIS, W. B. ALDEN and F. H. WYETH

Leeds and Northrup Co. Philadelphia, Pa.



Effect of temperature control in growing silicon. Crystal at right cannot be used

Growing a semiconductor crystal from induction-heated bath

trol compensates promptly for line voltage change and other spurious effects that upset the temperature of the crystal growing process.

Crystal-Pulling Procedure

The procedure of crystal-growing is to fasten a seed crystal to a motor-driven pulling apparatus, touch it to the surface of the molten silicon and pull it away slowly as the crystal grows on the end. The seed is a piece of a previously-grown crystal, machined to about a quarter-inch square and an inch long. It is fastened to the puller head's rod by a chuck.

With the seed in place, the operator heats the charge to good fluidity, which occurs at about 1,425 C. Melting takes 15 or 20 minutes. When the charge is thoroughly fluid, the operator reduces the power and watches the surface for the first trace of cloudiness as the molten silicon cools. By gradually lowering the set point of the temperature controller, the operator brings about a balance of heat input such that the surface develops and maintains this trace of cloudiness. It is in maintaining this condition that the temperature limit of about 0.25 deg is essential.

The operator now lowers the seed until it touches the surface and then starts the puller. The shape of the meniscus is his guide; he watches it and adjusts speed of pulling and temperature as experience indicates. The crystal is made to grow continuously, by accretion from the surface of the molten silicon. Pulling takes 60 to 90 minutes. Total preparation time is one to two hours a crystal.

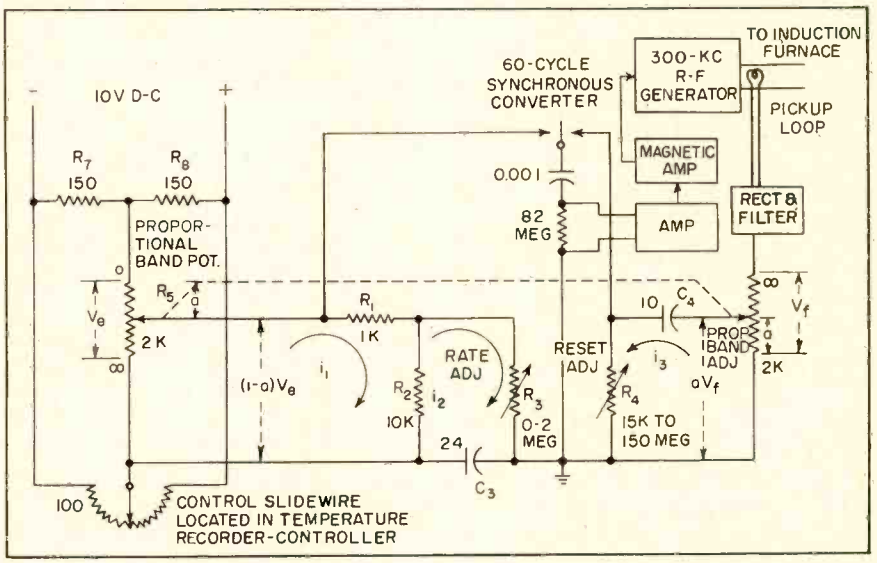


FIG. 2—Simplified computer circuit for current output controller

The current-adjusting controller *C* in Fig. 1 is an all-electronic unit in which output is related to its input on a three-function basis. A proportional component varies directly with the magnitude of the input signal to give proportional control. An integral component varies both with the magnitude of the input signal and its duration, to provide reset action. A derivative component varies with the rate of change of the input signal to supply rate action.

These three actions are suitably combined to produce the desired control signal for the process. Calibrated dials allow separate adjustment of each control function in accordance with the characteristics of the process under control to provide optimum control response.

The controller computing circuit used to derive the three basic control functions is shown in Fig. 2. At the left, a d-c Wheatstone bridge establishes an error voltage proportional to any deviation of temperature with respect to set point.

The control slidewire in temperature recorder-controller *B* is positioned by its control point setter. It is supplied with 10 v d-c and the voltage at its midpoint is just equal to a 5-v reference potential established at the junction of equal-valued resistors R_7 and R_8.

that are tied across the same 10-v supply.

The sliding contact is driven by the recorder-controller balancing mechanism, its position varying directly with temperature. The error voltage developed across the proportional band potentiometer R_5 varies from + 5 v d-c when temperature is low, through 0, to − 5 v d-c when temperature is high. The reference point is at the sliding contact of the control slidewire. Voltage V_e therefore indicates any deviation of the melt temperature from the set point and is equal to zero when temperature and set point are the same.

At the right side of Fig. 2 is the feedback circuit that develops a signal V_f proportional to the square root of the power delivered to the melt. This signal is obtained directly from the induction furnace input through a pickup loop that couples a small part of the r-f energy back to a rectifier and filtering unit. This in turn delivers a direct current to the controller. Over a reasonably small range, this current can be said to vary directly with furnace input. The feedback signal is converted into a voltage V_f through potentiometer R_6 and an adjustable portion of it is used by the controller computer circuit in developing the desired control action.

The passive network constituting the computer section of the controller may be analyzed mathematically to yield the following control equation

$$V_f = \frac{(1-a)K}{a} V_e\left[1+10\,\frac{T_3p}{T_3p+1} + \frac{1}{T_4p}\left(1+10\,\frac{T_3p}{T_3p+1}\right)\right]$$

Where K = a controller constant
a = the angular position of the proportional band potentiometer expressed as a percentage

$\frac{(1-a)K}{a}$ = the reciprocal of the proportional band adjustment

T_3 = the rate circuit time constant R_3C_3

T_4 = the reset circuit time constant R_4C_4

and p = the operator $\frac{d}{dt}$

Vf = the feedback voltage developed across R_6

V_e = the error voltage across R_5

From the above control equation, three functions will be observed. The first is a pure proportional action $(1 - a)K/a$, which depends only upon the proportional band adjustment a. The second is an approximate rate action that approaches a true derivative function for slow changes in the measured variable (where T_3p is much smaller than 1) but which reaches a limiting value of $10(1 - a)\ K/a$ when the measured variable changes rapidly.

The third function is a reset action that integrates the sum of proportional plus rate action with respect to time. The combination is thus a three-action control circuit that can be tuned to the process through the suitable selection of a (proportional band), T_3 (rate) and T_4 (reset).

Signal Comparison

The current-adjusting type controller is actuated by the presence of an unbalanced condition at its input. A differential amplifier compares the error signal derived from the measuring bridge (suitably operated upon by the computer circuit) with the feedback signal from

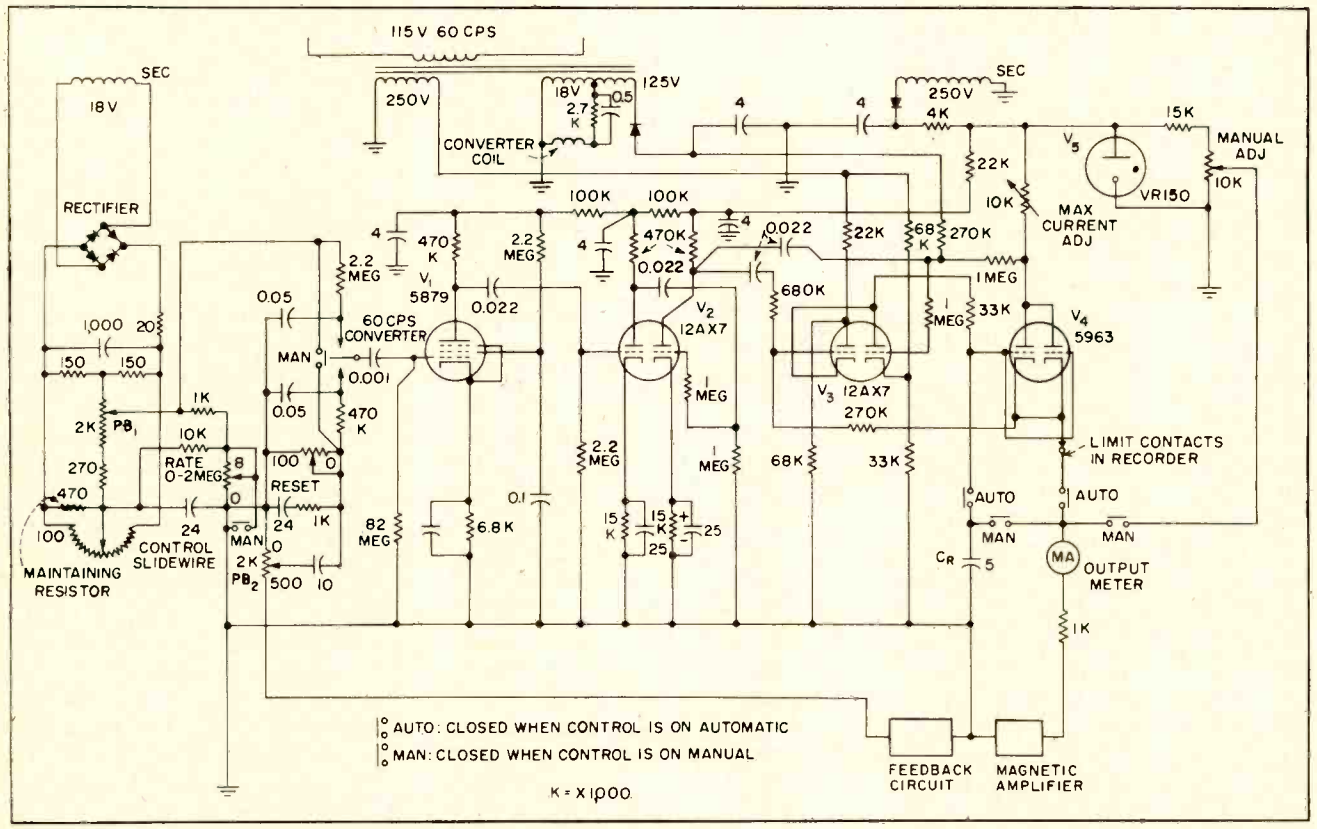


FIG. 3—Complete circuit diagram showing basis of temperature control

the furnace output (also operated upon by the computer). Any discrepancy between these two signals is seen by a 60-cycle synchronous converter that passes the resulting a-c voltage representing their difference to a high-gain amplifier.

Figure 3 shows in schematic form the controller amplifier and current adjusting circuit. Tubes V_1 and V_2 comprise a three-stage amplifier whose output, as measured on the final plate, is a 100-volt maximum peak-to-peak square wave reached when the input differential is one millivolt.

The phase of this square wave is the same as that of the line voltage supplied to the controller when the feedback signal indicates that the furnace input is too low. It is 180 deg out of phase with the line when this input is too high. The square wave thus derived is used as a gating signal to control the action of a phase sensitive charge-discharge tube V_3.

The output stage V_4 is essentially a cathode follower and delivers current to the magnetic amplifier load in accordance with the potential maintained at its grid by the charge-discharge tube operating into capacitor C_R. The operation of this circuit can be described by assuming that the furnace temperature is low. In this case, the differential amplifier produces a square wave at its output that is in phase with the line. This signal is applied to the grids of both the charge and discharge tubes, suitable d-c bias being maintained to limit or prevent conduction when the square-wave signal is absent.

Charge-Discharge

To make the charge and discharge sections of V_3 phase sensitive, they are fed from a 60-cycle voltage source. The plate of the charge section and the cathode of the discharge section swing with the line so that the former is blocked during the negative half cycle while the latter is blocked during the positive half cycle. Charging and discharging the capacitor C_R is therefore a function of the phase relationship between the signal present at the amplifier output and the line.

When these two voltages are in phase, as in the case under consideration, the charge tube is permitted to conduct during the positive half cycle since both its grid and plate have become positive with respect to its cathode. The discharge tube remains inoperative because its cathode is made positive with respect to its plate during the half cycle that its grid is moved in a positive direction. This results in a charging of capacitor C_R once each cycle until such time as the input signal to the amplifier is again brought into balance.

As C_R is charged, the output current from the controller increases in accordance with the requirements of the output tube characteristics, thus causing the furnace temperature to rise. A maximum current adjustment is provided in the plate circuit of V_4 to prevent the output from exceeding the value required for maximum furnace input. This adjustment sets the point at which the grid potential will exceed the potential of the cathode and thus prevent further charging of reference capacitor C_R.

The controller output current varies from 0 to 5 ma and operates through a total resistive load in the cathode circuit of 5,000 ohms. Thus the cathode of the output stage swings from zero to 25 v. The reference capacitor C_R voltage changes from −12 v at cutoff to +25 v at full output.

Error Signal

To function properly the current-output controller must maintain a close balance between the charge and discharge tubes over its relatively wide operating range. A small error signal is required at the input of the amplifier to hold a given output level. This is necessary to compensate for tube and other circuit component variations.

The size of this error signal tends to be a function of current output so that automatic internal adjustments are required for uniform controller operation. This is accomplished by changing the bias levels on these two tubes to compensate for the charge variation on capacitor C_R. As this latter voltage changes, the cathode of the charge tube and the plate of the discharge tube change in like manner. For this reason, the bias on the charge tube is driven in a positive direction with increasing output current, through a 270,000-ohm resistor, which connects to the cathode of the output stage.

This resistor is necessary to compensate for the cathode potential that is also moving in a positive direction. Similarly the bias on the discharge tube must go in a negative direction with increased current output, to compensate for its plate potential, which is becoming more positive. This action is achieved by running the grid circuit back to a voltage divider located between the plate of the output tube and a negative voltage source. Since the plate voltage of V_4 swings in a negative direction with increasing output current, the desired operating voltage for the discharge tube grid is obtained.

Current output of the controller in the order of 0 to 5 ma is fed to a magnetic amplifier where it is converted to a current ranging from 0 to 3 amperes.

Power Control

These reactors are connected in series with the r-f generator and regulate the power delivered to the equipment through changes in their reactance. The d-c control signal is fed to the reactor through a special winding, the ampere-turns being such as to saturate the core when 3 amperes flow.

Under this condition its reactance becomes negligible and the generator operates with maximum voltage supplied to its plates. Conversely, when the current to the reactor drops to zero, its reactance becomes a maximum and most of the supply voltage is dropped across the reactor, leaving little for the generator.

The magnetic amplifier and saturable-core reactors used for this application will respond to input changes in 0.1 sec or less, so the secondary or stabilizing control loop has an overall response time of about 0.5 second.

Among those who have contributed to the application of this control method are C. S. Duncan of Westinghouse Electric Co., S. L. Parsons and W. Moll of Philco.

INSTANTANEOUS

By CHARLES R. RUTHERFORD
Temco Aircraft Corp.
Dallas, Texas

SUMMARY — Maximum range of air-to-ground communications systems is extended up to 100 percent by use of speech compressor combining advantages of clipper and agc types. Use of transistors permits construction of unit that plugs into carbon microphone jack

MILITARY tactical requirements have increased the required distance for communication by 25 to 50 percent over the maximum range obtainable with existing communication equipment.

Communication range with an amplitude-modulated transmitter is a function of the transmitted sideband power and is independent of the transmitted carrier power. Because of the wide variations in amplitude of normal speech, voice peaks producing 100-percent modulation will give an average modulation of only 30 percent. A 30-percent modulation level results in the sideband power being down 10.5 db from the 100-percent modulation level.

Since intelligibility, not quality of speech, is the primary requirement for field communications, a transistorized speech clipper would increase maximum range on many existing communication sets.

The increase in maximum range when a speech clipper is used would be due to two factors: Higher average percent modulation would give a higher average transmitted side-band power, and the power of the intelligence carrying consonant sounds would be a larger percent of the total speech power. Assuming that a 50-percent word intelligibility is the minimum for useful communication, tests show that use of a 24-db speech clipper is equivalent to increasing transmitter power by 14 db. This increase is equivalent to a power gain of 25.

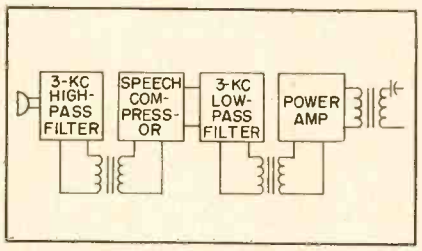


Fig. 1—Filters before and after compressor increase intelligibility

Speech compressor mounted beneath transmitter feeds microphone input

The ratio of the peak voltage of the average vowel to the peak voltage of the average consonant is about 12 to 15 db. Clipping can be used to make the intelligence carrying consonant sounds at least equal to the vowel sounds.

One type of simple speech clipper is a vacuum tube that is biased such that speech will drive the tube from cutoff to plate current saturation. A serious disadvantage of the saturation type of speech clipper is that when the talker is in a noisy location, such as an airplane, the speech clipper seriously decreases the speech-to-background noise ratio.

To prevent degration of speech-to-background noise ratio, conventional automatic gain control circuits have been used to control average percent modulation. This type of speech compressor will hold the average level of speech, and therefore the average percent modulation, constant. However, the circuit will not hold constant the peak values of the voice signal. With the agc type of speech com-

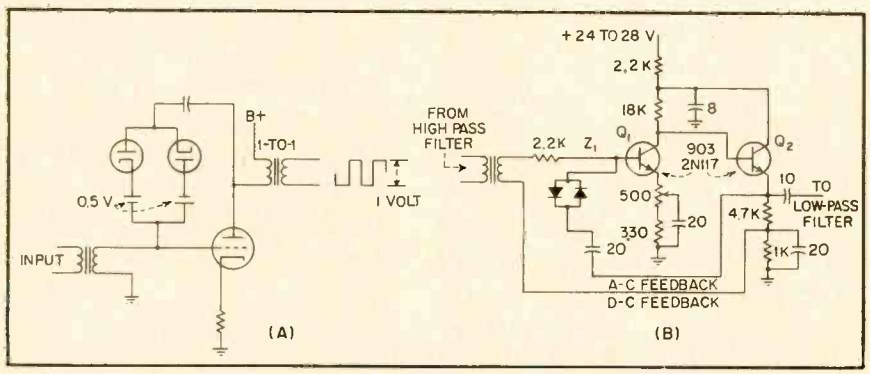


FIG. 2—Vacuum tube a-c feedback type compressor (A) operates in manner similar to the transistorized unit (B) used for air-to-ground communications

SPEECH COMPRESSOR

pression, normal speech will have peak voltages that are 12 db above the average voltage.

Circuit Operation

The instantaneous speech compressor system, shown in block form in Fig. 1, combines the advantages of both the clipper and the compressor and does not appear to have the disadvantages of either system.

As a-c feedback would decrease the background noise by the same factor as the voice signal, the circuit uses a delayed type of a-c feedback. Figure 2A uses a vacuum tube to illustrate the system principle. For signals with an a-c value at the plate of the tube less than 0.5 v the circuit will act like a conventional amplifier. For an instantaneous voltage that is greater than 0.5 v, one of the diodes will conduct and the signal will be fed back to the grid with a 180-deg phase reversal. If resistances of the diodes and batteries are low and gain of the tube is high, the waveform in the output circuit will be the same as the waveform obtained with a conventional speech clipper. However, as both signal and noise are fed back when the diodes are conducting, the speech-to-background noise ratio remains about the same.

A schematic of the transistorized instantaneous compressor circuit is shown in Fig. 2B. Basically, this circuit is a common-emitter amplifier direct coupled to a common collector stage. The bias for the first transistor is obtained from a d-c voltage divided in the emitter of the second transistor. As a common-emitter circuit gives a phase reversal, while a common collector circuit gives an in-phase signal, this method of obtaining bias for the first transistor results in a circuit with a high degree of d-c stability. The common-collector

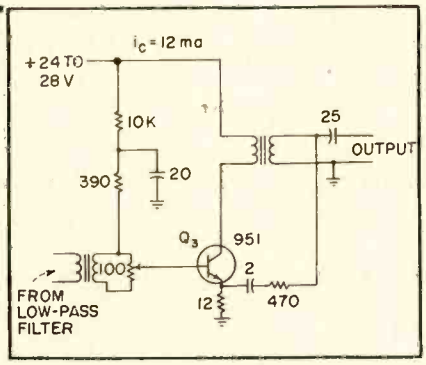


FIG. 3—Output amplifier feeds into aircraft radio microphone jack

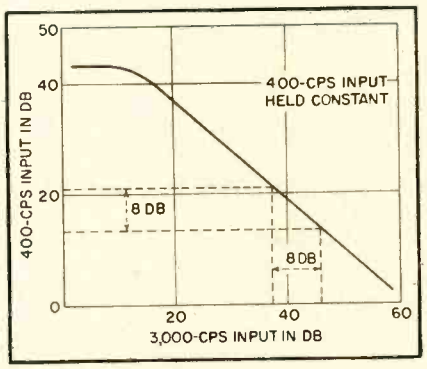


FIG. 4—Tests show ratio of voice to noise signal remains constant

stage gives a low-impedance source for driving a low-pass filter in the output and the a-c feedback circuit to the base of the first transistor. The transistors used are low-gain silicon type 903 having an alpha of 0.9 to 0.95.

The unique feature of this circuit is the use of silicon diodes in the a-c feedback circuit. The diodes will not conduct in the forward direction until a voltage of about 0.5 or larger is impressed across the diode. As a result, the forward resistance of the diode is very high until the instantaneous value of the a-c feedback signal is greater than 0.5 v. Above this level, the impedance of the diode is low. In addition to the compression obtained by feedback, compression is also caused by the sudden decrease in input impedance of the first transistor. When the diodes are not conducting, the impedance Z_1 is about 4,000 ohms as compared to 300 ohms when conducting.

Output Amplifier

The output amplifier, shown in Fig. 3, uses type 951 silicon power transistor. A feedback network from the secondary of the output transformer to the emitter resistor minimizes phase shift in the output transformer. The 25-μf capacitor in the secondary of the output transformer isolates the transformer winding from the d-c voltage applied to the microphone.

To check the effect of the instantaneous speech compressor on the speech-to-background noise ratio, a 400-cps signal of fixed amplitude and a 3,000-cps signal whose amplitude could be varied were fed to the input of the compressor. Figure 4 is a plot showing how the 400-cps output from the compressor varied as the amplitude of the 3,000-cps input signal was increased. When the 3,000-cps input is increased the 400-cps output must decrease if the speech-to-background noise ratio is to remain constant.

Intelligibility of speech in the presence of low-frequency noise can be greatly increased by using proper filtering before and after a speech clipper. The filter preceding the clipper attenuates the low frequencies at the rate of 6 to 12 db per octave. The filter following the clipper attenuates the high frequencies at the rate of 18 to 24 db per octave.

Although controlled intelligibility tests have not been made, short-range tests on two pieces of military equipment have shown that sideband power is increased at least by a factor of 4 when the speech compressor is used.

A disadvantage of the instantaneous speech compressor is that when the talker is in a noisy location, the amplitude of the noise between speech will be practically the same as the amplitude of the speech. However, tests at the Harvard Psycho-Acoustic Laboratory have shown that noise that is present only between words does not affect the intelligibility of the message.

Portable TV Station

By L. E. FLORY, G. W. GRAY, J. M. MORGAN and W. S. PIKE

RCA Laboratories
Princeton, New Jersey

SUMMARY — Designed to be carried on a man's back, nineteen-pound television transmitting station includes camera, monitor, sync generator, 2,000-mc transmitter and power supply. Total transistor complement of 72 is employed in addition to vidicon, kinescope and transmitter tubes. Camera delivers 1.5-v p-p composite video signal to line or transmitter

BROADCASTERS have need *for* lightweight portable television pickup equipment for spot news coverage and other events. An experimental portable television transmitting station has been developed that generates a picture of adequate quality for remote-broadcast purposes and transmits it for over a distance of approximately one mile. This equipment was used at recent political conventions to make possible remote pickups that would not have been possible by any other method.

System Description

Employing 72 transistors, the equipment includes, in addition to the camera, a sync generator, picture monitor and transmitter, as illustrated in the block diagram of Fig. 1.

The camera contains a video preamplifier, horizontal and vertical deflection circuits and a blanking amplifier in addition to the vidicon with its yoke and focus magnet. Horizontal drive pulses, vertical drive pulses and mixed blanking pulses, as well as d-c voltages are supplied to the camera over a four-foot cable from the backpack. The video signal from the camera video preamplifier is sent back to the backpack on a coaxial conductor braided into the same cable.

As in the miniature transistorized television camera described in the Jan. 1, 1957 ELECTRONICS, use is made of a new miniature vidicon only one-half inch in diameter.

The monitor contains horizontal and vertical deflection circuits and a video amplifier.

A switch on the backpack permits the operator to monitor either the video signal at a suitable point in the modulator or a rectified and amplified sample of the transmitter output. The latter gives the operator an instantaneous indication of transmitter overmodulation. The electronic viewfinder also permits the cameraman to check the vidicon electrical focus, which would be impossible with an orinary optical viewfinder.

The backpack contains a rechargeable battery, a transistor power converter to supply high voltage for the camera, monitor and transmitter tubes, a crystal-controlled sync generator, a 2,000-mc transmitter, a modulator amplifier in which d-c level setting, sync addition and set-up addition are performed, and a small auxiliary video amplifier and rectifier which samples the transmitter output. The transmitting antenna projects from the top of the backpack.

Compared to similar vacuum tube equipment built by the authors several years ago[1], the camera with its viewfinder weighs four pounds while the earlier unit, which used a one-inch vidicon and a similar monitor tube, weighed eight pounds. The backpack unit weighs 15 pounds and is 3 by 12 by 13 inches in size. The present equipment consumes 30 watts and operates for nearly five hours on a smaller size battery.

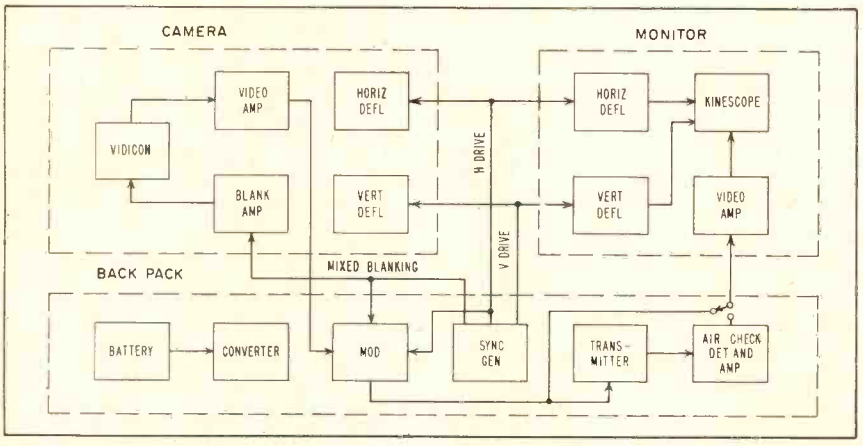


FIG. 1—Diagram of principal units of system—camera, monitor and backpack

Camera

The circuit of the camera video preamplifier is shown in Fig 2, along with the blanking amplifier and the vidicon beam, focus and target voltage controls.

Common-emitter amplifier Q_1 is directly connected to the vidicon cathode. Negative mixed-blanking

for Remote Pickups

signals from the sync generator in the backpack are applied to its base. Twenty volts peak-to-peak of positive mixed blanking are available at the collector of Q_4. This is adequate to prevent landing of the vidicon beam under any conditions during the horizontal and vertical retrace periods.

It has been established that in video amplifiers the best signal-to-noise condition is obtained if the vidicon is operated into a high impedance even though the input circuit has high capacity. The effect of this high capacity is compensated by a high-peaker circuit.

The input amplifier employs transistors, Q_1, Q_2 and Q_3 and exemplifies in Q_1 and Q_2 a type of feedback pair which has been freely used in later stages, particularly in the modulator. The pair consists of transistors of opposite conductivities, with feedback from the collector of the second to the emitter of the first.

This arrangement is d-c stable, has high input impedance and has low output impedance from which either output polarity may be derived. In this case, the collector of the second transistor is d-c connected to the base of the third, Q_3.

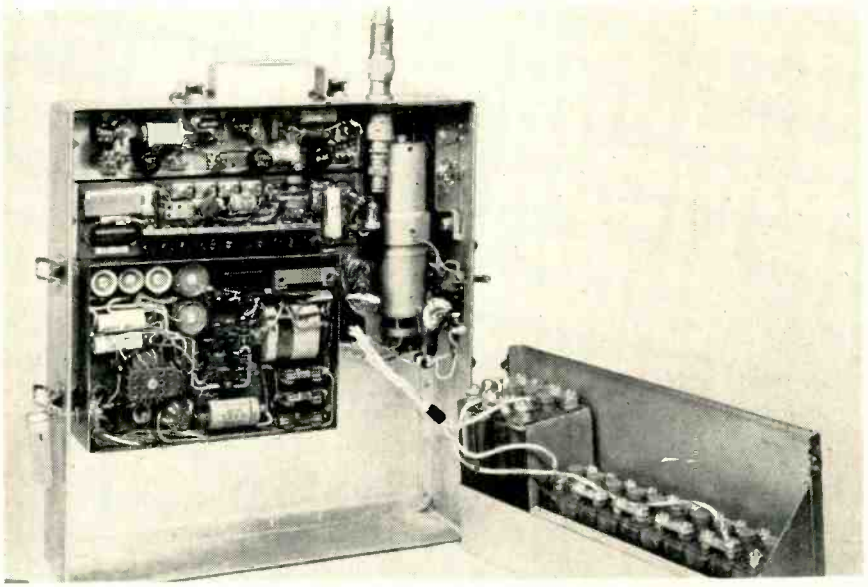
The response of this circuit is maintained flat to six mc with peaking inductance L_1 and by shunting the emitter resistor of Q_3 with C_1.

Bias control R_1 sets the operating point for this circuit.

Stage Q_5 is an ordinary common-emitter stage which drives the high peaker. High-frequency response is maintained by C_2 and overall low-frequency compensation is provided by C_3.

Stages, Q_6 through Q_9 are ordinary common-emitter amplifiers. They are, however, overcompensated as far as high-frequency response is concerned; the cumulative effect of overcompensation supplies aperture correction.

Video gain control R_2, compensated by C_4, is inserted between Q_8 and Q_9. Transistors Q_{10} and Q_{11} comprise another feedback pair which drives the interconnecting cable. The latter feedback pair delivers about 0.5 v of six-mc video signal to the 75-ohm line with good linearity. In this case, output is taken from the emitter of the second transistor of the pair.



Backpack houses sync generator (top left), power converter (lower left), transmitter (center) and rechargeable cells (right)

Camera Deflection

The camera deflection circuits are shown in Fig. 3. The sync generator in the backpack supplies negative horizontal and positive vertical drive pulses to the camera. The negative horizontal pulses turn on Q_{31}. Amplified positive horizontal pulses appear at its collector.

Output transistor Q_{32} is driven by a step-down transformer. It acts as a switch to interrupt the build-up current in the coil. Ringing is prevented by the damper diode.

The vertical deflection circuit is driven by the positive vertical drive

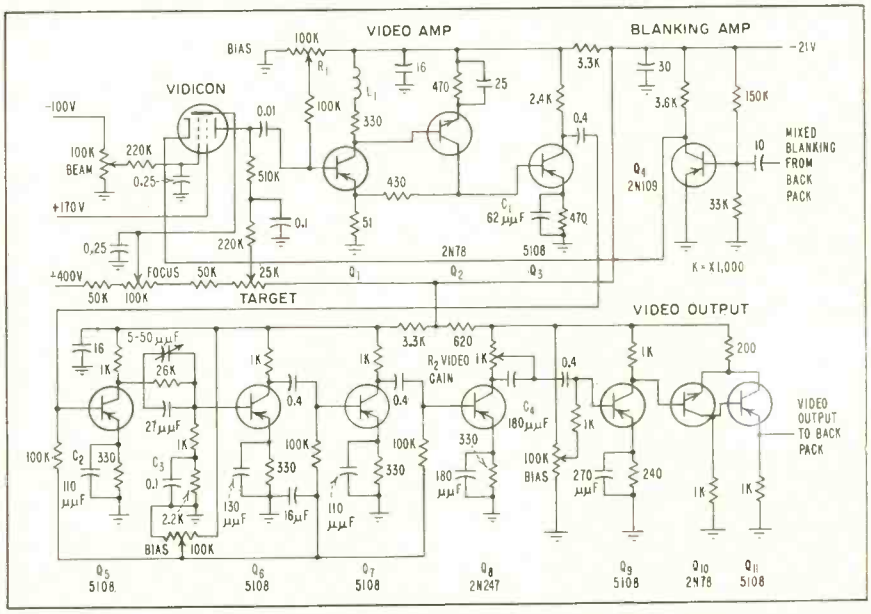


FIG. 2—Camera preamplifier employs 11 transistors and miniature vidicon pickup tube

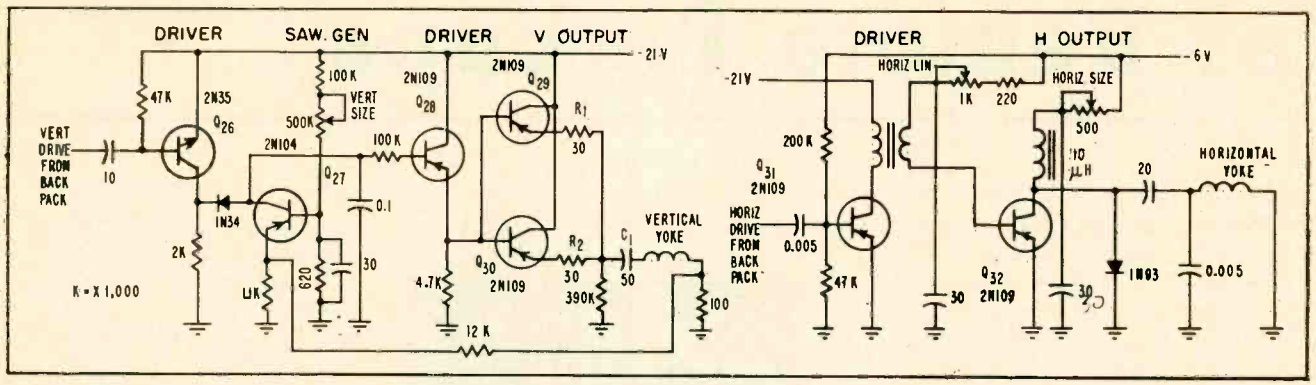


FIG. 3—Camera vertical (left) and horizontal (right) deflection circuits use low-power transistors because of miniature vidicon's modest deflector requirements. Vertical and horizontal drive are supplied via cable from backpack

pulses. These are inverted by Q_{26}, which drives a sawtooth generating circuit comprising Q_{27} and its associated components.

The vertical drive to the yoke is provided by two paralleled emitter followers, Q_{29} and Q_{30}. Resistors R_1 and R_2 equalize the currents in the transistors.

Negative feedback assists in linearizing the yoke current and circumventing the shortcomings of the necessarily small coupling capacitor, C_1.

Modulator and Transmitter

The modulator and transmitter are shown in Fig. 4. The transmitter, depicted at the upper right of this diagram, is a self-excited cavity-stabilized planar triode oscillator which is grid modulated. Output frequency is adjustable from 1,900 to 2,100 mc. The maximum output power with the voltages available is about 0.5 w.

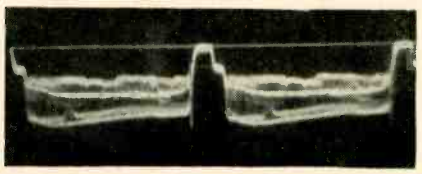
A video signal of one to two volts amplitude is sufficient to modulate fully the transmitter. This signal is supplied by transistors Q_{12} through Q_{16}.

The camera video signal is coupled from cable termination R_1 into the base of Q_{12} through a relatively small capacitor, C_1. A keyed clamp sets the d-c level at this point at the start of each horizontal line. This action is provided by Q_{17}, which is turned on by negative mixed-blanking pulses applied to its base. In somewhat unconventional fashion this also clamps the base of Q_{12} during the entire vertical blanking interval. The clamping potential is adjustable by the bias control, which is bypassed by C_2.

Since d-c information is reinserted into the signal, the following stages must be d-c coupled for this information to appear in the output signal. By employing alternate *npn* and *pnp* transistors, a five-stage amplifier of adequate stability has been constructed. The stage gains of this amplifier are not high; the large number of stages is necessitated by the many other functions which must be performed. Mixed sync, for example, from sync amplifier Q_{21} is inserted on the emitter of Q_{12}. Adjustable set-up is inserted on the base of Q_{14}, by feeding in a small amount of mixed blanking of the correct polarity at this point.

Feedback pair Q_{12} and Q_{13}, is similar to others previously used. This circuit is advantageous here because it presents a high impedance to the clamp circuit and thus does not discharge C_1. This would cause horizontal shading. Stage Q_{14} has been included to get a low-impedance point from which to drive auxiliary amplifiers Q_{15} and Q_{19}, as well as the actual modulator output stage which comprises feedback pair Q_{15} and Q_{16}. This stage will deliver about 1.5 v of video signal to the transmitter.

Emitter follower Q_{18} drives the line to the monitor amplifier when the monitor input selector switch is in the video position. Stage Q_{19} provides an auxiliary video output if it is desired to operate into a video line rather than use the transmitter.



Composite video output from camera

Transistors Q_{22} and Q_{23} amplify the output of diode D_1, which rectifies a sample of the transmitter output. When the monitor input selector switch is in the air-check position, the output of this amplifier drives the video line to the monitor.

Voltage Regulator

Regulator Q_{20} assists in maintaining the correct operating point of the transmitter as the batteries discharge during operation. It was found that as the six-volt portion of the battery discharged, the slight change in the voltage of the transmitter heater was sufficient to upset its operating point.

As regulation of the 0.9-ampere current of this heater would be a difficult task, it was found that a slight readjustment of the transmitter bias would accomplish the necessary correction. However, the sense of the requisite bias change is opposite to the sense of the change of heater voltage causing the trouble; Q_{20} accomplishes the necessary sense reversal. Its base is connected to the 6-v battery, through the network comprising R_2, R_3, R_4 and D_2, which sets the base potential at the correct d-c operating point.

The collector of Q_{20} is connected to the potentiometer which sets the clamp potential, thus inserting the required correction at this point. Direct-current degeneration in this compensating circuit is provided by R_5, with the loop gain adjusted to maintain nearly perfect compensation during the useful operating life of the battery.

For stability reasons, it is also

necessary to regulate the supply voltages of all these amplifiers. Regulated buses of six and 12 volts are supplied. The 12-v regulator comprises emitter follower Q_{25}, with the base potential set by zener diode D_3. The six volt regulator is Q_{24}, with base potential set by a potentiometer across the regulated 12-v supply.

Monitor

The monitor is shown in Fig. 5. As no suitable commercially available cathode-ray tube could be found for this unit, a special 1½-inch tube was made in the laboratory. The tube is magnetically deflected and electrostatically focussed. With an ultor voltage of 2,000 v, its resolution exceeds 300 lines. It fits a standard one-inch vidicon yoke, which requires about 400-ma peak-to-peak horizontal deflection current.

Complementary symmetry and negative feedback are used in the vertical circuit. Here Q_{37} and Q_{38} are power transistors with rated dissipations of one watt each, without heat sinks.

The video signal from the backpack is amplified by Q_{42} and Q_{43}. This circuit is a transistor version of the familiar electron tube long-tailed pair, providing a push-pull output with the cathode and grid of the monitor simultaneously driven in antiphase. By this means, the effective video drive on the monitor is made about 35 v peak-to-peak.

Driven clamp Q_{41}, which sets the d-c level of the monitor amplifier, is identical to that in the modulator except that only horizontal pulses from the monitor deflection circuit are used to drive it.

Sync Generator

The synchronizing generator, located in the backpack has two sections. The master oscillator and divider chain, comprising the first, is shown in Fig. 6 and the wave-shaping circuits and line drivers comprising the second, is shown in Fig. 7.

Operating at twice the 15.75-kc horizontal scanning frequency, master oscillator, Q_{44} in Fig. 6, is a negative-resistance oscillator. Use is made of the fact that a parallel

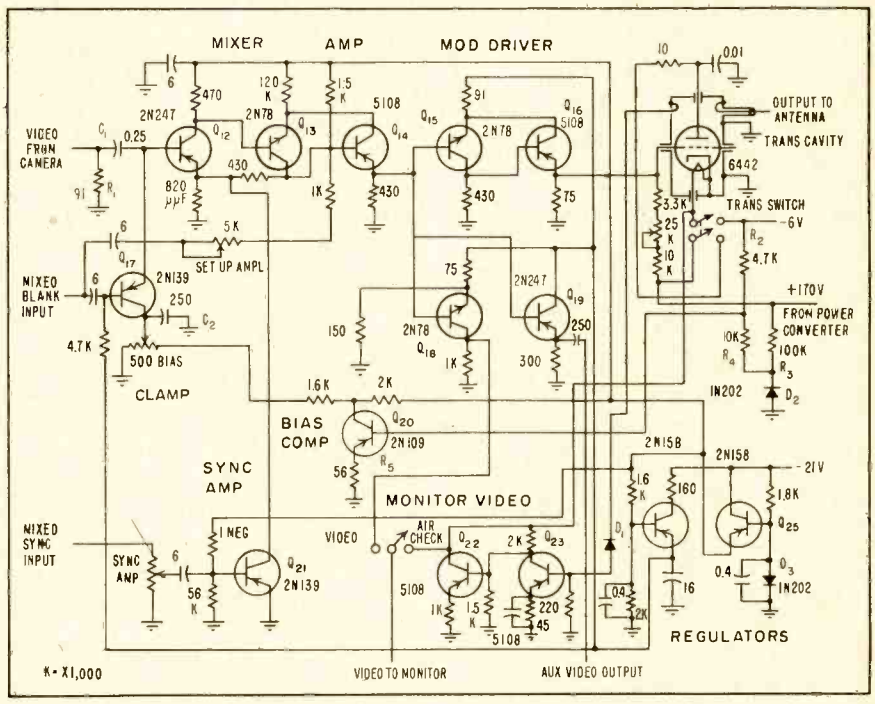


FIG. 4—Two-thousand-mc transmitter, video modulator and associated circuitry

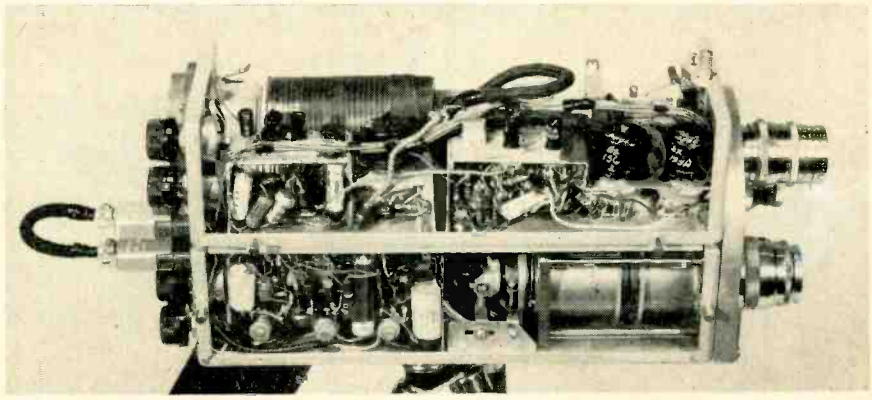
L-C circuit in the emitter of a grounded-collector transistor amplifier will cause a negative resistance to appear at the base terminal of the transistor at frequencies for which the emitter load is capacitive. With a quartz crystal placed in the base circuit, a large negative resistance appears in series with it, if the resonant frequency of the emitter circuit is less than the operating frequency of the crystal, and oscillation occurs.

Output is taken across R_1 in the collector circuit to drive isolation amplifiers Q_{52} and Q_{45}.

Horizontal Divider

The horizontal divider, which divides by two, is blocking oscillator Q_{53} using an autotransformer wound on a small toroidal ferrite core. A positive pulse of a few volts amplitude and about 1.5-μsec duration appears at the collector of Q_{53} each time the blocking oscillator fires. This is called the positive horizontal trigger and is used, after some processing, to initiate the leading edge of the horizontal blanking and drive pulses.

A delayed trigger pulse is derived from Q_{54}. An auxiliary winding on T_1 drives this transistor. The waveform on this winding is a considerably distorted single cycle of a sine wave; the width of each half-cycle is about 1.5 μsec. The winding polarity is such that the positive going half-cycle occurs first; Q_{54} does not conduct during



Side view of camera (bottom) and monitor (top) shows vidicon and kinescope yokes

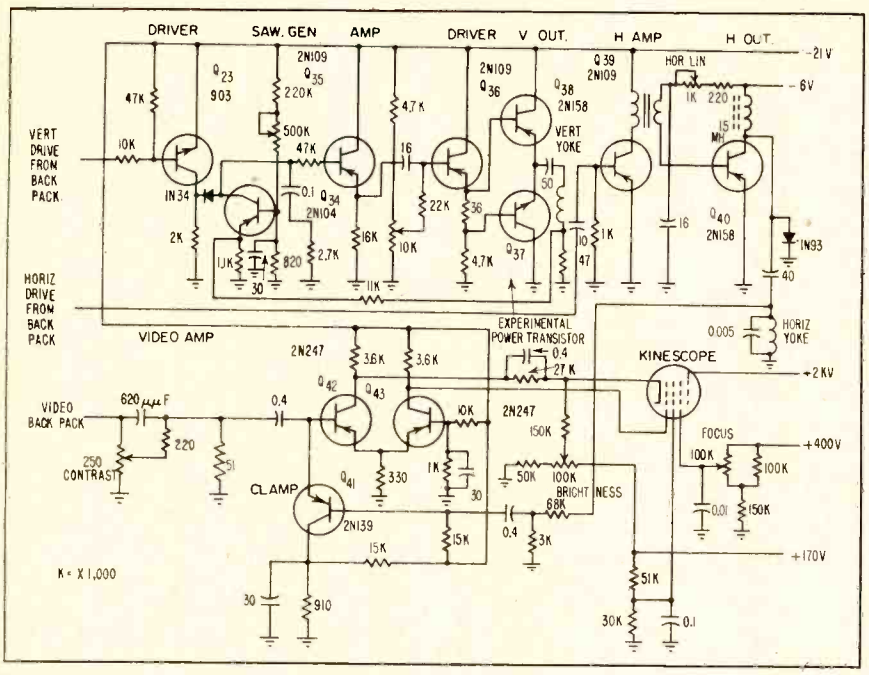


FIG. 5—Complete monitor circuitry for camera; kinescope is 1½ in. in diameter

this portion of the cycle.

On the following negative half-cycle, Q_{54} conducts and a positive pulse is generated at its collector. This pulse is delayed, with respect to the pulse from the collector of Q_{58} by about 1.5 μsec and is used as the delayed horizontal trigger pulse. The leading edges of the horizontal sync pulses and the serrations in the vertical sync pulses are derived from this delayed trigger.

This scheme sets the width of the front porch of the composite video output at 1.5 μsec, or the amount by which the delayed horizontal trigger lags the undelayed trigger.

Vertical Divider

The vertical divider chain comprises Q_{46} through Q_{49}. Each is a blocking oscillator with feedback from collector to base and the R-C circuit controling the repetition frequency in the emitter.

Temperature stability of this circuit is superior to that of other circuits in which the frequency-determining elements are in the base circuit because it isolates these elements from the effects of the temperature-dependent base-to-collector leakage current I_{co}.

As space is limited in the sync generator, the frequency determining elements of each divider are fixed and the amount of sync injection has been made adjustable to control the division ratio. Capacitors C_1 through C_4 are used for this purpose and require appreciably less volume than adjustable potentiometers. Voltage divider R_2 R_3 biases all the divider stages.

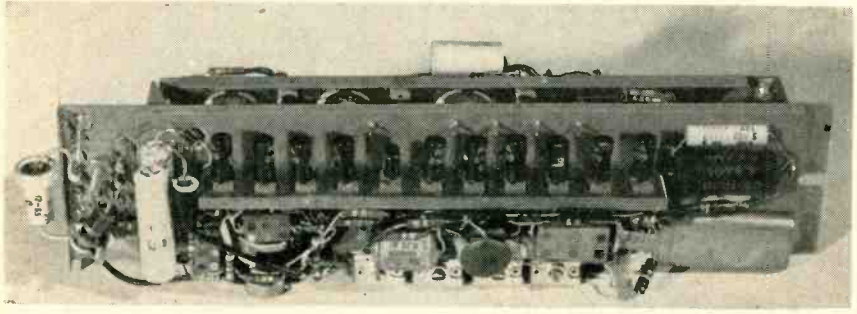
The vertical frequency pulses at the output of the last divider, Q_{49}, are too narrow to be used directly. Vertical pulses of the desired width are generated by the flip-flop comprising Q_{50} and Q_{51}. Each time Q_{49} fires, a pulse from its collector cuts off Q_{51}. The usual regenerative action in the flip-flop assists this and turns on Q_{50}. This action is reversed on the 15th, 21st or 35th cycle of the master oscillator after the firing of Q_{49} by a pulse taken from the collector of Q_{47} and fed to Q_{50}. This scheme causes the flip-flop to generate clean positive and negative vertical pulses, set at widths of 7½, 10½ or 17½ horizontal lines by adjustment of the order in which the usual divisors of three, five, five and seven are assigned to the various dividers.

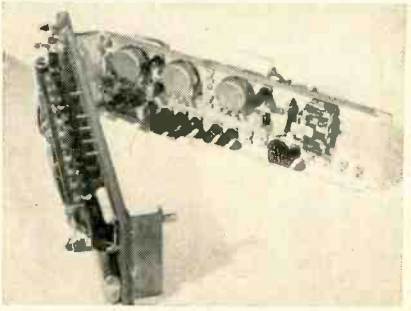
Pulse Forming

The output pulses from the divider chain consists of four kinds of pulses: positive horizontal trigger pulses, positive delayed horizontal trigger pulses, negative vertical pulses and positive vertical pulses. The waveshaper, shown in Fig. 7, synthesizes the following signals from these trigger pulses: positive vertical drive pulses; negative horizontal drive pulses; positive and negative mixed blanking pulses and negative composite sync pulses.

Vertical drive pulses are formed from the positive vertical pulses at the divider output by the amplifier and line driver comprising Q_{60} and Q_{70}. These are connected in the same feedback pair configuration used in the monitor. This amplifier makes positive vertical pulses of about five-volts amplitude available at a relatively low impedance.

Horizontal drive pulses are formed by an identical amplifier, Q_{67} and Q_{68}, driven from the undelayed horizontal trigger pulses at the divider output.





Sync generator consists of pulse shaper (left) with master oscillator chassis attached at rear (right) by hinge

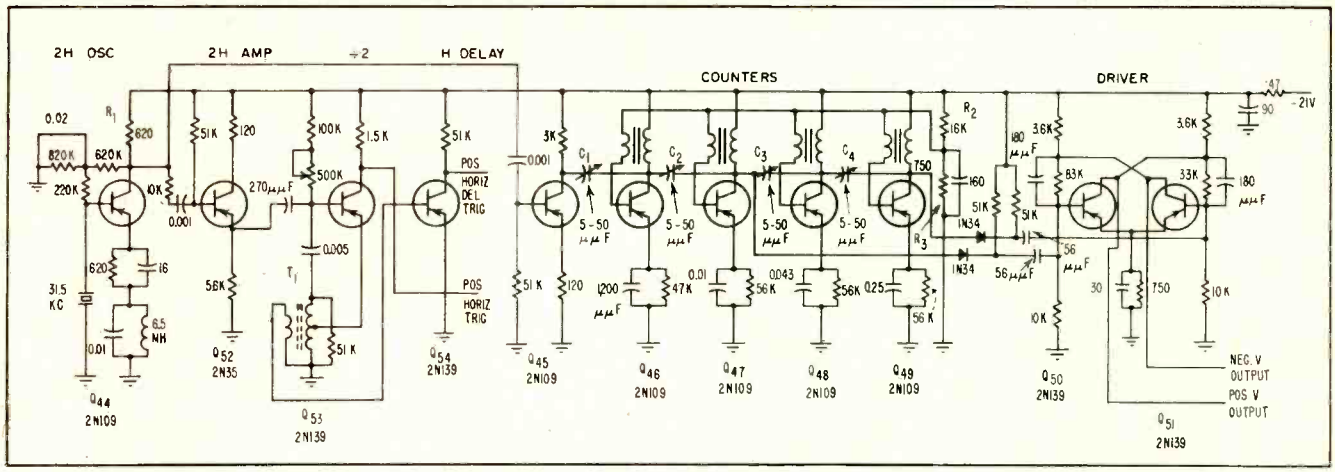


FIG. 6—Timing portion of sync generator includes 2H crystal-controlled master oscillator and blocking-oscillator count-down chain

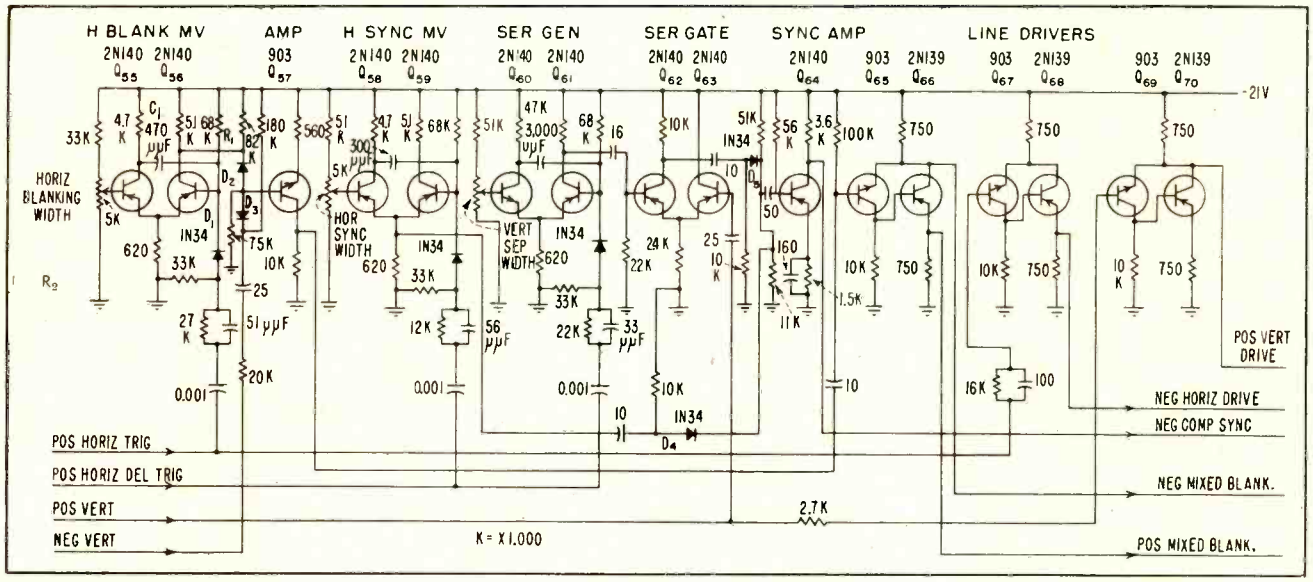


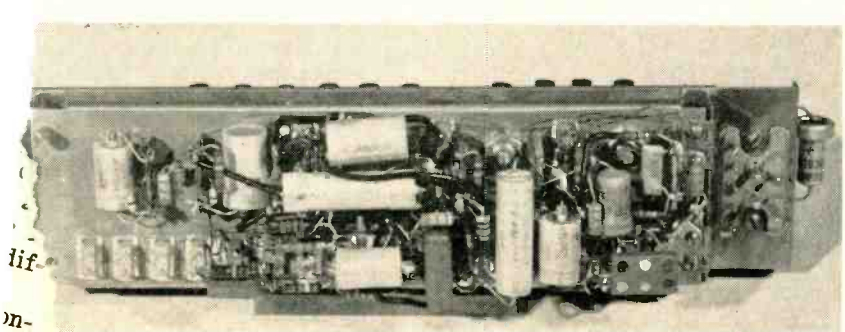
FIG. 7—Pulse shaping and gating section of sync generator turns out mixed blanking, composite sync and drive signals

Mixed blanking signals are synthesized from the undelayed horizontal trigger pulses and the negative vertical pulses from the divider by Q_{50}, Q_{56}, Q_{57}, Q_{65} and Q_{66}. Monostable emitter-coupled multivibrator Q_{55} Q_{56} determines the horizontal blanking width. Normally Q_{55} is off and Q_{56} on. Horizontal trigger pulses are applied to the base of Q_{56} via diode D_1; each pulse turns off Q_{56} and turns on Q_{55}. The circuit remains in this state for a period of time determined by time constant of C_1 R_1 and the voltage at the slider of R_2. It then flips back to its original state. Adjustment of R_2 varies the horizontal blanking pulse width between the limits of five and 15 μsec.

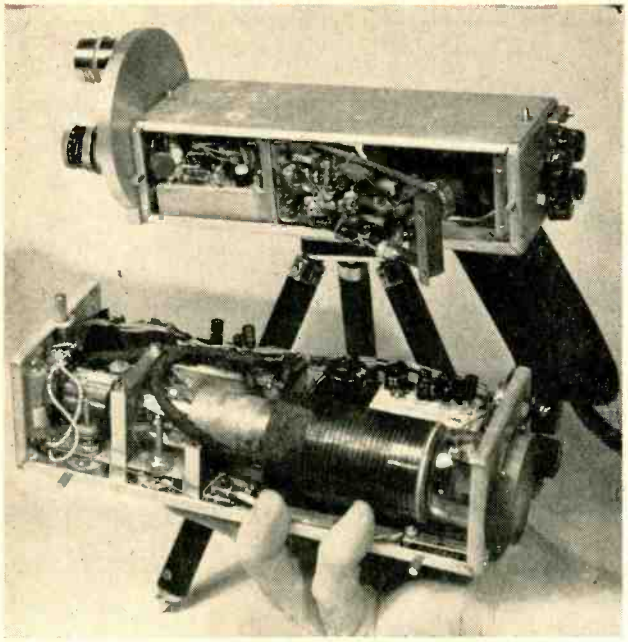
Negative horizontal blanking pulses from the collector of Q_{56} are mixed with the negative vertical pulses from the divider in an or gate comprising D_2 and D_3. The gate output is applied to Q_{58} and then to line driver Q_{65} Q_{66} from which both polarities of mixed blanking are available.

The three outputs from the sync generator just discussed must be transmitted via cable to the camera and monitor. Line driving amplifiers are provided for this reason.

The remaining transistors, Q_{58} through Q_{61}, are employed in generating composite sync. This signal is nonstandard, as illustrated in Fig. 8, in that there are no equal-



...w of sync generator shows master oscillator and counter chassis



Close up of monitor-viewfinder detached from camera

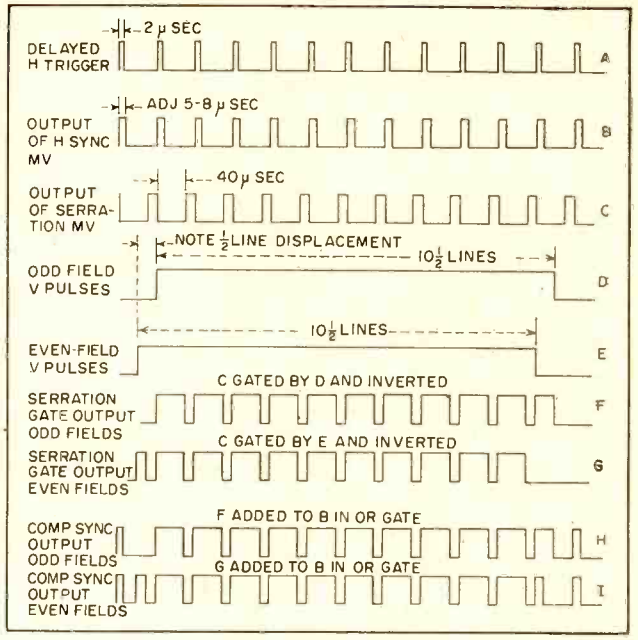


FIG. 8—Synthesis of sync pulses in circuit of Fig. 7

izing pulses. The vertical synchronizing interval is the same length as vertical blanking and there are serrations in the vertical sync pulses at horizontal frequency.

Sync signals are synthesized from the delayed horizontal trigger pulses and the positive vertical pulses from the divider chain. Monostable multivibrator Q_{58} Q_{59}, similar to that used to generate horizontal blanking pulses, generates horizontal sync pulses adjustable in width between the limits of five and eight μsec.

A similar multivibrator, Q_{60} Q_{61}, generates serration pulses of about 40 μsec width. The output of the serration multivibrator is gated by serration gate Q_{62} Q_{63}. This gate is open only during the vertical pulses from the divider.

The output of the serration gate thus consists of bursts of serration pulses which are timed to occur during each vertical pulse from the divider. This signal is mixed with the output from the horizontal sync multivibrator in another or gate comprising D_4 and D_5. It is then amplified and clipped by the sync output amplifier Q_{64}.

The power converter, shown in Fig. 9, steps up the low voltage available from the battery to the high voltages necessary to operate the transmitter, monitor and camera tubes.

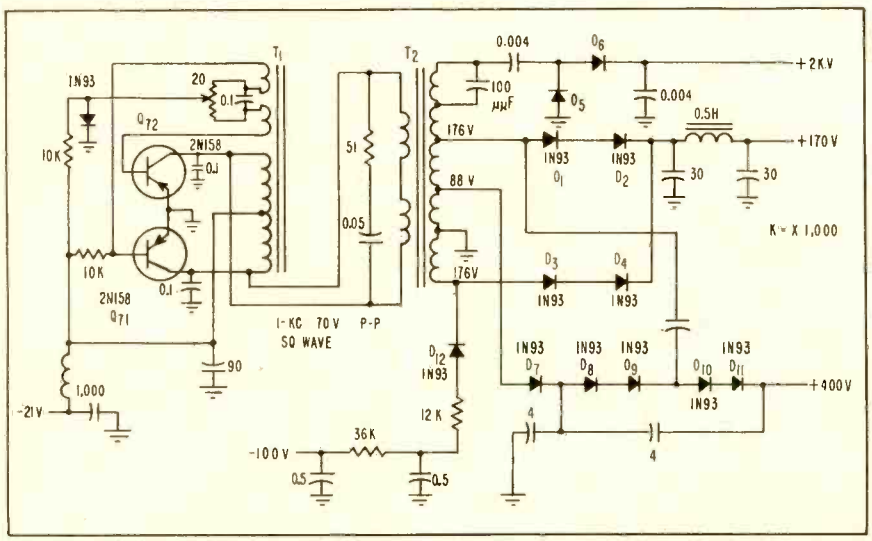


FIG. 9—Power converter uses one-kc square-wave generator for high-efficiency

Power Oscillator

Basically two transistors are used as a form of power oscillator to convert d-c to a-c. The latter is then transformed up to the desired voltage levels and reconverted to d-c by rectification. As the switching speed of the transistors is high, a 1,000-cps operating frequency, considerably above that of commercial vibrators, is employed to reduce the weight and size of the iron-cored components.

The power converter oscillator is similar to that described by Uchrin and Taylor[3]. However was found advantageous to slight modify their circuit. Separ transformers are used to con the frequency of oscillation an effect the necessary voltage t formation.

Transformer T_1 in Fig. wound on a small toroidal cor is designed to handle only the ing power for the base circui the transistors. A 1,000-cps s wave of about 90 v peak-to- appears from collector to colle of Q_{71} and Q_{72}. This signal is plied to the power transformer which steps it up to several d ferent voltages.

Most of the power from the c verter is delivered to the plus 17

bus. The principal load, about 50 ma, is the transmitter. This is supplied by the full-wave rectifier comprising D_1 through D_4. The 2,000-v ultor voltage for the monitor tube is supplied by the doubler comprising D_5 and D_6 driven by an additional winding.

The 400-v bus which supplies accelerating and focus potentials for the vidicon and monitor is served by the tripler comprising D_7 through D_{11}. The minus 100-v bus, which is used only for bias on the vidicon, is fed by half-wave rectifier D_{12}.

Overall efficiency of the power converter is about 90 percent.

Primary power for the entire unit is supplied by a bank of Yardney Silvercell batteries. Four LR-10 cells in series supply the six-volt bus which powers the heaters of the tubes and portions of the horizontal deflection circuits. Nine LR-5 cells in series with the six-volt portion of the battery power the 21-v bus. The flat voltage characteristic of these cells during discharge helps maintain stable operation of the more critical circuits, such as the sync generator dividers. This battery complement will operate the equipment for about five hours, before recharging.

Pickup Tube

The experimental miniature pickup tube, which was developed in an independent program of the Electronic Research Laboratory by A. D. Cope, has features which make it adaptable to transistor circuitry. The half-inch by three-inch vidicon operates in an axial ne
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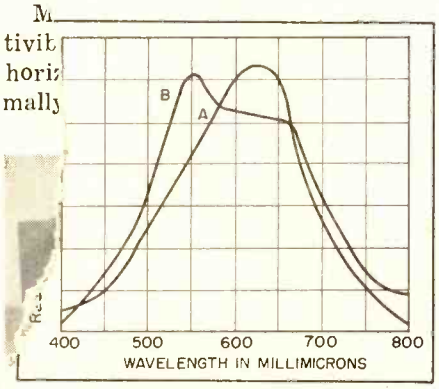


FIG. 10—Spectral response of miniature vidicon for equal values of radiant flux at all wavelengths

electromagnetic or permanent magnet field of about 80 gausses.

Power required to deflect the tube electromagnetically is about 20 ampere-turns or approximately ¼ that for the larger vidicon. This modest power requirement falls within the capabilities of low-power transistors of the audio amplifier variety.

The gun dissipates approximately 0.8 watt, a fourth that of the larger tube. Beam spot has been made smaller by reduction of the limiting gun aperture and path length so that the resolution is not greatly sacrificed over larger tubes, even though the scanning raster is only 0.24 by 0.18 in.

Photosurface

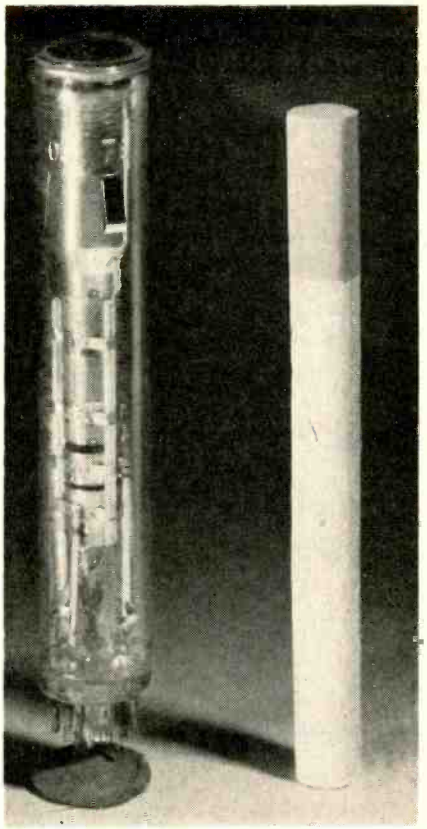
With such a small photolayer area, the use of a photoconductor having the sensitivity of that used in conventional vidicons would require an excessively fast lens or an increase in scene illumination. A new photoconductor surface has been developed which has sufficient operating sensitivity to more than offset the reduction in light-collecting area.

The photoconductive layer used has a sensitivity in the range from 1,000 to more than 2,000 μa per lumen when operating at signal levels of the order of 0.02 to 0.05 μa. The spectral response for the higher-sensitivity layers peaks at 650 millimicrons, as shown by curve *A* in Fig. 10. A more panchromatic layer with a peak response at 550 millimicrons, as shown by curve *B*, can also be made.

The gamma of the photosensitive surface depends upon the current density. At low illumination levels the signal varies linearly with light. At higher levels, for an output signal of 0.05 μa or greater, the gamma drops to 0.5.

The signal decay as a function of time for the new photosurface when compared with the photosurface used in earlier vidicons is somewhat different. The initial decay is not as rapid, but there is a smaller long term component of lag. This makes exact comparison difficult by subjective tests.

Tests were conducted with an experimental one-half inch vidicon and a typical one-inch tube operating in the same type of equipment and producing comparable images of the same scene. With 10 to 20 footcandles falling on the scene, equivalent output signals with comparable lag were observed in each picture when the small camera was operating with the lens at *f*/4 and the lens of the large camera at *f*/2. The combined difference of two lens stops and the four-to-one area difference indicates an operating sensitivity for the small tube 16 times greater than for the larger tube.



Experimental pickup tube has half-inch diameter and is three inches long

The authors wish to acknowledge the direction of V. K. Zworykin in this project and the cooperation of A. D. Cope who supplied the miniature vidicon. The assistance of Lawrence A. Boyer in design and construction contributed materially to the success of the work.

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(1) L. E. Flory, J. E. Dilley, J. M. Morgan and W. S. Pike, A Developmental Portable Television Pickup Station, *RCA Rev*, p 58, Mar. 1952.

(2) G. C. Uchrin and W. O. Taylor, A New Self-Excited Square Wave Transistor Power Oscillator, *Proc IRE*, p 99, Jan. 1955.

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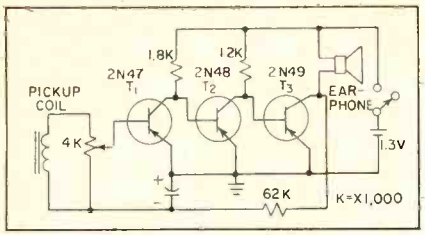

FIG. 1—Circuit of three-transistor portable receiver. Direct-coupled amplifier has feedback from output to input

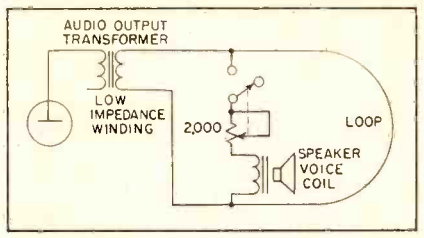

FIG. 2—Parallel operation of loudspeaker and paging system with separate volume control for speaker

Table I
Wire Size vs Impedance

AWG	Ohms per 1,000-ft length
16	3.8
14	2.7
12	1.9
10	1.2
8	0.75

SUMMARY — Transistor device smaller than a cigarette lighter and weighing one ounce provides sound reception without wires connected to the user or radio-frequency transmission requiring a license. Audio amplifier serves as the paging source, eliminating customary lights, gongs or loudspeakers

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AUDIO INDUCTION

ENERGY flowing through a loop of wire around the listening area is picked up by the miniature loop of a receiver, then amplified and converted to sound for the wearer of the instrument in this inductive paging system.

Because the sending loop is low impedance, it can be fed directly from the output of an audio amplifier, a tv set or a radio. Input to the audio amplifier can be a microphone for paging purposes or an f-m or a-m tuner for radio reception on planes, buses or trains. In the home, the tv set, record player or tape recorder could be used for the signal source.

Signal Propagation

The equation in the box indicates that radiated field strength is proportional to I, inversely proportional to λ and inversely proportional to distance d from the antenna. At the antenna, electric and magnetic fields are greater in magnitude and different in phase from the radiated field calculated from Maxwell's equations. The induction field diminishes at a faster rate with distance from the antenna than the inverse relationship of the radiation field and becomes negligible at a distance of a few wavelengths from the antenna or loop.

At a small fraction of a wavelength, the induction field is much stronger than the radiation field. For a loop antenna, the induction magnetic field is much stronger than the induction electrostatic field, while the reverse is true of the straight-wire induction field. The stronger induction magnetic field of the loop antenna is used in this system.

Interference from 60-cycle equipment such as transformers is limited to the induction source and this area is directly proportional to current. For 60-cycle equipment not over 1,000 watts in size, this interference distance is limited to a few feet.

Radiation from a Wire

The strength E of the radiated field from an elementary antenna is given by

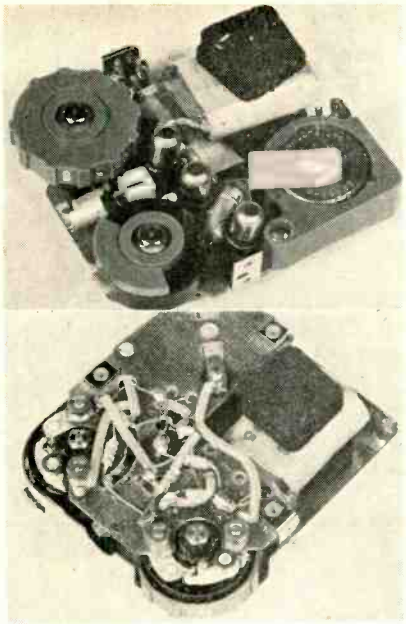
$$E = \frac{60\pi L}{d\lambda} I \cos\omega\left(t - \frac{d}{c}\right)\cos\theta$$

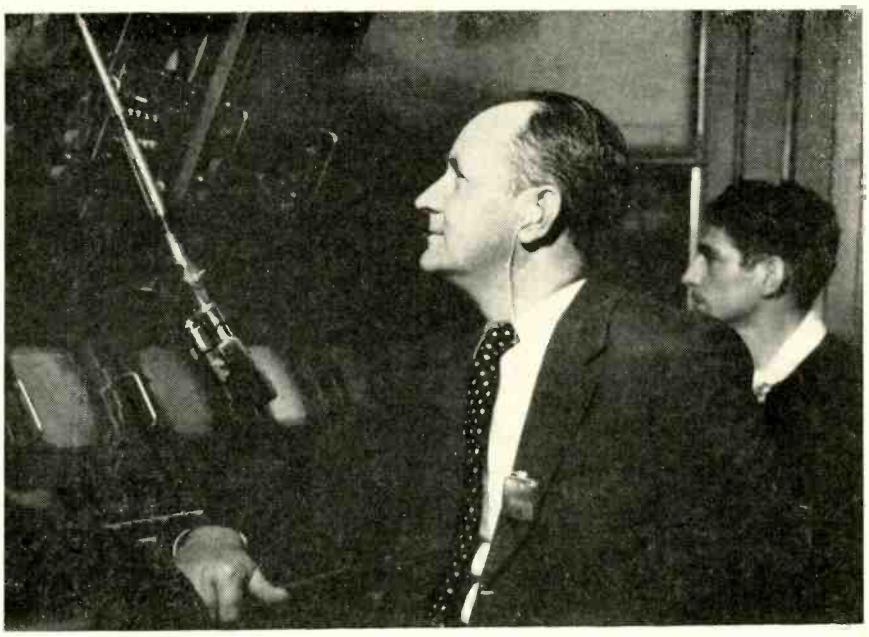
E = field strength in millivolts per meter
L = length of wire in meters
d = distance from antenna in meters
λ = wavelength in meters
I = current magnitude
t = time
C = velocity of light = 3×10^8 meters per sec
θ = angle of elevation from plane of antenna

Circuit Description

Low-impedance pickup coil (Fig. 1) is coupled to an audio taper volume control at the input of T_1. Output of T_1 is loaded by the input impedance of T_2 and T_1 output voltage conveniently provides bias for T_2 which, in turn, provides bias for T_3. Output stage, T_3 is biased to provide maximum undistorted current swing across the earphone.

The earphone acts as a d-c load for the stabilizing energy, which is fed back to the input resulting in low-frequency degradation and





Internal views of the miniature induction receiver show transistors and battery (top) wiring board (below). Audipage units find practical application in television studios allowing production personnel freedom of movement and instant liaison with control (right)

PAGING SYSTEM

25-db gain per stage at higher audio frequencies. With V_{ce} of T_1 equal to V_{be} of T_2, the point of quiescent operation is near the knee of the E_c-I_c curves. However, since the output of T_1 and T_2 is fed into the low impedance of T_2 and T_3 respectively the shunting effect of R_c (1-α) is negligible and allows operation of the amplifier down into and below the knee region of the E_c-I_c curves.

As the collector-to-emitter voltage falls toward zero from this knee region, alpha also approaches zero. Keeping alpha near normal and consequently maintaining the circuit gain limits the operating point to this knee region or above.

Power gain G_P of a common emitter transistor amplifier is expressed as

$$G_P = \frac{R_L}{R_{IN}} \times \left(\frac{\alpha}{1-\alpha}\right)^2$$

when R_L is the load resistor and R_{IN} is input impedance.

When $R_L = R_{IN}$, that is, T_2 provides the load for T_1 and T_2 and T_3, the gain becomes

$$G_P = \left(\frac{\alpha}{1\,\alpha}\right)^2 = 1{,}520 = 31.8 \text{ db}$$

where $\alpha = 0.975$

The above represents the maximum available gain of a direct-cascaded common-emitter configuration. Approximately 25 db per stage is realized in this direct-coupled circuit. Approximately the same gain results from a common-base amplifier configuration but represents only one component per stage (a resistor) for amplification.

Installation

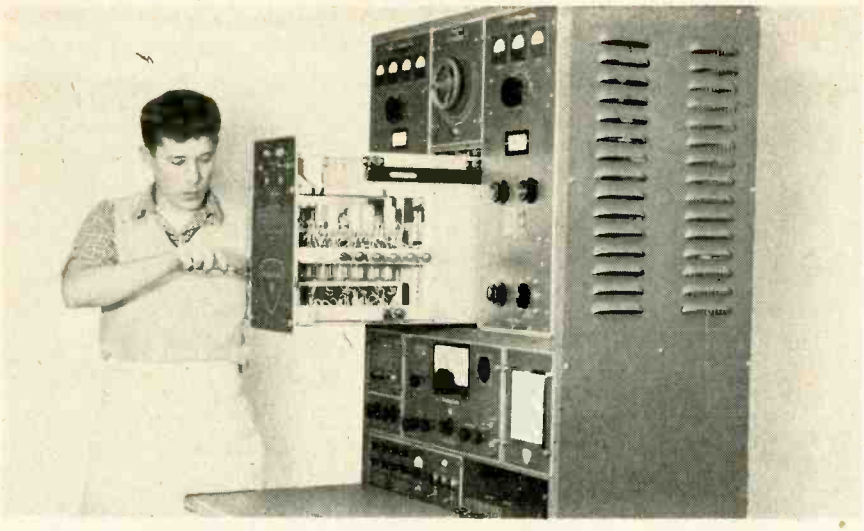
The loop of wire that sets up the magnetic field is low impedance and is fed from the output of an audio amplifier. Any size of wire from No. 20 to No. 8 awg can be used for the loop. For best reception, the loop impedance should be matched to the output impedance of the driving transformer. Typical impedances for a loop length of 1,000 feet are shown in the table.

A small radio, battery portable or tape recorder provides sufficient drive for a home or office area 20 by 30 feet. For larger areas the power required is calculated on the basis of 50 to 500 milliwatts per 1,000 sq ft depending upon the ambient background noise of the paging area. For areas larger than 5,000 sq ft, multiloops fed in series and phased so that the magnetic flux is additive, will improve performance.

Multiloop Use

In multifloor buildings, loops on different floors must also be in phase to prevent cancellation of flux. For widely separated areas, one amplifier can be used with distribution lines to step-down matching transformers for each loop. The area of adequate listening signal level outside and in the plane of the loop is equal to approximately three times the area of the loop.

The distance perpendicular to the plane of the loop for adequate pickup is approximately equal to plus and minus the smallest dimension of the loop.



Autoalarm unit (left) mounts in rack of marine transmitting and receiving equipment

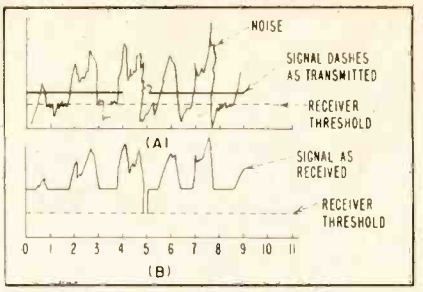


FIG. 1—Modification of autoalarm signal by noise

SHIP AUTOALARM Uses

SINKING OF THE S. S. TITANIC on April 14, 1912 with a heavy loss of life, despite the relative proximity of potential rescue ships, focused attention of the major maritime countries upon means for enhancing the safety of life at sea.

Since failure of radio calls from the *Titanic* to alert nearby ships was regarded a paramount cause for the casualties, international agreements on radio installations and on distress calls have been major aspects of minimal standards since set up. Because most merchant ships carry only one radio operator, continuous aural monitoring on the 500-kc international marine distress is not generally feasible.

Accordingly, an international autoalarm standard was adopted, specifying that a ship in distress shall transmit for 1 minute a series of 4-second dashes separated by 1-second spaces prior to transmission of SOS calls. It is required that ships be equipped with an autoalarm tuned to 500 kc, which upon reception of 3 or 4 consecutive dashes of the signal shall actuate warning bells aboard the ship. Tolerances on the transmitted signal allowed dashes 3.5 to 4.5 sec and spaces 0.5 to 1.5 sec.

The possible case illustrated in Fig. 1 indicates that a signal transmitted within specified timing limits can be modified to constitute, as received, a signal differing considerably from that transmitted. Such random modification of an autoalarm signal may consist in extending the duration of a 4.0-sec transmitted dash beyond 4.5 sec as received; there may be an effective filling up of a transmitted space with a consequent duration of the space as received of less than 0.5 second. Apparent gaps in a transmitted dash can result from blocking of the autoalarm receiver.

Because of discrepancies between transmitted and received signals, new standards have been adopted for which the major technical requirements are shown in Table I.

The medium frequency marine autoalarm described here automatically monitors the 500-kc international distress channel while a ship's radio operator is otherwise engaged.

Receiver Design

The sole function of an autoalarm receiver is to mark for the associated selector the presence or absence of on-frequency signals above the receiver signal threshold. While the international marine distress channel from 492 to 508 kc is designated primarily for distress and safety traffic, the channel serves also for intership and shoreship calling. Accordingly, except during the international silent periods from 15 to 18 and from 45 to 48 minutes after each hour calls from a number of radiotelegraph

Table I—Autoalarm Specifications

The autoalarm shall respond to reception of four consecutive dashes timed as follows: minimum duration of each dash is 3.5 seconds, maximum duration of each dash is 6.0 seconds, minimum duration of each space is 10 milliseconds or less, maximum duration of each space is 1.5 seconds. The autoalarm shall respond to signals between 100 microvolts and 1 volt. The autoalarm shall respond to the alarm signal through interference (provided it is not continuous) caused by atmospherics and powerful signals other than the alarm signal. In presence of atmospherics or interfering signals, the autoalarm shall automatically adjust itself so that within a reasonably short time it approaches, insofar as is practicable, the condition in which it can most readily distinguish the signal

SUMMARY —— Automatic alarm for distress signal, required by law for certain vessels not covered 24 hours a day by licensed operator, has often been subject to malfunction resulting from interference and atmospherics. New device meeting more stringent FCC requirements is entirely electronic, using gate and counter circuits

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Mackay Radio and Telegraph Co.
Div. of I. T. and T.
Clark, N. J.

Computer Techniques

stations, transmitting simultaneously, are present on this channel.

Such radiotelegraph interferences are superimposed upon the diurnal and the noncyclic variations in intensity of atmospherics. They result in conditions whereby the level of sensitivity required for optimum discrimination of the autoalarm signal may change radically during unattended autoalarm watches. Earlier autoalarms, provided with manual gain controls, can be effectively disabled unless the gain control is readjusted to match alteration in the intensity of atmospherics and radiotelephone interference.

In such equipments, a warning lamp on the bridge lights to indicate that the receiver manual gain control requires resetting. Conventional gain control circuits are not suitable for an autoalarm receiver, since the receiver sensitivity, if instantaneously controlled by amplitude of signals, permits a stronger interfering signal effectively to capture the channel with consequent loss of a weaker alarm signal.

Reception of an autoalarm signal can be regarded as reception of a sequence of four intervals, 3.5 to 6.0 seconds long, during which the autoalarm receiver is in the signal-on state and these signal-on periods are separated by intervals not exceeding 1.5 seconds during

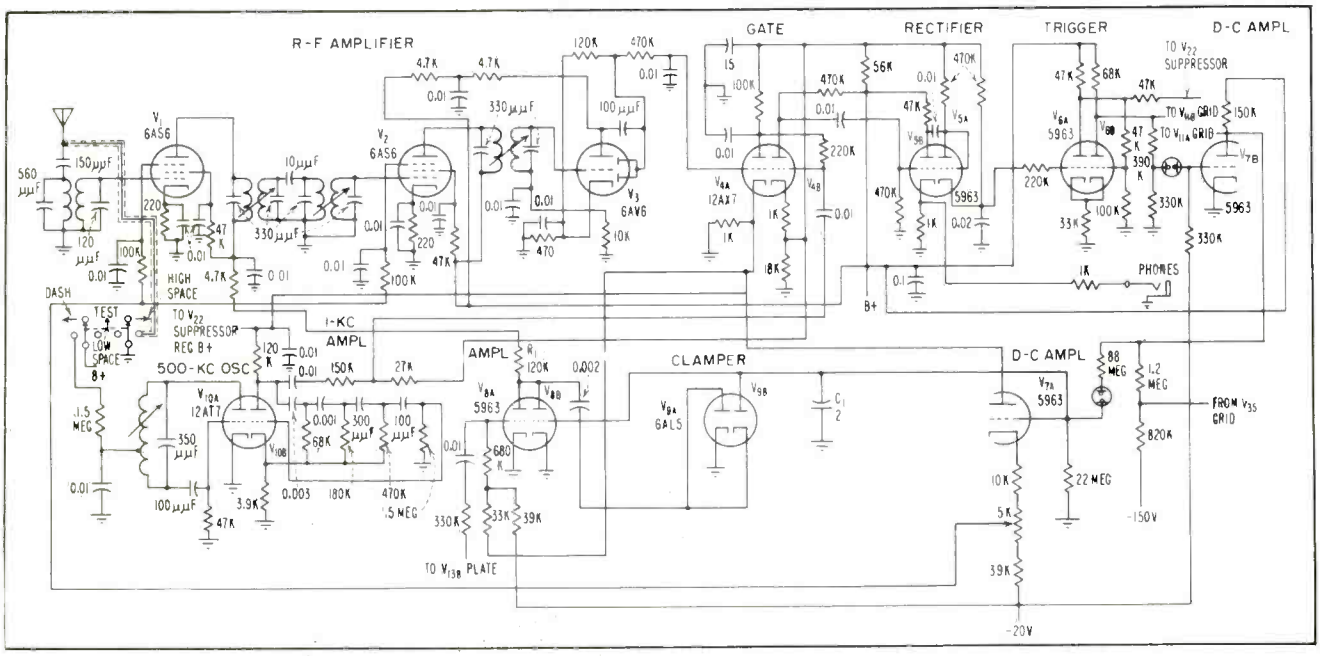


FIG. 2—Receiver used to pick up 500-kc signals is interconnected with selector circuit shown in Fig. 3

which the receiver is at least once in the signal-off state.

Gain Requirement

It is only when the interfering signals and atmospherics are sufficiently dense to keep the receiver from discriminating at least one gap each half-second that the receiver is incapable of responding to an autoalarm signal and requires a decrease in sensitivity. Improved performance should result from any system of agc in which the receiver threshold sensitivity is proportional to an integral with respect to time of a voltage step function. Such a characteristic could result in a linearly decreasing sensitivity during receiver signal-on states and an increasing sensitivity during signal-off states.

The rates of sensitivity increase and decrease should be contrived to prevent too rapid a decrease in sensitivity during an interval of 24 sec, which represents the maximum duration of an acceptable autoalarm signal and to result in constant sensitivity over periods during which the receiver discriminates at least one gap during each half-second.

The function of an autoalarm selector are:

(1) To time the durations of signal-on and of signal-off intervals.

(2) To register the number of consecutive acceptable signal dashes.

(3) To erase recorded dashes upon interruptions of an acceptable signal sequence by either a dash or a space outside the tolerances specified for each.

(4) To actuate warning bells upon reception of four consecutive acceptable and properly spaced dashes.

Since international minimal recommendations, which form the basis for the specifications drawn up by each maritime administration, do not include tolerances on duration of acceptable dashes and of acceptable spaces, such tolerances are specified by each administration and differ widely.

The autoalarm receiver shown in Fig. 2 is fixed tuned to 500 kc with a passband of 16 kc. The three stage signal frequency amplifier, V_1, V_2 and triode section of V_3 utilizes two 6AS6 tuned stages, with agc voltage applied to grid 3 of each and an aperiodic triode stage. The signal grids of the 6AS6 stages return directly to ground to assure rapid recovery from impulse static and strong signals.

A locally generated voltage at 1,000 cycles is rectified by V_{5A} and serves to control a Schmitt-type trigger stage V_6, which in conjunction with the cascaded two-stage d-c amplifier V_7 provides all output voltages required by the associated selector. The incoming signal, rectified and filtered for audio as well as r-f, is used only to control application of the 1,000 cps voltage to the Schmitt stage through gated amplifier V_4. A 500-kc signal generated locally by V_{10A} serves for testing the operation of the entire autoalarm.

As described below, the onset of a signal above the receiver threshold initiates in the associated selector a square voltage wave at 2.5 cps. This voltage is applied to the signal grid of V_{8A}, which serves as a variable-gain amplifier. The square-wave output of V_{8A} is clamped to ground by V_{9A}, while its negative excursions are applied by V_{9B} to charge capacitor C_1.

The staircase accumulation of charge on C_1 is linearized by applying the negative voltage across the capacitor to control the current drawn by V_{8B} through the common plate resistor R_1. This form of feedback serves to increase the amplitude of the charging pulses with increase of charge on C_1, resulting in effective linearization of the voltage across the capacitor. This voltage is applied to the grid of cathode-coupled triode V_{7A}, the output of which serves to control the gain of signal frequency amplifiers V_1 and V_2. Gaps in the signal allow capacitor C_1 to discharge.

In the presence of steady unbroken signals or static too dense to be resolved by the receiver the gain of the receiver decreases until the level of the unbroken static is just above the receiver threshold. At this level, the 2.5 cps square wave swings the gain control voltage, thereby effectivly injecting gaps into the solid signal.

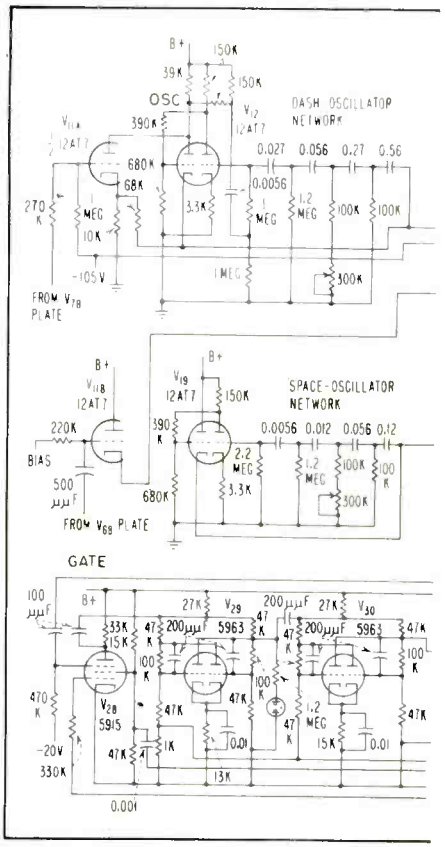
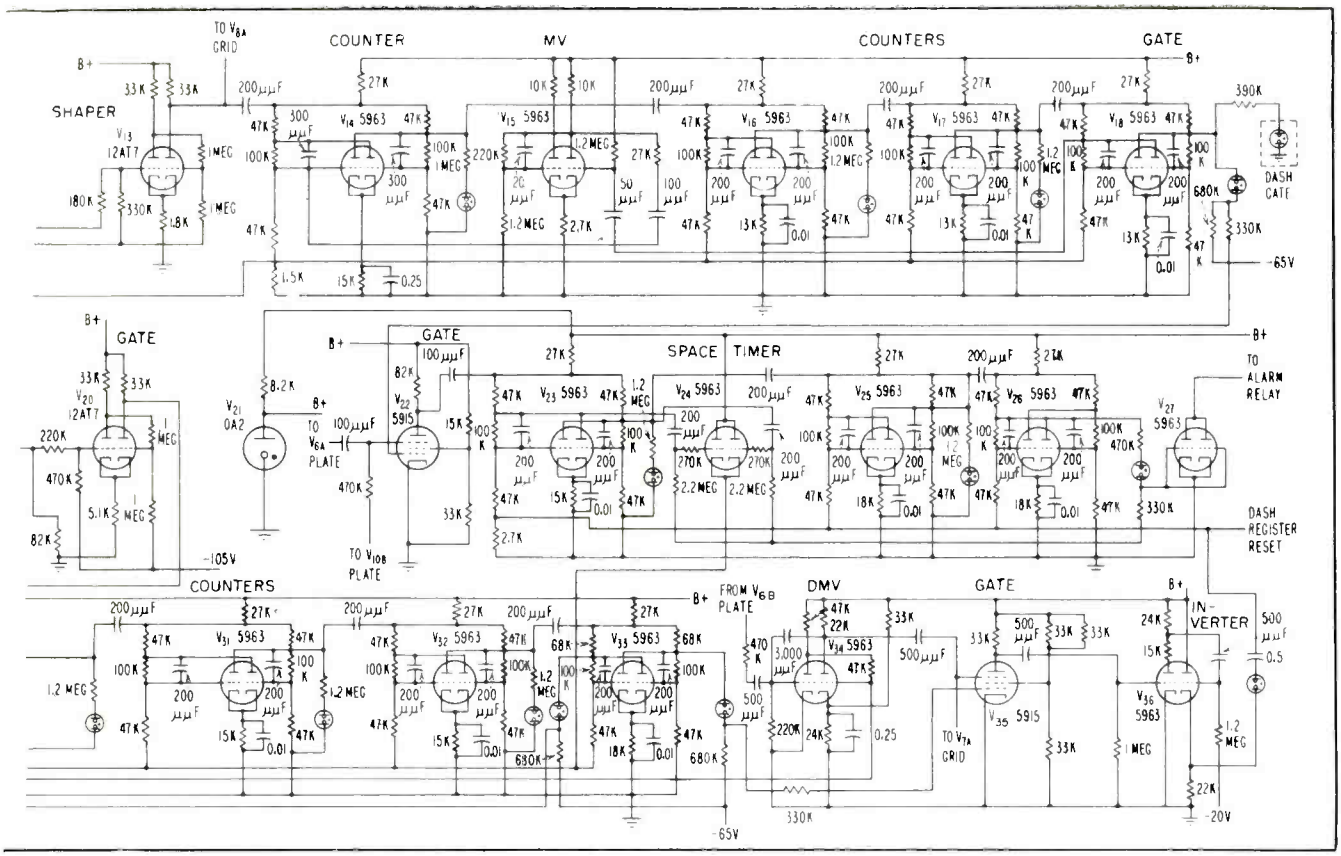


FIG. 3—Selector discriminates between

These forced gaps arrest further decrease in receiver sensitivity and the autoalarm, in this condition, can respond in a normal manner to an alarm signal above the level of the unkeyed signal or of the solid static. In the presence of impulse static or of several simultaneous radiotelegraph interfering signals, the gain of the receiver is reduced by the agc to a level at which signal gaps (occurring in a random manner in such interference) are within the resolving capability of the receiver. Gain is maintained at the level at which the receiver discriminates at least one gap per half second.

Duration of receiver signal-off states is timed by gated oscillator-regenerative shaper V_{12} and V_{13} in Fig. 3. The step-voltage generated by the receiver Schmitt stage V_6 turns the oscillator on and off by means of gating triode V_{11A}. An additional connection from V_{11A} plate to the V_{12} grid provides tighter phase-lock in starting and stopping of the oscillator. The tapered four-mesh phase-shift oscillator is sufficiently accurate for current



signal gaps caused by noise and those of the autoalarm signal. Interconnected with receiver (Fig. 2)

American tolerances.

Output from V_{13} is a square wave with a period of 0.4 second. This wave is applied to the four-stage dash-timing binary counter comprising V_{14}, V_{16}, V_{17} and V_{18}. The final counter stage V_{18} serves to control gated pulse amplifier V_{22}. The onset of a signal, as well as the end of each signal break, resets the dash timing counter through triode V_{11B}. The counter then operates to open gate V_{22} at the predetermined count of eight (corresponding to a signal duration of 3.2 seconds) and closes the gate at the count of 15.

The trailing edge of each signal is applied to gate V_{22} and any unbroken signal that terminates with an elapsed time t such that $3.2 \leq t \leq 6.0$ sec results in an output pulse from the gate. This pulse is recorded by the dash-registering three-stage binary counter comprising V_{23}, V_{25} and V_{26}. Monostable multivibrator V_{15} serves to impose the 8/7 duty cycle on the dash-counter gate controlling stage V_{18}. This multivibrator can be connected to result in V_{18} duty cycle ratios corresponding to ratios of integers such as 1/1, $n/(15\text{-}n)$, $n/(14\text{-}n)$ and so on. Selection of a particular duty cycle ratio with a corresponding selection of the dash-timing oscillator frequency can modify the device to accept dashes of duration other than 3.2 to 6.0 seconds.

Dash Timer

The dash register at the count of four actuates the warning bell circuit by cutting off V_{27}. A space-timing oscillator-shaper similar to the dash-timing oscillator operates at a frequency of approximately 10 cps. The output of this oscillator is applied through gated amplifier V_{28} to the space-timing five-stage binary counter comprising V_{29}, V_{30}, V_{31}, V_{32} and V_{33}. The final counter stage V_{33} serves to control gate V_{28}. The trailing edge of any acceptable dash is recorded by the dash register, as described above and simultaneously resets through V_{24} the space timer thereby opening gate V_{28}.

During the approximately 1.6 seconds elapsing before gate V_{28} is closed by the final counter stage V_{33}, the dash register reset circuit is rendered ineffective by gate V_{20}. This prevents noise pulses as well as keyed Morse signals during the 1.6 sec intervals following an acceptable dash from resetting the dash register. At the end of the 1.6 sec interval immediately following termination of an accepted dash, V_{33} applies a reset pulse to V_{34} which, provided no signal is present, resets the dash register. The signal, if present during the 1.6 sec time, can then terminate either as an acceptable dash or a dash too long or too short.

Registration

If this signal terminates as an acceptable dash, it is registered and the space timer proceeds through its timing cycle during 1.6 sec following the end of the acceptable dash. If, however, this signal terminates as a dash longer than 1.6 seconds but shorter than 3.2 seconds, the dash is not acceptable and its trailing edge actuates V_{13} to reset the dash register. If this signal terminates as a dash longer than 6.0 seconds, it serves to reset the dash register in the same manner as a dash too short.

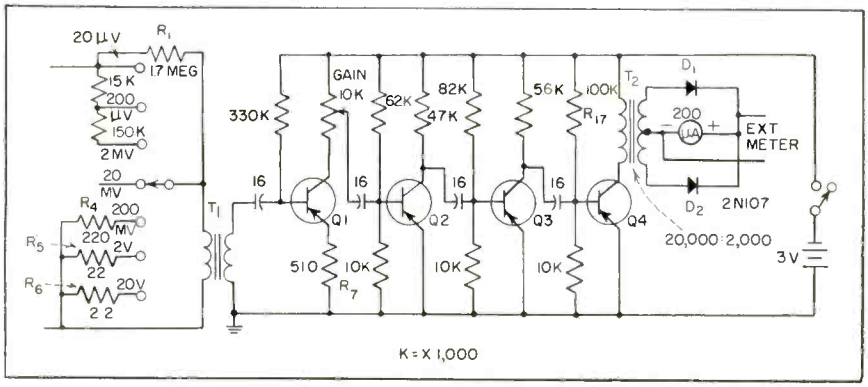


FIG. 1—Four-stage amplifier uses low current-gain transistors

By CARL DAVID TODD

Semiconductor Products Department
General Electric Co.
Syracuse, New York

SUMMARY —— Designed for use in laboratory, production line and shop, instrument has seven input ranges from 20 μv to 20 v. Readily available transistors are used in four-stage amplifier circuit. Expensive junction diodes, required for accurate low-voltage detection, are replaced by inexpensive transistors providing equal characteristics. Construction details are given

Transistor Null Detector

IMPORTANT CHARACTERISTICS of a null detector are high sensitivity, low internal noise, moderately fast response to changes in input levels, and an ability to withstand a large overload.

Circuit Description

The complete schematic diagram of a null detector with these characteristics is given in Fig. 1. It is basically a high-frequency audio amplifier whose output is rectified and fed into a sensitive d-c microammeter.

The input impedance varies when switching from the 20-microvolt range to the 20-millivolt range. After reaching the 20-mv range, it remains constant. This was done to avoid high resistance values normally required for the higher voltage ranges and also partially to eliminate noise in the input.

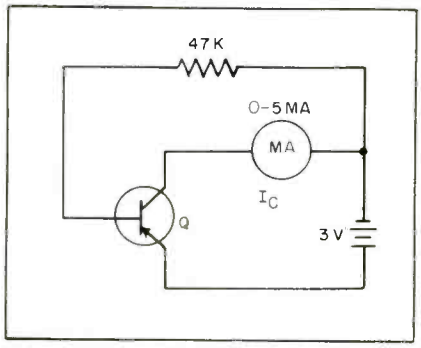


FIG. 2—Test circuit measures relative current gain h_{fe} of transistors

The input transformer is a modified push-pull driver transformer. The center-tapped secondary was modified to give two identical windings. By breaking the center lead and bringing out both wires separately a unity ratio transformer is obtained.

The input impedance to the null-detector amplifier was approximately 20,000 ohms. With the transformer connected, the input impedance dropped to 2,000 ohms.

The four-stage transistor amplifier uses low current-gain transistors. The amplification is sufficient. High-gain transistors may be used with slightly better results accompanied by a higher price tag.

The amplifier output is fed into a transformer originally designed as the driver interchange transformer for a push-pull amplifier. The centertap allows full-wave rectification without need of a bridge.

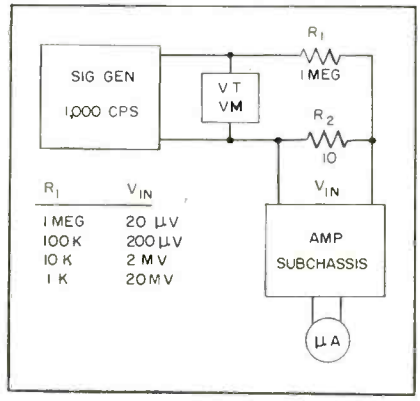
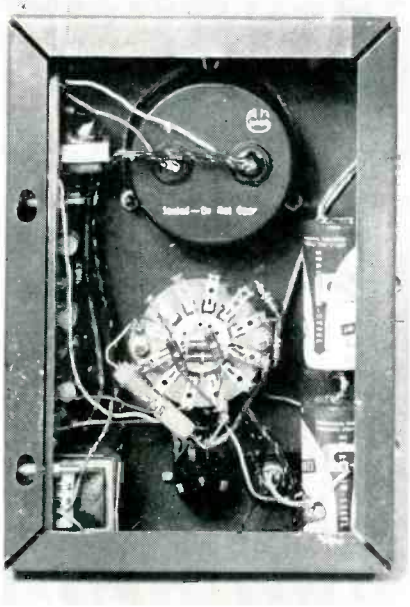


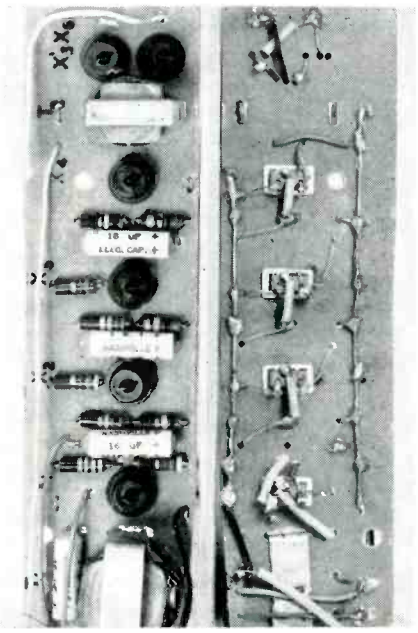
FIG. 3—Test set-up to determine values of detector input attenuator resistors

To achieve good results at low voltages, junction diodes are required for the rectifiers. At the present time, junction diodes are expensive. Type 2N107 transistors sell for much less and make excellent junction diodes. Either the emitter-base diode or the collector-base diode may be used. Both diode sections can not be used since they

Null detector fits in 5 by 7-in. case



Internal view shows parts layout



Subchassis parts layout and wiring

Has HIGH SENSITIVITY

are not independent.

Terminals are provided so the 200-microampere meter may be used for external functions. No switching is necessary to disconnect the output circuit from the meter since the diodes isolate the meter from the null detector whenever current is supplied to the external terminals.

Construction

The null detector was built in a 5 by 7 by 2-in. aluminum chassis. The amplifier and rectifier circuitry are mounted on a Textolite board subchassis. This is in turn mounted to the side of the main chassis. Printed circuit techniques are not used, but rather, small wires are employed to connect the various components together.

The current gain h_{fe} of the transistors used as diodes is not important. It may be wise, therefore, to use the two lowest h_{fe} units for this function saving the others for the amplifier.

The test circuit shown in Fig. 2 may be used to measure relative gains of the transistors. The transistor that has the highest collector current will, in general, have the highest h_{fe}.

The transistors had an h_{fe} ranging from 18 to 40. If transistors with current gains greatly different from this are used, it will be necessary to change the resistors supplying the d-c base-bias current. As a general rule, the base-to-supply resistor should give a collector current of about 0.5 ma.

Tests

A 1,000-cps signal applied to the amplifier input as shown in Fig. 3 allows measurement of the input voltage in the microvolt range. The exact values of the resistors used in the attenuator depend on the 1,000-cps voltage amplitude and the lowest voltage that may be measured by a vtvm or an oscilloscope.

The values shown are for use with a signal generator capable of delivering 2 volts rms. When two volts are applied to the input attenuator, 20 microvolts will appear across the 10-ohm resistor. This voltage should produce a deflection on the meter. If there is no deflection, the gain of the amplifier may be too low. To determine this, increase the input voltage by using a smaller series resistor R_1. Several values are given in Fig. 3. Once a deflection is obtained, the transistors should be swapped back and forth to maximize the gain.

Final gain adjustment is done by varying the value of resistor R_7.

The input-attenuator resistors are best determined by using a potentiometer for the resistor, applying the desired full-scale voltage to the input as shown in Fig. 3, then adjusting the potentiometer to give a full-scale meter reading.

The resistors should be determined in numerical order. With resistor R_1 connected in place, resistor R_2 is selected to give full-scale deflection with 200 microvolts applied. Resistor R_3 is selected in a similar manner.

Resistors R_4, R_5 and R_6 when placed across the amplifier input should produce full-scale readings at the desired voltages.

L NETWORK Design

SUMMARY —— Technique for using Smith chart to speed design of L matching networks for transmission lines and waveguides using lumped parameters. Shaded-area charts show at a glance impedance ranges that can be matched with each type of L network

By H. F. MATHIS
Goodyear Aircraft Corp.
Akron, Ohio

THE FAMILIAR Smith chart for transmission lines is also a useful tool for designing matching networks. As an example, consider the case where it is desired to match an impedance $Z_L = (0.3 - j1.6)R_o$ to R_o with the L matching network shown in Fig. 1. It is assumed that the inductances are lossy so that $R_1 = X_1 \tan\theta = 0.2X_1$ and $G_2 = -B_2 \tan\theta = -0.2B_2$. All impedances and admittances are normalized with respect to R_o and $G_o = 1/R_o$, respectively.

Let $Z_A = Z_L + R_1 + jX_1$ and $Y_A = 1/Z_A$. Since $Y_A + G_2 + jB_2 = 1$, Y_A must lie on curve $Y = 1 - k(\tan\theta - j)$, where k is a real variable. This curve is circle OA' with center C. To locate C, lines OC and OD are drawn as indicated in Fig. 1. Point D bisects its line. Point C is located as indicated.

Point C is inverted to obtain C' on line OC so that $C'O = \overline{OC}$. Since Y_A must lie on circle OA', Z_A must lie on circle OH whose center is C'. To determine Z_A, plot curve $Z = Z_L + p(\tan\theta + j)$, where p is a real variable. Point A, where this curve intersects circle OH, is the desired value of Z_A. The value of Y_A is found by inverting point A to obtain A'. Finally, $R_1 + jX_1 = (Z_A - Z_L)R_o = (0.498 - j0.610) - (0.3 - j1.6)R_o = (0.198 + j0.990)R_o$ and $G_2 + jB_2 = (1 - Y_A)G_o = 1 - (0.803 + j0.985)G_o = (0.197 - j0.985)G_o$.

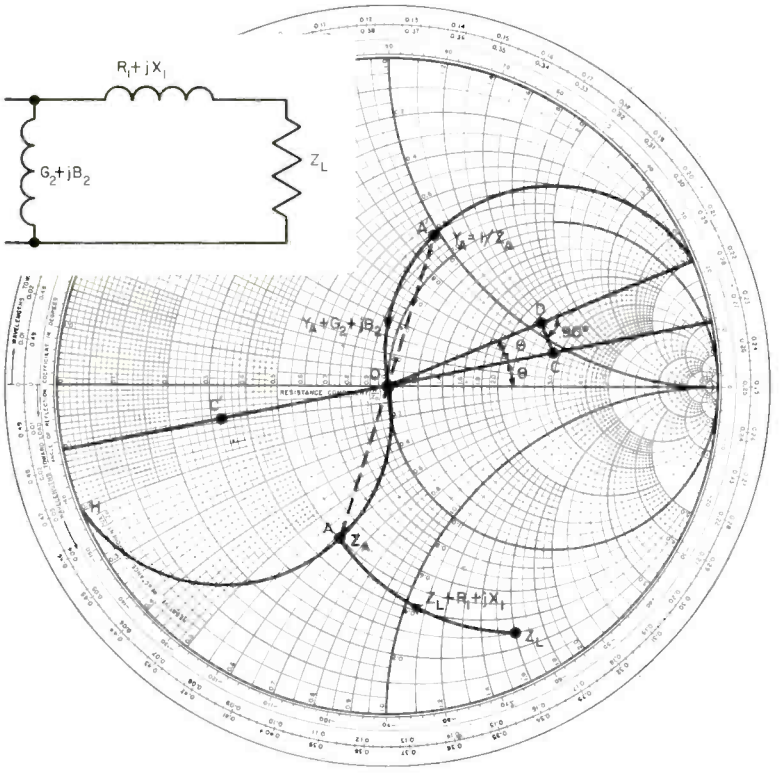


FIG. 1—Smith-chart procedure for determining parameters of L matching network

General Procedure

In general, for L matching networks plot Z_L or Y_L first on the Smith chart. Next, plot the impedance or admittance into which Z_L is to be transformed, and find a suitable path connecting these points.

It is impossible to match all possible values of Z_L with a given type of L network. For example, if $Z_L = 0.5R_o$, the matching network shown in Fig. 1 could not be used. Impedances which may be matched with a given type of L network are shown as areas on Smith charts in Fig. 2. It is assumed that it is desired to transform Z_L into R_o and that Z_L is normalized with respect to R_o.

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P. H. Smith, Transmission-Line Calculator, ELECTRONICS, p 29, Jan. 1939.
P. H. Smith, An Improved Transmission-Line Calculator, ELECTRONICS, p 130, Jan. 1944.

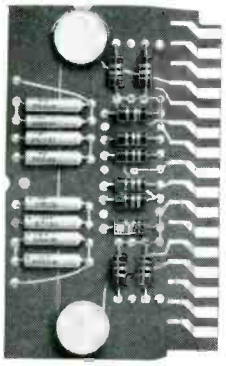
(Continued on page 188)

ELECTRONICS REFERENCE SHEET

CONSIDER a typical design in which there are 1200 packages each of which averages 25 connections—a total of 30,000 connections.

If these are wired by hand in the traditional manner, the time required to wire the device is but one of the very costly aspects of the problem. There are equally important difficulties such as the many varieties of wiring errors due to the human element which will occur even though the wiring is done by skilled technicians and which must be located and corrected by skilled personnel through laborious wire tracing methods.

The tremendous advantages gained by using package organization in an electronic device *are reduced appreciably by having to use an inadequate technique for interconnecting these packages.*



Component board (Typical printed wire package assembly).

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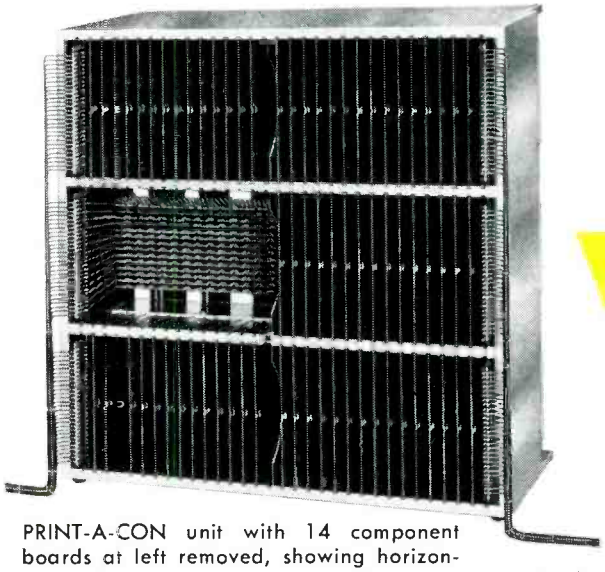
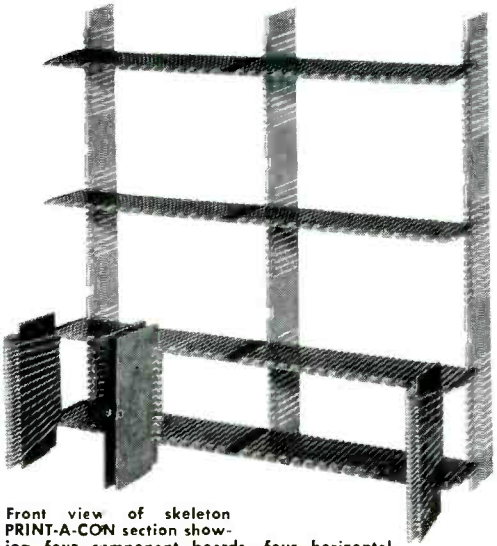


PRINT-A-CON unit with 14 component boards at left removed, showing horizontal and vertical wiring boards in back, also showing a view of the edge connectors mated with the interconnecting boards of the unit. PRINT-A-CON unit shown here is approximately 1½ ft. square by 1 ft. deep.

A multitude of horizontal and vertical wiring paths are available between all points on all component boards in the unit integrally with a means of interconnecting these paths in any desired pattern.

PRINT-A-CON opens the door to countless other approaches in the realm of mass producing complex circuitry and although it was developed initially for use in computers and control devices, its usefulness is not necessarily limited to these.

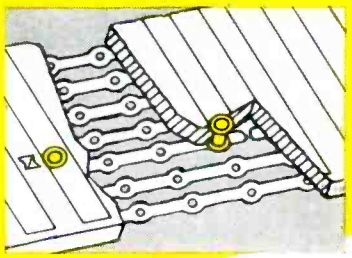
It is a newly developed component available to the electronics engineer with possibilities as unlimited as the imaginations of those who use it.



Front view of skeleton PRINT-A-CON section showing four component boards, four horizontal wiring boards and three vertical wiring boards.

Centrally located plants at Chicago, Illinois; Shelbyville, Indiana; LaPuente, California; St. Louis, Missouri.

Fig. 4—Cutaway showing "short" wires on top side and "long" wires on under side interconnected by an eyelet. This interconnection may also be made by plating through holes which have been punched prior to final fabrication.



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L Network Design (continued from p 186)

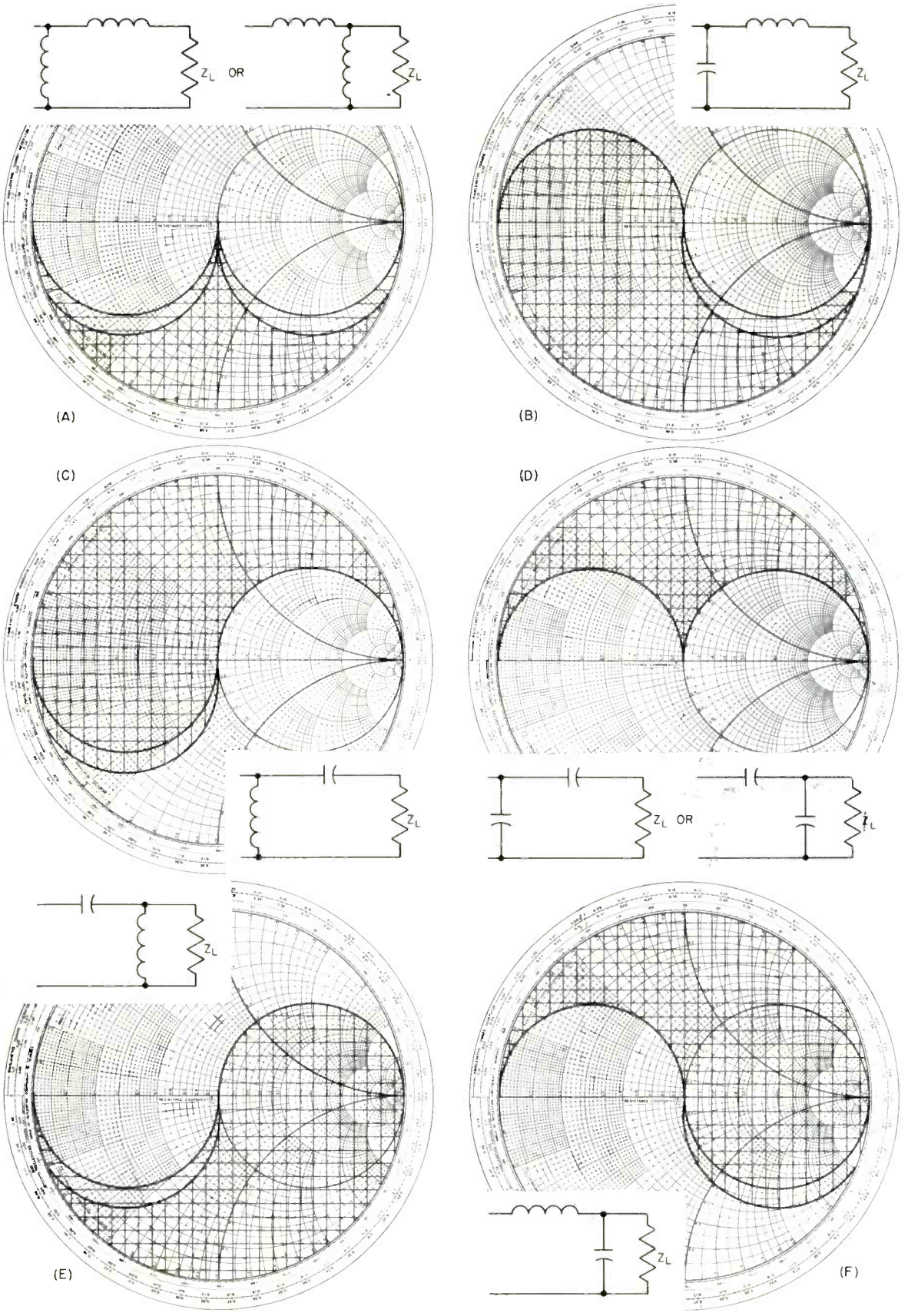
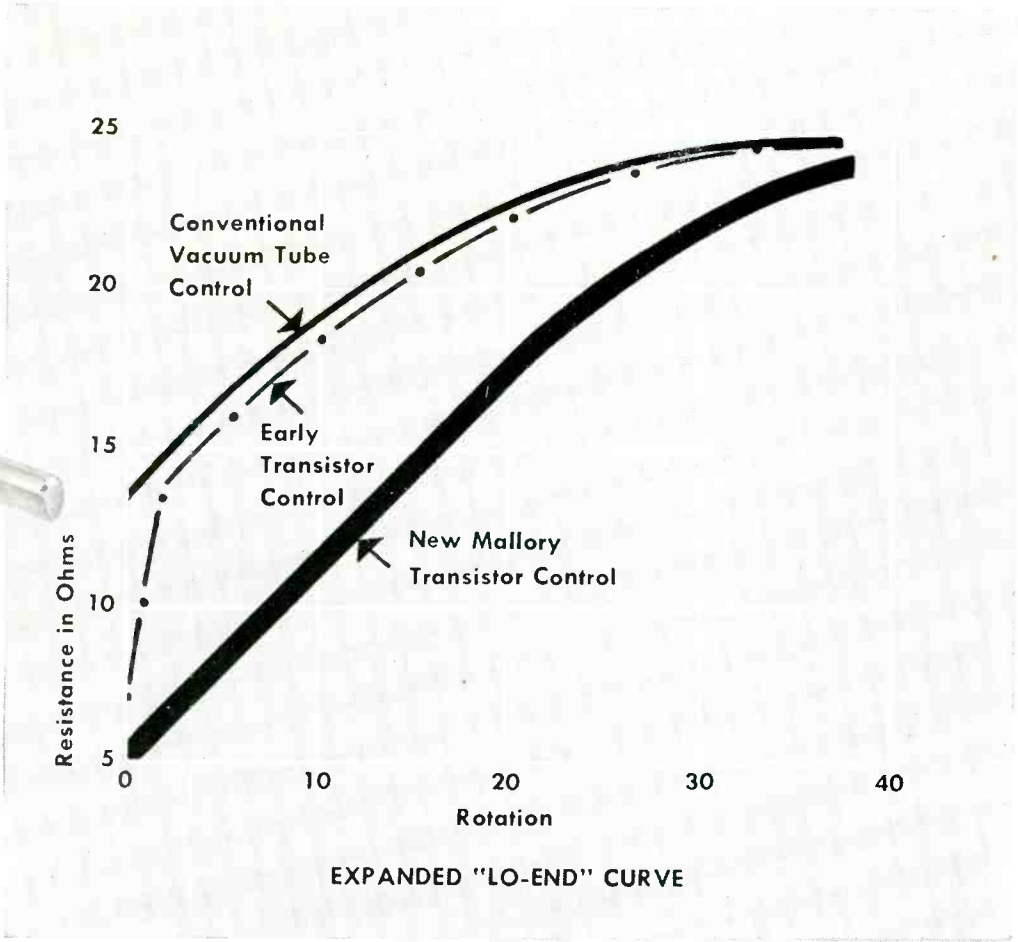


FIG. 2—For each network, horizontally shaded areas on accompanying Smith chart show impedances which may be matched with lossless reactance. Vertically shaded areas may be matched with reactances for which tan $\theta = 0.2$

ELECTRONICS REFERENCE SHEET



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Electrons At Work

Edited by ALEXANDER A. McKENZIE

Satellite Equipment Being Assembled

Electronic circuit package held by Naval Research Lab employee fits into baby-moon shell shown below. Printed wiring typical of that used can be seen on boards at bottom of picture. Eighteen units of this kind are now under construction. They will be launched from three-stage rockets during the International Geophysical Year

Flat Tube Suitable For Color TV

DRASTICALLY cutting the depth required for a television kinescope, a developmental type invented by Denis Gabor may prove to be commercially feasible (ELECTRONICS, p 14, Jan. 1, 1957) for color.

Figure 1 shows the cross-section of the beam. Although they come from three separate cathodes, the color beams merge during most of their transit and only at the end strike the screen at different angles to activate the appropriate phosphor strip at the desired point.

As indicated in Fig. 2, the final bending and scanning takes place as the result of a potential phenomenon. Just behind the scanning array is a metallic plate that acts as a magnetic screen. The scanning array itself comprises about 120 horizontal conducting lines printed upon a flexible insulating base.

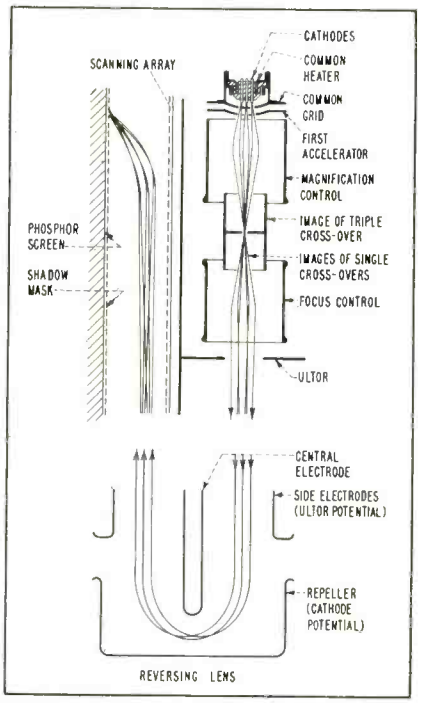

FIG. 1—Principle of self-scanning by the writing beam

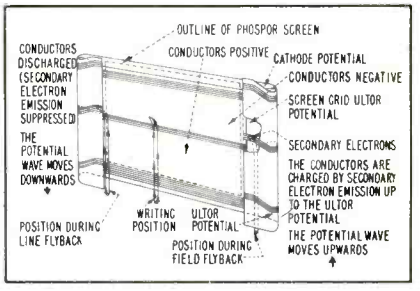

FIG. 2—Printed circuit scanning array

▶ **Printed Lines** — At the sides, where the base is bent, the conducting lines are staggered upwards. In operation, a potential wave travels down this array vertically. Up to a certain level, the conductors are charged to maximum positive potential. Above, there occurs a transition zone of lesser potential. When the beam reaches the transition zone it is bent towards the screen.

When a beam has completed line

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MODEL	Volts	Current	Regulation Line 105-125	Regulation Load 0-Max.	Ripple	Recovery Time*	Stability For 8 Hours	Output Impedance DC-20 ~	Output Impedance 20 ~ –100 KC	Dimensions W	Dimensions H	Dimensions D	Price
2600	0-60	0-2 Amp.	5 Mv.	5 Mv.	1 Mv.	50 μ sec.	10 Mv.	0.002 Ω	0.0005Ω	19"	10½"	17"	$690
2650	0-60	0-5 Amp.	5 Mv.	5 Mv.	1 Mv.	50 μ sec.	10 Mv.	0.001 Ω	0.0002Ω	22½"	28"	19"	$1190

***Good** stability*
***Fast** recovery time*
***Low** output impedance*
***Excellent** regulation*
***Low** ripple*

POWER REQUIREMENTS: 105-125 volts, 60 cycles.
FUSE PROTECTION: Input and output fuses on front panel. Time delay relay is included to prevent unregulated voltage from appearing at the output terminations.

OUTPUT TERMINATIONS: DC terminals are clearly marked on the front panel. Either positive or negative terminal of the supply may be grounded. DC terminals are isolated from the chassis. A binding post is available for connecting to the chassis. All terminals are also brought out at the rear of the unit. Two terminals are mounted at the rear of the chassis to provide for picking up the error signal directly at the load. This connection compensates for the voltage drop in the wires (and ammeter) connecting the power supply to the load.

METERS: Ammeter: 0-2 amperes, 4" rectangular for Model 2600
0-5 amperes, 4" rectangular for Model 2650
Voltmeter: 0-60 volts. 4" rectangular

CONTROLS: Power on-off switch, DC on-off switch, remote error signal on-off switch, coarse and fine voltage controls. The coarse voltage control is a ten turn potentiometer which varies the voltage from 0-60 volts. The fine voltage control is a ten turn potentiometer which varies the voltage 1 volt. The voltage divider network allows a 61 volt variation in output voltage.

*Recovery time is less than 50 microseconds. The excursion in the output voltage during the recovery period is less than 50 millivolts for line fluctuations from 105-125 volts or load variations from 0-to maximum current.

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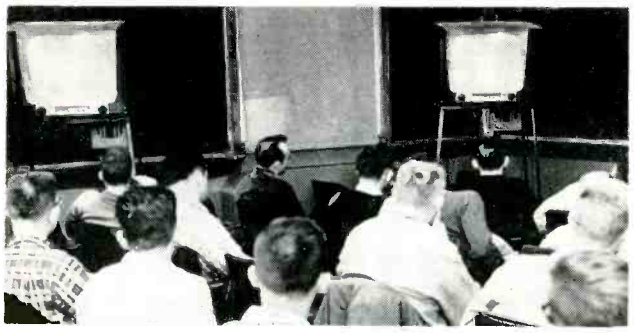
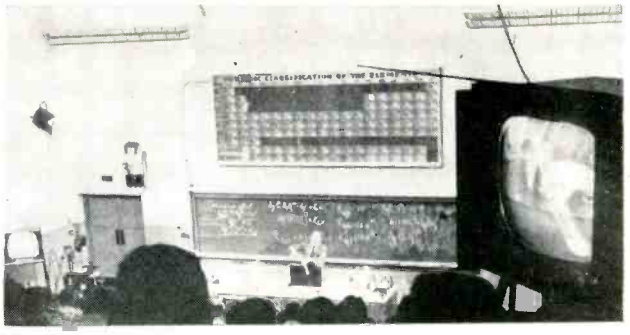
scan, after rapid flyback, it rests in the loop at the left and falls on the conductors in the transition zone. These are partially discharged, moving the zone a little downwards. Since this zone runs down as a wave the lines are self-scanned. With the line stopped and the beam resting in the loop at the right, a screen grid causes the array conductors to charge, the beam creeps up to repeat the cycle.

Television Expands Teaching Staff

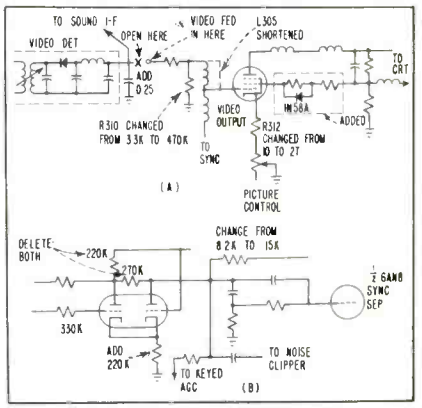




Demonstrations in a general chemistry class are made visible in more detail to those in the rear of the lecture hall as well as to students in other classrooms at Pennsylvania State University

UNDER a grant from the Fund for the Advancement of Education, Pennsylvania State University has been using closed-circuit television to administer a part of their instruction to some 4,700 students in 30 sections of 13 courses.

Original equipment included two Dage dual-camera vidicon television systems. Six 24-inch Westinghouse receivers were modified to accept video from the control console at the receiver video amplifier input.



Connection of video to modified receiver (A) and changes made to Westinghouse receivers to stabilize sync (B)

Sound was carried at r-f on channel 4 to the antenna terminals. To connect the video into the receiver and allow sound to remain unchanged the video amplifier was cut from the detector output and a 1N58A crystal added for d-c restoration as shown at (A) in the circuit diagram.

The agc tube (6AU6) was removed because voltage developed by the strong video signal was sufficient to cut off r-f and i-f tubes

Fuel Injection Triggered By Engine Needs

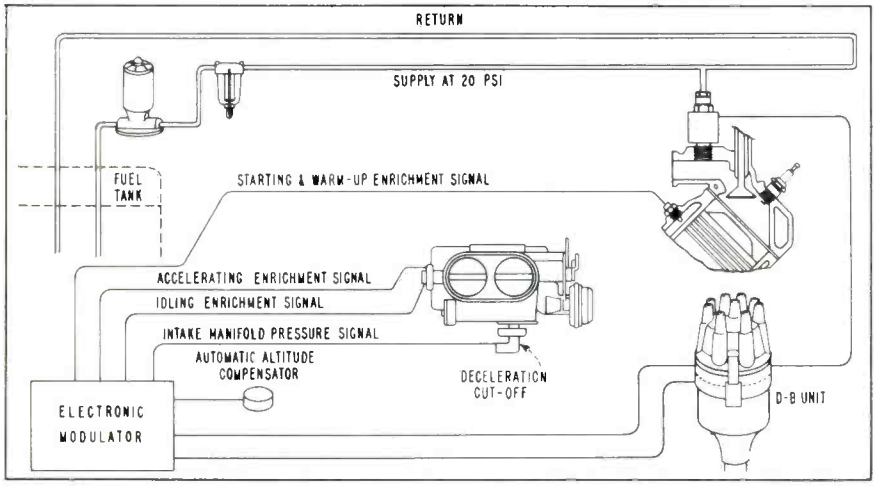


Diagram shows the intercommunication of sensors and controls in Electrojector system

ENGINE needs are automatically sensed as driving conditions vary or as altitude changes. A so-called modulator circuit integrates incoming signals from various sensors, such as inlet manifold pressure, starting enrichment thermistor or acceleration enrichment control. An output pulse varies in width to suit transient engine demands. Pulse current is amplified and distributed to operate fuel injectors. Ignition breaker points are synchronized with injector-timing points to send out spike signals that trigger a multivibrator. In typical tests, brake reaction torque was about 20 ft-lb higher from 800 to 3,600 rpm in a car equipped with the new system as compared with one using a four-barrel carburetor. This system is built by Bendix.

THE FRONT COVER

THE cover picture shows the test setup for 300 feet of line being tested for vswr and attenuation at the Andrew Corp. transmission line testing site. For the vswr measurements, a slotted line was used at each end with readings taken every megacycle over the range. The load was tuned to a vswr of 1.01 or less for each frequency recorded. The vswr of this line is under 1.05 for 300 feet.

Attenuation was also measured on 300 feet of line by shorting the far end and measuring vswr at the generator end. From these measurements, the power rating of the line was calculated. Attenuation and power rating vary from 0.037 db per 100 ft and 350 kw at 100 mc to 0.082 db and 158 kw at 400 mc. Peak power rating for pulse use is in the megawatt range and depends upon pulse length and duty cycle.

The new line has a characteristic impedance of 50 ohms. The inner conductor is supported on Teflon peg insulators. In the photograph, a clamp is being placed on the flange to hold two sections of line together.

and prevent sound from passing through. To stabilize sync, R_{102} was changed to 15,000 ohms and R_{440} and R_{400} removed as shown at (B). A 220,000-ohm resistor was added in series with the cathode of the 12AT7 sync control tube.

However, with an audio-video mixer added to the control room equipment, both picture and sound are used to modulate an r-f carrier on channel 4 and this output is fed through a 72-ohm cable to each room. This arrangement obviates the need for modifying the receivers.

Forty-Meter Transistor Transmitter

POWERED by two flashlight cells, the crystal-controlled transmitter shown in the diagram has been used in the amateur 7-mc band to communicate with stations all over the United States, parts of Canada and the Hawaiian Islands.

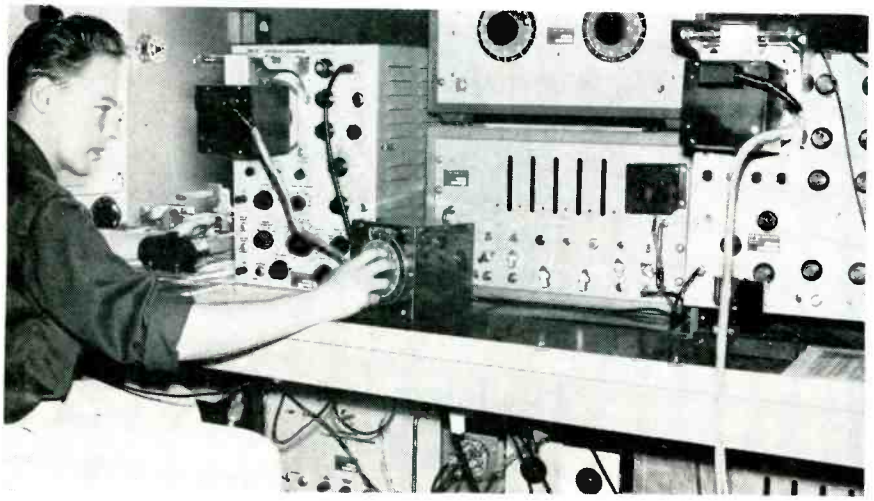
The equipment requires 120 milliwatts input. Several precautions have been taken to insure stable operation. Grounded base is used in the amplifier to reduce feedback, obviating the need for neutralization. The small amount of capacitive feedback is regenerative but no instability has resulted.

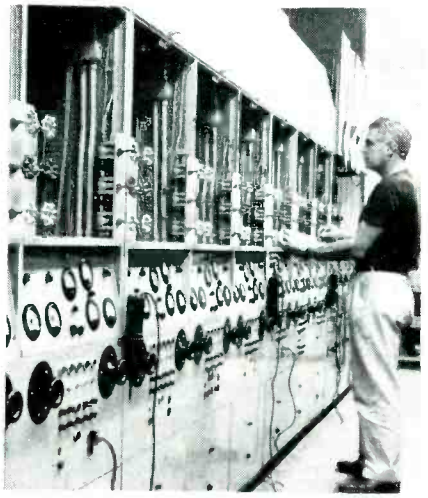
▶**Stabilization** — A minimum resistance in the emitter is essential to temperature stability and to lessen the danger of current runaway, but series dropping resistors are otherwise minimized. Capacitor C_1 is a phasing adjustment to be set at the point of best stable operation of the oscillator under keying. It also permits slight frequency change.

For maximum output, the sbdt transistor can be immersed in a silicone-oil bath or other appropriate means of removing heat. The circuit and equipment described has been operated by Forrest Bigelow, W3FBL, Laverock, Pa. and the information has been furnished by Philco Corp.

(continued on page 196)

Test and Pumping Equipment for Microwave Tubes





Frequency, time and amplitude-jitter tests performed on the equipment at left have reduced measurement time in klystrons from eight man hours to 15 minutes. Elaborate exhaust equipment is used at Litton Industries in San Carlos, Calif. for micro-wave tubes (right)

Transitron

MILITARY type silicon diodes

1N457
1N458
1N459
1N251

TRANSITRON'S Military type silicon diodes are designed to meet the requirements of MIL-E-1, and are characterized by reliability under the most severe operating conditions.

Their subminiature size and rigid specifications make them ideal for a wide range of applications. Types 1N457, 1N458, and 1N459 are intended for low and medium frequency uses, requiring voltage ratings up to 175 V. Type 1N251 is a high frequency diode especially designed for detector and high speed pulse units.

In addition to these four military types, silicon diodes meeting many other application requirements are also available. These include high conductance types, as well as fast switching-high voltage diodes.

Type	Minimum Forward Current at + 1 v (ma)	Inverse Current at Specified Voltage (μa)	Maximum Operating Inverse Voltage (volts)	MIL-E-1 TSS #
1N457	20	.025 @ −60 V	60	1026
1N458	7	.025 @ −125 V	125	1027
1N459	3	.025 @ −175 V	175	1028
1N251 *	2	.2 @ −10 V	30	1023

*Inverse recovery time under .15 microseconds

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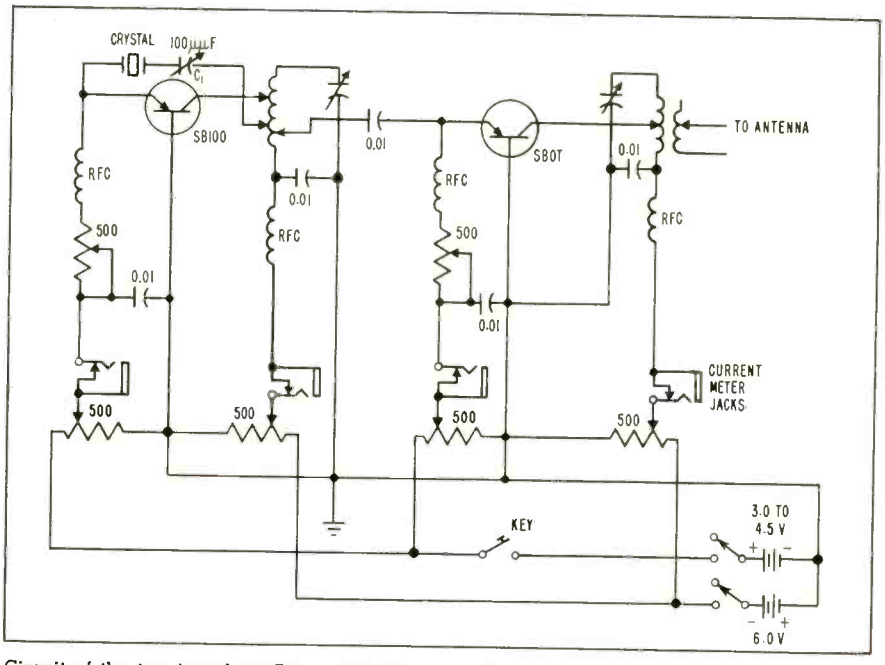
Germanium Diodes Transistors Silicon Diodes Silicon Rectifiers



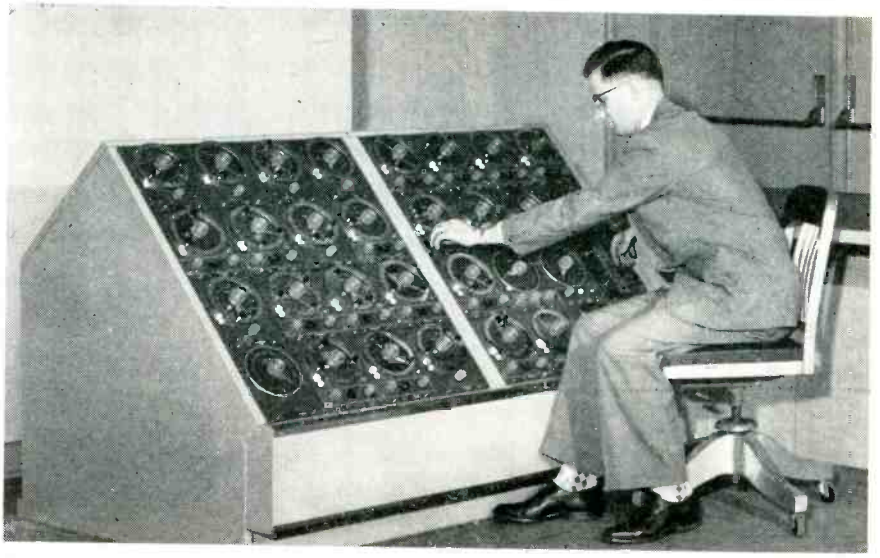
Circuit of the two-transistor 7-mc transmitter described on the previous page

Fork-Driven Dual Tone Standard

By Byron H. Kretzman
Erco Radio Laboratories
Garden City, N. Y.

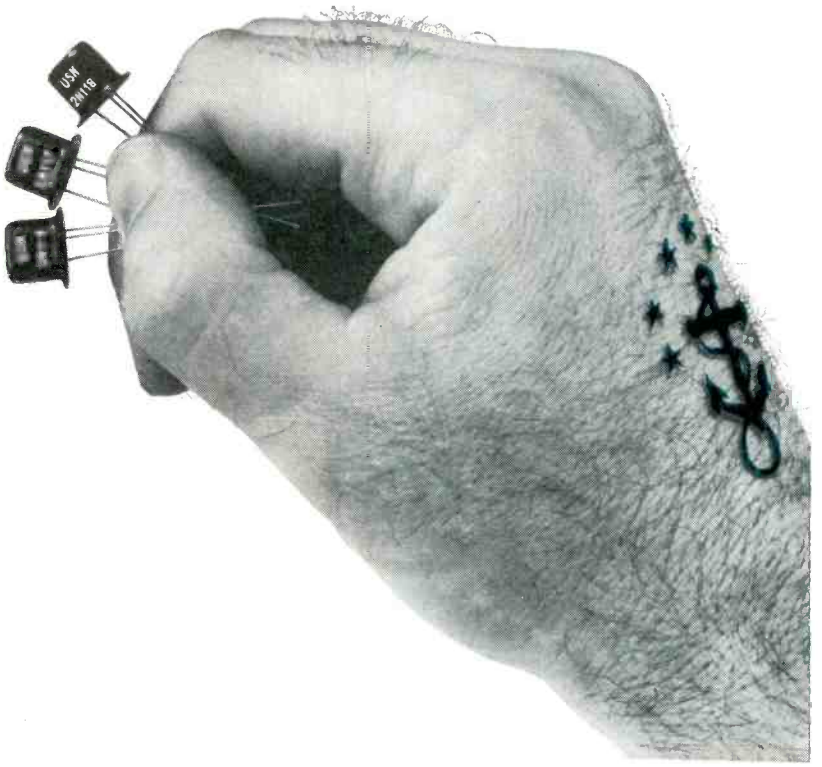
In tuning the selective amplifiers of an a-f type radioteleprinter converter designed for 850-cycle shift, the usual method is to use a tunable audio oscillator as a signal generator. Some means of accurately

Computer Solves Power Dispatch Problem



Principal inputs, such as station costs and constants of the transmission system are set on dials of the automatic dispatch computer shown. Curves corresponding to the combination of units in service are selected. With all other information set in, the operator indicates total required generation. The computer then positions automatically to show optimum dispatch of power for various units of the system. Westinghouse has delivered this unit to West Penn Electric Co.

FIRST silicon transistors meeting NAVY SPECS



For *reliability* under *extreme* conditions... design with TI's military silicon transistors... built to give you high gain in small signal applications at temperatures up to 150°C. Made to the stringent requirements of MIL-T-19112A (SHIPS), MIL-T-19502 (SHIPS), and MIL-T-19504 (SHIPS) – these welded case, grown junction devices furnish the tremendous savings in weight, space, and power you expect from transistorization... *plus* close parameter control that permits you to design your circuits with confidence.

All 20 Texas Instruments silicon transistor types have proved themselves in military use. First and largest producer of silicon transistors, TI is the country's major supplier of high temperature transistors to industry for use in military and commercial equipment.

degradation rate tests for TI's USN-2N117, USN-2N118, and USN-2N119

test	condition	duration	end point at 25°C
lead fatigue	three 90-degree arcs	——	no broken leads
vibration	100 to 1000 cps at 10 G	3 cycles, each x, y, and z plane	I_{CO} = 2 μA maximum at 5V
vibration fatigue	60 cps at 10 G	32 hours, each x, y, and z plane	h_{ob} = 2 μmhos maximum
shock	40 G, 11 milliseconds	3 shocks, each x, y, and z plane	h_{fb} = −0.88 minimum (USN-2N117)
temperature cycle	−55°C to +150°C	10 cycles	h_{fb} = −0.94 minimum (USN-2N118)
moisture resistance	MIL-STD-202	240 hours	h_{fb} = −0.97 minimum (USN-2N119)
life, intermittent operation	P_c = 150 mW, V_c = 30V	1000 hours, accumulated operating time	
life, storage	150° C, ambient	1000 hours	
salt spray	MIL-STD-202	50 hours	no mechanical defects interfering with operation

LOOK TO TI FOR: SILICON HF, MEDIUM POWER, POWER, AND SMALL SIGNAL TRANSISTORS
SILICON DIODES AND RECTIFIERS • GERMANIUM VHF, POWER, RADIO, AND GENERAL PURPOSE TRANSISTORS

pioneer producer of silicon transistors

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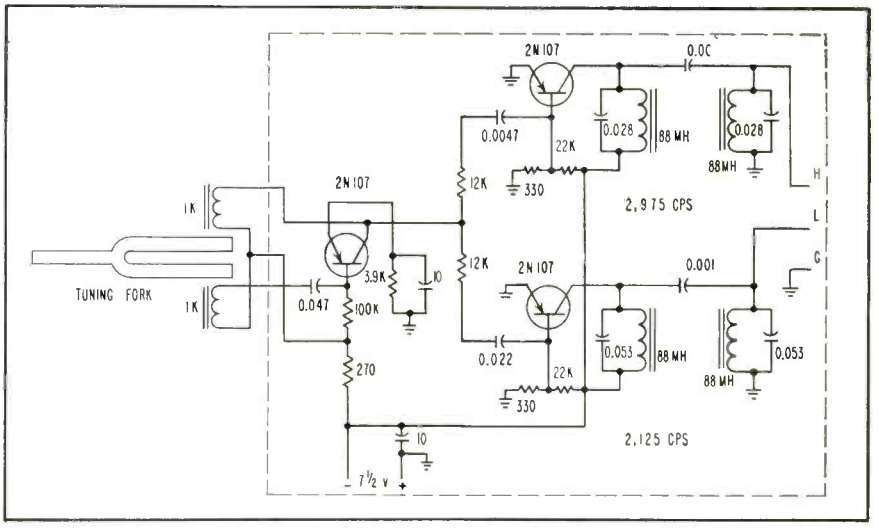


Circuit of the tuning-fork controlled standard with two outputs

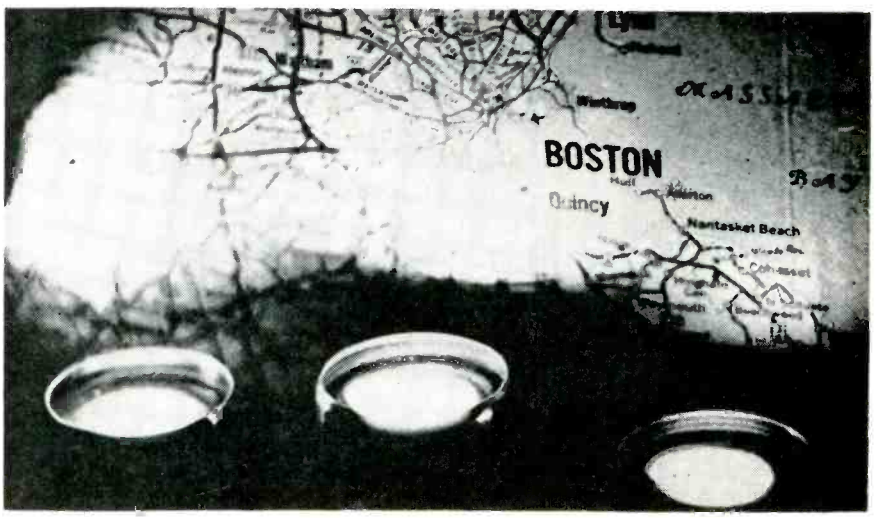
setting the oscillator to either of the standard mark and space frequencies, namely 2,125 and 2,975 cycles, is necessary.

Common practice is to compare the frequency of the tunable oscillator with a 425-cycle tuning fork standard. Lissajous figures on an oscilloscope are then obtained in the 5-to-1 and 7-to-1 ratios as required. This procedure may prove unreliable if the a-f oscillator is unstable. Described below is a fork-driven standard that provides 2,125 and 2,975 cycles directly. Using this standard, it is unnecessary to employ an a-f oscillator or even an oscilloscope to align a converter. Operation is simplified by using transistors and a self-contained battery power supply.

Construction is simplified by using an etched or printed-circuit wiring board. The transistor oscillator is a pulse-generator driven by a 425-cycle tuning fork. Transistor amplifiers tuned to the fifth and seventh harmonics amplify the 2,125 and 2,975-cps components.

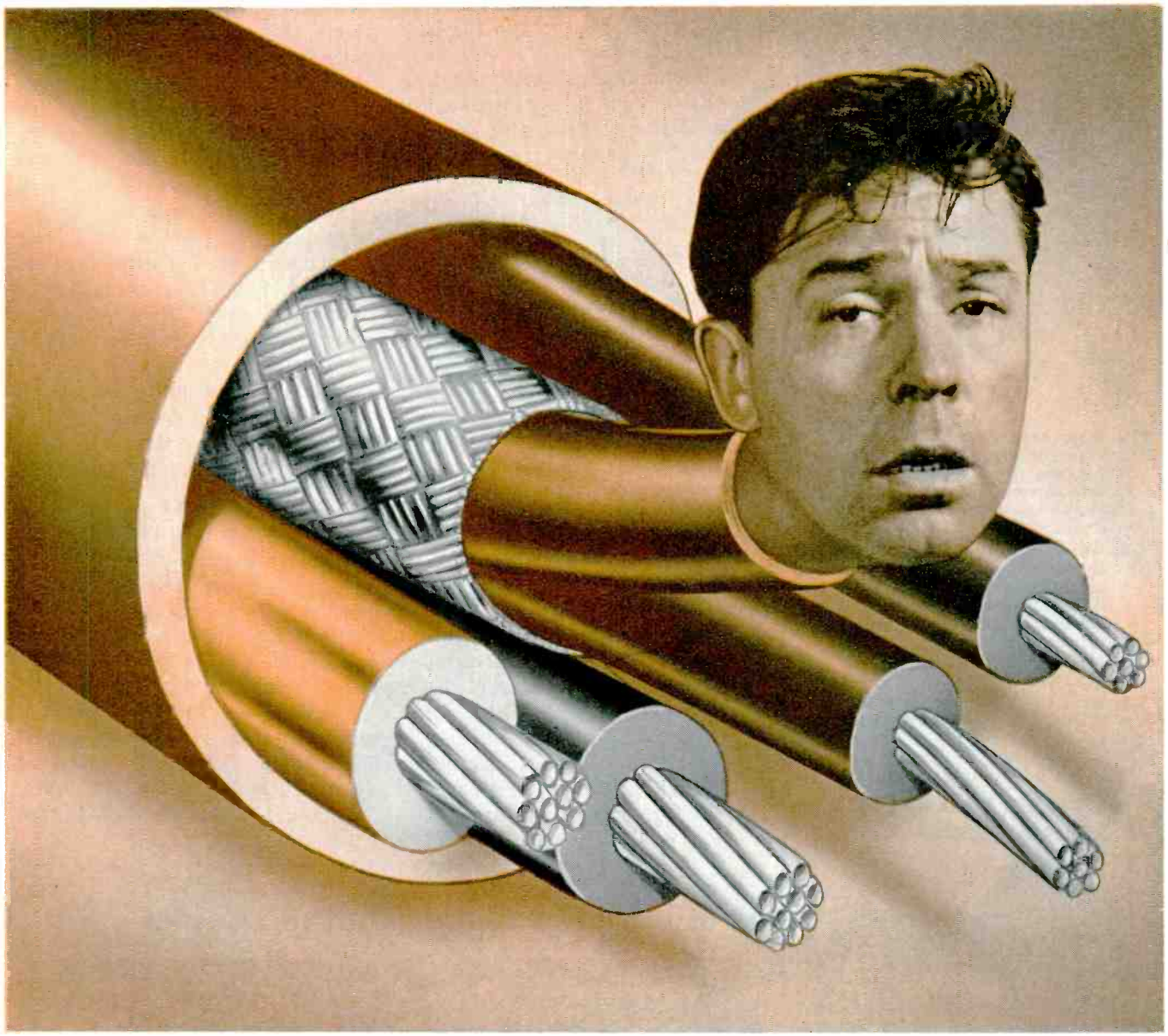
► **Construction** — Physically, the tone standard is built on a 3.5 by 7

Atomic Flashlight Burns Years



Using an essentially nonhazardous radioisotrope, a new type of light source is available in several different colors for dial markers, critical controls and other markings in electronic equipment. The material furnishing the illumination has a half life of about 12 years, according to New England Nuclear Corp., developers. The map shown was photographed in the illumination from three of the new lamps

Got Your Neck Out On A Cable Problem?



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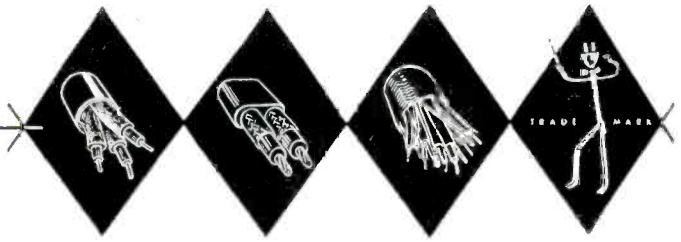
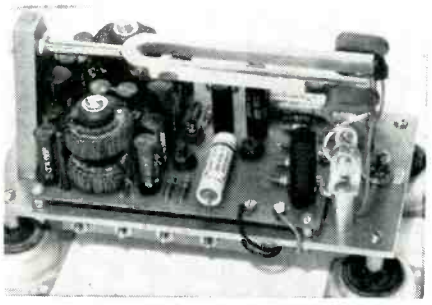


in. aluminum plate, ⅛ in. thick. Steel was avoided to insure a magnetic circuit only through the fork itself. The aluminum plate is mounted on four vibration-isolating shock mounts to prevent mechanical transmission of the tuning fork vibrations to the table.



Complete transistorized dual-tone audio generator operates from a 7.5-v battery beneath the chassis

This treatment was found to be necessary, since the vibrations resounding through the workbench can be both annoying and confusing. A 7.5-volt C battery is clamped underneath the aluminum plate. A control toggle switch is mounted through the plate at one end.

The printed circuit wiring board in 3.5 by 5 in. Screw terminals for the exciting coil connections, battery supply and output were made by tapping, with a 4-40 tap, hollow rivets after they were soldered in place. In laying out the printed circuit, as much copper as possible was left for these screw terminals to reduce the possibility of separating the copper foil from the board while soldering.

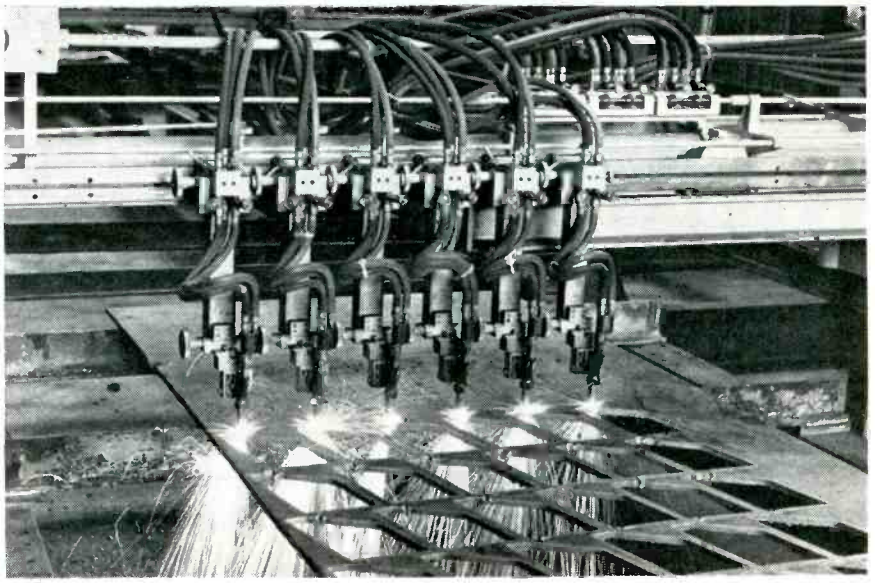
Three holes, properly spaced, were drilled for the transistor leads in an open spot. The leads were not trimmed. Small tubing was slipped over these leads as some of the printed circuit wiring is crossed.

All capacitors, except for the two low-voltage electrolytics, are molded tubulars, made for end-mounting on printed circuit boards. Both leads come out the same end.

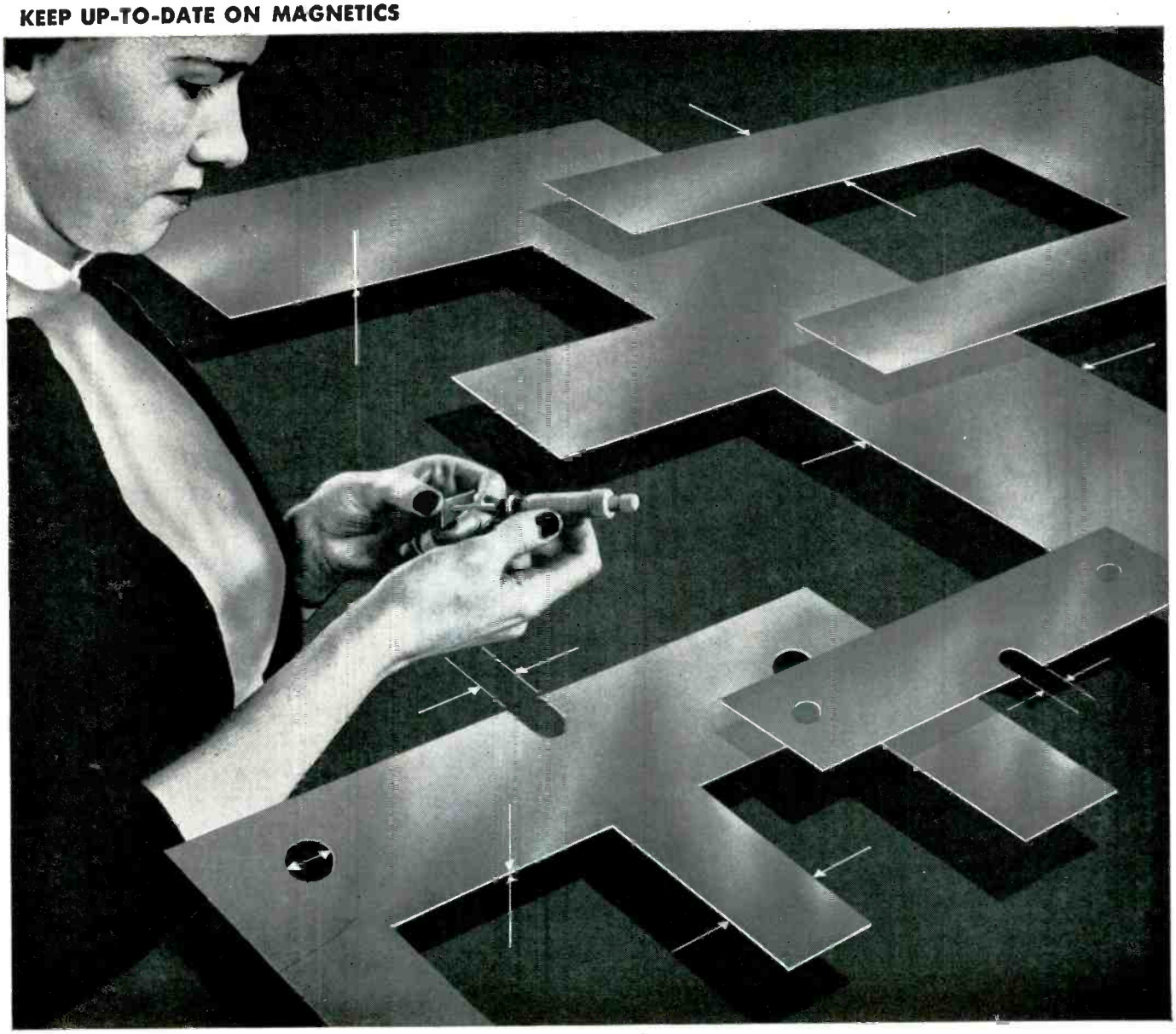
▶ **Magnetic Circuit** — Originally, the standard was a 435-cycle fork. The softer crotch part was notched with a good round file to move the frequency lower, comparing it with another fork of the correct frequency. Not much filing is necessary to move only 10 cycles.

Exciting coils for the fork were obtained from a high-impedance headphone. Each coil measured about 1,000 ohms d-c resistance. Magnetic bias for the fork is sup-

Profile Cutter Makes Multiple Copies



The oxygen cutting machine shown above is half of a double unit that can cut steel plate from ⅛ inch to 15 inches thick from a few square inches up to 10 by 60 feet. A black and white drawing is used as the pattern and followed on the cutter by photoelectric means. The electronically controlled cutter was developed by Messrs. Hancock & Co., Ltd. of Croydon, England



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Now everyone "hydrogen" anneals—but not everyone *dry-hydrogen* anneals. You can't use bottled hydrogen, without leaving a surface oxide injurious to magnetic properties and making soldering virtually impossible. So we dry our hydrogen to a dewpoint of —60° C, removing the water vapor which is produced by the reduction of hydrogen. Carbon reduces to methane, sulphur to sulphur dioxide, and both are removed by the continuous flow of dry hydrogen during the 24-hour cycle.

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MAGNETICS inc.

CABLE: MAGNETICS

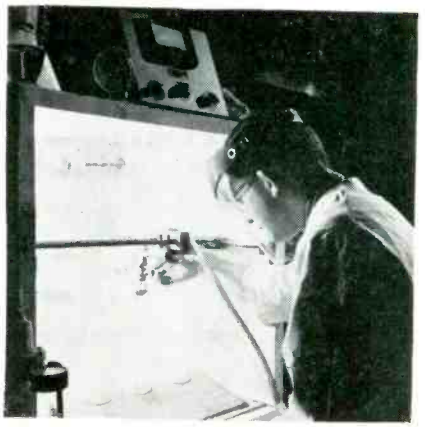
plied from a ½-in. round by ½-in. long permanent magnet from a small a-c/d-c set speaker. Hex-head ¼-20 steel bolts were soldered to each end of the magnet to extend the magnetic circuit to the coil pole pieces. An air gap of about 64-in. is between each of the pole pieces and the tines of the fork. The handle of the fork was threaded with a ¼-28 die and bolted to a triangular mounting bracket.

▶ **Electrical Circuit**—The oscillator uses a 2N107 *pnp* transistor. The circuit is that of a pulse generator whose repetition rate is controlled by the mechanical resonance of the tuning fork. Resistance-capacitance coupling is used to couple to the amplifiers, each of which also uses a 2N107 transistor in a grounded-emitter circuit.

Toroidal inductors paralleled with capacitors tune each collector output circuit to the correct harmonic. Each collector circuit, in turn, is capacitance coupled to another similar tuned circuit to further peak the desired frequency.

With the nominal 88 mh toroids used, it was found that approximately 0.053 μf was required for resonance at 2,125 cycles. At 2,975

Luminous Panels



Enameling steel coated with a mixture of ceramic and phosphor, a tin salt solution and then a transparent conducting surface of a tin compound forms the basis of Sylvania's Panelescent lamps. Sheets 0.02-inch thick are cut to desired shapes and processed with several coatings and firings. Light is produced through the phenomenon of electroluminescence

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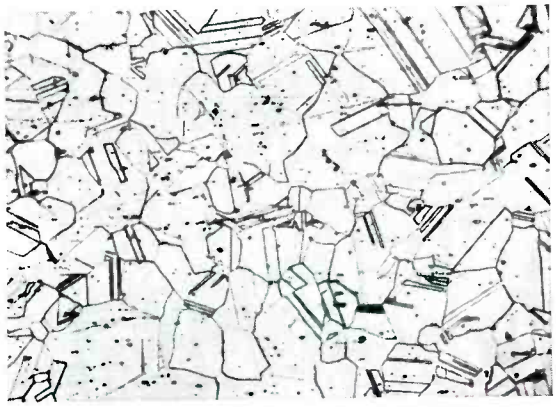
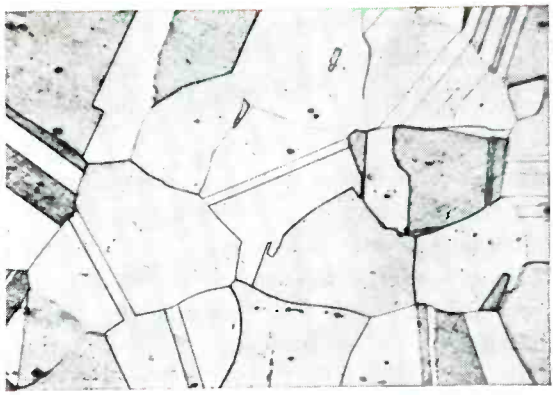
3. Complete elimination of gas, not from the surface only but from the entire mass. Alloys so produced are therefore more desirable in the manufacture of electron tubes.

4. General improvement in electronic, electrical, and mechanical properties to meet specifications. Because closer control of analysis is a primary advantage of vacuum melting, we can now achieve these specific improvements with remarkable certainty.

Almost all of the Driver-Harris Alloys now vacuum melted and processed under close physical and analytical control show improvement in one or more of the above ways. If you are seeking further improvements in the D-H Alloys you use, inquire now for information on how Driver-Harris Vacuum Melting Service can help you. Address your inquiry to Dept. VMS.



Polished and etched sample of Air Melted NICHROME V in annealed condition.*



Vacuum melted NICHROME V, annealed. Note that reduced inclusions result in much larger grain size for the same annealing treatment.

*T. M. Reg. U. S. Pat. Off.

Driver-Harris COMPANY HARRISON, NEW JERSEY

BRANCHES: Chicago, Detroit, Cleveland, Louisville, Los Angeles, San Francisco In Canada: The B. GREENING WIRE COMPANY, Ltd., Hamilton, Ontario

MAKERS OF THE MOST COMPLETE LINE OF ALLOYS FOR THE ELECTRICAL, ELECTRONIC, AND HEAT-TREATING INDUSTRIES

cycles, approximately 0.028 μf was required for resonance.

Output is high impedance, in the order of two to three volts rms. Distortion, measured at 2,125 and 2,975 cycles is less than 3 percent, which is a usable value. By careful selection of the capacitors tuning the toroids to resonate the circuits as closely as possible, distortion could be further reduced to less than 1 percent.

Loading the output circuit increases distortion. Wherever possible, coupling to the amplifier being aligned should be to a grid, through a blocking capacitor.

Audio Clipper Extends Coverage

BY R. B. SEALS
Engineer
Collins Radio Co.
Dallas, Texas

AIRLINE services operating outside the continental U. S. and a few within desire the additional range that the Collins 17L4 transmitter might give if the average percentage of modulation were maintained at a reasonably high level. To extract maximum communications ability from the transmitter an audio clipping and filtering circuit has been designed for addition to the equipment.

The unit for which the circuit is shown in Fig. 1 employs two Texas Instruments, type 601C silicon diodes in a biased clipping circuit

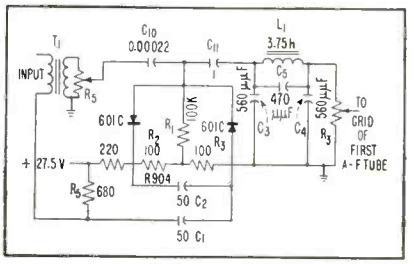
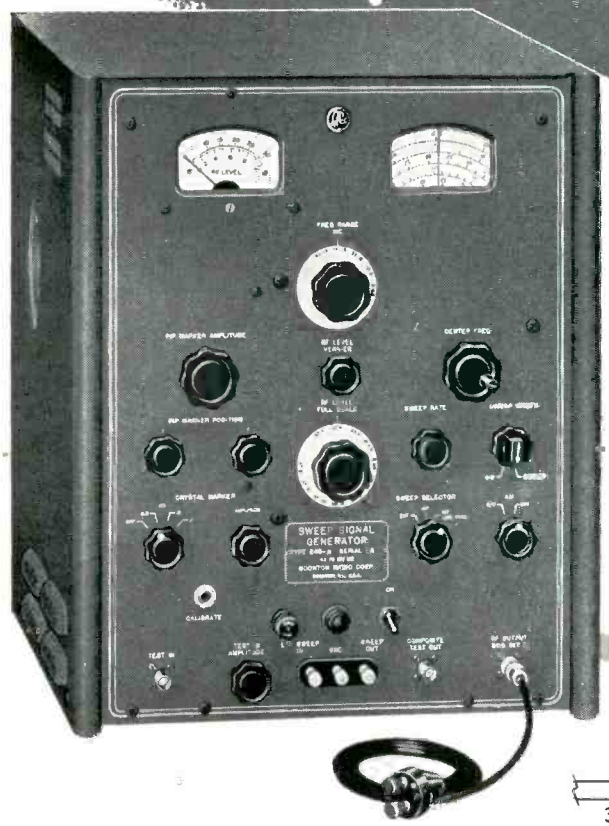


FIG. 1—Circuit diagram of the clipper

operating from the high impedance secondary of the microphone transformer T_1. Biasing voltages are obtained from the primary 27.5-volt bus and dropped to proper voltage by a divider network made up of R_1, R_2 and R_3. Filtering is ac-

Sweep Frequency Coverage

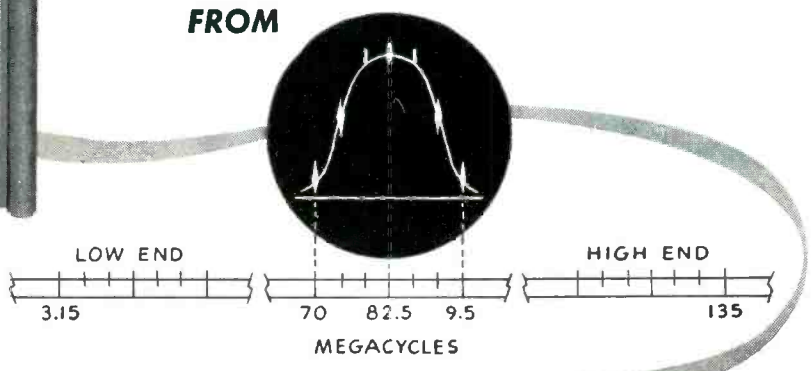


with this

BRC SWEEP SIGNAL GENERATOR

Type 240-A

having Crystal-Referenced Birdie-Type Markers and two individually controlled Pip Interpolation Markers



USE THIS SWEEP GENERATOR FOR

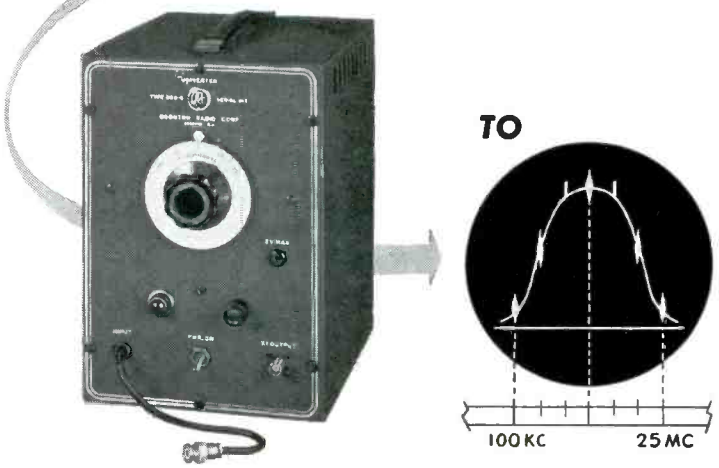
(1) The determination of selectivity and sensitivity of test circuits,
(2) The study of band-pass characteristics,
(3) The adjustment of stagger tuned circuits,
(4) The determination of linearity of FM discriminators, and
(5) The study of crystal modes.

Features include (A) Crystal-Referenced Birdie-Type Markers, (B) Adjustable Pip-Interpolation Markers, and (C) A composite signal containing the markers added to the response of the system under test. Provisions have also been made for operation as a C.W. or A.M. Signal Generator.

CENTER FREQUENCY: 4.5 MC to 120 MC, accurate to ±1%, continuously variable in five self-contained ranges. Output frequencies are fundamental oscillations.

SWEEP WIDTHS: Continuously variable from ±1% to ±30% of center frequency or ±15 MC, whichever is smaller.

PRICE: $1375.00 F.O.B. Boonton, New Jersey



TYPE 203-B UNIVERTER

This accessory, a frequency converter having unity gain, effectively extends the low-frequency range of the Type 240-A Sweep Signal Generator down to approximately 100KC.

PRICE: $345.00 F.O.B. Boonton, New Jersey

BOONTON RADIO CORPORATION
Boonton, New Jersey

Want more information? Use post card on last page.

complished by R_1 and C_9, a 50-μf tantalum capacitor, which also serves to produce a low impedance bias source at audio frequencies.

A coupling network from T_1 to the clipping diode and thence to the audio filter is made up of C_{10} and C_{11}. These capacitors serve for d-c blocking and also modify the frequency response of the system by rolling off the lows. Frequency response that is down approximately 10 db at 300 cps reduces distortion at low harmonic frequencies that cannot be filtered in the output filter.

The output filter made up of L_1, C_3, C_4 and C_5 comprises two m-derived half-sections with m set equal to 0.6 and cutoff frequency

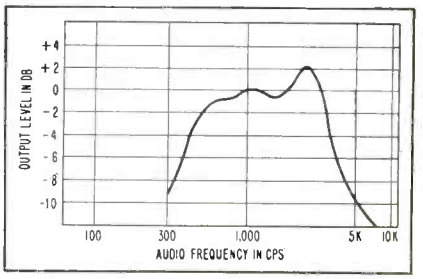


FIG. 2—Output level versus audio frequency

selected at 3,750 cps. The compensation of the coupling net and the filter produces the frequency response shown in Fig. 2.

The input variable potentiometer R_5 is used to set the a-c voltage level at that point and can thus determine the input voltage that will overcome the bias and produce clipping. The variable output potentiometer R_3 is used to set the a-c voltage level to the grid of the first audio tube and thus determines the modulation level.

Operating parameters are selected so 0.2 volt a-c rms at the input to the microphone transformer will just produce the 5 v a-c rms at the grid of the first audio tube necessary to produce 95-percent modulation. At these levels the clipper is just beginning to clip. Any increase in level above the 0.2-v a-c input thus may be clipped proportionately.

By appropriate adjustment clipping in the order of 6 to 8 db is produced by the output of a typical

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New TDI Type 1202A Voltage Controlled Oscillator*

Actual Size of Unit (Height: 3⅛", Width: 1 15/16", Depth: 1 1/16", Weight: 8 ounces).

*Pat. Pending

This new TDI voltage-sensing subcarrier oscillator weighs in at only 8 oz.—is approximately one-half the size of previous oscillators—contains only two tubes, compared to present day five-tube circuits—but these are no indication of its outstanding performance! Reliability under typical (and that means extreme) environmental conditions is nothing short of amazing.

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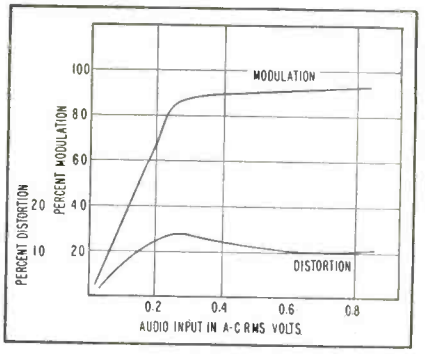


FIG. 3—Modulation percentage and distortion vs 1-kc audio input

carbon microphone. The frequency response of the transmitter audio system, with the clipper-filter unit installed, is ± 10 db of 1,000 cps response from 300 to 3,000 cps. Distortion does not exceed 15 percent throughout the operating frequency of 300 to 3,000 cps. Figure 3 indicates modulation percentage and distortion vs input voltage that points out the clipping thresholds and the amount of clipping available at various input voltages.

Nike Hercules Guidance

AUGMENTING defense installations already existing around many American cities, equipment for use by Army Ordnance in the Nike Hercules program is now coming off production lines.

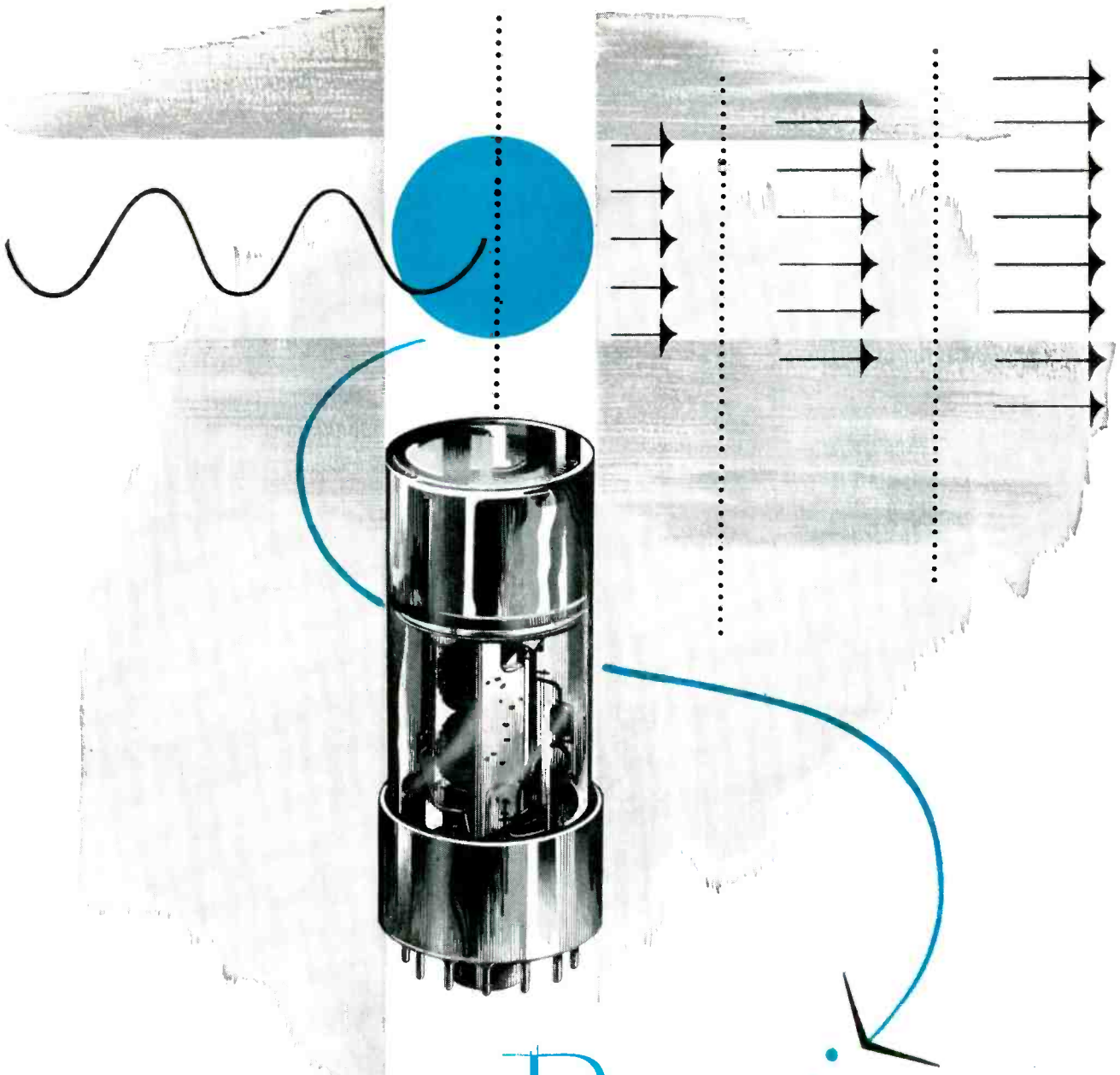
The first set of ground guidance equipment has just been released from Western Electric's Burlington, N. C. plant.

Field Direction Oscillator

BY FRED M. LEWIS
Fairchild Aerial Surveys, Inc.
AND ALLAN R. RADER
Herbert E. Hill Advertising
Los Angeles, Calif.

EXPERIMENTS on an electromagnetic device utilizing transfer of energy between coils that are magnetically perpendicular appear to show a wide range of potential applications including distortion-free magnetic amplification.

Called the field direction oscillator, the device has a core in the form of a hollow toroid. Outer (toroidal) and inner (annular) coils are interlocked such that the



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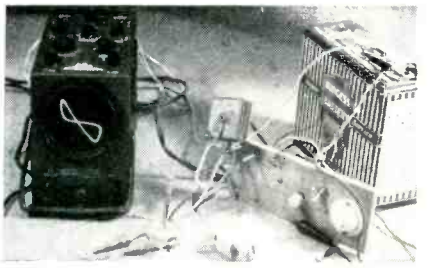
two magnetic fields generated when the coils are energized separately are perpendicular to each other at all points. When one of the two magnetically perpendicular coils is energized with a-c and the other



Experimental equipment used in making studies on field direction oscillator

with d-c, the resultant magnetic field appears to oscillate in twist.

Core and windings are shown in Fig. 1A and the directional dotted curve of Fig. 1B suggests the instantaneous pitch and polarity of an arbitrary resultant field. Pitch is determined by the ratio of input ampere-turns in the perpendicular coils. Polarity is determined by the combination of polarities of the perpendicular inputs.

When the toroidal winding is energized with unbiased a-c and

One-Day Memory

Naval Research Lab scientist Franklin H. Harris holds memory tube capable of storing a radar map or other electronic display for hours. Denominated by its inventor as a REO (regenerated electrical output) the storage device has been developed primarily for military use and is not available commercially

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- No moving parts, assuring long equipment life and reliable operation

Polarad **Model ESG** Microwave Sweep Generator makes possible rapid, dynamic testing of broadband and narrowband microwave systems and components. Its operation is completely electronic, eliminating the need for point-by-point measurement. An integral variable r-f attenuator is provided with each microwave oscillator unit, and the r-f power output level is continuously monitored. This versatile instrument may be used for fixed frequency measurements. Frequency is read directly on face of meter.

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SPECIFICATIONS

Basic Unit: Model E-B

MODEL	FREQUENCY RANGE	POWER OUTPUT
Model E-L1	1000 to 2,000 mc	80 to 1000 mw
Model E-L2	1600 to 3,200 mc	80 to 1000 mw
Model E-S1	2000 to 4,000 mc	80 to 800 mw
Model E-C1	3600 to 7,200 mc	25 to 400 mw
Model E-C2	4800 to 9,600 mc	20 to 150 mw
Model E-X1	6500 to 11,000 mc	20 to 100 mw
Model E-X2	7500 to 15,000 mc	15 to 40 mw

Sweep Width: Continuously adjustable to full frequency range of Microwave Oscillator Unit in use.

Sweep Rate: 60 cps

Internal Modulation Rate, during Sweep Operation:
(a) 1000 cps square wave. (b) 456 kc square wave.

Modulation capabilities, during non-swept Operation:
(a) 1000 cps square wave. (b) 456 kc square wave.
(c) External modulation.

Output when modulated with external pulse:
(a) Pulse rise time less than 0.15 microsecond.
(b) Minimum pulse width less than 0.3 Microsecond.

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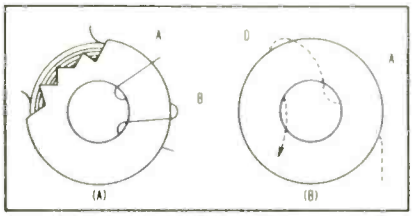

FIG. 1—Toroidal and annular windings (A) when properly excited produce twisted field (B)

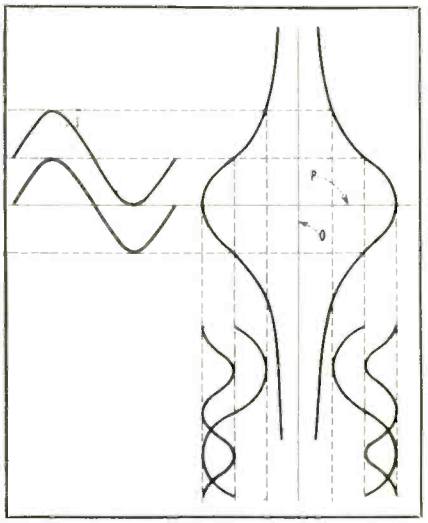

FIG. 2—Effect of applying a-c to one winding and control d-c to another

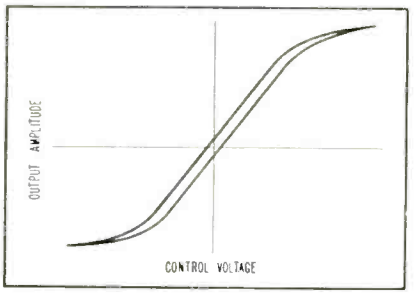

FIG. 3—Output amplitude versus control current

control direct current in the annular winding is zero, the induced field oscillates in intensity and polarity, retaining an annular orientation and no signal will be induced in the annular output winding.

But with appreciable control d-c applied, a-c with double frequency will be induced in the output coil as shown in Fig. 2. Illustrated are two cases of exciting a-c, one unbiased, the other biased to eliminate frequency doubling. Likewise shown are two conditions of control d-c having equal magnitude and opposite polarity.

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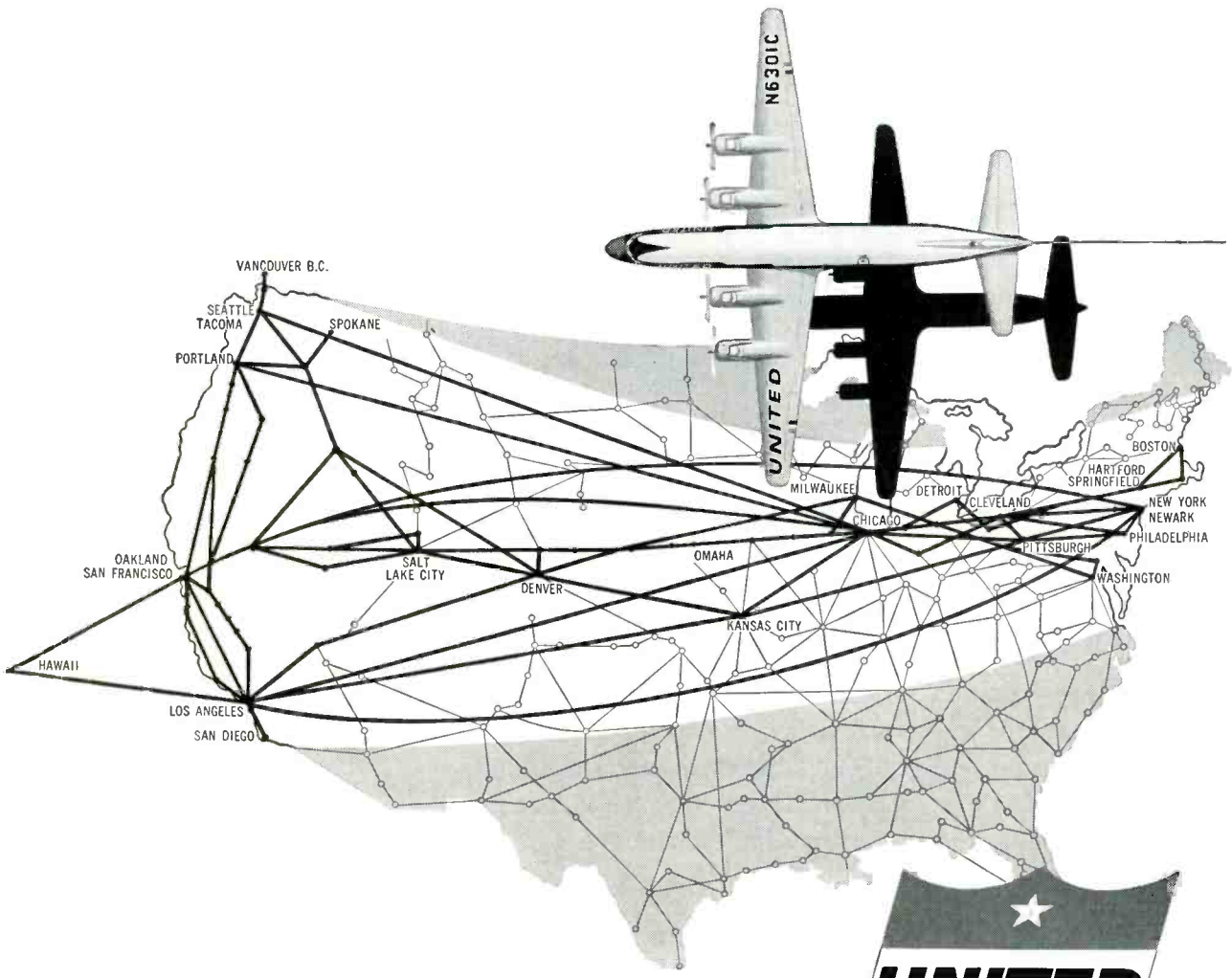

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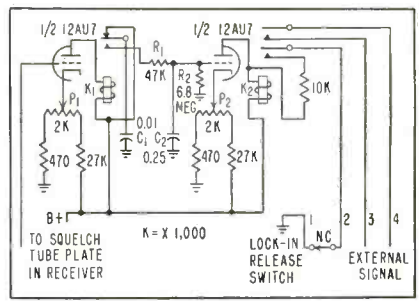
considered, the qualitative prediction of output amplitude versus control current takes the from shown in Fig. 3. Besides its use as a modulator, the device can also be used as a variable inductance.

Mobile Communications Impulse Signaling

By A. E. Olson

Nor-Cal Tele-Radio System
Eureka, Calif.

Need arises at times for the driver of a mobile radio unit to signal a base station whose operator may not be monitoring all calls, as in an industrial system, where mobile units normally talk only to each other, with the base station operator performing other duties. The equipment described will enable a mobile unit operator to signal the base station operator by pressing his microphone button 4 or 5 times in rapid succession. This will operate a relay to sound a bell or other

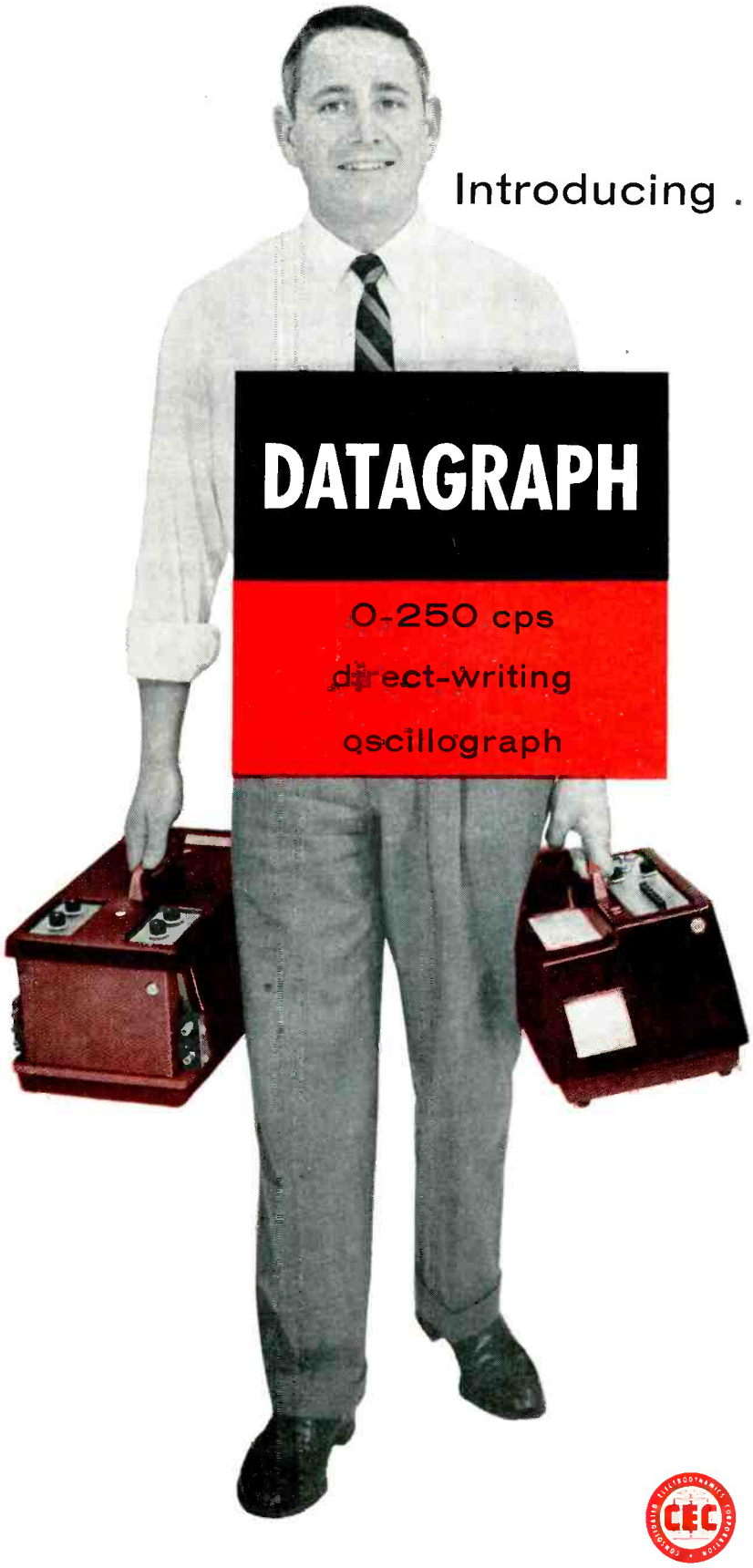


Circuit of the impulse signal device that operates from receiver squelch tube plate

signal. Provision is made to lock in a circuit indicating the receiver alarm is actuated. This is particularly helpful if multiple receivers are used.

▶**Squelch Actuated**—The method of operation is to connect a load to the receiver squelch tube plate. This will operate K_1 through the first triode section. Each time this relay operates C_1 receives a charge from the B plus bus and discharges it through R_1 into C_2.

Values are chosen such that four rapid squelch breaks will transfer from C_1 to C_2 sufficient voltage to operate relay K_2 in the second tri-



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WHERE CAN YOU USE IT? Datagraph can be used to record voltages from many sources . . . e.g., magnetic-tape playback units, carrier amplifiers, audio amplifiers, d-c amplifiers, telemetering discriminators, etc. Its high input impedance adapts it to a myriad of input devices.

WHAT ARE THE SYSTEM SPECIFICATIONS?

FREQUENCY RESPONSE....flat ±5% from 0 to 250 cps.

RECORD SPEEDS.....0.05, 0.2, 1, 5, 10 and 20"/sec.

NUMBER OF CHANNELS....2

RECORD SIZE.....70 mm x 500 ft.

AMPLIFIER INPUT IMPEDANCE .....100,000 ohms

SENSITIVITY .....1 inch per volt; 1 inch maximum peak-to-peak amplitude

DIMENSIONS AND WEIGHT:

Oscillograph .....9" x 10½" x 17¼", 60 lbs.

Amplifier .....9" x 10½" x 17¼", 50 lbs.

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ode circuit. This relay will signal by a device connected to terminals 3 and 4 that a call has been received.

Normal operation of the receiver with single squelch breaks now and then will not operate the device, since the energy transferred at a slow rate from C_1 into C_2 is dissipated too rapidly by R_2 for the second tube to reach the point of relay closure. Potentiometers P_1 and P_2 adjust tube operation for satisfactory relay performance in the two circuits.

If it is desirable to provide a lock-in on the circuit, a normally closed switch is connected to terminals 1 and 2. Pressing this switch will restore the circuit to normal.

Integrating Circuit For Direct Recorder

By W. E. Gilson and John Andrea
Department of Medical Electronics
University of Wisconsin Medical School
Madison, Wisconsin

In cardiovascular research it is customary to use a planimeter to measure blood-pressure tracings to obtain an approximation of the mean pressure. Recent introduction of an integrating circuit in the carrier-amplifier strain-gage channel of rectilinear and ink writing polygraphs has eliminated the need for this measurement, as it averages the pressures of several cardiac cycles.

The following circuit modification for application to the Sanborn direct writing instrument is pre-

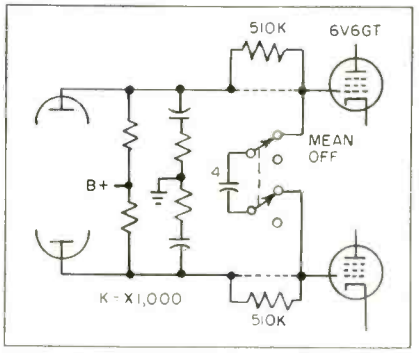

FIG. 1—Circuit modification of Sanborn strain-gage amplifier to obtain mean pressure reading

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APPLICATIONS: Electronic, medical, geophysical, chemical, metallurgical research and development . . . transistor production and circuit design . . . thermocouple calibration . . . null detector . . . recorder driver amplifier . . . and as a general purpose laboratory instrument wherever dc voltages and currents are measured or amplified.

SPECIFICATIONS

Voltage Range (full scale)	100μv to 1000v
Current Range (full scale)	100μμa to 100 ma
Input Impedance	10 megohms below 10 mv, 30 megohms at 30mv, 100 megohms above 30mv
Impedance Accuracy	±1.5%
Accuracy on All Ranges	±3% of full scale
Maximum Gain as Amplifier	80 db ±1.5%
Output Rating	1v across 1000Ω
Output Impedance	less than 5Ω
Drift (after 15 min. warmup)	10μv equivalent input
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FIG. 2—Pressure curve shows effects of integration

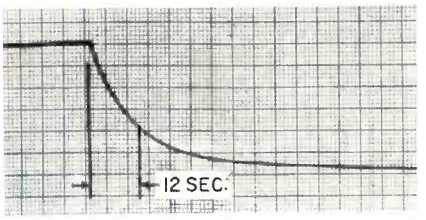


FIG. 3—Recorder chart shows 12-sec response time

sented here for possible use by others.

The circuit changes consist of placing a 4-μf 600-v oil-filled capacitor across the grids of the power output stage after inserting 500,000-ohm series grid resistors. This modification gives a time constant of about 12 seconds and is shown in Fig. 1. A pressure recording and the mean pressure record obtained with this circuit are shown in Fig. 2 while Fig. 3 shows the time constant obtained.

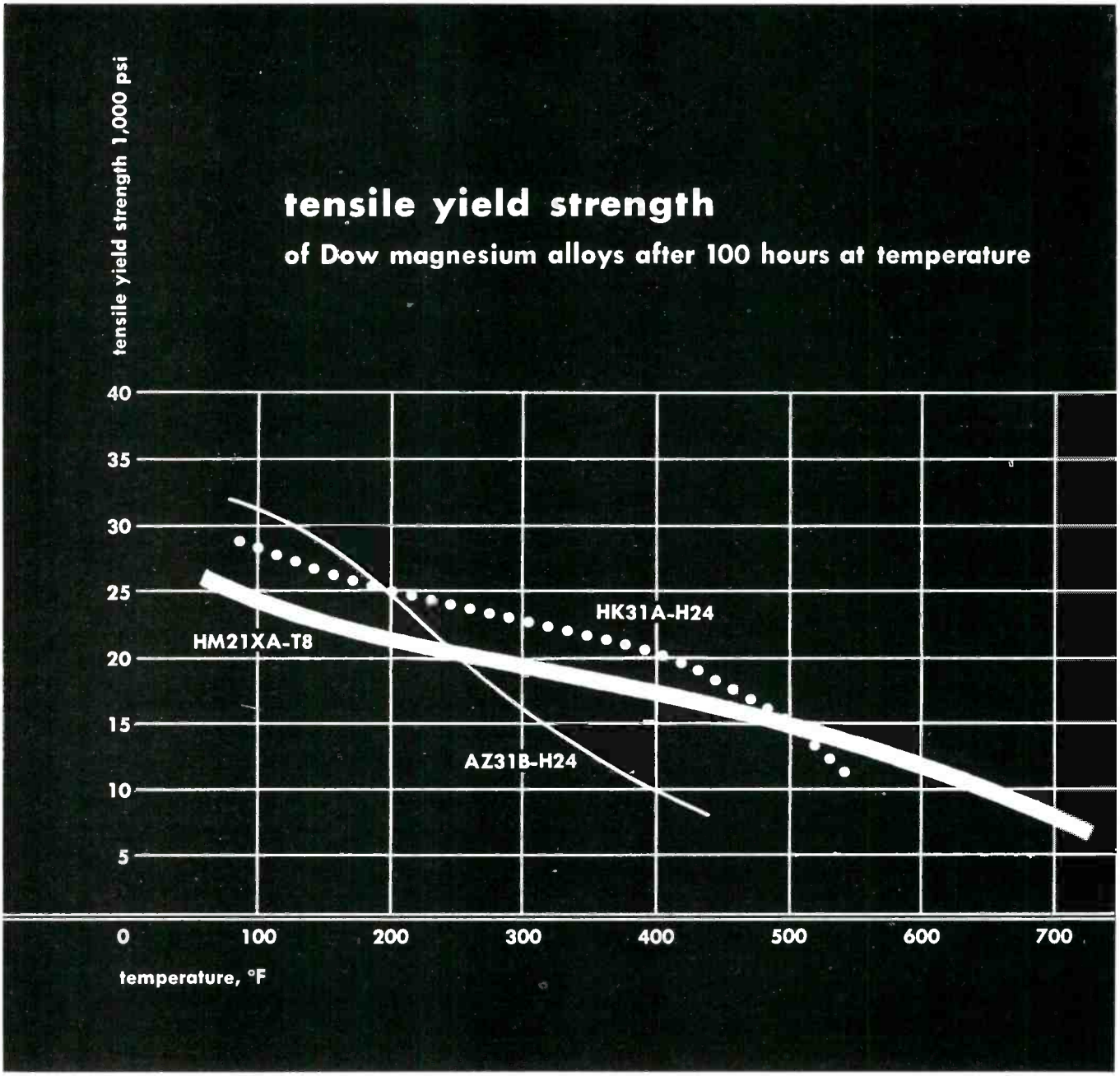
Transistor Tuned Oscillators

By H. L. Armstrong

National Research Council
Ottawa, Ontario
Canada

For transistor oscillators, as for those using vacuum tubes, it is convenient in the lower frequency range to use resistors and capacitors as the frequency-determining elements. The possibilities include the feedback oscillator, using a two-stage amplifier with feedback through a network whose transmission peaks at the desired frequency. The phase shift oscillator uses a one-stage amplifier with feedback through a network that produces a phase reversal at the desired frequency.

While the networks used in vacuum-tube oscillators may be applied directly to transistors, they are often not the most advantageous. With tubes, the networks work from a fairly high output



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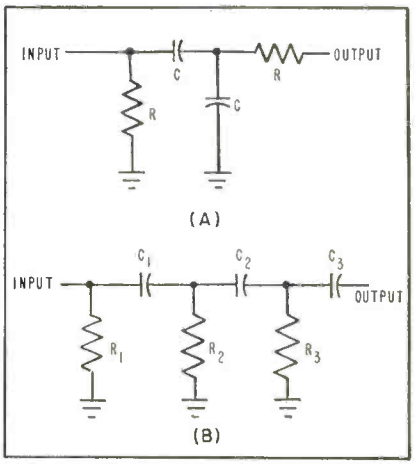

FIG. 1—Network used for oscillator (A) peaks transmission at desired frequency while network with phase reversal is shown at (B)

impedance into a very high input impedance. With transistor circuits they work from a fairly high output impedance into a low input impedance. Thus, for transistor circuits, it is advantageous to consider, not the voltage, but rather the current transmission of the networks.

Figure 1A shows a network whose current transmission, when it works out of a very high impedance into a very low impedance peaks at the frequency $f = \frac{1}{2\pi_{CR}}$, at which frequency the phase shift is zero. Figure 2 shows a two-stage feedback oscillator using this network. One resistor of the feedback network serves also as the load resistor for one transistor.

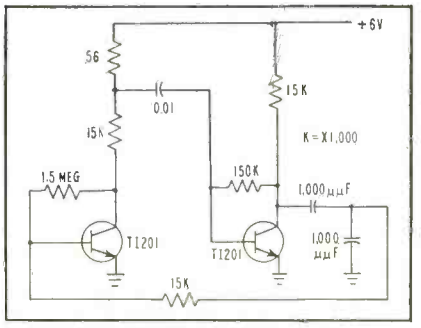

FIG. 2—Two-stage feedback oscillator uses network shown in Fig. 1A

The resistors between the collector and base on each transistor provide bias current. This manner of obtaining the bias provides a measure of stabilization for the circuit. The actual frequency is about 10 kilocycles; the difference between this and the theoretical

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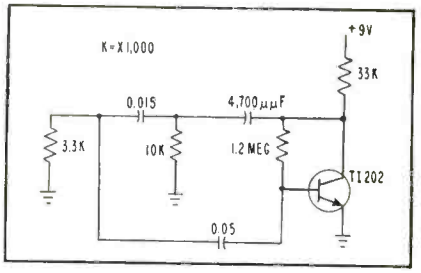
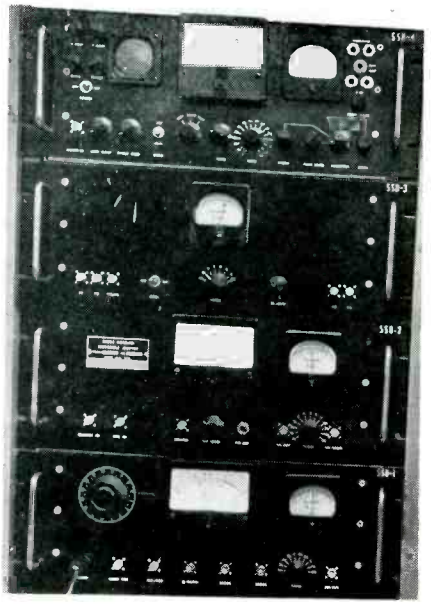


FIG. 3—Phase-shift oscillator uses circuit of Fig. 1B

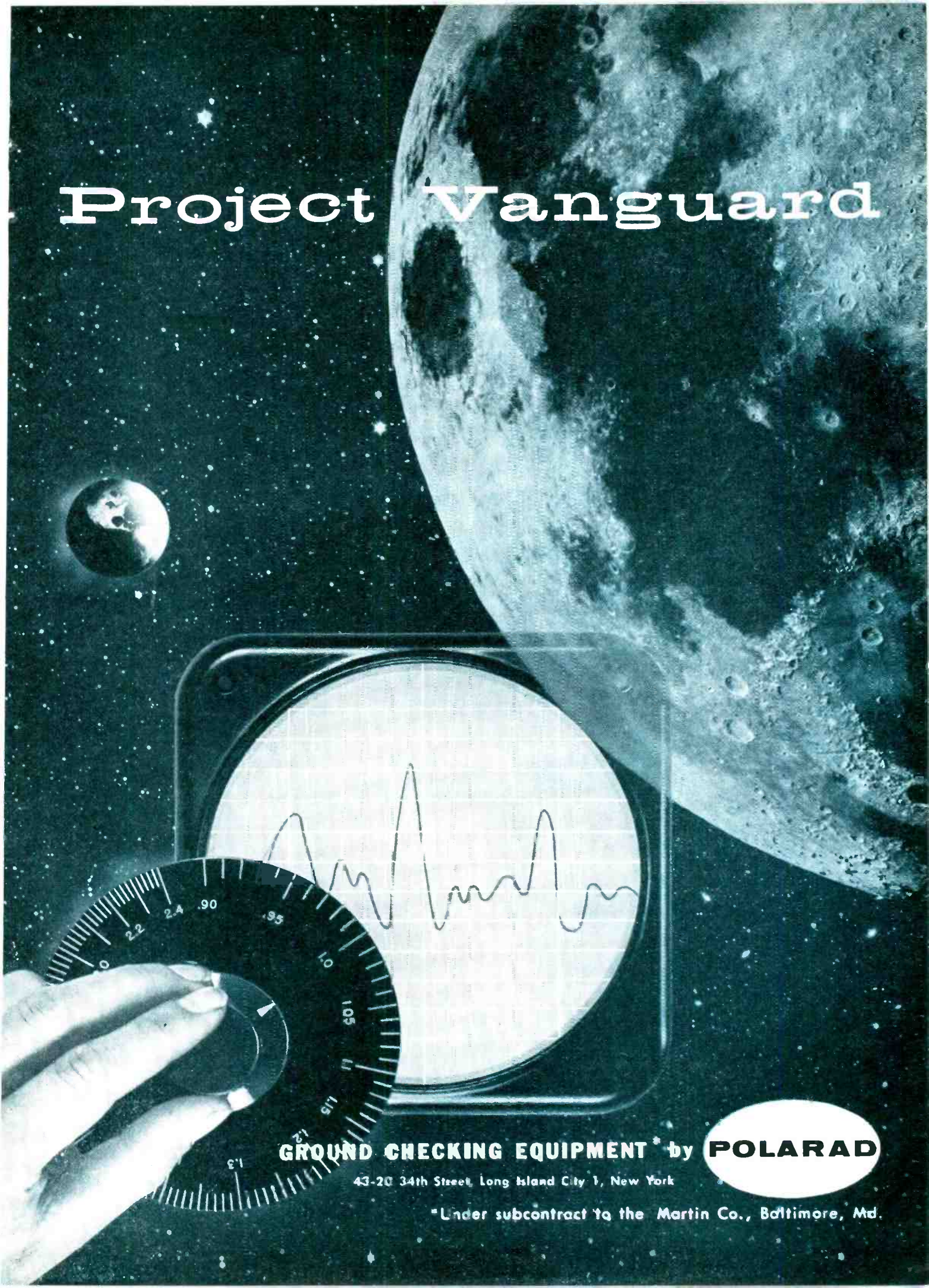
value may be ascribed to phase shift in the coupling circuit between the two transistors. It is necessary in this circuit to keep the amplitude small if distortion is to be avoided.

Figure 1B shows a network whose current transmission will have a phase reversal at some frequency. If the network is sufficiently tapered so $R_1 >> R_2 >> R_3$ and $C_1R_1 = C_2R_2 = C_3R_3 = CR$ this frequency is given by $f = 1/2\pi\sqrt{3}CR$. By having the network tapered, its loss is decreased and a lower transistor gain will suffice for

WMGM Tests CSSB



Compatible single-sideband transmitter adapter shown was developed by Kahn Research Laboratories for use at broadcast station WMGM, New York. Tests started in mid-January will permit measurements of reduction in bandwidth and interference, improvement in fidelity and reduction in fading distortion. Similar transmissions from Voice of America's Munich megawatt transmitter can be received on conventional a-m receivers without distortion


Project Vanguard
GROUND CHECKING EQUIPMENT * by POLARAD
43-20 34th Street, Long Island City 1, New York
*Under subcontract to the Martin Co., Baltimore, Md.

oscillation. The taper is the opposite of that used with vacuum-tube circuits, the impedance level decreasing along the network.

Figure 3 shows a phase-shift oscillator using this network. Again the load resistor is part of the phase-shift network, and the bias is arranged as it was in the other oscillator. Frequency is about 500 cycles.

The taper in the phase-shift network is only by a factor of about three but this seems helpful. It is easier to get a good waveform with this oscillator than with the other, probably because this circuit provides strong negative feedback for higher harmonics of the waveform, tending to decrease them.

High Speed Strobe Checks Tube Vibrations

By KENNETH LEIB and NORMAN RITCHEY

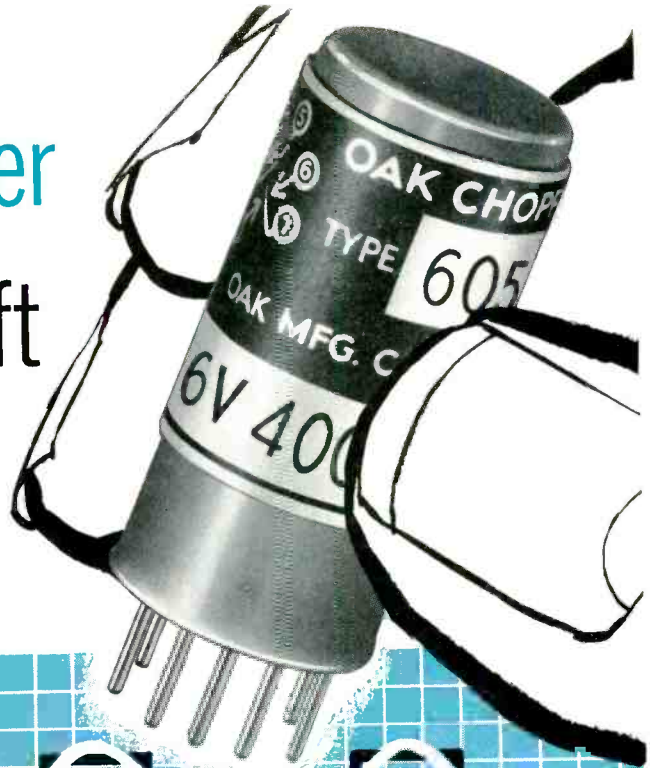
Product Development Laboratory
Sylvania Electric Products, Inc.
Kew Gardens, N. Y.

DURING development work on military-type vacuum tubes, it is often advantageous to examine tube element motion under vibration at high g levels at those frequencies giving highest microphonic output. In the majority of cases, these frequencies are above the fundamental ranges of commercial stroboscopes.

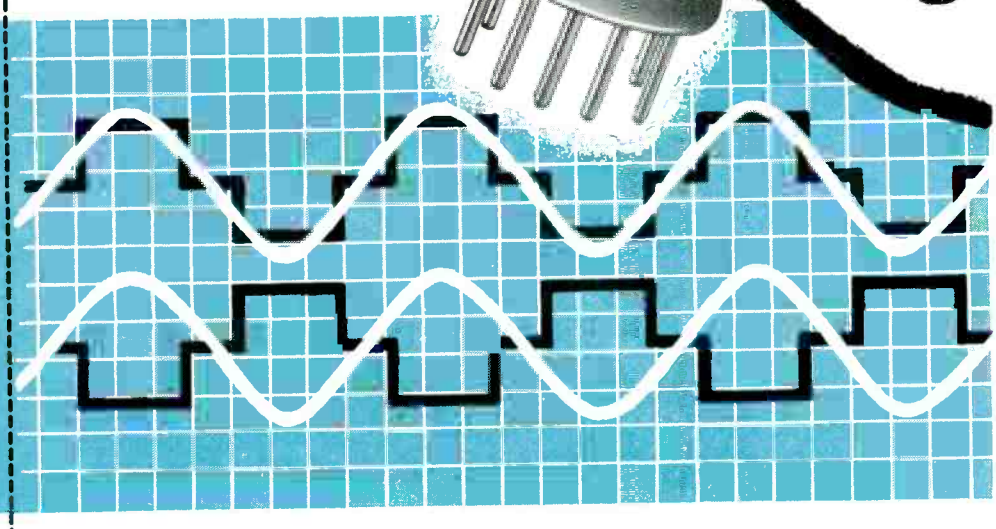
Above 2,000 cps many stroboscopes work on a harmonic of their operating range with the result that micro-movements are not readily observed since the light source illuminates the subject on alternate cycles for the second harmonic, once every third cycle for the third harmonic, and so on. To overcome these limitations, Type R1131C slow modulator tubes were used. Variation of tube current provides a modulated light output of high intensity. In many cases it was possible to leave the filament of the tube under test on and thereby maintain electrical microphonic output without loss of movement detection ability.

The Type R1131C cold-cathode light modulating tube has a crater-type cathode which provides a high ionization density and a narrow light beam particularly useful in

new OAK chopper needs no phase-shift circuit!



HAS 0° or 180° PHASE-LAG "DESIGNED-IN"



SPECIFICATIONS

Coil: Current, 25 ma; impedance, 190 ohms; resistance, 160 ohms.

Contacts: Dwell time, 150-160°; rating, 100 V, 2 ma. Resistance, less than 200 milliohms.

Phase Change: ± 10° At constant 400 cps under all conditions of use and life.

Noise: Less than .5 millivolt RMS into 1 meg.

Vibration: 10-55 cps.

Weight: Less than 1 oz; dia. 11-16".

Height: Seated, 1⅝".

Inherent in every device of the vibrating reed type are two phase-lags—an electrical phase angle resulting from the current lagging the applied voltage in the drive coil, and a mechanical angle due to the inertia of mass in the moving reed, lagging further behind flux from the driving current.

In OAK's new Type 605 Chopper, these two lags have been carefully brought to a total of 180°. Thus, the chopper can be so wired to be exactly 180° out of phase, or reversed to be 360° out (in phase). This design eliminates the R-C circuit ordinarily needed to bring this coincidence of voltage and output phase—saving circuitry, parts, and weight.

Shown at the left is the new chopper with side mount. Also available with flattened and pierced pins, solder loops, or as a vertical flange mount unit.

OAK MFG. CO.

Dept. G, 1260 Clybourn Ave., Chicago 10, Illinois
Phone: MOhawk 4-2222

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Want more information? Use post card on last page.

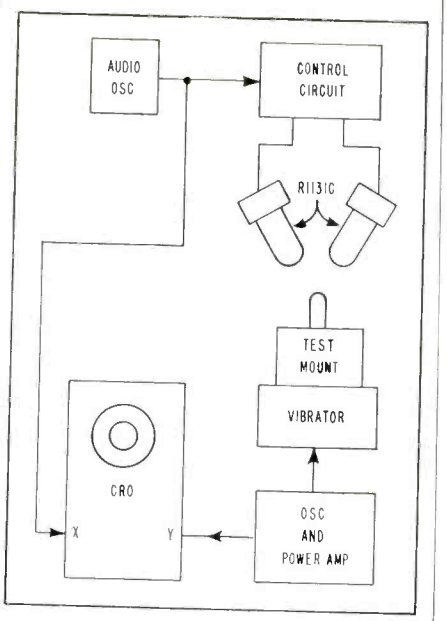


FIG. 1—Simple control circuit for two cold-cathode light-modulator tubes

the investigation of microphonics in tubes with T_5 to T_9 envelopes. The cold-cathode tube has been used for several years in facsimile equipment as well as in picture transmission applications.

The R1131C is connected as the load of a triode connected 6L6 in the circuit of Fig. 1. Sufficient fixed bias is used so that the tube barely conducts. The light output although steady is quite low. Application of 25 to 30 volts rms to the grid results in a light output of high intensity, with the light quite sufficient for the observation of moving parts. The tube current during operation shows in Fig. 2. Fig. 2.

Although various modifications can be effected as conditions warrant, the modulation-type stroboscope was employed as in the block

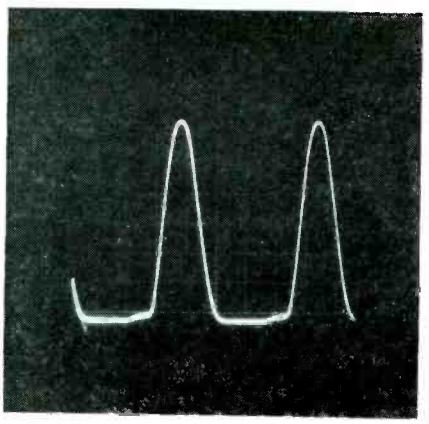
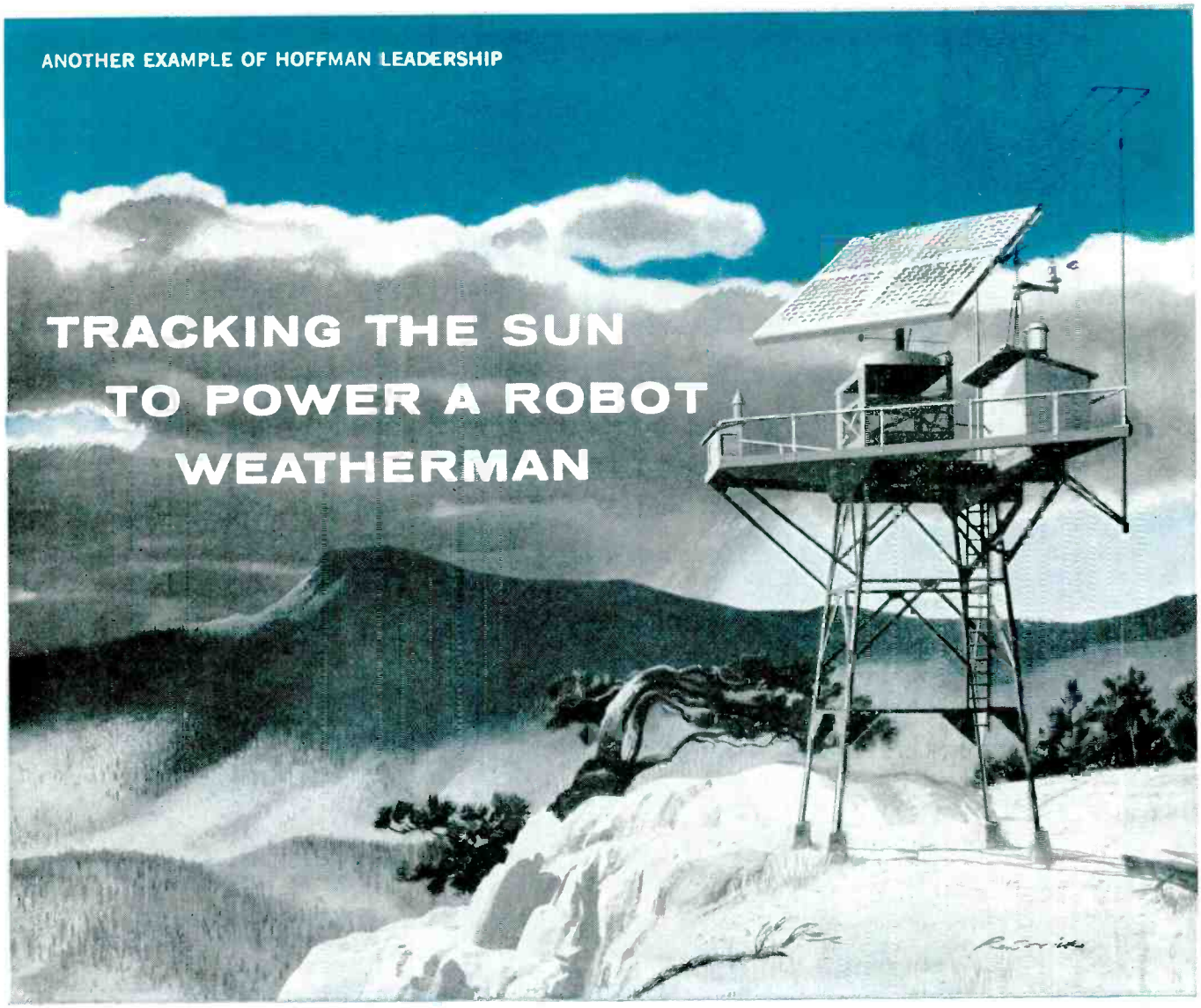


FIG. 2—Waveform of current through modulator tubes

ANOTHER EXAMPLE OF HOFFMAN LEADERSHIP



TRACKING THE SUN TO POWER A ROBOT WEATHERMAN

BIG BERTHA

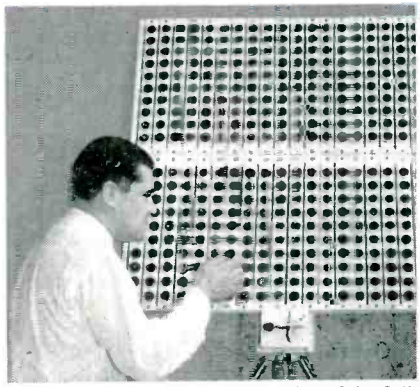
Solar Energy Converter Panels

Powering unmanned weather stations is just one of the many uses for Big Bertha—newest, most exciting product of Hoffman electronics research. Solar Energy Converter Panels like this can be installed wherever an economical and efficient source of electrical energy is needed to power transistorized signal, telemeter, communications and similar electronic equipment.

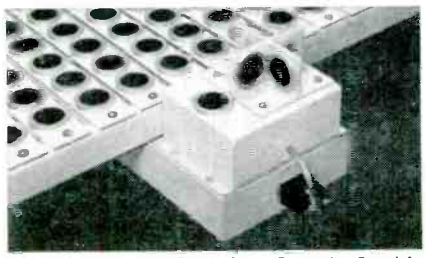
Hoffman silicon junction Solar Cells blanket the face of Big Bertha, convert sunlight directly into electricity to charge batteries and operate equipment—produce 80 watts of power output for each square yard of surface. Panels of almost any size or configuration can be built at modest cost.

Important potential applications for Hoffman Big Bertha Converter Panels include: untended telephone repeaters, unmanned radio relay stations, pipeline transmitters, Forestry Service radio units, telemetering equipment, railroad signaling apparatus, and all types of transistorized radio, TV, telephone and telegraph equipment

Solar Energy Converter Panels can be supplied in tracking and non-tracking models, with special mounting stands or brackets designed to meet individual requirements. For additional technical information, please write the Applications Engineering Division, Hoffman Electronics Corporation, 3817 South Grand Avenue, Los Angeles 7, Calif.



BIG BERTHA consists of banks of Hoffman Solar Cells interconnected to attain specified power requirements—produces 80 watts per square yard of surface.



SUN TRACKER automatically turns Converter Panel to "follow" sun's transit across sky, assures maximum conversion efficiency throughout the daylight hours.

Hoffman ELECTRONICS CORPORATION

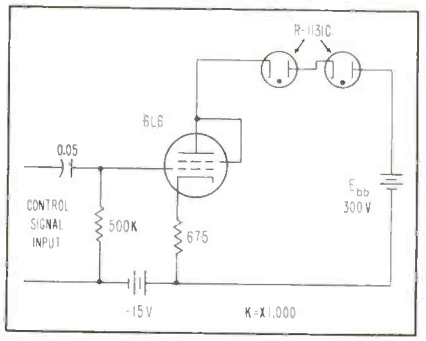


FIG. 3—Block system of setup for examining microphonic tubes

diagram of Fig. 3. Under this setup, the tube under test was vibrated through the frequency range of interest. Where a peak signal is noted, the light source is focused on the tube under test and adjusted to a frequency a few cycles different from the vibrator drive frequency, by use of a Lissajou pattern. To date, the highest frequency at which movement has been observed is 7,400 cps in a T_2 envelope even though the R1131C modulating range is from 15 to 15,000 cps. The present application utilized two modulator tubes to eliminate or minimize shadows. With slight modifications, this could readily be extended to three or possibly four glow tubes if required.

The photograph shows the system used during the analysis of a subminiature tube type. The stroboscopic system, including the power supplies, oscillator and monitoring oscilloscope, can be combined on one chassis and inserted in a 3-in. oscilloscope case. In addition to the advantages of a unified control, this can minimize required bench space.

Miniature tube on vibrator is illuminated by glow molulator tube on left for examination under vibration conditions

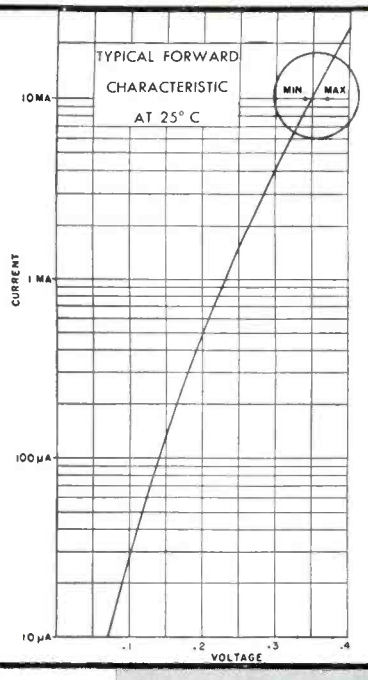
If forward voltage drop is a problem in your diode circuitry...see the

RADIO RECEPTOR

Germanium Diode DR 385

Available now in production quantities for immediate delivery

with controlled forward voltage drop between 0.34 and 0.37V at the 10MA level



Design engineers working with transistorized circuits, computers and other applications will find that RRco. Type DR 385 has extremely low forward voltage drop as well as other desirable features... The specifications speak for themselves!

Characteristics at 25° C

Forward voltage drop @ 10MA	
Minimum	0.34V
Maximum	0.37V
Maximum reverse current at −10V	10UA
Peak inverse voltage	60V

Maximum Ratings at 25° C

Maximum inverse operating voltage	50V
Continuous DC forward current	100MA
Surge current for 1 second	500MA
Average power dissipation	80MW
Derating above 25° C	10MW/10° C

DR 385 exhibits fast transient response and similar diodes can be offered fully tested to your recovery conditions.

In Radio and Electronics Since 1922

Further information on DR 385, or any other RRco. diode type will be sent you at once upon request to section E-2.

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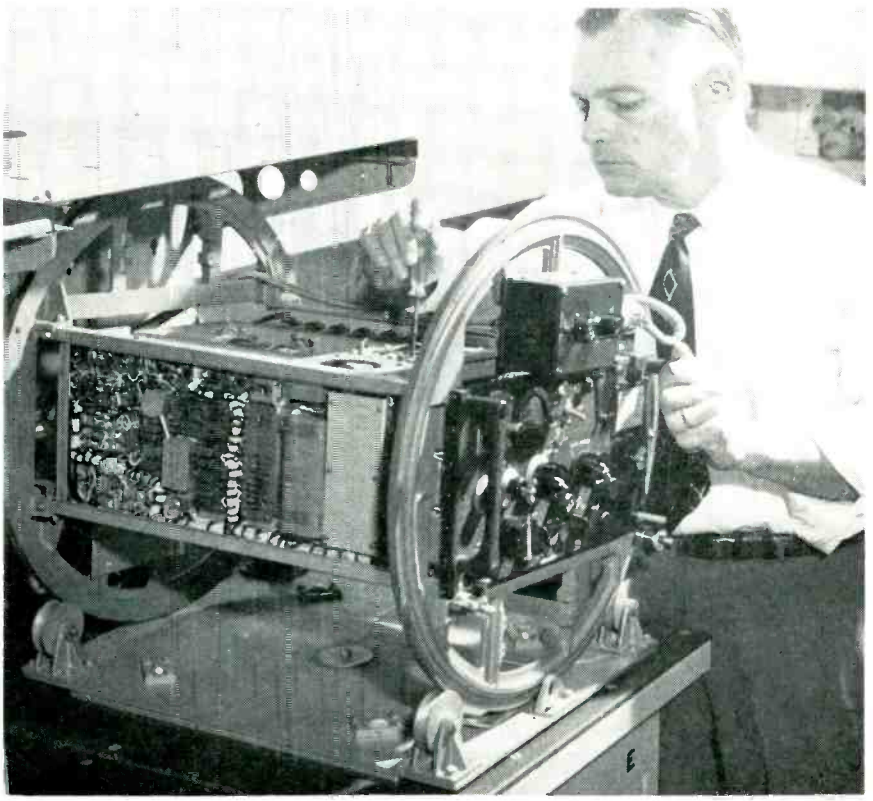
Production Techniques

Edited by JOHN MARKUS

Chassis Rack Pivots and Rotates on Test Bench

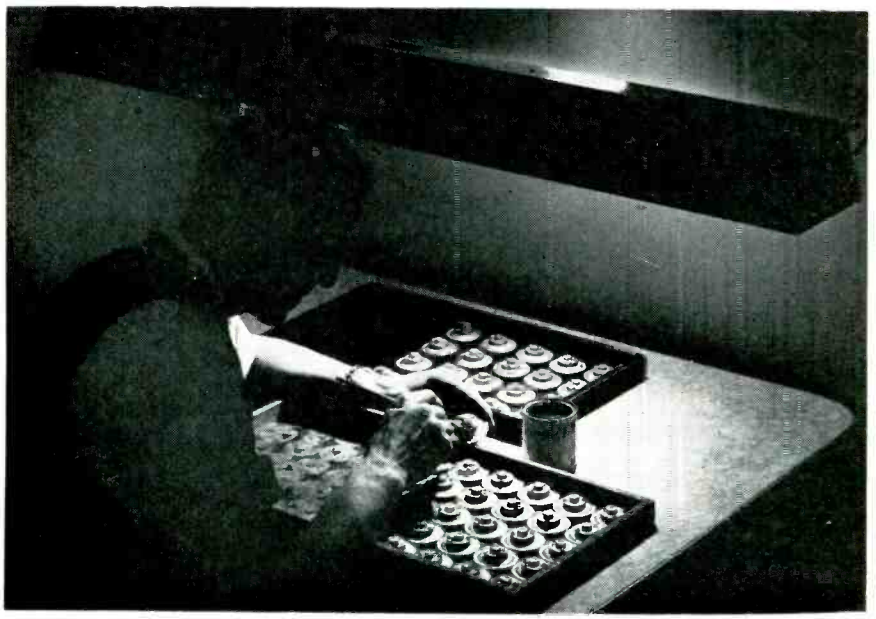
WHEEL-LIKE chassis-holding racks designed by the Naval Aviation Service Department hold and conveniently position airborne transceivers for rapid servicing and maintenance. The rack is made by American Measuring Instruments Corp., 240 W. 40th St., New York.

The rack consists of a frame mounted on two large wheels that ride freely in four grooved wheels attached to a moveable base which revolves about a center pivot point. The chassis to be serviced is mounted on the frame between the large wheels and can then be moved in any position. Since it is necessary, when aligning AN/ARC-2 transceivers, to work on at least three sides of the equipment, the rotating rack is an excellent time-saver for this piece of equipment. In addition, it is used for servicing AN/ARC-1, AN/ARC-27 and AN/ARN-21 (Tacan) equipment, as well as a variety of other electronic units. Chief advantage is ability to turn over a chassis almost instantly without damaging components, wires or subassemblies.



Method of using pivoted rotating rack for servicing airborne transceiver AN/ARC-2 (made by Collins Radio Co.) at Servicing Unit of Naval Receiving Station, Washington, D. C. Circular outer support rings ride freely in grooved wheels mounted on base that is supported just enough by pivot to clear top of bench

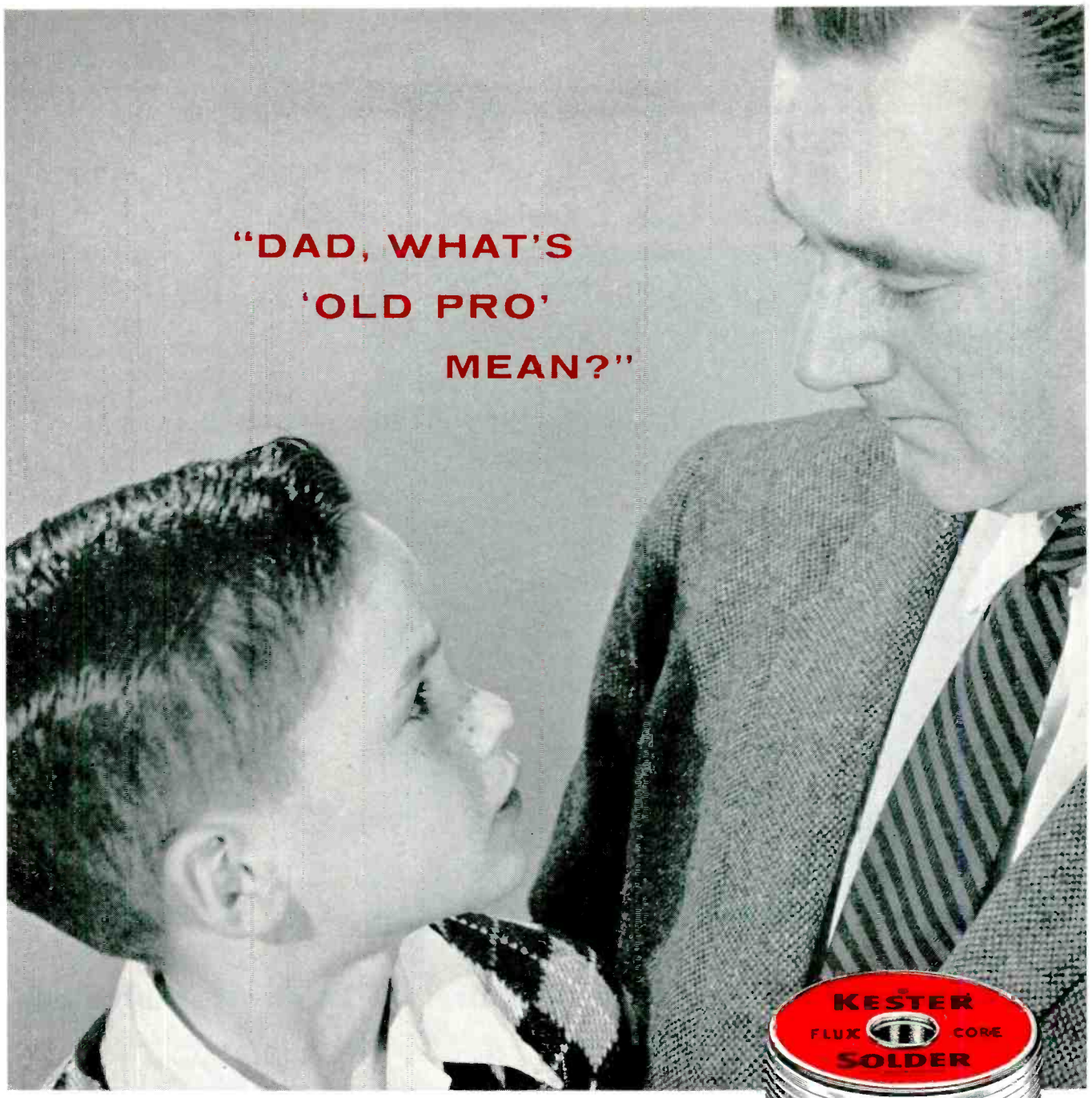
Cool Ultraviolet Shows Fungicidal Varnish During Application



Applying fluorescent fungiproofing varnish to microphone terminals under long-wave lamp that plugs into any 115-volt a-c outlet and operates like standard fluorescent lamp. Varnish glows bright green where applied, so operator detects misses himself

REJECTS BY military inspectors because of missed coatings on connections have been cut to zero at American Microphone Co. in Pasadena, Calif. by checking with ultraviolet light at the time that the moisture-proofing fungicidal varnish is applied. This varnish contains an additive which fluoresces a vivid bright green under activation by 3,660 A long-wave ultraviolet.

Although such light was used heretofore for inspection, the man who applied the varnish had to work in the dark, so to speak, because the varnish is transparent under ordinary light. Use of a new Blak-Ray cool 4-foot lamp (available from Black Light Eastern Corp., Long Island City, N. Y.) at each terminal-painting position gives adequate fluorescence despite normal room illumination, so the



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It's like that with solder. No meager test dependent upon a "sample" or even a "one-line operational test" is going to prove conclusively the merits of a "Johnny-come-lately" solder from that second source of supply. The wise buyer knows that the solder used on his production line must do the job he requires day-in and day-out without question.

And KESTER SOLDER has been time-tested and industry-proved for over 50 years.

That's what we mean by "old pro," Sonny!

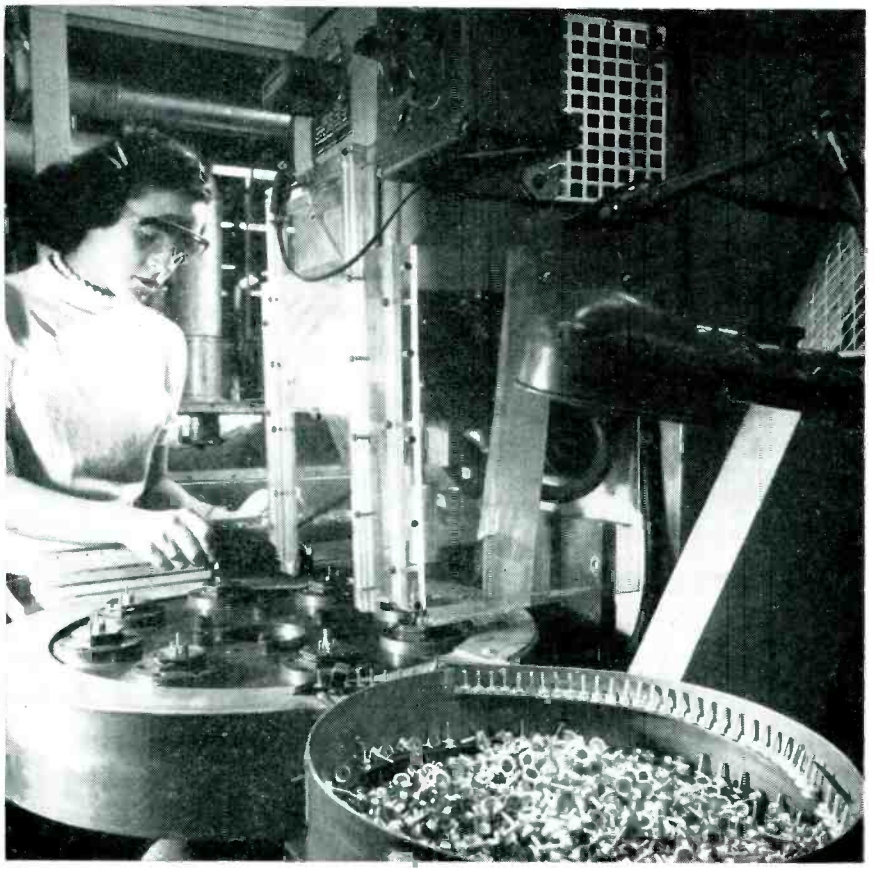
SEND TODAY for your copy of the 78-page Kester textbook, "Solder . . . Its Fundamentals and Usage." It's free!

KESTER SOLDER *Company* 4204 Wrightwood Avenue, Chicago 39, Illinois

Newark 5, New Jersey • Brantford, Canada

operator can see when he misses a spot or a complete connection. The change in setup speeds application of the varnish and eliminates costly retouching of misses detected by the military inspector under conventional hot-quartz long-wave light. The technique is particularly valuable with complex assemblies because it eliminates need for remembering which terminals have been painted after an interruption.

Automatic Turntable Feeds Transistor Cap Welder



A STANDARD COMMERCIAL welder has been adapted by General Electric at its Semiconductor Products plant at Syracuse, N. Y., for welding the two basic subassemblies of a transistor together. By welding the transistor cap onto the header which holds the germanium or silicon wafer and leads, rather than soldering the two parts together, greater reliability of the device is assured. Leakage of contaminating air, the bugaboo of transistor reliability, is thus avoided.

The machine is capable of handling better than 800 transistors an hour. The table used as the electrode base and conveyor moves the eight welding stations counterclockwise. As each station moves into the proper position, an air-operated index locks the electrodes.

Operator loads headers into pockets of turntable manually, after which Syntron work feeder setup drops caps over headers automatically. Vertical plastic slides hold plastic window used to block flashes of molten metal; window is raised here to show welding position

Mark-Sensing Cards Aid Quality Control on Tacan Assembly Lines

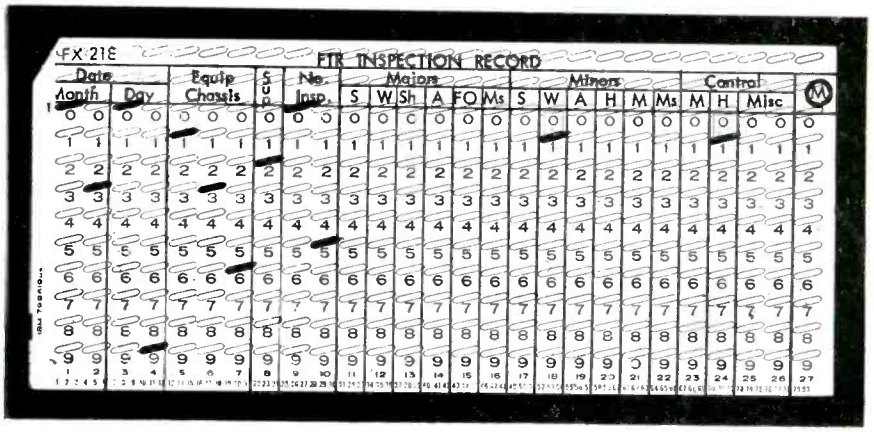
USE OF MARK-SENSING punched cards now expedites the collection and analysis of routine quality control data during manufacture of Tacan airborne units and other electronic equipment.

Mark-sensing is a variation of the punch card system wherein the original information is entered directly on a card form by making a mark with a special lead pencil. A machine then transforms the marks into punched holes by means of timed electronic impulses. This contrasts with the key punch method whereby the original raw data is transferred from data sheets to the card form manually by a key punch operator.

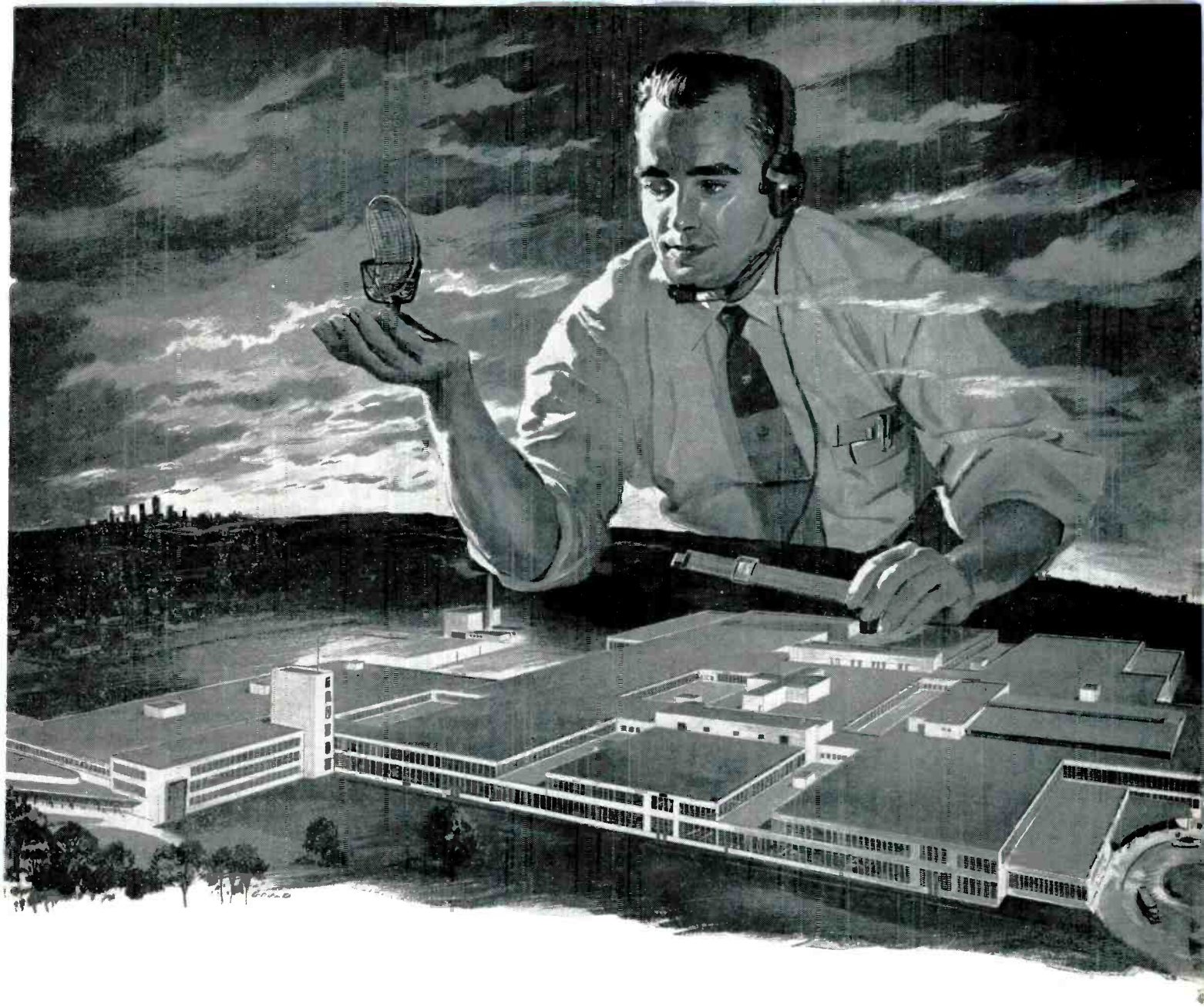
By LEAH HAZARD

Coordinator—Quality Control
Federal Telephone and Radio Co.
Division of I.T.&T.
Clifton, N. J.

► **Record Cards**—A special inspection record card was developed to record the necessary basic information pertaining to the act of inspecting equipment. It contains spaces for identifying such items



Example of marked card covering inspection of five AN/ARN-21 i-f amplifier units. Two defects are checked, one in minor wiring and the other in control hardware. Card is standard size, 7⅜ inches wide and 3¼ inches deep



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Your guess is as good as anyone's as to whether our Government or our industrial customers give us the more interesting challenges.

Take TACAN—or an ARN-32 marker beacon—or missile guidance systems, countermeasures, automatic test equipment, automatic assembly techniques, on all of which we are privileged to work. Certainly, they demand the utmost in precise engineering and manufacture.

Then, on the civilian front, there are projects like completely transistorized telephone switchboards, and electronic systems for recording data about every freight car in transit over a railroad. These also require nothing less than perfection.

The net result of America's insatiable appetite for electronic research and production has been a phenomenal growth in our business and the establishment of the new Stromberg-Carlson "Electronics Center"—the 800,000 square foot plant pictured above. Every inch and every person in it are dedicated to continuous advances in national security and the home-front economy. We're proud to be at your command.

And there are plenty of career opportunities for engineers who wish to grow with electronics' finest. Write to Mr. R. W. Holmes for further information.

S-C STROMBERG-CARLSON

STROMBERG-CARLSON COMPANY

A DIVISION OF GENERAL DYNAMICS CORPORATION

General Offices and Factories at Rochester, N. Y.—West Coast plants at San Diego and Los Angeles, Calif.

GD GENERAL DYNAMICS

Inspection position at which defects in airborne unit of Tacan equipment are marked on inspection record card. Complete unit mounted in quick-flipover plastic enclosure provides convenient visual comparison guide

as date of inspection, unit of equipment, production supervisor responsible for producing it and the number of units inspected. These items take up the first 10 vertical columns of the card. The remaining 17 columns provide space for recording the frequency of occurrence of defects in workmanship.

Workmanship defects are separated into categories of Major, Minor and Control, in accordance with the degree of effect each would have on the life or operation of the equipment. Within these categories the separate columns are given a letter heading to signify the type of defect to be recorded. The individual letters are translated as follows: S—Soldering; W—wiring and cabling; SH—shorts; A—assembly; FO—foreign objects; Ms or Misc—Miscellaneous; H—hardware; M—marking.

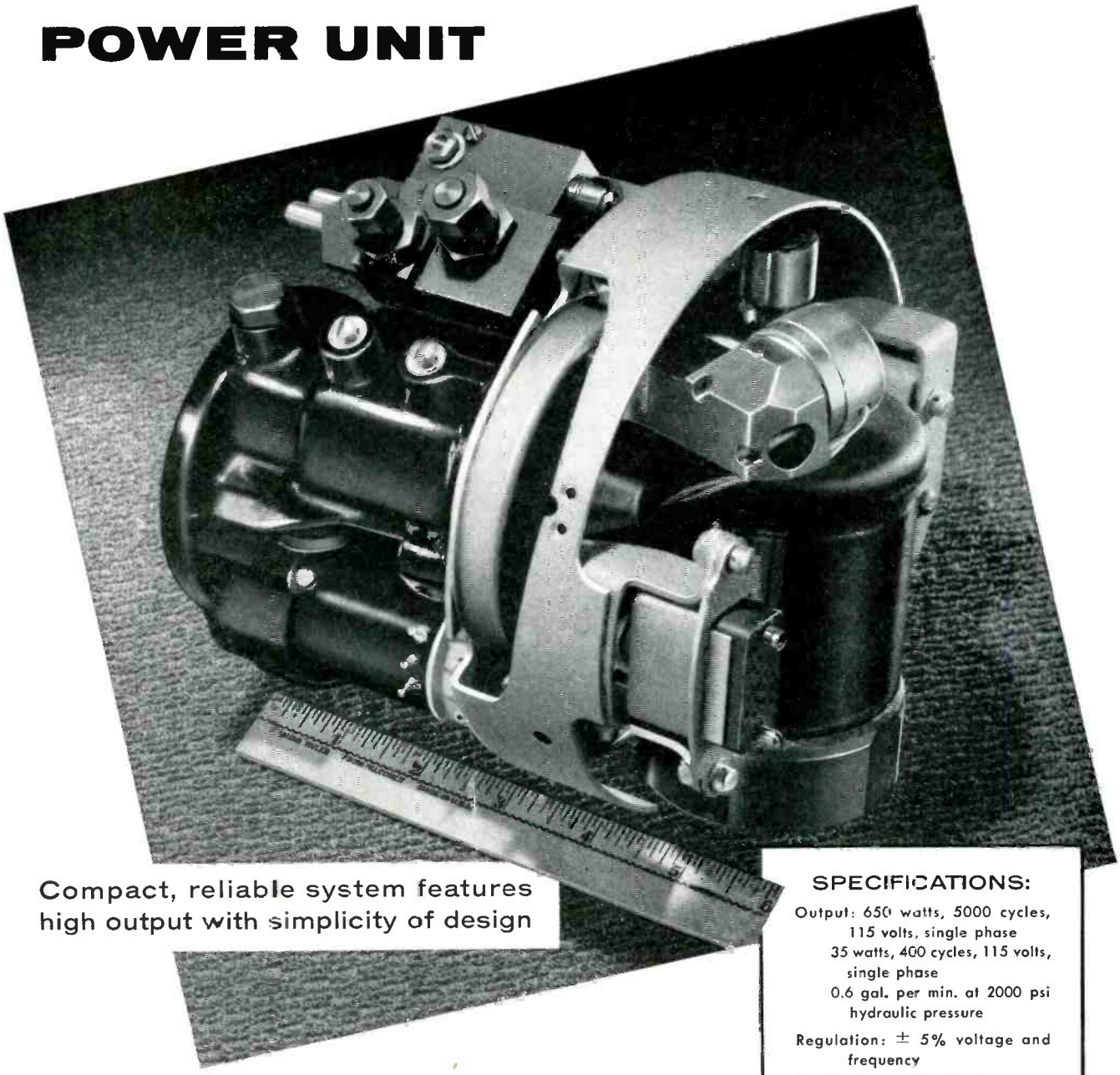
The character M heads a column which is used by quality control personnel to assist in the preparation of a quality rating of production supervisors. Items tallied in this column are those major defects found by inspection which are not directly chargeable to the supervisor responsible for the unit. Such defects, for example, might be found on a subassembly produced under another supervisor.

▶ **Summary Reports**—The inspection cards are normally collected at the close of each shift. Cards are processed and summary reports are made ready for the next starting time of that shift. The summary report is a printed compilation of information contained in the deck of inspection cards, together with computations of process averages for each chassis. Tabulating and electronic calculating machines perform the necessary computations. Such summary reports can be issued daily, weekly, monthly or at any desired time.

▶ **Advantages** — Machines can process cards much more rapidly

Mark sense reproducer machine in foreground converts pencil-marked cards into standard punched cards suitable for machine at rear that is printing data summary on special report sheet

AiResearch MISSILE AUXILIARY POWER UNIT



Compact, reliable system features high output with simplicity of design

SPECIFICATIONS:

Output: 650 watts, 5000 cycles, 115 volts, single phase
35 watts, 400 cycles, 115 volts, single phase
0.6 gal. per min. at 2000 psi hydraulic pressure

Regulation: ± 5% voltage and frequency

Duration:	27 seconds
Weight:	9.5 pounds
Size:	6.14 in. diam., 6.74 in. long

Ground power: compressed air

This AiResearch auxiliary power package operates the vital electrical and hydraulic systems in a missile.

Gases from a solid propellant spin the unit's turbine wheel at 50,000 rpm. The turbine's shaft drives the following: a 650 watt generator which supplies electrical power to run the missile's guidance system; a 35 watt generator which runs the missile's gyros; a hydraulic pump which in turn powers the servos that control the movable flight surfaces of the missile's airframe.

The hydraulic system features drilled passages which eliminate the need for potentially troublesome plumbing. It includes reservoir, filters, temperature compensator, relief valve, check valve, and squib valve within a single housing.

This auxiliary power system is an example of AiResearch capability in the missile field. Inquiries are invited regarding missile components and sub-systems relating to air data, heat transfer, electro-mechanical, auxiliary power, valves, controls and instruments.

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FX 223

Federal Telephone and Radio Company
Quality Control Report
Summary and Analysis of Inspection Data

Equipment: Period:

Date	Unit	Sup	No. Insp	MAJOR DEFECTS								MINOR DEFECTS								CONTROLS			Ⓜ	Supervisor Proc. Aug.
				Sold	Wir	Short	Assem	For. C	Misc	Total	Proc. Aug.	Sold	Wir	Assem	Hdwr	Mark	Misc	Total	Proc. Aug.	Mark	Hdwr	Misc		
1/30	102	6	57																					
1/30	102	6	54																					
2/1	102	6	40																					
2/07	102	6	82																					
2/07	102	6	99		2																	6		
2/09	102	6	61	6																				
2/09	102	6	99		3																			
2/10	102	6	99																					
2/10	102	6	99																					
2/10	102	6	27																					
2/13	102	6	43																					
			760	6	5					11	0.01							0	0			6	0	0.01
2/15	101	6	6																			2		
2/02	103	6	5				3														1			
2/24	103	6	7				1															2		
2/24	103	6	6																					
2/13	103	6	12																					
2/15	103	6	6																					
			42				4			4	0.09							0	0		1	4	0	0.09
1/30	104	6	5																					
1/27	104	6	4																					
2/01	104	6	22																					

Portion of summary report that is printed automatically by card-sorting machine. Actual form is approximately 15 inches wide and 11 inches deep

and accurately than can human beings. Therefore, the new system, which requires no extra time and energy on the part of the inspector (the card was substituted for a former data sheet) saves time, energy and money with respect to correlating, analyzing and distributing the information gained by inspection.

The speed with which information can be disseminated provides opportunity for rapid preventive as well as corrective action. This in turn reduces poor workmanship and reduces the percentage of future scrap and rework.

Analysis of inspection information and useful reporting of the findings can be extended to include wider and more detailed areas without increase in indirect labor, because of the saving of time through use of computing machines.

Cards can be sorted to provide a picture of the quality of workmanship performed on any group of equipments or on any single unit group under the direction of any supervisor. Cards can also be sorted to provide a picture of the quality of any workmanship characteristic, either for purposes of investigation and training or for comparison.

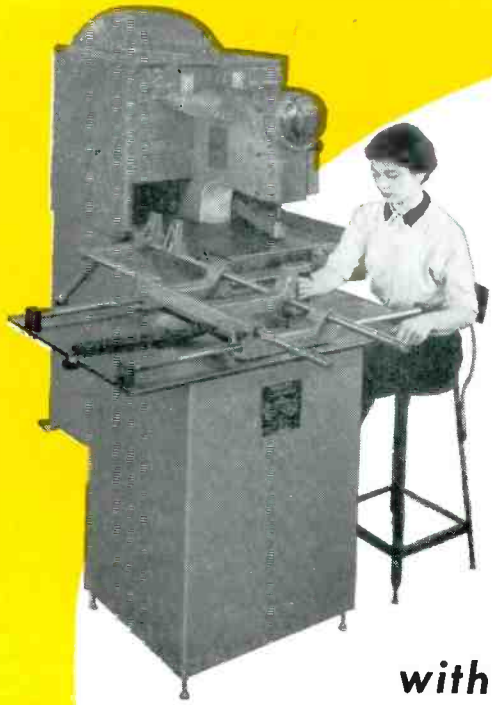
Localized Plating of Etched Wiring

SELECTIVE ELECTROPLATING of terminals on etched wiring boards and flanges on waveguides can be achieved at high speed by the Dalic process, originally developed by the Laboratoires Dalic in France. The required electrodes and supplies are now available from Marlane Development Co., 153 E. 26th St., New York City. The technique is also suitable for build-up of worn components and for numerous other applications where high-speed deposition is required on small areas without stopping-off or dismantling.

► **How It Works**—The principle is similar to that of ordinary contact plating, whereby a cotton pad dipped in plating solution is connected to the anode bar and the work is connected to the cathode bar. The new development lies in the use of insoluble graphite anodes and a wide range of organic plating solutions. These solutions are nontoxic, give off no harmful fumes and are quite safe to handle without protective gloves.

Another feature is the high rate of deposition afforded by the high current densities used with these organic solutions. The deposits obtained have good mechanical properties with high adhesion and little or no porosity, because the current for the process is supplied by a specially designed transformer and rectifier unit operating from a 220-v single-phase a-c line and delivering up to 40 amperes d-c at low voltage. With a small plating pad this can give current densities as high as 6,000 amperes per square foot.

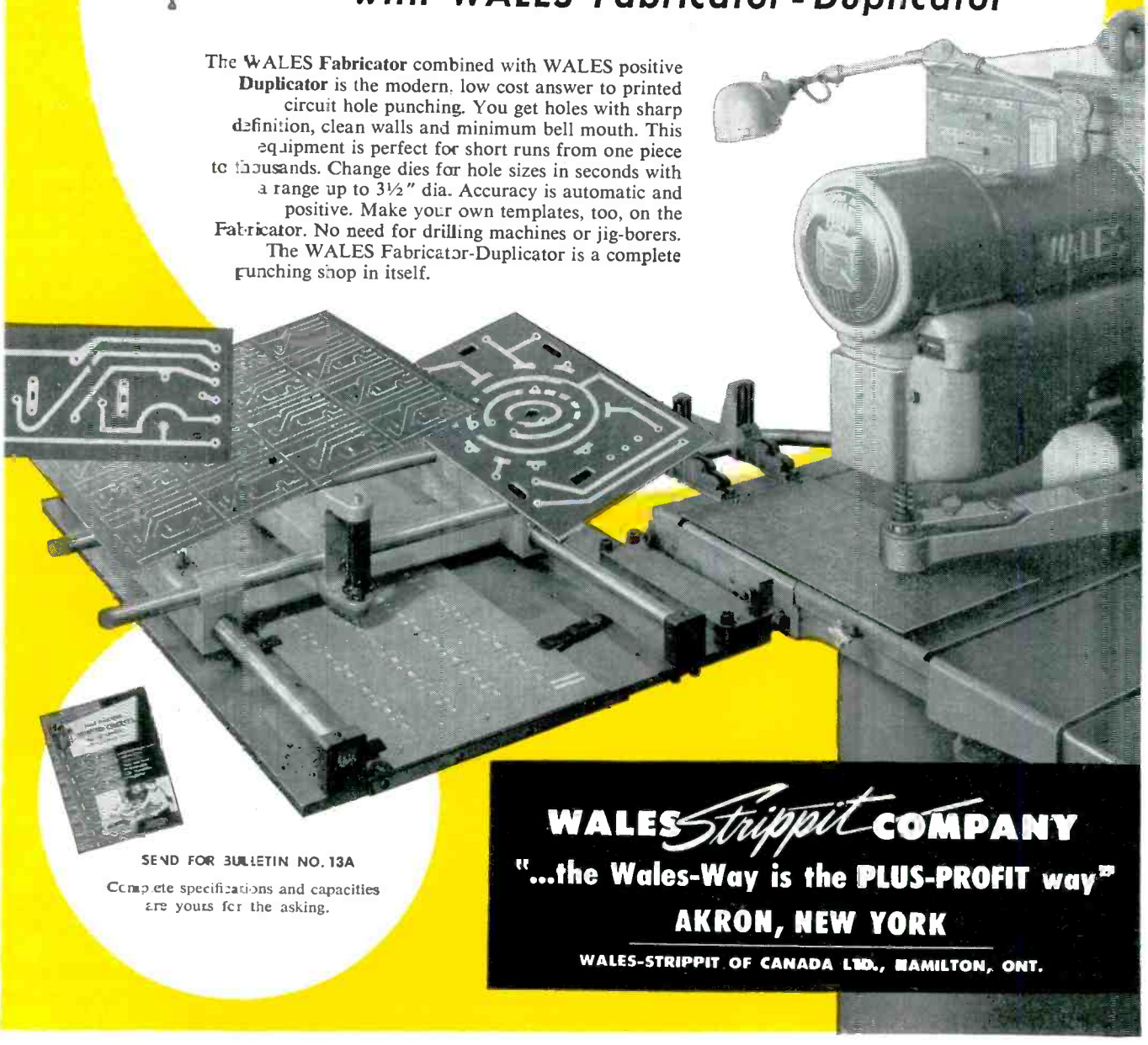
The cathode lead is connected to the workpiece with a large insulated crocodile-type clip. The anode lead plugs into various types



Punch PRINTED CIRCUITS Cold...

with WALES Fabricator-Duplicator

The WALES **Fabricator** combined with WALES positive **Duplicator** is the modern, low cost answer to printed circuit hole punching. You get holes with sharp definition, clean walls and minimum bell mouth. This equipment is perfect for short runs from one piece to thousands. Change dies for hole sizes in seconds with a range up to 3½" dia. Accuracy is automatic and positive. Make your own templates, too, on the Fabricator. No need for drilling machines or jig-borers. The WALES Fabricator-Duplicator is a complete punching shop in itself.



SEND FOR BULLETIN NO. 13A

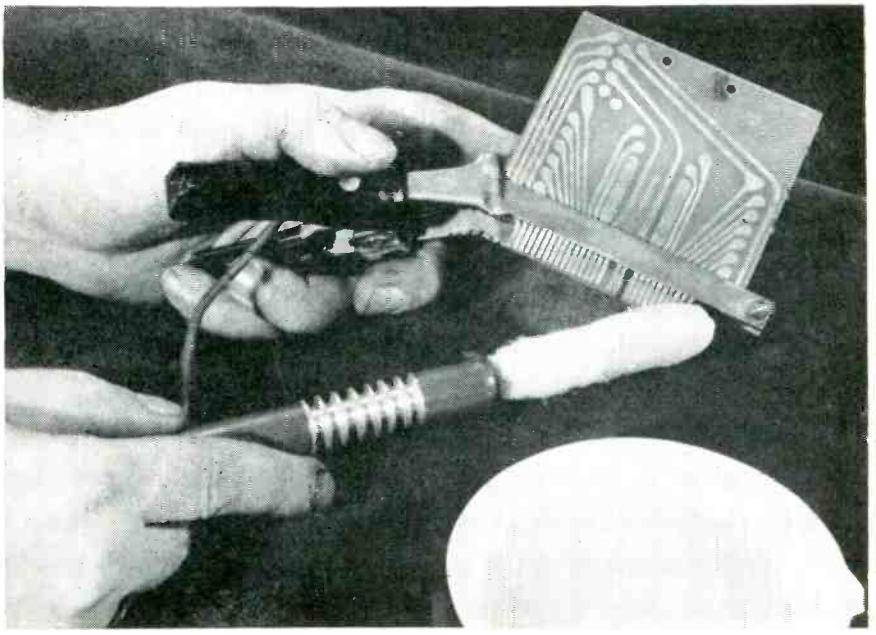
Complete specifications and capacities are yours for the asking.

WALES Strippit COMPANY

"...the Wales-Way is the PLUS-PROFIT way"

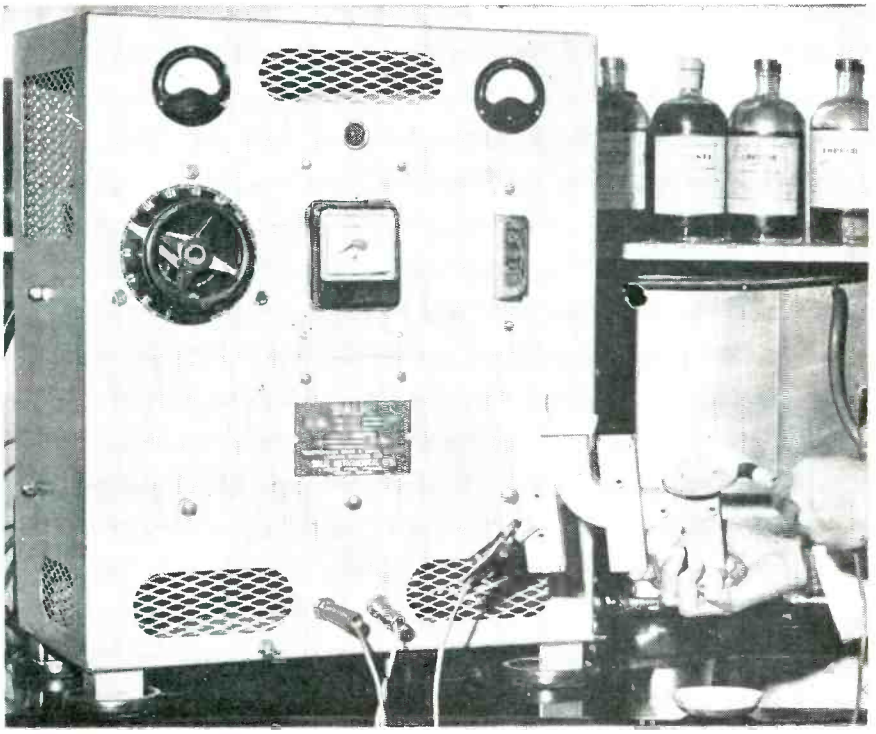
AKRON, NEW YORK

WALES-STRIPPIT OF CANADA LTD., HAMILTON, ONT.



Cotton-wrapped graphite plating anode is dipped in electrolyte in dish, then wiped over sliding contacts of etched wiring board to place 0.00015-in. deposit of gold on them, followed similarly by 0.00005 in. of rhodium. Combination of metals improves conductivity and minimizes wear. Metal bar across board makes contact with all parts of printed circuit and serves as stop-off for plating

of anode holders, most of which are fitted with air-cooling fins. The electrolyte is applied by means of a pad of absorbent cotton wrapped around the graphite anode. The wrapped anode is merely dipped into the solution of the required metal and applied to the material to be plated with a rubbing motion, the current density having been preset on the power unit. The current quickly raises the solution to boiling point and plates rapidly, as indicated in Table I. Times are for plating an area equal to that of the pad electrode used. There is no residual problem; the solutions are organic compounds and at boiling point the radicals are decomposed. The only subsequent treatment



Complete bench-top plating setup, here being used to plate 0.5 to 1 mil of indium on butt joint area of waveguide to provide ductile compression gasket

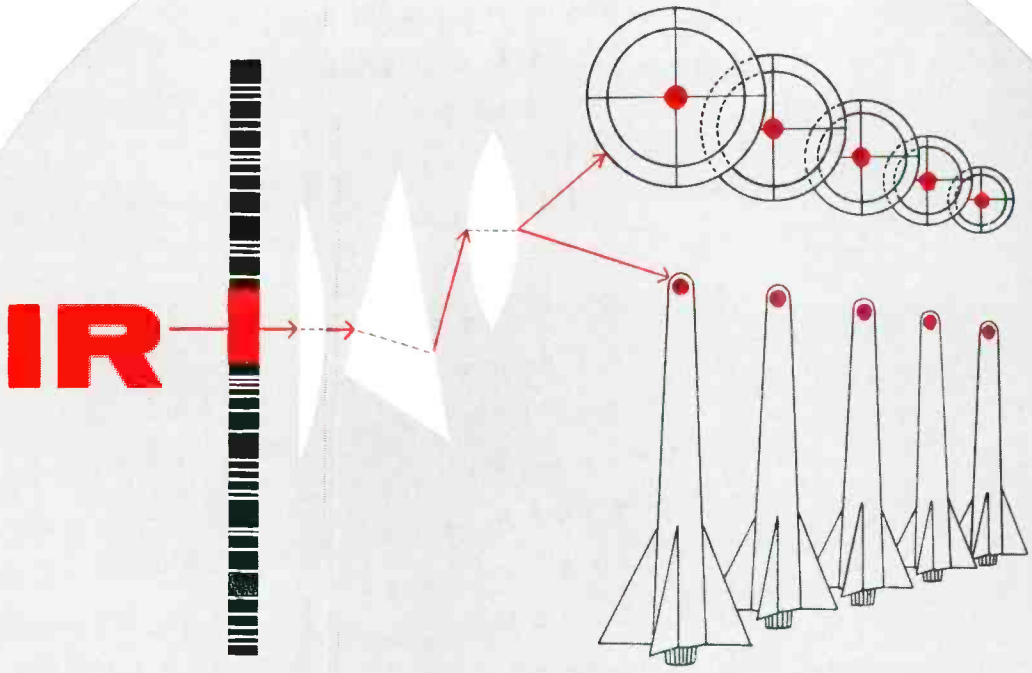


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Table I—Plating Times and Current Densities

Metal Being Deposited	Maximum Current Density in Amp per Sq Ft	Time in Seconds to Deposit 0.0001 Inch
Bismuth	1,500	7.5
Cadmium	6,000	2.5
Chromium	4,000	63.0
Cobalt	1,500	7.6
Copper	6,000	2.5
Gallium	1,000	17.5
Gold	2,000	6.2
Indium	4,000	2.5
Iron	3,000	10.0
Lead	5,000	3.8
Nickel	5,000	5.0
Palladium	1,500	10.0
Platinum	3,000	17.5
Rhodium	3,000	70.0
Silver	1,250	5.0
Thallium	2,000	12.5
Tin	5,000	2.5
Zinc	3,000	3.8

needed is a rinse under a tap.

▶ **Preparation**—For the removal of light rust or for new parts, the work is connected to the negative lead and cleaned and deoxidized with the cleaner supplied. This is applied by the cotton-wrapped anode dipped into the solution. The work is rinsed with water and is then ready for plating.

Aluminum, stainless steels and hard steels can be plated easily but require a slight etch, obtained with a special solution supplied, and a little abrasion with aluminum oxide. After vapor blasting, titanium and molybdenum can also be plated successfully, the latter being coated with platinum by many electronic equipment manufacturers in Europe.

▶ **Applications**—For electrical and electronic contacts the process is particularly effective. Contacts are usually only plated over a small area and consequently extensive stopping-off is ordinarily necessary. With this process even the smallest sections can be silver or gold plated, with additional rhodium plating for abrasion resistance if desired, at relatively low cost. Silver-plating aluminum bus bar is also an important application.

Metal inserts and contact faces in molded plastic parts, which

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• We appreciate your having given Photocircuits Corporation so many orders for Printed Circuitry and allied electronic sub-assemblies. We believe you will continue to do so because of our . . .

1) Technological LEADERSHIP. Pioneering, and our policy of promoting the free exchange of engineering information, have been the "role" of Photocircuits Corporation in the relatively new field of printed circuitry. The recently published "Standard Printed Circuit TOLERANCES" has been well received. After quickly dispensing 15,000 copies, we are heavily backlogged with requests for additional copies.

2) Production EXPERIENCE and CAPACITY. Over 7000 different applications of printed circuits and associated assemblies have been produced to date by Photocircuits Corporation! This is the kind of experience in production that has led to the building of our large new plant shown below . . . exclusively for the research, development and production of the industry's expanding printed circuit requirements.

3) Reputation for QUALITY. "Ask the man who . . .", to paraphrase a famous slogan, and you will receive testimony other than our own self-appraisement! A recent, impartial, survey placed Photocircuits "first" by a factor of 3 over our nearest competitor among those considered in purchasing printed circuitry! Our aim is to continue to merit your CONFIDENCE.

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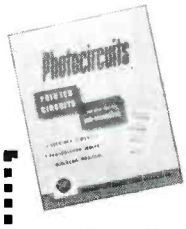

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- ☐ *Photocircuits' Engineering Brochure*
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- ☐ *P-4 Etched or Plated Conductor Characteristics*
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- ☐ *P-6 Switch Plates & Commutator Discs*
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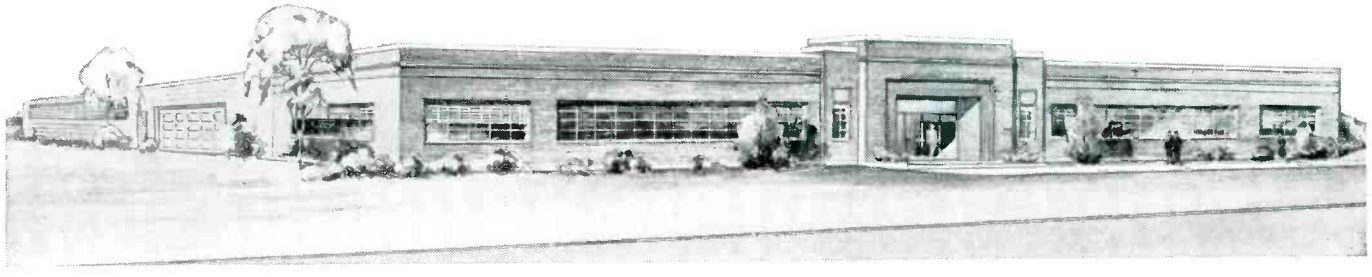


cannot usually be immersed in a bath of plating solution without risk of distortion or erosion of the plastic material, can be plated easily.

When gallium and indium are being used for forming a vacuum seal for tubes, a small ridge is machined on one of the nonferrous (usually copper) mating surfaces. This ridge is gold-plated, after which the mating surfaces are coated with gallium or indium by the process. Hand pressure at room temperature for gallium, or a low-temperature furnace for indium, creates diffusion of the metals, forming an alloy and producing a tight seal.

Among other uses are the plating of radar waveguides and platinum plating of molybdenum wire for electronic tubes to control secondary emission. This is being done on a commercial scale by automatic operation. The wire, unwinding from a reel, passes through a series of padded styluses which are drip-fed with the solutions, the intermediate rinsing being carried out by sprays.

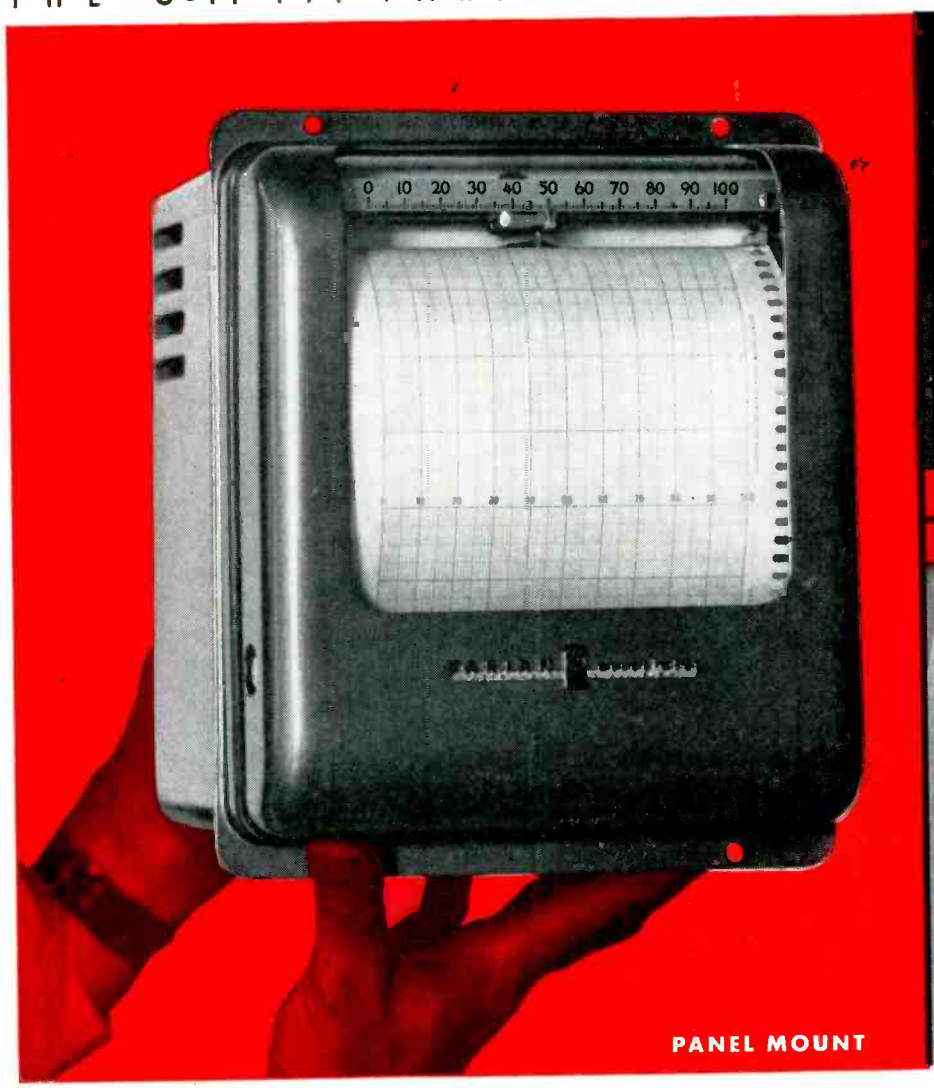
Jig Transits Speed Antenna Tower Welding

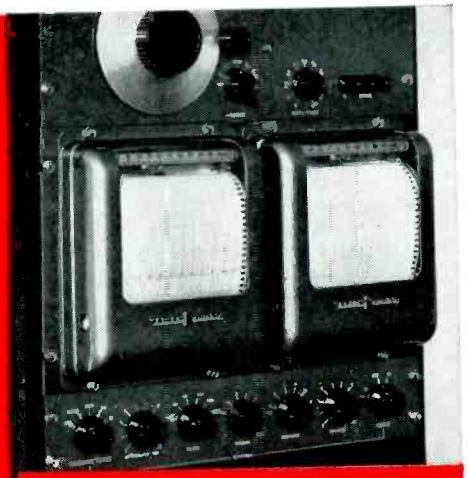
JIG SETUP TIME for making prefabricated sections of television towers has been greatly reduced by using Keuffel & Esser jig transits for alignment in the North Wales, Pa. plant of Stainless, Inc. With this optical tooling instrument, the

Examples of tower sections welded with aid of precisely aligned fixture

NEW STRIP CHART POTENTIOMETER RECORDER $395

THE G-11 . . . VARIAN'S NEWEST ACHIEVEMENT





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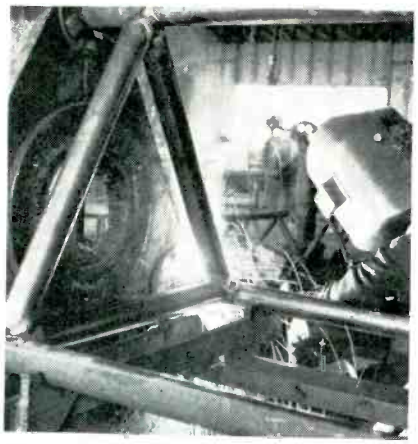


Welding tower tubing to flange bolted to pad on base plate

towers are now being held to tolerances of 0.001 inch, whereas formerly it had been difficult to hold the towers to tolerances of 0.008 inch when using a conventional surveyor's transit.

▶ **The Problem**—The antennas are manufactured in sections 20 or 25 feet long, for on-the-spot bolting to form guyed towers up to 1,200 feet high for uhf and vhf television transmitters, microwave repeaters and other uses. In a tower this high, perfect alignment without the slightest twist or tilt is highly important because a tower which is not completely plumb is potentially dangerous.

In constructing prefabricated triangular sections of a television tower which will rise one-fifth of a mile into the air, a chief difficulty is to make the six ends of each triangular section completely parallel, so that when 50 or more sections are fastened end to end the resulting tower will be rigidly perpendicular.

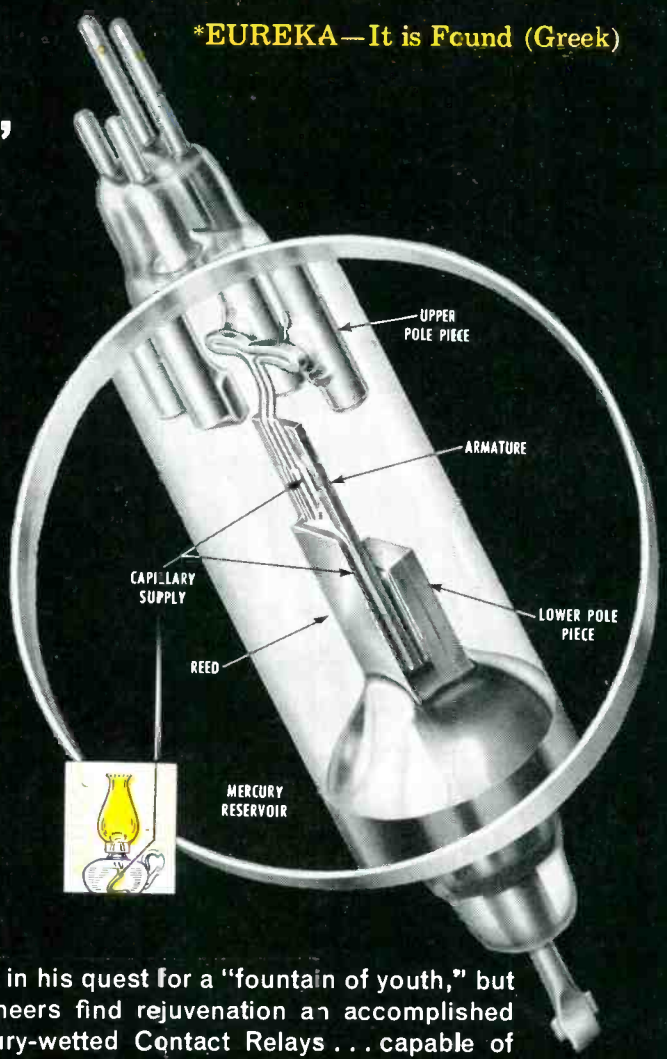
The individual triangular sections, which are usually of a welded lattice-work construction using tubular members, are set up in horizontal jigs between reference pads on two vertical plates, each having three reference pads for

Welding tower section in aligned fixture

ΕΥΡΗΚΑ*

*EUREKA—It is Found (Greek)

INDUSTRY FINDS A "FOUNTAIN OF YOUTH" IN THIS SELF-REJUVENATING CLARE RELAY



Drawings (left) from stroboscopic photographs show the cycle. (a) Filament of mercury forms between the contacts as they separate. (b) This becomes narrower in cross section and (c) finally parts at two points, allowing a globule of mercury to fall out. Mercury flows up the capillary path, replaces amount lost, restores the equilibrium. (d) The momentary bridging of the parting contacts—and the extremely fast break that ends it—minimizes the arc and adds greatly to contact load capacity. Contact closure between the two liquid surfaces bridges mechanical bounce and prevents any chatter from appearing in the electrical circuit.

Ponce de Leon failed in his quest for a "fountain of youth," but modern design engineers find rejuvenation an accomplished fact in CLARE Mercury-wetted Contact Relays . . . capable of billions of operations.

Contacts of these relays are constantly renewed. By capillary action, like that of a lamp wick, a new film of mercury coats the contacts with every make and break.

The magnetic switch is sealed in a high-pressure hydrogen atmosphere in a glass capsule. Surrounded by the operating coil, the capsule is enclosed in a vacuum-tube-type steel envelope.

Unlike ordinary relay contacts, these contacts never wear out; never get dirty; never lock or weld; never get out of adjustment; never bounce.

Send for CLARE Engineering Bulletins No. 120 and 122. Address C.P. Clare & Co., 3101 Pratt Blvd., Chicago 45, Illinois. In Canada: C. P. Clare & Co., 659 Bayview Avenue, Toronto 17. Cable Address: CLARELAY.

CLARE RELAYS

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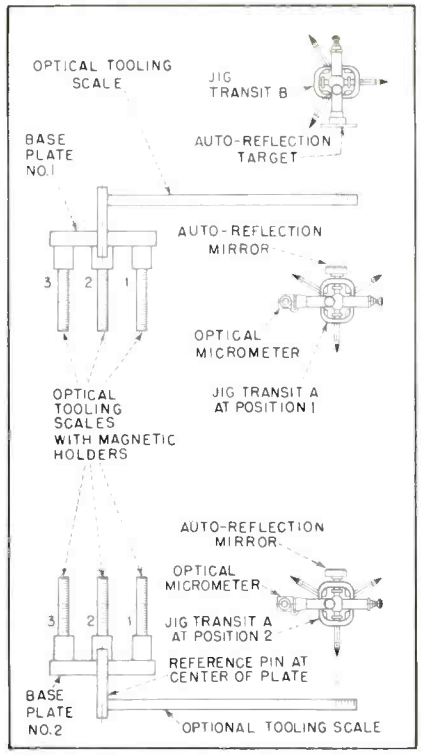


FIG. 1—Steps in aligning base plates between which a 20-foot antenna tower section is assembled and welded

the tower rods. Before welding begins, it is essential that these reference pads be parallel to each other and perpendicular to a reference line through the center of the jig.

▶ **The Tool** — Fundamentally, the jig transit is a surveyor's transit without horizontal or vertical circles and verniers and with only a single center such as is used in a conventional level.

▶ **Procedure** — The first checking step in the setup procedure, as developed by John Amey of the antenna firm, is to buck in a jig transit on vertical base plate No. 1 to check its vertical plane. As shown in Fig. 1, jig transit A is mounted on a mechanical lateral adjuster supported on a tripod at position 1. Optical tooling scales with magnetic holders are placed on two of the tower flange locations, such as at pads 1 and 3.

The jig transit is now placed so the telescope line of sight is parallel to the plane of the fixture head. The instrument tripod is set up in line by eye first. A pair of adjacent leveling screws is now loosened and the leveling head is rotated until

Selected MINIATURES for TRANSISTOR and PRINTED CIRCUIT APPLICATIONS

Good-All capacitors

Design and component engineers are invited to acquaint themselves with the wide variety of miniature low voltage capacitors developed by Good-All Electric. These compact new designs are ideal companion items for use with transistors and other printed circuit components.

Many space-saving Good-All types are as useful for military as for civilian applications. This is particularly true of the molded-in-Epoxy types. It has also proven to be the case with "wrapped" mylar designs which lend themselves to use in potted subassemblies.

Mylar* dielectric is frequently selected for Good-All miniatures because of its superior electrical characteristics — high I.R., low power factor and excellent stability with life. The space-saving it offers in low voltage designs is also an attractive feature.

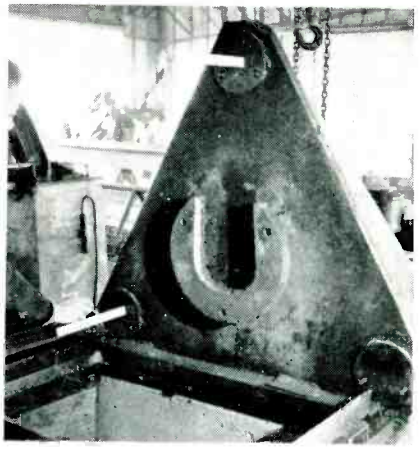
Good-All offers a wide selection in 50 Volt miniature designs

	REPRESENTATIVE TYPES	TYPICAL SIZE COMPARISONS Cap.	Volts	Diam. Lgth.
AXIAL LEAD	**600UE** . . . Mylar dielectric winding molded in dense, moisture-resisting Epoxy.	.01 .1 .47	50 50 50	.312 x 15/16 .438 x 1-3/16 .562 x 1-15/16
	**663UW** . . . Mylar dielectric winding with tough plastic film case and thermo-setting end seals.	.01 .1 .47	50 50 50	.188 x 11/16 .281 x 15/16 .437 x 1-15/16
	613G . . . Mylar dielectric winding, extended foil construction, hermetically-sealed metal housing.	.01 .1 .47	50 50 50	.173 x 23/32 .313 x 27/32 .50 x 1-3/16
RADIAL LEAD 	**600RE** . . . This novel design combines features of conventional tubular capacitors and upright mounting types. The mylar dielectric winding is completely encapsulated in Epoxy. In addition to its attractive glossy red appearance the Epoxy formulation developed by Good-All yields a tough, durable coating with excellent dielectric strength.	.01 .1 .47	50 50 50	.250 x 11/16 .375 x 15/16 .50 x 1-3/4
UPRIGHT MOUNTING 	**600UPE** . . . Mylar dielectric winding molded in dense, moisture-resisting Epoxy.	.01 .1 .47	50 50 50	.438 x 15/16 .562 x 1-3/16 .688 x 1-15/16
	620UPB . . . Mylar dielectric winding with molded bakelite housing and thermo-setting plastic end seal.	.01 .1 .47	50 50 50	.375 x 1 .375 x 1-1/4 .625 x 1-7/8
	620PM . . . Mylar dielectric winding encapsulated in a plastic impregnated paper tube.	.01 .1 .47	50 50 50	.343 x 15/16 .410 x 1 .562 x 1-3/4
EPOXY COATED CERAMIC DISCS 	These Epoxy coated discs are ideal for use on printed circuit boards that are to be dip soldered, since no wax coating is necessary. The available types of ceramic discs are too numerous to describe in detail. A complete brochure with specifications on each type will be mailed to you upon request.	Dimensional information is contained in the Good-All ceramic disc brochure.		

*DuPont's trademark for polyester film.

Write or phone for consultation on specific design problems or to secure detailed specifications on the various capacitor types shown.

GOOD-ALL ELECTRIC MFG. CO.
OGALLALA, NEBRASKA *A leading manufacturer of Tubular and Ceramic Disc Capacitors*



Base plate at end of fixture, showing scales with magnetic holders on two of the three pads for the tower flanges

Checking base plate No. 1 with first jig transit

a pair of opposite leveling screws is roughly in line with the vertical plane to be established. The two plate bubbles on the transit are centered. The transit telescope is aimed at a graduation on the far scale, then aimed at the near scale without turning the instrument about its vertical axis.

After noting where the line of sight falls on the near scale, the instrument is moved with the mechanical lateral adjuster until the line of sight has moved in the direction of, and slightly beyond the corresponding graduation on the near scale. The photo bubbles are recentered, the telescope is re-aimed at the far scale, the near scale is checked again, and the adjustments are repeated until the line of sight checks out the same on both scales.

One of the scales is now moved to pad 3 on base plate No. 1 and this point is similarly checked by

CANNON ELECTRIC

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3 IMPORTANT ANNOUNCEMENTS

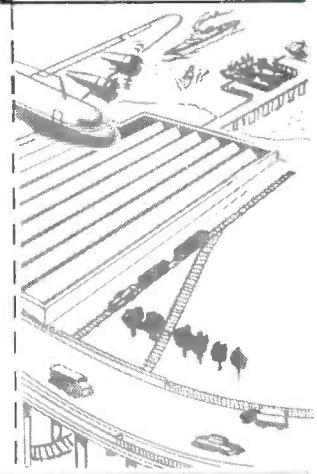
FOR BUYERS OF MULTI-CONTACT ELECTRIC CONNECTORS!

1 DIAMOND DIVISION MOVES TO SALEM, MASS.

On December 1, 1956 the Diamond Division of Cannon Electric Co. moved headquarters and all manufacturing facilities from Wakefield, Mass. to the Salem Industrial Center, Salem, Mass., in the heart of the Eastern Electronics Industry.

Faster Service. The new location has excellent sea, air, truck and rail facilities and will provide faster service for all Cannon Electric customers east of the Mississippi.

Duplicate Tooling. The new Salem plant has 100,000 square feet which leaves plenty of room for expansion. Duplicate tooling is planned of many of Cannon proprietory items, which will give you, our customers, a dual source of supply. In addition to supplying Cannon coaxial connectors, the Salem plant will produce the D miniature line, and the DPX connectors to start with, additional lines and items being added later. Further expansion is planned, including modern molding and die-casting facilities, which will practically be duplicating facilities of our parent plant in Los Angeles.



2 CHANGES NAME TO EASTERN DIVISION, CANNON ELECTRIC CO.

Effective December 1, 1956 the Diamond Division Cannon Electric Co., has been changed to EASTERN DIVISION, Cannon Electric Co.

EAST OF THE MISSISSIPPI

Send Orders for standard AN's, audio connectors, D miniatures, coaxial connectors, K miniatures and standard K connector distributor items to:
CANNON ELECTRIC CO., EASTERN DIVISION
PINGREE & LEAVITT STS., SALEM, MASSACHUSETTS
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WEST OF THE MISSISSIPPI

Send Orders for all Cannon products to:
CANNON ELECTRIC CO.
3208 HUMBOLDT ST.
LOS ANGELES 31, CALIFORNIA
Telephone: CApitol 5-1251
Teletype: Los Angeles, Calif. 872

3 WILL CONSOLIDATE FACILITIES AND SERVICES WITH THOSE OF EAST HAVEN, CONN. PLANT

All East Coast Facilities Under One Roof. On March 1, 1957 all manufacturing and service facilities of the East Haven, Conn. plant of Cannon Electric Co. will be moved to the Salem, Mass. plant. These operations, combined with the former Diamond Division equipment, will give a consolidated plant offering the most modern manufacturing, engineering, design, and laboratories available on the East Coast for the production of high-reliability multi-contact electric connectors.

Service Store Operation Expanded. Greatly expanded facilities, and expanded inventories, will provide better "off-the-shelf" service by the Cannon East Coast Service Store, which will also be at the Salem plant (moving from East Haven) after March 1.

7 PLANTS AROUND THE 7 SEAS!

Cannon Electric Co. is the world's largest manufacturer of multi-contact electric connectors for the aviation, electronics, broadcasting and automation industries. Plants in Los Angeles, Salem, Mass., Toronto, Can., Melbourne, Austl., London, Eng. Manufacturing licensees in Paris and Tokyo.

Manufacturers Representatives,
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CANNON PLUGS

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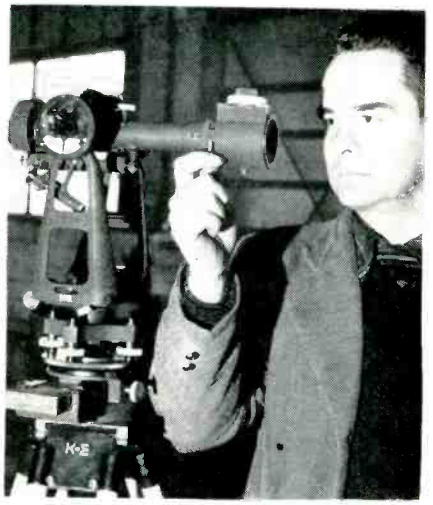
swinging the telescope up and down. If the third point is not in line, the pad on the base plate is adjusted until it does line up with the other two pads in a vertical plane.

▶**Setting Second Transit** — The next step is placing jig transit B in position so its line of sight is exactly at right angles to that of jig transit A. This part of the procedure utilizes an auto-reflection mirror on jig transit A and an auto-reflection target on the telescope of jig transit B. The position of the second transit is so adjusted that the image of the target as seen in the mirror with the telescope is clearly centered on the viewing cross-lines of jig transit B. This transit now establishes a line of sight at right angles to the plane of base plate No. 1, hence parallel with the tower section.



Auto-reflection mirror is mounted at end of telescope axle, and optical micrometer fits over barrel of telescope as shown

▶**Checking Base Plate No. 2** — Transit A is now moved to position 2 in Fig. 1 and placed in the line of sight of transit B by adjusting until the image seen in the mirror is again centered on the cross-line of transit B. Transit A now establishes a vertical plane parallel to the plane of base plate No. 1. The scales are now transferred to the pads of base plate No. 2 and the telescope is swung up and down to determine whether base plate No. 2 is parallel with the other plate within the acceptable tolerance limits. If parallel, the telescope

DOW CORNING CORPORATION

Silicone Dielectrics

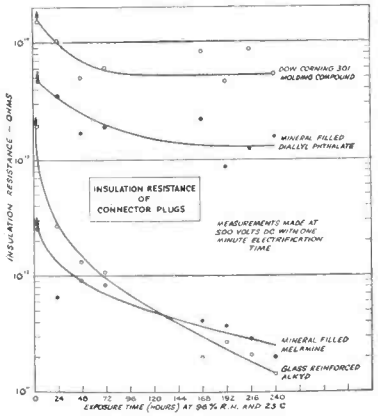
ELECTRICAL AND ELECTRONIC NEWS No. 10

Silicone Molding Compound Has Superior Insulation Resistance

While Dow Corning 301 Molding Compound is frequently specified for electrical parts because of its outstanding resistance to high temperatures, this versatile material also has electrical properties superior to comparable plastics at room temperature. Take insulation resistance, for example—

The accompanying graph traces a summary of tests run on four miniature 26-contact connectors molded by Continental Connector Corporation, Long Island City, N. Y. All plugs were identical in physical form, but each was molded from a different material as indicated on the graph.

Not only did the plugs made of 301 Molding Compound have the highest initial insulation resistance, but their margin of superiority broadened substantially after 240 hours at 96% RH. These tests were

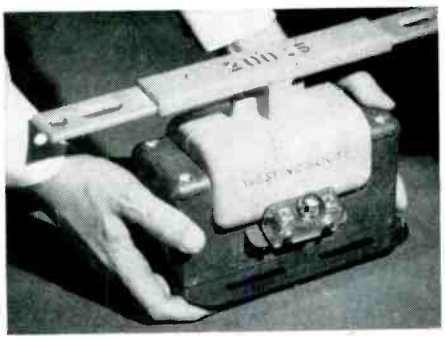


conducted at room temperature; at elevated temperatures the superiority of the silicone molding compound is even more pronounced.

Performance like this is one of the reasons why Continental, among the world's largest producers of connectors, reports increasing interest in "301" molded units. Already undergoing tests in guided missiles, industrial ovens and even kitchen ranges, 301 Molding Compound is manufactured to meet Specification MIL-M-14E, Grade MSI-30. Continental has announced that its entire connector line will soon be available in 301 Molding Compound. *No. 41*

Protect Current Transformer With Silastic Encapsulation

Encapsulation in Silastic*, Dow Corning's silicone rubber, has proved to be an ideal solution to the problem of protecting electrical and electronic components from vibration, heat, moisture and corrosive conditions. An excellent example is found in the new Type 5-kv current transformer made by Westinghouse.



A highly compact unit designed for indoor metering or relaying applications, the SM-5 transformer is the smallest, lightest and most durable 5-kv unit ever built. Silicone insulated throughout, the SM-5 easily meets all ASA and NEMA standards.

To further assure top dependability, the entire core-coil assembly is encapsulated in an attractive, one-piece silicone rubber jacket. This jacket remains resilient and retains its original dielectric properties even in locations subject to extreme changes in temperature and humidity. The silicone rubber also expands and contracts with the coil. As Westinghouse aptly describes it, "transformer performance is sealed in to stay." *T. M. REG. U. S. PAT. OFF. *No. 42*

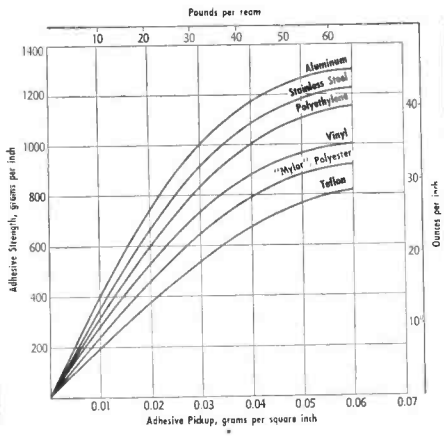
New Pressure Sensitive Tape Offers Outstanding Adhesion at −65 to 500 F

Designers looking for new ways to cut production costs or to improve product performance are certain to find many applications for Permacel EE-3621, a glass-cloth-reinforced tape coated with a pressure sensitive Dow Corning silicone adhesive.

Adhesion values for the new Permacel tape are exceptionally high at extreme temperatures. A 1-inch strip holds—

50 ounces at 150 F
30 ounces at room temperature
74 ounces at −65 F

TYPICAL ADHESIVE STRENGTH OF EE-3621 ON VARIOUS SURFACES



The tape remains tacky and flexible at −65 F and does not become hard or brittle in service at 500 F. It retains excellent moisture resistance and dielectric strength at all temperatures.

Permacel EE-3621 is supplied with a corrugated glass cloth backing to minimize slippage of wire bundles in the production of electrical components.

Although designed primarily for use in Class H motors and transformers, the silicone adhesive permits EE-3621 to be used for many taping applications where extreme temperatures are the order. *No. 43*

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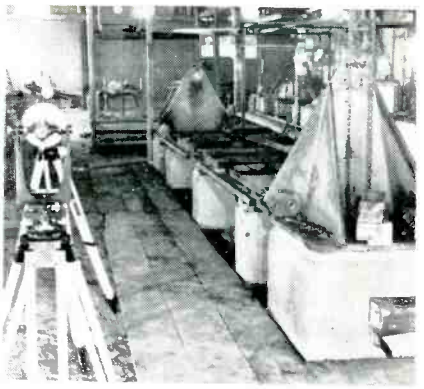


Setup for establishing line of sight parallel to bed of fixture, after checking base plate No. 1 in foreground

sees the same scale reading at each of the three pads. An error as small as 0.001 inch can be detected.

The bed of the fixture is checked by measuring with an optical tooling scale from a center reference pin on each base plate to the line of sight established by jig transit B. The scale is read at each position with an optical micrometer attached to jig transit B. The distance between the base plates is measured with steel tape.

Plastic Cases Protect Airborne Radar Jammers

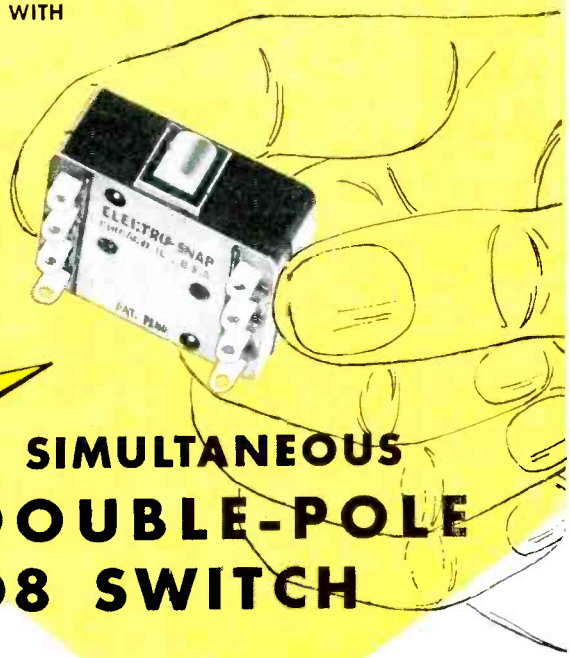
HIGH-SPEED mass production of fibrous glass reinforced plastic shipping containers for GE airborne radar jammer units has been

New process molds nonuniform sections automatically without hand positioning of fibrous reinforcement. Knob is stacking lug, formed in final molding operation in upper half of container. Bottom half has corresponding indentations

Where the switching job is big, but the space is small . . .

Specify . . . **THE ORIGINAL DOUBLE-POLE SWITCH WITH EIGHT CONTACTS.**
Makes possible a wide variety of circuit combinations.

- **THE ORIGINAL DOUBLE-POLE SWITCH WITH SIMULTANEOUS "MAKE AND BREAK" ACTION.**
  Reduces arcing, prolongs switch life, increases electrical capacity and permits unusual applications.
- **THE SMALLEST DOUBLE-POLE SWITCH.**
  Saves weight and space; allows more compact designs.



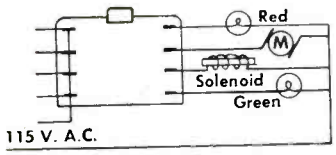
the original

ELECTRO SNAP

SIMULTANEOUS DOUBLE-POLE D8 SWITCH

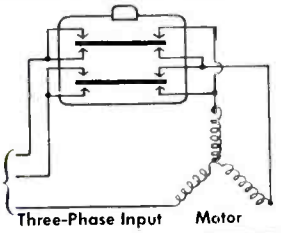
Look What You Can Do With It . . .

Control Four Circuits with ONE Snap



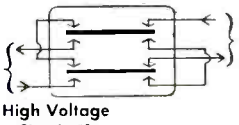
Used in motor control device at left, switch, when actuated, (1) turns off red pilot light; (2) completes circuit to motor winding, starting motor; (3) opens circuit to solenoid latch; locking door to motor gear box; and (4) turns on green pilot light.

Start, Stop, Reverse Three-Phase Motors



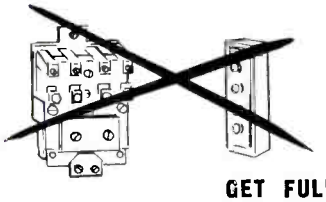
Because this new double-pole switch can simultaneously break or reverse current flow through *two* windings of a three-phase motor, you can use it as an inexpensive limit switch on three-phase lathes and drills. Use it to control automatic sequences, to limit motion of machine members driven by three-phase motors and as a start-and-stop switch.

Wire Movable Poles in Series to Switch High Current or High Voltage



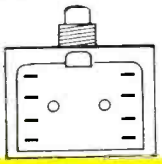
As proof of simultaneous action, you can connect the two movable poles in series to increase contact area for high current applications and to increase number of contact breaks for high voltage switching.

Eliminate Expensive Relays and Additional Switches in Many Applications



This double-pole switch offers designers a wide variety of circuit hook-ups that were formerly possible only with complicated relays or a number of separate switches. Controlling three-phase motors is but one example.

Equip with Actuator



Push-button actuator may be added for panel mounting or for long overtravel. Switch is rated at 15 amps 125/250 v. AC or 10 amps inductive, 30 v. DC. Case dimensions are only 1½" x ⅞" x ½". Weighs only 20 grams.

OTHER ELECTRO-SNAP PRECISION SWITCHES

Standard Basic Switch
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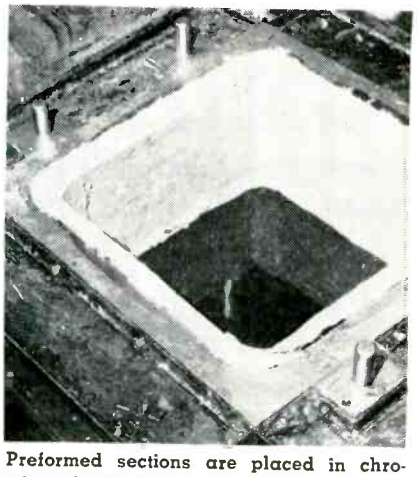
Preformed sides, tops and bottoms for containers are oven-dried for 65 minutes at 160 C



Preformed sections are placed in chromium-plated steel mold, liquid polyester resin is poured in, mating portion of mold is brought down by press and pressure is applied for approximately 4 minutes at 100 C to distribute thermosetting resin evenly through entire preform

achieved by Pressurform Container Corp., Swarthmore, Pa. through use of precision low-cost preforms that eliminate time-consuming layup of reinforced areas. The new process, fully automatic and continuous, makes possible low-cost production of products of nonuniform thickness.

The preforms are the shape of the finished product but consist only of reinforcing material. Ribs, bosses and other protuberances become integral parts of the preform in one operation. The reinforcement is varying proportions of glass fibers and one of several organic materials. The preform, along with a resin such as liquid polyester, is placed in a mold under

Compact amplifier-voltmeter with millivolt sensitivity

High frequency extended range oscillator

Low-distortion, wide-band bridge type signal generator

BIG PERFORMANCE IN SMALL PACKAGES

Type 346 double-duty meter instrument. Serves simultaneously as vacuum tube voltmeter and highly sensitive a-c voltage amplifier.

METER RANGES: 0.001, 0.003, 0.01, 0.03, 0.1, 0.3, 1.0, 3.0, 10.0, 30.0, 100.0, and 300.0 volts full scale. **ACCURACY:** ±3%, 20 cps to 1 mc, ±5%, 10 cps to 2 mc. **STABILITY:** ±1% at any line voltage between 105 and 130 volts ac. **INPUT IMPEDANCE:** 10 megohms – shunted by 24 uuf. **AMPLIFIER:** Maximum voltage gain 1000; maximum output voltage 1 volt. **OUTPUT IMPEDANCE:** 600 ohms resistive. **HUM AND NOISE:** One minor division max. **OVERLOAD:** Automatic overload protection. **POWER REQUIREMENTS:** 117 volts ±10%, 50-400 cps 40 watts. **SCALE:** Illuminated 4¼″ damped meter movement. **DIMENSIONS:** 6½″ high, 4¼″ wide; and 7½″ deep overall. Weight: 6½ lbs.

PRICE **$200***

Type 347 extended range oscillator featuring extended high frequency range, low waveform distortion, constant level output and remarkably small physical size.

FREQUENCY RANGE: 18 cycles to 1.1 mc in five overlapping ranges. **DISTORTION:** Total harmonic distortion of waveform less than 2/10 percent when operated into 10K ohms or higher load. **CONSTANT OUTPUT:** Output voltage constant to within ±½ db from 18 cps to 200 kc for any output over 0.1 volt. High range ±2 db. **OUTPUT LEVEL:** 10 volts open circuit. Maximum load current: 4 ma. rms. **OUTPUT CONTROL:** Logarithmic control calibrated in volts. **INTERNAL IMPEDANCE:** Approximately 400 ohms. **CALIBRATION ACCURACY:** ±2% (+1 cycle) from 18 cps to 210 kc, +10% to 1.1 mc. **STABILITY:** ± 0.3% for line voltage range of 105 to 130 volts, and ±0.5% for temperature range of 0 to 50°C. **HUM AND NOISE LEVEL:** 3.0 Millivolts or 60 db below output signals, whichever is greater. **DIMENSIONS:** 6½″ high, 4½″ wide, 6″ deep overall. Weight: 6 lbs.

PRICE **$150***

Type 348 signal generator provides low distortion sinewave signals between the frequencies of 0.9 cps and 510 kc. Just right for design investigations of magnetic amplifiers, servomechanisms, computers and general laboratory and field use.

FREQUENCY CHARACTERISTICS

RANGES: 0.9 cps to 510 kc in six ranges. **STABILITY:** ±0.5% for frequencies up to 100 kc for line-voltage variations 105 to 130 volts and temperature within 0 to 50°C. **CALIBRATION ACCURACY:** ±2% (+½ cycle) above 10 cps; ±5% below 10 cps. **DISTORTION:** Less than 0.1% over most of the useable range rising to less than 0.3% at 30 cps.

AMPLITUDE CHARACTERISTICS

OUTPUT LEVEL: 50 volts, ±10% 2 watts or 40 ma maximum. **OUTPUT RANGES:** Continuously variable from 0 to 0.05V.; 0.5 volts; 5.0 volts; 50.0 volts. **STABILITY:** ±0.5 db referred to 1 kc over the entire frequency range. **OUTPUT IMPEDANCE:** At the 50 volt output range – 6 ohms in series with 1000 microfarad; 5 volt output range–6 ohms in series with 1000 uf; 0.5 volt range–55 ohms; 0.05 volt range–6.2 ohms. **POWER SUPPLY REQUIREMENTS:** 117 volts ac, ±10%; 50-400 cps, 110 watts. Fuse protection; 1.6 amperes, slow-blow. **DIMENSIONS:** 9-7/8″ high, 7-5/16″ wide, 10-11/16″ deep overall. Weight: 19 lbs.

PRICE **$325***

** Price slightly higher in 50 cycle areas.*

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pressure to produce the finished product.

Preforms can be turned out by the new Pressurform process in 30 seconds to 2½ minutes, depending on design.

The precision with which the preform is made permits use of the entire preform in the mold, eliminating the waste of pinchoffs. The process also achieves a product of uniform density by maintaining a constant ratio between the glass reinforcement and the resin regardless of varying container wall thickness. Different proportions of glass to other reinforcements can be used to meet different strength and cost requirements.

Removing container half from mold, completely finished and ready for attachment of hardware

First commercial mass production of military containers of reinforced plastic went to the Light Military Electronic Equipment Department of General Electric Co. in Utica, N. Y. for use with radar jammer units.

► **Problems**—In recent years, the military supply system has been attempting to find an acceptable container for packaging various components. Many different models are now being accepted in spite of the fact that they cannot meet pressure retention requirements after undergoing the rough handling tests prescribed in MIL-P-116B.

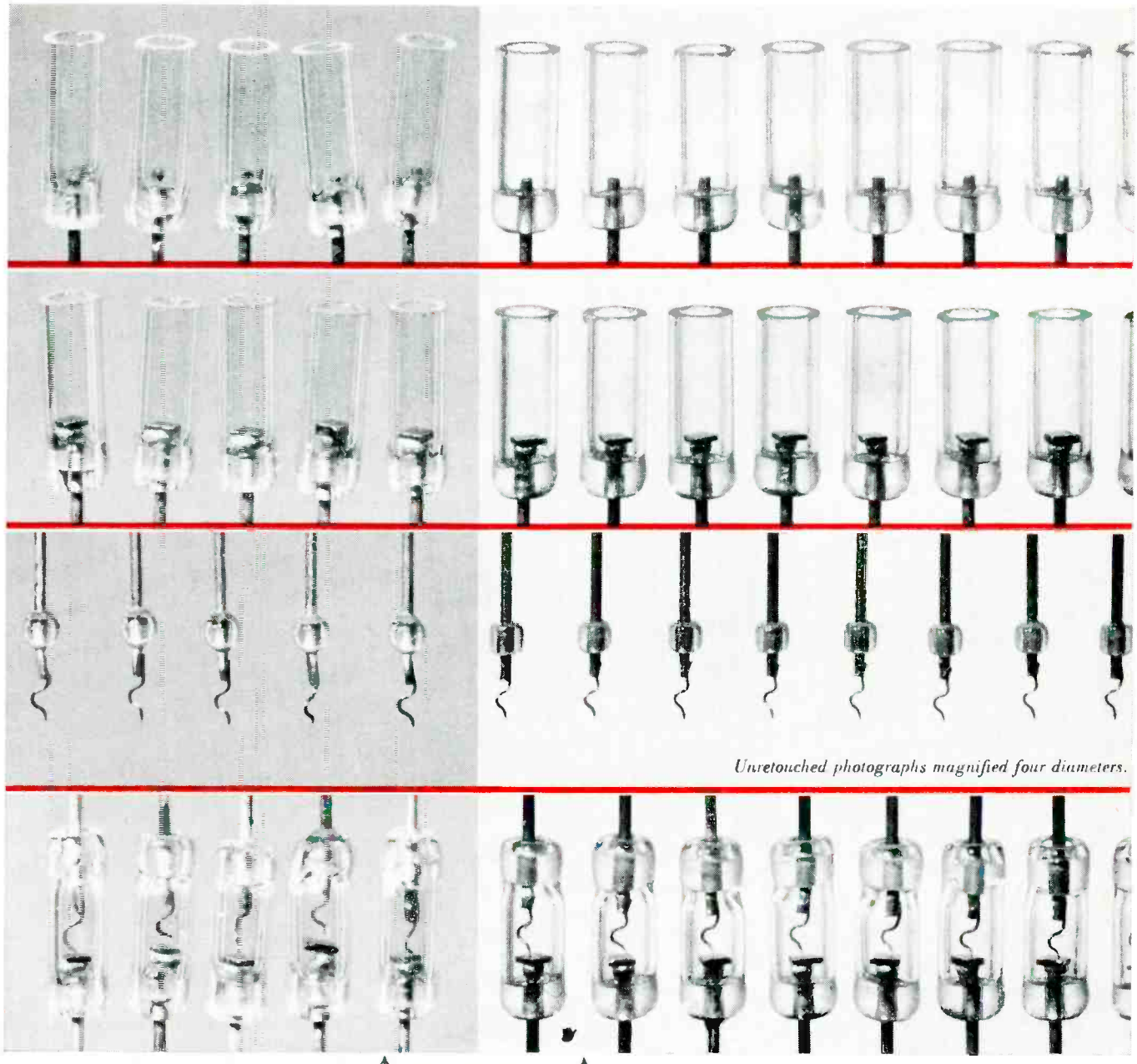
Rust and distortion are not the only enemies of a container. The concept of air-lifting military

hardware and spare parts has added several new problems to those previously encountered. At present, transport planes fly at an average altitude of 25,000 feet. Future planes are expected to cruise at 40,000 feet. This makes it necessary to consider the variations in pressure and temperature that are encountered when an airtight container is carried from sea level to an extreme altitude. The pressure differential between sea level and 40,000 feet is approximately 12 pounds. With this in mind, Wright Air Development Center included in its specifications a 10 pounds per square inch test for all containers, not as a check of the seal but to ascertain whether or not the container would rupture or distort when subjected to high internal pressure.

With aluminum and steel containers this problem can be licked by the use of pressure relief valves that allow air to escape as the plane climbs but prohibit air from entering. A manually operated air valve must then be installed to allow air to be bled back into the container under controlled conditions after landing. If this were not done, the partial vacuum would make it impossible to open the container.

Fibrous reinforced plastic con-

GE packaging engineer Richard H. Thomas demonstrates how top cover is closed after setting electronic unit in recess of rubberized fiber inner cushion



Unretouched photographs magnified four diameters.

Hand assembled diodes ↑ **COMPARE** ↑ *Automatically assembled CBS diodes*

UNIFORMITY

by and for automation

The increasingly automatic assembly of electronic equipment is placing serious limitations upon component manufacturers. Rigid, tight tolerances must be maintained to avoid jamming the automatic machines. This spells automation for components, too.

CBS has done something about it. On seven integrated machines, CBS glass diodes are automatically assembled, packaged, tested. The picture tells the story . . . compares the results of this automatic assembly with that of ordinary hand assembly. The controlled uniform quality is apparent. As you would expect, the uniformity is both mechanical and electrical.

Take advantage of CBS Advanced-Engineering. Specify CBS glass diodes for uniformity . . . for dependability . . . for automatically controlled quality.

CBS semiconductors

Reliable products through Advanced-Engineering

CBS-HYTRON
Semiconductor Operations, Lowell, Mass.
A Division of Columbia Broadcasting System, Inc.

Ordinary pliers suffice for tightening or loosening quick-opening fastener used on containers. Aluminum gasket retaining rings inside facing surfaces provide air-tight seal when container is locked. All four sides have locks

tainers eliminate the need for costly and weight-consuming valves because the plastic can expand easily and contract to adapt to atmospheric or environmental conditions without distorting or rupturing.

Automatic Tapper for Vacuum-Tube Testing

By R. J. MEAGHER
Senior Product Engineer
Receiving Tube Operations
CBS-Hytron
Danvers, Mass.

HAND TAPPING of tubes to reveal intermittent opens or shorts during electrical testing is satisfactory if done properly all the time in a vacuum-tube manufacturing plant. The standard JAN method is to tap the tube three times and then three times again at right angles to the first three blows, using a standard cork mallet. The prescribed distance of swing is usually 4 inches. It is extremely difficult to keep a group of test operators tapping properly, however, since it is considerable effort to swing a mallet 2,000 to 3,000 times an hour.

Previous industry attempts to achieve automatic tapping all seemed to be a compromise between cost of the unit, repeatability, and reliability. The project for mechanizing the tapping operation was therefore divided into

Rugged E-I Compression Seals are the industry's standard for superior performance in commercial and military service. Practically indestructible, they provide the maximum immunity to shock, vibration and temperature changes.

Available in miniature or sub-miniature types, these super-dependable hermetic seals are supplied in economical standard types to meet practically any sealing requirement.

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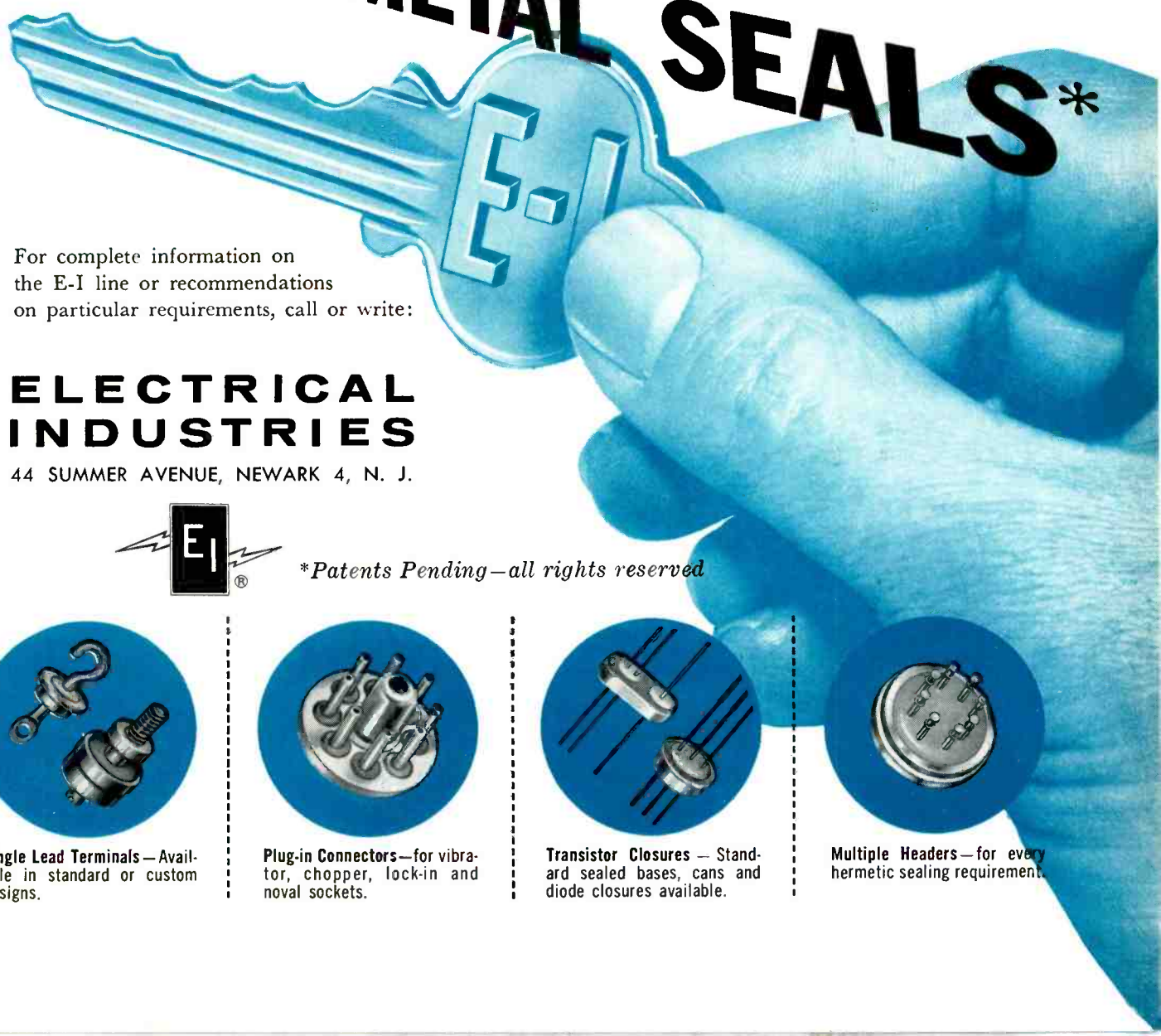
E-I GLASS-TO-METAL SEALS*



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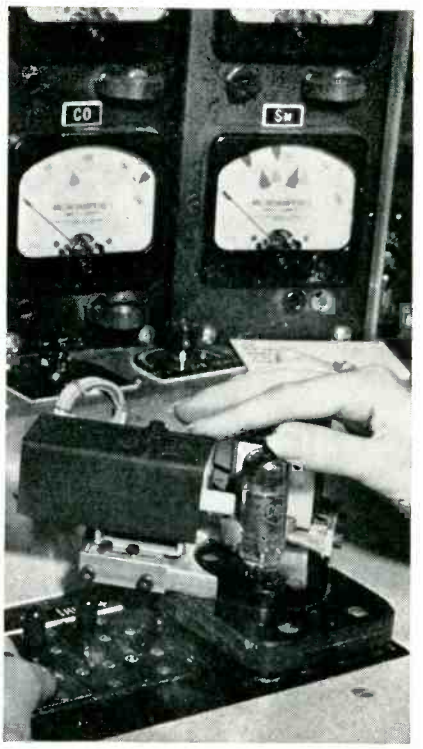
Multiple Headers—for every hermetic sealing requirement.



New automatic tapper in use

five steps: (1) Design and construct the tapping device; (2) establish a primary standard device having proven correlation to hand tapping; (3) design a secondary standard device, easily portable for maintenance; (4) prove the reliability and improvement in inoperables testing; (5) equip production test equipment with automatic units.

▶ **Problems**—A copy of an old two-unit tapper, with the drive supply separate from the tapper head, was made and tried out. It had all three undesirable characteristics in that it was not repeatable, required a great deal of maintenance and was expensive.

The inner bearing surfaces of the solenoids were bored out and a loose-fitting Oilite bearing was installed as in Fig. 1. This elimi-

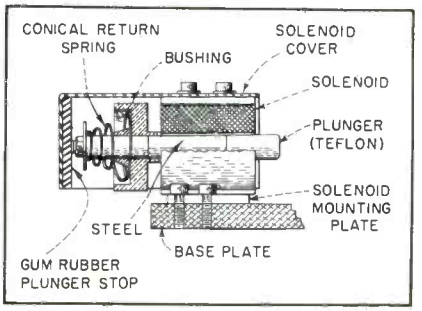
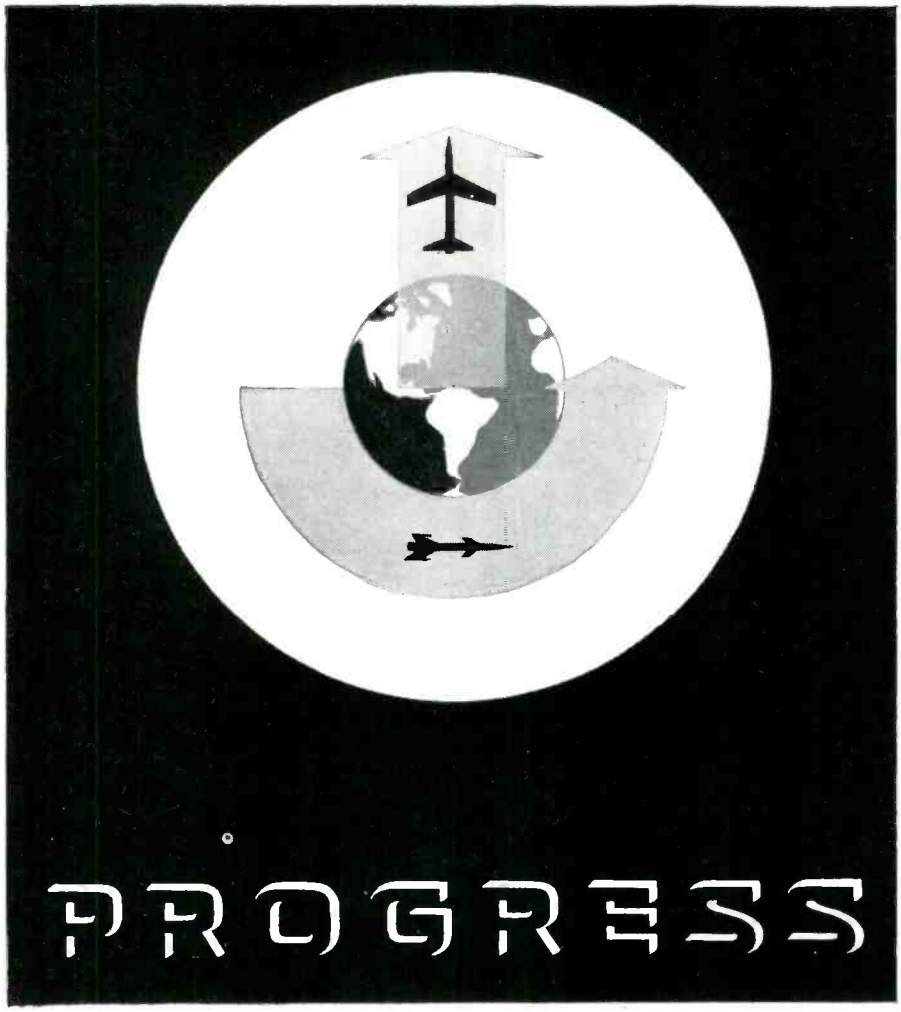


FIG. 1—Construction of tapper solenoid



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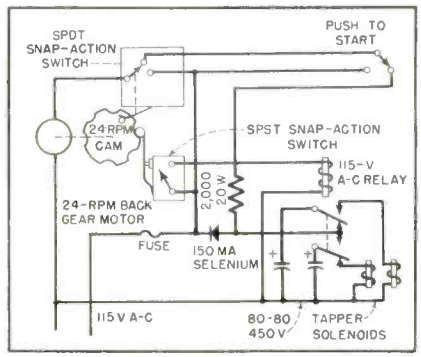
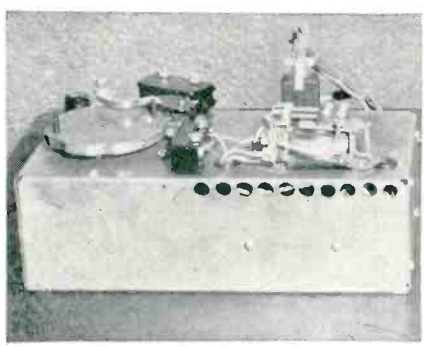


FIG. 2—Complete circuit of tapper

nated binding of the tapper.

All types of materials were tried for the tapping plunger tip, ranging from sponge rubber tips to solid Bakelite. None were satisfactory until Teflon was tried. This material has ideal characteristics in that it is resilient, has a slippery surface and does not wear to any degree. These two steps corrected the repeatability problems.

▶ **Solutions**—The maintenance troubles all occurred in the drive unit, since the old system was a multivibrator-thryatron-relay system which had numerous possibilities of failure. The new system is a motor-driven cam unit with only one relay, using the circuit of Fig. 2. The electromechanical tapper drive unit is designed to energize the two tapping solenoids alternately three times each. Closing the push-to-start initiating switch removes the d-c braking voltage from the motor and applies a-c line voltage to the motor. The motor turns and cam-actuates a snap-action switch that actuates a relay. This relay in turn applies d-c (from a capacitor-discharge supply) alternately to one solenoid and then the other. The rate of tapping and number



Tapper drive unit. Motor-driven cam at left actuates two snap-action switches

ANNOUNCING THE 104 MEMO-SCOPE

The MEMO-SCOPE Model 104 is a new memory oscilloscope with a selection of 5 plug-in preamplifiers that will satisfy the most critical production, test and laboratory requirements. MEMO-SCOPE incorporates the famous Hughes-developed Memotron direct-display storage tube that captures and retains any number of traces indefinitely at a constant intensity until intentionally erased. Traces are readily visible in a brightly-lighted room, and may be easily photographed for file records.

MEMO-SCOPE 104 SPECIFICATIONS

ERASURE: internal waveform generator triggered by front panel push button or by external switch.

DC BLANKING: CRT grid direct coupled to external or internal blanking gate allows beam to be turned off except during sweep and insures constant sweep-time intensity over any sweep duration.

DEFLECTION PLATES: available at rear terminal strip for direct connection.

MAIN VERTICAL DEFLECTION AMPLIFIER: frequency response of DC to 700 kilocycles within 3db. Rise Time of 1/2 microsecond.

TRIGGERED LINEAR SWEEP: range of 10 μsec to 10 seconds per division, adjustable continuously or in 18 calibrated steps. Trigger: vertical amplifier signal, AC line or external pulse, either polarity, DC or AC coupled. Minimum external trigger amplitude: 0.1 volt. Neon ready lamp indicates sweep is at left side of screen, ready for trigger.

AMPLITUDE CALIBRATOR: available at front panel terminal—one kilocycle square wave with peak-to-peak amplitude of 0.01, 0.1, 1.0 or 10 volts, within 3%.

BEAM POSITION INDICATORS are four neon lamps showing position of writing beam when not on screen.

ILLUMINATED GRATICULE: scale calibrated in 1/3" squares in 10 X 10 array.

RACK MOUNTING: Model 104 available on standard 14" X 19" relay rack panel.

DIMENSIONS: 13" wide, 14" high, 20" deep. Etched circuit epon-glass electrical chassis. Hinged camera mount optional.

OPTIONAL PLUG-IN PREAMPLIFIERS INCREASE FLEXIBILITY

(All units with frequency response from DC to 250 kilocycles down 3db.)

WB/4. Wide Band, DC.

WB/SE/5. Wide Band, DC plus Speed Enhancement.

HS/6. High Sensitivity—1mv/division differential.

HS/SE/7. High Writing Speed, High Sensitivity.

HS/D1/10. High Sensitivity, Dual Input.

For additional information or demonstration of the new Model 104 write to HUGHES PRODUCTS
ELECTRON TUBES
International Airport Station
Los Angeles 45, California

HUGHES PRODUCTS

Want more information? Use post card on last page.

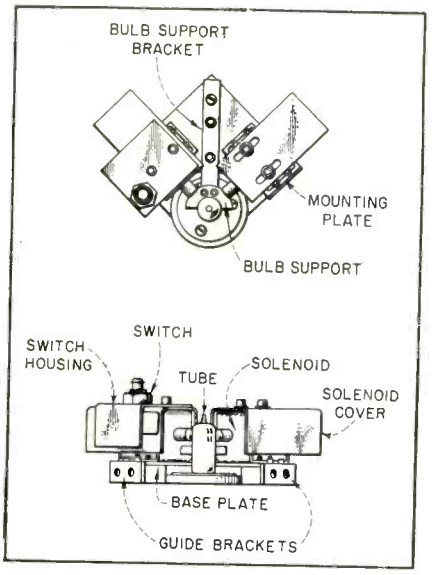


FIG. 3—Tapper solenoid mounting

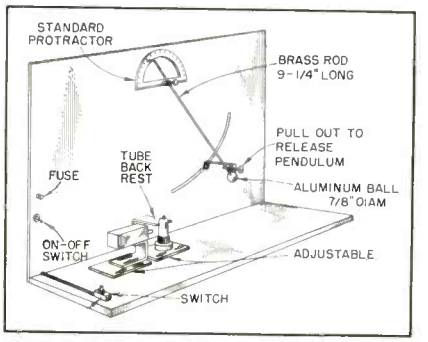


FIG. 4—Details of calibrating pendulum

of blows are predetermined by motor speed and cam design. Tapper solenoid mounting details appear in Fig. 3.

► **Calibration**—A pendulum standard was constructed in Fig. 4 and ten good operators were selected. With a tube in the socket of the standard, each operator tapped the tube ten times on the side opposite the pendulum while the pendulum ball rested against the tube. The rebound reading of each tap on the pointer scale above the pendulum was recorded. Eliminating wild taps, they caused the pendulum to swing back between 6 degrees and 8 degrees. Thus 7 degrees was accepted as the standard blow. Now, one solenoid of an automatic tapper was mounted in the same position as for hand tapping and the tapper was adjusted for a 7-degree blow. This became the primary standard with its own check device.

► **Dummy Standard**—The second-

TECHNIQUES and DEVELOPMENTS in oscillographic recording

PHASE SENSITIVE DEMODULATOR PREAMPLIFIER PROVIDES A DC VOLTAGE PROPORTIONAL TO AN INPHASE COMPONENT OF AN AC VOLTAGE WITH RESPECT TO A REFERENCE.

THE measurement of the amplitude of an AC voltage component is often necessary in performance studies of servo systems or of suppressed carrier signals over the carrier frequency range from 60 to 10,000 cps. In such cases the demodulator responds to inphase signals and rejects quadrature signals.

A circuit with these characteristics for use in an oscillographic recording system can be seen in the Model 150-1200 Servo Monitor (Demodulator) Preamplifier. It was developed by Sanborn as one of twelve interchangeable, plug-in front ends for "150" Series equipment, to be used with the appropriate Driver Amplifier-Power unit in any channel of a "150" system. Elements comprising the circuit from input to output, include: compensated stepped attenuator and cathode follower input circuit, phase inverter, push-pull mixer and demodulator stages, differential DC output amplifier and low pass filter. In addition, the chassis contains a VTVM to facilitate accurate adjustment of the reference voltage, and an overload indicator which lights a warning lamp when excessive quadrature voltages exist.

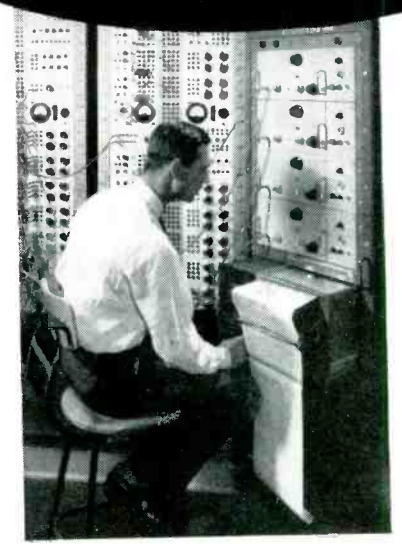
Adaptability to a fairly wide variety of applications is accomplished through broad input voltage, reference voltage and frequency ranges. In order, these are 50 mv to 50 v (for full scale 5 cm deflection), 10 v to 125 v; 60 cps to 10kc. Rise time with low frequency plug-in demodulation filter is 0.1 seconds; with high frequency filter, 0.01 seconds. Quadrature rejection is better than 100:1; for carrier frequencies up to 5000 cycles.

Two representative uses of the Servo Monitor Preamplifier are in the design and adjustment of servo systems, and with instruments used in the design, development or adjustment of other apparatus. The first is illustrated by use of the Preamplifier and associated equipment in the recording of the output shaft amplitude and driving frequency of an AC positional servo; the second by recordings made with a similar setup of the difference between output signals from a gyroscopically-controlled stabilizing device and the "pitch" and "roll" signals generated by a "Scorsby Table" used for testing the device under dynamic conditions.

For a detailed discussion of the principles and design considerations involved in the Servo Monitor Preamplifier, refer to the February, 1955 issue of the Sanborn RIGHT ANGLE, for Dr. Arthur Miller's article on "Measurements with the Servo Monitor Preamplifier."

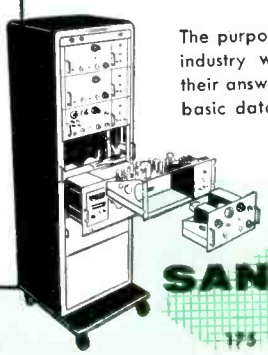
Technical literature and engineering assistance on specific problems are always available from our engineering department.

FROM **SANBORN**



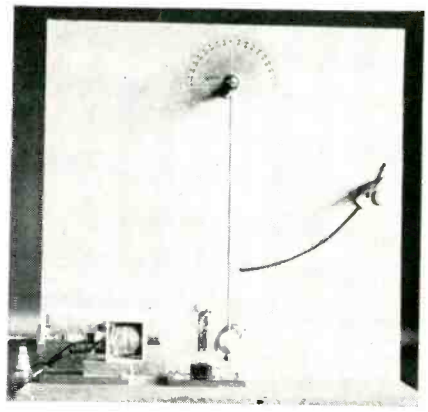
BASIC FACTORS IN SELECTING OSCILLOGRAPHIC RECORDING EQUIPMENT

WHEN considering any oscillographic system or equipment for your application, three useful "yardsticks" to apply are (1) the recording method, (2) equipment adaptability, and (3) variety of equipment available. Here are the answers to the three, as they apply to Sanborn systems. In the record, rectangular coordinates accurately correlate multiple traces, simplify interpretation and eliminate errors. Permanent traces, produced by a hot ribbon stylus without ink, provide sharp peaks and notches, and clearly reveal all signal changes. One percent linearity results from current feedback driver amplifiers and high torque galvanometers of new design; maximum error is ¼ mm in middle 4 cm of chart, ½ mm across entire chart. From the standpoints of "adaptability" and "variety", Sanborn "150" equipment offers the versatility of 13 different plug-in front ends for any basic system . . . the choice of one- to eight-channel systems . . . the variety of nine chart speeds, timing and coding controls, console or individual unit packaging . . . availability of equipment as either complete systems or individual amplifier or recorder units.

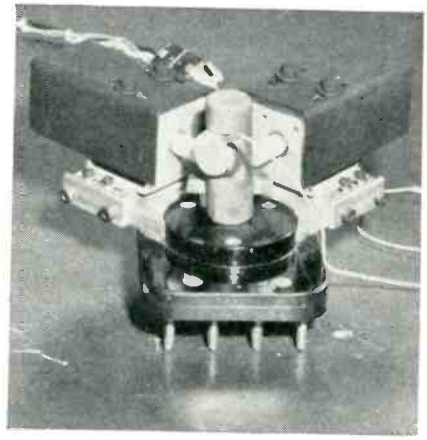


The purpose of the foregoing information is to better acquaint industry with typical oscillographic recording problems and their answers, design considerations in Sanborn equipment, and basic data on what Sanborn makes and how it is being used.

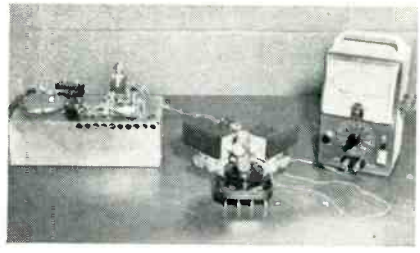
SANBORN COMPANY
INDUSTRIAL DIVISION
175 WYMAN STREET, WALTHAM 54, MASS.



Pendulum-type primary standard



Dummy tube with attached hearing-aid earphone serves as secondary standard. Banana plugs permit plugging tapper into any tube test set



Complete tapper-calibrating setup

ary standard was made up by mounting a hearing aid earphone on a dummy tube made of fibre rod. This hearing aid was directly connected to an a-c vacuum-tube voltmeter. This dummy was mounted in the primary standard, tapped with the preset tapper and the reading on the vtvm noted. This dummy could now be inserted in any tapper and its solenoid position adjusted to give the same vtvm reading. Only the first blow is used, because additional taps would occur while the meter needle is still in motion from the first blow. Since each tap varies somewhat, an average must be taken and a range set around it.

Continental Connectors
TAPER PIN TERMINAL BLOCKS

. . . machine tapered for precision, molded-in for ruggedness

Precision machine tapered feed-through receptacle is permanently molded-in.

HERE IS AN IMPROVED terminal block design featuring precision reamed taper pin receptacles. *Molded-in* for maximum durability, these receptacles maintain a permanently secure electrical and physical contact with AMP Series "53" solderless taper pins.

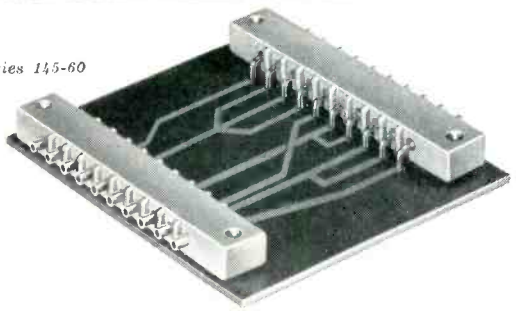
Continental can supply all types of taper pin blocks and connectors for conventional wiring and printed circuitry in any combination of feed-through shorting or non-shorting terminals. Our Engineering Department will gladly cooperate in solving your taper pin application problems. For technical information write to *Electronic Sales Division*, DeJUR-AMSCO Corporation, 45-01 Northern Boulevard, Long Island City 1, New York.

SPECIFICATIONS				
TAPER RECEPTACLES	Brass, gold plated over silver for low contact resistance. 9 lbs. minimum gripping pressure on AMP Series "53" solderless taper pins.	BODY	Molded of high impact Plaskon reinforced (glass) Alkyd 440A (MIL-P-14D, Type MAI-60). Other molding materials on request.

Series 145-58

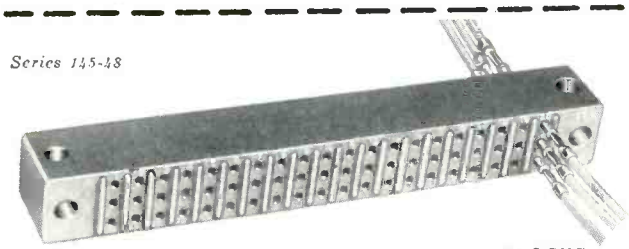
SINGLE ROW TAPER PIN TERMINAL BLOCKS. Available in any combination of feed-through shorting or non-shorting terminals. Molded holes for stacking or mounting.

Series 145-60



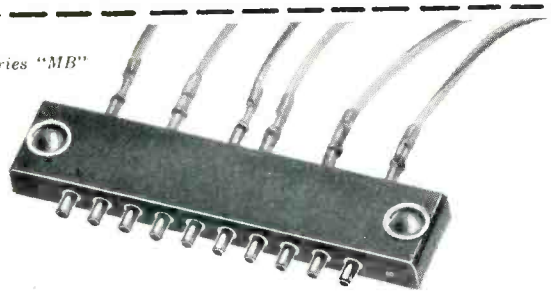
TAPER PIN TERMINAL BLOCKS FOR PRINTED CIRCUITRY. Precision tapered molded-in right angle terminals for dip soldering to printed circuit boards.

Series 145-48



TRIPLE STACKED TAPER PIN TERMINAL BLOCKS. Continental can supply stacked taper pin blocks in any combination of feed-through shorting or non-shorting terminals. Molded holes for right angle and perpendicular mounting.

Series "MB"



TAPER PIN TERMINATION FOR CONVENTIONAL WIRING. Solder cups are provided for terminating conventional wiring to solderless taper pins.

You're always sure with DeJUR electronic components

New Products

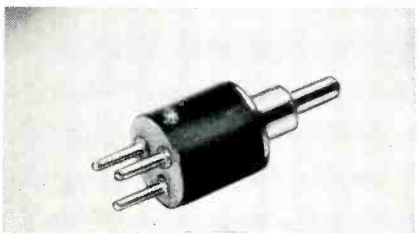
Edited by WILLIAM P. O'BRIEN

81 New Products and 53 Manufacturers' Bulletins Are Reviewed . . . Control, Testing and Measuring Equipment Described and Illustrated . . . Recent Tubes and Components Are Covered

PRECISION POTS

for printed circuits

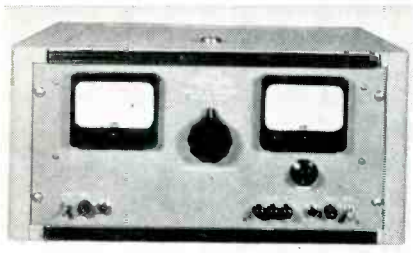
WATERS MFG., INC., P. O. Box 368, South Sudbury, Mass. Simplifying installation in miniaturized assemblies that use printed-circuit techniques, the model APP-½ precision potentiometer is provided with a three-prong base that fits standard three-circuit microphone sockets. The plug-in connection afforded by this unit is also advantageous in automated assemblies for precise positioning and rapid installation.



The potentiometer is available in resistance ranges of 10 ohms to 100,000 ohms, with standard accuracy of five percent below 50 K and two percent above 50 K. **Circle P1 inside back cover.**

D-C POWER SUPPLY

mag-amp controlled



UNIVERSAL ELECTRONICS CO., 1720 Twenty-Second St., Santa Monica, Calif. The Unireg model U32-10 is a wide-range magnetic amplifier controlled d-c power supply. Voltage range extends from 0 to 32 v continuously variable without switching, at currents from 0 to 10 amperes.

This rugged, tubeless unit is regulated for line or load to +1 percent. Ripple is 0.25 percent for all load and line conditions. Transient response is faster than 0.2 sec. Line input range is from 105 to 125 v a-c at 50 or 60 cycles.

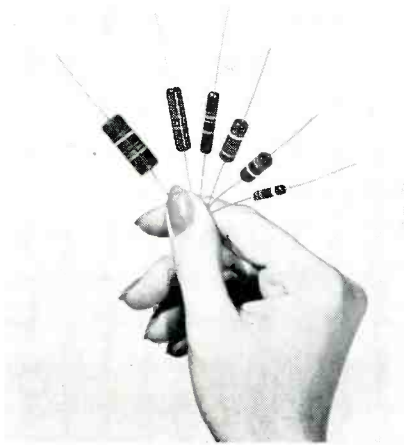
Dimensions are 8¾ by 19 by 14⅞ in. It is available for either rack or cabinet mounting. Net weight is approximately 125 lb. **Circle P2 inside back cover.**

MOLDED CAPACITORS

nine different sizes

GENERAL ELECTRIC CO., Schenectady 5, N. Y., announces a new line of molded PVZ capacitors. They operate from −55 C to +125 C without voltage derating and are for applications in computers, missiles, telephone equipment and other high grade military and commercial equipment. Available in 100, 200, 300 and 400 v ratings, they can be supplied from 0.00047 to 0.022 μf in the 400-v range and from 0.00047 to 0.15 μf at 100 v.

The molded PVZ capacitor is a paper tubular capacitor impregnated with a high temperature organic material which is polymerized into a solid resin. The solid capacitor rolls are contained in a mineral filled phenolic plastic. After molding, the unit is completely solid and has excellent shock and moisture resistance and vibration properties. **Circle P3 inside back cover.**



CIRCUIT PRINTER

allows faster output

GRANT PRODUCTION CO. LTD., 4 Rathbone Place, London, W. 1., England, announces a compact printing unit in which a new kind of light source allows much faster output of printed circuits.

Printed circuits are produced by an ordinary photoengraving process using an improved sensi-

our leadership protects yours...

Our reputation as the world's most Consistently Dependable producer of capacitors has been maintained for over 46 years. But *any* reputation can be lost overnight. That's why we resist the temptation to gain temporary advantage through methods that risk *our* reputation or yours. C-D's Consistently Dependable products can mean PLUS dollars to you.

Widest Choice of Impregnants and Dielectrics to meet your needs: More than a score of liquid and solid impregnating media and dielectrics, including Polystyrene, Mylar*, Teflon, metallized paper and metallized Mylar, are readily available to meet your temperature, size and other circuit requirements. Operating temperature ranges from −40°C to +85°C and −60°C to +200°C. Whatever your capacitor problems, depend on Cornell-Dubilier to fulfill your needs most promptly, most economically and most satisfactorily.

Write for catalog to Cornell-Dubilier Electric Corporation, South Plainfield, New Jersey.

(*DUPONT TM)

CONSISTENT HI-DEPENDABILITY
CORNELL-DUBILIER CAPACITORS

SOUTH PLAINFIELD, N. J.; NEW BEDFORD, WORCESTER & CAMBRIDGE, MASS.; PROVIDENCE & HOPE VALLEY, R. I.; INDIANAPOLIS, IND.; SANFORD, FUQUAY SPRINGS & VARINA, N. C.; VENICE, CALIF.; & SUB.: THE RADIART CORP., CLEVELAND, OHIO; CORNELL-DUBILIER ELECTRIC INTERNATIONAL, N. Y.

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tizer. The process consists of printing a film negative of the original diagram on a copperfoil-clad sheet of Bakelite. The copper foil is cleaned, dried and then coated with a light-sensitive emulsion. The film negative of the circuit diagram is positioned on the sensitized copper and exposed to light on a printing frame.

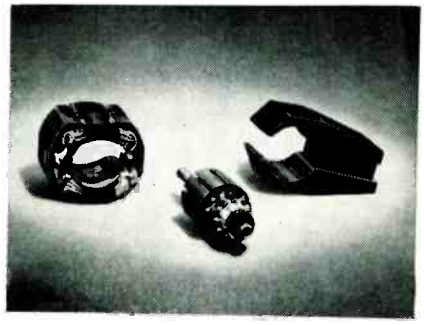
The Mervac printer contains an exposing unit which, instead of the traditional carbon arc, has a totally enclosed mercury vapor light source which cuts normal exposure time to less than one-third and yet provides an image of outstanding definition and strength. Two Mervac models are available. The first, particularly suitable for experimental work in research laboratories, has an exposure time of three minutes. The second is a production model, having an automatic vacuum catch, with an exposure time of only 1½ minutes.

The new printer can be used to produce the film negatives as well as to make the actual printed circuits. The whole unit is operated at bench height and occupies a floor space of only four by three ft. **Circle P4 inside back cover.**

CERAMIC MAGNET

stronger by 3½ times

THE INDIANA STEEL PRODUCTS CO., Valparaiso, Ind. Indox V, a new oriented ceramic permanent magnet material that produces a high peak energy product, and makes possible substantial savings in both magnetic material and space, has been announced. Made of a new ferrite magnetic material which is oriented in the direction of pressing, Indox V produces a peak energy product of approximately 3.5 by 10^6. Its light weight (0.181 lb per cu in.) makes its energy comparable to Alnico V. Because of its 2,000-oersted coercive force, the length of Indox V required is only 28 percent that of Alnico V at optimum operation.



Residual induction is 2,840 gauss. The new product provides a wider high-efficiency operating range than Alnico V because the maximum energy product does not have a sharp peak.

Indox V contains noncritical materials, features high resistivity and a low incremental permeability. It is well suited for such uses as d-c motors, synchronous drives, tv focusers, twt's, loudspeakers and magnetic clutches.

The illustration shows, left to right, an electromagnetic stator, a rotor and an Indox V stator. Additional information on Indox V permanent magnets, with various shapes and sizes available, may be found in catalog No. 16. **Circle P5 inside back cover.**

ACCELEROMETER

weighs only 3 oz

HUMPHREY INC., 2805 Canon St., San Diego 6, Calif., is introducing a miniature accelerometer, weighing only three oz, for use in instrumentation and control systems. Series LA03-0200 is simply and ruggedly designed, has a high output potentiometer pickoff and a pressure-sealed case, and is already in use on target drones and missile systems.

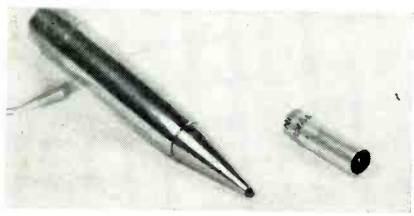
Available with or without connector, the latter uses solder terminals instead. In this design the case height is only 1.5 in.

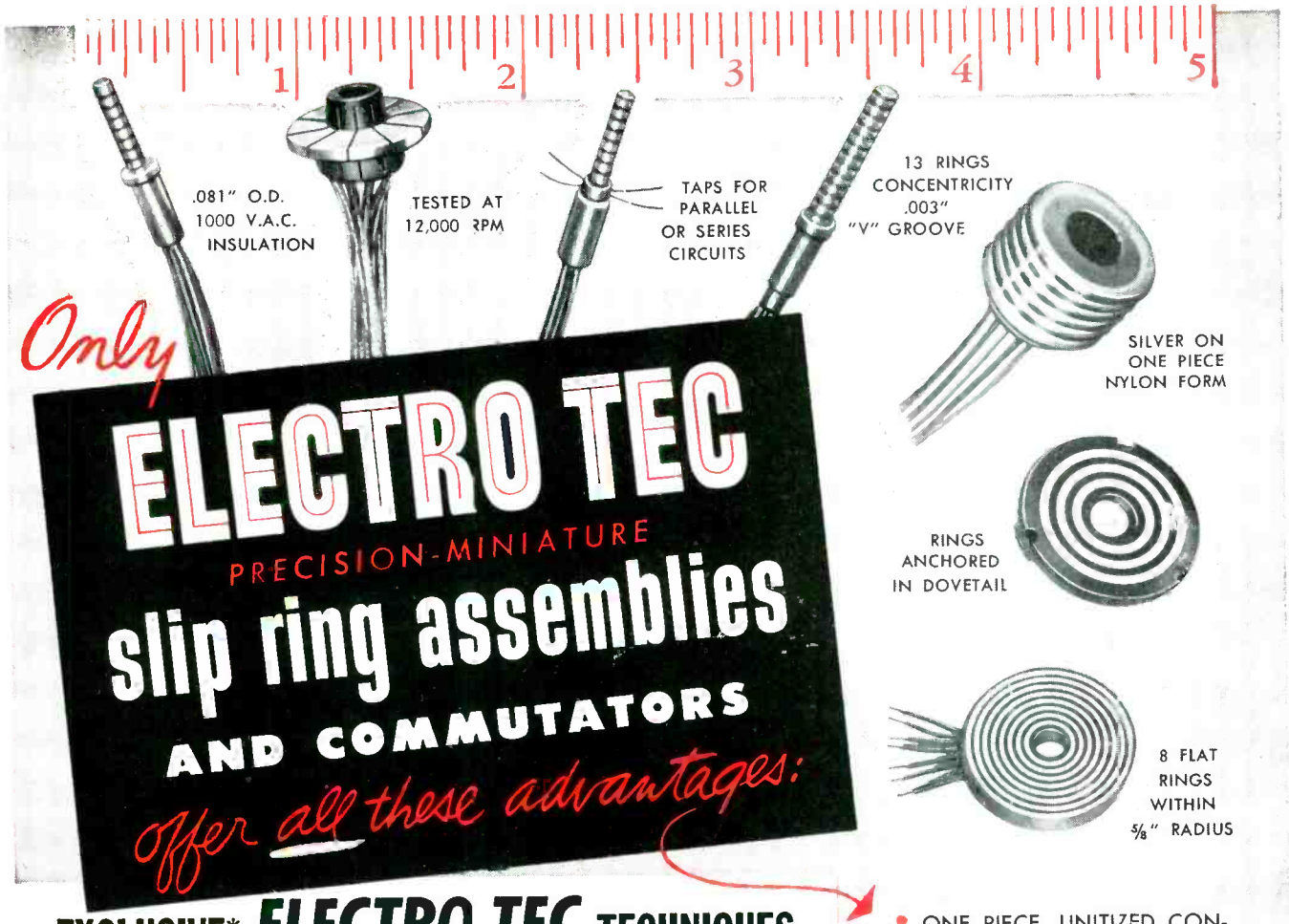
▶ **Features** — Operating temperature ranges from −50 C to +100 C. The unit withstands vibration from 0 to 2,000 cps to 10 g and is shock resistant to 40 g. Linearity is 0.5 to 1.5 percent. Hysteresis is rated at 0.2 to 1.0 percent; friction at 0.15 percent to 1.0 percent; natural frequency at 50 cps (±15 g). Pickoff potentiometer 500 to 10,000 ohms; resolution to 0.3 percent. **Circle P6 inside back cover.**

TRIPOLAR CRYSTAL

for military applications

SYLVANIA ELECTRIC PRODUCTS INC., 1740 Broadway, New York 19, N. Y., has announced a new microwave video detector crystal for military applications which will operate at temperatures up to 150 C. Type IN630 small tripolar crystal operates over a frequency of 1,000 to 12,400 mc, providing a tangential sensitivity of −40 dbm over the range. It differs from conventional crystals in that it provides for a second signal terminal on the coaxial crystal in contrast to the ordinary single-ended construction. This design





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PRECISION-MINIATURE

slip ring assemblies AND COMMUTATORS

offer all these advantages:

EXCLUSIVE* ELECTRO TEC TECHNIQUES

insure closer tolerances, absolute uniformity, and the ultimate in miniaturization

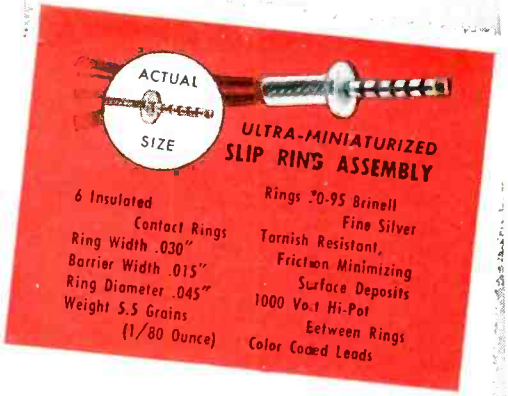
Electro Tec units are the product of an exclusive manufacturing technique that results in accuracy unattainable by conventional fabricating methods. In this process a plastic is moulded around the wire leads. Accurate machining reduces this blank to the proper shape, complete with grooves. Hard silver is deposited into the grooves by electroplating to produce the required rings. Final machining insures concentricity and dimensional accuracy. The result is one-piece, unitized construction with conducting rings of 70 to 95 Brinell hardness.

Diameters of these assemblies range from .045" to 24" cylindrical or flat. Cross-sections may range from .005" to .060" or more. Rings are polished to a jewel-like finish and can be held to 4 micro-inches or better. Even the smallest sizes withstand a 1000 V.A.C. breakdown test. Most types easily withstand rotational speeds up to 12000 rpm.

ELECTRO TEC Assemblies are Specified by the Nation's Leading Precision Instrument and Equipment Manufacturers for Proven Greater Dependability, Longer Life, Smoother Functioning.

The uniformly superior performance of Electro Tec slip ring and commutator assemblies in thousands of industrial and governmental applications has resulted in wide adoption of these component units by most leading manufacturers of precision instruments and equipment. Although these products provide improved performance and extra dependability, prices are strictly competitive. Write today for fully illustrated literature.

- ONE PIECE, UNITIZED CONSTRUCTION
- ABSOLUTE MINIMUM TORQUE FRICTION
- DIAMETERS FROM .045" TO 24.0"
- MINIMUM 1000 V.A.C. HI-POT INTER-CIRCUIT
- UNIFORMLY HARD SILVER RINGS PLATED INTO GROOVES ON PRECISION MACHINED ONE PIECE PLASTIC FORM
- SPECIAL SURFACE DEPOSITS PREVENT TARNISH, MINIMIZE FRICTION, BRUSH NOISE AND PRACTICALLY ELIMINATE WEAR



*PAT. NO. 2,696,570

ELECTRO TEC CORPORATION

SO. HACKENSACK NEW JERSEY

PRODUCTS OF PRECISION CRAFTSMANSHIP BY A NEW AND REVOLUTIONARY PROCESS

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has made possible the simplification and reduction in cost of crystal holders. **Circle P7 inside back cover.**

DELAY NETWORK
available in four models

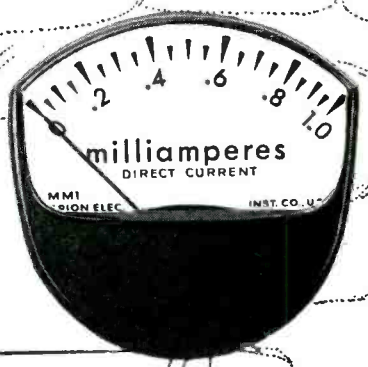
ADVANCE ELECTRONICS LAB., INC., 451 Highland Ave., Passaic, N. J., announces the type 801 continuously variable delay networks with incremental time delay less than 0.08 millimicrosecond and total time delay up to 1,000 μsec. There are four models available each with different total delay. Input impedance is 500 ohms and output impedance is 1,000 ohms for all types.

The temperature coefficient is less than 0.005 percent per deg C. **Circle P8 inside back cover.**

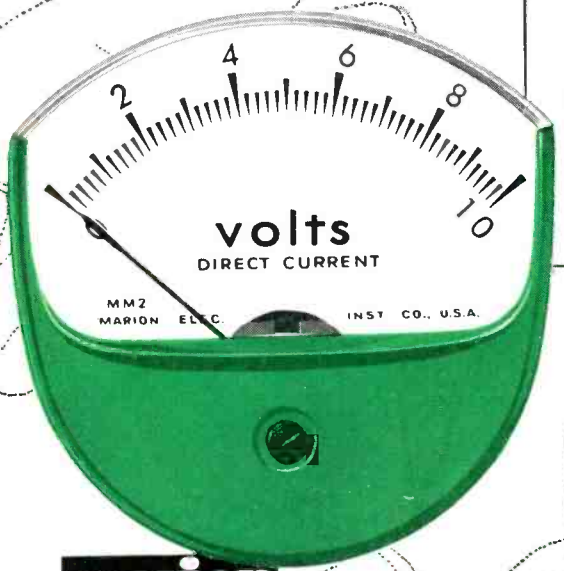
X-Y DIAL DRIVE
for automatic plotting

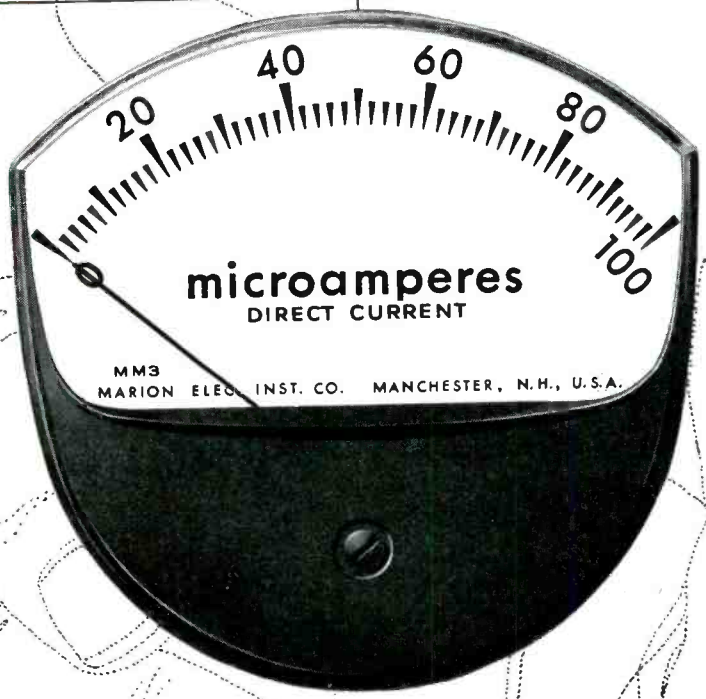
GENERAL RADIO CO., 275 Massachusetts Ave., Cambridge 39, Mass. Automatic sweeping techniques can be used with existing test equipment with the new X-Y dial drives. The new drives make it possible to use a two-axis plotter to obtain permanent and precise recordings of data. The task of reading, logging and plotting point

WHERE ELECTRONICS MEETS THE EYE



marion MEDALIST meters





marion
advancement in instrument design

Three things set Medalists apart from other panel instruments: style, color and readability. Their distinctive shape enhances whatever equipment they become a part of; standard or custom-matched case and dial colors further improve equipment appearance. Longer scale length, larger numerals and better over-all dial illumination vastly increase their readability.

Medalists are made in all standard ranges, in 1½", 2½" and 3½" sizes. They provide a functional beauty that is unique among panel instruments today.

At the I. R. E. Show, March 18-21:
Booth 2126

marion electrical instrument company
GRENIER FIELD, MANCHESTER, NEW HAMPSHIRE

by point values is thus eliminated in either laboratory development or production testing.

Two sizes of drives are available, one for four-in. and the other for six-in. gear-driven precision dials. In each size two speeds are offered, one eight times the other. All models use synchronous motors.

The potentiometer included in the X-Y dial drive is used with a source of d-c to provide a d-c voltage proportional to the independent variable. The output characteristic as a d-c signal is used to drive the Y axis of the recording pen.

All models are priced at $55 each and can be easily installed on General Radio oscillators covering the 20 cps to 2,000 mc range. Separate gear driven dials are available for equipment not already having suitable dials. **Circle P9 inside back cover.**

H-V POWER SUPPLY
is closely regulated

DRESSEN-BARNES CORP., 250 N. Vinedo Ave., Pasadena, Calif., has announced a closely regulated, h-v power supply for use with h-v tubes, twt's, klystrons, photomultipliers and in tube development work. Output range is 400 to 4,000 v d-c, continuously variable without switching; current rating is 0 to 100 ma. Regulation for output voltage range of 2,000 to 4,000 v d-c is 0.1 percent no-load to full-load; below 2,000 v d-c the regulation is 0.25 percent no-load to full-load. For line voltage of 115 v a-c ±8 percent, the change in out-

put voltage from 2,000 to 4,000 v d-c is 0.15 percent. Below 2,000 v d-c the change is 0.3 percent.

Ripple and internal noise are below five mv rms for any voltage or load within the rating. The unit is equipped with positive or negative grounding switch, and three-turn Helipot for vernier adjustment of output voltage. Designed for standard 19 in. rack panel mounting, model 4K-100B is 19¼ in. high and 18 in. deep. Literature is available. **Circle P10 inside back cover.**

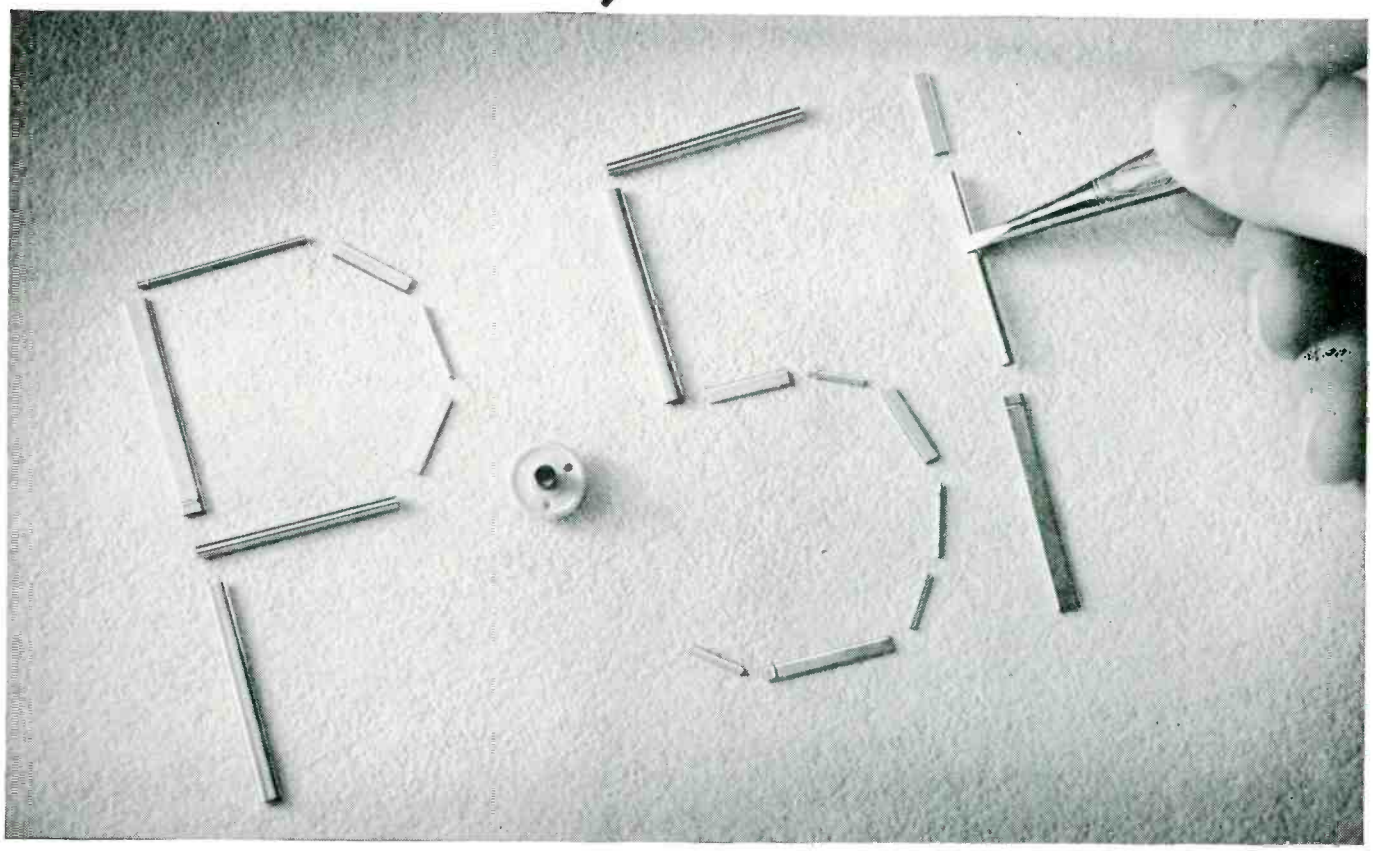
HIGH-POWER KLYSTRON
for radar, linear accelerators

EITEL-MCCULLOUGH, INC., San Bruno, Calif. The X626 klystron is capable of generating 100,000 w of average r-f power and more than 1,000,000 w of peak pulse power. It will be used in radar and linear accelerator operation. The king-size tube, 10 ft 5 in. in length, is the first of a series of super-power Eimac klystron tubes. **Circle P11 inside back cover.**

REJECTION FILTER
for the vhf band

ENTRON, INC., 4902 Lawrence St., Bladensburg, Md. Model DBR is a vhf band rejection filter which

Now—Stronger Passive Cathodes!



Superior announces Cathaloy P-51

— a new passive cathode material

- *100% stronger than Cathaloy P-50, ideal for ruggedized tubes*
- *Free of sublimation and grid emission troubles; low interface impedance*
- *Available in seamless, Weldrawn® and Lockseam* forms*

Latest addition to Superior Tube's family of Cathaloys is Cathaloy P-51 —a passive cathode material with entirely new properties.

NEW INGREDIENT

Cathaloy P-51 is similar to Cathaloy P-50 in chemical composition and electrical characteristics. But the addition of approximately 4% tungsten greatly increases its strength.

HIGH HOT STRENGTH

Tests prove that Cathaloy P-51 is twice as strong as Cathaloy P-50 at operating temperatures. This means it is especially useful in ruggedized tubes. In all tubes, it reduces the risk of failure from shock and of bowing. As with all Cathaloys, the composition of Cathaloy P-51 is carefully controlled by Superior. Every melt is checked in an electron tube before being approved for production.

UPGRADE YOUR TUBES

Cathodes made from Cathaloy P-51 are available in either seamless, Weldrawn or Lockseam form, and can be fabricated to your exact dimensional specifications. Write for technical information. Superior Tube Company, 2500 Germantown Ave., Norristown, Pa.

*Manufactured under U.S. patents.

NOTE. Cathaloy is a trademark of Superior Tube Co., Reg. U.S. Pat. Off.

Superior Tube

The big name in small tubing

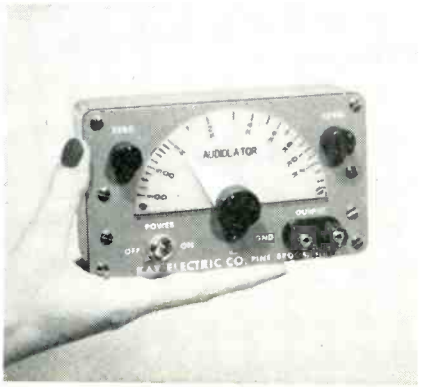
NORRISTOWN, PA.

Johnson & Hoffman Mfg. Corp., Mineola, N. Y.—an affiliated company making precision metal stampings and deep-drawn parts

achieves extreme stability and flexibility with separately tuneable high Q rejection sections. It is especially useful in eliminating adjacent broadband interference or multiple spurious signals and is particularly well suited for use in removing interference to color tv signals. This unit has a nominal 0.5-db insertion loss and ± 0.5-db passband response. Twelve superimposed asymmetrical notches permit a great variety of precision response shapes to be easily achievable. Typical adjustments provide a rejection band 600 kc wide with minimum attenuation of 90 db, 1 mc wide with 75 db attenuation or 6 mc wide and 25 db attenuation.

As a bandpass filter, it will provide 60-db attenuation approximately 1 mc outside the passband with 35-db attenuation 6 mc outside the passband.

Current model (DBR-26) is tuneable in the range of 50 mc to 100 mc. **Circle P12 inside back cover.**



AUDIOLATOR
an all-transistorized bfo

KAY ELECTRIC CO., 14 Maple Ave., Pine Brook, N. J., has announced the Audiolator, a fully transistorized beat-frequency audio oscillator designed for field service, industrial, commercial and military applications. Powered by long-life batteries, a single sweep of the dial covers the audio range of 50 cycles to 15 kc.

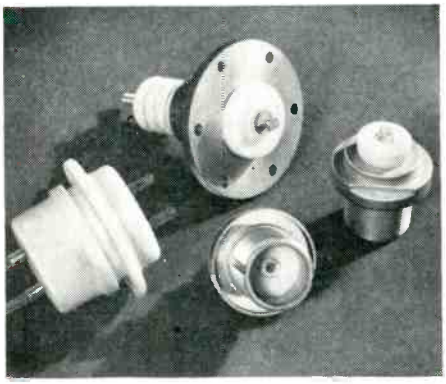
The unit features constant output, built-in stability, no hum and flat output, constant with frequency, of one db over range. No grounds are needed for the instru-

DU PONT
Better Things for Better Living
. . . through Chemistry

ELECTRONIC DESIGN NEWS
LATEST PROPERTY AND APPLICATION DATA ON
TEFLON® tetrafluoroethylene resin

Du Pont TEFLON® resists temperature extremes in electronic aircraft equipment

Lead-through bushings of TEFLON® feature hermetic sealing



LEAD - THROUGH BUSHINGS made with Du Pont TEFLON have excellent corona, arc and ohmic resistance . . . are hermetically sealed against gases, vapors, liquids. (Manufactured by the Joclin Manufacturing Company, North Haven, Connecticut.)

Sensitive tests with the mass spectrometer have proven that gases, conventional insulating oils, silicone oils and their vapors cannot penetrate through connectors using TEFLON tetrafluoroethylene resin as their dielectric. The bushings maintain their seal when cycled repeatedly over a temperature range from −85° F. to +302° F.

In addition, the connectors are resistant to shock. The specially prepared insulators of TEFLON provide mechanical resilience not possible with the usual rigid construction. The moisture-repellent qualities of TEFLON make it possible to use the bushings under the most adverse conditions of humidity. They conform to the applicable sections of Specification MIL-E-5272A.

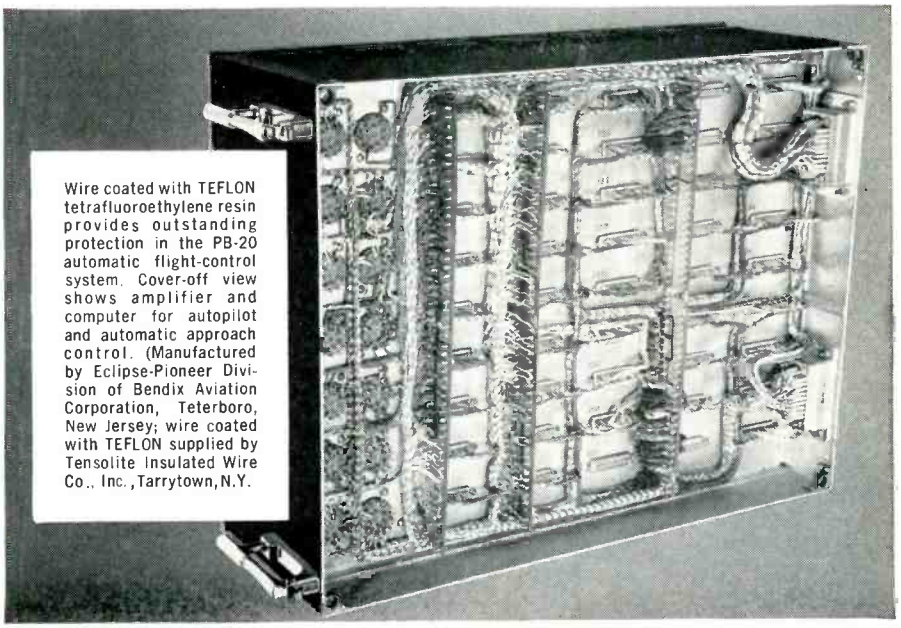
Where components are subjected to a wide range of temperature, pressure, humidity and mechanical shock and vibration, Du Pont TEFLON provides outstanding performance. In your designs, too, components of TEFLON may well be the decisive factor in meeting acceptance standards.

Wire insulated with TEFLON is used in new transistorized flight-control system

The transistorized PB-20 is the latest development in the field of automatic flight-control equipment. It has been specified for use in many advanced aircraft, such as the Boeing 707 jet transport. The PB-20 depends extensively on wire coated with TEFLON for reliable operation.

Tough and durable TEFLON can be used up to 500° F. and displays excellent properties at sub-zero temperatures. Thin-walled coatings on wire will not burn, melt or decompose when connections next to it are soldered. The dielectric strength and arc resistance of TEFLON are excellent. Its dissipation factor of less than 0.0003 from 60 cycles to 3,000 megacycles assures low losses in high-frequency communications equipment. Very few chemicals exist which can injure TEFLON . . . it is not affected by aircraft fuels, lubricants or solvents. It is inert to fungus, rot and mildew and will not absorb moisture. Articles of Du Pont TEFLON will meet the requirements of many military specifications relative to jet-aircraft applications.

You can meet the increasing demands for extreme temperature range, higher frequencies, higher voltages and greater resistance to corrosive environments by specifying TEFLON. Find out now how TEFLON can improve your products.



Wire coated with TEFLON tetrafluoroethylene resin provides outstanding protection in the PB-20 automatic flight-control system. Cover-off view shows amplifier and computer for autopilot and automatic approach control. (Manufactured by Eclipse-Pioneer Division of Bendix Aviation Corporation, Teterboro, New Jersey; wire coated with TEFLON supplied by Tensolite Insulated Wire Co., Inc., Tarrytown, N.Y.

TEFLON®
is a registered trademark...

TEFLON is the registered trademark for Du Pont tetrafluoroethylene resin, and should not be used as an adjective to describe any other product or any component part; nor may this registered trademark be used in whole, or in part, as a trade name for any product.

SEND FOR INFORMATION

For additional property and application data on Du Pont TEFLON tetrafluoroethylene resin, mail this coupon.

E. I. du Pont de Nemours & Co. (Inc.), Polychemicals Dept.
Room 182, Du Pont Building, Wilmington 98, Delaware

Please send me more information on Du Pont TEFLON tetrafluoroethylene resin. I am interested in evaluating these materials for_____

Name_____

Company_____ Position_____

Street_____

City_____ State_____

Type of Business_____

In Canada: Du Pont Company of Canada (1956) Limited, P. O. Box 660, Montreal, Quebec

ment—it can be placed across any transmission system.

▶ **Partial Specifications**—Frequency range is 50 cps to 15 kc; output voltage, one v at 600 ohms; output impedance, 600 ohms; output flatness, one db over entire range; attenuator, 0 to maximum, continuously variable.

Complete information and detailed specifications are available. **Circle P13 inside back cover.**

ACCELEROMETER
for l-f measurements

GULTON INDUSTRIES, 212 Durham Ave., Metuchen, N. J. Slowly varying environmental phenomena, from steady state to 40 cps, can now be measured by a new series of differential transformer accelerometer. The Glennite ADT-700 series feature high output with high resolution, no friction and small size.

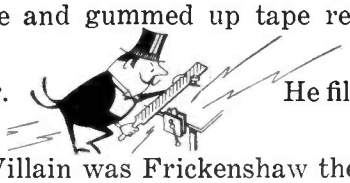
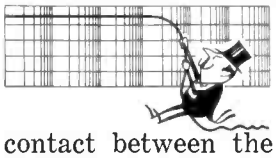
The line includes units with range of from one g to 10 g, linearity within one percent, and sensitivities from 10 mv per g per v input to 100 mv per g per v input. Other specifications include hysteresis of less than 0.25 percent, output impedance of 1,900 ohms at 400 cps and a weight of three oz. **Circle P14 inside back cover.**

COMPONENT OVEN
used on 115 v circuits

WILLIAMSON DEVELOPMENT CO., INC,. 317 Main St., West Concord, Mass., has announced a component oven that controls temperature of crystals and electronic circuitry. A standard unit is available for use on 115-v circuits, having a 35-w heater and bimetal thermostat control. The oven has inner and outer metal cans with Terne

The 7 Old-Fashioned Villains of Tape Recording

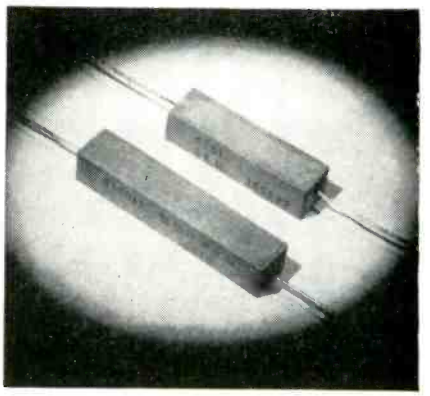
...and How irish BRAND FERRO-SHEEN Foiled Them All

Once upon a time, 7 Old-Fashioned Villains like this  were wreaking endless woe on Decent People with Tape Recorders. The 1st Villain was Oxenscheid the Oxide Shedder.  He scraped away at the crumbly oxide coating of old-fashioned tape and gummed up tape recorders with the shedding particles. The 2nd Villain was Wearhead the Head Wearer.  He filed down the magnetic heads with the abrasive coating of old-fashioned tape. The 3rd Villain was Frickenshaw the Frequency Discriminator.  He dragged down the high-frequency response of old-fashioned tape through inadequate contact between the "grainy" coating and the head. The 4th Villain was Noysenhiss the Noise Generator. He generated tape hiss and modulation noise  as a result of the random vibrations and irregular flux variations caused by the uneven magnetic coating of old-fashioned tape. The 5th and 6th Villains were Dropofsky the Drop-Out Artist and Pringlethorpe the Print-Through Bug.  They put nodules and agglomerates into the oxide emulsion of old-fashioned coated tape, causing "drop-outs" whenever these trouble spots lost contact with the record or playback head, and inducing "print-through" on the recorded tape when the extra flux at the trouble spots cut through adjacent layers on the reel. The 7th Villain was Brattleby the Embrittler. 

He dried out the plasticizers in old-fashioned coated tape and embrittled irreplaceable recordings. Then: OCTOBER, 1954! That's when a very un-old-fashioned little man by the name of F. R. O'Sheen  announced that he had developed the revolutionary new **irish FERRO-SHEEN** process of tape manufacture and presto!  the 7 Old-Fashioned Villains were sent a-scurrying with cries of "Confound it—Foiled again!" Yes, F. R. O'Sheen had made the new magnetic oxide lamination of **irish FERRO-SHEEN** tape so smooth-surfaced and non-abrasive, so firmly anchored and homogeneously bonded to the base, so free from nodules and agglomerates, that the 7 Villains were evicted—for good! **Moral:** Don't let Old-Fashioned Villains do you out of your hi-fi rights!  Just say "No, thanks" to ordinary coated tape and ask for F. R. O'Sheen **irish FERRO-SHEEN**, that is! ORRadio Industries, Inc., Opelika, Alabama.

Inquiries Invited on
irish
BRAND
FERRO-SHEEN
INSTRUMENTATION
AND
COMPUTER TAPE

plate finish to facilitate hermetic sealing. The space between the cans is insulated with glass wool and asbestos. The standard unit will control to 5 C at a setting of 75 C in an ambient of 0 to 60 C. Inside dimensions of the standard unit are 3 5/16 by 3 1/2 by 5 3/16 deep. Special sizes may be had on request. **Circle P15 inside back cover.**



POWER RESISTORS
square-body type

CLAROSTAT MFG. CO., INC., Dover, N. H., has announced square-body Greenohm Jr. miniature power resistors, series C7GL and C10GL. The wirewound resistance element is placed in a square-body steatite casing and imbedded and sealed in inorganic cement. Axial pigtail leads provide connections and also support for the resistor in point-to-point wiring. The square-body shape facilitates certain kinds of assembly and wiring operations. They are available in seven-w and 10-w ratings, 1 3/8 in. and 1 7/8 in. long, respectively and of the same 3/8 by 11/32 in. cross-section. Resistance values are from one ohm to 6,000 ohms, and one ohm to 11,000 ohms, respectively. **Circle P16 inside back cover.**

RIGHT ANGLE SOCKET
mounts tubes horizontally

AEROVOX CORP., 2724 South Peck Road, Monrovia, Calif. A new alkyd-base tube socket that mounts tubes horizontally to reduce space requirements has been especially designed for use with printed circuits.

The sockets mount at right angles to the plane of the wiring

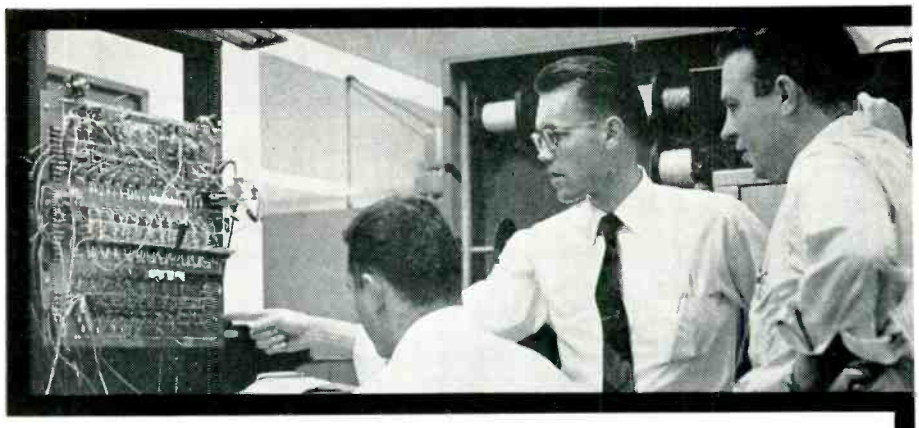
You owe it to yourself *and your family*

to compare these multiple advantages offered only by Consolidated . . .

Find out now how CEC's engineers enjoy a combination of advantages unique in electronics, and made possible by executives with both scientific and professional management backgrounds. CEC's policy of recognition for the individual has built a pioneering, multi-million dollar organization—the recognized leader in the application of electronics to chemical analysis, process monitoring, dynamic and static testing, and automatic data processing...

YOUR CREATIVE IMAGINATION PAYS OFF AT CEC

In development engineering laboratory, George M. Slocomb (center), 31, supervisor of digital data processing section, explains new test procedure in transistor circuitry for digital data handling. Viewing breadboard demonstration are engineers Bob Kelly (left) and Wayne Hodder. *CEC's substantial R&D budget is 2-3 times greater than normal budgets—totals 10-15% of sales.*



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HOW TO ENJOY YOUR WORK and make your family happy . . . CEC's progressive administration emphasizes *excellent working conditions in modern buildings. Your family will enjoy the beauty of CEC's non-industrial location!*

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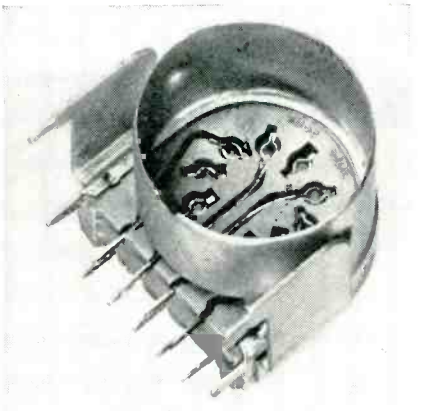
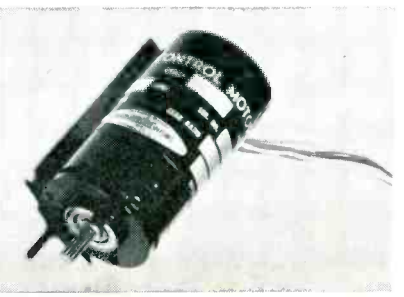


board. This places the longitudinal axis of the tube parallel to the plane of the board. Beside saving space, the lower position of the tube mass reduces strain on the socket caused by acceleration in the plane of the mounting surface. The new sockets are suited for hand or mechanized insertion into printed wiring boards utilizing in-line, punched round holes. The leads are simply dropped in and soldered.

Plaskon alkyd was selected for the body of the socket because of its superior properties of arc resistance, great dielectric strength, dimensional stability and high resistance to heat and moisture. **Circle P17 inside back cover.**

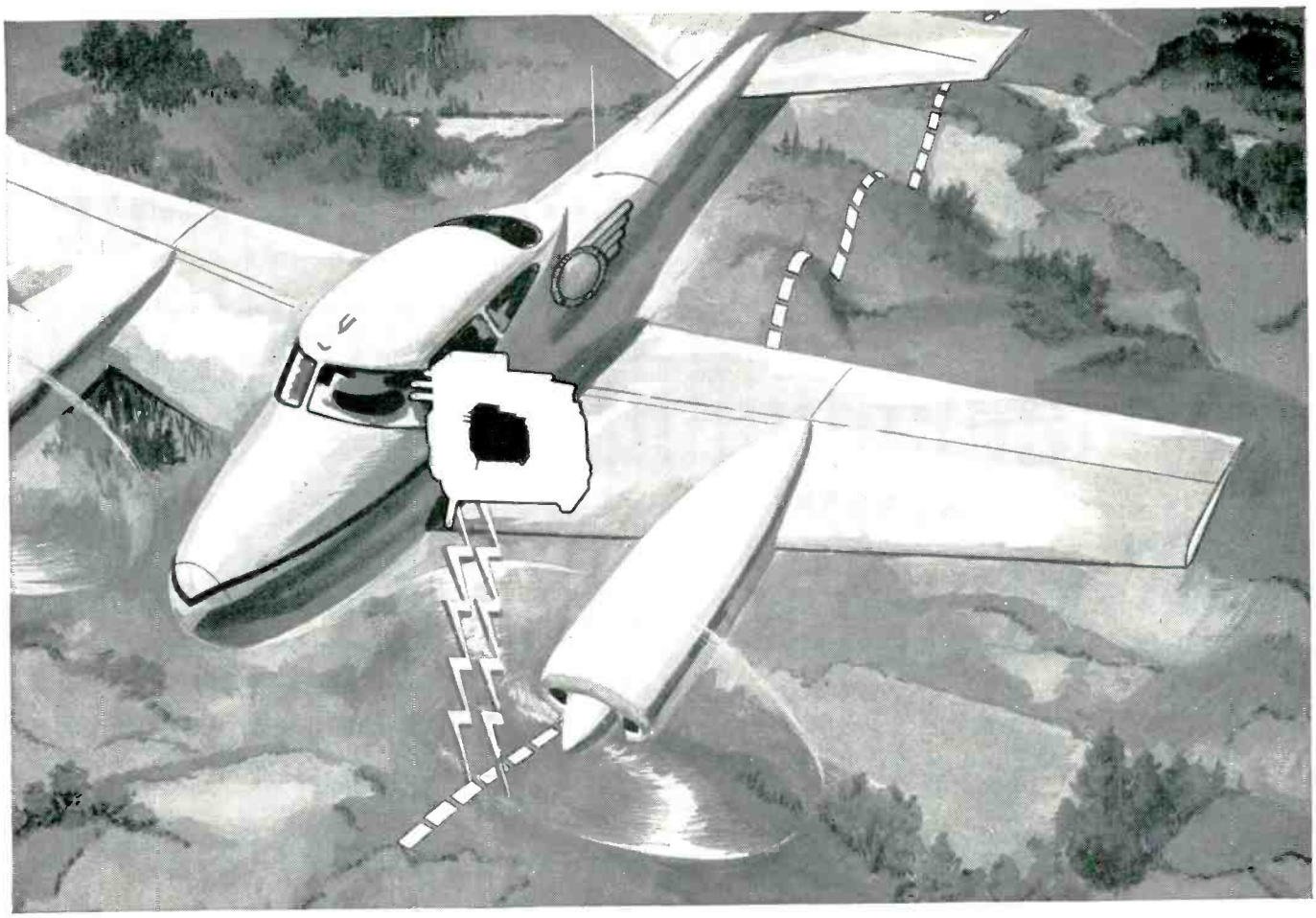


SERVO UNIT
motor-gearhead-clutch

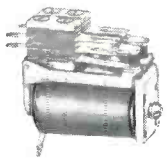
SERVOMECHANISMS, INC., 625 Main St., Westbury, N. Y., has available a miniature motor-gearhead-clutch Bu Ord size 10, (0.938 in. in diameter), with a maximum length of 1¾ in., and designed to operate directly from either a 115 or a 26-v line.

This 400-cycle servo unit has motor and gearhead enclosed in a common aluminum housing. The housing design minimizes alignment and assembly problems while the use of aluminum makes pos-

Potter & Brumfield *engineering is in this picture*



Which P&B relay did Television Associates specify
FOR THEIR AIRBORNE COMPUTER?



MH Series

MB Series

MC Series

Surveys for pipe lines, electric transmission routes and microwave paths are now made from the air, by radar. Television Associates of Indiana, Inc. developed this speedy new technique—and the equipment—which provides clients with detailed profiles of the terrain to be crossed.

Part of the equipment, an intricate airborne computer, requires relays that are fast-acting, light weight, versatile. They must have high shock and vibration resistance and remain operative in temperatures ranging from —45° C to +85° C.

Modified MH relays by P&B were specified. These miniature relays meet all Television Associates' requirements and provide high reliability in a mighty small package. Challenging relay problems are solved daily at P&B. Twenty-five years of creative engineering are behind every P&B relay. Write today for our new catalog.

ENGINEERING DATA

SERIES: MH Miniature Telephone.

CONTACTS: Up to 18 springs, maximum 9 in each stack, forms A, B, C, D, E, X and Y. AC relays are limited to a maximum of 2 poles. Various contact material available.

VOLTAGE RANGE: DC-.05 to 110 V.—AC-6 to 230 V. 60 cycle.

COIL RESISTANCE: 22,000 ohms maximum.

TEMPERATURE RANGE: High temperature range (DC) —55° C. to +135° C.
Standard DC —55° C. to +85° C.
Standard AC —45° C. to +40° C.
Other temperature ranges available to specification.

TERMINALS: Standard pierced solder lug holes will take (2) No. 18 hook-up wires. Adaptable for printed circuits.

ENCLOSURES: Dust cover plus wide range of hermetically sealed covers and types of terminations.

DIMENSIONS: 1-9/16" L. x 25/32" W. x 1⅜" H. (4c Relay).

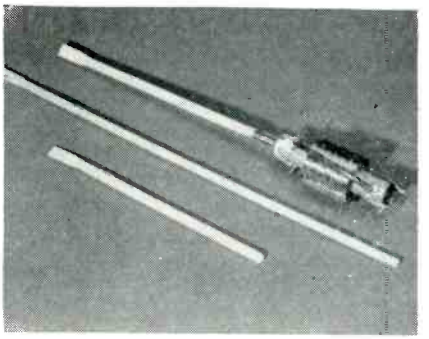
P&B RELAYS AVAILABLE AT MORE THAN 500 DISTRIBUTORS IN ALL PRINCIPAL CITIES

Potter & Brumfield, inc. PRINCETON, INDIANA

Subsidiary of AMERICAN MACHINE & FOUNDRY COMPANY • Manufacturing Divisions also in Franklin, Ky. and Laconia, N. H.

sible a minimum weight and temperature rise.

Gearing and loads are protected by an integral slip clutch. The use of this clutch as a control element is especially important when confronted with the high stall torques resulting from the use of high gear ratios. **Circle P18 inside back cover.**



EXTENSION SHAFTS
with flattened ends

ANCHOR PLASTICS CO., INC., 36-36 36th St., Long Island City 6, N. Y., has developed highly rigid, heat-resistant nylon extension shafts. They can be used in applications where greater torque is encountered.

The company has also developed automatic machinery to produce these shafts with flattened ends which eliminates the necessity for knobs. Illustrated is a coil using one of the shafts. **Circle P19 inside back cover.**

V-R POWER SUPPLY
with low ripple

KEPCO LABORATORIES, INC., 131-38 Sanford Ave., Flushing 55, N. Y. The new model 2500 voltage-regulated power supply features a 0-2,500 v, 0-50 ma continuous duty d-c output. In the range 0-2,500 v,

meet FRANK ROBERTS ...he's paid to solve your problems

Frank is chief engineer, components division, at National Company. He heads the proficient engineering group whose job is to modify present catalog items, develop new components to meet your specifications, and to help solve your components problems. While our catalog lists over 300 different parts, over 60 per cent of orders received are for "other than catalog items;" therefore, National is geared to provide many types of **special** services.

The capabilities and facilities of National's components engineering division are as excellent as they are varied. Some of our facilities are illustrated. Our capabilities include the design and development of:

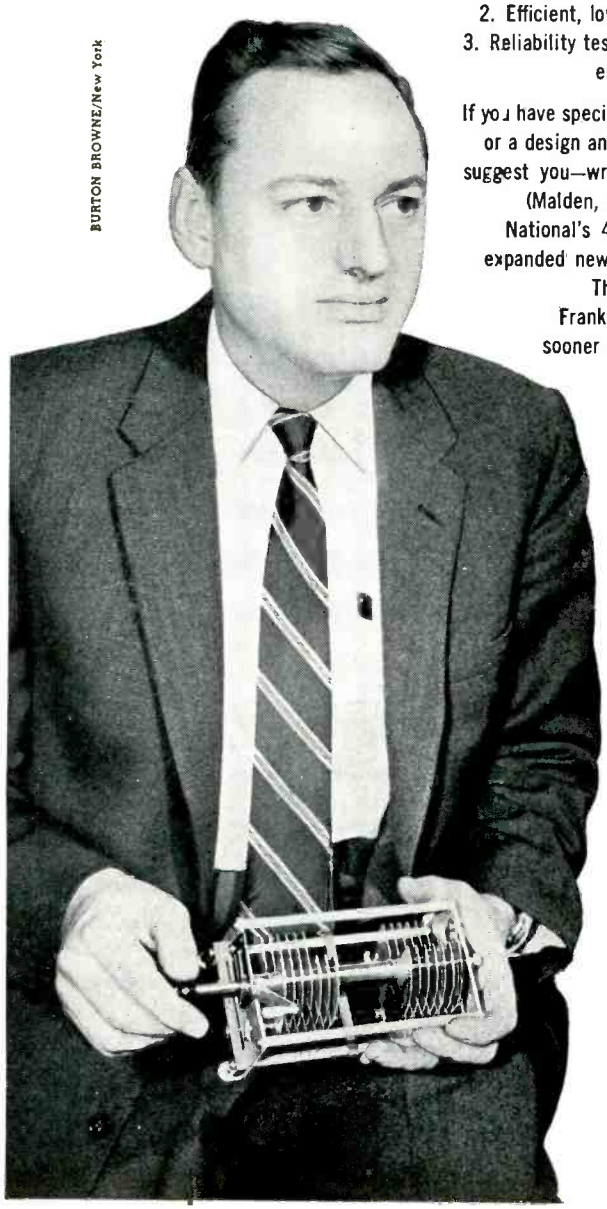
1. Commercial and precision type variable capacitors.
2. Communications type filters and networks.
3. Chokes and special coils.
4. Knobs and precision vernier dial mechanisms.
5. The design and fabrication of special hardware for the electronic industry including coil forms, shaft locks, dial locks, insulated bushings and captive nuts.

In addition our components division offers:

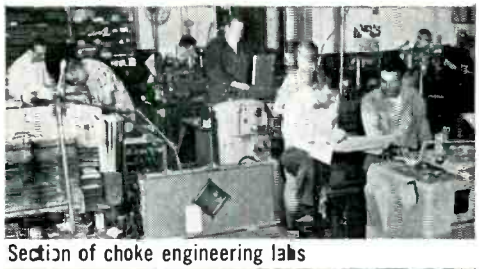
1. Complete model shop facilities.
2. Efficient, low cost production facilities.
3. Reliability test programs. U.S.A. approved environmental test facilities.

If you have special components requirements or a design and development problem—we suggest you—write, wire or call NATIONAL (Malden, Mass. 2-7950) at once. Put National's 42 years of experience and expanded new facilities to work for you. The sooner you have men like Frank Roberts working for you the sooner your components problems will be solved.

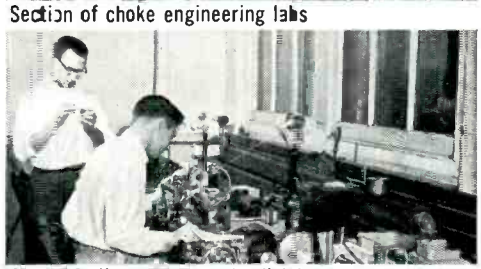
BURTON BROWNE/New York



Model shop facilities



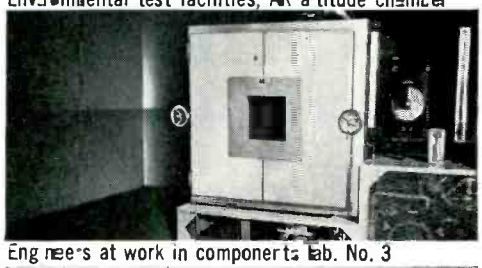
Section of choke engineering labs



Assembly line, components division

Mechanical engineering section, components division

Environmental test facilities, AR a titude chamber



Engineers at work in components lab. No. 3

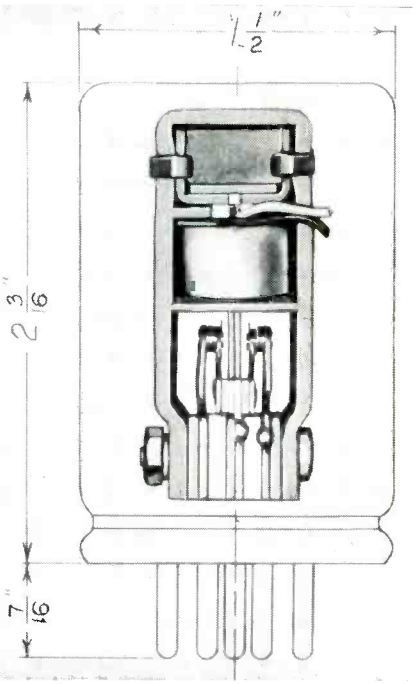
MEET THE MEN FROM NATIONAL AT THE I.R.E. SHOW— Booths 1401-1407

Eight out of every ten U.S. Navy ships use National Receivers

National NC® tuned to tomorrow MALDEN 48 MASS.

the output voltage variation is less than 0.1 v for load variations from 0 to maximum current and less than 0.2 v for line fluctuation from 105 to 125 v. Ripple is less than three mv rms. Recovery time is less than 50 μsec. Stability for a period of eight hours is within 0.2 v. Output impedance is less than 0.1 ohm from 20 cps to 100 kc and less than 0.5 ohm from d-c to 20 cycles.

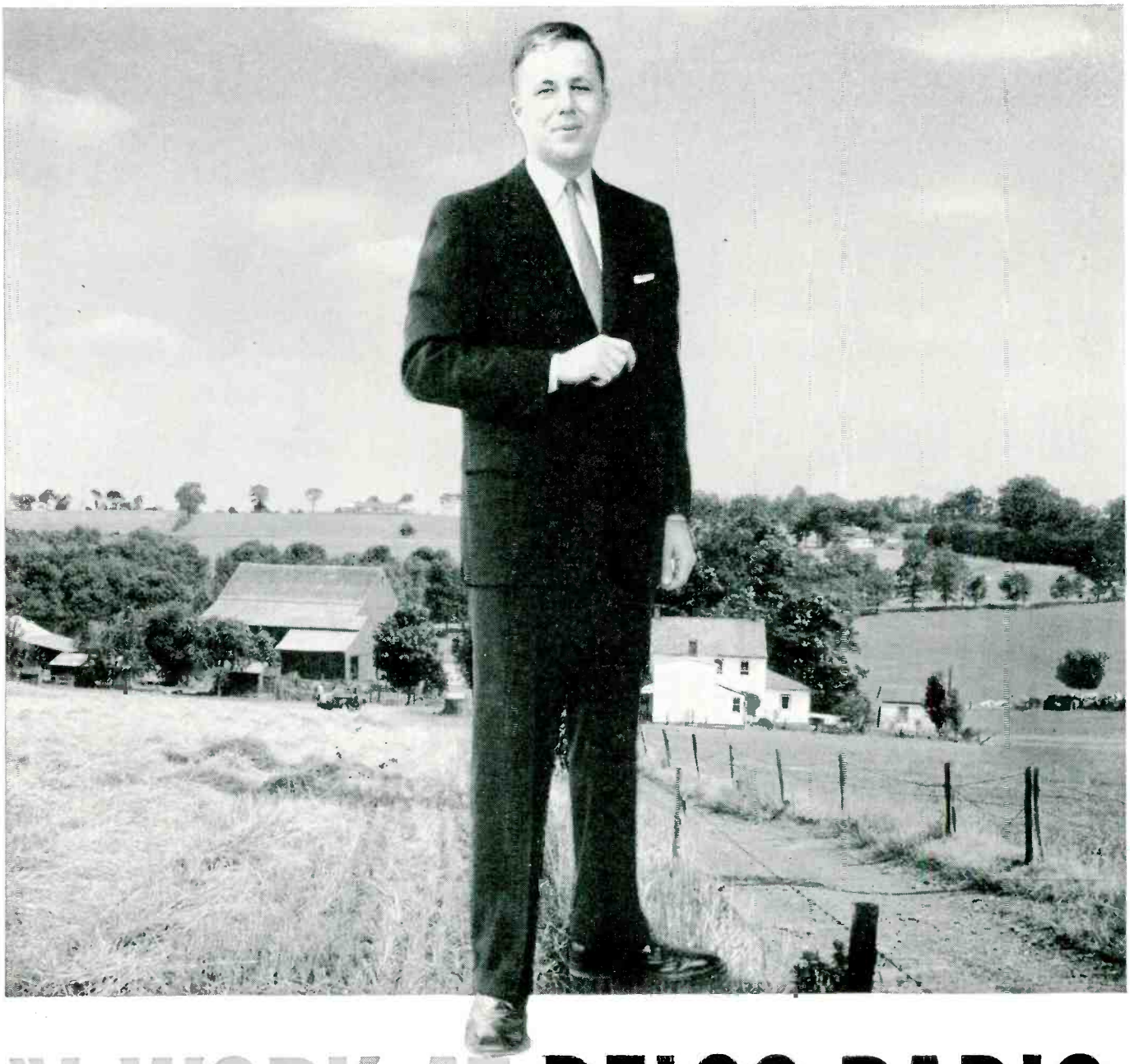
Height of the unit is 12¼ in.; width, 19 in.; depth, 17 in.; weight, 65 lb. This supply is available with or without meters. **Circle P20 inside back cover.**



INSTRUMENT CHOPPER
has 6.3 v, 60 cps driving coil

JAMES VIBRAPOWR CO., 4050 N. Rockwell, Chicago 18, Ill. Model C-1800 commercial type instrument chopper is designed for systems with moderate low level signal requirements. It is a spdt chopper with a 6.3-v, 60-cps driving coil. The base is a standard octal type with neoprene seal. Through use of a unique mounting assembly, costly silicone cushioning has been eliminated.

Coil current is 175 ma maximum; phase lag, 26 ±7 deg; contact on time, 150 ±15 deg; contact symmetry, 15 deg; contact bounce, 4 deg maximum in initial 10 deg on time; contact rating, 50 v at 1 ma; life,



"I WORK AT DELCO RADIO.

The laboratory is 10 minutes or less from this homey spot in central Indiana. I earn a big-city salary and enjoy many opportunities to see my ideas used in the finished products of General Motors."

Delco Radio, first organization to develop and use high-power germanium transistors for automotive applications, offers challenging positions to men qualified to pioneer new ideas in the field of semiconductors and electronics. Good pay, permanent General Motors employee benefits, modern work facilities are only a few of the advantages you'll enjoy at Delco Radio. Opportunities for recognition and achievement are not limited. Why don't you write and tell us about your background and ambitions, including information on your education, experience and accomplishments. Please address your letter to: Personnel Director—L, Delco Radio, Division of General Motors, Kokomo, Indiana.

QUALIFIED SCIENTISTS AND ENGINEERS **with baccalaureate and advanced degrees —also those with electrical, chemical, mechanical, metallurgical, physical, or physical chemistry experience—are urgently needed at Delco Radio for permanent positions in research, development and design of semiconductor devices, and their applications and production.**

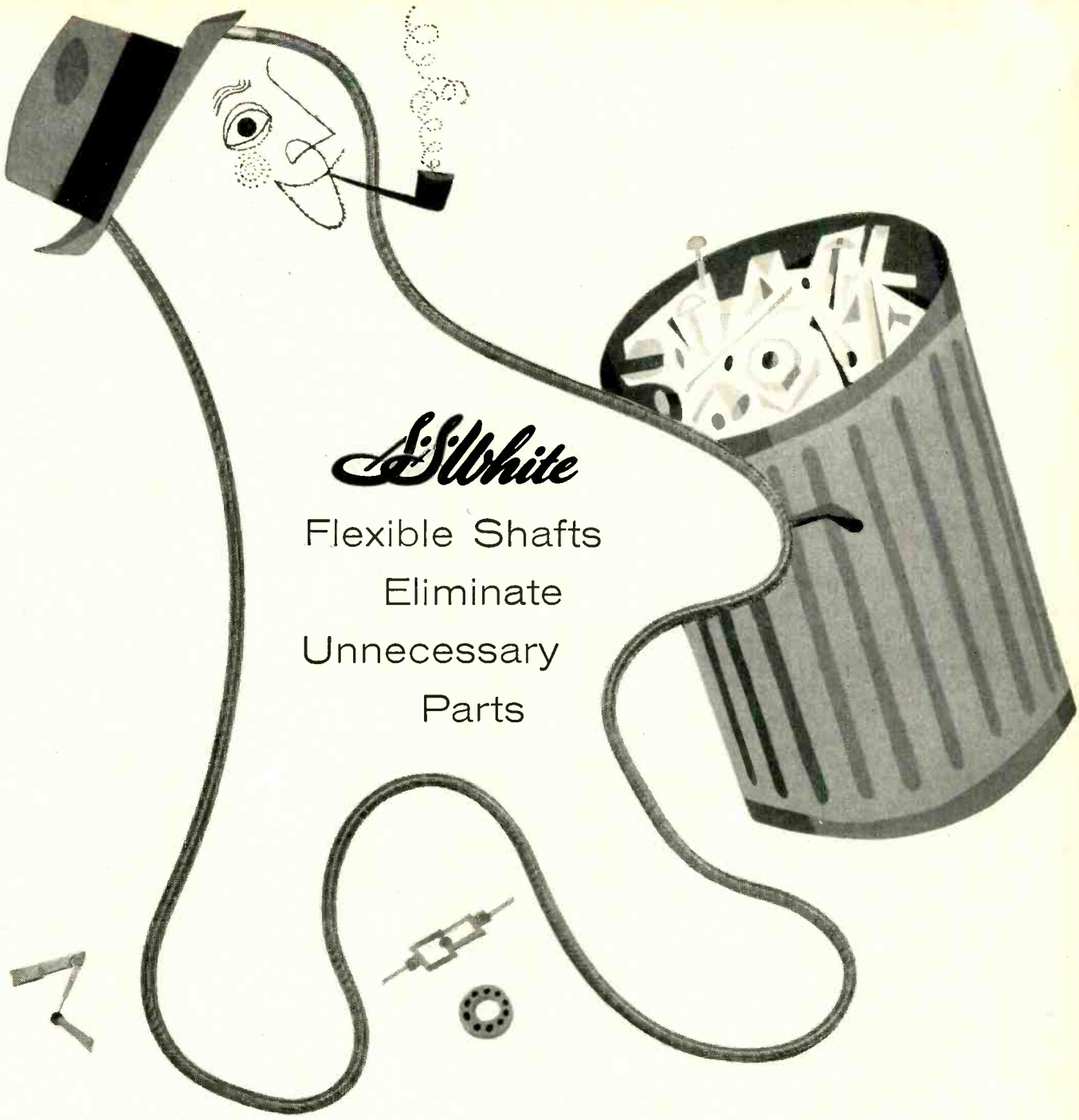
1,000 hours nominal; residual noise, 1 mv as measured into one-megohm impedance — proportionally lower with reduced input impedance. **Circle P21 inside back cover.**

CAPACITORS
designed for ultrasonics

FILM CAPACITORS, INC., 3400 Park Ave., New York 56, N. Y. The new type U line of capacitors utilize a special high-breakdown plastic film dielectric and have high insulation resistance. Capacitance stability is of the order of 0.5 percent. As a result, optimum Q and stability can be maintained in the ultrasonic circuits themselves. A typical capacitor rated at 0.07 μf is 2½ in. in diameter by 1½ in. long and can carry 500 circulating volt-amperes. Detailed literature is available on request. **Circle P22 inside back cover.**

FUEL GAGE TESTER
for aircraft applications

TELECTRO INDUSTRIES CORP., 35-18 37th St., Long Island City 1, N. Y.,

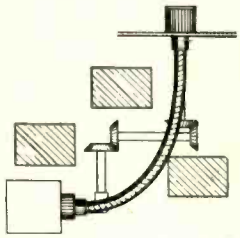


S.S.White Flexible Shafts Eliminate Unnecessary Parts

One manufacturer used flexible shafts to replace 35 parts in a Hydraulic Power System . . . cut costs by 90%. Four flexible shafts replaced a 35-part remote-control system . . . simplified design . . . made assembly easier . . . eliminated alignment problems . . . improved performance!

This is only one of hundreds of remote control and power drive problems these quality flexible shafts are solving in every industry today. Can S.S. White flexible shafts help improve *your* product? Perhaps make it lighter in weight . . . cut production costs . . . eliminate unnecessary parts?

If you'd like to know more about flexible shafts, the advice of our engineers costs you nothing. Just write to



S. S. White Industrial Division, Dept. E, 10 East 40th Street, New York 16, N. Y.
Western Office: 1839 West Pico Blvd., Los Angeles 6, Calif.

S.S.White

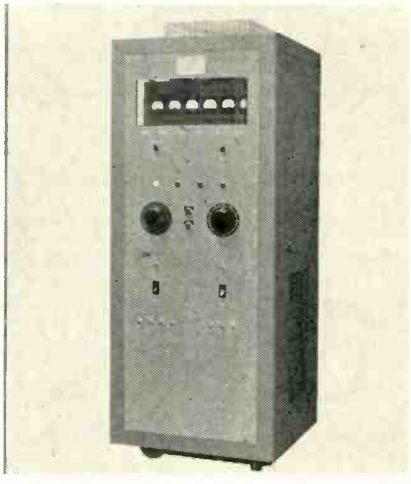
FIRST NAME IN FLEXIBLE SHAFTS

Useful data on how to select and apply flexible shafts! Write for Bulletin 5601.

announces availability of the type MD-1 aircraft fuel gage tester designed specifically to test and calibrate aircraft capacitance type fuel gages. It qualifies under AF Spec MIL-T-8579 and meets all its requirements.

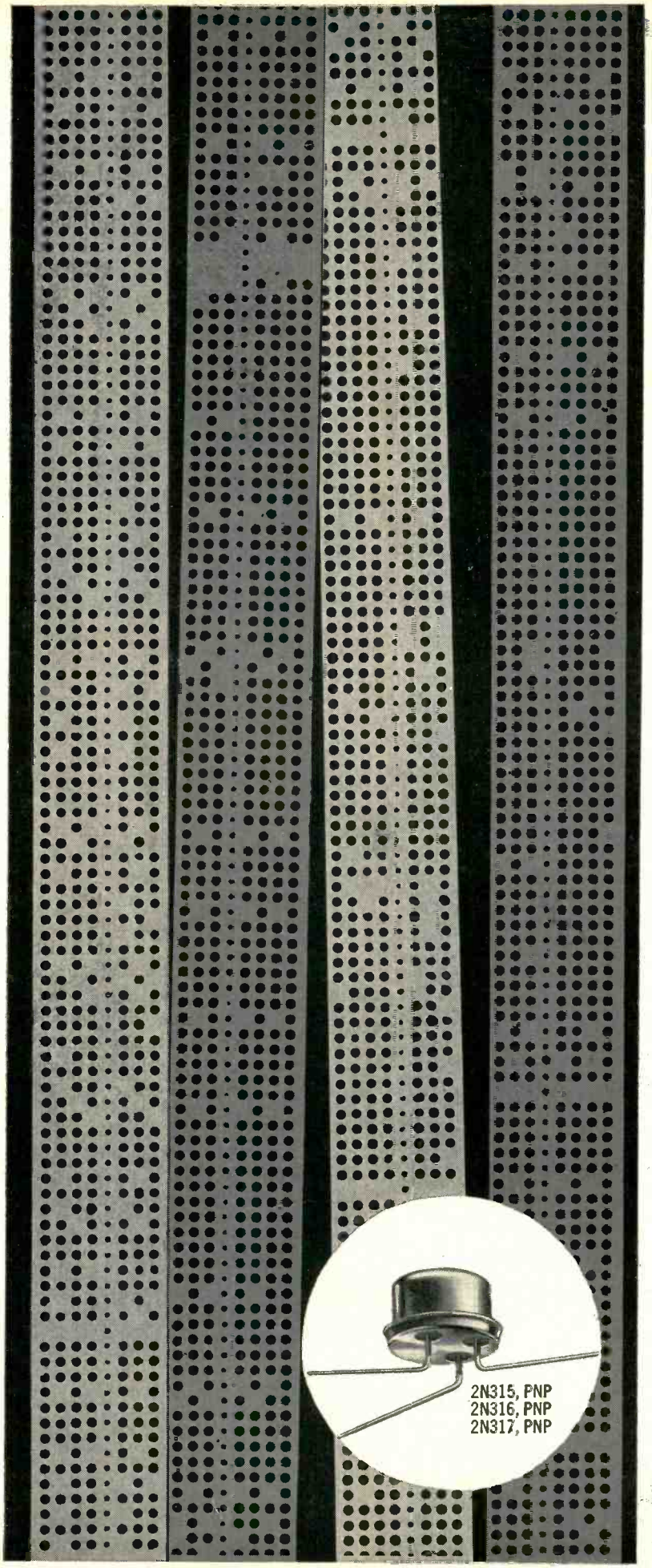
The MD-1 is a direct reading variable capacitor with a range of 10 to 6,200 $\mu\mu$f. Accuracy is 0.1 percent and through the use of a mina dial and a vernier dial, capacitance values in increments of 0.1 $\mu\mu$f are readily obtained. The dial is designed with a special positive locking device and a mechanical arrangement that eliminates backlash.

No external power source is required. The tester is lightweight, portable, rugged and sealed against moisture, and is supplied with nine accessory cables for connecting to all types of aircraft capacitance fuel gages. **Circle P23 inside back cover.**



POWER SUPPLY
filament-focus unit

LEVINTHAL ELECTRONIC PRODUCTS, INC., 760 Stanford Industrial Park, Palo Alto, Calif. Developed for klystrons with bombarded cathodes, model PC51 power supply provides 0 to 3 kv d-c at 0.9 ampere with less than 0.5-percent ripple, 0 to 20 v a-c at 60 amperes and 0 to 750 v d-c at 20 ma. All three supplies are insulated at 30 kv d-c above ground for operation with a separate beam power supply. Meters are available for measuring bombarder voltage and current, filament voltage and cur-



General NEW HI-SPEED SWITCHING TRANSISTORS Assures Computer Reliability

Computer engineers long seeking PNP transistors in applications requiring high current and fast switching will specify General Transistor's new 2N315, 2N316, and 2N317 for peak reliability.

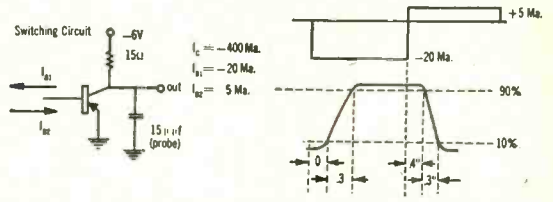
2N317: As developed by General, a typical switching speed of .3 of a microsecond at 400 milliamps of collector current is possible with only 20 ma. of drive current.

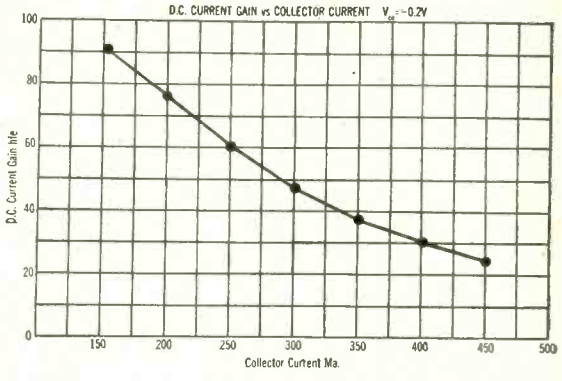
The series resistance of these GT transistors, when conducting, is ½ ohm; the nonconducting series resistance is as high as 10 megohms with a result that approaches optimum efficiency at high current levels.

Computer manufacturers know they can depend on General's engineering and development as well as their quality and service. That's why GT is the largest supplier of transistors for computers.

CHARACTERISTICS

Parameter	Conditions	Min	Typical	Max
Collector-Base Voltage (Vcbo) Emitter Open	Ic = –25μa	–20V	–30V	
Collector Cut-off Current (Icbo)	Vcb = –5V		–1μa	–2μa
D.C. Current Gain (hfe)	Ic = –400ma Vce = –.2V	20	30	50
Alpha Cut-off Frequency (fafb)	Vcb = –5V Ic = –1ma		20mc	



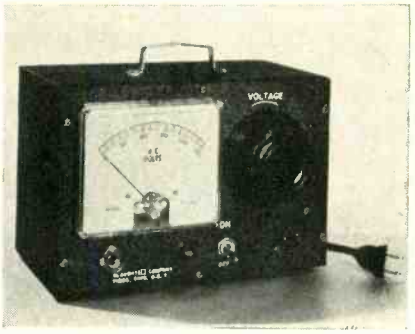


Write for GT's special Computer Transistors Specifications Bulletin.

GENERAL TRANSISTOR CORP.
Richmond Hill 18, N. Y.—VIrginia 9-8900
Cable: Transistor New York

rent, and focus-electrode voltage and current.

The unit is completely protected by interlocks and has appropriate time-delay and sequential operation built in, to prevent operation of any supply before the filament is on and hot and the bombarder supply is on and up. **Circle P24 inside back cover.**



A-C POWER SUPPLY
for general utility service

SLAUGHTER CO., Piqua, Ohio. Model 109 a-c power supply features a fuse protected variable autotransformer, a neon pilot light and a highly legible 4½-in. voltmeter with an essentially linear scale. Nominal input is 115 v, 60 cps and output rating is 3 amperes, with voltage infinitely variable from 0 to 135 v.

With this unit it is practical to conduct all operating tests under controlled input voltage conditions, regardless of line voltage, as well as to simulate the effect of abnormally high and low voltages. **Circle P25 inside back cover.**

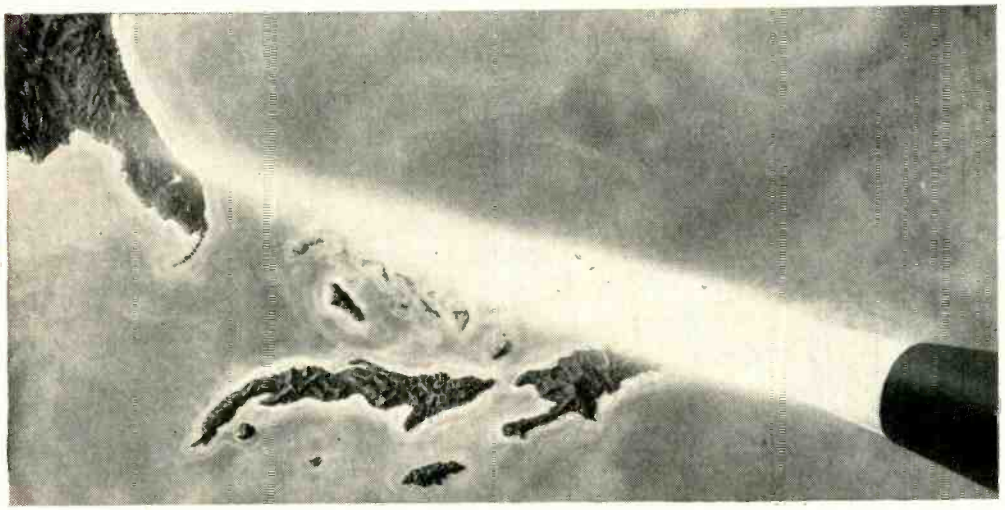
KLYSTRON MODULATOR
one-megawatt equipment

LEVINTHAL ELECTRONIC PRODUCTS, INC., 2760 Fair Oaks Ave., Redwood City, Calif., has available model PC43 modulator designed for high-power tube-development applica-

Wanted!

Engineers to sign on for one of the most exciting scientific expeditions of our time:

The SM-64 Navaho Missile



The men behind this invitation are pioneers in missile development. Ten years ago they started from scratch. There were no texts to consult, no rules to follow. Today their technological achievements are so great ... their jobs so broad ... there is room at every level of engineering for additional mindpower.

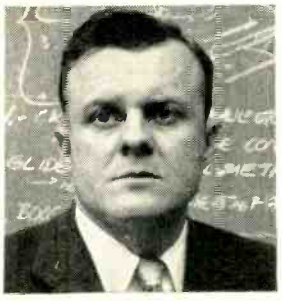
Accept this challenge and you can travel faster and farther than you ever thought possible on one of the most important programs in the free world today—North American's complete weapons system responsibility for the Air Force SM-64 Navaho Intercontinental Strategic Guided Missile.

DOUGLAS K. BAILEY received his BS degree from the University of California. He joined North American ten years ago as a senior design engineer. Today he is chief, Missile Design Section—responsible for missile design engineering and analysis. Doug and his family live in Long Beach where he participates in golf, bowling and sports car activities. He is currently organizing road races in Southern California for the Long Beach MG Club.

Unprecedented programs have been completed and more are to come. Others are being developed, modified and perfected as we enter another exciting phase following a successful flight test program at Patrick Air Force Base using a test vehicle known as the X-10.

The fascinating nature of this work has already attracted the world's best informed missile men. Top-tier men have opportunities in almost every field of engineering—including some of the most advanced work being done today in aerodynamics, thermodynamics, high temperature materials and aero-elasticity.

Solving these problems is bringing forth new formulae and new production techniques. One example is Chem Mill, the process of shaping metals—including titanium and newest alloys—to previously unattainable designs by chemical etching. This method reduces weight ... increases strength. The idea came from a North American Missile engineer.



Navy vet **GEORGE W. JEFFS** earned both his BSAE and MSAE from the University of Washington. About 9 years ago he started his professional career with North American as a junior aerodynamics engineer. Now, 5 promotions later, this 30-year old veteran of missile work is chief, Advanced Design Section. He lives in Downey, California with his wife and 3 children. His hobbies include fresh-water fishing and hunting for quail and pheasant.

This is the kind of opportunity open to you. You can share our knowledge and add to it.

Recent graduate engineers can step into established groups. Experienced men will find even greater opportunities in the new groups that are being formed. And you'll do this in a management climate that stimulates personal growth and rewards it with responsibility, professional recognition and material benefits. Further, you can continue your studies with the aid of North American's Educational Refund Plan ... live and work in Southern California ... in near-ideal climate.

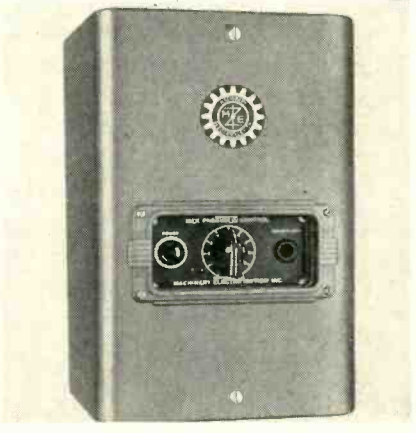
Let us know what kind of creative engineering interests you. (Please include highlights of your education and experience.)

Write today to: Mr. R. L. Cunningham, Engineering Personnel Manager, Dept. 91-2-EL
Missile Development Division, 12214 Lakewood Blvd., Downey, California.

NORTH AMERICAN AVIATION, INC.

tions. Equipment consists of a 40-kw X-band magnetron driver; a 15-kv power supply rated at 1.6 ampere with less than 0.1- percent ripple; a complete control console for remotely operating the klystron and all associated equipment; a line-type modulator operating with a pulse length of 0.5 μsec at repetition rates from 10 to 4,000 cps; and a pulse transformer tank including a 140-kv 60-ampere pulse transformer and a capacitance voltage divider, as well as peak-current and average-current monitoring circuits.

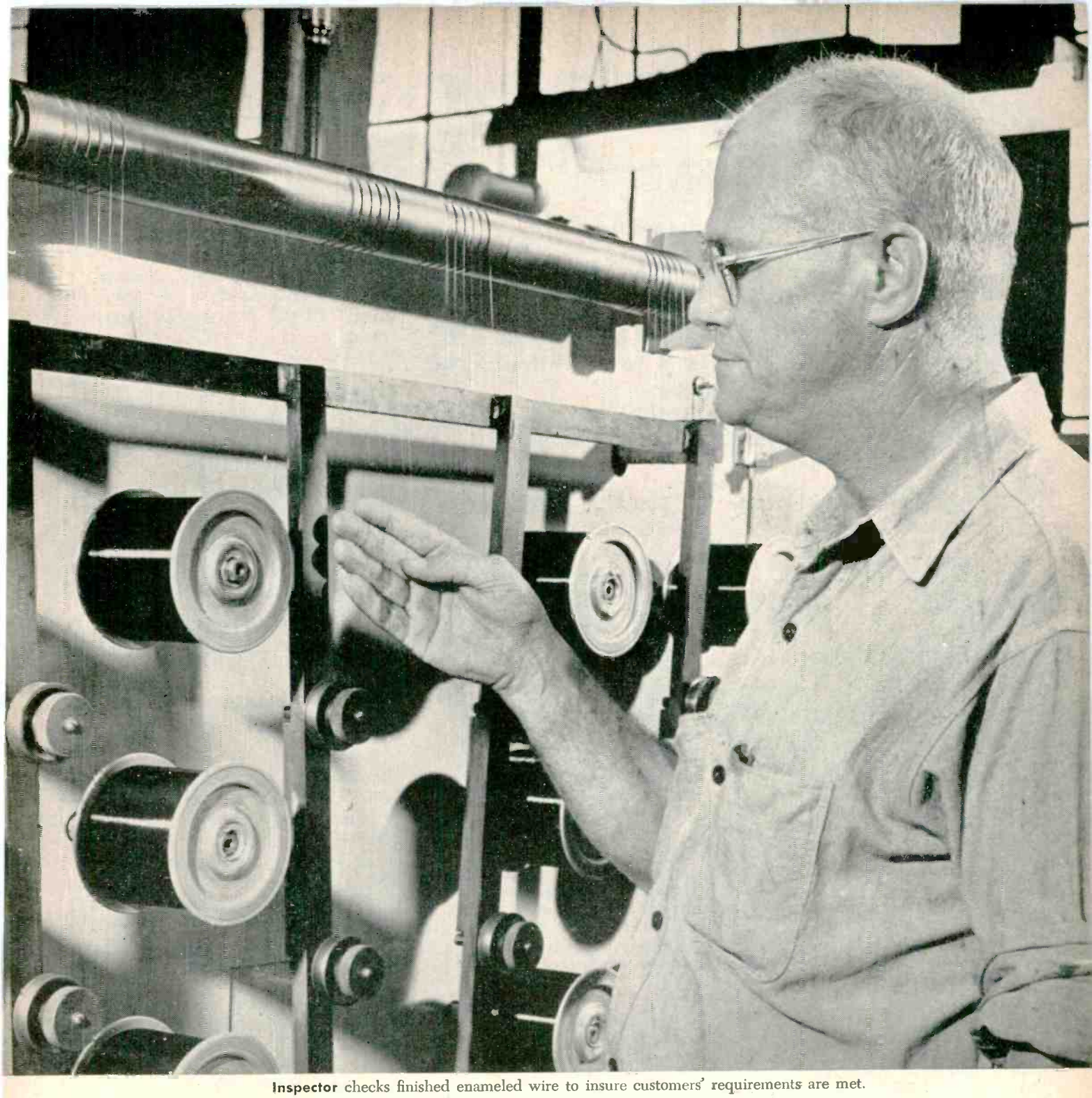
The modulator uses five 1754 hydrogen thyratrons to handle the average power. These tubes are sequentially switched by a unique ring system that keeps the pulse-to-pulse jitter below 0.05 μsec. An inverse-current circuit with adjustable overload protection as well as a linear charging choke, hold-off diodes and a pfn are included in the unit. **Circle P26 inside back cover.**



PROXIMITY CONTROL
may be used in many ways

MACHINERY ELECTRIFICATION, INC., Northboro, Mass., has announced the development of the MEK-3030 electronic proximity control. It detects the presence of an insulator or conductor at the detecting point without making contact with the surface.

The MEK-3030 can be used as a limit switch which does not require physical contact with the controlling surface; as a level control of such materials as soap, coal or oil; and as an interface control between two dissimilar fluids. It



Inspector checks finished enameled wire to insure customers' requirements are met.

THIS MAN CAN HELP YOU

Eliminate cost of incoming magnet wire inspection!

This inspector acts as customers' agent in the Anaconda magnet wire mill.

Result: Anaconda Magnet Wire complies with such exactness to specifications that many customers have felt it possible to *eliminate incoming inspection* . . . at considerable savings in money, time and manpower.

More than this, customers say Anaconda quality control pays off in smoother winding room performance . . . and helps them produce a consistently high quality product at lowest cost.

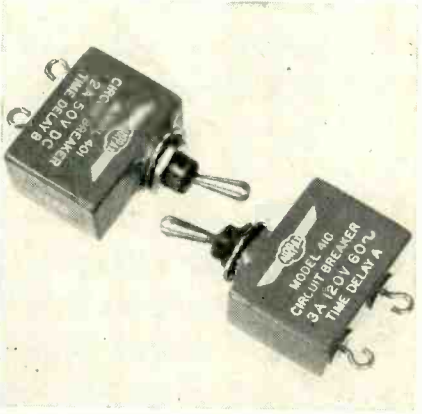
Talk to the Man from Anaconda about a trial run of Anaconda wire to prove it to yourself. Call or write: Anaconda Wire & Cable Company, 25 Broadway, New York 4, New York. 56322

ASK THE MAN FROM ANACONDA® FOR MAGNET WIRE

features voltage regulation, plug-in relay and visible contacts.

▶**Specifications**—Input voltage is 115, 60 cps; line consumption, 25 va; relay capacity, five amperes, 115 v; contact available, spdt.

The unit works on a principle of h-f energy. Complete information is available from the company. **Circle P27 inside back cover.**



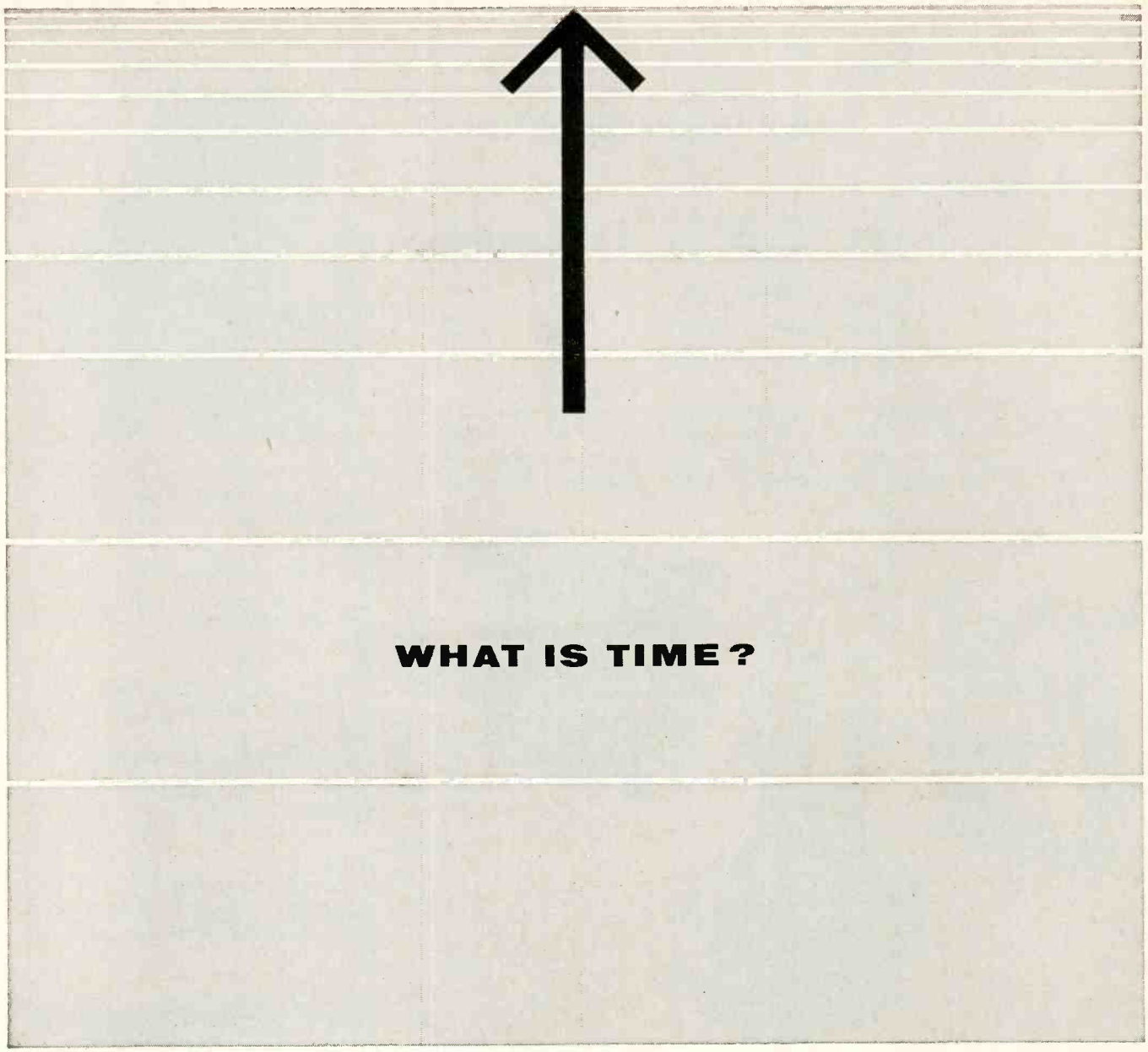
CIRCUIT BREAKER
has improved design

AIRPAX PRODUCTS CO., Middle River, Baltimore 20, Md., announces several significant improvements in its miniature magnetic circuit breaker. This breaker is specially built for use in protecting electronic equipment.

On earlier units it was 0.06 in. total excursion from 10 to 55 cps. Newer production units also withstand 10 g at 55 to 1,000 cps. The trip level has also been raised to 135 percent of rated load current. Units are available for interrupting 50 volts d-c at currents from 0.05 to 10 amperes and for interrupting 120 volts rms, 60 or 400 cps, at currents from one to 10 amperes. The toggle bushing of this breaker is the same as on conventional ON-OFF switches. **Circle P28 inside back cover.**

TRANSIFIER
video transistor amplifier

KAY ELECTRIC CO., 14 Maple Ave., Pine Brook, N. J. Model 126A Transifier, a completely transistorized broadband video amplifier, is a true modular plug-in unit



WHAT IS TIME?

Anything that can be postulated is possible, says science—including *timelessness*.

The latest table-talk among the rocket and missile men has to do with the physics (and metaphysics) of photon propulsion: thrust for a space vehicle derived by shooting incredibly concentrated beams of light (photons) from its tail. Result—speeds approaching that of light! Round trips to distant galaxies could thus be accomplished in a single generation of the crew. Meanwhile, however, the Earth would have passed through a billion years—possibly into cosmic oblivion!

The space-time ratio is increasingly a factor in the calculations of a brand new field of science known as astronautics...Work in this field at Martin is already at the threshold of tomorrow.

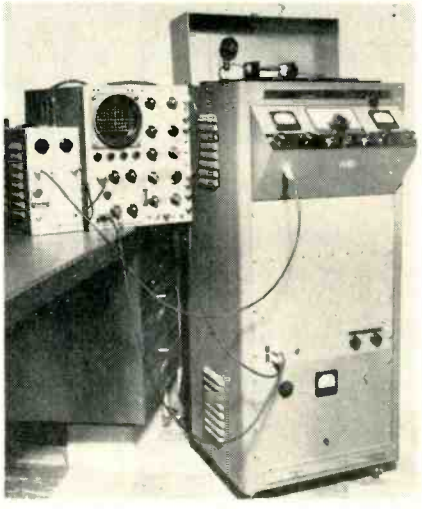
MARTIN

BALTIMORE · DENVER · ORLANDO

with feedback circuit built in for stabilized signal gain. All the advantages provided by transistors —small size, lightness, portability, long-life, rugged operation, low power consumption and high conversion efficiency—are offered by this tubeless instrument.

► Uses—Among the uses served are the following: as a preamplifier for oscilloscopes and vtvm's; as a humless audio amplifier; as a wide-band video amplifier; and as a modular in control circuitry and all types of audio-video electronic devices.

Complete technical specifications are available from the company. **Circle P29 inside back cover.**



TEST SET
shows semiconductor lifetime

MARVELCO ELECTRONICS division of National Aircraft Corp., 3411 Tulare Ave., Burbank, Calif. Now available to electronic laboratories is a new test set for deter-

ASCOP

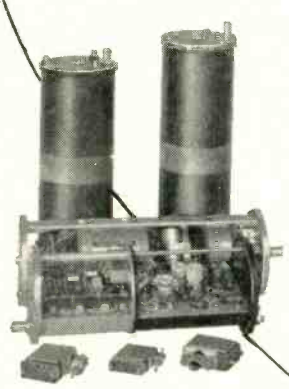
PW DATA SYSTEMS

MULTICHANNEL DATA TRANSMISSION OR RECORDING, USING RF CARRIER, FM SUBCARRIER, OR SINGLE MAGNETIC TAPE TRACK

Pulse width coding and time division multiplexing techniques result in systems of large numbers of data channels, excellent accuracy, and exceptional simplicity of operation.

TYPICAL SYSTEM PERFORMANCE

NUMBER OF DATA CHANNELS	26	41	86
SAMPLES/CHANNEL/SECOND	30	20	10
FREQUENCY RESPONSE, CPS	5	3.3	1.6
Linearity	Better than 0.5% of full scale		
Stability	Long term drift less than 1% of full scale		

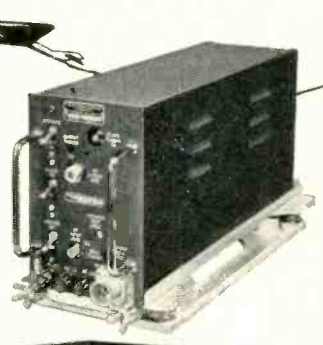


← F SERIES MISSILE TELEMETERING SETS

For short life applications, where the ultimate in compactness, ruggedness, and performance are required. Standard packages as shown are available for 30x30 and 45x20 operation. Special configurations, using standard functional components may be ordered. Some components are sold separately.

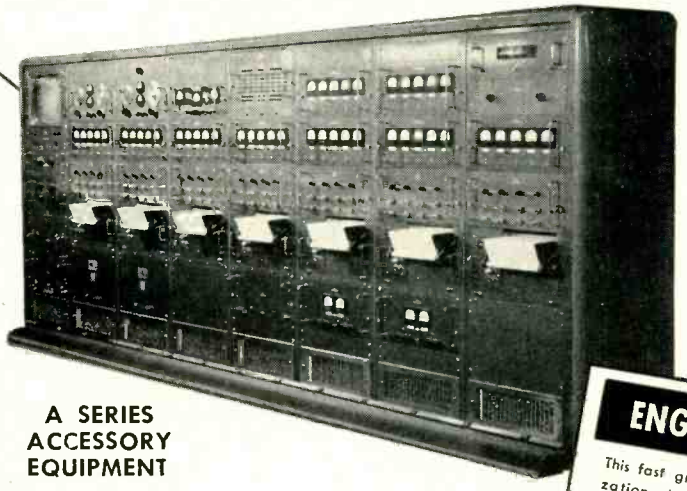
D SERIES MULTICODERS AND TELEMETERING SETS →

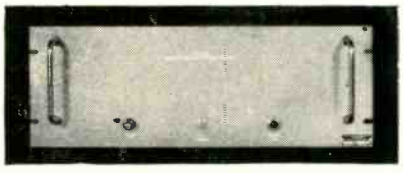
For applications where repeated use is required. Available for 30x30, 45x20, and 90x10 operation, 0 to 5 volt or 0 to 30 millivolt sensitivity, 28 volt DC or 115 volt 400 cycle primary power, for RF carrier, FM subcarrier, or magnetic tape recording. 45 watt RF power amplifier available.

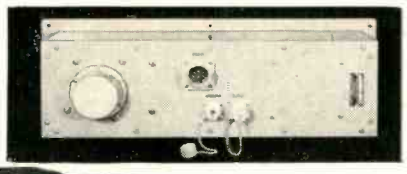


M SERIES PW GROUND STATIONS

Operate on pulse width signals from RF receiver, Subcarrier discriminator, or magnetic tape playback unit to produce visual monitoring of all data channels and reduced graphic output records of selected channels, in real time.







A SERIES ACCESSORY EQUIPMENT

RF Preamplifier units, for greatly increased receiving range, and RF Multicoupler, for operation of up to 4 receivers from a single Preamplifier or antenna. Broad band operation 215 to 235 megocycles.

G SERIES FIXED INSTALLATION MULTICODERS (Not shown)

PW Multicoders for multichannel tape recording or transmission from fixed installations. Operate from standard 60 cycle power lines . . . Designed for long life . . . easy accessibility.

ENGINEERS

This fast growing organization has immediate openings for:

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Transistor Engrs.
Sales Engrs.

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Los Angeles, Calif., Crestview 1-8870

mining minority charge carrier lifetime of a semiconductor material. The system is made up of three units: a test cabinet, a 535 Tektronix oscilloscope with a 53/54C dual beam plug-in unit and a Tektronix 121 preamplifier.

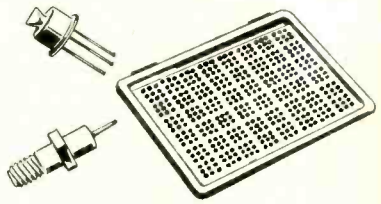
A trigger and two signals are supplied to the scope from the pulse generator and test specimen. One signal is the decay characteristic of the crystal, the other is a standard decay characteristic. For comparison the R-C standard is variable by a calibrated control on the test cabinet. Comparison of the two signals, by using a chopped sweep for simultaneous display, provides a method of reading lifetime directly to an accuracy of 5 percent by adjusting both curves for coincidence. **Circle P30 inside back cover.**

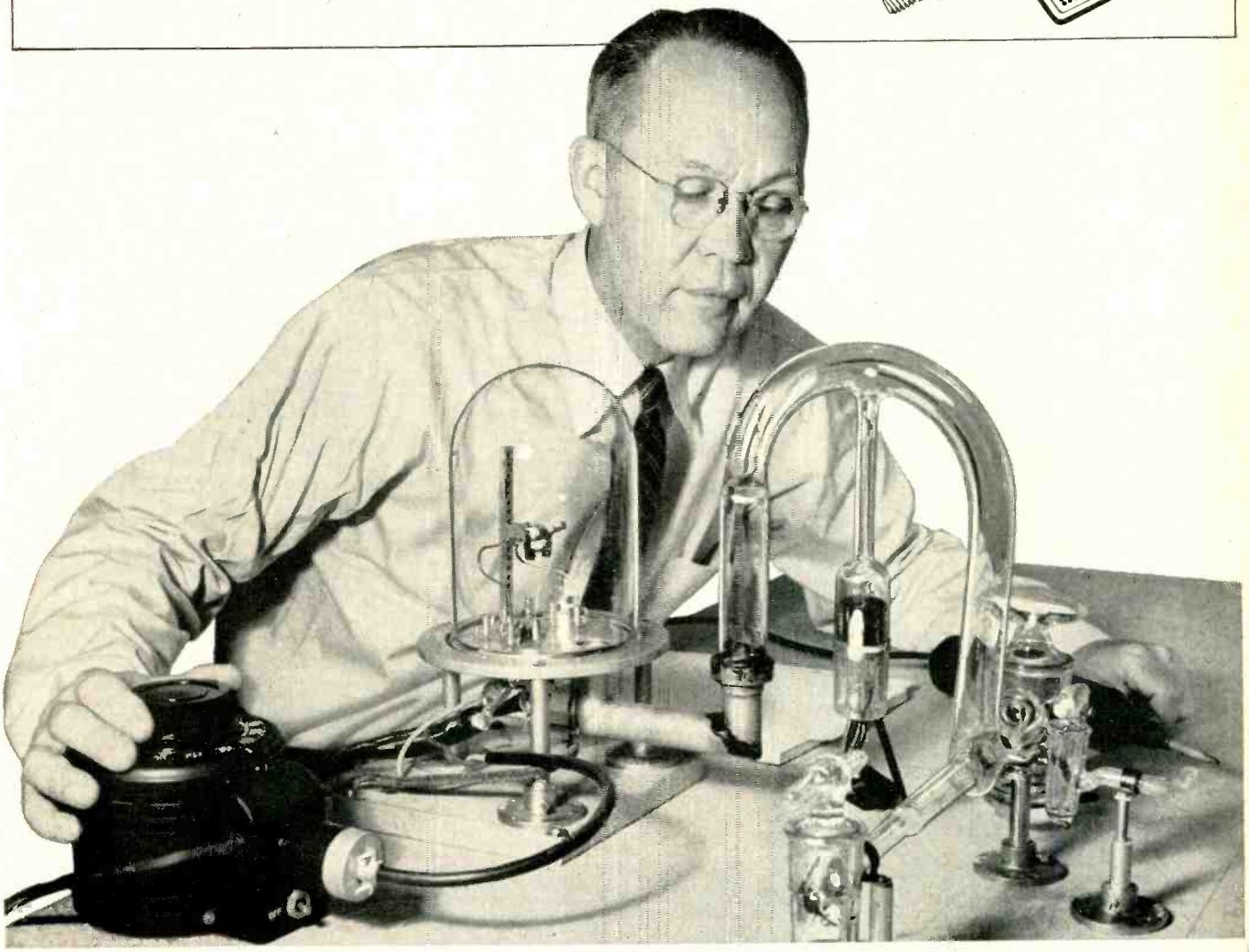
BEAM POWER TUBE
of the glass-octal type

RADIO CORP. OF AMERICA, Harrison, N. J. The 6DG6-GT is a beam power tube of the glass-octal type designed primarily for service as an output tube in audio amplifier applications. Having a 6.3-v, 1.2-ampere heater and a maximum heater-cathode voltage of ±90 v, the tube is intended especially for use in audio equipment requiring a tube having high power sensitivity and high efficiency at relatively low plate and No. 2 grid voltages.

For example, in class A1 a-f service, a single 6DG6-GT operating at a plate voltage of 200 v and a grid No. 2 voltage of 125 v, will deliver 3.8 w of audio power with a peak a-f signal-grid voltage of

New technique shapes future of transistors...
LEADS TO THREE MAJOR INVENTIONS





Calvin S. Fuller, Ph.D. in Physical Chemistry from the University of Chicago, is a pioneer in development of the diffusion technique. Here he controls a heating current through a strip of silicon while diffusing into its surface a film of aluminum less than 1/50th of a hair's breadth in thickness.

Transistor makers have a very difficult problem. They must add a mere trace of an "impurity" to a semiconducting metal. But they must add it only in very thin layers, without affecting the bulk of the material.

Bell Laboratories scientists developed an efficient new way to produce such layers. They expose the metal to a hot gas containing the impurity. Atoms bombard the surface and—through a process known as "diffusion"—force their way into the metal to form a microscopic film which can be controlled in thickness to a few millionths of an inch.

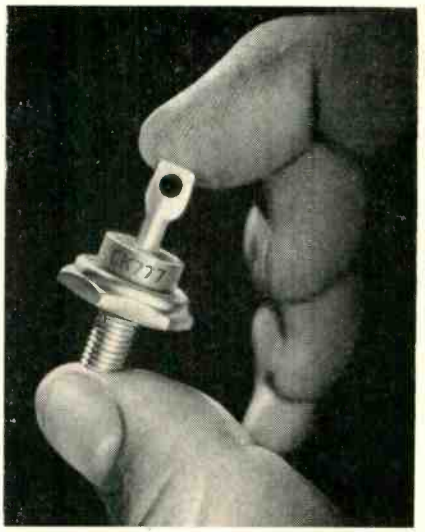
The diffusion technique opened the way to three major Bell Laboratories inventions in the semiconductor field; the Bell Solar Battery, Silicon Power Rectifier and the Diffused Base Transistor. Right now the technique is providing a key to many other developments of great promise for telephony. It is another example of how Bell Labs works to improve telephony through fundamental research in materials.

BELL TELEPHONE LABORATORIES

WORLD CENTER OF COMMUNICATIONS RESEARCH AND DEVELOPMENT

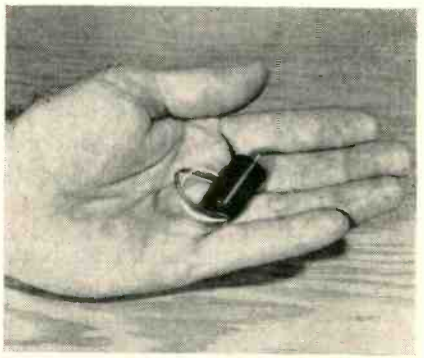
Want more information? Use post card on last page.

only 8.5 v. **Circle P31 inside back cover.**



SILICON RECTIFIERS
have piv rating of 325 v

RAYTHEON MFG. CO., 55 Chapel St., Newton 58, Mass., has added to its line of silicon power rectifiers the new type CK777 having a peak inverse rating of 325 v and an average current rating of 5 amperes at 125 C. Maximum reverse current at the piv of 325 v is only 5 ma and the maximum forward voltage drop at 10 amperes is only 2 v. The addition of type CK777 provides a line of 5-ampere, 125 C silicon rectifiers having peak inverse ratings from 25 to 325 v. Data are available from the company. **Circle P32 inside back cover.**



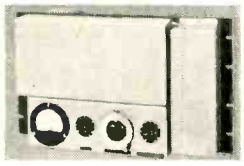
TINY SERVO MOTOR
a high-precision unit

FORD INSTRUMENT CO., Division of Sperry Rand Corp., 31-10 Thomson Ave., Long Island City 1, N. Y. With nominal dimensions of only

JK PRODUCTS

PACKAGED FREQUENCY MANAGEMENT

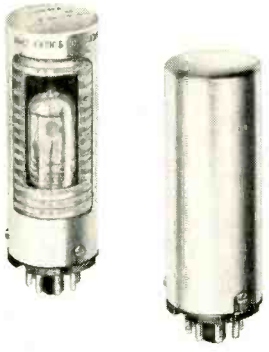
JK SULZER FREQUENCY STANDARD



JK Sulzer Frequency Standard: For your most precise laboratory measurements, the JK SULZER 1 megacycle Frequency Standard provides stability of better than 1 part in 10^9 per day. Frequency is variable over a range of 0.9 cycles or more, and capable of being reset to 5 parts in 10^{10}.

JK THERMYSTAL

JK TRANSISTOR OSCILLATOR



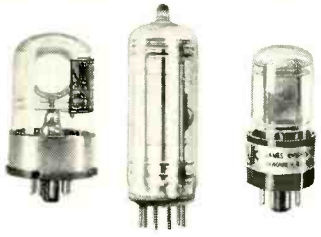
JK Thermystal: An advanced-design frequency control unit combining plug-in simplicity with extreme precision. *Frequency stability:* 30 to 900 kc, ±.0001%; 1000 kc to 150 mc, ±.00005%.

JK Transistor Oscillator: Complete, compact, precise plug-in signal source providing fixed temperature and humidity environment for transistor and circuitry elements. *Frequency stability:* (24-hr. period) 1 part in 10^6.

JK CRYSTAL FILTERS

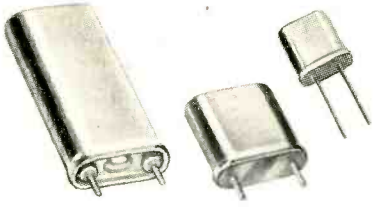
JK Crystal Filters: Compact, rugged, hermetically-sealed and stable, JK CRYSTAL FILTERS (band pass filters) have a *Frequency Range:* 1 mc to 17.5 mc., and are available for special filtering purposes to 150 mc. *Band Width* at 6 db: 0.01% to 4% of nominal on all frequencies, and up to 12% for certain frequencies.

JK GLASLINE CRYSTALS



JK Glasline Crystals: For ultra stable frequency control, JK GLASLINE CRYSTALS provide unprecedented stability and reliability. Compact, evacuated and hermetically-sealed against moisture, contamination, shock, and barometric pressure. Over a complete range of 800 cycles to 5 mc. and up.

JK MILITARY TYPES



JK Military Types: Hermetically-sealed, JK MILITARY TYPE CRYSTALS are metal-cased and in *Frequency Ranges:* 16 kc to 100 mc.

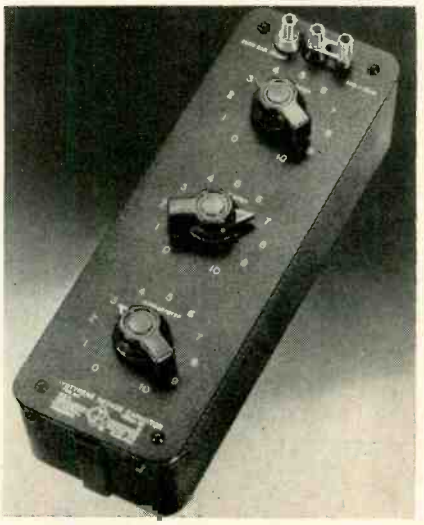
JK OVENS

JK Ovens: Capable of maintaining set temperatures around components or cicuitry with less than ±1° C. variation over the range of −55° to +100° C., JK OVENS are light, compact, inexpensive, uniform and reliable.

THE JAMES KNIGHTS COMPANY Sandwich, Illinois

⅝ in. diameter by 1 in. long (plus shaft extension) the SM-58 servo motor weighs under 1 oz. It is widely applicable to servomechanisms, computers, indicating devices, missile control systems, air craft control systems and similar equipment.

▶**Technical Data**—Featuring extremely high torque to inertia ratio, it operates on 26 v 400 cps, with a control voltage range of 0 to 26 v. Typical characteristics include: 2½-w input; 1/10-w output; 0.063 in.-oz stall torque; 8,800-rpm no-load speed; 0.00038 oz-in.^{2} rotor inertia and 64,000-rad/sec^2 theoretical acceleration at stall. Ambient range is −75 to +200 F. **Circle P33 inside back cover.**



DECADE CAPACITORS with polystyrene dielectric

GENERAL RADIO CO., 275 Massachusetts Ave., Cambridge 39, Mass. Polystyrene capacitors are now offered in the form of decade units. The individual capacitor units are noninductively wound with purified high-molecular-weight polystyrene tape and carefully heat treated. Units are hermetically sealed in brass cans with Teflon insulators. Polystyrene and Teflon are used as dielectrics in the decade switches. The decade assembly has an insulation resistance of greater than 10^{12} ohms at 100 v. Dissipation factor is specified to be less than 0.0002 in the audio range and is usually

New Allen-Bradley developments

GREATER COLOR PURITY—BETTER CONVERGENCE

1. FULL ROUND YOKE CORES

FOR COLOR TV

ALSO BLACK AND WHITE

Allen-Bradley has developed a method of producing ferrite deflection yoke cores as a full 360° ring! Unlike cores made from quarter rounds, the new full round cores are perfectly concentric and have parallel inner surfaces. They require no grinding. The round rings are "cracked" into halves and taped for shipment. Assembly is quick and economical. The tape is rolled back, the core is slipped over the coils, and the tape put back in place. The core's concentricity assures better convergence and greater color purity.

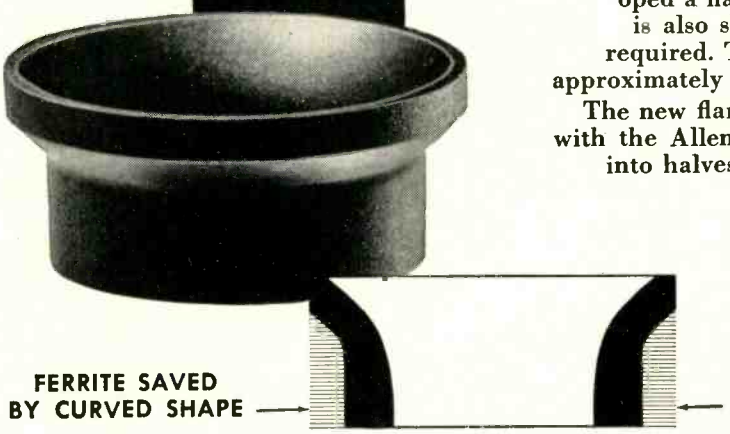
These ferrite yoke cores are produced as full rounds, and are "cracked" into halves and taped, as shown, for easy assembly.

2. FLARED YOKE FERRITE CORES

FOR NEW 110° TUBE . . . SAVES WEIGHT

For the new 110° picture tube, Allen-Bradley has developed a flared yoke ferrite core whose outer surface is also shaped to reduce the amount of material required. This makes possible a weight reduction of approximately 30% over conventional cylindrical cores.

The new flared yoke is produced as a solid piece but, with the Allen-Bradley method, the yoke is "cracked" into halves, yet a perfect ring is maintained. Available in Allen-Bradley Class WO-1 ferrites which are to be preferred because of their uniform magnetic characteristics.



Allen-Bradley Co.
110 W. Greenfield Ave.
Milwaukee 4, Wis.

In Canada—
Allen-Bradley Canada Ltd., Galt, Ont.

A-B Quality

ALLEN-BRADLEY

RADIO, ELECTRONIC, AND TELEVISION COMPONENTS

QUALITY

about half that amount.

Individual type 980 decade capacitor units in steps of 0.001, 0.01, and 0.1 μf are available as well as a 3-dial type 1419-A decade capacitor with a range to 1.11 μf in steps of 0.001 μf. **Circle P34 inside back cover.**

VACUUM CAPACITOR
designed for strenuous use

DOLINKO & WILKENS, INC., 1907 Summit Ave., Union City, N. J. Type VC500-32 high-capacitance, high-voltage, high-current vacuum capacitor is designed for strenuous application in electronic heating and transmitting equipments. Constructed of OFHC copper with Pyrex glass seals and bulb it gives low-loss, low-inductance service in r-f tank usage. It is rated at 500 $\mu\mu$f, 32 kv peak and 120 rms amperes. Dimensions are $7\frac{5}{8}$ in. overall length, $3\frac{9}{16}$ in. diameter; mounting centers are $6\frac{5}{8}$ in. and contact diameter 2 in. **Circle P35 inside back cover.**

DELAY LINES
large delay to size ratio

MAG ELECTRIC, Electronic Division, National Aircraft Corp., 3411 Tulare Ave., Burbank, Calif. Designed for both commercial and military applications, the new

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Do the booklets, pamphlets, and manuals you use really *work* for you? Are these vital publications, that tell the story of your products and your company, as effective, readable, well designed and illustrated as they can be? Today more than ever, your entire operation is judged by each annual report, employee manual, and public relations piece that you produce. Have you examined your communications lately? If you have any doubt as to the impact of your instructional and promotional literature, remember . .

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model ED delay lines are now available, which provide exceptionally large delay to size ratio. Featured are hybrid forms of bank and other layer type windings.

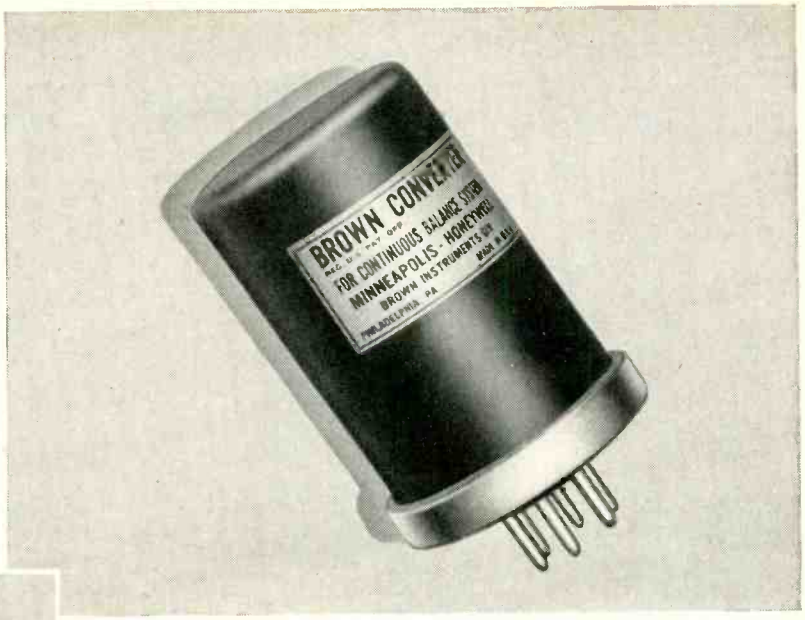
The units discussed are cast in resin and are equipped with hole or stud type mountings and can be furnished with taps.

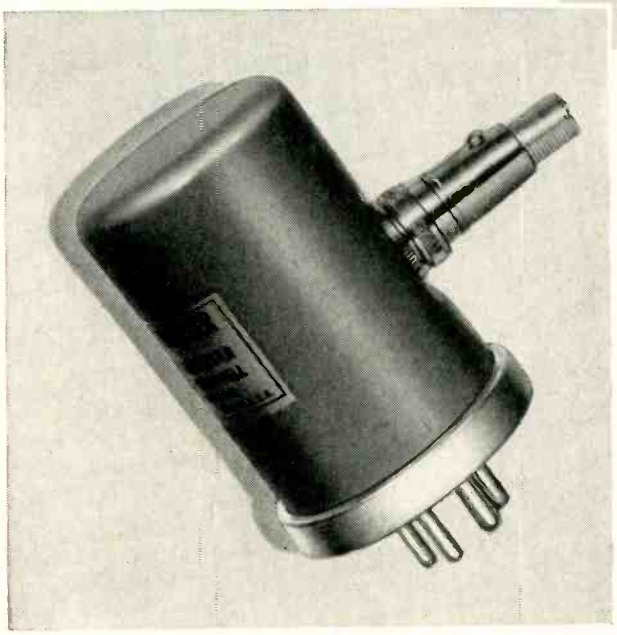
Specifications include: delay range—0.1 to 20.00 μsec in multiples of 0.1 μsec; rise time, 10 to 15 percent of delay times; impedance range, 500 to 5,000 ohms, ±10 percent. Attenuation is 2 percent per μsec delay; distortion, less than 5 percent; operating temperature, −55 to +125 C; working voltage, 500 v d-c. **Circle P36 inside back cover.**

POWER SUPPLY
constant current, voltage

MATTHEW LABORATORIES, 146 Riverdale Ave., Yonkers, N. Y. Model CVPS-105 is a dual purpose power supply designed to provide either constant current or constant voltage as desired, for use in semi-conductor and electronics research, or as a general laboratory supply. The required current or voltage remains constant at the selected value under varying load or input line conditions. Regulation is provided by feedback loops, a control amplifier and series regulator tubes. The current or voltage, at any desired value from zero to maximum, is set by continuously variable coarse and fine controls.

The output is monitored by a multirange combination voltmeter-milliammeter. On constant current, the output is 0 to 130 ma, with the voltage automatically ad-





Brown Converters

put stable performance in your measuring and servo loops

THESE synchronously-driven choppers convert d-c signals as low as 10^{-8} volt to ac, with freedom from pickup and exceptionally low thermal noise.

Ideal for radar, computers, servomechanisms and null balance circuits, Brown converters are built for long, dependable service. Thousands of them have been used for continuous duty for years in *ElectroniK* instruments.

In standard models, each contact closes for 55% of the cycle. Other closure cycles can be supplied. Output signal lags line voltage by 17° ± 5. Power rating is 0.1 milliwatt.

Four standard models are available. In addition, many variations can be provided for special requirements.

• ***ORDER NOW!*** Prices from **$36.00** (even more favorable depending on quantity).

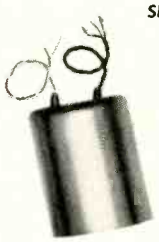
MINNEAPOLIS-HONEYWELL REGULATOR CO., *Industrial Division*, Wayne and Windrim Avenues, Philadelphia 44, Pa.—in Canada, Toronto 17, Ontario.

Available in these ratings

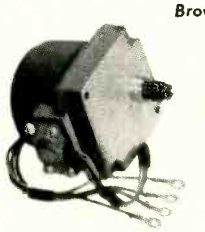
Nominal frequency, cps	25	40	50-60	400
Synchronous range, cps	23-28	36-44	45-66	360-440
Driving coil	6.3 volts, 60 ma.			18 volts, 94 ma.

MINNEAPOLIS **Honeywell**
BROWN INSTRUMENTS
First in Controls

Other Brown components for servo systems

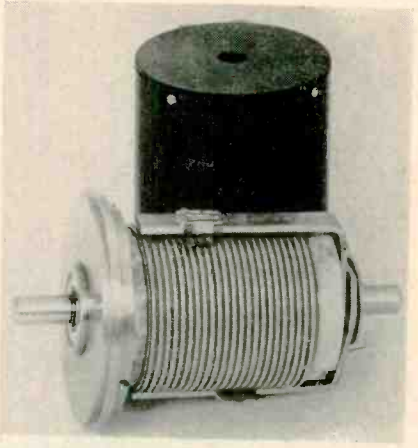


Shielded low-level transformers, for input or coupling circuits, faithfully handle low-frequency a-c, or chopper-modulated d-c signals from 0.0005 to 200 millivolts. Highly effective electrostatic and magnetic shielding. Wound for maximum cancellation of strays. Three models; impedances 1,300, 7,500 and 50,000 ohms input at 60 cycles. Prices from $21.00.



Brown Servo Motors. 2-phase reversible motors with high torque at low speed. Totally enclosed. Permanently lubricated. 60-cycle models with no-load shaft speeds of 27, 54, 162, 333 and 1,620 rpm. 25-cycle models also available. Prices from $42.00.

justing itself between 0 and 400 v. On constant voltage, the output range is 0 to 500 v and 0 to 200 ma. In addition, 6.3 v a-c at 4 amperes is provided. **Circle P37 inside back cover.**



PRECISION POT
in several ganged versions

LITTON INDUSTRIES, 5873 Rodeo Road, Los Angeles 16, Calif. Model No. MD20 2-in. diameter ultraprecision potentiometer is available in several ganged versions designed for use under extremely rugged environmental conditions. Utilizing a new design, independent linearity may be provided as close as 0.01 percent. For highest stability, the resistance coil is externally wound on a nonhygroscopic ceramic core which is chemically inert and dimensionally stable. For greatest physical strength and dimensional accuracy, all operating parts are supported by a new one piece, central aluminum hub.

Length of the 10-turn MD20 is $1\frac{35}{64}$ in. In a length of $2\frac{3}{16}$ in., it can be supplied with two gangs of 10 turns, a single gang of 15 or 20 turns and other combinations of turns not readily available previously.

Rugged metal-to-metal traveling-nut-stops withstand 500 in.-oz. The wiper arm operates independently of the stops and, to minimize wear, only the wiper touches the resistance element. Electrical angle is 3,600 deg with 90-deg overtravel at each end. Resistance values of 1,000 to 100,000 ohms are standard for the two-gang 10-turn version. Torque on

Henry Rempt (center), head of the Electronics and Armaments Systems Division, discusses advanced data transmission and data handling systems for A.E.W. aircraft with Systems Engineer Bruce MacDonald (left) and Dominick Amara, head of the Advanced Systems Dept.

To electronics engineers who seek a wide range of assignments

Electronics systems engineering appeals particularly to engineers who require varied outlets for their abilities. And at Lockheed's California Division, engineers interested in systems endeavor find the broadest field for their efforts. For Lockheed's activities and assignments cover virtually every type of aircraft – radar search planes, high-speed fighters, cargo and passenger transports, bombers, jet trainers and other classified projects.

These brief facts illustrate the extent of Lockheed diversification and varied assignments – 15 models of aircraft are in production; 48 major projects are in research and development stages.

Career-minded engineers will find recent organizational changes at Lockheed of great interest. To keep pace with its increasing emphasis on electronics, Lockheed has expanded and centralized electronic research and development under the Electronics and Armament Systems Division. The expanded division originates and develops all complex electronics and armament systems for new Lockheed aircraft.

Technical management positions are open in fields of:

Fire control, countermeasures, inertial systems, weapons, communications, infra-red, optics, sonics, magnetics, antennas and micro-waves.

Systems engineers in these areas will supervise and participate in conceiving advanced systems and then performing research, development and evaluation up to production stages on all Lockheed aircraft.

Previous systems experience is not necessary to join Lockheed. Inquiries are welcomed from engineers who have been specializing in a narrow field of electronics and wish to broaden their approach.

NATIONAL ENGINEERS' WEEK
FEBRUARY 17-23, 1957
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Electronics Engineers possessing experience or keen interest in systems activities are invited to write E. W. Des Lauriers, Dept. 0902

California Division

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AIRCRAFT CORPORATION • BURBANK

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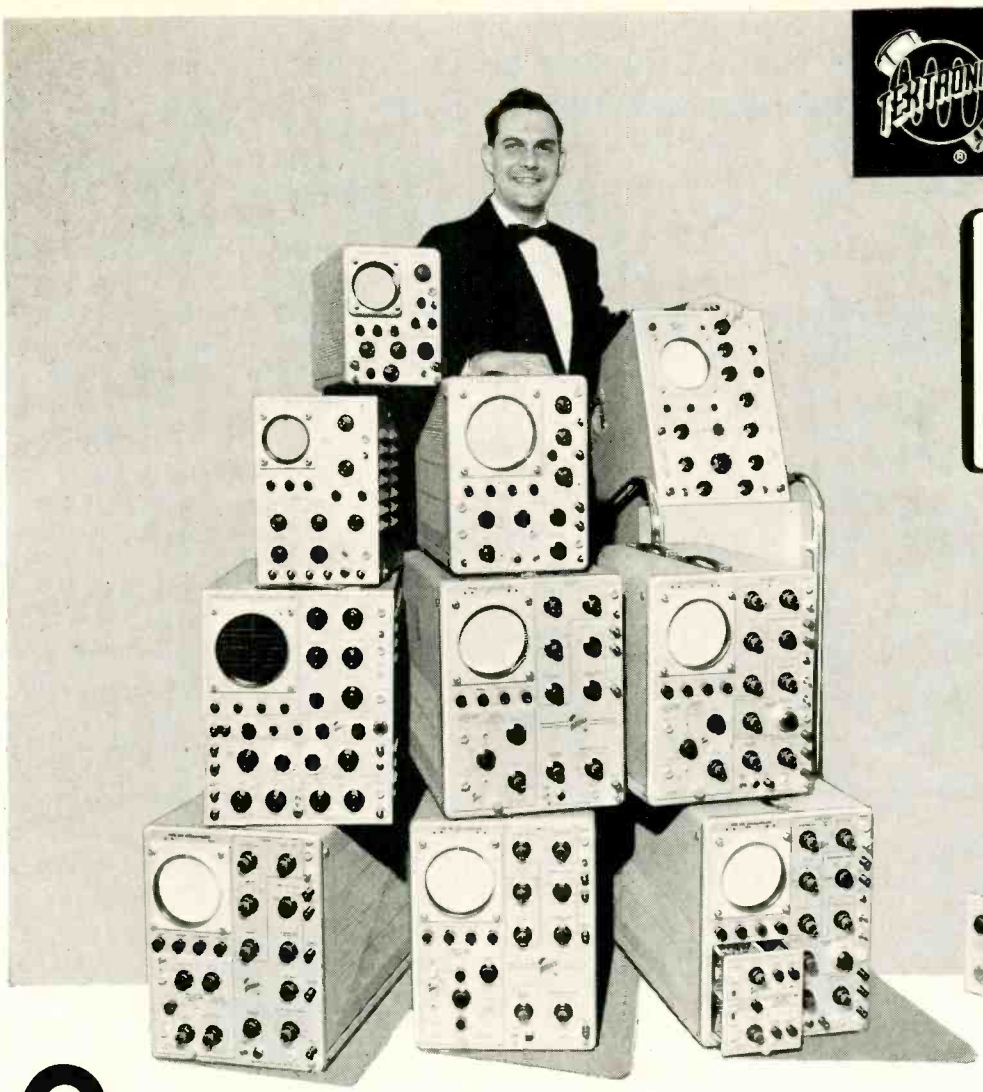
dual section versions is as low as 1.5 in.-oz. **Circle P38 inside back cover.**

FERRITE YOKE CORES for tv picture tubes

ALLEN-BRADLEY Co., 136 West Greenfield Ave., Milwaukee 4, Wisc., has announced a new ferrite full-round deflection yoke core for use in tv picture tube assemblies. The yoke core is pressed as a ring of perfectly uniform section and circularity. It is then cracked into two halves for later assembly over deflection coils and fitting to the tube. The mated halves are shipped held together mechanically to avoid possible damage in transit. Such circular yokes eliminate the grinding, fitting and setting necessary with quarter-round sections. Inner and outer surfaces are always perfectly concentric and parallel. Result is better convergence, greater color purity and reduced assembly time. **Circle P39 inside back cover.**

VOLTAGE GENERATORS use computer circuitry

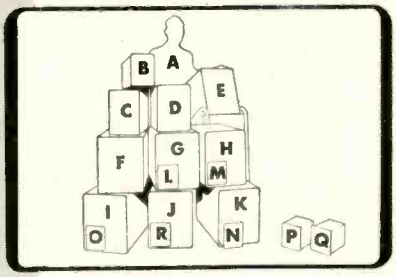
INTERCONTINENTAL DYNAMICS CORP., 170 Coolidge Ave., Englewood, N. J., has announced a line of random voltage generators, producing l-f noise with precisely



A. Tektronix Field Engineer.

B. Type 310 Oscilloscope. 3" portable, dc to 4 mc, weight only 23½ lbs. Price $595.

C. Type 315D Oscilloscope. 3" portable, dc to 5 mc, weight only 36 lbs. Price $770. Rack-mounting model also available.

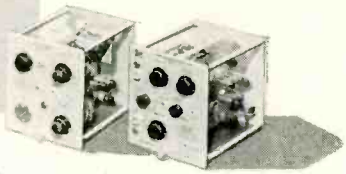


D. Type 515 Oscilloscope. 5" portable, dc to 15 mc. Weight only 40 lbs. Price $750.

E. Type 517A High-Speed Pulse Oscilloscope. Seven-millimicrosecond risetime, 24 kv accelerating potential. Price $3500.

F. Type 524AD Television Oscilloscope. DC to 10 mc, 0 to 25 millisecond sweep delay. Price $1180.

G, H, I, J, K. Oscilloscopes using plug-in preamplifiers. Seven Plug-in Units available. Extra wide sweep range. Extreme versatility.



One of these oscilloscopes may belong in *YOUR* picture

If an oscilloscope with the right characteristics will help speed progress in your work, you'll be interested in the performance range covered by these ten Tektronix Oscilloscopes. Each has been designed for a particular application, from the compact Type 310 Portable Oscilloscope to the Type 517A, specialized for high-speed pulse analysis. Each of the five oscilloscopes designed to work with interchangeable plug-in preamplifiers offers an extremely high degree of versatility in a single instrument.

Your complete oscilloscope requirement may be satisfied by one of the more versatile instruments. Or, you may have an unusual requirement that can be satisfied only by a highly-specialized oscilloscope. In selecting the right oscilloscope for your present and future needs, a consultation with your Tektronix Field Engineer can be very helpful. It's a matter of great importance to him that you make the best possible selection, because his term of responsibility parallels the useful life of your Tektronix instrument . . . and that's a huge chunk of his future.

ENGINEERS—interested in furthering the advancement of the oscilloscope? We have openings for men with creative design ability. Please write to Richard Ropiequet, Vice President, Engineering.

G. Type 531 Oscilloscope. DC to 10 mc, 10 kv accelerating potential. Price, without plug-in units, $995.

H. Type 535 Oscilloscope. DC to 10 mc, 10 kv accelerating potential, 1 μsec to 0.1 sec sweep delay. Price, without plug-in units, $1300.

I. Type 532 Oscilloscope. DC to 5 mc, 4 kv accelerating potential, 8-cm linear vertical deflection. Price, without plug-in units, $825.

J. Type 541 Oscilloscope. DC to 30 mc, 10 kv accelerating potential. Price, without plug-in units, $1145.

K. Type 545 Oscilloscope. DC to 30 mc, 10 kv accelerating potential. 1 μsec to 0.1 sec sweep delay. Price, without plug-in units, $1450.

PLUG-IN UNITS

L. Type 53/54A Wide-Band DC $85

M. Type 53/54B Wide-Band High-Gain 125

N. Type 53/54C Dual Trace Fast-Rise DC 275

O. Type 53/54D Differential High-Gain DC 145

P. Type 53/54E Differential Low-Level AC 165

Q. Type 53/54G Differential Wide-Band DC 175

R. Type 53/54K Fast-Rise DC . . 125

All prices f.o.b. Portland, Oregon

Tektronix, Inc.

P. O. Box 831 • Portland 7, Oregon

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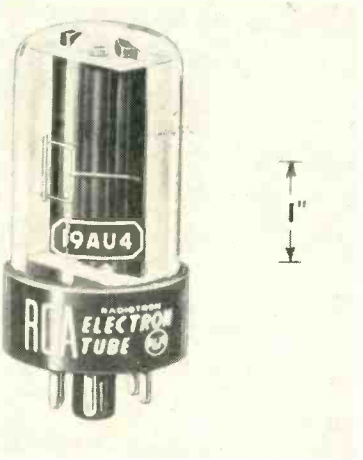
controlled power frequency spectra and predetermined amplitude probability characteristics. The generators are designed to provide ultrastable, accurate statistical functions for computer analysis, missile system analysis, instantaneous servo transfer function derivation, radar countermeasure studies, as a driving source for truly random vibration and shaker testing, and for general l-f noise analysis purposes.

▶ **Ranges**—Available in six different models covering the frequency ranges from 0.01 to 50, 1,000, 3,000 and 5,000 cycles and to 1 and 5 mc, the generators provide noise signals whose amplitude distribution with time is accurately Gaussian, at an output level of 5 v rms into 600 ohms with direct-reading calibrated attenuation.

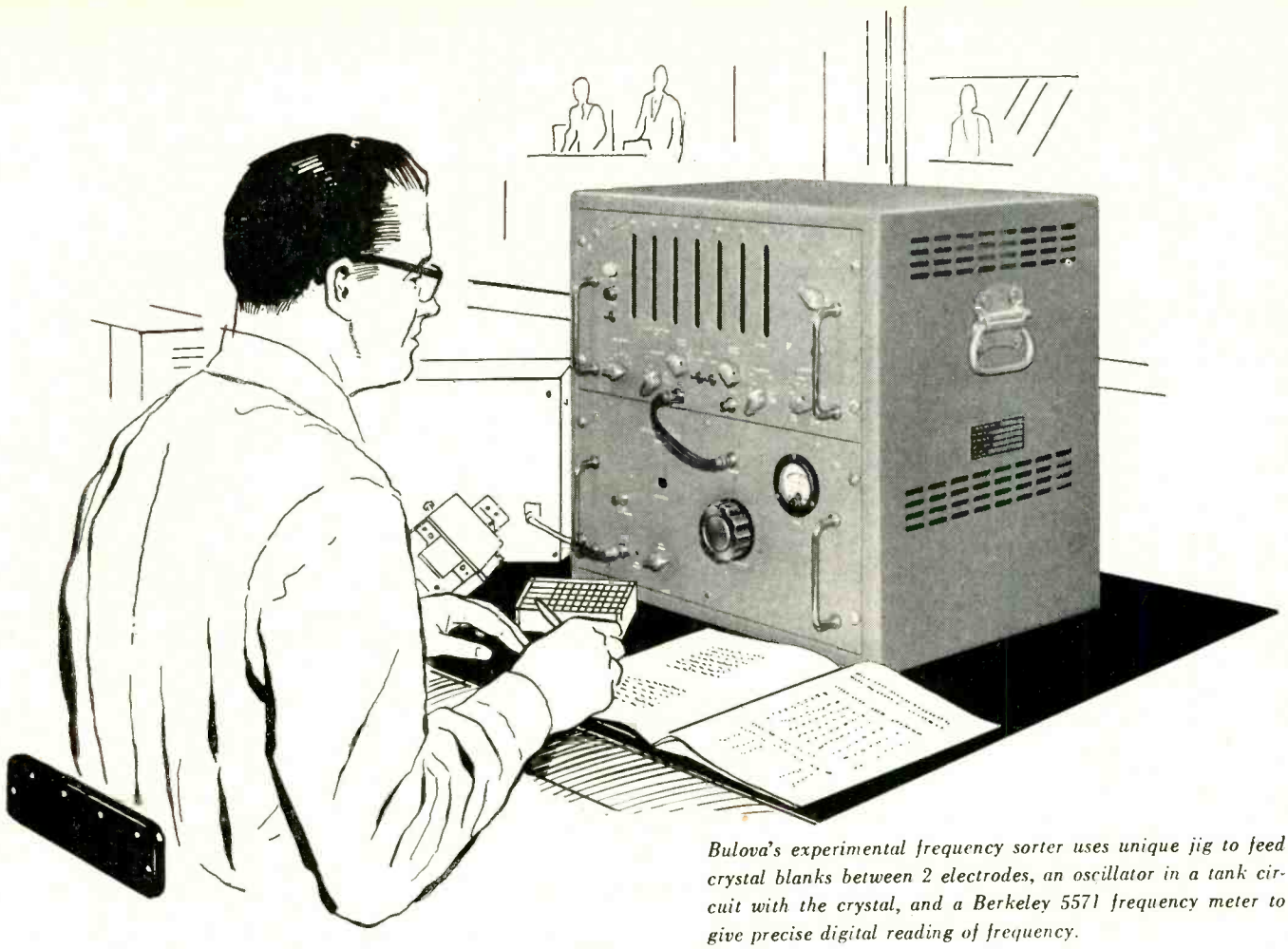
Complete specifications are available on request. **Circle P40 inside back cover.**



DAMPER DIODE
for tv receivers

RADIO CORP. OF AMERICA, Harrison, N. J. The 19AU4 is a half-wave rectifier tube of the glass-octal type intended for use as a damper diode in horizontal-deflection circuits of black-and-white tv receivers. This tube is designed with an 18.9-v, 600-ma heater having a controlled heating time to insure dependable performance in tv receivers utilizing series-heater-string arrangement.

Rated to withstand a maximum peak invert plate voltage of 4,500 v (absolute), the tube can supply



Bulova's experimental frequency sorter uses unique jig to feed crystal blanks between 2 electrodes, an oscillator in a tank circuit with the crystal, and a Berkeley 5571 frequency meter to give precise digital reading of frequency.

Doing a day's work in 12½ minutes!

Mechanizing military crystal production posed plenty of problems for Bulova Research and Development, Inc. The Signal Corps wanted 50,000 crystal blanks a day processed, a sizeable increase over the 1500 a day by current techniques.

From the experimental setup pictured above, they developed an automatic frequency sorter with a capacity of 2 blanks per second, or 1500 in 12½ minutes, (now being built by Berkeley Systems Engineering group). Tolerance is 0.005% of normal frequency, range is 4 to 54 mc.

Without the Berkeley 5571 frequency meter as a basis, this development would not have been possible. The services of Gawler-Knoop, Berkeley's engineering representative in the New York area, were equally invaluable in making this 5571 application and subsequent service a success for Bulova.

If your work involves measurement of frequency ratio, frequency period, or frequency from 0 cps to 1100 mc it will pay you to investigate the versatile 5571—the meter that literally "grows with the job."

118

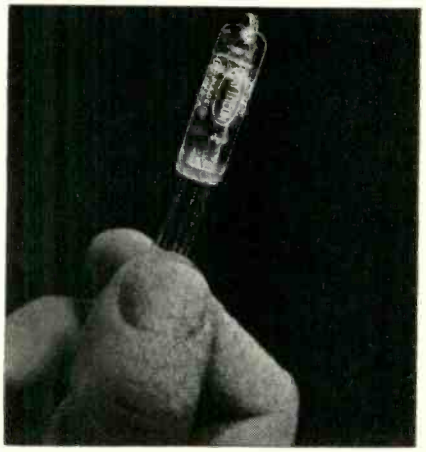
Write now for technical data; please address Dept. G-2.

Beckman®

Berkeley *Division*

2200 Wright Avenue, Richmond 3, California
a division of Beckman Instruments, Inc.

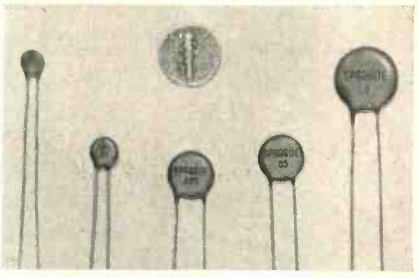
a maximum peak plate current of 1,050 ma and a maximum d-c plate current of 175 ma. A technical bulletin is available. **Circle P41 inside back cover.**



TINY TWIN TRIODE with low microphonics

RAYTHEON MFG. CO., 55 Chapel St., Newton 58, Mass. Designed especially for d-c amplifier and computer applications, the type CK6832 is a subminiature twin triode with unusually low microphonics and grid current. It is controlled for balance between the two sections including stability with time, shock and variation in heater voltage.

The CK6832 is electrically similar to the miniature type CK5755. **Circle P42 inside back cover.**



TINY CAPACITORS high-dielectric constants

SPRAGUE ELECTRIC CO., 125 Marshall St., North Adams, Mass., has standardized for mass production a new subminiature series of high-dielectric constant Cera-mite capacitors. Intended for transistor radios and similar applications, they are rated at 50 v d-c. They have been tooled for volume pro-

THE

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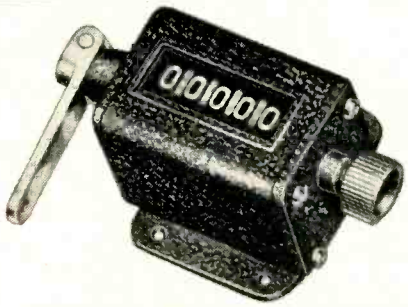
OF

1 2 3

Why is COUNTROL

important in every business today?

Countless times a day, every business needs to know "how many? . . . how much? . . . how far? . . ." and many other questions that can be answered only by facts-in-figures. But how to get these figures . . . from so many different machines, processes, operations and systems? Veeder-Root Counters are doing it every day, by means of:



MECHANICAL COUNTING

Small Resets count strokes, turns, or pieces . . . are used by thousands for moderate duty in parts inspection, quality control, conveyors, machine tools, light presses, etc.

HAND COUNTING

Where objects or units cannot be counted electrically or mechanically, hand-operated counters like this Hand Tally do the job. For instance, quick spot checks of production or performance, traffic count, inventory, etc. Fits palm of hand, counts one for each pressure of thumb lever, resets to zero by turning knob.

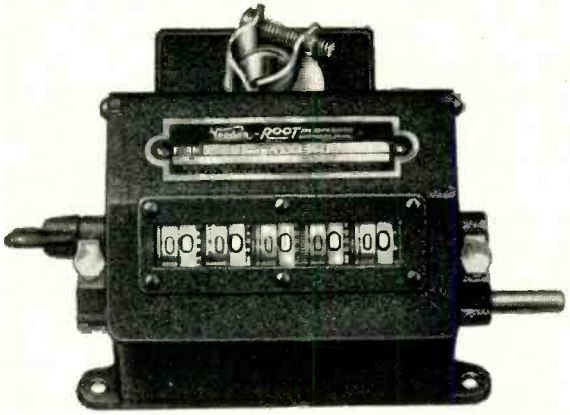
Insist on Standard

VEEDER-ROOT COUNTERS

from your Industrial Supply Distributor

ELECTRICAL COUNTING

These remote-indicating counters bring your production machines as close as your office wall. AC or DC, they can be connected in series with any simple switch, and will transmit production figures *instantly* over any distance. May be panel-mounted in groups.



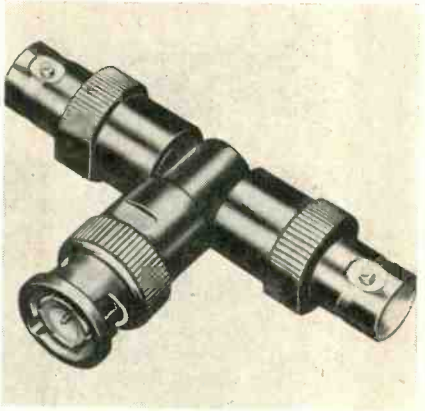
CONTROLLING

Set it for the exact number of turns, pieces, or operations required . . . and this Predetermining Counter will control the run *exactly* . . . preventing over-runs and shortages. When the predetermined number is reached, counter will light a light, ring a bell, or actuate a stop-motion.

IN SUM: *If it can be counted or controlled . . . count on Veeder-Root to do it. Get in touch with your Industrial Supply Distributor for standard counters for application to your production machines and processes. And get in touch with Veeder-Root for counters to be built into original equipment.* **Veeder-Root Inc., Hartford 2, Connecticut.**

duction in standard capacitances of 0.005, 0.01, 0.025, 0.05 and 0.1 μf.

Full performance characteristics on the bantam capacitors are given in engineering data sheet 6121. **Circle P43 inside back cover.**



TINY COAX PARTS incorporate BNC connectors

MICROLAB, 71 Okner Parkway, Livingston, N. J., announces a new line of miniaturized coaxial components incorporating type BNC connectors. The line is designed for airborne and other applications requiring compact, lightweight components.

Included are fixed pad attenuators, coax terminations, low pass and high pass filters, power dividers, crystal mounts and double stub tuners. The line provides considerable space and weight conservation for missile and aircraft designers without sacrificing electrical performance. A complete catalog of miniaturized components is available on request. **Circle P44 inside back cover.**

SOLDER RESIST for printed circuits

LONDON CHEMICAL CO., INC., 1535 N. 31st Ave., Melrose Park, Ill. A new solder resist which permits selective soldering, minimizes bridging over close tolerances and reduces solder waste has been developed for printed circuits. The PC No. 33 solder resist is an organic coating which affords high insulating resistance across the circuit pattern. It has a low temperature cure of 200 F and requires a cure time of only 20 to

the delicate touch . . . *is repeated hundreds of times in many different ways to build a rugged Varian klystron cathode.*

In airborne use, the cathode must operate with complete reliability . . . withstand constant shock and vibration without malfunction or failure.

It takes a delicate touch in the use of intricate fabrication techniques to build small yet rugged cathodes. For example, the tiny cathode button — often not much larger than the head of a pin — is carefully electropolished, then spray-coated with a precisely controlled mixture of rare earth oxides. Why?

To assure uniform emission of electrons . . . vital factor in reliable performance.

Optimum structural rigidity is achieved by skillful metallic bonding of each electrode to a ceramic disc . . . connections are individually brazed with a copper-gold alloy. Pressure-ventilated assembly benches are used to keep air superclean . . . prevent contamination from microscopic particles which might affect performance or cause failure.

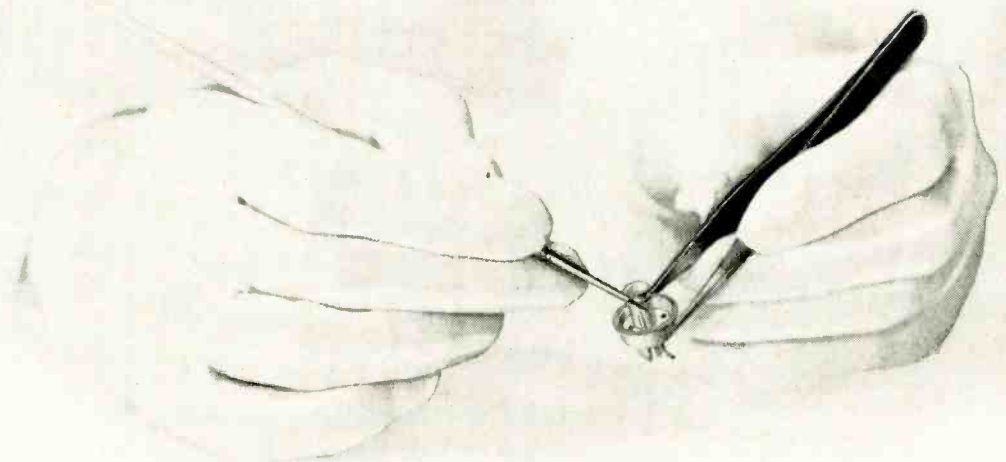
Painstaking techniques like these exemplify Varian's manufacture of more than 60 different klystrons for every application.

THE MARK OF LEADERSHIP

VARIAN associates

PALO ALTO, CALIFORNIA

Representatives in all principal cities



FOR COMPLETE INFORMATION... write for the Varian Klystron Catalog... address Applications Engineering Department K-2.

KLYSTRONS, TRAVELING WAVE TUBES, BACKWARD WAVE OSCILLATORS, LINEAR ACCELERATORS, MICROWAVE SYSTEM COMPONENTS, R. F. SPECTROMETERS, MAGNETS, MAGNETOMETERS, STALOS, POWER AMPLIFIERS, GRAPHIC RECORDERS, RESEARCH AND DEVELOPMENT SERVICES

30 minutes. The film it deposits is resistant to peeling, pitting or blistering and will not break down at high solder pot temperatures up to 650 F, with immersion of 10 to 15 sec.

▶ **Application**—Recommended procedure calls for screening circuits with a 165-mesh stainless-steel or equivalent silk screen, after which they are cured for 20 to 30 minutes at 200 F. Regular assembly, fluxing and soldering can proceed immediately after the circuit cools.

The resist can be applied as received or thinned to desired viscosity with PC No. 33 solder resist thinner. **Circle P45 inside back cover.**

MATCHING UNIT
used with audio oscillator

WAVEFORMS, INC., 333 Sixth Ave., New York 14, N. Y., announces a new device for use with the 510B audio oscillator. The T-10 matching unit consists of a repeat coil and resistive network designed to furnish a balanced signal of up to +8 dbm. Impedances of 150 or 600 ohms ±5 percent over the range 18 cps to 50 kc are selected by straps at the binding posts.

The unit is housed in a sheet metal enclosure which forms a permanent part of the oscillator assembly. Price $40. **Circle P46 inside back cover.**

RESISTOR BOBBINS
composed of expoxide resin

NORRICH PLASTICS CORP., 35 E. 32 St., New York, N. Y. A new line of bobbins, used for the construction of hermetically sealed re-

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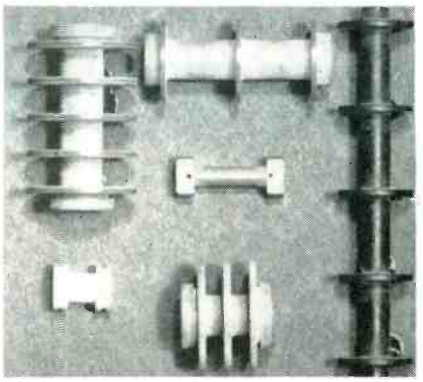
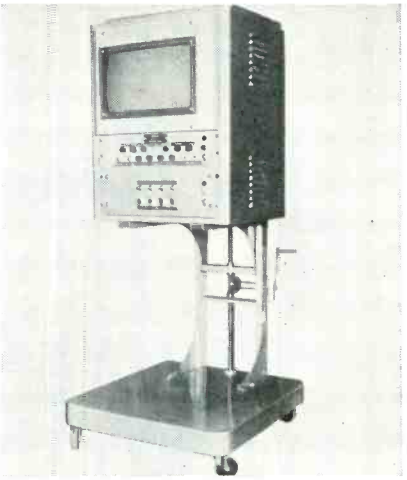


sistors, are machined from filled thermosetting epoxide resin rods. This resin was selected because of its exceptional electrical and mechanical properties. Its outstanding adhesion quality is ideal for hermetic sealing of wire wound resistors.

The bobbins are not affected by extremes in humidity, altitudes nor corrosive influences. The potting compound used for the encapsulating of the resistors is composed of the same resin as the bobbin form. This technique insures the hermetically sealed condition of the resistor at extreme temperatures, since the bobbin and encapsulation contract and expand to the same degree. **Circle P47 inside back cover.**



MONITORSCOPE
aid to the medical field

ESSENTIAL ELECTRONICS CORP., 1011 Power Ave., Cleveland 14, Ohio. The Monitorscope permits instantaneous observation of the electrocardiograms, electroencephalograms and electromyograms of a patient in the operating room or in the laboratory. It is an oscil-

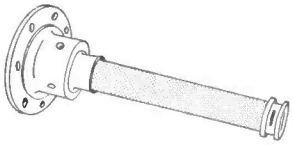
TAYLOR
Laminated Plastics
Vulcanized Fibre

Shop Talk

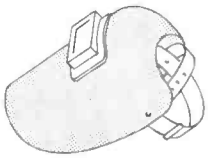
TAYLOR FIBRE CO.
Plants in Norristown, Pa. and La Verne, Calif.

PHENOL—MELAMINE—SILICONE—EPOXY LAMINATES • COMBINATION LAMINATES • COPPER-CLAD LAMINATES • VULCANIZED FIBRE

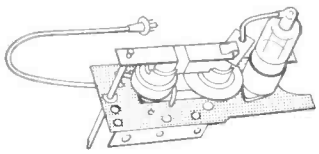
Tips for designers



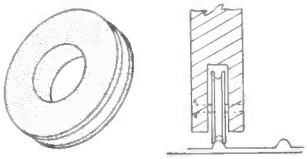
Aircraft fuel gage tank unit uses a tube of Taylor epoxy glass base laminate . . . an unusual material noted for excellent corrosion resistance and electrical insulation over a wide humidity range.



Welders' helmets are fabricated from tough durable Taylor vulcanized fibre . . . readily formed to many desired contours.



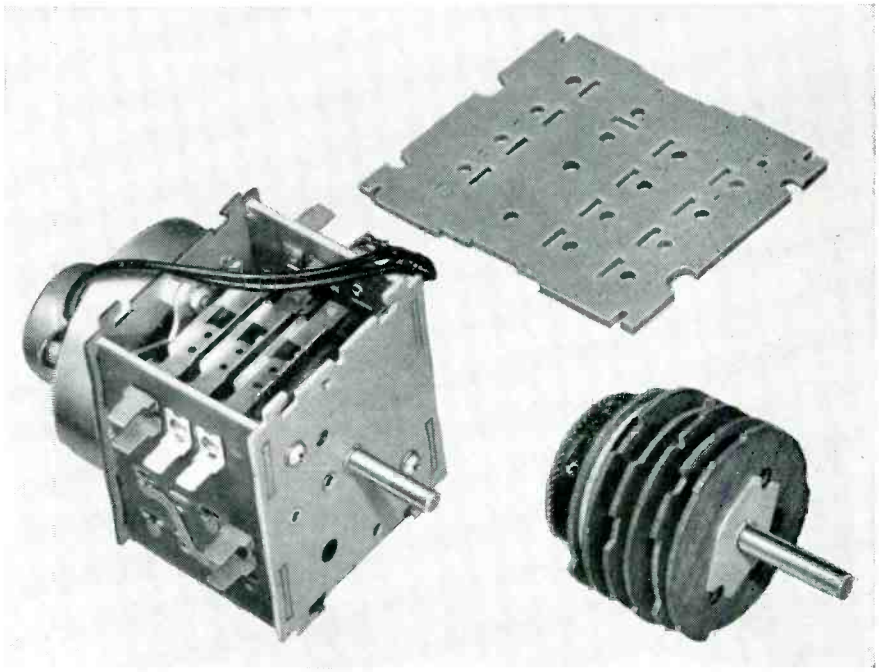
Base plate for high-voltage TV component, punched from Taylor canvas melamine laminate, has high dielectric strength and arc resistance.



Rollers for flush doors are now being made from Taylor paper base tubing with ball bearing insert . . . providing smooth, silent operation at a low cost.

NEW TAYLOR
COPPER-CLAD LAMINATES

Taylor GEC (glass-epoxy) Copper-Clad and Taylor XXXP-242 cold punching (paper-phenol) Copper-Clad. Taylor uses high purity rolled copper on base materials with outstanding electrical properties.



Interval timer switches, made by P. R. Mallory & Co. Inc., use various grades of Taylor paper base phenol laminates for cams and terminal boards. These laminates provide electrical insulation, strength, dimensional stability.

Tough specifications?
check Taylor phenol laminates

Choose from over 30 grades of Taylor phenol laminates, for the combination of electrical, physical, and machining properties you want. These rugged, versatile laminates can meet your most demanding specifications, improve end-product performance . . . and bring you major savings in material and fabrication costs.

These laminates, consisting of a paper, cotton fabric, asbestos, glass cloth or nylon base impregnated with Phenol resins, were developed to meet the need for dependable, moisture resistant insulation. They possess high dielectric and mechanical strength. Unaffected by heat or cold (except extremely high temperatures) they resist oils and most chemicals, and are especially suited to the punching and machining of accurately-sized parts. Because of their high moisture-resistance qualities, Taylor phenol laminates will not readily warp or become distorted when subjected to alternating wet and dry conditions.

You'll like the way these laminates handle in the shop . . . how they punch and stake cleanly, how they readily machine to hairline tolerances. And you'll like the way they perform in product application, how they retain their original characteristics over long periods of time and under severe operating conditions.

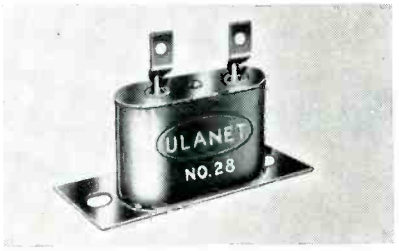
Taylor offers the service of its field specialists to help you choose the grade of material that matches the exact requirements of your application. Check with Taylor now. Write for the general catalog of Taylor materials. And contact your nearest Taylor sales engineer for a discussion of your particular requirements.

loscope distinguished by its 17-in., multichannel, long-persistent c-r screen; its mobility; its adaptability and its operating room safety.

With either two or four channels (optional) that may be operated independently and simultaneously, the Monitorscope displays the EKG, EEG or EMG in large complexes, each channel appearing as a separate horizontal trace. When all channels are not needed, the unused traces may be turned off.

For safety of operation during surgery, the Monitorscope is equipped with a frame which elevates the cabinet above 5 ft for operating room service and lowers it for transport. Each unit is equipped with an output jack for operating either direct-writing or photographic recorders, so that recording as well as monitoring is possible simultaneously. Direct photography of the large screen is also possible.

Further information and an illustrated brochure are available. **Circle P48 inside back cover.**



SMALL THERMOSTAT
is hermetically sealed

GEORGE ULANET CO., 425 Market St., Newark 5, N. J., has available in quantity a hermetically sealed surface-sensing miniature thermostat that meets stringent aircraft and military applications. New design shortens the heat path between the mounting surface and thermal-sensing element thus decreasing the response time over 50 percent.

Units are precalibrated to specified temperature and adjustment screw is sealed. Strain relief construction prevents calibration drift when the unit is subjected to temperature variation between −50 C and +200 C.

Size is $\frac{5}{16}$ in. wide, $\frac{7}{16}$ in. high

NEW

General Plate COPPER CORED Glass Sealing Alloy Wire

Increases Electrical Conductivity — Saves Time — Cuts Cost

Here's a case where two metals are much better than one. Built around a 30% copper clad core, General Plate Glass Sealing Alloy Wires have up to three times more electrical conductivity than solid lead wires of the same size.

This means you can substantially increase the current carrying capacity of your solid sealed leads without going to larger diameters — or, if you have a miniaturization problem, you can reduce sealing wire diameters correspondingly by using General Plate Cored Wire.

General Plate Copper Cored Glass Sealing Wires are being used more and more for better performing glass-to-metal seals in hermetically sealed devices such as switches, relays, coils, controls and vacuum tubes.

General Plate Copper Cored Glass Sealing Wires are now available in #52 alloy, Type 446 Stainless, low carbon steel and other glass sealing alloys. Write for Technical Data Bulletin 706.

For full details on the complete line of General Plate Clad Metals, write today for your free copy of our new PR-700A Catalog.

You can profit by using General Plate Clad Metals

METALS & CONTROLS CORPORATION

General Plate Division

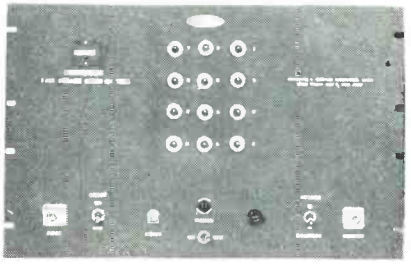
1302 Forest Street
Attleboro, Massachusetts

exclusive of terminals, ¾ in. long. Ratings are: 5 amperes 28 v d-c noninductive load; 5 amperes 115 v a-c. **Circle P49 inside back cover.**

OSCILLOGRAPH TUBE
for pulse-modulated uses

RADIO CORP. OF AMERICA, Harrison, N. J. The 5FP14-A is a 5-in. oscillograph tube featuring high resolution capability and a medium-long persistence characteristic. It is intended particularly for pulse-modulated applications, such as radar indicator service.

Employing magnetic focus and magnetic deflection, the tube is designed with a high-resolution gun capable of providing a line whose width will not exceed 0.010 in. measured with ultor current of 200 μa, ultor voltage of 4,000 v. and 49-line shrinking raster. The 5FP14-A has a deflection angle of 53 deg and a minimum useful screen diameter of 4½ in. **Circle P50 inside back cover.**

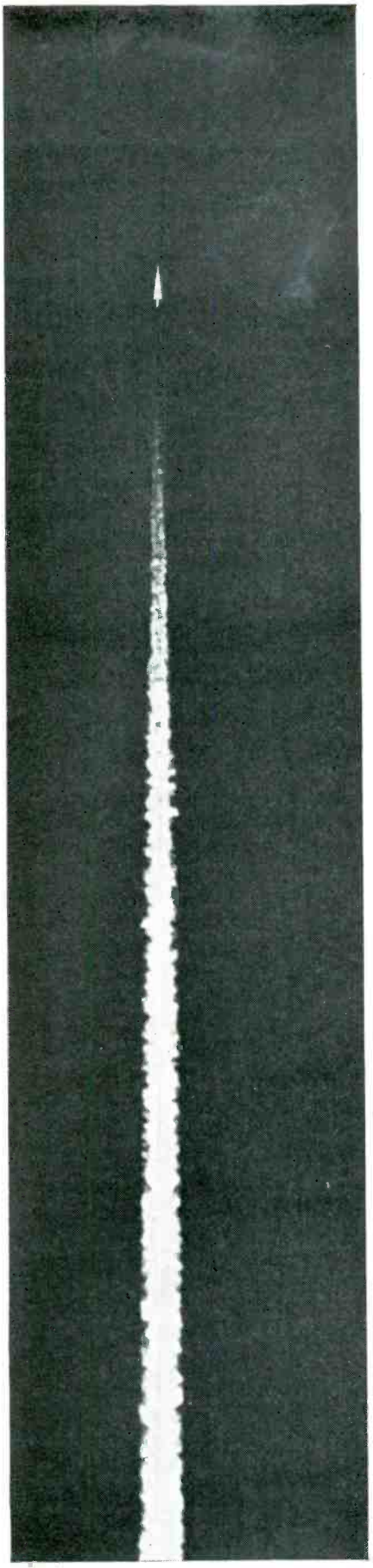


DECADE SCALER
with long term reliability

ELECTRICAL AND PHYSICAL INSTRUMENT CORP., 42-19 27th St., Long Island City 1, N. Y. The model

Engineers wanted for this assignment:

TAKE MAN HIGHER...FASTER ...THAN EVER BEFORE



The men who create tomorrow's hypersonic, high flying aircraft will have to engineer them to withstand the weird phenomena of the stratosphere. Here in deep blue space, violent 200-mile-per-hour winds fight each other. Fantastic air temperatures and aerodynamic heating become incredible, contradictory forces.

The airplane of the future will have to overcome *all* the problems of this eccentric environment, and do one more thing —house and protect a human pilot.

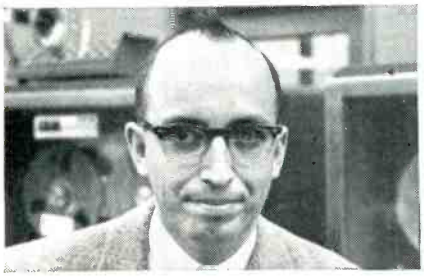
At two times the speed of sound the lowest temperature anywhere on the airplane is 250°—hot enough to rob aluminum alloy of 20% of its strength. At Mach 3 temperatures zoom to a blood-boiling 650°. And yet thermodynamics is just one package of problems confronting today's aircraft engineer. There are many more to be unwrapped before this space-age accomplishment is real.

The aeronautical researcher has, however, an outline picture of his airplane of the future. He knows that its configuration will be designed to reduce friction ... its wing will be razor-thin ... the nose needle-sharp to avoid detached shock waves. He also knows that his brainchild will have to prove itself high above the atmosphere!

One day soon this missile-like airplane will take man where he's never been before ... to the very frontier of space.

If you accept this challenge we promise you a management climate that stimulates personal growth and rewards initiative. Engineers have constantly guided the long-range technological advancement of North American where research and development on the X-15—a manned aircraft for the investigation of speeds and temperatures at very high altitudes—is now in progress.

Write today for full particulars to: Mr. T. J. Wescombe, Engineering Personnel Manager, Dept. 2EL, North American Aviation, Inc., Los Angeles 45, California.



CHUCK PRICE earned a BS in 1944, MS in 1947, and a PHD in Mathematics in 1950—all from the University of Chicago. In 1953 he joined North American's Advanced Design Department. Since then he has earned three promotions and is now a Group Leader supervising 36 engineers working on new aircraft design. His Group's objective—to select the aircraft configuration best suited to perform a specific mission.

MIT graduate **HAROLD RAIKLEN** received his BS in Mechanical Engineering in 1947—his MS two years later. His first North American assignment was to analyze and test dynamic stability and response of powered flight controls. Today, less than four years after joining the Company, Hal heads a section devoted to design and study of mechanized components, including flight control systems—his third supervisory position.

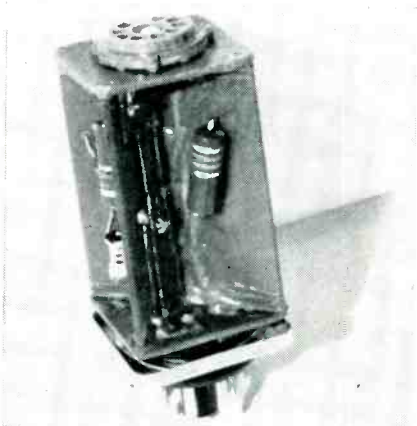
NORTH AMERICAN AVIATION, INC.

NORTH AMERICAN HAS BUILT MORE AIRPLANES THAN ANY OTHER COMPANY IN THE WORLD

414 fast decade scale of 1,000 has been designed to allow accurate high speed counting with a long term reliability previously approached only in much slower equipment. The gated decade system does not use feedback and makes possible a decade with a large bias range and an inherent reliability approaching that of a binary. Diode input coupling to each flip-flop in the 10-mc and 1-mc sections and at the input of the slower decades further enhance reliability.

A high capacity forced air blower system keeps operating temperature and moisture content low.

A five-digit electrical register which resets automatically with the scaling stages follows a scale of 1,000 which can be increased on special order up to a scale of 1,000,000. Pulse resolution is 0.1 μsec and continuous counting rates to 10 million per sec can be provided. **Circle P51 inside back cover.**



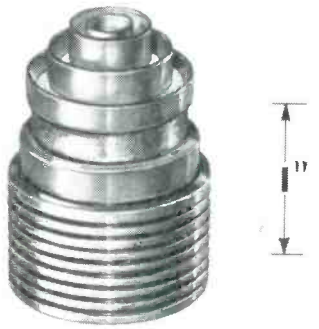
PLUG-IN MODULE
uses printed circuits

ARTHUR ANSLEY MFG. CO., New Hope, Pa., has announced a new modular construction using standard printed-circuit materials and techniques with standard components. Called the Plus module, it features compactness, rugged mechanical construction, great flexibility of design and easy accessibility of the components for servicing.

A standard size is offered, approximately 1⅜ in. sq and 2½ in. high, either with an octal plug-in

base which makes the unit directly interchangeable with many hand-wired modules, or with a new type of plug known as the Plug base that provides up to 32 contacts. A 7 or 9-pin tube socket is incorporated in the top of the unit or it can be adapted to transistors or subminiature tubes. Other sizes and shapes can be made, supporting two or more tubes.

The company offers engineering help in converting circuits to the new construction and is prepared to furnish the complete modules assembled and dip soldered. A standard laboratory unit is also available with a printed-circuit grid which permits engineers to experiment with the new module in their own applications. **Circle P52 inside back cover.**



RCA - 6816

BEAM POWER TUBES
with ceramic-metal seals

RADIO CORP. OF AMERICA, Harrison, N. J., has developed two new extremely small transmitting-type uhf beam-power tubes (types 6816 and 6884) weighing only 2 oz each, with a diameter of 1¼ in. and a length of 1⅞ in. The tubes were developed for oscillator, multiplier and amplifier applications in communications equipment where light weight and physical compactness are important. They have a continuous-wave useful power output of 80 w at 400 mc and 40 w at 1,200 mc.

Through the use of one-piece construction which combines each electrode, its support and its external contact surface, all welding of tube elements to their individual supports and internal leads

is eliminated. This provides low-inductance, high-conductivity paths to the electrodes themselves. The coaxial-electrode structure with its ring-type ceramic-metal seals having graduated diameters, facilitates use of these tubes in circuits of the coaxial-cylinder cavity type. The 6816 has a 6.3-v, 2.1-ampere heater; the 6884, a 26.5-v, 0.52-ampere heater. **Circle P53 inside back cover.**

D-C POWER SUPPLY
is mag-amp regulated

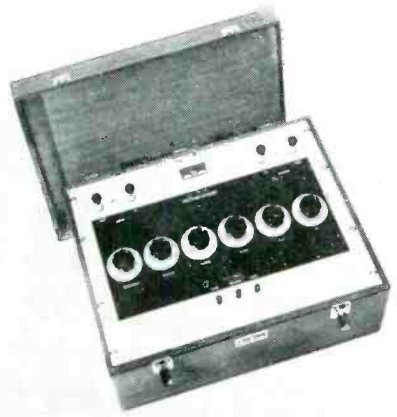
ARNOUX CORP., 11924 W. Washington Blvd., Los Angeles 66, Calif. Designed to supply regulated, d-c voltage for powering airborne electronic equipment from 115 v, 400 cps, single-phase source, this new line of packaged power supplies operates reliably under aircraft and missile environments.

Regulation, provided entirely through magnetic amplifiers, is 0.10 percent; ripple, 0.05 percent. Units meet MIL E-5272A and 1-6181B specs and are potted in hermetically sealed drawn-steel cans. AN connectors or solder headers are available. Mounting is through studs projecting from base.

Standard sizes are 100 to 600 v d-c, up to 1,000 ma. **Circle P54 inside back cover.**

VOLTAGE DIVIDER
accurate to 0.0001 percent

JULIE RESEARCH LABORATORIES INC., 556 W. 168th St., New York 32, N. Y. The VDR-106 is a six-decade Kelvin-Varley type voltage divider. It provides an output volt-



age which is a precisely settable fraction of applied voltage. Six panel-mounted dials permit the voltage division ratio to be set to any discrete value between 0.000000 and 1.000000 with an accuracy and resolution of 0.000001. The effective resolution may be conveniently increased by a factor of 10 by interpolation with the null detecting device.

The device also features switch-operated fixed oil-immersed resistors in all decades, eliminating the conventional interpolating potentiometer. Thus no accuracy determining component is subject to mechanical wear.

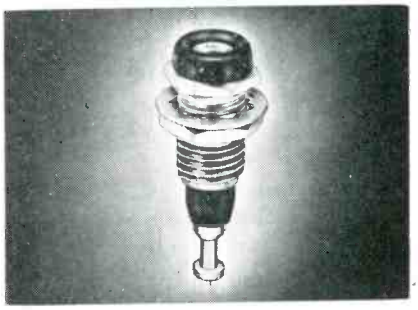
Input impedance is 100,000 ohms permitting input voltages of up to 300 v. Case dimensions are 20 by 15 by 9¼ in. with an inner metal case suitable for relay rack mounting. **Circle P55 inside back cover.**

V-T MILLIVOLTMETER
for field measurements

FISHER RESEARCH LABORATORY, INC., 1961 University Ave., Palo Alto, Calif. Direct, accurate, in-the-field measurements of small potentials are easily and quickly made with this new battery operated v-t millivoltmeter. Essentially infinite input resistance, 10 megohms, on all ranges provides minimum disturbance to the cir-

minimum disturbance to the circuit under test. Six full-scale ranges between 0-25 and 0-1,000 mv and two additional ranges, 0-10 and 0-100 v, are provided. Scale divisions are divided on the 0-25 mv scale so that measurements to 50 μv are possible. The instrument is available in both d-c and a-c models.

An entirely new circuit provides a stable, reliable and all-electronic method of obtaining measurements. Instrument accuracy, ± 1.5 percent on all ranges, is completely independent of tube and battery variations due to a unique amplifier design providing infinite gain in the amplifier circuit combined with 100-percent negative feedback. Size is 5 by 8 by 4 in. Weight is 5 lb complete with leather carrying case. **Circle P56 inside back cover.**



TEST JACK
designed for long life

RAYTHEON MFG. CO., 100 River St., Waltham 54, Mass., has announced a new standard test jack, developed for use in both military and commercial applications. Designed for long electrical and mechanical life, it meets all requirements of MIL-STD-242 (Ships). It features a beryllium copper-spring pin contact which insures consistently smooth insertion and withdrawal of standard 0.080-in. diameter test prods. A nickel-plated brass mounting bushing provides secure mounting under extreme conditions of shock and vibration. The mounting bushing is insulated from the contact assembly by a full-length nylon sleeve.

The entire contact assembly is silver plated with gold wash, providing extremely low contact resistance with the test prod and facilitating fast, strong solder

connections at the solder terminal. The nylon insulator is available in nine brilliant colors for convenient visual circuit identification. Mounting hardware consists of a nickel-plated brass nut and phosphor-bronze lock washer. **Circle P57 inside back cover.**

TEST ROOMS
walk-in environmental type

HUDSON BAY CO., Div. of Labline, Inc., 3070 W. Grand Ave., Chicago 22, Ill., has available a complete line of walk-in environmental test rooms, ranging in size from 4 by 4 by 7 ft high to 4 by 8 by 7 ft high, or other sizes to suit specific needs.

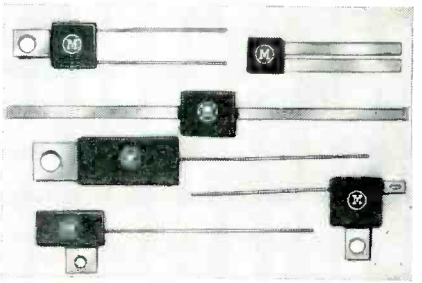
Units are all self-contained, complete with refrigeration, humidity and temperature controls. Temperature ranges from 30 to 200 F and relative humidity, 20 to 95 percent. Interiors are made of heavy gage aluminum. Heliarc welded.

All rooms are double-wall construction, with vapor-sealed fibre glass insulation. Doors have triple seal door gaskets, with multiple panel Thermo-Pane windows.

Interiors can be equipped with aluminum shelving for either work space or storage of samples. **Circle P58 inside back cover.**

CERAMIC CAPACITORS
versatile lead arrangements

MUCON CORP., 9 St. Francis St., Newark 5, N. J., has available subminiature ceramic capacitors



with a great variety of lead arrangements of wire, ribbon or tab leads to fit a wide range of terminal requirements. For extremely tight space applications where high capacitance is required, connecting leads may be ordered of any desired number or thickness, radially or axially arranged, or in any other configuration to provide the most efficient assembly operation. Lower inductance for uhf is obtained with ribbon leads.

The shapes of the ceramic elements vary from square to rectangular with thickness as little as 0.065 in. if needed. Where larger values of capacitance are required in the same area, two or more plates are stacked and connected in parallel.

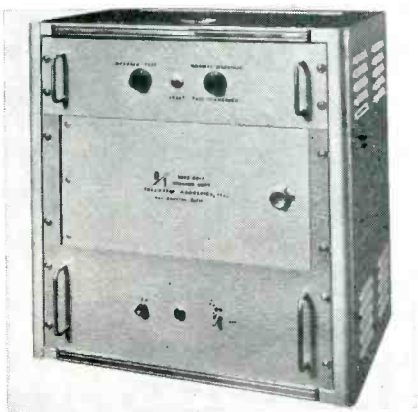
Wide application of these capacitors are in the fields of transistor circuitry, guided missiles, computers, radio and tv, filters, radar and uhf. Bulletin F2 is available. **Circle P59 inside back cover.**

VACUUM RELAY
has three h-v terminals

JENNINGS RADIO MFG. CORP., P. O. Box 1278, San Jose, Calif. The type RE4 spdt vacuum transfer relay has three h-v terminals that are equally spaced on a 2⅜-in. diameter glass bulb giving the longest possible flashover path in a relay this size. Its operating

voltage rating is 25 kv peak and for high altitude operation at this voltage it is provided with a flange that can be soldered to the side of an oil filled or pressurized container. When used in this manner its 26.5 v d-c, 5-w actuating coil can still be removed from below the flange mount.

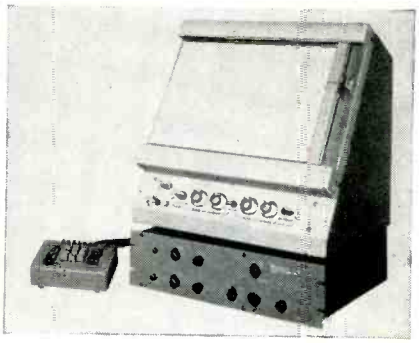
The vacuum dielectric and high temperature processing of this relay insures clean contacts that stay clean, eliminates contact sticking or welding and makes possible small contact actuating mechanisms that resist vibration and shock forces. These features make it especially well suited for antenna switching, d-c pulse switching and straight d-c switching in airborne equipment. **Circle P60 inside back cover.**



STORAGE UNIT
has 1092 character capacity

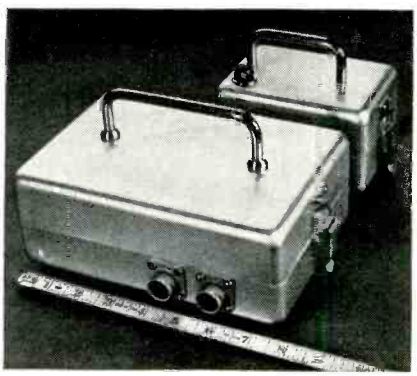
TELEMETER MAGNETICS, INC., 2245 Pontius Ave., Los Angeles 64, Calif. The 1092-BU-7 coincident-current magnetic core storage unit has unique properties which make it ideal for application as a temporary store, buffer or delay unit in data-processing, computing and automation systems. It has a capacity of up to 1,092 characters, each of which may be up to 7 binary digits in length. The seven bits of each character are loaded and unloaded from the memory in parallel. The characters are introduced into the store sequentially and are immediately available at the output in the same sequence as the loading sequence. Minimum time for loading or unloading operation is 14 μsec per character with 6 μsec

being required to switch from a loading to an unloading operation or vice versa. **Circle P61 inside back cover.**



KEYBOARD
for X-Y recorders

ELECTRO INSTRUMENTS, INC., 3794 Rosecrans, San Diego 10, Calif., now offers a keyboard accessory for its 11 in. by 17 in. X-Y recorders. Model 175 consists of a 10-key keyboard (6 in. by 6 in.) and a rack-mounted program and memory unit (5¼ in. by 19 in.). The keyboard uses the touch system and can be operated by either left or right-hand operators. Six digits are entered serially, with a point or symbol plotting automatically on the sixth digit entry. Indicator lights show the number of digits entered. A "minus" sign, "clear keyboard" and "hold X hold Y" controls are added. No plot or plus operations are required. **Circle P62 inside back cover.**



LIQUID-LEVEL DETECTOR
completely transistorized

SOUTHERN ENGINEERING, 5874 Dayton Blvd., Chattanooga 5, Tenn., has available compact, completely transistorized, high reliability, single and multichannel conductivity-type liquid-level detectors. Detection accuracy is better than 0.02 in.

An excitation frequency of 1 kc assures high-speed operation. The controlling current through the liquid is only a few microamperes. Explosion-proof, portable and conduit-box packaging, together with operation from 28 v d-c, 117 a-c or self-contained batteries, are standard. Signal output is by relay operation.

Germanium transistors are employed for normal environmental conditions and silicon units for high ambient temperatures. **Circle P63 inside back cover.**

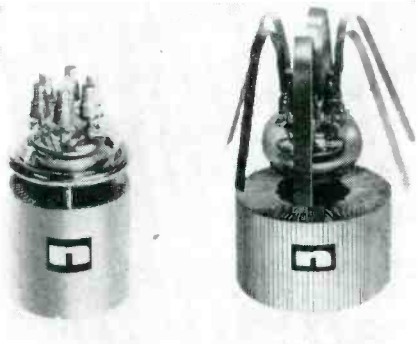
VIBRATOR CHECKER
an inexpensive unit

ELECTRONIC MEASUREMENTS CORP., 280 Lafayette St., New York, N. Y. Model 906 vibrator checker is a ruggedly constructed instrument that checks both 6-v and 12-v vibrators reading condition on a BAD-GOOD scale. It checks both interrupter and self-rectifier type for proper starting point as well as quality of operation and can be used with any battery eliminator such as the model 905.

Model 906 is available at $28.90 wired and tested and $15.50 in kit form. **Circle P64 inside back cover.**

POWER TUBES
three-electrode types

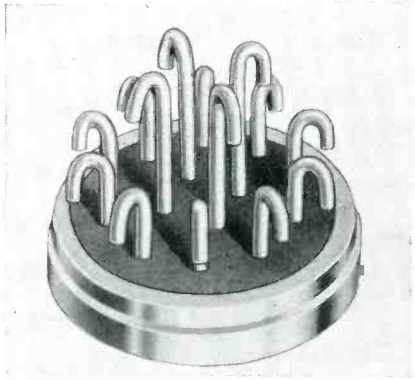
CENTRAL ELECTRONIC MANUFACTURERS, INC., Denville, N. J. Tube types 5680 and 6366 are general purpose, three-electrode power tubes specially designed for industrial and communication appli-



TYPE 5680 TYPE 6366

cations. Each type features a sturdily supported, double spiral thoriated tungsten filament for long life. Greater protection against mechanical stress and thermal shock is insured by ruggedly fabricated Kovar grid and filament seals. The flexible leads of the 6366 are constructed of OFHC copper which can be tailored to individual requirements. Full input ratings apply to 30 mc, reduced ratings to 50 mc.

Partial specifications for the type 5680 include: anode dissipation, 2,500 w; plate input, 12,000 w. Type 6366 has a high-efficiency low-pressure-drop radiator, an anode dissipation of 3,000 w and plate input of 7,000 w. **Circle P65 inside back cover.**



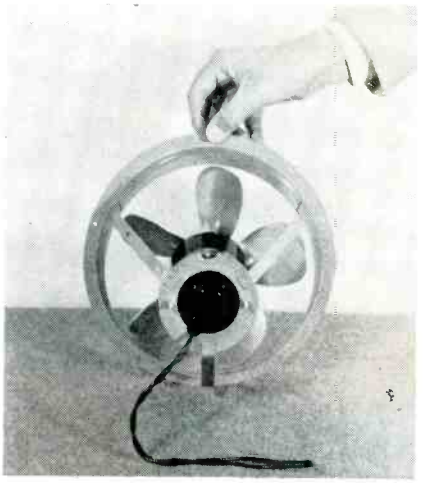
TERMINALS
resist vibration and shock

FUSITE CORP., 6000 Fernview Ave., Cincinnati 13, Ohio, has announced a new line of glass-to-steel terminals for application in electronics. Based on the company's new formula V-24 glass, the new headers are made with solid glass interfusion between glass and electrodes plus controlled compression. They offer greater resistance to vibration and mechanical and

heat shock. There will be less rejects due to in-plant handling.

Four different base designs are available in the new line. One to 21 electrode pins may be mounted in each base depending on size and type. There are six different electrode pin styles. Altogether, there are 88 types with 37 different pin layouts in three series.

Insulation resistance of 100,000 megohms and hot tin dipped finish are standard features of these terminals. Volts rms range from 1,400 to 2,500. **Circle P66 inside back cover.**



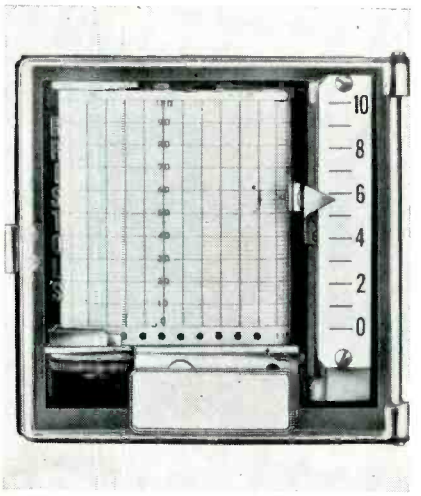
COOLING FAN
for electronic cabinets

McLEAN ENGINEERING LABORATORies, P. O. Box 228, Princeton, N. J., announces production of a new fan suitable for a variety of electronic cooling applications. Model 1E80 features air deliveries of 330 or 395 cfm at zero pressure. Dimensions are 8 in. fan diameter and 10½ in. o-d. Motors are available totally enclosed or open and operate on 15 v, 60 cps at 1,500 rpm.

This fan may be used in any position and is available in other sizes and modifications with air flow push or pull over motor. Further information is available. **Circle P67 inside back cover.**

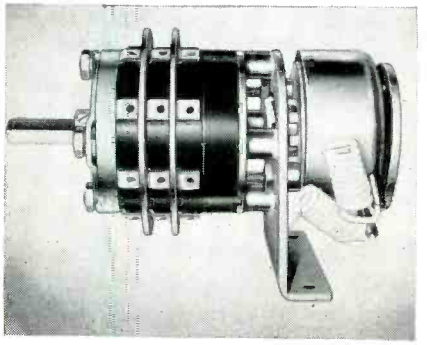
ELECTRONIC RECORDER
housed in a 5-in. sq case

THE BRISTOL CO., Waterbury 20, Conn., has announced a new self-balancing electronic potentiometer which gives a continuous record on a 3-in. strip-chart.



The small-size self-balancing instruments are furnished in indicating models also. The indicating and recording chassis are both built for full plug-in service and can be interchanged with each other in a matter of seconds. Offered in either potentiometer or a-c bridge models, the new instruments can be used to measure and indicate or record any variable which can be converted into an electrical quantity, such as temperature, pressure, flow, speed, pH, smoke density or resistance.

With these new electronic recorders and indicators, a complete process can be monitored with miniature instruments, making possible a complete graphic panel or console-type operation, where desired. Additional information is available in bulletin P1271. **Circle P68 inside back cover.**

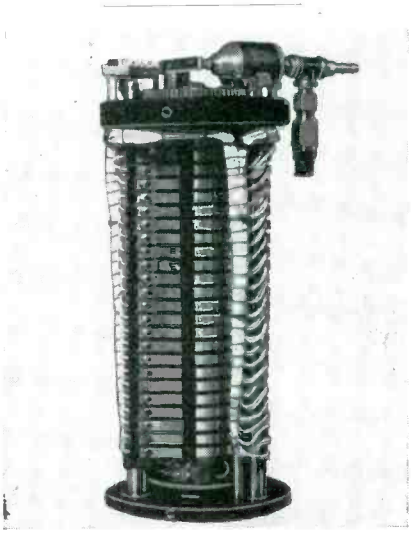


ROTARY SWITCHES
are solenoid-operated

ELECTRO SWITCH CORP., 167 King Ave., Weymouth 88, Mass. Heavy-duty switches assembled with solenoid rotating devices that

drive the switch through the cycle of contact positions, provide remote automatic or semiautomatic control of a series of complex circuits. The indexing stroke of the solenoid device is matched to the degree of rotation between contact positions of the switch and drives the rotor one position each time the solenoid circuit is closed. This circuit may be closed by pushbutton or by simple mechanical motion of the governed machine, providing the control needed for automation.

Solenoid-operated switches are custom-built by the company to customer's specifications. **Circle P69 inside back cover.**



SLIP RING ASSEMBLY
a versatile system

ELECTRO-MINIATURES CORP., 1060 Elm Ave., Ridgefield, N. J., has announced a new type of slip ring assembly. The new construction provides continuously variable remote control of brush pressure by means of a miniature air cylinder built into the brush housing assembly.

Among the many advantages of this versatile system are: (1) Positive, continuous compensation to permit minimum wear on both brush and ring surfaces to attain minimum noise levels. (2) Adaptability to applications requiring either high or low brush pressure. (3) Extended life at all speeds.

This variable brush pressure can be incorporated into strain gage and thermocouple slip ring assemblies, power slip ring units

and a broad variety of other applications. **Circle P70 inside back cover.**

FILTER
for r-f noise suppression

ASTRON CORP., 255 Grant Ave., East Newark, N. J., has designed and manufactured a miniature r-f noise suppression filter for the industry. Model AE1047 is protected from environmental conditions, hermetically sealed and unaffected by elevated operating temperatures or extreme shock and vibration. The eight-section filter contains 11 capacitor sections, 11 toroids and two resistors.

The lightweight filters can be custom designed without shape limitations for use in missile, portable, or airborne applications and surpass government specifications. Technical data are available on request. **Circle P71 inside back cover.**

JACK PANEL
with indirect lighting

HOLLAND ELECTRONICS, 2133 Central Drive South, East Meadow, L. I., N. Y., has developed an illuminated jack panel for use in darkened areas such as tv and radar control rooms.

Circuit designations are legible in total darkness and may be printed on any translucent material such as tracing paper. Illumination is provided by standard miniature lamps and may be regulated by a simple rheostat. The space which may be utilized for designations is almost double that of previously available panels, allowing up to 3 lines of large easily read type.

Either Western Electric or A.D.C. jacks may be used and spacing is suitable for single or double-plug patch cords. Standard relay rack mounting is provided. **Circle P72 inside back cover.**

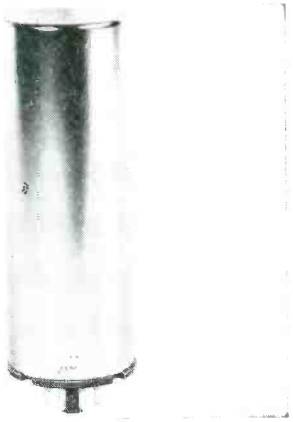
JUNCTION TRANSISTOR
used in computer switching

RADIO CORP. OF AMERICA, Somerville, N. J., has developed a junction transistor of the germanium *pnp* type designed especially for use in switching circuits of electronic computers. The 2N269 has a maximum emitter current and collector current of 100 ma, a minimum large-signal d-c current transfer ratio of 35 at a collector-to-emitter voltage of only −0.15 v, and a minimum alpha cutoff frequency of 4 mc.

The transistor discussed is hermetically sealed, utilizes an insulated metal envelope and has flexible leads which may be soldered or welded into associated circuits. It measures 0.24 in. in diameter and 0.405 in. in body height. **Circle P73 inside back cover.**

CRYSTAL OVEN
weighs only 4.6 oz

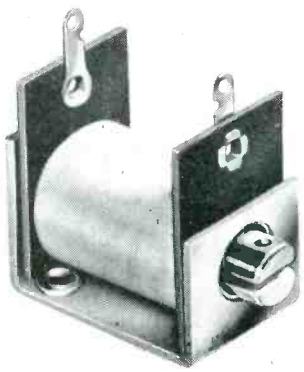
JAMES KNIGHT CO., Sandwich, Ill. The JKO-12 crystal oven is relatively small, weighing only 4.6 oz, yet is capable of meeting a spec-



ification of less than ±1-C temperature variation over a temperature range of −55 C to +75 C. Other features include a quick detachable cover, new high temperature heater bonding tape, bifilar low-inductance heater winding and radio interference filter.

The oven houses one G-9 crystal or HC-15U holder, plugs into an octal base and is available in a choice of heater voltages from 6.3 v to 115 v, a-c or d-c. Its warmup time is 15 minutes at −55 C. Maximum power consumption is 40 w.

The JKO-12 is supplied in heights to a maximum of 4½ in. **Circle P74 inside back cover.**



SOLENOID

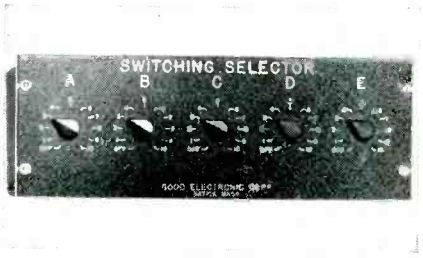
small, light, low-cost unit

ARTISAN ELECTRONICS CORP., Morristown, N. J. Designed for both continuous and intermittent duty in industrial and commercial use, model DS solenoid is suitable or a-c and d-c applications in automatic machines requiring a moderate amount of power.

The coil of the new model is varnish impregnated to protect it under conditions of high humidity. A smooth brass tube provides low

friction characteristics; all ferrous parts are cadmium plated to prevent corrosion. The plunger stop is constructed of Armco iron to prevent the plunger from sticking.

The new solenoid has a maximum stroke of $\frac{3}{8}$ in. and is available in three mounting styles for operating from 3 to 115 v. It is also available for operation under high temperature conditions. **Circle P75 inside back cover.**



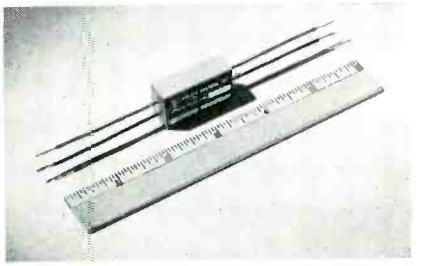
SELECTOR SWITCH
a fifty-channel unit

GOOD ELECTRONIC CORP., P. O. Box 406, Natick, Mass. A new 50-channel selector switch is mainly designed for strain gages, thermocouples, transducers, accelerometers and multichannel testing. The change in contact resistance of any switch point does not exceed 0.48 milliohm and averages 0.08 milliohm.

Alphlex insulation is used throughout. The unit is suitable for bench use or standard 19 in. relay rack. Low loss switching is assured. **Cricle P76 inside back cover.**

CHOPPER
operates to 125 C

AIRPAX PRODUCTS CO., Middle River, Baltimore 20, Md. Type 310 chopper is rated for operation at 400 cps. Contacts handle up to 2 ma at 100 v. Phase angle lies between 50 and 80 electrical degrees lagging from −20 C to +100 C, between 50 and 88 electrical degrees from −65 C to −20 C, and between 45 and 80 electrical degrees from +100 C to +125 C. Drive coil is rated for 6.3 v rms. Units are permanently adjusted at the factory and hermetically sealed to assure uniform operation in any atmosphere at any barometric pressure. **Circle P77 inside back cover.**



CRYSTAL FILTER
occupies ½ cu. in. in volume

HYCON EASTERN, INC., 75 Cambridge Parkway, Cambridge 42, Mass. A miniature crystal filter, weighing approximately one oz, can be used for single conversions from uhf or vhf in a-m or f-m receivers. Center frequency is 20 mc. Bandwidth at six db attenuation is 50 kc. Insertion loss is three db maximum. Technical bulletins are available. **Circle P78 inside back cover.**

LOAD ISOLATOR
covers from 12.4 to 18.0 kmc

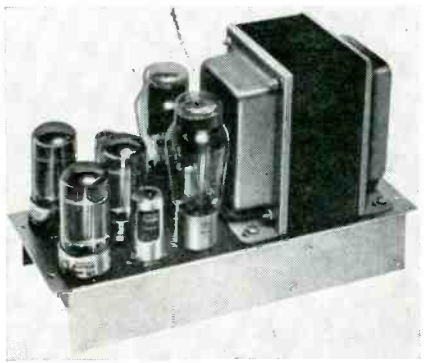
CASCADE RESEARCH CORP., 53 Victory Lane, Los Gatos, Calif., introduces another broad-band Uniline load isolator, the model KU-143. It covers a frequency range of 12.4 to 18.0 kmc, over which vswr is less than 1.10, insertion loss 0.5 db.

Load isolation is 20 db at band center, 13 db at band edges. Power rating is 100 w average, 100 kw peak. Waveguide is RG91/U (0.702 in. by 0.391 in.). Flanges are UG419/U. **Circle P79 inside back cover.**

MAGNETIC AMPLIFIER
potted in epoxy resin

FEEDBACK CONTROLS, INC., 899 Main St., Waltham 54, Mass., has introduced the Blue-Line premium magnetic amplifiers. Magnetic output stage model D-4 delivers 4 w, half-wave, 400 cps to Bu Ord MK14 servomotor or equivalent. Chief features are precision matched cores, heavy Formvar magnet wire and silicon diodes

coupled with component selection and in-process quality control. Model D-4 has control windings for both transistor and v-t preamplifiers. Complete specifications are available. **Circle P80 inside back cover.**



D-C POWER SUPPLY
compact and adjustable

DRESSEN-BARNES CORP., 250 N. Vinedo Ave., Pasadena, Calif., announces a regulated sub-chassis-mounted d-c power supply which is adjustable. Output of the unit, 500 v d-c at 300 ma maximum, may be adjusted to provide any voltage between 300 and 500 v d-c by minor internal changes. The unit also supplies 6.3 v a-c filament voltage at 6 amperes maximum.

Regulation for a line voltage of 105 to 125 v a-c is 0.5-percent change in output voltage; for no-load to full-load, output voltage change is one percent. Ripple is below 10 mv rms for any voltage or load within ratings. Model 5-300XA measures 12½ in. long, 5 in. wide, 5⅝ in. above chassis and 2 in. below chassis. Weight is 23 lb. **Circle P81 inside back cover.**

New Literature

Delay Line Lab Report. ESC Corp., 534 Bergen Blvd., Palisades Park, N. J., offers a complete laboratory report with every delay line prototype. The report includes the customer's electrical requirements; a list of the test equipment used, so that test procedures are reproducible; a series of photo-oscillograms indicating input and output pulse shape and output rise time; an evaluation of photographs and conclusions which cover all pertinent electrical characteristics.

The lab report, evidencing the electrical characteristics of a delay line, can be used effectively as a guide for redesigning samples and reevaluating requirements and serves as an additional production check in maintaining delay line quality. **Circle L1 inside back cover.**

Differential Transformers. Minatron Corp., Belle Mead 14, N. J. Two new price and specification sheets have been issued on differential transformers. Present units cover a range of ± 0.003 in. to a new model with a range of ± 3.00 in. They feature infinite resolution, Teflon leads, and epoxy potting.

They are available from stock for 220 F, and to order for 500 F continuous ambient temperature. If request is made on company letterhead, a copy of *Technical Application Notes* will also be included. **Circle L2 inside back cover.**

Time Delay Relays. The A. W. Haydon Co., Waterbury, Conn., has released a new bulletin to supersede pages 1 and 2 of their current catalog. Bulletin AWH TD403 contains details on the function of the three basic time delay relays, along with catalog part numbers for the standard ranges and voltages in a-c, d-c and 400 cps. These timers are now available in improved extruded aluminum dust covers.

The bulletin sheet is clearly blocked out, with readable size type and illustrations including photos of the models, diagram of wiring, principle of operation and overall and mounting dimensions, along with a complete chart of catalog part numbers for the three series. The bulletin is part of the company catalog. **Circle L3 inside back cover.**

Test Equipment. Industrial Instruments, Inc., 89 Commerce Road, Cedar Grove, Essex Co., N. J., has available a new 24-page catalog of test equipment. Catalog No. 21 lists electronic measuring and control equipment for use in the laboratory and on the production line.

Included in the catalog are automatic component testers, cable and arc resistance testers, voltage breakdown testers, capacitance and resistance decades, decade potentiometers, limit and wheatstone bridges, ohmmeters and megohmmeters, switches and test fixtures.

Complete technical specifications, schematic diagrams and photographs of each unit are included along with comprehensive charts and tables. **Circle L4 inside back cover.**

Toroidal Coil Winder. Donald C. Harder Co., 3710 Midway Drive, San Diego 10, Calif. A single-page bulletin covers the model 0-3 subminiature toroidal coil winding machine. The instrument described operates on an application of the basic Harder patents covering the combination of a smooth grooved winding ring in combination with a circumferential retaining coil spring. Illustration and specifications are included. **Circle L5 inside back cover.**

Self-Calculator Disk. Federated Purchaser, Inc., 1021 U.S. Route 22, Mountainside, N. J. Engineers can save time, trouble and often error by using the Fedisc or self-calculator now being offered. Various formulas such as Ohm's law, voltage or current vs decibels, capacitance reactance vs frequency, and inductance reactance vs frequency, are covered in turn by the series. A different Fedisc may

be obtained each month free and without obligation. **Circle L6 inside back cover.**

Products Brochure. Milro Controls Co., Hawthorne Ave., Park Ridge, N. J., has published a brochure illustrating some of the products which it designs, develops and manufactures. The publication covers a d-c power supply, computer power supply, line voltage regulator and instrument amplifiers. **Circle L7 inside back cover.**

Fluxes. Accurate Specialties Co., Inc., 9-01 43rd Ave., Long Island City, N. Y., has available a technical bulletin giving a complete description, application and advantages of No. 910 mild acid flux, No. 310 nonactivated rosin flux and No. 183 activated rosin flux. The information will be of particular interest to those involved in the problems of electronic, electrical, dip and printed circuit soldering. **Circle L8 inside back cover.**

Ultrasonic Soldering Iron. Acoustica Associates, Inc., Glenwood Landing, Long Island, N. Y. How to solder aluminum and other light metals ultrasonically is described in bulletin SOL-109. The bulletin points out how soldering with ultrasonic soldering irons and tinning baths produces strong, noncorrosive bonds, not possible with conventional soldering.

Also revealed in a schematic drawing, is the electronic circuit for the soldering iron and the design features which enable stable nondrifting r-f output at the tip of the soldering iron during operation. **Circle L9 inside back cover.**

Tube Cap Connectors. Alden Products Co., 117 N. Main St., Brockton 64, Mass. A complete guide to tube cap connectors for every type of tube is now available in a new section for the Alden handbook. It contains important new designs and the latest specifications on tube cap connectors for airborne and missile equipment, power supplies and transmitters, color tv and radar equipment, radio and tv sets. Tube cap

connectors are classified by cap size, then grouped by types. **Circle L10 inside back cover.**

Capacitance/Inductance Measurement. Kay Lab, 5725 Kearney Villa Road, San Diego 12, Calif. A single-sheet bulletin illustrates and describes the model 402-B dynamic Micro-Miker for measuring capacitance and inductance under operating conditions. Applications, circuit description, specifications and price are included. **Circle L11 inside back cover.**

Quick Recovery Diodes. Hughes Products, a division of the Hughes Aircraft Co., International Airport Station, Los Angeles 45, Calif. Specifications DS-38 covers a line of quick recovery silicon junction diodes. The diodes described are high-speed, high-voltage, high-temperature devices which can replace vacuum and germanium diodes in most high frequency or fast switching circuits. They are applicable to computer and pulse circuitry design. **Circle L12 inside back cover.**

Ceramic Capacitors. Centralab, a division of Globe-Union Inc., 900 E. Keefe Ave., Milwaukee 1, Wisc. An eight-page technical bulletin gives basic data on ceramic capacitors. Included are background material, illustrations, advantages and characteristics, and specifications for various types. Data to furnish on inquiries are also given. **Circle L13 inside back cover.**

Antenna-Pattern Transmitter. Color Television Inc., 1445 Old County Road, Belmont, Calif. Illustrated and described in a new leaflet is the model 119 X-band antenna-pattern transmitter, a convenient r-f source designed for antenna-pattern measurements. As illustrated in the literature, the equipment includes a weather-proofed housing for the modulator and a remote control unit which can be located anywhere on the antenna range. Comprehensive specifications are included covering the antenna assembly, the modulator and the re-

mote control unit. **Circle L14 inside back cover.**

Computing System. Remington Rand Univac Div. of Sperry Rand Corp., 1902 W. Minnehaha Ave., St. Paul, Minn., has published a nine-page operational guide to the new Univac scientific 1103A electronic computing system. The letter-size booklet includes a three-page section on the terminology of the system, containing definitions of word length, instruction word, address allocations, control registers, input-output registers, magnetic tape and magnetic drum storage, program sequence control and automatic program interruption.

A keyed block diagram of the system together with general descriptions of the computer's characteristics and mode of operation are also included. Ask for form LSC-56,000. **Circle L15 inside back cover.**

TV Receiving Tubes. Radio Corp. of America, Harrison, N. J. A single-page chart covers 15 new receiving tubes intended for use in tv receivers utilizing 450-ma series-heater strings. The types shown have heaters with the same controlled warmup time to minimize voltage unbalance during starting. In addition these types have heater-cathode voltage ratings sufficiently high to insure dependable performance in series-string circuitry. **Circle L16 inside back cover.**

Slotted Line. Hewlett-Packard Co., 275 Page Mill Road, Palo Alto, Calif. Volume 8 No. 1-2 of the *Journal* contains an article illustrating and describing a micrometric 12 to 40-kmc waveguide slotted line with interchangeable sections and untuned probe. Specifications and prices are given. Also included is an index to Vol. 7 of the *Journal*. **Circle L17 inside back cover.**

Militarized Line Voltage Regulator. General Radio Co., 275 Massachusetts Ave., Cambridge 39, Mass. Volume 31 No. 6 of the *Experimenter* contains an illustrated article on the type 1570-ALS15 militarized line voltage regulator. Included are outstand-

ing features and specifications. Price of the unit discussed is $625. **Circle L18 inside back cover.**

Decade Resistance Units. Muirhead & Co. Ltd., Beckenham, Kent, England. Publication 1742-A illustrates and describes the type D-805 decade resistance units which are arranged for panel mounting and occupy the minimum of mounting space. The units discussed incorporate a new and improved switch which insures extremely low and constant contact resistance and abolishes the need for lubrication of the contact surfaces. Specifications, dimensional drawing and tables of standard models are included. **Circle L19 inside back cover.**

Closed-Circuit Television. Radio Corp. of America, Camden, N. J. A comprehensive, illustrated guidebook to the company's latest broadcast equipment and systems for color and black-and-white closed-circuit tv service in medical, educational, industrial and business fields has been announced.

The 28-page booklet employs color and monochrome photographs, diagrams and sketches to describe the nature and applications of the equipment. Also provided are case-history presentations of typical RCA closed-circuit tv installations. The booklet is available on letterhead request. **Circle L20 inside back cover.**

Magnetic Shielding. Magnetic Shield Division Perfection Mica Co., 20 N. Wacker Drive, Chicago 6, Ill. A new 33-page technical brochure entitled Data Sheets 101 completely describes construction features, performance characteristics and typical applications of nonshock sensitive nonretentive Fernetic and Co-Netic magnetic shielding material. Included are 12 pages of technical data, five pages of performance graphs, 14 pages of illustrations and a handy two-page comprehensive index. **Circle L21 inside back cover.**

ITV Equipment. Graybar Electric Co., Inc., 420 Lexington Ave., New York 17, N. Y. A new 64-page booklet describes a wide selection

of video, audio, lighting, transmission and distribution equipment and accessories. It also contains procedures for the servicing and maintenance of itv equipment, as well as several pages of engineering data permitting approximate layouts and costs of itv systems to be determined. **Circle L22 inside back cover.**

Grid Circuit for Thyratrons. Hanson-Gorrill-Brian, Inc., 85 Hazel St., Glen Cove, N. Y. A technical data sheet illustrates and describes the model 181-1 Thyra-Pulse. The unit discussed can be used in half-wave, full-wave and three-phase circuits, providing one-cycle fast response for critical control applications. Operation is based upon the saturation time of a magnetic core. Complete specifications are given. **Circle L23 inside back cover.**

Thermal Imaging Device. Baird Associates-Atomic Instrument Co., 33 University Road, Cambridge 38, Mass. Bulletin RD515 describes the Evaporograph, a direct thermal imaging device, which can be used for locating and monitoring either hot or cold spots. Applications of the instrument discussed include testing temperatures of electronic components in service, insulation studies and temperature studies of combustion equipment and determinations of cooling efficiency in certain types of electronic assemblies. Schematics, curves and engineering drawings, as well as specifications are included. **Circle L24 inside back cover.**

Ceramic Parts for the Electronics Industry. Electro-Ceramics Inc., 975 East Fifth South Street, Salt Lake City, Utah. A four-page folder covers the high-strength, low electrical loss G-73 Electro-Ceramics Alumina body. Properties, shapes available and advantages are discussed. Applications listed include vacuum tube envelopes, internal vacuum tube parts, metal-to-ceramic hermetic seals, and stand-off, lead-through and other types of insulators. **Circle L25 inside back cover.**

Fixed Composition Resistors. International Resistance Co., 401 N. Broad St., Philadelphia 8, Pa. Catalog data bulletin B-1A covers the type BT fixed composition resistors. The 12-page bulletin contains comprehensive data on construction, characteristics, solderability, heat dissipation, color coding, resistance values and tolerances. New design features and reliability data are shown. Detailed charts and graphs are given. **Circle L26 inside back cover.**

Waveguide and Coax Test Equipment. Admittance-Namco Corp., Farmingdale, L. I., N. Y. Waveguide and coaxial test equipment engineered and produced by the company is shown in an illustrated, 12-page, 2-color catalog just published. Tees, tuners, attenuators, couplers, crystal mixers, crystal mounts, probes, loads and other items are shown, with pertinent specifications. Copies are available on request. **Circle L27 inside back cover.**

Switch Catalog. Haydon Switch Inc., Waterbury, Conn. Catalog No. 5 is a handy permanent switch idea folder. Shown are the Haydon switch standards in hermetically sealed switches. Included are subminiature switches, the standard single blade, double blade and a page of special switches designed for custom applications. Also included are pages of standard and special actuators.

Complete data are given for component and electrical specifications of each switch. Typical schematic drawings are included for each series with engineering data. **Circle L28 inside back cover.**

Impedance Meters. The Narda Corp., 160 Herricks Road, Mineola, L. I., N. Y. Two models of coaxial impedance meters, operating in the frequency range of 1,500 to 12,400 mc and six models of waveguide impedance meters, operating in the frequency range of 2,600 to 18,000 mc are described

in a recent data sheet. Photographs, features, specifications and prices are included. **Circle L29 inside back cover.**

Component Packaging. American Rondo Corp., 100 Sanford St., Hamden 14, Conn. A four-page brochure deals with the modern packaging of electronic components. Process and design of packaging miniature and subminiature tubes, capacitors, diodes, resistors and special tubes are illustrated and described. Advantages of the system are listed. **Circle L30 inside back cover.**

Universal Testing Machines. Tinius Olsen Testing Machine Co., Easton Road, Willow Grove, Pa. A 40-page bulletin describes the complete line of Electromatic universal testing machines. In the machines described, load is applied by an electronically controlled mechanical system to assure positive crosshead speeds under load or no-load. Loads are then weighed and indicated electronically on the large Selectorange dial.

Bulletin No. 54 also covers Olsen compression and XY testing machines, electronic recorders, instrumentation and accessories. **Circle L31 inside back cover.**

Fabricated Metal Products. D. E. Makepeace Co., Pine and Dunham Sts., Attleboro, Mass. A fabricated-metal-products brochure suggesting solutions for a variety of electrical and electronic manufacturing problems has been published. Completely illustrated, it describes products the company is prepared to produce on a custom basis. Included are slip-ring assemblies, microwave assemblies and a variety of contacts. **Circle L32 inside back cover.**

Ultrasonic Fluxless Brazing. Aeroprojects Inc., 310 East Rosedale Ave., West Chester, Pa. A four-page leaflet discusses Sonobraze, the ultrasonic equipment for fluxless brazing and for coating of aluminum. Sonobraze is particularly suited to the joining of unstripped enameled aluminum wire.

Bulletin SBR-6A tells what

Sonobraze is, what is does, how it works and shows its advantages. Sonobraze equipment is also discussed. **Circle L33 inside back cover.**

Precision Instrument Components. PIC Design Corp., Division of Benrus Watch Co., Inc., 477 Atlantic Ave., East Rockaway, L. I., N. Y., announces release of the new catalog No. 11 which lists over 4,000 precision instrument and servo parts available from stock. It includes 128 pages of compact and concise engineering data for use in the electronic and instrumentation fields. **Circle L34 inside back cover.**

Receiving Tube Data. Westinghouse Electric Corp., Electronic Tube Division, Route 17, Elmira, N. Y. A 44-page booklet of essential data on Reliatron receiving tubes is now available. It presents more than 450 Westinghouse receiving tubes. Features incorporated are: large clear tube socket diagrams on the same page as the associated data, bold tube type numbers for quick location and open style data for easy readability. The booklet is priced at 35 cents a copy. **Circle L35 inside back cover.**

Thermal Conductivity Analyzer. The Hays Corp., Michigan City, Ind. A new 12-page color catalog, 56-1008-59, explains principle, construction, operation and features of both the Condu-Therm analyzer and the Acratron electronic recorder. The analyzer discussed can be used for determining amount of CO_2, H_2, He, CH_4 and the like, and employs the thermal conductivity method of analysis. The catalog contains a special section on gas sampling systems and how and why this analyzer is used. **Circle L36 inside back cover.**

Auto-Navigation. Belock Instrument Corp., College Point, N. Y. A four-page folder illustrates and describes the company's dead reckoning analyzer and loran receiver which combine to form an automatic navigation system that will accurately indicate a ship's position anywhere at sea irrespective of atmospheric conditions or

the time of day or night. Specifications are included. **Circle L37 inside back cover.**

Panel Meters. Simpson Electric Co., 5200 West Kinzie St., Chicago 44, Ill. A new six page panel meter bulletin 2057 contains descriptions and specifications along with latest prices of over 800 models. The pages illustrate with photographs of meter styles and various types of meter movements available, also dimensional drawings for meter mounting. Additional information is also provided concerning the company's line of shunts and current transformers. **Circle L38 inside back cover.**

Controls Literature. Servo Corp. of America, 20-20 Jericho Turnpike, New Hyde Park, N. Y. A new periodical "Around the Servo Circuit" is now being issued. New developments in infrared control systems, a question and answer column describing special problems, and reports on new literature available are among items covered in the first issue. The newsletter is designed to keep engineering and other interested personnel informed of the company's latest developments in the control field. **Circle L39 inside back cover.**

Thyratron Pulse Modulator. Dormitzer Electric & Mfg. Co., Inc., 5 Hadley St., Cambridge, Mass., has published a circular illustrating and describing its model 12 laboratory modulator designed specifically for research in the fields of pulse power generation. The unit described has a rated peak power (into 50 ohms load) of 250,000 w. **Circle L40 inside back cover.**

Computer Tubes. Sylvania Electric Products Inc., Emporium, Pa. Three engineering data service bulletins cover types 6211, 6814 and 6888 computer tubes. Included are electrical and mechanical data, direct interelectrode capacitances, ratings and average characteristics. **Circle L41 inside back cover.**

Vacuum Seals. Glasseal Products Co., Inc., 1111 E. Elizabeth Ave.,

Linden, N. J. Manufacturers of electronic components that use glass-to-metal vacuum seals will find the new 12-page color catalog a valuable reference. Featuring the exclusive use of the Duro-Vac process, the catalog shows cross-sectional drawings, charts, descriptions and photographs of multiheaders, feed-throughs, stand-offs seals, AN connectors, transistors and diode terminals. The complete catalog is available to anyone requesting it on his letterhead.

Portable Potentiometer Pyrometer. Technique Associates, 211 E. South St., Indianapolis 25, Ind. A new eight-page bulletin 9B describes the improved Pyrotest, a portable potentiometer pyrometer with interchangeable direct-reading scales. The instrument discussed checks and calibrates all types of thermocouple-actuated temperature instruments and many electrical instruments. Temperatures or millivolts are read directly—without charts, graphs or conversion tables. **Circle L42 inside back cover.**

Wide - Band Oscilloscope. Tektronix, Inc., P. O. Box 831, Portland 7, Ore. An eight-page folder completely describes and illustrates the small, light and versatile type 515 wide-band oscilloscope. Chief features and specifications are shown. Price of the unit discussed is $750. **Circle L43 inside back cover.**

Flat Selenium Rectifiers. Radio Receptor Co., Inc., 240 Wythe Ave., Brooklyn 11, N. Y. Bulletin 237 covers the Siemens flat type selenium rectifiers which feature long life, smaller sizes, higher efficiency, low forward drop and low reverse leakage. Sizes, terminal arrangements and equivalent circuit ratings are shown. **Circle L44 inside back cover.**

System Test Equipment. Link Aviation, Inc., Binghamton, N. Y., has available a 22-page brochure, "Systems Evaluation Test Equipment," LP-3528, which explains the philosophy of system test

equipment for military electronic systems. It presents complete application information and design concepts of specific "go-no-go" testing devices which the company has custom built for use in conjunction with an existing analog bombing system.

The brochure describes typical applications of systems evaluation test equipment for testing complete systems and checking components within a system. It also discusses the economic advantages of this advanced approach to electronic testing. **Circle L45 inside back cover.**

Instrument Eyelets. Circon Component Co., Santa Barbara Municipal Airport, Goleta, Calif. A single sheet bulletin describes a line of instrument eyelets used for terminals, contacts, bushings, fasteners, grommets and printed circuits. Chief features and application data are included. **Circle L46 inside back cover.**

Receiving Tube Manual. Radio Corp. of America, Harrison, N. J. A new edition of the RCA receiving tube manual, revised, expanded and brought up-to-date, has been prepared. Designated RC-18, it contains technical data on more than 575 receiving tubes, including types for black-and-white and color tv and series-string applications. In addition, more than 75 picture tubes, including color types, are treated. Price is 75 cents. **Circle L47 inside back cover.**

D-C Power Supply. Consolidated Electrodynamics Corp., 300 North Sierra Madre Villa, Pasadena, Calif. Bulleting 1570 covers the type 3-131 26-v d-c power supply which increases versatility of airborne oscillographs. Included are an illustrated description, component information and a listing of specifications. **Circle L48 inside back cover.**

Thermostats. Stevens Mfg. Co., Inc., P. O. Annex 1007, Mansfield, Ohio. Bulletin 5000 describes a line of Stemco type C thermostats. Both hermetically sealed and semi-

enclosed types are covered.

Punched for insertion in standard three-ring binders, the bulletin describes operating principles, gives dimensional data, ratings and materials of construction. Available terminal and mounting arrangements are illustrated with photographs. **Circle L49 inside back cover.**

Precision Potentiometers. Helipot Corp., Newport Beach, Calif. Improved operating characteristics of the series B precision potentiometers are included in data sheet 54-18. The significant changes listed include more favorable values for best practical linearity tolerances above 999 ohms. For example, from 1,000 to 9,999 ohms, the best practical linearity tolerance is now ±0.015 percent rather than ±0.025 percent; for 10,000 ohms and above, it is ±0.01 percent. **Circle L50 inside back cover.**

Facilities Brochure. United States Dynamics Corp., 1250 Columbus Ave., Boston 20, Mass., has available an eight-page booklet stating the present position, aims and objectives of USD, a company organized to manufacture electronic components and systems, mechanical and electromechanical devices, and to conduct research and development for commercial and military applications. Also available are a number of silicon power rectifier data sheets covering a variety of types, as well as a price list. **Circle L51 inside back cover.**

Aircraft Hook-Up Wires. Revere Corp. of America, Wallingford, Conn. A series of single conductor, 600-v, high-temperature aircraft hook-up wires, designed to meet applicable requirements of military specification MIL-W-7139, are described in bulletin No. 1906. The wires discussed possess outstanding dielectric characteristics over the continuous temperature operating range from −68 F to +410 F. Available in sizes from 22 to 12 gage, the wires are insulated with Teflon and Teflon-impregnated glass to form a rugged insulation highly resistant to abrasion and corrosion. **Circle L52 inside back cover.**

Plants and People

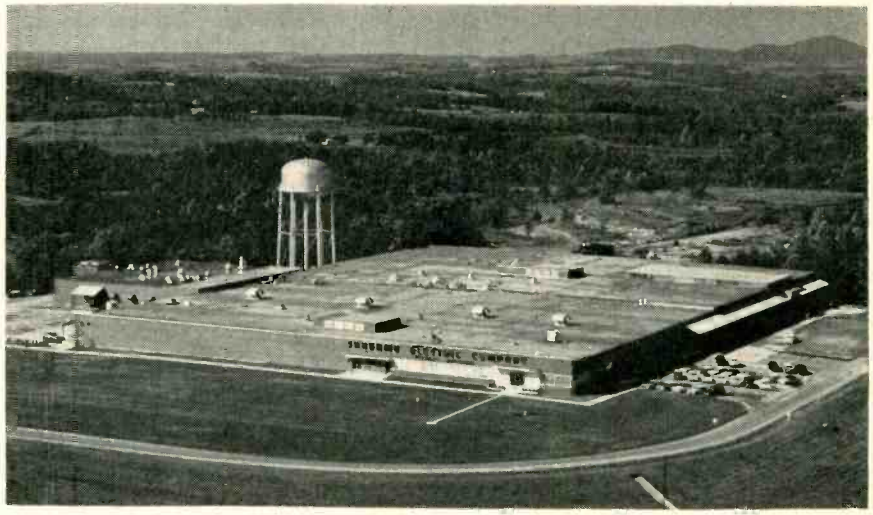
Edited by WILLIAM G. ARNOLD

Electronics manufacturers expand plants and facilities by acquisition, leases or new construction. Top engineers and executives in the industry are promoted and move to new responsibilities. Technical societies honor leading scientists

Sangamo Dedicates Capacitor Plant In South Carolina

THE SANGAMO ELECTRIC COMPANY'S $5 million plant in Pickens, South Carolina is in operation. Some 1,000 persons are employed in the 200,000 sq ft facility.

The company will produce electrolytic capacitors, power capacitors, motor generators, converters, dynamotors, and Navy electronic equipment there. South Carolina's Governor George B. Timmerman, Jr. and Senator Strom Thurmond participated in dedication formalities. C. H. Lanphier, Sangamo president, was the recipient of a bronze plaque commending the firm for its choice of a South Carolina site for the plant.



Sangamo Electric's new capacitor plant in South Carolina

Hoffman Electronics Elects New Laboratory President

JAMES D. MCLEAN, formerly of Philco Corp., was elected president and general manager of Hoffman Laboratories.

McLean resigned as vice-president and general manager of the government and industrial division of the Philco Corp. to head the wholly-owned Hoffman subsidiary. He succeeds John B. Moss who becomes chairman of the executive committee of the Laboratories and remains as a director of Hoffman Electronics Corp. He joined Philco in 1947 after 9 years with GE in engineering and sales.

McLean will have full responsibility for all phases of work carried on by Hoffman for the armed forces in the engineering, design and production of advanced electronics and electromechanical projects. The Laboratories have more than 50 active projects.

He will have supervision of over 400 engineers and 2,200 employees as well as the 12 service areas.

Sylvania Appoints Osgood Manager Of Waltham Laboratories

RICHARD M. OSGOOD has been appointed manager of the Waltham laboratories of Sylvania Electric.

He formerly was manager of the avionics laboratory at the Waltham facility. Before joining Sylvania, he was chief of the electronic defense systems division of the Air Material Command, U. S. Air Force. He succeeds Dr. O. G. Haywood, who has resigned to accept a top executive post with Emerson Electric Manufacturing Co., St. Louis, Mo.

Richard M. Osgood

In his new post, Osgood will have responsibility for the avionics laboratory, the missile systems laboratory, and the applied research laboratory, the three activities constituting the Waltham laboratories.

Osgood joined Sylvania in 1955 as manager of equipment fabrication at the Waltham Laboratories, becoming manager of the avionics laboratory in 1956.

As chief of the electronic defense systems division of the Air Material Command, Osgood held the rank of Colonel. He was responsible for the coordination of the design, production, and installation of a semi-automatic air defense system for the continental United States and for the "DEW Line".

Osgood began his research and development work in military elec-

MISSILES to MACHINERY

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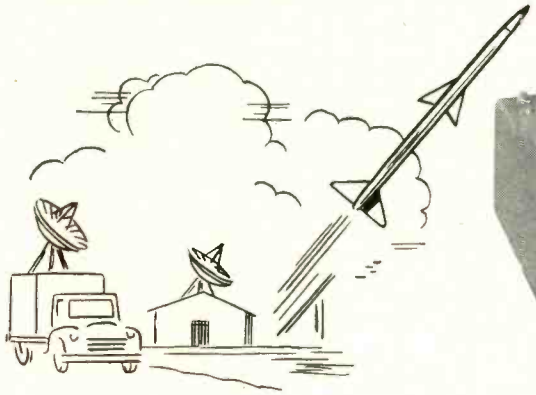
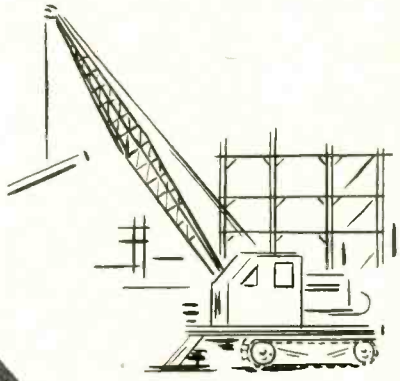
covers the oscillograph recording field





TELEMETRY APPLICATIONS

- QUICK-LOOK monitoring in the telemetry ground station permits continuous observation of missile in-flight programing results.
- ON-THE-SPOT monitoring permits making in-flight function corrections in controlled missiles or piloted aircraft.
- A NATURAL for mobile telemetry vans . . . compact, rugged, low power consumption, record is PERMANENT, no fading or fogging when exposed to direct sunlight.

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- PERMANENT record obtained at test site may be stored indefinitely for purpose of future data reduction.
- PORTABLE — extremely useful for field test applications where a "multiplicity" of data must be collected with the least amount of instrumentation.
- No amplifiers required for many applications.

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ENGINEERS . . .

Check your requirements against these FEATURES!

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- Developed record may be viewed an INSTANT after exposure.
- HIGH CONTRAST photographic qualities . . . black intelligence traces are recorded on light colored background.
- As many as 24 intelligence channels may be recorded on the 8-inch x 200-foot record roll.
- Record is REPRODUCIBLE without loss of contrast by Ozalid, Bruning, etc., processes . . . NO deterioration due to ultra-violet exposure.
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Tel.: 3-3524

tronics for the Air Force following his graduation from the United States Military Academy at West Point in 1941.

Meyer Leifer has been appointed assistant director of the electronic defense laboratory of Sylvania Electric, in California.

Before being named to the newly created post, he was engineering manager of the laboratory. In this assignment he headed the research and development program of the laboratory since it began operations in Mountain View, Calif. in 1953.

Leifer joined Sylvania in 1946 as an engineer in the physics labs.

NATO Electronics Chief Named

JOHN HESSEL, director of the radio communication division at Fort Monmouth since 1947, has been appointed by the State Department as chief of the electronics section, production division, North Atlantic Treaty Organization.

From 1942 to 1946 he served with the Army Signal Corps during which he was awarded the Legion of Merit with Oak Leaf Cluster. He held the rank of Colonel.

He has been employed at the Signal Corps Engineering Laboratories since 1931.

John Hessel

Motorola Opens New Home Radio Plant, Selects Military Head

New Motorola home and automobile radio plant in Illinois

MOTOROLA BEGAN operations in its new $2 million manufacturing facility in Quincy, Ill. The 185,000 sq ft plant was viewed by 7,500 area residents prior to going into the exclusive production of home and automobile radios. Total employment exceeds 1,500, and officials estimate more than 1,000,000 radios of various types will be manufactured in the plant in 1957.

The east wall of the new plant is 500 feet in length and is movable for future expansion. The plant is completely conveyorized and is equipped with automatic and semi-automatic manufacturing devices.

Motorola also announced that Major General Samuel R. Brentnall, U.S.A.F., retired, has been named vice-president and assistant general manager of the military electronics division.

General Brentnall, formerly Air Force assistant chief of staff for guided missiles, will supervise military electronics in Phoenix, Riverside, California and Chicago, and will administer the work of more than 2,500 persons.

Former posts held by Gen. Brentnall include chief, production engineering section, Wright Field, and special assistant to chief of staff for the B-47 program.

Kittel Awarded Buckley Solid State Physics Prize For 1957

AMERICAN PHYSICAL SOCIETY has awarded the $1000 Oliver Buckley Solid State Physics Prize for 1957 to Dr. Charles Kittel, professor of physics at the University of California in Berkeley.

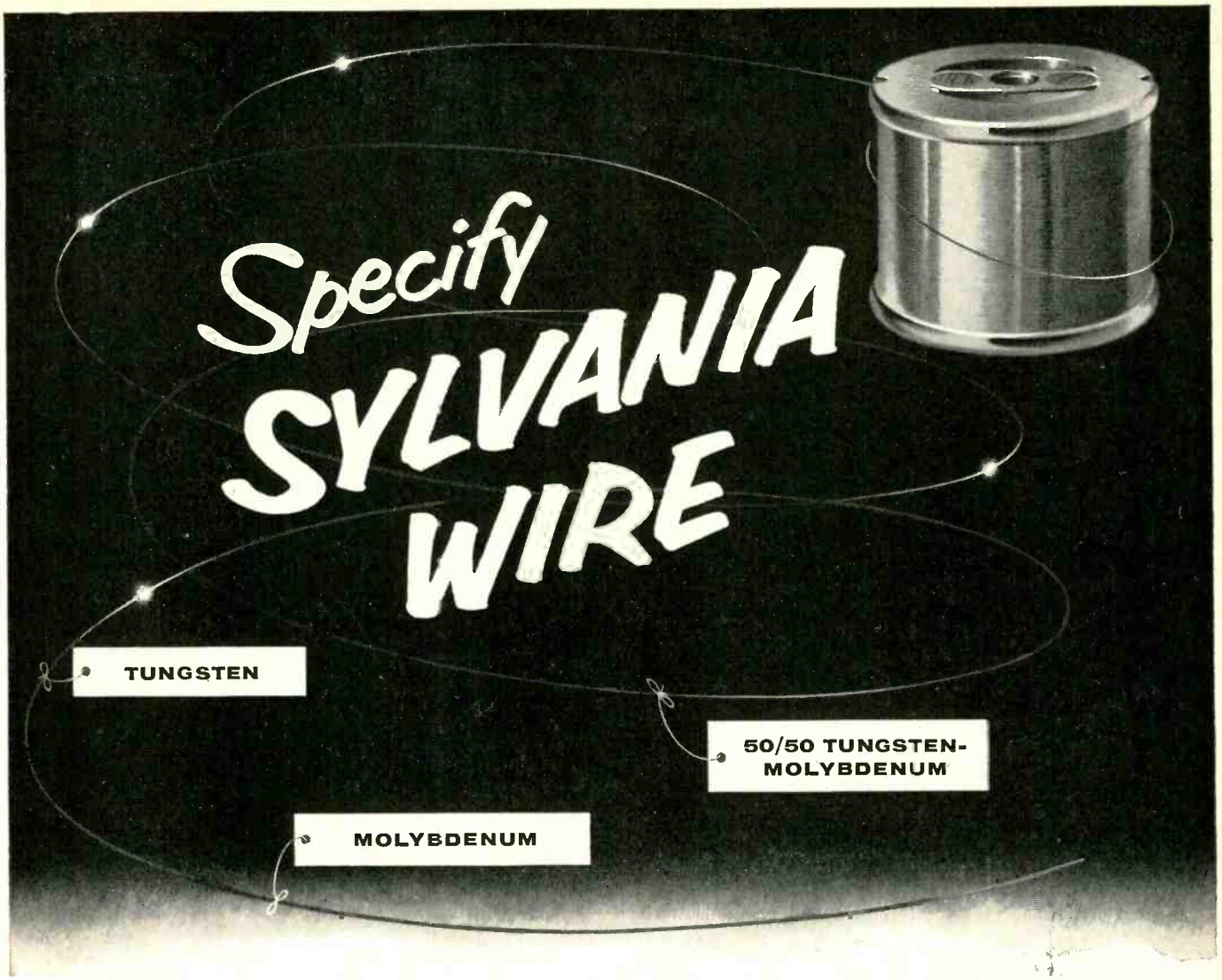
Dr. Kittel was selected for his applications of magnetic resonance methods to investigations of the electronic solids." This work was judged by the Society as "a most important contribution to the advancement in solid state physics" in the last five years.

Dr. Kittel has developed new theoretical techniques for investigating the electronic structure of solids by utilizing the interaction in a magnetic field of high frequency radio waves with the magnetic and electric properties of the electrons in solids.

Related experimental work on a number of these problems has been carried out by Dr. Arthur Kip, professor of physics. Drs. Kittel and Kip developed a "solid state cyclotron"—a tiny crystal—in which they whirl electrons through solid matter.

The Buckley award was established by the Bell Telephone Laboratories in honor of one of its last presidents, and it is administered by the American Physical Society.

The award will be presented to Dr. Kittel at the annual meeting of the Society in New York. At that time Dr. Kittel will deliver the Buckley Lecture, on "The Role of Magnetic Resonance Studies in the Physics of Solids."



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Because of high metal purity plus exceptional uniformity in size and physical properties, Sylvania wire will help you hold rejection losses to a minimum . . . help you maintain consistently higher product performance standards.

Quality-controlled to the exacting standards known to be needed for producing the world's finest vacuum tubes—every step in the wire-making process is done in Sylvania's own plants. From metal refining to drawing and finish plating . . . one manufacturer bears the entire responsibility of supplying the exact kind and quality of wire you need.

There is a Sylvania wire for every vacuum and gas tube application, in a full range of sizes down to the finest available—bare or plated with gold, rhodium, silver or nickel. Extra-long lengths can be supplied on order.

As the specifications for tube characteristics vary—so your wire requirements will vary. Next time you need standard or special wires, call in your Sylvania sales engineer. He will help you get exactly what you need, *when* you need it!

Sylvania Electric Products Inc.
Tungsten and Chemical Division, Towanda, Penn.

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Air Force Inspects Lewyt Factory

General Wray, head of Air Defense Engineering Service, tours Lewyt plant

ALEX LEWYT, president, Jerome L. Strauss and Arnold Wolf, vice-presidents, of the Lewyt Manufacturing Corp., recently were hosts to Brig. General Stanley T. Wray and Colonel O. M. Scott of the Air Force, S. P. Schwartz and Donald Wilkes of Western Electric and C. Shorey of the Cambridge Research Center, at the company's Long Island City plant.

On a tour, they were shown Lewyt's production of the Coordinate Data Transmitter AN/FST-1 and Coordinate Data Monitor OA-947/FST-1—used in SAGE.

Westinghouse Selects Research Head

CLARENCE ZENER has been appointed director of the Westinghouse research laboratories.

He assumes his new post after five years as an associate director and a year as acting director of the 800-member staff of the laboratories, which only recently occupied completely new research facilities in Churchill Borough, ten miles east of downtown Pittsburgh.

Formerly a professor in the Institute of Metals and department of physics at the University of Chicago, Dr. Zener is author of the Zener theory of ferromagnetism which explains why certain materials are strongly magnetic, and of the Zener effect, a theoretical explanation of the electrical breakdown in semiconductors such as germanium and silicon.

Since coming to the Westinghouse research laboratories as an associate director in 1951, Dr. Zener has initiated and helped develop a new approach to metallurgical research. In this approach alloys of metals are "predesigned" with certain "built in" characteristics that depend upon the magnetic structure of the metal atoms. This technique eliminates much of the tedious traditional approach in which different metals are mixed in varying proportions and are then tested for properties.

Vacuum Tube Products Builds New Plant

GROUND has been broken for the new 13,000 sq ft plant of Vacuum Tube Products Co. in Oceanside, Calif.

In 1946, when Harold Ulmer first formed V T P Co., it was located in the garage and basement of his home in Oceanside, Calif. Ulmer had years of experience in the electronic tube business with Raytheon and IT&T.

The company was established in 1946 on an experimental and developmental basis and, until 1955, it

ran as an advisory and research development.

James J. Sutherland formerly of Sylvania, is vice-president and general manager. Vacuum Tube Products employes 40 people, and has a half million dollars in backlog orders for the four classes of products it makes. When the new plant is completed, employment is expected to be about 200.

Radio Club Honors Eastham

Melville Eastham

RECOGNITION for outstanding contributions to the art of precision measurements in the field of radio and electronics was accorded Melville Eastham at the recent annual banquet of the Radio Club of America.

The recipient of the Armstrong Medal was a founder of the Clapp-Eastham organization before the formation of General Radio Co. where he served as chief engineer and also as president.

The citaion indicates in part that Eastham made available reliable test equipment of a standardized nature that previously did not exist or had to be especially assembled as a laboratory setup.

Raytheon Starts Lab, Appoints Manager

A new electronics laboratory at Maynard, Mass. with primary responsibility to design and develop airborne electronics equipment, has been formed by Raytheon Manufacturing Co.

The laboratory will work on such

devices as Doppler navigation instruments, aircraft intercept radars, altimeters, surface radars, and other classified items for the Defense Department.

The laboratory is housed in a 65,000 sq ft area presently leased by Raytheon in the former Assabet Mills textile center in Maynard.

Initially the laboratory will employ about 275 engineering and non-engineering personnel. The expected first year's growth will be about 20 percent, according to the firm.

Named as laboratory manager was Homer C. Knauss, who was promoted from his position as airborne systems branch manager at Raytheon's Wayland Laboratory radar department.

With Raytheon, Knauss has worked on various radar and communications systems. He was primarily responsible for a high-speed bombing radar system now being produced for the Air Force.

Sperry Builds New Plant In Arizona

SPERRY RAND'S Sperry Phoenix Co. began construction of an initial manufacturing facility in Phoenix, Ariz.

An 81,000-sq ft plant unit, which will cost about $3 million to build and equip, is expected to be completed and operating by next August. It will employ approximately 500 persons.

The initial 81,000 sq ft area plant unit will be utilized to manufacture various components of flight and engine controls systems.

The company begins preliminary manufacturing operations in 14,000 sq ft of leased space at the Arizona State Fair Grounds. A limited number of technical specialists, already selected, will be employed there and regular employee recruiting programs will begin later in 1957.

Bendix Acquires Firm, Appoints Two

BENDIX AVIATION plans to acquire the business and assets of the Sheffield Corp. of Dayton, O., a privately owned manufacturer of gauging and measurement instruments, and industrial inspection and quality control systems.

Bendix will issue approximately 230,000 shares of its common stock to acquire Sheffield. The firm will continue to operate under its present management as a wholly owned subsidiary of Bendix.

Annual sales of Sheffield run about $24 million having risen from $1 million sixteen years ago. It has 1,000 employees, and operates plants in eight cities.

Louis Polk will become a director, vice-president and group executive of Bendix and will continue as president of the Sheffield subsidiary.

Donald C. McDonald

▶ **Engineers**—Donald C. McDonald has been appointed to a new position of director of engineering by the Friez Instrument division of Bendix Aviation Corp.

He will be responsible for all engineering phases of divisional activity, ranging from research through production in the fields of weather instrumentation, automation, and electronics.

Previously he was assistant director and chief engineer of Cook Research Laboratories. He also was employed as a division supervisor at the Willow Run Research Center of the University of Michigan in the controls and instrumentation division. In addition, he has served as a project supervisor of the Doelcam Corp., and as senior research engineer at the M.I.T. servomechanisms laboratory.

Charles E. Miller has been ap-

pointed head of engineering services for Bendix Pacific.

He will be in charge of the reliability and standards, production procedures, design drafting and records, publications, environmental facilities, technician control, and instrument service and calibration groups.

GE Promotes Three To New Posts

Irvine D. Daniels

IRVINE D. DANIELS has been appointed as general manager of GE's receiving tube department.

Daniels has been manager of the Owensboro tube plant since 1950. He succeeds L. B. Davis who was advanced to the post of general manager of the firm's electronic parts division several months ago. In his new position, Daniels assumes responsibility for all operations of the entire department which includes receiving tube plants at Tell City, Ind., and Anniston, Ala., in addition to two factories in Owensboro.

He joined the engineering department of the former Ken-Rad Tube and Lamp Corp. in 1932. He assisted in setting up the factory engineering section and in developing new manufacturing techniques.

After General Electric purchased the Ken-Rad corporation in 1945, he was named assistant works engineer and a year later was appointed works engineer. He was promoted to assistant to the plant manager in 1948, and in 1950 was appointed plant manager. Notable advances

under his management, include the construction of a new manufacturing building in Owensboro, and the development of the "Snow White" manufacturing program.

Walter Hausz was appointed a member of the technical staff in the technical military planning operation (TEMPO) of GE's defense electronics division.

Hausz has been on special assignment in Washington, D. C. for the past several months. Prior to that, he was manager of the advanced electronics center at Cornell University in Ithaca, N. Y. The center is an applied research and advanced development laboratory primarily devoted to military systems studies. Projects at the center involve work on air defense, air-surface warfare, counter-measures, communications, navigation, detection, and automation.

Prior to his Ithaca assignment, Hausz was manager of development engineering at the G-E electronics laboratory in Syracuse, N. Y.

Herbert D. Barnhart was appointed manager-instrumentation, materials and processes laboratory of GE. He joined the firm in 1946 and has been in measurement engineering since 1950.

RCA Appoints Missile Engineers

Max M. Tall

THE MISSILE AND SURFACE RADAR DEPARTMENT of RCA has appointed Max M. Tall to head its expanding reliability program for missile control projects and activities.

He was formerly associated with Vitro Laboratories and the National Radio Institute of Washington, D. C. He is general chairman of the Third National Symposium on Reliability and Quality Control in Electronics.

Charles F. Woll has been appointed to the newly created post of manager of value engineering in the missile and surface radar department.

He will serve on the engineering staff with responsibility for effecting maximum economy in development and design programs.

Woll has spent the majority of his engineering career in the field of military electronics.

Consolidated Buys Firm, Names Two

CONSOLIDATED ELECTRODYNAMICS Corp. purchased the R. A. Castell & Co. of Glendale, California, electronic components manufacturer.

Formed in 1949, the components firm has specialized in electronic sub-assembly work as a sub-contractor in the missile field and in the development of miniature electrical connectors suitable for high-voltage operation at great altitudes and under adverse environmental conditions. Consolidated plans to broaden activities in these areas when Castell commences operations as the Glendale Division of the firm. R. A. Castell will serve as general manager of the division.

Glenn D. Maxwell

Glenn D. Maxwell was appointed assistant director of the advanced electronic data laboratory of Consolidated.

The AEDL, known as "Datalab," develops advanced equipment in the

magnetic-tape data-processing field.

Maxwell joined Consolidated as a project engineer in 1953. He became assistant supervisor, magnetic tape group, in 1955, and supervisory engineer, Datalab, in 1956.

Herbert I. Chambers has been appointed assistant chief development engineer of Consolidated.

He had been supervisor of electromechanical development. He joined the firm in 1954.

Previously, Chambers was supervisor of new product development for Electric Auto-Lite Co.; senior mechanical designer, Strong Electric Corp.; senior tool engineer, Electric Auto Lite Co., and tool designer, Toledo Scale Co.

Kaiser Promotes Production Head

JOHN ROWE has been appointed assistant to the vice-president of Kaiser Aircraft and Electronics Corp., and will be in charge of manufacturing and other supporting departments at the Richmond, Calif. machining plant. Rowe has been at Richmond since 1951, working as project engineer, chief inspector, quality control manager and production superintendent.

Ampex Adds Space For Recorders

A NEW $350,000 building is under construction in Redwood City, Calif. and will be leased to Ampex Corp. to house expanded production facilities.

The new plant contains 70,000 sq ft of space bringing the firm's total to 230,000 sq ft in the Redwood City area. The facilities are for the production of magnetic tape recorders. The company has long range plans to move its plant from Redwood City to Stanford Industrial Park, in Palo Alto, Calif.

Stackpole Elects New President

H. S. CONRAD was elected president of Stackpole Carbon Co to succeed Lyle G. Hall, and J. Hall Stackpole was re-elected chairman of the board of directors. A. A. Haberberger was elected vice-president

and general works manager and E. J. Hammer was elected vice-president and director of industrial relations.

Hall was re-elected as treasurer and chairman of the executive advisory committee, as were Harrison C. Stackpole as secretary; R. A. Scholes as assistant treasurer, and B. F. Goodrich as controller. Lyle G. Hall, Jr., was elected assistant secretary.

H. A. Williams was named general manager, electronic components division, and Harrison C. Stackpole, general manager, carbon division. These men have the overall responsibility for the sales and research and development activities of their respective divisions. Haberberger has responsibility for all of the manufacturing activity of the company.

Hall has been active with the company since 1912 and has served as its treasurer since 1916 and president since 1938.

The new president, Conrad, has been identified with the company since 1914. He was named vice president in charge of sales in 1923 and in 1929 was elected vice-president and general manager, a position he has held until this time.

Pacific Automation Names Two Engineers

Joseph J. Malneritch

JOSEPH J. MALNERITCH has been appointed chief engineer of Pacific Automation Products in Glendale, Calif. The company engineers and manufactures electronic cable. Malneritch was formerly with Northrop Aircraft as assistant superin-

tendent guidance manufacturing. He will be responsible for supervision and administration of product design and development.

Henry A. Burr was appointed as field service director. He was previously with Northrop Aircraft as staff engineer. He will direct and coordinate all technical field activities.

New Firm Formed In California

LEE CAHN, formerly chief project engineer for Beckman Instruments, formed the Cahn Instrument Co. The new company will design, manufacture, and sell scientific instruments. It is located in Downey, Calif.

Before Beckman, Cahn was with North American Aviation, and the Askania Regulator Co.

Western Adds Plant Space

WESTERN ELECTRIC will add a half-million square feet to its North Andover, Mass., plant opened some six months ago. The building will increase production space by about 50 percent. The firm has two other plants in this Merrimack Valley area. They are at Haverhill and Lawrence, Mass. Employment at the three is now about 6,400.

Kay Lab Promotes Production Manager

GEORGE D. RICE, production manager of Kay Lab of San Diego, Calif., was elected vice-president in charge of manufacturing and a member of the board.

He joined the firm in 1956. He was associated with Stromberg-Carlson since 1947 as assistant production manager and assistant chief electronics engineer.

Federal Sets Lab In Palo Alto

FEDERAL TELECOMMUNICATION LABORATORIES has established a branch communications laboratory in Palo Alto, Calif. Director of the new laboratory is W. S. Chaskin, former manager of carrier development at

Lenkurt Electric Co.

The new laboratory, presently in temporary quarters, has a staff of approximately 12 people. Present plans include a move early in 1957 to an approximately 4,000-sq ft plant in the same general area. Technically a branch of the Federal Telecommunication Laboratories in Nutley, N. J., the new facility is associated with the branch laboratory in San Fernando, California. Intended to concentrate on research and development, the new installation will be concerned with the development of a new line of telephone equipment and related communications accessories which will be manufactured by other groups within the IT&T family.

Radiation Adds Space, Picks Chief Engineer

Parker Painter, Jr.

RADIATION'S new instrumentation division building adds 28,000 sq ft to company facilities. The building will house offices, laboratories and hangar space for the instrumentation of aircraft, missiles, and other test vehicles. Also contemplated for the 320-acre site near Orlando, Florida, is a landing strip for company aircraft.

The quarter-million dollar addition brings total plant capacity to 120,000 sq ft in nine buildings at Orlando and Melbourne, Fla. Primarily engaged in electronic research and development, the firm now employs over 600 people.

Parker Painter, Jr., has recently been appointed chief engineer of Radiation. He will be responsible, under the director of engineering, for the operation and administra-

tion of the entire engineering department. Painter, who has been with the company since its early days, was previously head of its instrumentation division at Orlando, Florida.

Bell Appoints Electronic Engineers

Two appointments were made by Bell Aircraft's new avionics division.

Frank H. Andrix was appointed director of engineering. He joined Bell in 1946 to assist with the engineering of automatic guidance components for the firm's guided missile program and later was appointed chief servomechanisms engineer.

J. D. Schantz was named assistant to division manager. He was employed by Bell in 1949 as an electronics engineer and became head of the electronics department in 1951.

Formation of the avionics division was announced by Bell in line with a company re-organization. It is part of the new weapon systems division, of which Roy G. Sandstrom is vice-president and general manager.

Sanborn Completes New Plant

SANBORN COMPANY'S new $1 million building in the Waltham, Mass., has been completed. Operations will be moved from Cambridge, Mass.

The new 128,000 sq ft building was completed in ten months.

The company, employee owned, manufactures industrial instruments. It employs 750 persons, and for 1956 its volume of sales will top ten million dollars.

Electromation Acquires Hallen

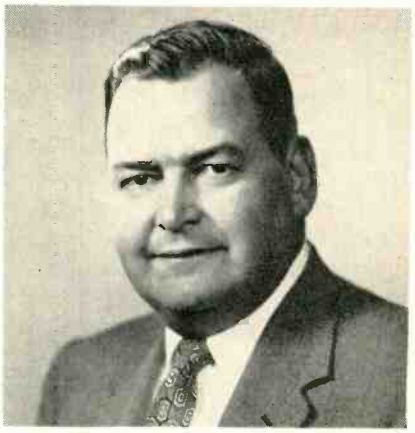
ELECTROMATION CO. of Santa Monica, Calif., acquired the corporate structure of Hallen Corp. of Burbank, magnetic film recording equipment firm.

Electromation acquired Kinevox, a motion picture sound equipment firm, a year ago. In 1956, it acquired Cado Manufacturing Co. of Santa Monica. Cado manufactures

microwave switching components.

Harold L. Powel, former president of Hallen Corp., will supervise the combined Kinevox-Hallen enterprise, as a division of Electromation Co.

Melco Names Engineering Head



William J. Field

MELCO PRODUCTS of Minneapolis, Minn., transformer manufacturers, appointed William J. Field as director of engineering.

During the past ten years Field was with Remington Rand's Univac division in charge of component design and development. He was a specialist in design of pulse, audio and power transformers. He had previously been employed by Minneapolis Honeywell and Bell Telephone Laboratory as a design engineer.

Field was appointed a consultant on inductors and transformers to the National Military Research and Development Board.

New Firm Formed In Boston

THE APPLIED ELECTRONICS CORP. has been formed in Boston, Mass.

It is engaged primarily in research, development and production for both industry and government agencies in the fields of digital and analog computation, data handling and conversion, and automation systems.

Principle officers of the new corporation are George H. Wayne, president, and George F. George, vice-president and treasurer. Wayne

previously was chief engineer of the systems engineering department of Electronics Corporation of America while George was manager of military operations.

NYT And Essex Merge Activities

ESSEX ELECTRONICS of North Hollywood, Calif. has merged with NYT Electronics of Burbank, Calif.

Essex produces transformers and coils and special encapsulated assemblies and networks.

NYT Electronics, an affiliate of New York Transformer Company, Alpha, N. J., manufacturers of transformers and electro-magnetic devices for industrial electronics, is also engaged in producing components.

Kollsman Promotes Production Heads

Philip E. Weber

A MAJOR reorganization of executive functions has taken place at the Kollsman Instrument Corp., subsidiary of Standard Coil Products Co.

Philip F. Weber, formerly Kollsman's factory manager has been appointed assistant to the president with the responsibility for monitoring production, providing interdepartmental liaison and maintaining central analysis for all instrument systems.

Frank Dupre has been appointed to the position of manager of manufacturing, and William McGurn is the new superintendent of the assembly department.

Weber, the new assistant to the president, joined Kollsman in 1935

as project engineer and became factory manager in 1945.

Joining Kollsman in 1939, Frank Dupre, the new manager of manufacturing, was superintendent of the assembly department for the past thirteen years.

William McGurn is promoted from assistant superintendent to superintendent of the assembly department. He joined Kollsman in 1940.

The firm employs about 4,600 people. New facilities in Syosset, N. Y., provide the firm with an additional 160,000 sq ft of plant space for its production of precision navigation and flight instruments.

Hall-Scott Adds Roesch Division

HALL-SCOTT, is integrating the operations of its subsidiary, Douglas Roesch, into its electronics plant at Burbank, Calif.

Douglas Roesch, acquired by Hall-Scott earlier this year, is to be known as the Douglas Roesch cable division of Hall-Scott. Orville W. Nickel will continue to head the division and all key Roesch personnel are being retained.

Norden-Ketay Expands Plant

NORDEN-KETAY CORP. has signed a lease for a new plant to be built as an extension to the Commack, L. I. plant of the precision components division. The new plant will have 31,000 sq ft for manufacturing and engineering activities and will increase the operations to over 85,000 sq ft. The precision components division produces servo mechanism components for aircraft, missiles and automation. General manager of the precision components division is Bernard Levine.

Varian Moves Carnahan To New Post

C. WESLEY CARNAHAN, vice-president and general manager of Varian of Canada Ltd., is now serving as technical assistant to H. Myrl Stearns, executive vice-president and general manager of Varian Associates. He continues as vice-presi-

dent of Varian in Canada.

Carnahan joined the firm in 1953, as an applications engineer specializing in guided missiles after 5 years as electronics research manager for Sandia Corporation in Albuquerque. He previously served in research capacities with Farnsworth, Sylvania, Zenith and Submarine Signal Co.

Nader Appoints Chief Engineer

Leon F. Edelson

NADER MFG. CO. of Monrovia, Calif., appointed Leon F. Edelson as chief engineer. He will be responsible for research and development on all semi-conductor applications.

He was formerly with the Jet Propulsion Laboratory, Pasadena, for 3 years as a research engineer transistorizing guided missile circuits.

Former chief engineer of the firm, Robert T. Schultz, is now general manager. Nader manufactures transistorized power supplies and transistorized digital counters, and develops semi-conductor applications. The plant was recently expanded to 10,000 sq ft.

Stromberg Division Adds Space

A FOURTH building in the West Los Angeles area has been leased by Electronic Control Systems, an affiliate of the Stromberg-Carlson division of General Dynamics Corp. The division makes Digimatic systems for the numerical control of machine tools, and other electronic equipment.

New Books

Circuit Theory and Design

By J. L. Stewart

John Wiley and Sons Inc., New York, 1956, 474 *p.* $9.50.

Within the past decade, the classical steady-state RLC circuit theory has become but a chapter of a much broader theory which includes the theory of active circuits and other types of linear systems. The text under review clearly reflects this fact. Unlike the more conventional texts on circuit theory, it ventures into the design of servomechanisms, feedback amplifiers and even oscillators. In addition, it contains a good deal of material on modern network theory which is not included in older texts.

▶ **Introductory Material** — The first three chapters of the book are introductory in nature. Chapter 1 is given over to a review of elementary circuit analysis and covers rather briefly the setting up of loop and node equations, basic circuit theorems, and the notions of duality and reciprocity. The concept of complex frequency is introduced in Chapter 2, following which some of the basic properties of functions of a complex variable are established. In Chapter 3 the material of the preceding chapter is applied to network functions and, in addition, an abbreviated exposition of the Laplace and Heaviside methods is presented.

▶ **Network Synthesis**—The introductory chapters are followed by: a chapter on elementary synthesis procedures; a chapter on approximation in the frequency domain, with emphasis on the approximation to ideal low-pass and pure-delay type of characteristics; a chapter on some of the more modern methods of synthesis such as the Darlington method. In the space allotted to this chapter (30 pages), the author can hardly be expected to treat the vast subject of network synthesis in any degree of detail. Of necessity his exposition of synthesis techniques is sketchy and, in places, quite inadequate.

▶ **Amplifiers**—The remainder of the text deals in the main with the design of electronic circuits, particularly low-pass and band-pass amplifiers. In addition, the design of feedback amplifiers is touched upon and a brief discussion of servomechanism functions is included.

Despite the very considerable effort which has gone into the writing of this book, the result has some negative features. Thus, the author's exposition is somewhat lacking in depth and not infrequently is marred by minor inaccuracies, ambiguities and excessive sketchiness. On the positive side, the text presents much information which heretofore has not been readily accessible. On balance, it is a welcome addition to the literature of network theory.—L. A. Zadeh, *Columbia University, New York* 27, *N. Y.*

Automatic Digital Computers

By M. V. Wilkes.

John Wiley & Sons, Inc., New York, 1956, 305 *p,* $7.00.

In the opinion of this reviewer, this book is the most noteworthy attempt to date to cover the fundamentals of large-scale digital computer design and use. The emphasis in this volume is on logical design, programming and some of the practical problems concerning the efficient use of computers; electronic circuit techniques are mentioned only briefly and qualitatively. Although most of the material in this volume can be found in various journals, the book is of particular value in that it presents an overall integrated picture to the reader.

▶ **History**—The first chapter presents a fairly extensive history of the development of digital computers up to about the year 1949. Later machines such as the IBM 701 and the Remington Rand UNIVAC receive only superficial coverage at various points throughout

the remainder of the text. Of course, any criticism of this nature must be viewed in the light of the tremendous task of writing a book on such a rapidly expanding subject as digital computers.

For the newcomer to the field, the book has much to offer. The chapters which are concerned with logical design, storage and electronic-switching and computing circuits are thorough, well-written and contain many important practical considerations which obviously have resulted from the author's close contact with these aspects of computer development.

The failure to mention some of the more modern techniques for minimization and general manipulation of Boolean algebra expressions, such as the map method of Karnaugh, is regrettable. Also disappointing is the omission of important new techniques developed from replacing static flip-flop circuits with dynamic one-bit storage circuits, such as those used in the National Bureau of Standards' SEAC and DYSEAC and the International Business Machines' NORC.

▶ **Programming**—A detailed introduction to the principles of programming is one of the outstanding features of the work. Subjects such as the use of subroutines, floating addresses, and the use of multiaddress codes are covered thoroughly enough so that the engineer can evaluate his work from the viewpoint of the programmer after having read and understood these sections. Again from the engineer's viewpoint, study of this section on programming will allow him to venture into the very important field of diagnostic programming, and therefore, help him to bridge the gap between the builder and the user of digital computers.

For the engineer who has no profound interest in programming techniques, but who has had some computer design or development experience (and therefore presumably has been exposed to the copious literature covering logical design, storage systems and switching circuitry), the last chapter of

the book entitled "The Design and Operation of Digital Computers" should be of more than routine interest. The subject of the relationship of the logical design of a computer to its efficient use from the points of view of the programmer, the maintenance engineer, the designer and the computing bureau administrator, is handled admirably. Controversial subjects among computer people, such as the use of error-detecting circuits, marginal checking, physical design, choice of order code and the organization of a scientific computer center, receive a very objective analysis from the author in this section.

This book will undoubtedly be useful as a text for courses introducing the subject of digital computers to electrical engineering students; the need for a text in this field has certainly been very great.—D. E. ROSENHEIM, *IBM Watson Laboratory at Columbia University, New York, N. Y.*

Kristalloden Technik

BY R. ROST, Dr.-Ing, and H. M. ERNST.
Wilhelm Ernst & Sohn, Berlin, 1956, 439 *p.*

THIS book is the second and greatly-enlarged edition of "Kristalloden Technik", which first appeared in 1954. The word Kristallode has been coined from the Greek root ode, meaning path, and is a broad term that the author applies to any device that bases its operation on the semiconducting properties of a crystal.

The first few chapters contain a brief discussion of semiconductors and the physical-electronic principles of germanium and silicon diodes and transistors. Several chapters are devoted to the manufacture of germanium and silicon diodes and transistors. In succeeding chapters, the application of transistors and diodes are discussed and representative circuits are presented.

▶ **Material Sources** — The book leans heavily on the pioneering work and advancements in the state

of the art that have been presented in the American literature and by American industry.

The final chapters present characteristics data of typical germanium and silicon diodes and transistors currently manufactured by German industry.

Since the book is in German, it will have a rather limited appeal to the reader of ELECTRONICS, especially since several good books in English are already available. For those concerned with the state of the germanium and silicon diode and transistor art in Germany, or for those who have to refer to characteristics of German diodes and transistors, the book will be of value.—HORST A. POEHLER, *General Precision Lab., Inc., Pleasantville, N. Y.*

Electrical Circuits: Direct And Alternating Current

BY CHARLES S. SISKIND

McGraw-Hill Book Co. Inc., New York, 1956, 516p, $6.75.

THE prime purpose, particular approach and broad scope of this excellently written two-semester text are, perhaps, best stated in the author's own words: "The circuit is the basis of all energy conversions and transformations associated with electrical equipment: it is logical, therefore, to precede the study of electrical machines and systems by a first course that thoroughly prepares the student to deal effectively with electric, magnetic and dielectric circuits.

▶ **Purpose**—"In organizing and developing the subject matter in this book [for such purpose] the author has endeavored to build a foundation of circuit principles that is both rigorous and consistent with good engineering practice. The wide range of topics is divided into two major sections: Part I deals with circuits in direct-current systems, while Part II builds upon the former and is concerned with alternating-current systems. Much emphasis is placed on similarities and differences between circuits that

are energized by direct current and by alternating current and on relationships that involve combinations of electric, magnetic and dielectric circuits."

▶ **Contents**—The disposition, relative emphasis and essential scope of content directed to these just-stated ends may be summarized as follows: Part I comprises a concise outline of the basic concepts of charge, current, electromotive force, resistance and of their mutual interrelationships; calculation of the resistance of cylindrical conductors, including dependence on temperature and resistivity; interrelation of power and energy and calculation of equivalent resistance of various regular combinations of conductors; a good account of Kirchoff's laws, the superposition and maximum-power-transfer theorems, Thevenin's Theorem, Δ-Y and Y-Δ transformations; basic concepts and calculation of flux density at points in the fields produced by solenoids and rectilinear conductors; calculation of fluxes and magnetomotive forces pertinent to the magnetic-material and air-gaps of multibranched magnetic cores; principles of operation, details of construction and some application of more commonly used d-c instruments and measuring devices; concepts of self and mutual inductance, principles of self and mutual induction, calculation of equivalent inductance, current transients in R-L circuits; concept of capacitance, calculation of equivalent capacitance, current transients in R-C circuits.

Part II comprises basic aspects of generation and calculation of sinusoidal voltages and currents; basic relationships in various circuits comprised of R, L and C parameters; complex-number computation and calculation of equivalent impedances; a detailed account of the principal phenomena of resonance in series and parallel circuit configurations; graphical delineation of voltages, currents and impedances in simple circuits with a variable parameter; the a-c counterparts of the d-c theorems and laws treated in Part I; calculation of current and voltages in coupled circuits with emphasis on the air-

core transformer and kindred devices; principles of operation, details of construction and applications of a selection of commonly-used instruments and measuring devices; a detailed account of calculation of voltage current and power in balanced and unbalanced three-phase circuits; a concise introduction to analytic and graphic determination of Fourier series representation of nonsinusoidal voltages and currents and power calculations therewith.

A subsequent appendix comprises derivation of certain equations merely stated in the context.

▶ **Features**—A careful reading revealed many admirable features, excellent physical details, accurate statement of theory, clear explanation of details of procedure and a systematic presentation of numerical computation. A wealth of auxiliary supporting detail includes a large number of fully worked-out at the end of each chapter a detailed set of questions provides an outline of the essential points covered in the chapter. An accompanying set of problems are sufficiently varied in scope to exemplify all the theory of the chapter and sufficiently great in a number to enable ample variation in assignments from year to year.

▶ **Practical Aspects** — A special and well-fulfilled effort of the author is to inculcate a practical bent to the text by providing: illustrations that are "counterparts of practical systems, devices and machines"; illustrative examples and problems that "correspond to existing electrical systems"; a treatment of the whole that "provides a realistic approach to courses in circuits and machines that are more advanced in character" and, finally, a stress of basic aspects of circuit theory, rather than special phases, so as to "provide the necessary background material for the study of most branches of electrical engineering".

These last-named merits, and the particular aspects noted above, yield a well-integrated, accurately-written and excellently supported

text of such considerable values that the reviewer warmly recommends it to the teacher in a technical institute who seeks a textbook for a two-term course in basic electric circuit analysis; to the teacher in an engineering school who would use this book for a course in circuit analysis for non-electrical engineering students; and —most highly—to the technician or engineer in practice who wishes to gain, or renew, a basic knowledge of electric circuit analysis through self-study.—THOMAS J. HIGGINS, *Professor of Electrical Engineering, University of Wisconsin, Madison, Wisconsin.*

Transistors Handbook

BY WILLIAM D. BEVITT
Prentice-Hall inc., New Jersey, 1956, 390 *p,* $9.00.

A HANDBOOK is a compact volume containing the essentials of a subject. It is a reference book which surveys a field and serves as a guide in the pursuit of further investigation of the subject or any portion of it. With the above definition in mind, the "Transistor Handbook" has a limited claim to the title of handbook.

▶ **Subject Division** — The author, attempting to review the entire field of transistor electronic circuits, has divided his book in two. The first half covers device characteristics and their measurements and transistors as circuit elements and their behavior. The second half covers applied circuitry. Highlights of most of the classic papers on transistor circuits and applications written between 1948 and 1953 are presented. A good bibliography is at the end of each chapter.

Many examples of the state of the art of circuit development to 1953 are given. Here the author emphasizes completed circuits rather than the methods used to design them. The reader must go to the source material to determine the considerations in the circuit design. The text intentionally avoids the physics associated with tran-

sistor devices, as well the mathematics of transistor circuits.

In the fast-moving field of transistor electronics, the task of presenting typical characteristics and circuits is most difficult. In this respect many of the circuits illustrated are already obsolete and some of the transistors shown are no longer produced.

The presentation of device characteristics and their behavior, which are fairly stable, could have been extended to increase the value of the text as a handbook; for example: a generalized equivalent circuit with its various frequency band approximations; interrelation of z, h etc., transistor parameters; include surface barrier transistor, field effect transistor and double-based diode characteristics; solid state diodes.

Despite its limitations the book should be of interest and aid to those surveying the transistor field and some of its circuit problems and accomplishments. The experienced transistor circuit designer must wait for a handbook to help him solve his problems.—F. BRONSTEIN, *Design Engineering Dept., Ford Instrument Company, Long Island City, N. Y.*

Radio Handbook, 14th Edition

EDITED BY WILLIAM I. ORR.

Editors and Engineers Ltd., Summerland, Calif., 1956, 761 *p*, $7.50.

THE 14th edition of the Radio Handbook is designed to provide a concise overall view of the radio segment of electronics and is slanted toward practical engineers, technicians, amateurs and radio men.

▶**Contents**—The Handbook contains 32 chapters which run the gamut from basic circuit and tube concepts to design principals of receiving and transmitting equipment. Of particular interest today are the chapters dealing with semiconductors and single-sideband operation.

In the chapter on semiconductors the characteristic curves of transistors are drawn in the same way

as those for vacuum tubes. While this may not be new, it does represent a deviation from the general practice and may prove to be a worthwhile change since quite often the method used hereofore could prove confusing to those used to working with vacuum tube characteristic curves.

▶**SSB**—The chapter on single-sideband transmission covers the commercial aspects of ssb, deviation and generation of ssb signals as well as reception and adjustment of ssb. Complete information is also given on the construction of an 80-meter filter-exciter for ssb operation.

The handbook is easy to read and should be interesting to all those engaged in electronics whether they are specifically allied to the radio end of the business or not.—*JMK*

Thumbnail Reviews

Hi-Fi From Microphone to Ear—Modern Sound-Recording and Reproduction Technique. By G. Slot, Philips Technical Library, Eindhoven, Holland, 1956, 169 p, $2.75. Though intended for nontechnical audio enthusiasts, this book includes much in the way of important basic concepts, which are not found in this country's publications on the same subject, to interest the engineer hobbyist. May be ordered directly from publisher, with no charge for postage.

Rapid TV Repair. By Warren Heath, Gernsback Library, Inc., New York, 1956, 224 p, $2.90 (paper). Reference guide for tv service technicans to aid rapid servicing of tv sets in the home. Troubles are listed alphabetically and cross-indexed.

An Introduction to Cybernetics. By W. Ross Ashby, John Wiley & Sons Inc., New York, 1956, 295 p, $6.50. Principles of cybernetics for those without a background in electronics and with only an elementary knowledge of mathematics. Techniques and principles of modern electronics, as presented here, offer an invaluable aid to the biological scientist interested in a behavioristic approach to the understanding of such complex mechanisms as the human being and human societies.

Backtalk

Thank You

DEAR SIRS:

IT CERTAINLY isn't often that quantity and quality are found in the same publication, but your magazine ELECTRONICS has been consistently maintaining the combination. In addition to the very fine articles, the advertising adds much information and valuable reference material.

While I have only been subscribing since November 1955, my brother has been a subscriber for more than 10 years. Recently, he gave me issues that he has been keeping since 1950, and gradually I am getting them read.

Again I must say that your magazine is the best in the field and you can expect to get a renewal from me in the near future.

ROBERT A. RAY
Columbus, Ohio

F-M and PCM

DEAR SIRS:

IN his last article on noise (Part V, "Reducing Noise in Communications Systems," ELECTRONICS p 148, July, 1956), W. R. Bennett claimed that pulse-code modulation is the "most efficient" method for reducing noise in a communication system. The use of the term "most efficient" is somewhat dubious.

Undoubtedly, pulse-code modulation serves quite well for special applications such as teletype communications or the transmission of certain types of continuously-variable numerical data. But the implication that such a system is much superior to frequency modulation seems to be unjustified if no reservations are made.

From time to time people familiar with frequency modulation hear rumors to the effect that if the FCC had it to do over again, it would probably choose a broadcast system using pulse modulation rather than f-m. But, when all the pros and cons are considered, it seems very unlikely that such a choice would have been a wise one.

In the first place, pulse-modulation systems require a much greater bandwidth than f-m. (Pulse-code modulation seems to be the worst offender, taking perhaps nine times the bandwidth needed in f-m) The larger bandwidth not only shows a poor economy of spectrum, but also allows more radio noise to get a chance to override the signal.

Secondly, through the use of properly designed receivers,* f-m is capable of suppressing radio interference which all but equals the amplitude of the desired signal. (Bennett and I seem to disagree on this point.) Since ordinary pulse modulation systems require that the received signal be at least twice the amplitude of the noise, this is a definite advantage for f-m. In particular, severe cochannel, adjacent-channel, and multipath interference can be dealt with more effectively in f-m than in ordinary pulse-modulation systems.

*REFERENCES

(1) Arguimbau, L. B. and Granlund, J. "The Possibility of Transatlantic Transmission by Means of Frequency Modulation," International Radio Congress, Rome, Sept.-Oct. 1947.

(2) Arguimbau, L. B. and Granlund, J. "The Possibility of Transatlantic Communication by Means of Frequency Modulation," *NEC Proc.*, Chicago, Nov. 1947.

(3) Granlund, J. "Interference in Frequency-Modulation Reception," MIT Res. Lab. of Electronics: Technical Report No. 42 (Jan. 20, 1949).

(4) Arguimbau, L. B. and Granlund, J., ELECTRONICS, Dec. 1949, p 101.

(5) Arguimbau, L. B. "Frequency Modulation", *Jour. Madras Inst.* Tech., Nov. 1953, p 153.

(6) Baghdady, E. J. "Frequency-Modulation Interference Rejection with Narrow-Band Limiters," *Proc. IRE, Jan.* 1955, p 51.

BRUCE G. CRAMER
Harrisburg, Pennsylvania

DEAR MR. CRAMER:

RESPONSE to the articles on noise has been highly gratifying and I would like to express my thanks to you and others for taking the trouble to write letters about the subject.

I did not intend to claim unconditional superiority of pcm over all other transmission systems in combatting noise. Individual transmission problems require individual scrutiny and certainly there are cases where f-m, for example, is a more sensible choice. In fairness to pcm, however, I would like to add

a few reservations to your reservations.

With regard to your statement that pcm requires a greater bandwidth than f-m, it is important to keep in mind that the transmission quality within the band in the two cases may be quite different. You state that it is possible to suppress many kinds of interference with f-m even when the amplitude of the interference all but equals that of the desired signal. I agree that this may be feasible in single-hop systems provided that you do not mean absolute elimination, but only a sufficient reduction in amount of interference relative to signal to make the received signal quality acceptable.

One must distinguish here between single-hop applications and radio relay. Interference which produces a negligible effect in one hop may, when added to a number of like contributions from successive repeaters, become disastrous. The unique advantage of pcm is that it is able to exploit bandwidth of mediocre quality by regenerating the signal and thereby preventing accumulation of trouble.

Each link of a pcm relay can contain noise, interference and waveform distortion in any amount short of causing actual recognition errors. In an f-m relay, on the other hand, the output signal-to-noise ratio from the first link must be made considerably better than the requirements on the entire system since defects add from link to link.

A monograph by C. B. Feldman and myself deals with a number of these problems in more detail. There is no claim for an all-inclusive set of answers.

W. R. BENNETT
Bell Telephone Labs, Inc.
Murray Hill, N. J.

DEAR MR. BENNETT:

I WAS pleased to receive your reply to my letter regarding f-m and other modulation systems. Thank you also for the copy of the 106-page monograph by Feldman and yourself.

Since I am presently writing a magazine article, I can well appreciate the amount of work that must have gone into your series of five

articles. I have not yet had the time to read the first four, but an engineer friend of mine speaks quite highly of your work and tells me he has found these articles very informative.

In my letter to ELECTRONICS magazine it was my intention to be concerned only with broadcast systems rather than the more general approach which you used. In particular I first wanted to say a reassuring word about the advantages of f-m over various pulse modulation systems for the transmission of high-quality audio.

Secondly, I wanted to point out that the theoretical threshold for f-m quieting lies where the interference is 100 percent of the desired signal rather than 50 percent or less. Since the inception of f-m there has been a gross misunderstanding on this point which still seems to be widespread. As Arguimbau and Granlund mentioned (reference 4 in my other letter), "this idea of a threshold perhaps arose from the difficulties of computing the interference from ratios near unity and from the fact that with heavy interference receivers depart from our idealized notions of what they should do."

Receiver Problem

On pages 90 and 91 of your monograph I notice that you consider the f-m interference due to an undesired signal which differs from the desired signal by a frequency equal to $(q - p)$. As you show, the output from an f-m broadcast receiver under this condition would be an infinite series of harmonic tones whose fundamental frequency would be $(q - p)$. If we consider only a small amount of interference the harmonics of $(q - p)$ can be neglected—only the fundamental remains important.

Many investigators in the past have found this mathematical expedient too tempting to pass up. When it was found that conventional receivers reacted poorly under 25 percent or more interference, the harmonics were blamed for it.

With new and surprisingly simple mathematical artillery, Granlund (reference 3) has shown that an

f-m receiver need not exhibit more than 4.44 per cent interference so long as the noise remains less than the signal. And when the radio interference is 50 per cent, a good detector will show no more than 1.48 percent noise. (These figures assume a 75-kc deviation and a 75-μsec time constant.) Of course, in the more normal situation the radio interference is dispersed throughout the 200-kc bandwidth, making most of the noise superaudible.

The references I listed in my letter tell what is wrong with conventional receivers and just what to do about it. (I should also have referenced Arguimbau's text: *Vacuum Tube Circuits.*)

I consider it unfortunate that the large majority of receiver manufacturers have remained ignorant about the facts of good receiver design although much technical information has appeared on the subject since 1947. Out of a list of 38 "Hi-Fi" tuner manufacturers only three can claim a high capture ratio.

Relay Systems

As you indicate, the telephone company is most concerned with multiple hops to carry messages 3,000 miles or so. Disregarding scatter propagation systems, the transmitter power used in such hops is microscopic when compared to high-power broadcast stations. Due to its unique noise property, pcm seems like a truly clever innovation for this assignment.

Some f-m broadcast stations, however, have been used in multiple hops to provide various f-m networks. The quality of the audio from the last station in a line of six or eight has often been quite poor. The major blame in this particular case is not with the transmision medium or the system of modulation. Instead the trouble lies in the fact that at each transmitter the signal is demodulated (often by questionable equipment), processed and then remodulated.

This trouble could be solved by limiting and heterodyning the received signal to its new carrier frequency without any demodulation taking place. So far as I know, no

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f-m station has done this. (Incidentally, this method offers the additional advantage of rebroadcasting multiplexed programming without the use of multiplex equipment at any but the originating station).

You are certainly correct in stating that noise is additive in f-m repeaters. However, it seems possible to rebroadcast high-quality signals from high-power f-m transmitters. For example, the programs from WQXR-FM, New York, are rebroadcast by WFMZ in Allentown, 80 miles distant. Even at this distance their excellent location allows them to receive WQXR-FM on a piece of twin-lead just 5 feet off the ground.

It would seem reasonable to expect perhaps no more than 1 or 2 percent interference (r-f) using a well-placed highly directional antenna. This, multiplied by the 30 or 40 transmitters necessary to hop across the country, would give from 1 to 2.5 percent audio noise in San Francisco! Again, we would probably be limited by the additive tube noise from each station. (Of course, as you say, even this would be taken care of by pcm.)

The plan seems practical. I am told that Major Armstrong had hopes of establishing a nation-wide f-m network.

I have taken this opportunity to try to bring to light some of the facets of f-m radio, especially the results of Arguimbau's work. The technical difficulties must be cleared away before we can expect f-m to assume its proper niche in broadcasting.

BRUCE G. CRAMER
Harrisburg, Penna.

Goose Egg

DEAR SIRS:

IN your October issue on page 404 you ran a notice about Pacific Automation Products, Inc.

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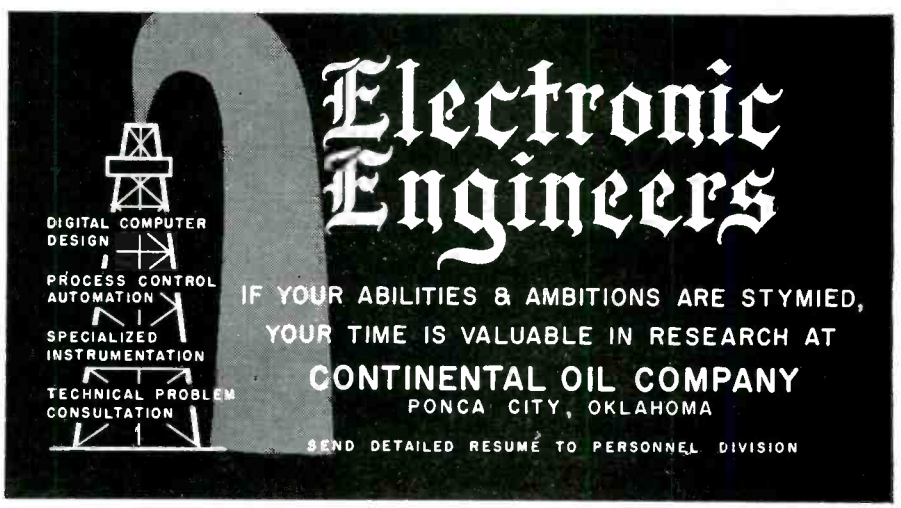

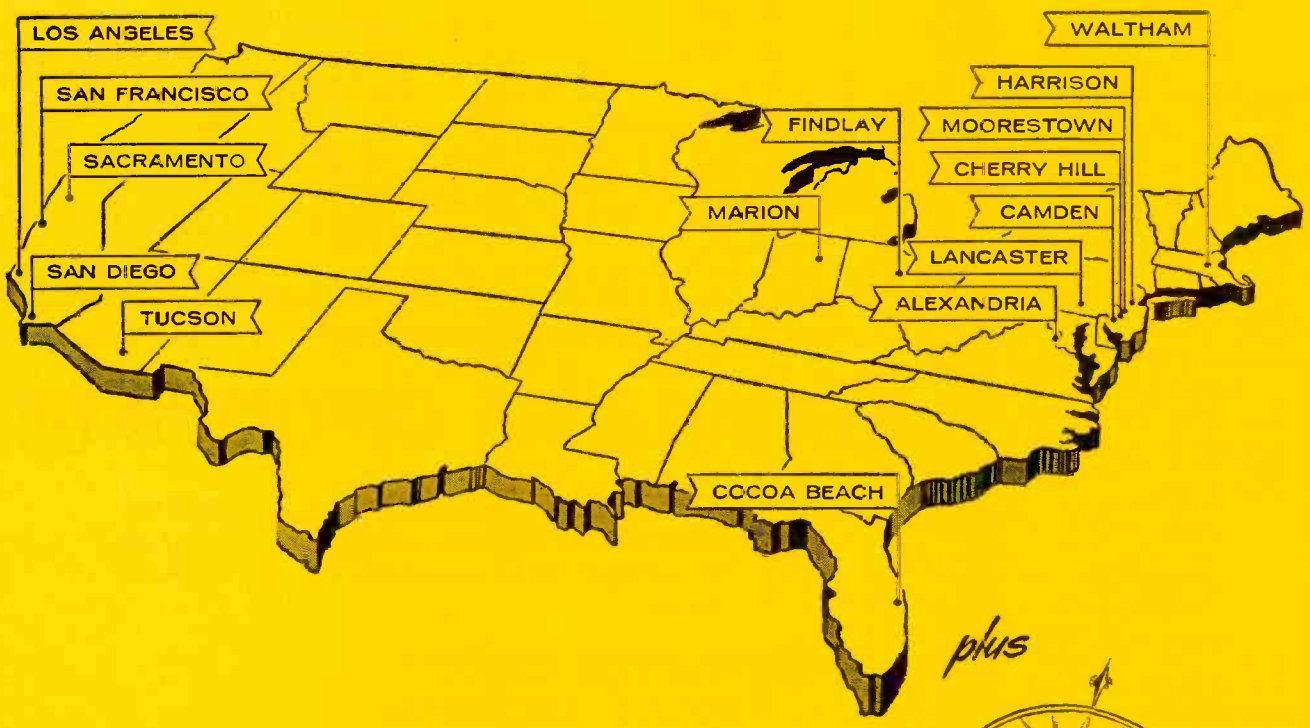

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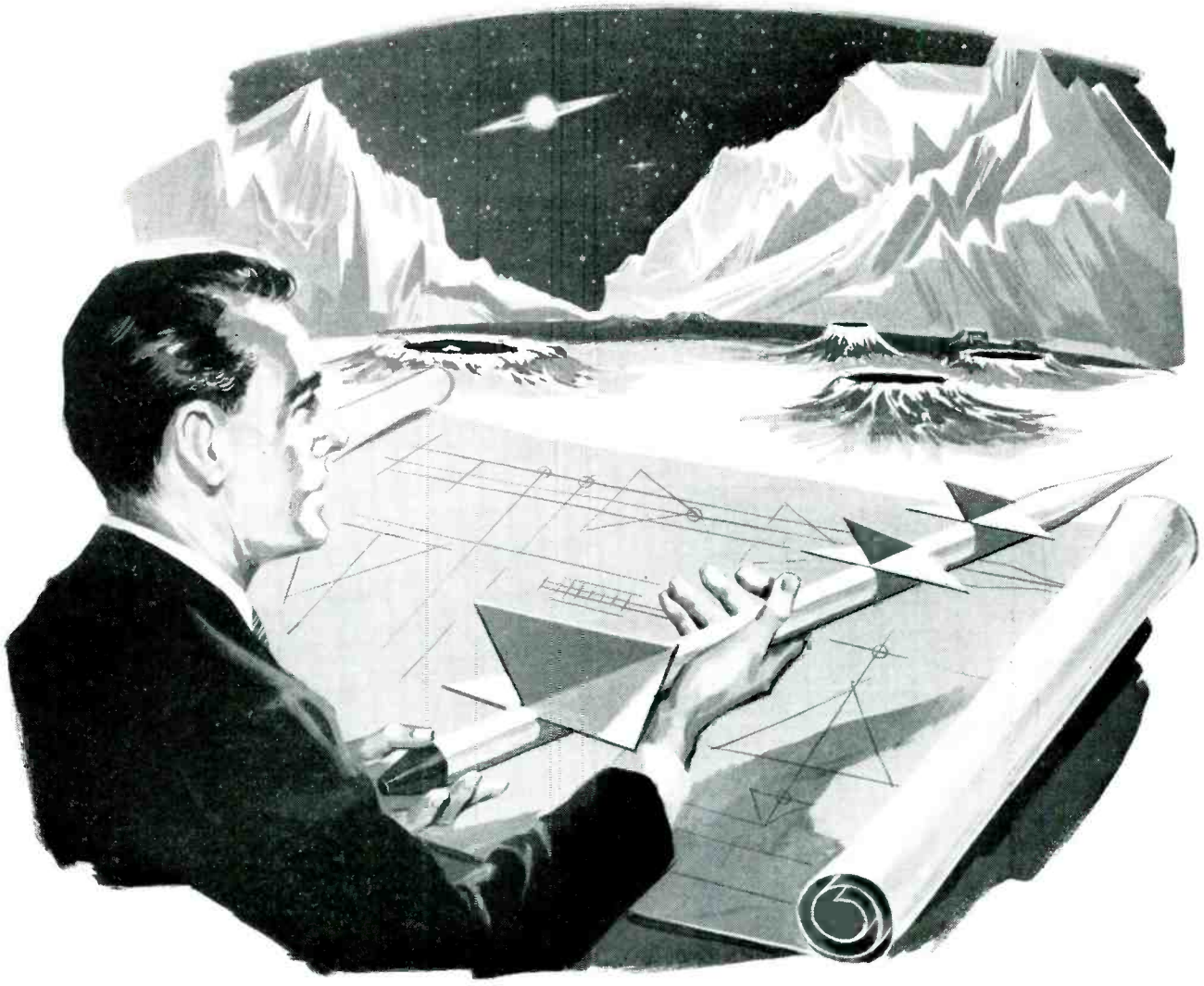

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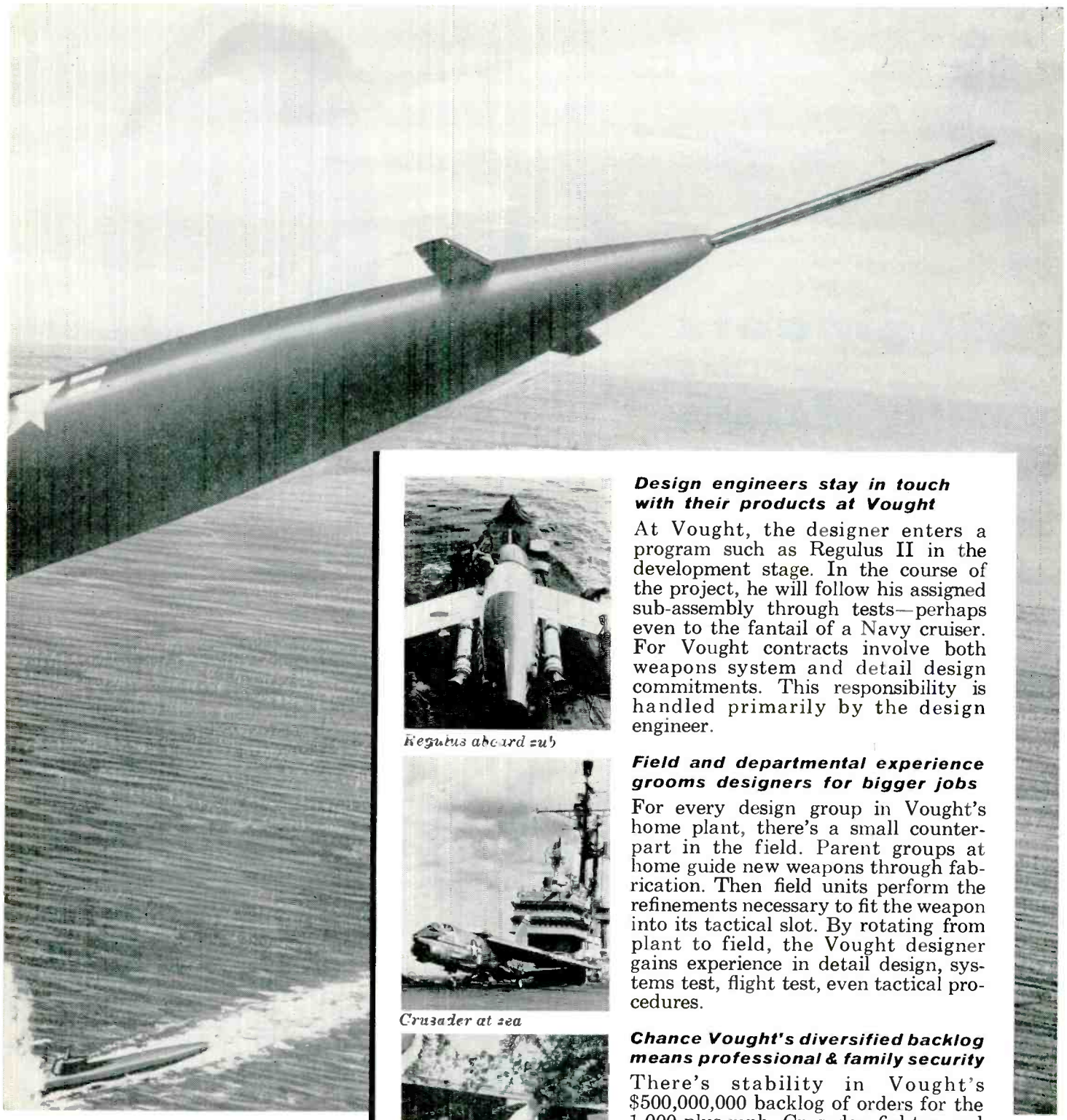

Regulus aboard sub

Crusader at sea

Design engineers stay in touch with their products at Vought

At Vought, the designer enters a program such as Regulus II in the development stage. In the course of the project, he will follow his assigned sub-assembly through tests—perhaps even to the fantail of a Navy cruiser. For Vought contracts involve both weapons system and detail design commitments. This responsibility is handled primarily by the design engineer.

Field and departmental experience grooms designers for bigger jobs

For every design group in Vought's home plant, there's a small counterpart in the field. Parent groups at home guide new weapons through fabrication. Then field units perform the refinements necessary to fit the weapon into its tactical slot. By rotating from plant to field, the Vought designer gains experience in detail design, systems test, flight test, even tactical procedures.

Chance Vought's diversified backlog means professional & family security

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Mr. J. W. Larson,
Ass't. Chief Engineer
Engineering Personnel Dept. 1-E

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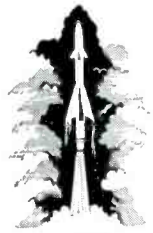
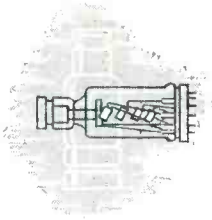
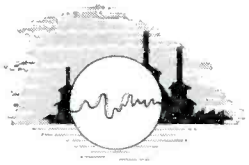


MISSILES



SPECIAL PURPOSE TUBES



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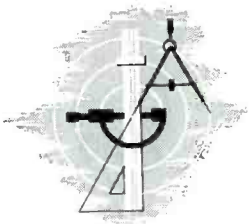
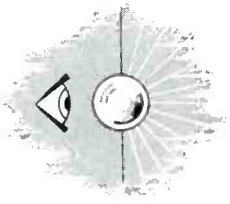
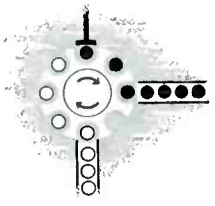


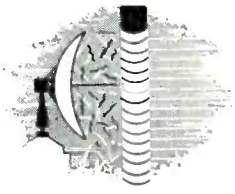
PRODUCT ENGINEERING



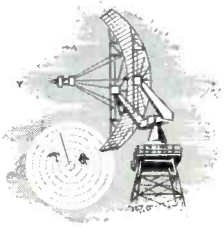
INFRA-RED



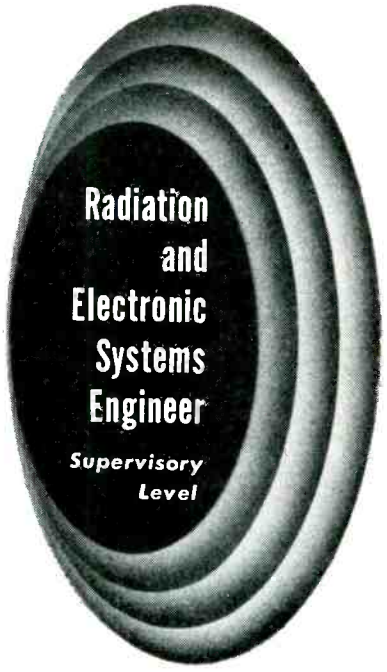
PRODUCTION



COUNTER-MEASURES



RADAR



The Missile & Ordnance Systems Department of General Electric, prime contractor for the development of the ICBM and IRBM nose cones, has a responsible opening for a qualified engineer or scientist in its Nuclear Ordnance Projects Component Equipment Design Operation.

Position Responsibilities: Design, development, and evaluation of passive and active radiation type systems (i.e., radar, infra-red, ultra-violet, optical, etc.) as applied to arming and fuzing of missile systems.

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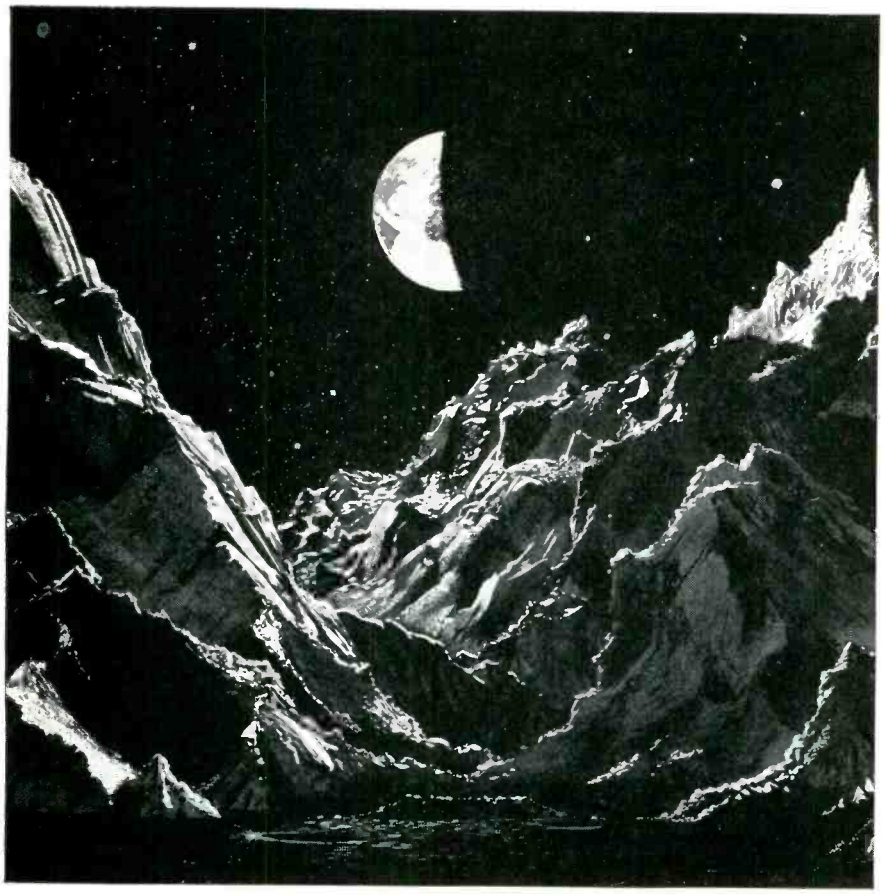

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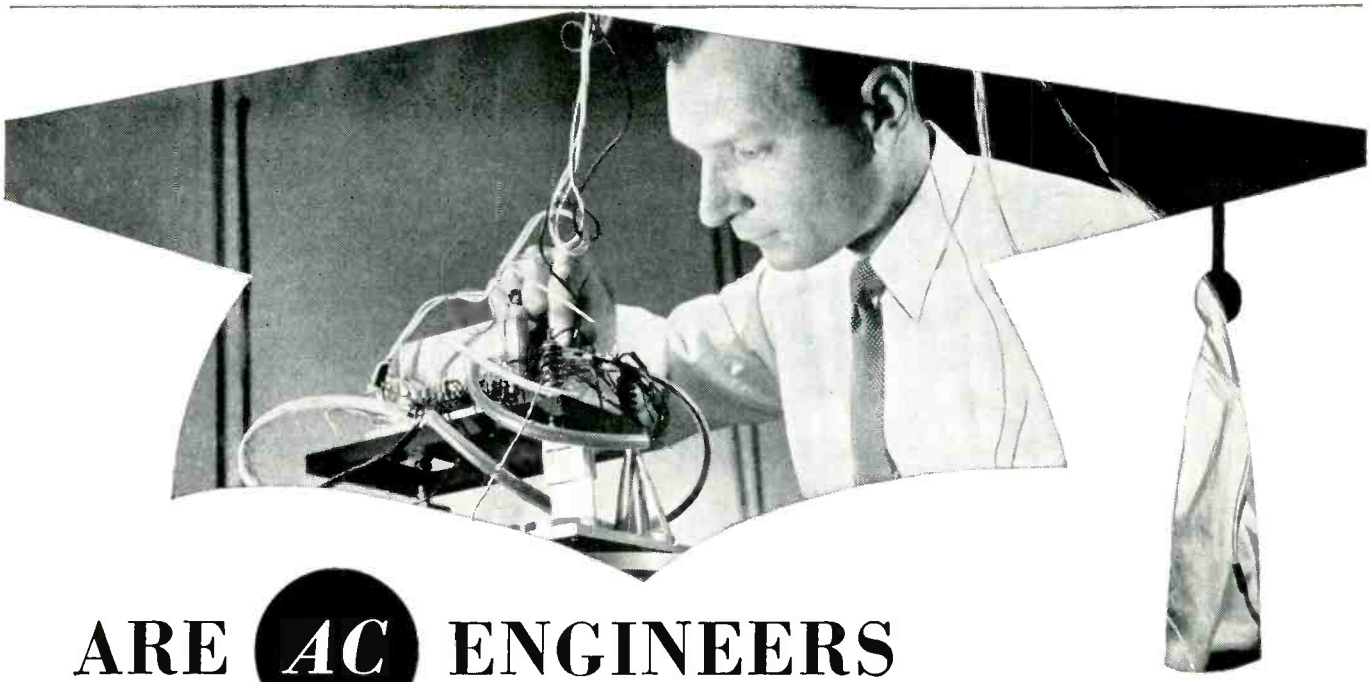

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AC has worked out a Master's Degree Graduate Program (evenings) at the University of Wisconsin, Milwaukee. AC pays all tuition fees for this program.

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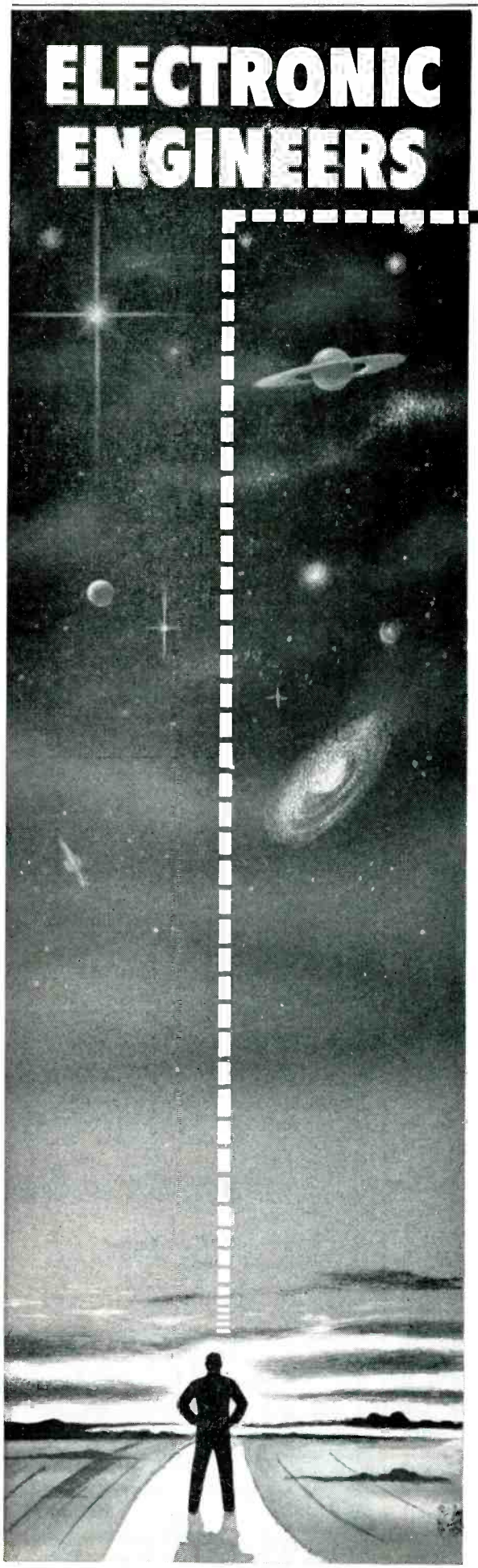

Consider the significance of your profession!

The shape of things to come is being designed by electronic engineers of professional stature, the exceptional engineers who—by education and experience—are qualified to fulfill an important destiny. Such men are needed at Bendix Radio to do research and development on the most advanced electronic systems in both military and commercial fields.

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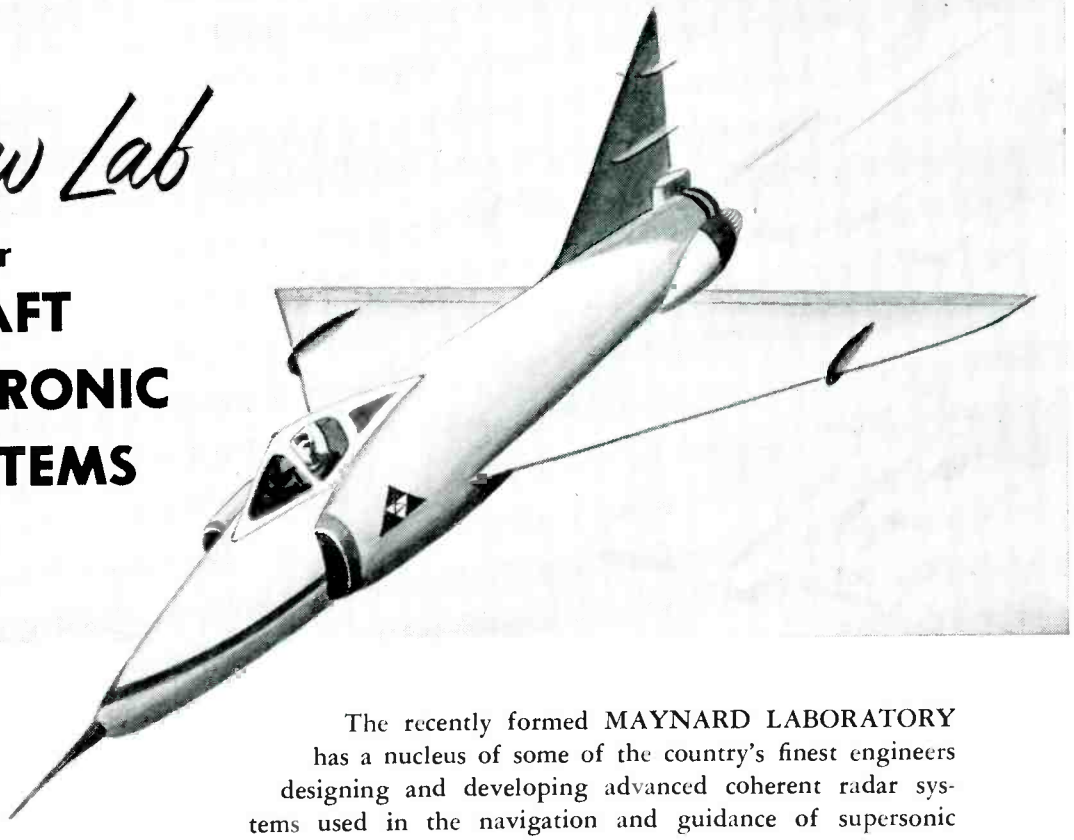

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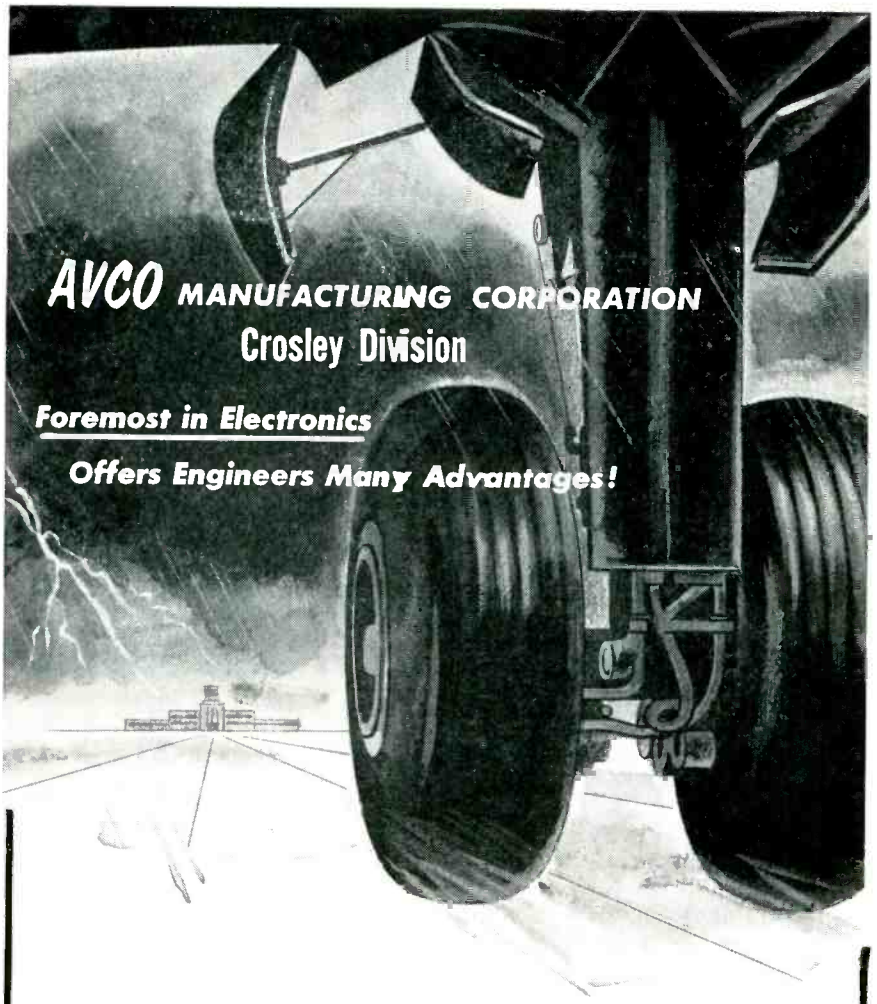

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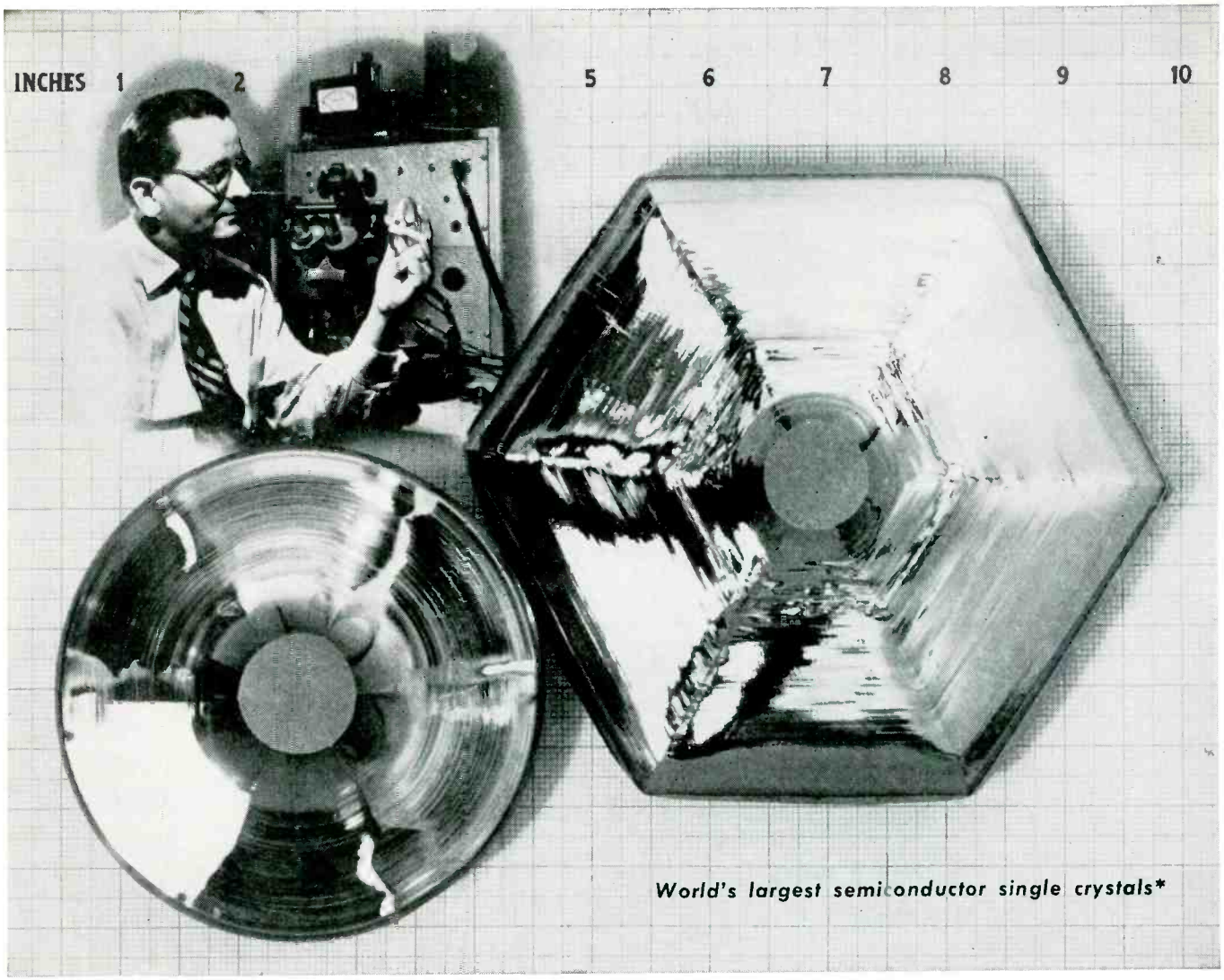

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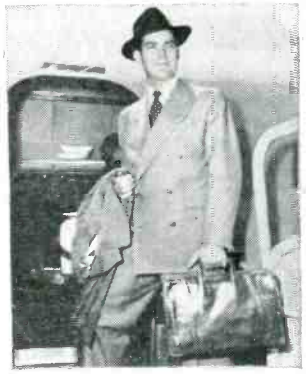
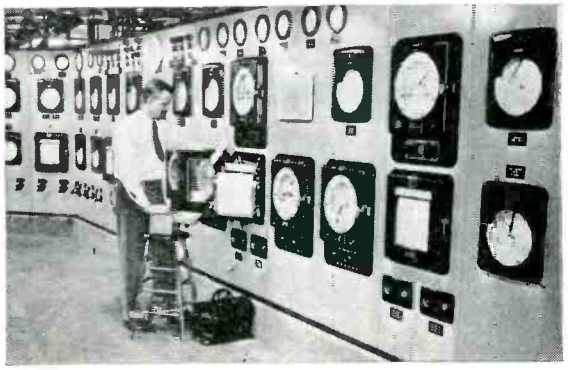


• *Visit Customer Plants*

• *Plant Engineer Contacts*



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MISSILE RADAR SYSTEMS ENGINEERS
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MICROWAVE DEVELOPMENT ENGINEERS
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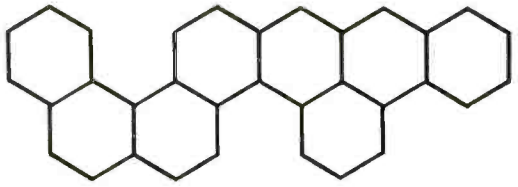

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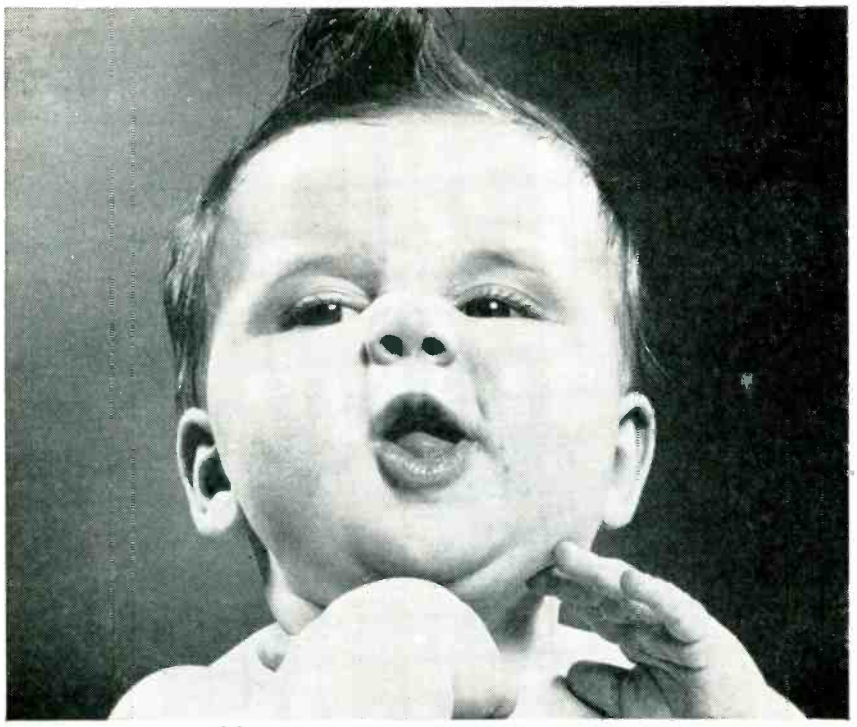

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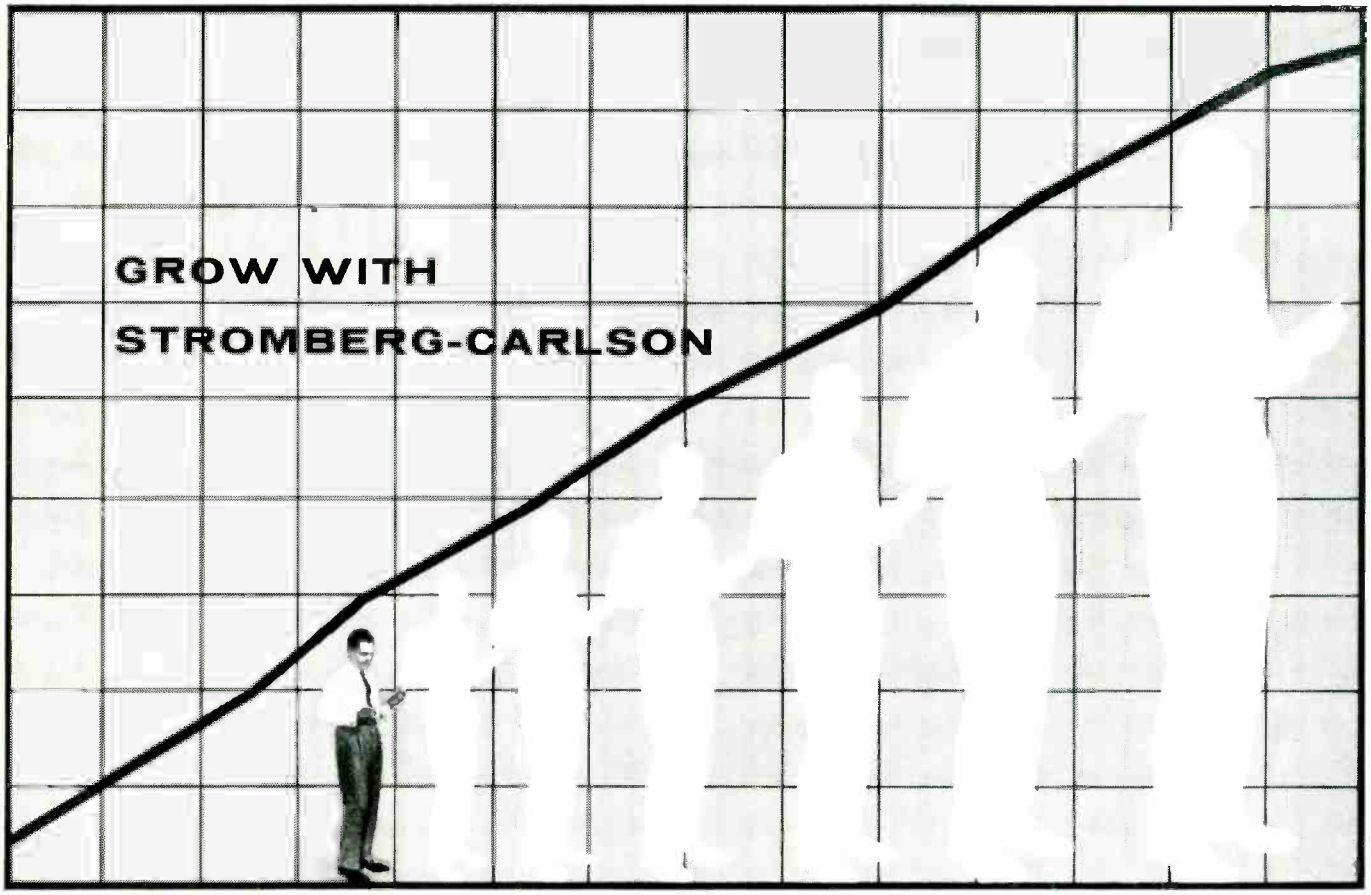

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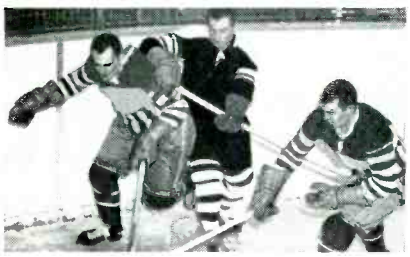

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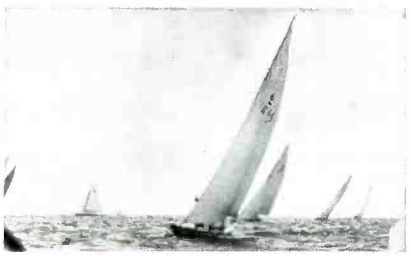

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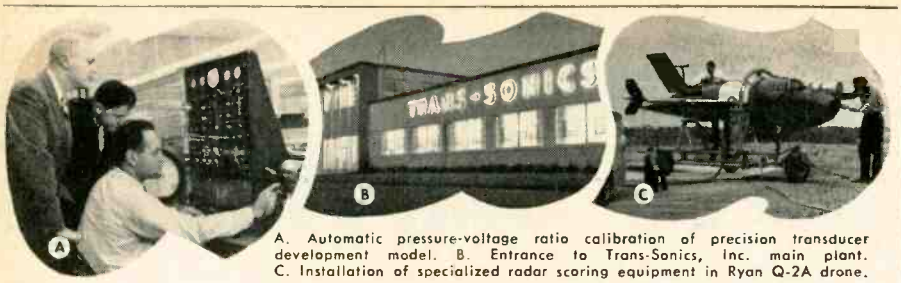

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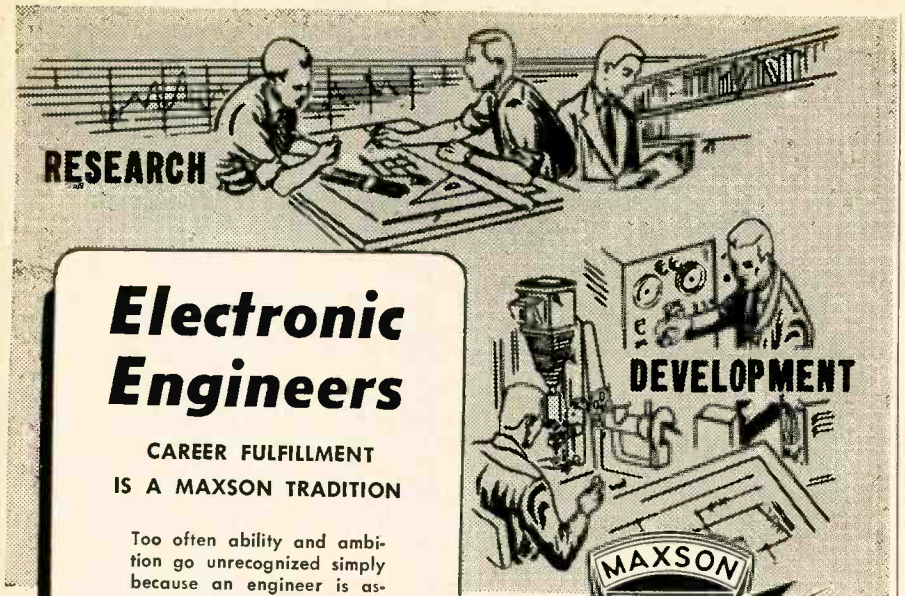

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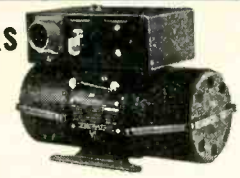

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Output: 115 V; 3 phase; 400 cycle; amps. .5 Input: 24 VDC; 12 amp. **$49.50**

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Output: 26 volts; 3 phase; 400 cycle; 10 VA; 6 PF. Input: 27.5 volts DC; 1.25 amps. **$24.50**

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Output: 125.5 VAC; 1.5 amps. 400 cycles single phase, 141 Va. Input: 20-30 VDC. 18-12 amps. Voltage and frequency regulated. **$49.50**

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Output 250 VA, 115 volts, 3 phase, 400 cycle, 1.25 amp., 0.8 pf. Input 27.5 volt DC, 20 amp. **$59.50**

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Output: 115 volts AC; 750 VA, 3 phase, 400 cycle, .90 pf and 26 volts. 50 VA single phase, 400 cycle, .40 pf. Input: 27.5 VDC 60 amps. cont. duty, 6000 rpm. Voltage and frequency regulated. **$59.50**

10339 Leland
Output: 115 volts; 190 VA; single phase; 400 cycle, .90 pf. and 26 volts; 60 VA; 400 cycle, .40 pf. Input: 27.5 volts DC, 18 amps. cont. duty, voltage and freq. regulated. **$49.50**

10486 Leland
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1:1 reverse ratio, 60 teeth on large gear; ¼" shaft. Size: 3" long with 1-15/16" dia.

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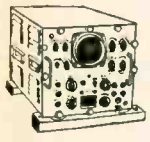

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4J26	100.00
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6J6W	1.00
6K4	2.25
6L6WGB	3.75
6L6Y	2.00
6SK7W	1.00
6SL7W	1.25
6SU7GTY	2.25
6X4WA	2.25
6X5W	1.00
6X5WGT	1.25
7UP7	20.00
7YP2	150.00
SRC-12	150.00
12AY7	1.70
12DP7	15.00
12GP7	15.00
12SP7B	25.00
X-13	150.00
BL-15	Q
BL-16	Q
PG-17	3.95
RX-21	3.50
PJ22	Q
HK24	3.00
26A7GT	3.00
26E6WG	2.50
RK-28A	2.50
BK29D	Q
VR33	89.50
35T	3.00
D-42	40.00
RK47	3.00
V-50	75.00
V-50XR	75.00
HK-54	2.00
QK-57	Q
QK-59	20.00
QK-60	20.00
RK-60/1641	1.25
QK61	20.00
RK-61	2.50
QK-62	20.00
HY-65	1.00
RK-65/5D23	7.50
FG-67	9.00
HY-69	2.25
RKR-72	.50
RKR-73	.50
FG-95	16.50
ML-100	50.00
100TH	6.50
WE101D	3.00
WE101F	3.00
FG-104	29.50
FG-105	11.00
F-123A	2.50
F-128A	10.00
FG-154	10.00
VT158	9.75
FG-166	6.75
FG-172	17.50
QK-181	12.50
HF-200	10.00
WL-200	75.00
QK202	165.00
203A	3.50
204A	25.00
205F	6.00
207	75.00
211/VT4C	.50
212E	15.00
WL-218	15.00
CEP220	4.00
QK221	150.00
RX233A	.75
QK235	Q
QK-243	50.00
QK-249	150.00

WE245A	6.45
249B	2.50
249C	3.00
250-R	4.50
250TH	21.00
250-TL	12.50
WE-251A	49.50
WE-252A	7.50
QK253	Q
WE-254A	2.50
FG-258A	80.00
WE-258B	5.00
V-260/VA-6310	75.00
V-262	75.00
FP-265	20.00
WE-269A	6.00
FG-271	25.00
271A	6.00
WE-274B	.90
FG-280	27.50
WE-282A	2.75
WE-282B	5.00
WE283A	3.50
QK283A	150.00
QK284A	150.00
WE-285A	5.00
WE-286A	5.00
287-A	2.20
WE-290A	7.00
GB-302	5.00
304TL	12.50
WE-305A	2.85
307A/RK75	.75
WE-308B	12.50
WE-310A	4.00
WE-311B	4.00
WE-312A	1.50
WE-315A	10.00
WE-316A	.50
QK-319	Q
WE-323A	10.00
WE-336A	5.00
WE-337A	5.50
WE-338A	5.00
WE-348A	6.00
WE-349A	5.00
WE-350A	2.50
350B	2.00
354C	5.00
WE-355A	9.95
WE-356B	3.50
WE-359A	2.00
368AS	1.00
385A	Q
WE-388A	1.20
WE-393A	4.50
WE-394A	3.00
WE-396A	3.25
FP-400	20.00
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WE403B/5591	2.75
WE-404A	15.00
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WE-408A	2.25
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GL-414	63.00
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WE-428A	40.00
GL-434A	5.00
WE-438A	40.00
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RH-507	20.00
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527	25.00
WL-530	17.50
559	.40
CUE578	8.50
579B	Q
583	2.00
KU-610	3.50
KU-627	7.50
KU-628	7.50
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GL-672	20.00
WE-701A	2.50
702A	.50
WE-703A	1.25
WE-704A	.60
WE-705A	.75
706AY-GY	10.00
707B	2.50
WE-708A	.75
WE-709A	1.50
714A	7.50

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726A	5.00
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807W	2.00
808	1.00
809	2.25
811	2.90
812A	3.50
813	9.00
814	1.35
815	1.50
828	8.00
829	5.00
829B	8.50

1636	.75
1641	1.35
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2050	1.00
2051	.65
HK3054	100.00
ZB3200	99.50
4210	C
R-4330	9.00
R-4340	9.00
5516	5.50
5517	1.00
5531	C
5544	25.00
5545	25.00
5551/FG271	25.00
5553/FG258A	80.00
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5560	16.50
5561	29.50
5586	110.00
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1623	1.25
1624	1.15
1625	.30
1626	.25
1631	1.00

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5644	6.50
5645	6.00
5646	4.50
5647	5.00
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5651	1.40
5654	1.50
5654/6AK5W/6096	3.25
5656	7.00
5657	100.00
5663	1.25
5665	35.00
5667	125.00
5670	2.00
5670WA	4.25
5675	7.00
5676	1.15
5683	5.75
5686	1.75
5687	2.75
5687WA	4.75
5691	5.00
5692	5.00
5693	4.50
5696A	1.25
5702	1.50
5702WA	6.00
5703	.90
5703WA	4.00
5704	1.60
5718	1.75
5719	1.50
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5726/6AL5W/6097	3.25
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5750	3.00
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5814	.65
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5837	50.00
5840	3.50
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5844	1.50
5847/404A	15.00
5851	4.00
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5853	Q
5876	8.00
5879	1.25
5881	2.50
5893	9.00
5894	15.50
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5898	Q
5899	4.00
5902	4.50
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5902A(CL)	2.50
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5907	14.00
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5915	.50
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6046	.75
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6074	2.50
6080	4.00
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6081/ATR407	22.50
6088	1.50
6095	2.00
6096	1.30
6097	1.50
6099	1.40
6100/6C4WA	2.25
6101/6J6WA	2.25
6110	6.00
6111	4.00
6112	4.50
6116	150.00
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6130	7.50
6134	3.50
6136	2.50
6147	3.00
6159	3.00
6161	60.00
6169	Q
6177	75.00
6189/12AU7WA	3.00
6201/12AT7WA	3.00
6203	2.75
6205	4.50
6211	1.25
6264	11.50
VA-6310/V260	75.00
6339	20.00
6533	10.00
6788	8.50
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Heavy Duty Includes Headset, Chest Mike and 20 Ft. Cord. $14.88 ea.
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6 RPM reversible.....$10.00
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P.M. motors. Made for 24 volts. Will work at lower speed at 12v. or 6v. Battery or Rectifier. Size 1"x1"x2". $3.75

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4 mfd.—600 V . . . . . $.95
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16 mfd.—600 V $1.89
Dual 8 mfd oil filled cond. hermetically sealed and packed. Tobe type PT-SC-11 measuring 3¾"x2⅝"x2⅝". Stud mntg. centers 2". Plugs into standard four prong socket.

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.005	15KV	9.75
.005	25KV	20.95
.005	50KV	29.50
.01	1500	.65
.012	25KV	12.95
.015	16KV	14.50
.02	8000	4.75
.02	10KV	5.25
.02	20KV	10.95
.025	50KV	32.95
.03	7500	4.25
.03	16KV	6.95
.04	17KV	8.95
.05	7500	4.25
.05	25KV	16.50
.05-.05	12KV	9.95
.08	12.5KV	8.95
.1	1250	.29
.1	1500	.39
.1	2000	.58
.1	2500	.79
.1	3000	.69
.1	3000	1.19
.1	4000	1.39
.1	5000	3.25
.1	6000	2.25
.1	7500	.95
.1	7500	4.25
.1	10KV	8.25
.1	12KV	6.95
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.1	20KV	19.50
.1	25KV	24.50
.125	27.5KV	27.50
2x.1	2000	.89
2x.1	6000	2.29
.2	10KV	8.50
.2	13KV	10.50
.2	15KV	13.90
.2	50KV	69.50
3x.2	4000	2.85
.25	1500	.88
.25	2000	.98
.25	3000	1.45
.25	4000	1.98
.25	6000	.89
.25	15KV	15.95
.25	20KV	19.95
.25	25KV	40.00
.3	2000	.49
2x.25	2000	.98
.4	10KV	10.90
2x.4	7500	5.25
.5	600	.39
.5	1500	.59
.5	2000	1.19
.5	2500	1.29
.5	3000	2.39
.5	5000	3.05
.5	7500	5.75
.5	12.5KV	37.50
.5	25KV	39.95
.5-.1	2000	.39
2x.5	600	.69
2x.5	9000	9.25
1	500	.35
1	600	.44
1	1000	.69
1	1500	.99
1	2000	1.85
1	2500	2.20
1	3000	2.95
1	4000	4.95
1	5000	6.25
1	6000	6.50
1	6000	8.95
1	7500	14.75
1	10KV	25.95
1	15KV	32.50
1	20KV	51.95
1	25KV	65.00
1	25KV	75.00
1	30KV	PUR
2x1.25	7500	20.00
1.25	330VAC	.49
1.5	15KV	49.50
2	600	.55
2	1000	.79
2	1000TLA	1.29
2	1500	1.15
2	2000	2.80
2	2500	3.45
2	4000	7.50
2	5000	12.50
2	7500	23.25
2	10KV	59.95
3	1000	.98
3	2000	2.50
3	4000	8.50
3	8000	29.50
4	600	.75
4	600TLA	.95
4	1000	1.10
4	1500	2.65
4	2000	3.75
4	3000	6.99
4	4000	17.50
4	5000	24.95
4	7500	59.50
4	10KV	74.50
4	15KV	PUR
5	220AC	1.19
5	330AC	1.39
5	1000	1.89
5	1500	2.45
5	5000	27.50
2x5	400	.89
2x5	600	1.19
6	600	1.69
6	330AC	1.69
6	1000	1.95
6	1500	2.95
6	2000	3.50
6	7500	63.50
7	110AC	.59
7	600	1.35
7	800	1.55
8	600	1.29
8	1000	2.15
8	1000	1.39
8	1500	3.65
8	2000	6.95
8	2500	9.50
2x8	600	1.89
4x8	600	3.85
9	10KV	PUR
2x2.5-5	600	1.75
10	400	.65
10	600	.75
10	600	1.50
10	1000	3.75
10	1500	4.25
10	2000	6.35
10	2500	10.95
10	4000	PUR
10	5000	PUR
12	1000	3.50
13.5	10KV	PUR
12	660AC	3.95
14	660AC	4.25
15	440AC	3.85
15	1000	4.10
15	1500	6.35
20	330AC	3.25
20	4000	PUR
24	500	1.98
28	1000	5.95
30	2500	13.50
32	600	3.85
42	600	4.75
50	330AC	6.50
80	4000	45.50

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Mfd	Wvdc	Price
.00001	600	.20
.000024	2500	.35
.000025	1200	.29
.00003	600	.24
.00003	1200	.28
.00003	2000	1.25
.00003	2500	.35
.000047	2500	.30
.00005	600	.23
.00005	1200	.29
.00005	2500	.33
.00005	3000	1.25
.000051	5000	1.75
.00007	2500	.26
.000075	5000	1.45
.0001	600	.24
.0001	1200	.27
.0001	2500	.36
.0001	5000	1.95
.00015	600	.23
.00015	2500	.33
.00015	5000	1.95
.0002	600	.23
.0002	1200	.29
.0002	2500	.34
.0002	5000	1.95
.00025	600	
.00025	1200	.19
.00025	2500	.35
.00025	5000	1.95
.00027	1200	.27
.00027	2500	.36
.0003	600	.23
.0003	2500	.36
.0004	600	.23
.0004	1200	.29
.0004	2500	.29
.0004	5000	1.95
.00047	2500	.40
.0005	600	.23
.0005	1200	.29
.0005	2500	.39
.0005	3000	1.25
.0005	5000	2.45
.001	600	.23
.001	1200	.32
.001	2500	.49
.001	4500	1.65
.001	5000	2.25
.001	8000	3.98
.0015	600	.23
.0015	2500	.53
.0015	5000	2.25
.002	600	.27
.002	1200	.39
.002	2500	.63
.002	5000	2.25
.002	6000	2.40
.0024	5000	2.25
.0025	600	.28
.0025	1200	.43
.0025	2500	.65
.003	600	.31
.003	1200	.52
.003	2500	.73
.003	3000	1.65
.003	5000	2.25
.004	600	.29
.004	1200	.49
.004	2500	.91
.005	600	.35
.005	1200	.45
.005	2500	.98
.005	3000	1.65
.006	600	.36
.006	1200	.55
.006	3500	1.65
.0062	2500	.94
.0075	3000	1.75
.008	600	.35
.008	1200	.57
.01	600	.48
.01	1000	.50
.01	1200	.69
.01	1250	.69
.01	2500	.94
.012	1200	.64
.014	600	.45
.014	1200	.64
.015	600	.55
.015	2000	1.75
.02	600	.21
.02	1200	.99
.02	2000	.98
.025	600	.45
.03	600	.65
.03	1200	1.18
.03	2000	1.98
.039	600	.67
.05	1500	1.95
.025	250	1.95
.4	600	.25
2x.1	250	1.98
.115	2000	4.65

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OA4G	1.00	4C35	17.50	VX-33A	5.00	446B	1.25	5638	6.50
OA5	3.50	4E27	7.00	35T	3.00	450TH	35.00	5639	6.00
OB2	.60	4J38	100.00	35TG	3.00	450TL	35.00	5639A	6.50
OB3/VR90	.75	4J39	100.00	VX-41	5.00	464A	2.00	5640	6.50
OC3/VR105	.60	4J46	25.00	FP-54	25.00	CK-503AX	.75	5641	5.00
OD3/VR150	.60	4J52	50.00	HK-54	3.00	GL-575A	10.00	5642	1.00
EL-C1A	6.00	4J61	100.00	VX-55	7.00	631-P1	6.00	5644	6.50
1AD4	.90	4X100A	10.00	FG-57	10.00	WE-701A	1.50	5645	5.50
1AE4	1.00	4X150A	18.50	RK-60/1641	1.00	707B	2.00	5646	4.00
1AF4	2.50	4X500F	50.00	RK-61	2.25	715B	2.50	5647	5.00
1AG5	2.00	5A6	2.00	RK-65/5D23	6.50	715C	10.00	5650	60.00
1B22	1.00	5ABP1	20.00	FG-67	8.00	717A	.35	5651	1.35
1B23	2.00	5AP1	5.00	HY-69	2.00	719A	15.00	5651WA	3.50
1B24	6.00	EL-5B	5.50	RK-73	.75	721A	.50	5654	1.35
1B35	3.50	5BP1	2.50	RK-75/307A	.50	721B	7.00	5656	6.00
1B35A	7.50	5BP1A	7.50	75TL	7.50	723A/B	7.50	5663	.95
1P21	35.00	5BP2A	5.00	FG-81A	3.50	WE-725A	2.50	5670	1.85
1P22	5.00	5C22	25.00	FG-95	15.00	726A	4.50	5672	1.00
1P28	7.50	5CP1	2.00	100R	2.50	726B	15.00	5675	7.00
2AP1	3.00	5CP1A	7.50	100TH	5.00	726C	20.00	5676	1.00
2AP1A	6.00	5CP7	6.00	VU-111S	1.00	802	2.50	5678	1.00
2C36	35.00	5CP7A	8.00	WE-121A	1.50	803	2.50	5685	12.00
2C39	5.00	5CP11A	9.50	WE-122A	1.50	804	7.50	5686	2.00
2C39A	10.00	5CP12	10.00	WE-123A	2.50	805	5.00	5687	2.85
2C40	8.00	5FP14	6.50	WE-124A	3.50	807	1.15	5687WA	5.50
2C42	8.00	5GP1	3.50	VT-127	1.50	807W	1.50	5691	4.50
2C43	8.50	5HP1	2.00	F-128A	7.50	807WA	5.00	5692	5.00
2C46	5.00	5HP1A	10.00	VXR-130	1.50	808	1.00	5693	4.50
2C50	6.00	5J29	4.00	VT-158	10.00	809	2.00	5696	1.00
2C51	3.00	5J30	4.00	FG-172	15.00	810	10.00	5703	1.00
2C52	2.75	5JP1	8.50	FG-190	2.50	811	3.00	5719	2.00
2C53	10.00	5JP2	5.00	HF-200	10.00	812	2.50	5720	15.00
2D21	.70	5JP2A	7.50	CE-203	5.00	813	10.00	5725	2.25
2D21W	.90	5JP4	5.00	203A	2.50	814	2.00	5726	.75
2E22	2.50	5JP5A	10.00	WE-211D	8.00	815	.90	5727	1.25
2E24	2.25	5JP11A	10.00	233	250.00	816	1.25	5728	8.00
2J21A	2.00	5LP1	8.00	CE-235A	5.00	826	.75	5734	12.50
2J26	2.50	5LP2A	10.00	FG-235A	55.00	828	9.00	5740	25.00
2J50	35.00	5R4GY	1.25	WE-242C	10.00	829	3.50	5750	2.50
2J51	150.00	5R4WGY	2.50	QK-243	50.00	829B	8.50	5751	2.50
2J52	50.00	5RP1A	17.50	WE-244A	7.50	832	2.50	5755	7.50
2J53	2.50	5RP11A	35.00	WE-245A	6.50	832A	5.00	5762	125.00
2J54	25.00	5SP1	50.00	WE-249B	3.50	836	1.25	5763	1.15
2J55	35.00	5X3	2.50	WE-249C	2.50	837	1.25	5771	275.00
2J56	50.00	5XP1	50.00	250R	5.00	845	3.00	5787WA	6.00
2J59	50.00	5Z2P7	25.00	WE-251A	50.00	849	25.00	5796	10.00
2J61	15.00	5Z4P11	50.00	WE-253A	2.00	850	10.00	5798	10.00
2J61A	40.00	EL-C6J	12.00	WE-254A	2.50	851	7.50	5800	7.50
2J62	5.00	EL-C6L	6.50	WE-257A	3.00	860	2.50	5801	5.00
2J62A	40.00	EL-6C	7.00	FG-258A	75.00	866A	1.35	5803	7.00
2J64	100.00	6AC7W	.85	WE-262B	5.00	866 JR	1.25	5814	.75
2K25	10.00	WE-6AK5	1.35	FP-265	18.50	868/PJ23	1.50	5814WA	3.50
2K26	35.00	6AK5W	1.25	WE-267B	7.50	869B	50.00	5827	5.00
2K29	25.00	6AL5W	.75	WE-268A	5.00	872A	1.25	5828	7.50
2K30	50.00	6AN5	2.25	WE-271A	5.00	874	.85	5829	1.00
2K33A	57.50	6AQ5W	1.85	WE-274B	.75	884	1.00	5830	85.00
2K34	100.00	6AR6	1.35	WE-275A	3.50	885	.85	5840	3.85
2K35	100.00	6AR6WA	2.50	WE-276A	7.50	902-P1	2.00	5842	15.00
2K41	100.00	6AS6	1.25	WE-282A	2.25	917	1.50	5847	15.00
2K45	30.00	6AS6W	2.25	WE-282B	4.50	918	1.50	5876	7.00
2K47	100.00	6AS7G	3.00	WE-283A	3.50	920	2.00	5881	3.50
2V3G	1.25	6AU6WA	2.50	WE-285A	5.00	922	1.50	5886	2.75
2X2A	.85	6C21	15.00	WE-286A	3.50	923	1.25	5902	4.50
3ABP1	75.00	6F4	2.25	WE-287A	2.00	927	.75	5915	.75
3AP1	2.00	6J4	1.50	GL-299	1.50	931A	3.50	5932	3.50
3AP11A	5.00	6J4WA	2.50	WE-300B	6.00	956	.25	5933	1.50
3B4	1.75	6J6W	1.00	304TH	10.00	958A	.35	5933WA	5.00
3B24	1.00	6K4A	3.50	304TL	15.00	959	1.25	5948/1754	200.00
3B24W	4.00	6L4	3.50	307A	.50	991/NE-16	.25	5962/BS-101	5.00
3B24WA	8.00	6L6WGA	3.75	WE-310A	4.00	CK-1006	2.50	5963	1.25
3B25	3.50	6L6WGB	3.50	WE-311A	4.00	1500T	100.00	5964	1.00
3B26	2.75	6Q5G	2.50	WE-313CD	4.00	1608	4.00	5977	3.00
3B28	4.50	6SJ7WGT	2.00	WE-316A	.50	1611	1.00	5979/BS-1	10.00
3B29	4.50	6SK7W	1.00	WE-323A	9.00	1614	1.50	5980/BS-2	8.50
3BP1	2.00	6SK7WA	2.00	WE-323B	5.00	1619	.30	5981/5650	60.00
EL-3C	4.50	6SL7WGT	1.25	WE-328A	3.50	1624	1.50	6005	1.85
EL-C3J	7.50	6SN7WGT	1.50	WE-336A	4.50	1625	.30	6021A	4.50
EL-C3JA	9.00	6SU7GTY	3.00	WE-338A	4.00	1846	50.00	6037	50.00
3C23	3.50	6X4WA	2.00	WE-339A	10.00	1945	50.00	6038	7.50
3C24	3.50	6X5WGT	1.25	WE-347A	2.50	2000T	150.00	6073	2.00
3C33	6.00	7BP7	3.50	WE-348A	5.00	2050	1.00	6087	4.25
3C45	6.00	7BP7A	7.00	WE-350A	2.50	5528	6.50	6098	2.50
3D21A	3.00	7CP1	5.00	WE-350B	2.00	5550	25.00	6136	2.50
3D22	7.50	7HP7	10.00	WE-352A	15.00	5551	40.00	6189	3.00
3DP1A	5.00	7MP7	10.00	WE-354A	10.00	5552	55.00	6201	3.00
3E22	4.85	10KP7	25.00	WE-355A	10.00	5553	75.00	6280	35.00
3E29	8.50	12A6	.60	371B	1.50	5556	6.75	6328	5.00
3FP7A	2.50	12AP7	50.00	WE-388A	1.50	5557	3.50	8002R	15.00
3GP1	1.85	12DP7	15.00	WE-393A	3.50	5558	4.00	8005	4.50
3HP14	2.00	12GP7	15.00	394A	2.50	5559	10.00	8012A	3.50
3J21	50.00	FG-17	3.50	WE-396A	3.00	5560	15.00	8013	2.50
3J31	40.00	RK-20A	6.75	WE-403A	1.35	5584	3.00	8013A	3.00
3JP1	7.50	HK-24	2.00	WE-404A	15.00	5610	1.00	8020	1.00
3JP12	10.00	HK-24G	3.50	WE-409A	1.25	5632	7.50	8025	1.00
3K27	150.00	26E6WG	2.50	WE-416B	35.00	5633	6.00	9001	.75
3KP1	7.50	26Z5W	3.00	WE-417A	15.00	5634	6.50	9002	.50
3X2500A3	100.00	FG-27A	10.00	WL-417A	2.00	5635	6.00	9003	1.00
4-65A	14.00	FG-32	4.00	WE-418A	15.00	5636	2.75	9005	2.50

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The RDO is a very elaborate radar search receiver greatly improved over the APR-4. The set uses APR-4 tuning units, but is much more versatile, having input metering. D.B. output meter, automatic noise limiter, and greater selectivity and sensitivity. The RDO is recommended when only the very best will do. Input 110v 60 cyc.

AN/ASQ-1 AIRBORNE MAGNETOMETER

This is an airborne chart recording magnetometer. The set consists of an amplifier, oscillator, detector head, chart profile recorder, power supply. The equipment has a sensitivity of 2 gamma. The AN/ASQ-1 records on an Esterline angus recorder disturbance in the earth's magnetic field. An indicator is provided that gives a bearing on a magnetic disturbance. Input is 28v DC. Weight about 130 lbs.

SHORAN

AN/APN-3-AN/CPN-2

The AN/APN-3 and AN-CPN-2 are Precision distance measuring installations. This equipment operates on 225 mc. The range is 250 miles with an accuracy of 25 feet. This equipment is widely used by geological companies for prospecting and mapping. Power input is 110v 400cyo and 28v DC.

AN/GSQ-1 SPEECH SCRAMBLER

This is a unit designed to be attached to either a radio or telephone circuit to scramble speech or code. This equipment utilizes coded cards in each terminal equipment. Unless the properly numbered card is inserted on the receiving end the speech can not be unscrambled. This provides an excellent privacy system. 24 VDC input. Mfg. Western Electric.

AN/TPS-1B

200 MILE AIR SEARCH RADAR

The TPS-1B is a very late type L-band mobile or portable air search radar. This set will detect aircraft up to 200 miles and up to 40,000 ft. The set is composed of small portable carrying cases that are bolted together to make up the set. A 7" P.P.I. and a 5" "A" scope are provided. This set is in use by the Air Force and Marine Corps. Complete sets available. P.O.R.

AN/TPS-3-AN/TPQ-3

Airsearch or artillary shell tracking radar. The AN/TPS-3 is a 600mc airsearch portable radar. The set has a range of 120 miles on aircraft up to 40,000 ft. This set has a 7" P.P.I. and a 5" "A" scope. The AN/TPQ-3 is a modification of the AN/TPS-3 to provide mortar and artillary shell tracking and plotting. A computer is provided to compute shell trajectories and provide information for counterbattery fire. This set is completely portable and can be set up in the field in a few hours. Complete sets avail. P.O.R.

AN/TRC-1-3-4

100 MC RADIO-RELAY EQUIPMENT

The AN/TRC series is a mobile portable set for duplex or simplex radio telephone point to point communication. This set will operate with the CF series carrier systems to provide multi channel operation. The TRC operates on 100 MC with an output of 10-50 watts. The set is crystal controlled. Complete sets avail. with all components. Input 110v 60 cys.

CARRIER EQUIPMENT

CF-1 4 CHAN. VOICE AND TELEG. TERMINAL 115v 230v A.C. 12v D.C.
CF-2 4 CHAN. TELEGRAPH AND TELETYPE TERMINAL 115v 230v A.C. 12v D.C.
CF-3 4 CHAN. INTERMEDIATE REPEATER 115v, 230 A.C. 12v D.C.
CF-4 CARRIER CONVERTER. Used to adapt the CF-1 and 2 for operation on a simple 2 wire trans. line instead of using spiral 4. 115v, 230v A.C. 12v D.C.
TH-1 TELEGRAPH TERMINAL

SCR-536 HANDI-TALKIE

Freq. range 3.7.5 5mc crystal controlled battery operated handi-talkie. The range of this equipment is approximately 2 miles. We can supply these sets to your specified freq. Completely reconditioned and guaranteed.

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SCR-291-A 1.5-20 mc direction finder
SCR-300 40-48 mc walkie-talkie
SCR-399 1.5 mc-18 mc mobile radio
SCR-499 1.5 mc-18 mc field radio
SCR-508-528 28 mc FM field radio
SCR-608-628 30 mc FM field radio
SCR-506-A field radio
SCR-694 field radio
AN/ARN-6 Airbourne D.F.
AN/ARN-7 Airbourne D.F.
AN/APN-9 Loran
AN/APA-11 pulse analyzer
AN/APA-17 300-10,000 direction finder
AN/APR-1 38-4,000 mc receiver
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AN/APR-6 3,000-10,000 mc receiver
AN/ART-3 THRU 11 jammer
AN/ARQ-1 THRU 12 jammers
AN/APQ-2 THRU 9 jammers
AN/PRT jammers
AN/ARC-1 100-156 radio set
AN/AN/ARC-12 200-325 mc radio set
AN/ARC 27 200-400 mc radio set
AN/APS-2 THRU 34 airbourne radar
AN/PRC-6 handi-talkie FM
AN/PRC-8, 9, 10 walkie talkie FM
AN/GRC-9 field radio
AN/GRC-3-8 FM field mobile radio sets
AN/TXC-1 page printing facsimile
AN/TRC 7 100-156 mc walkie talkie
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C5B	.49	OB2	.89	2K25	18.99	5BP4	2.99	15E	1.25	**274B**	**1.79**	706C	17.50	826	.75	1625	.29
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CK-551AX/2E41	1.79	**1B24**	**5.99**	**2K33A**	**59.95**	5CP1	3.99	26A7/GT	2.99	276A	7.25	707A	3.55			1629	.29
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EM-34GA	39.50	**2AP1A**	**6.44**	2V3/G	1.39	5FP7	3.99	10Y	.39	304TL	13.95	714AY	24.95	837	1.99	1644	.48
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FG-105	**14.99**	2C21	.49	3A5	.69	5JP4	14.99	35T	4.99	310A	3.99	715C	14.50	843	.49	2050W	2.40
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FG172	**24.95**	2C26	.39	**3AP11A**	**4.95**	5J33	65.00	53A	2.29	329A	4.69	717A	.49	851	16.50	5651	1.39
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HK-24	3.69	2C33	.69	3B23	3.25	5NP1	6.99	RK65/5D23	**14.95**	350B	2.99	719A	14.65	861	19.00	5656	3.25
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HY-65	1.20	2C39A	11.50	**3B24W**	**4.99**	6C21	19.95			388A	1.49	721A	1.49	865	.49	5686	1.79
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RK-73	.69	2J21	2.99	3C45	6.25	6AS6	1.19	215A	3.25	CK-508AX	1.10	801A	.42	918	1.99	5963	1.19
RX-233A	.69	2J21A	4.95	3CP1	2.25	6AS7/G	2.49	217A	2.99	CK-521AX	1.10	802	2.89	927	1.45	5964	.74
VT25/10	.49	2J22	4.99	3D23	4.99	6BM6	39.50	217C	4.99	527	14.50	803	2.69	931A	2.99	5977	3.89
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VR-105	.79	2J61	16.40	4C28	35.50	12AT7	.85	264C	3.90					1608	2.99	9002	.69
		2J62	**9.60**	4E27	9.95	12DP7A	18.95	269A	13.50					1613	.95	9004	.19
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OC3	.60	3GP1	2.00	101D-W.E.	2.50	422AW.E.	7.50	884	1.00
OD3	.55	3HP14	1.75	101F-W.E.	2.50	446B	1.50	891	75.00
1B26	1.25	3JP7	3.45	VU111S	.75	464A	2.00	893A	375.00
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1L33	22.00	4J29	75.00	F-128A	7.50	CK503AX	1.25	1616	.35
1P23	1.75	4J30	90.00	GL-152	10.00	CK505AX	1.00	1619	.25
1P41	2.50	4J33	75.00	FG-154	10.00	CK506AX	1.00	1625	.25
2C22	.35	4X150A	20.00	204A	25.00	CK507AX	1.25	1626	.25
2C26	.25	5BP1	1.25	AV209	5.00	CK522AX	1.25	1629	.10
2C27	5.00	5BP4	3.50	215AW.F	20.00	WL532A	.25	1631	1.00
2C33	.50	5B21	1.25	217C	1.75	705AW.E.	.65	1632	.20
2C34	.25	5C22	17.50	220B	90.00	706AY	15.00	1680	1.00
2C39A	10.00	5D21	5.00	221A	100.00	707B	2.50	1846	50.00
2C46	5.00	5D23	10.00	222AW.E.	100.00	713A	.25	2051	.65
2E22	2.75	5D24	15.00	249B	3.00	715A	2.00	5517	1.25
2E25	2.50	5JP2	6.00	250TL	12.50	717A	.35	5518	275.00
2E36	1.35	5MP1	2.75	253AW.E.	2.00	718CY	25.00	5650	50.00
2J49	25.00	5R4WGY	2.50	254A-W.E.	2.50	720BY	35.00	5651	1.25
2K26	35.00	5SP7	50.00	259B	5.00	721A	.75	5672	1.00
2K33	100.00	5SP11	50.00	274AW.E.	2.50	722A	.75	5676	1.00
2K33A	50.00	5SP11A	50.00	285AW.E.	5.00	724B	.50	5693	4.50
2K33B	100.00	6AC7W	1.00	313C	3.00	730A	5.00	5719	1.50
2K37	100.00	6C21	15.00	348AW.E.	4.75	801A	.25	5726	.75
2K39	75.00	6X4W	1.00	356BW.E.	3.00	803	2.00	5744	1.00
2K56	50.00	7BP7	2.75	368AW.E.	2.00	805	5.00	5814	1.00
2X2	.15	9GP7	10.00	374AW.E.	1.75	807	1.25	5825	6.25
EL-3C	3.45	12DP7	10.00	375AW.E.	10.00	811	3.00	5827X	5.00
3B27	3.75	12DP7A	20.00	387AW.E.	5.00	813	9.50	5838	5.00
3BP1	1.25	15R	35.00	394A	2.50	829B	8.45	5933	1.50
3C37	20.00	28D7	1.00	402AW.E.	12.50	832A	6.25	6035	10.00
3CP1	2.50	FG32	3.50	404AW.E.	15.00	836	1.25	6038	5 00
3CP1S1	2.00	RK-34	.50	416AW.E.	Q	841	.29	6098CT	2.00
3DP1S2A	7.50	L40CT	2.00	416BW.E.	Q	842	1.00	6099	1.00
3D21A	3.25	HK54	4.00	417AW.E.	15.00	843	.35	8068	3.00
		RK59	1.75	419AW.E.	90.00	845	5.00	8012	1.00
		RK60	1.25					D178461W.E.	Q

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I-166
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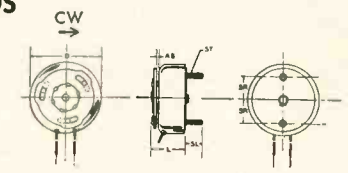
AS Axial Stroke (Approx)		.0315"	.055"	.066"
SL Stud Length		7/16"	1/2"	5/8"
SR Stud Radius		7/16"	5/8"	23/32"
ST Stud Thread		5-40	8-32	10-32
Weight (Approx-Bare)		3-1/2 oz	9 oz	18 oz
Torque lbs-inches‡		1.0	4.0	7.5
Finish	Nickel or Black Nicke			



‡ The Torque values given are average and are based on the ampere-turns for a normally intermittent duty cycle.

In the Ledex rotary solenoid the magnetic pull moves the ormature along the solenoid axis. This linear action is effectively converted into a rotary motion by means of ball bearings on inclined races.

Listed below are Ledex solenoids from our stock. These all have a 45° stroke. Both continuous and intermittent duty voltages are indicated. The intermittent voltage listed is for ten seconds or less and the "off" time is nine times the "on" time. Under these circumstances the units should be installed so that there is free circulation of air around them.

Type	Rot.	Stroke	Wire Size	Ohms	Volts DC Cont.	Volts DC Int.	Return Spring	Finish	X Features	Stk #	Ea*
BD6SR45-22X7X8	CW	45°	22	2.2	8.3	26	yes	Cad.	Dust Cover	R1219	3.75
BD5SL45-23X3	CCW	45°	23	2.0	6.0	19	no	Blk	5/16" L.Shaft Extension	R1220	2.00
BD5SL45-25X3	CCW	45°	25	5.0	9.5	30	no	NKL	5/16"L. Shaft Extension	R824	2.00
BD5SL45-26X3	CCW	45°	26	7.7	12	38	no	NKL	5/16"L. Shaft Extension	R825	2.00
BD5SR45-33X2	CW	45°	33	185	60	190	no	NKL	Forward Engaging Pawl	R597	2.00
BDOER45-29X5	CW	45°	29	5.0	5.2	16	no	Blk	Offset Drive Pin	R827	1.50
BDOER45-32X5	CW	45°	32	22	11	32	no	NKL	Offset Drive Pin	R826	1.50

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All units with shafts are supplied with hardware for mounting standard wafer switches.

Type	Shaft Rot.	Shaft Length	Stroke	Self Pulsing Deck	Wire Size	Volts Ohms	Volts Cont.	Volts Int.	X Features	Stk #	Ea*
BD3ER30-28X8	CW	7/8"	30°	yes	28	8	8.4	26.5		R1222	4.75
BD3ER30-28X8X9	CW	7/8"	30°	yes	28	8	8.4	26.5	Dust Cover	R1223	5.00
BD3ER30-37X9	CW	1-1/4"	30°	no	37	426	67	210	Mtg Flange	R1224	5.00
BD5SR30-33X6	CW	1-1/4"	30°	yes	33	176	60	190	Threaded Holes	R1225	4.00
BD5SR30-34X6	CW	1-1/2"	30°	yes	34	270	76	240	Threaded Holes	R1226	4.00
BD5SR45-26X9	CW	7/8"	45°	yes	26	5	8.4	26.6		R1227	5.00
BD5SR30-26X7	CCW	1-1/2"	30°	yes	26	5	8.4	26.6	Terminal Board	R1228	5.50
BD5SR30-26X7	CCW	1-1/2"	30°	yes	26	5	8.4	26.6	Mtg Flange	R1229	5.50

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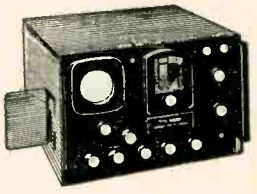

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DELCO APPLIANCE 5069625—27 VDC—Gear reduction to 120 RPM output. Governor controlled speed. Size: 1⅜" x 4½". Shaft size: ¼" x ⅜". Wt. 8 oz.

HOLTZER CABOT Type 2505—115 VAC 60 Cy. 9 Watt 1.9 RPM Reversible 75 oz. torque. Has multiple disc coder wheel with micro switch mounted on bracket assy. Overall size: 3⅜" x 4¾" x 4". Wt. 3 lb. 2 oz. **$9.95**

AIR ASSOCIATES EE1530—Gear reduction, 24 VDC @ .8 A. 25 lb. inch torque, 5 RPM Reversible. Size: 4½" x 3½" x 5½". Keyed shaft: ½" x 1¾" with a 4" arm attached. Wt. 5 lb. **$7.95**

JOHN OSTER Shunt Motor B-9-1—27½ VDC @ .7 A. 5600 RPM. Aluminum cased motor and gear assy. Motor is flange mounted to gear case. Two gear reductions 22 and 51½ RPM on ¼" x 1¼" shafts. Size: 2¾" x 3" x 7". Wt. 1 lb. 14 oz. **$3.95**

BENDIX LM108J—24 VDC 1/25 HP—15000 RPM Series Motor. Geneva Loc. Actuator. Shaft rotates ¼ revolution and stops, is locked in place until next contact is made, then the cycle is repeated. Time per cycle: approx. 3 seconds. Size: 4" x 2¼" x 5½". Shaft size: ¼" x ½". Wt. 1 lb. 14 oz. **$7.95**

24 VAC Gear Motor No. 14-343—3 RPM output. Size: 5" x 2½" x 1¼". Shaft size: 5/32" x ⅝". Wt. 1 lb. 2 oz. **$1.95**

New List— *Just Out — Including many other Motors, Blowers, Dynamotors, etc. Free—Write for copy today!*

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FOR MORE QUALITY-PER-DOLLAR, BUY RECONDITIONED

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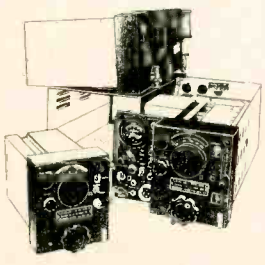
WE WILL QUOTE ON NEW AND USED TOP-QUALITY COMMERCIAL BRANDS AND SELECT MILITARY SURPLUS ITEMS IN OUR CHOICE STOCK, TO YOUR NEEDS.



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Complete with all five Tuning Units, covering the range 38 to 4,000 Mc; wideband discone and other antennas, wavetraps, mobile accessories, 100 page technical manual, etc. Versatile, accurate, compact—the aristocrat of lab receivers in this range. Write for data sheet and quotations.

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434 PATTERSON ROAD DAYTON 9, OHIO

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Diamond Replacement Needles Gtd.

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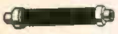

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100 Meg/10w/15KV MVP .... $3.50 @; 12/$36
Deduct 10% Disc Qtys—100. May Be Asst'd

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LAB & HIFI, LAB Built & ready to work. HIFI uses "SOLA" constant voltage Filament & Power Xfmr w/rectifier tubes. Low Resistance Brute Force Filter. Furnishes 400VDC @ 250 ma from filter system & 3% regulated & 12V @ 5A filtered DC for filaments. 45 lbs. "TAB" $39.00

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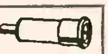

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IN21 .... 5 for $1
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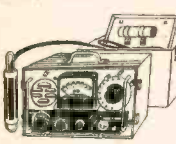
1N22 $1 @, 1N21B $2 @, 1N25 $5 @, 1N32 $12 @
CK5697/CK570AX Submin Triode $2 @, 6/$10



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TS174U F.M. 20 to 250 mcs AC operated ... $265
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0-135V/3A 10.63
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Cased/0-270V/3A 22.10
Uncased/0-270V/3A 17.00
Cased/0-135V/15A 39.10
Cased/0-270/9A 39.10
Uncased 0-27V/7.5A 51.64
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Cased 0-270V/20A 124.95
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TUBES

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OA2	$ .74	2K29	28.85	6BL7	Q	245A	15.00	717A	.29
OA3/VR75	.89	2K30	100.00	6C4	.35	250TL	12.00	723AB	8.00
OB2	.60	2K33	120.00	6F4	2.99	252A	7.95	726B	25.00
OB3/VR90	.84	2K39	100.00	6H6	.49	254A	4.00	726C	21.75
OC3/VR105	.59	2K41	95.00	6J7	.85	259A	Q	807	1.19
OD3/VR150	.57	2K45	50.00	6L6	1.55	274B	1.95	808	1.75
1AD4	1.00	2K50	165.00	6Q5G	3.65	275A	3.45	809	2.75
1AH4	1.00	2K55	15.00	6SL7GT	.76	276A	8.45	811	3.85
1B3GT	.69	2V3G	.98	6SN7GT	.72	303A	6.75	812	3.85
1B23	5.00	3A4	.58	6SU7GT	2.75	304TH	11.00	813	10.00
1B24	4.95	3A5	.39	6Y6GT	.59	304TL	18.00	814	2.98
1B26	1.00	3B4	2.00	6X4	1.00	307A	.59	815	2.25
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1B35	4.50	3B28	5.00	8D21	150.00	322	6.90	832A	5.00
1B37	6.00	3C22	72.00	12AL5	.60	323	10.50	837	1.95
1B41	50.00	3C33	7.50	12A6	.39	324A	Q	866A	1.25
1B42	4.00	3C34	4.95	12AU7	.50	348A	6.90	872A	1.29
1B46	1.25	3C45	8.00	12AX7	.72	349A	10.00	875A	18.00
1B56	30.00	3D21A	3.95	12AY7	.65	350	3.00	889A	75.15
1B63	19.00	3D23	4.98	12H6	.63	353	3.75	931A	4.50
1D21	4.95	3K23	150.00	12K8	.69	354	15.00	991	.20
1L4	.58	4B27	2.50	SRC12	200.00	355	12.00	1005	.35
1T4	.65	4B36	4.75	15E	1.25	356	4.00	1620	3.00
1Z2	1.95	4J31	215.00	NE16	.25	359	1.70	1625	.30
2A3	.98	4J51	215.00	SRX16	125.00	366	Q	1629	.30
2A4G	1.98	4J52	50.00	FG17	2.60	368AS	3.95	2050	.95
2C43	9.00	4J53	Q	24G	3.00	371B	.85	5517	2.10
2C44	.30	4X150A	22.50	25A6	1.65	380A	.80	5844	.85
2C51	3.95	4X500A	65.00	25T	3.35	387A	4.00	5870	98.00
2C52	2.75	5AW4	1.17	28D7	.75	388A	1.15	5875	2.05
2D21	.75	5C22	19.10	35T	3.00	394A	1.85	5879	1.50
2E22	1.89	C5B	1.00	HK54	4.00	395A	4.25	5881	2.95
2E30	1.95	5D21	7.95	RK59	1.88	399A	4.50	5965	1.85
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2E32	1.00	5T4	1.45	QK81	50.00	421A	6.90	8011	1.50
2E35	1.95	C6A	6.59	82	1.20	460	17.00	8013A	3.95
2E36	2.15	6AG7	1.14	83	2.25	WE417A	15.00	9001	.80
2E43	1.50	6AH6	1.29	83V	1.25	CK502	1.70	9003	1.25
2G21	1.75	6AK5	.75	FG105	11.00	CK503	1.00	9004	.28
2J21	2.95	6AK6	.55	FG166	6.75	CK525	2.95	5BP1	2.49
2J27	5.99	6AN5	2.25	FG172	19.50	CK526	1.75	5BP4	2.95
2J34	14.50	6AQ5	.45	FG190	7.00	CK531	1.89	5CP1A	9.00
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2J55	35.00	6AS6	1.20	204A	25.00	538DX	.98	5LP2	27.50
2J56	40.00	6AS7G	2.50	RX215	27.00	539DX	2.50	5LP7A	45.00
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2K23	12.50	6BD4A	8.73	242C	12.50	715B	3.85	7BP7	9.00
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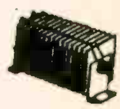
TOP $$$$ PAID FOR LAB TEST EQUIPMENT Kay, G.R., H.P., L&N, G.E., RCA, DuMont, Tektronix, Weston, Boonton, Measurements, Ballentine & others.

NEW "TABTRON" SELENIUM RECTIFIERS*



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Max Amp	18VAC* 14VDC	36VAC* 28VDC	45VAC* 42VDC	72VAC* 56VDC	130VAC* 100VDC	226VAC 217VDC	Ctr Tap AC/DC 30/12	3 Phase 120VAC 150VDC	Bridge 240VAC 300VDC
1	$1.40	$2.80	$3.70	$4.45	$7.40	$25.00	$2.40	$17.10	$33.25
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3	2.90	4.10	5.75	7.80	12.70	37.00	3.05	20.00	49.50
4	3.50	6.40	11.25	14.30	25.00	45.00	3.40	21.70	55.75
6	3.95	7.70	12.75	17.25	29.65	59.00	3.70	24.00	59.90
10	5.85	11.35	19.40	24.75	41.25	85.00	5.45	42.40	94.25
12	7.20	14.25	22.00	29.50	43.85	100.00	6.80	Q	Q
20	13.00	25.00	37.00	48.00	78.00	161.00	9.15	Q	Q
24	15.00	28.50	44.25	57.50	Q	Q	Q	Q	Q
30	17.85	34.25	56.25	70.50	Q	Q	Q	Q	Q
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50	29.40	54.00	105.00	115.00	Q	Q	Q	Q	Q

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230 to 115 V Autoformers

For 220v/50cy Input. To 110-120V or Step up. † With Cord Plug & Receptacle.
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T28V12ACC	12 Amp (1% Ripple)	$160
T28V12A2CC	12 Amp 0.01% Ripple	$220
T28V24A†	0-28 VDC at 24 Amp	$155
T28V24ACC†	24 Amp (1% Ripple)	$225
T28V24A2CC†	24 Amp 0.01% Ripple	$310
T28V50A†	0-28 VDC at 50 Amp	$285
T28V50ACC†	50 Amp (1% Ripple)	$410
T28V100A†	0-28 VDC at 100 Amp	$500
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Meters; All Others 4" Meters

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CE156M 6000MFD 15V ...... $2 @; 2/$3; 10/$12
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"TABTRAN" Rectifier Chokes

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CR6003/ 5 Amp/.07 HY/.6 Ohm 7.95
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†Wndgs In Series at Ratings shown; Parallel 2X Current: Voltage 0-9-15-18.
*Dual Pri 115 & 220V 60 cy

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MULTIPOT 25, 100, 300, 2000, 5000, 10000, 20000 Ohms/0.5%/ 10 Turns Equiv. HELIPOT
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GR#314/50,000 ohm/8Watt .... 2.45 @
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TRIMPOT Miniature 2,000 ohms CW .. 1.50 @
Fairchild #746/2.5Watt/±.5%, 5K, 9.5K, 10K, 20K, 40K .... DUAL $4 @, TRIPLE $6 @

NEW MICA CONDENSERS GTD.

MFD	WVDC	Price
.03	600	45c; 100/$35
.01	1200	35c; 100/$25
.001	1200	20c; 100/$15
.002	1200	35c; 100/$30
.015	2500	75c; 100/$50
.002	2500	45c; 100/$35

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Sold on Money Back Guarantee

7" REEL, 1200 FOOT Highest Quality Precision Coated & slit, FERRO-SHEEN processed quality controlled, constant output. Noise Free Plastic tape. Splice Free. Freq. 7½ IPS 40-15 KC Oxide Wnd In. "TAB" SPECIAL @ $1.59 EA; 3 @ $1.50 EA; 12 FOR $1.45 EACH....1000's SOLD
New 1st Quality "MYLAR" 2400 ft.—7" Reel, Ferro-Sheen processed Recording Tape @ $4.49 "TAB" Special @ .... 3/$12; 12/$45

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Heineman El. Mag. Bkr. Amp: 3, 5, 9, 10, 12, 35, 80 @ $1.50 EACH 12 FOR $16 .... 50 FOR $50
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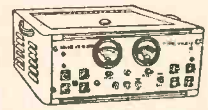
Klixon Thermal Push Button Bkrs. Amps: 5, 10, 15, 25, 30, 35 @ 59c EA; 8/$4; 25 FOR $10.



TEST EQUIPMENT

G.E. YYZ-1 Decade Scaling Unit for high speed

COUNTING OR NUCLIONICS, contains two Decade scaling ckts count rate 5x106/R.T./0.1 Mu Sed, 115V/60cy operation $150

G.E. MICROWAVE Sig Generator 9 to 11cm/3333 to 2724 mcs op/115v/60cy. CW or Pulsed. direct reading $200

WESTON Model 45 Range/0-150VDC/Lab. Std. $45
LAVOIE Model 105 MW/freq Meter/300 to 600 mcs $45
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F3 or CW3 Coils per Set (3) $10

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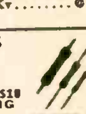

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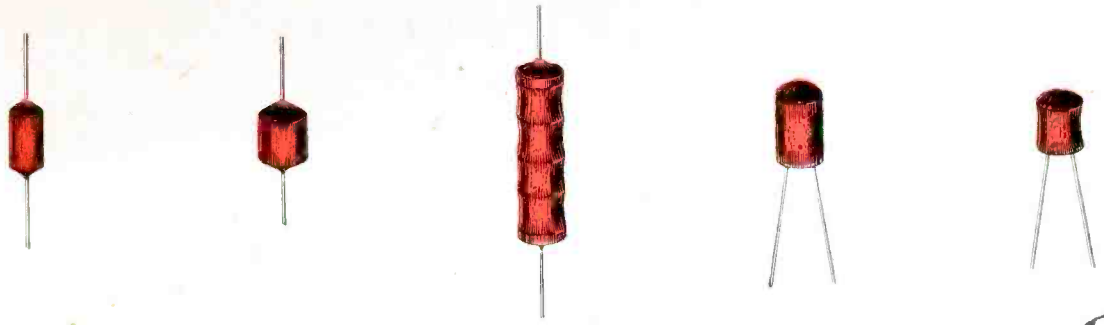

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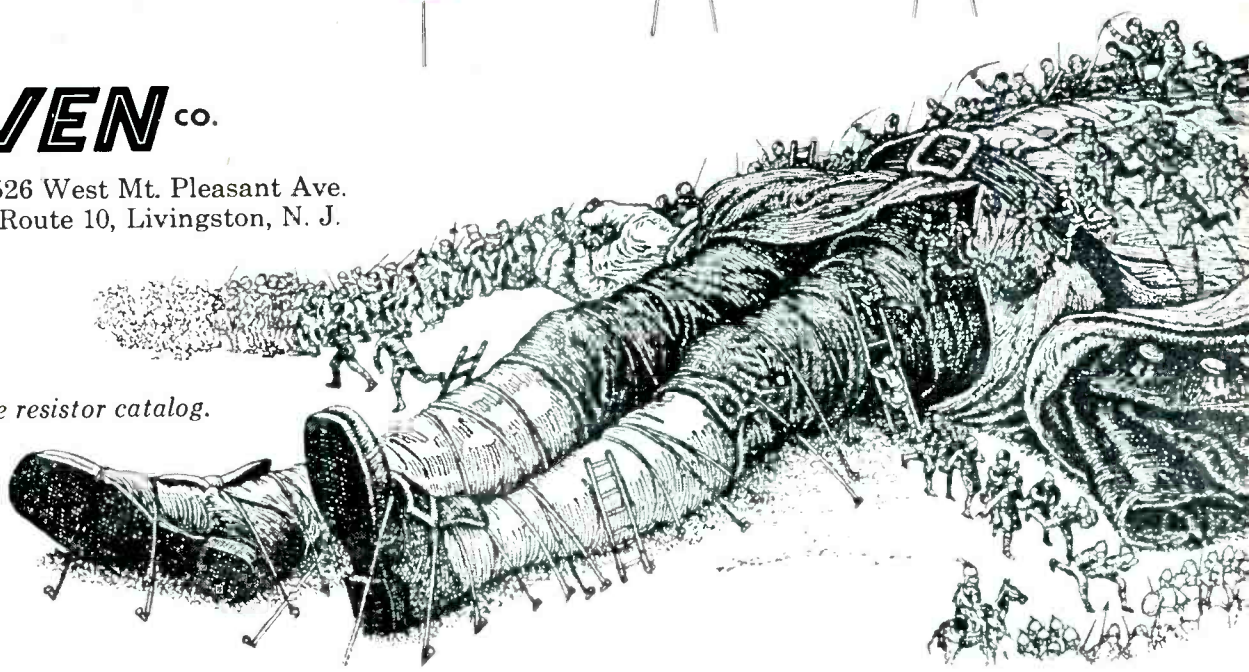

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