

RADIOTRONICS

AMALGAMATED WIRELESS VALVE COMPANY LIMITED



In this issue:—

6L6 Beam Power Valve, Metal Type
6F5 Additional Data
Bases and Dimensions

Technical Bulletin No. 62

Issued 6th May, 1936

Editor's Note:—The information on the use of Radiotron 1C4 as a single I.F. amplifier has had to be left over from this issue and will be given in Technical Bulletin No. 63, which will be available very shortly.

RADIOTRON 6L6

THE NEW BEAM POWER AMPLIFIER

(Tentative Data)

The Radiotron 6L6 is a power-amplifier valve of the all-metal type for use in the output stage of radio receivers, especially those designed to have ample reserve of power-delivering ability. This new valve provides high power output with high power sensitivity and high efficiency. The power output at all levels has low third and negligible higher-order harmonic distortion.

These distinctive features have been made possible by the application of fundamentally new design principles involving the use of directed electron beams. The beams of high electron density are produced by constraining the electrons with potential fields set up by the valve electrodes arranged to give the desired effects.

Primary features resulting from this arrangement are that the screen does not absorb appreciable power and that efficient suppressor action is supplied by space-charge effects produced between the screen and the plate. Secondary features are high power-handling ability, high efficiency, and high power sensitivity. Furthermore, large power output is obtainable without any grid current flowing in the input circuit.

In the design of the 6L6, the second-harmonic distortion is intentionally high in order to minimize third and higher-order harmonics. Experience has shown that second harmonics are far less objectionable in the audio-frequency output than harmonics of higher order. The second harmonics can easily be eliminated by the use of push-pull circuits, while in single-valve, resistance-coupled circuits, they can be made small by generating out-of-phase second harmonics in the pre-amplifier.

Because of the high power sensitivity of the 6L6, it is practical to use circuits which avoid the troublesome effects of loud-speaker resonance and variable impedance. In such circuits, the 6L6 not only maintains its high efficiency, but also provides power sensitivity and stability equal to or better than that of a triode.

BEAM POWER AMPLIFIER

(TENTATIVE DATA)

Heater Voltage (A.C. or D.C.)	6.3 Volts
Heater Current	0.9 Ampere
Maximum Overall Length	4-5/16"
Maximum Diameter	1-5/8"
Base	Small Octal 7-Pin

STATIC AND DYNAMIC CHARACTERISTICS.

Heater Voltage	6.3 Volts	Plate Resistance	22500 Ohms
Plate Voltage	250 Volts	Mutual Conductance	6000 Micromhos
Screen Voltage	250 Volts	Plate Current	72 Milliamperes
Grid Voltage	-14 Volts	Screen Current	5 Milliamperes
Amplification Factor	135		

SINGLE-VALVE CLASS A₁ AMPLIFIER

Subscript 1 indicates that grid-current does not flow during any part of input cycle.

Plate Voltage	375 max. Volts
Screen Voltage	250 max. Volts
Plate and Screen Dissipation (Total) †	24 max. Volts Watts

Typical Operation:—

Heater Voltage ‡	6.3	6.3	6.3	6.3 Volts
Plate Voltage	375	250	300	375 Volts
Screen Voltage	125	250	200	250 Volts
	Fixed Bias.	Self Bias.*	Fixed Bias.	Self Bias.*
D-C Grid Voltage °	-9	-9	-14	-13.5
Peak A-F Grid Voltage	8	8.5	14	14
Zero-Signal D-C Plate Current	24	24	72	75
Max-Signal D-C Plate Current	26	24.3	79	78
Zero-Signal D.C. Screen Current	0.7	0.6	5	5.4
Max-Signal D-C Screen Current	1.8	2	7.3	7.2
Load Resistance	1400	2500	4500	4500
Distortion:				
Total Harmonic	9	10	11	14.5 per cent.
2nd Harmonic	8	9.7	10.7	11.5 per cent.
3rd Harmonic	4	2.5	2.5	4.2 per cent.
Max-Signal Power Output	4.2	4	6.5	6.5

PUSH-PULL CLASS A₁ AMPLIFIER

Plate Voltage	375 max. Volts	Fixed Bias.	Self Bias.		
Screen Voltage	250 max. Volts	32	35.6 Volts		
Plate and Screen Dissipation (Total) †	24 max. Watts	120	120 Milliamps.		
Typical Operation—2 Valves:		140	130 Milliamps.		
Values are for 2 Valves.		10	10 Milliamps.		
	Fixed Bias.	Self Bias.	16	15 Milliamps.	
Heater Voltage ‡	6.3	6.3 Volts	5000	5000 Ohms	
Plate Voltage	250	250 Volts	Distortion:		
Screen Voltage	250	250 Volts	Total Harmonic	2	2 per cent.
D-C Grid Voltage °	-16	-16* Volts	3rd Harmonic	2	2 per cent.
			Max-Signal Power Output	14.5	13.8 Watts

† Precautions should be taken to insure that dissipation rating is not exceeded with expected line-voltage variations, especially in the case of fixed-bias operation. Fixed-bias values up to 10% of each typical screen voltage can be used without increasing distortion.

‡ The heater should be operated at 6.3 volts. Under no condition should the heater voltage ever fluctuate so that it exceeds 7.0 volts. The potential difference between heater and cathode should be kept as low as possible.

* With no signal.

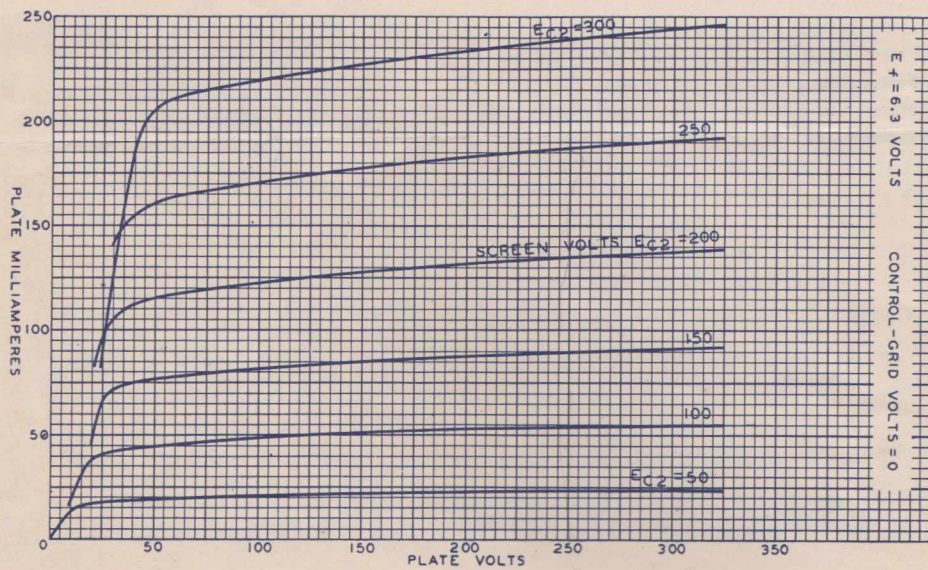
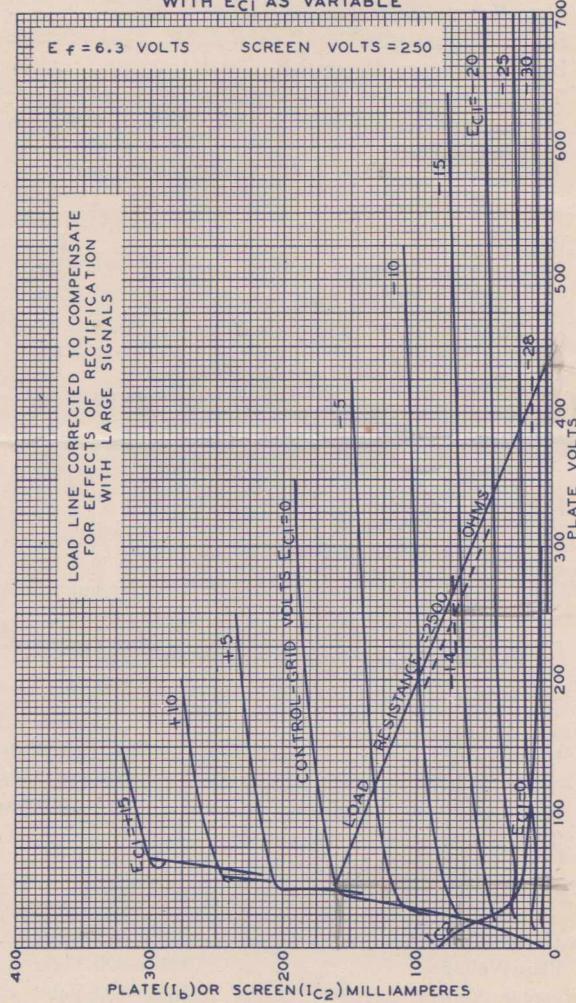
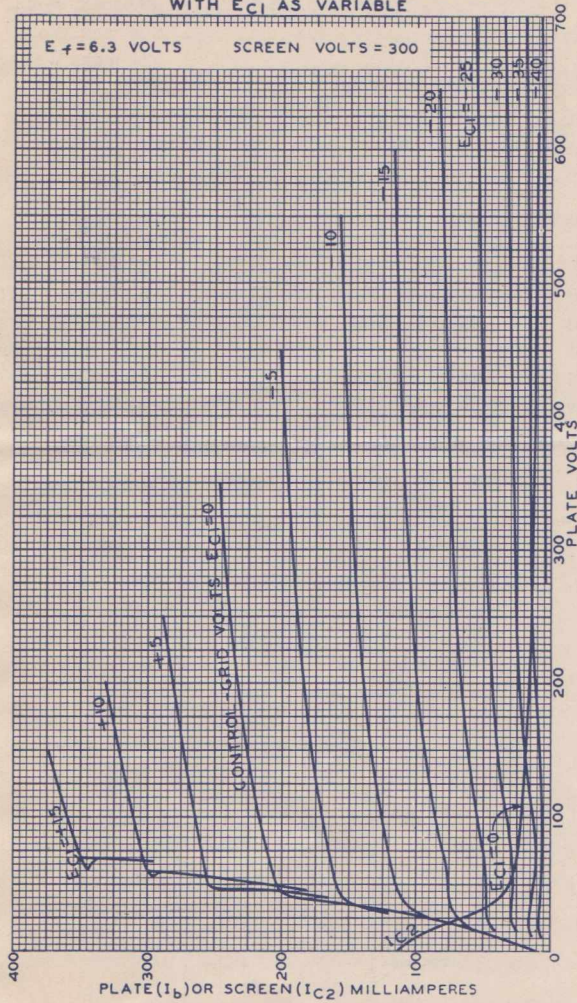
° The type of input coupling used should not introduce too much resistance in the grid-circuit. Transformer or impedance-coupling devices are recommended. When the grid circuit has a resistance not higher than 0.05 megohm, fixed bias may be used; for higher values, self-bias is required. With self-bias, the grid circuit may have a resistance as high as, but not greater than, 0.5 megohm, provided the heater voltage is not allowed to rise more than 10% above rated value under any condition of operation.

RADIOTRON 6L6

RADIOTRON 6L6

AVERAGE PLATE CHARACTERISTICS WITH E_{C1} AS VARIABLE

AVERAGE PLATE CHARACTERISTICS WITH E_{C1} AS VARIABLE



RADIOTRON 6L6

RADIOTRON 6F5

(Information additional to that given in Technical Bulletin No. 56)

Many modern broadcast receivers require at least two stages of audio amplification in order to obtain rated power output. The gain necessary in

For example, the high gain obtainable through the use of a 6F5 in the first stage of a three-stage amplifier makes it possible to feed to the first a-f valve only a part of the total audio voltage developed by the detector. The smaller the fraction of the total detector output voltage that is fed to the first a-f valve, the larger the per cent. modulation that can be handled with small distortion. The utilization of less than maximum a-f voltage is not serious in a high-gain amplifier.

DIODE CHARACTERISTICS SHOWING DIODE DISTORTION OF A HIGH-PERCENTAGE MODULATED CARRIER

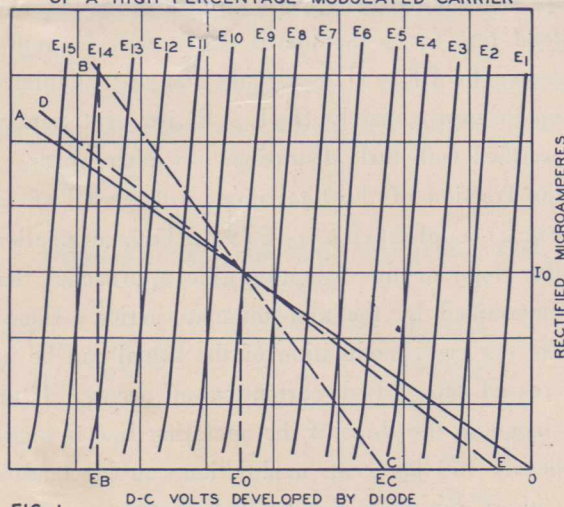


FIG. 1

the first stage depends upon the a-f voltage developed by the detector, which is usually a diode, and the input-voltage requirements of the second audio stage. When the number of valves in the audio amplifier is restricted to two, it may be necessary to use a high-gain first-stage valve in order to meet the input-voltage requirements of the output stage, especially when a low-percentage modulated carrier is to be received. The 6F5, the all-metal high-mu triode intended for use in high-gain resistance-coupled amplifier circuits, can be used to advantage in this case.

The 6F5 may also be used to advantage in receivers having more than two a-f amplifier stages.

To understand why utilizing a part of the diode voltage is desirable, let us consider that the characteristics of a certain diode are as shown in Fig. 1. For a given carrier voltage (E_1 , or E_2 , ——— E_{15}) at the detector, the ordinate and abscissa indicate, respectively, the d-c current through and the d-c voltage across a suitably by-passed resistance (R) connected in series with the diode; the ratio of the d-c voltage across R to the d-c current

LOW-DISTORTION CIRCUIT USING THE 6F5 IN A HIGH-GAIN AMPLIFIER

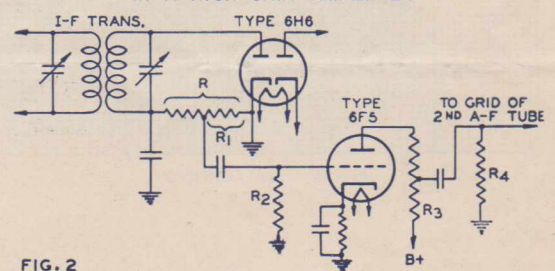
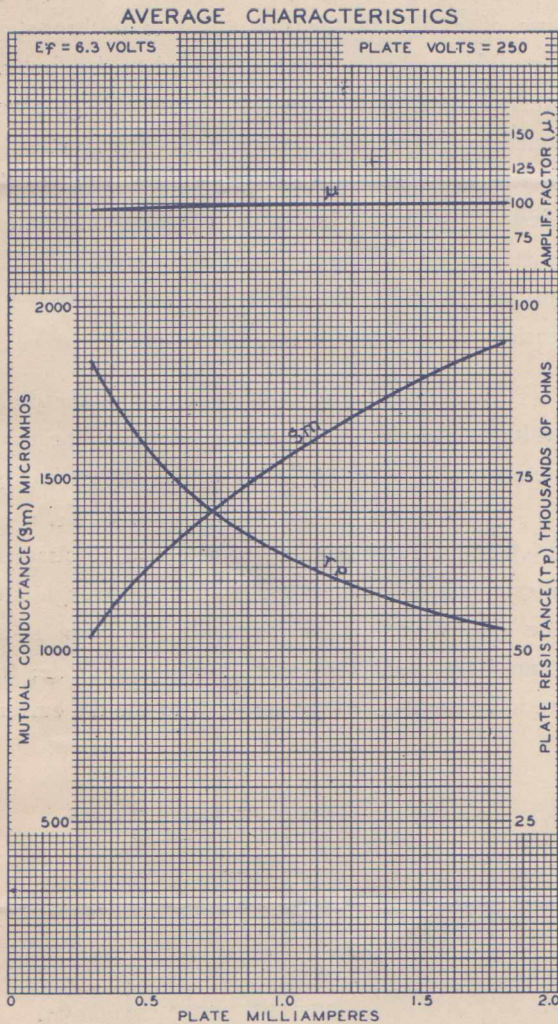


FIG. 2

through R equals the resistance of R . Hence, the intersection of a load line (whose cotangent is R) with any single carrier-voltage curve determines

the value of the d-c current flowing in the circuit. Thus, if an unmodulated carrier voltage having a value E_0 is impressed across the input of the circuit consisting of R , suitably by-passed and the diode

RADIOTRON 6F5



coupling condenser; the grid of this a-f valve is grounded through a high resistance (R_2). When the carrier is modulated, the diode load (R_d is then essentially $R_d = R \times R_2 / (R + R_2)$). The reciprocal of the slope of the line (BC) equals R_d ; BC passes through point (E_0, I_0). If the per cent. modulation is such that the minimum amplitude of the carrier is less than E_4 , small carrier amplitudes will be cut off. Therefore, the maximum per cent. modulation that can be handled by this circuit is $(E_0 - E_4) / E_0$. On the other hand, if R_2 is connected to only a portion of R , then the load line for a modulated signal may be represented by DE. Thus, signals that are modulated up to approximately $(E_0 - E_1) / E_0$ per cent. can be rectified with little distortion. In other words, as the fraction of the total diode voltage (R_1/R in Fig. 2) coupled to the first a-f valve becomes smaller, the slope of the operating line approaches that determined by the unmodulated carrier. Hence, the per cent. modulation of the signal can be increased before diode-current cut-off occurs. If the change in the slope of the operating line is small, nearly 100 per cent. modulation can be handled without distortion, due to diode-current cut-off.

Diode biasing of the grid of the 6F5 does not produce this type of distortion, but is not generally suitable because of the probability of plate-current cut-off, even with relatively small signal voltages applied to the diode circuit. The use of a 6F5 in the first a-f stage of a high-gain amplifier, highly modulated signals with little distortion.

in series, a d-c voltage (E_0) will be developed across R and a d-c current (I_0) will flow in the circuit.

The audio voltage appearing across R is usually fed to the grid of the first a-f valve through a

The design of a receiver may be such that, even though a part of the audio voltage developed by the diode is applied to the grid of the 6F5, the signal voltage at the grid of the second a-f valve may be more than necessary. Under these conditions, the plate resistor of the 6F5 may be tapped,

so that only a fraction of the voltage developed across this resistor is applied to the grid of the second a-f valve. This circuit will tend to minimise plate-circuit distortion in the 6F5, caused by plate-current cut-off during the negative voltage excursions of the signal. Figure 2 shows a circuit that permits the rectification of highly modulated carriers with little distortion, and also tends to minimise any plate-circuit distortion.

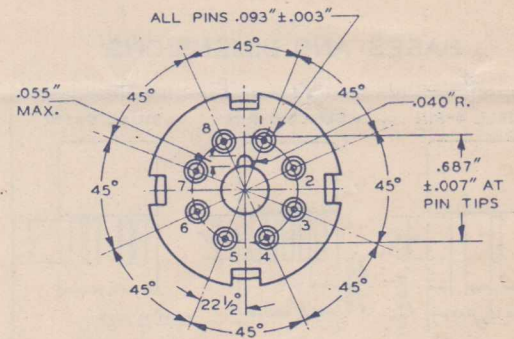
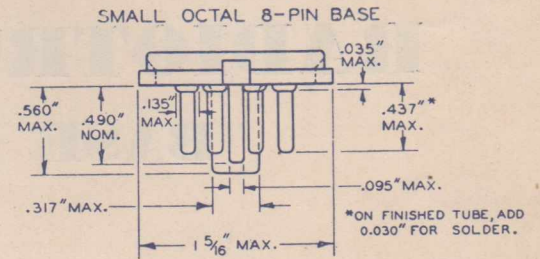
When the 6F5 is used in conjunction with a 6H6, the all-metal twin diode, the combination may be used as a detector, a.v.c. valve, and first a-f amplifier. A variety of circuits are possible with this combination, because each of the two diodes in the 6H6 has its own cathode and corresponding base pin.

TENTATIVE CHARACTERISTICS OF THE 6F5.

Heater Voltage (A.C. or D.C.)	6.3 Volts
Heater Current	0.3 Ampere
Plate Voltage	250 max. Volts
Grid Voltage	-2 Volts
Plate Current	0.9 Milliamperes
Plate Resistance (r_p)	66000 Ohms
Amplification Factor	100
Grid-Plate Transconductance	1500 Micromhos
Input Capacitance	6 $\mu\mu$ F
Output Capacitance	12 $\mu\mu$ F
Grid-Plate Capacitance	2 $\mu\mu$ F

Note: The d-c resistance in the grid circuit of the 6F5 should not exceed 1.0 megohm.

BASES AND DIMENSIONS



BOTTOM VIEW OF BASE

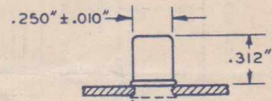
SMALL OCTAL 7-PIN BASE
AS ABOVE, OMITTING PIN NO 6

SMALL OCTAL 6-PIN BASE
AS ABOVE, OMITTING PINS NO 4 & 6

SMALL OCTAL 5-PIN BASES

ARRANGEMENT NO 1 - AS ABOVE, OMITTING PINS NO 3, 5 & 7
ARRANGEMENT NO 2 - AS ABOVE, OMITTING PINS NO 3, 5 & 6

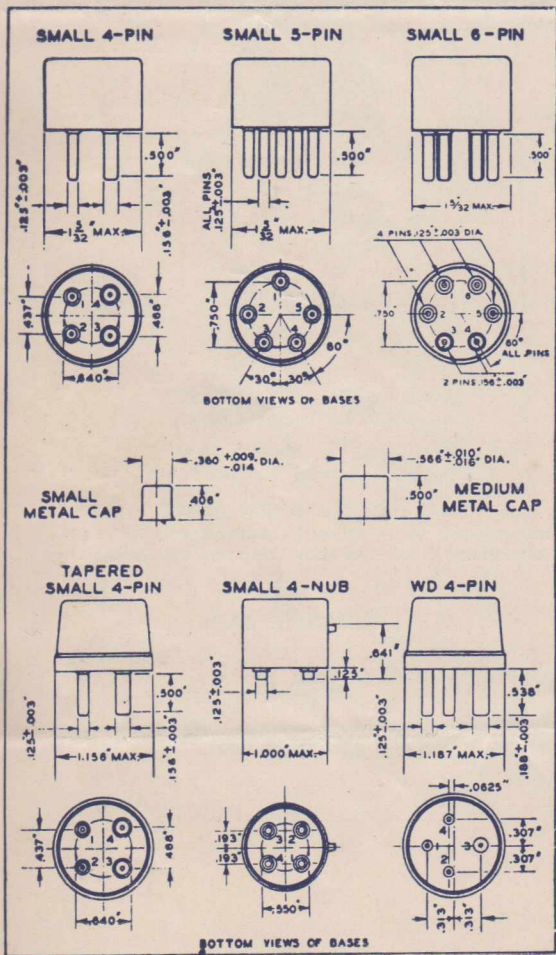
MINIATURE CAP



RADIOTRON VALVES

BASE LAYOUTS

BASES AND DIMENSIONS



BASES AND DIMENSIONS

