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in emergency broadcasting?**

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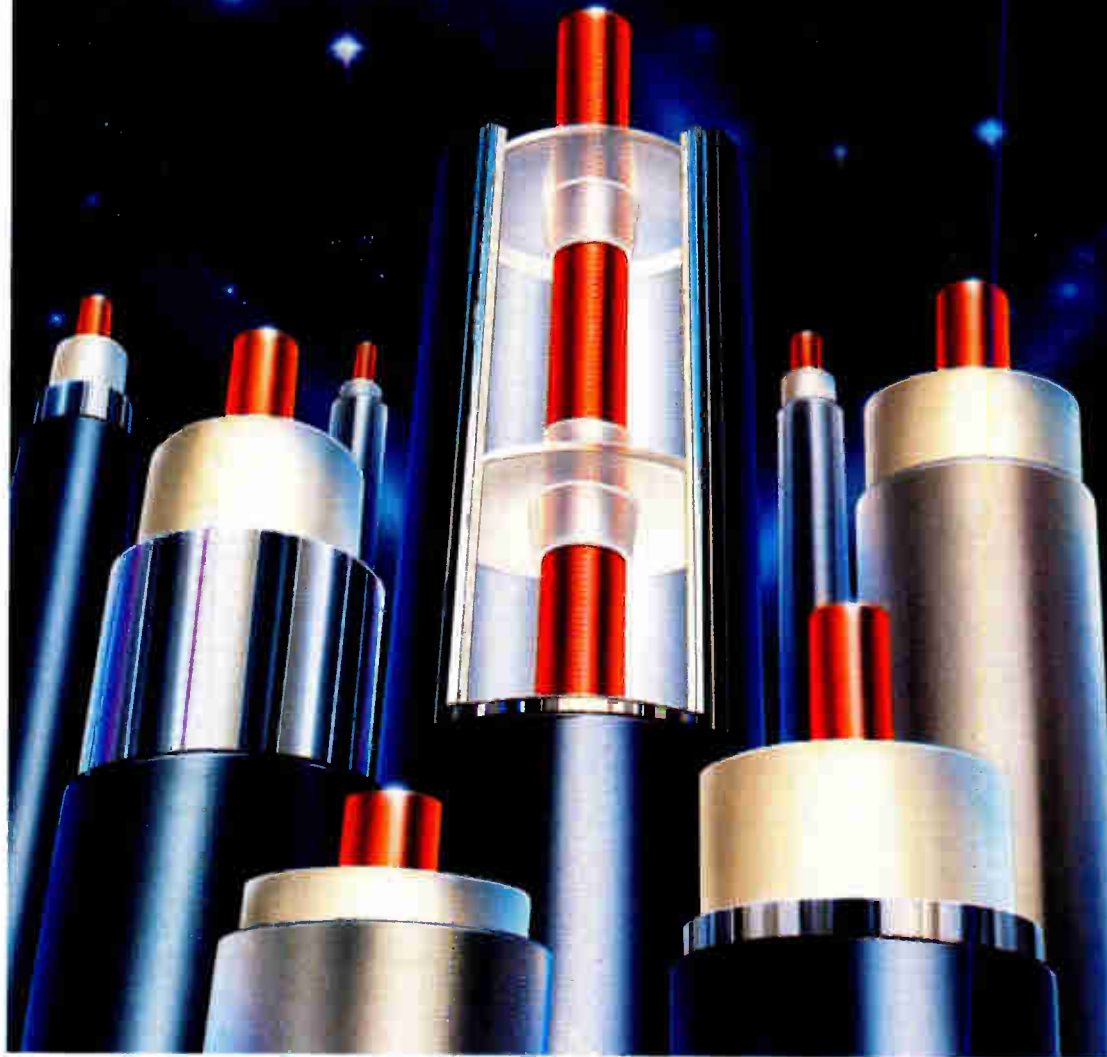
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Gearing up for Emergency Broadcast 32

With more than 55 million viewers actively watching cable television, many think it makes sense to broaden the scope of the current emergency broadcast system beyond broadcast television and radio transmissions. *CED's* Roger Brown examines the efforts of the FCC and other state groups to make an automated, cable-delivered EBS system possible.

Editorial Index 1a

Pull out and keep this handy reference tool to all technical CATV articles published between October, 1990 and October, 1991. Designed as a supplement to last year's comprehensive, three-year index, this guide includes articles that have appeared in *CED*, *Cablevision* and *Communications Technology*.

Fiber in rural builds 36

No longer is the implementation of optical fiber and electronics an option just for major, high density builds. David Heyrend of United Video Cablevision of Sidney, Maine explains how the implementation of fiber helped to hook up rural subscribers in an economical fashion.

Grounding and bonding methods 40

Grounding and bonding outside plant to the power utilities can be a tricky situation, both from a safety and an isolation perspective. Roy Rohrer of Warner Cable discusses methods of grounding and bonding, in conjunction with the National Electrical Safety Code, in this excerpt from his book on the subject.

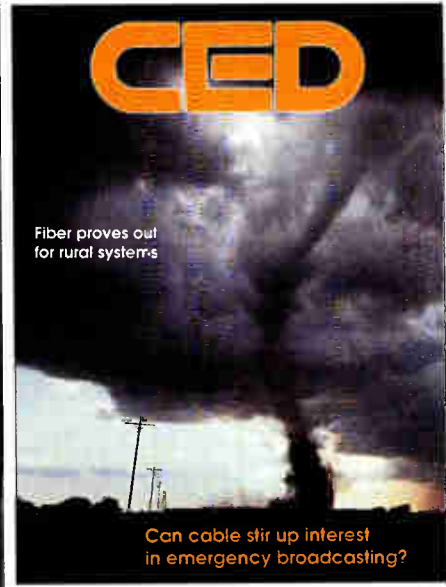
Satellite movement and its implications 48

The next few years mark a period of shift in the orbital arc. John Vartanian of HBO discusses the technical implications caused by the movement in space in this revised article reprinted from the 1991 SCTE Technical Papers. The paper was also delivered at a recent Hudson Valley SCTE chapter meeting.

Preventive maintenance as a way of life 50

As Walter Gerber of Star Cable Associates of Pittsburgh, Pa. explains it, he has yet to find a proactive, usable manual on preventive maintenance—so he wrote one himself, in this article outlining hands-on maintenance techniques for day-to-day operations. Also, Kevin Collins of Century Cable TV in Liberal, Kan. shares the results of an eight-year preventive maintenance plan.

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How cable TV can deliver EBS signals. Photo by The Stock Market.

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Composite triple beat

Like much of the technology in cable TV, intermodulation in frequency division multiplexed (FDM) transmission systems was described and analyzed by the Bell Telephone Laboratories many years before CATV was born. As early as 1935, M.A. Weaver struggled with a form of intermodulation he called non-linear crosstalk. In 1953, Elmen-dorf and others demonstrated by measurements on FDM voice frequency group transmission cascades that second order intermodulation product amplitudes tend to add as a power law function of the number of tandem amplifiers ($10 \log N$); while third order products tend to add as a voltage function ($20 \log N$).

In 1970, Ken Simons of Jerrold Electronics published an excellent and comprehensive mathematical power series analysis of The Decibel Relationship Between Amplifier Distortion Products (Proc. IEEE July 1970). This was an expanded version of the analysis in his famous "Blue" and "Red" books published by Jerrold several years earlier.

Power Analysis

The power series equation defines the total instantaneous output voltage E resulting from an input voltage e :

$$E = k_1e + k_2e^2 + k_3e^3 + \dots k_n e^n$$

By Archer S. Taylor, Senior Vice President, Engineering, Malarkey-Taylor Associates, Inc.

Modern push-pull circuitry tends to cancel out the even ordered products (k_2, k_4 , etc). Modern cable TV amplifiers are so nearly linear that terms of higher than third order can safely be neglected in normal practice. Furthermore, power law build-up of second order products in amplifier cascades is much slower than the voltage build-up of the third order.

Thus, the k_3e^3 term provides the controlling contribution to intermodulation in amplifier cascades.

The instantaneous input voltage, considering any three carriers in the system, is:

$$e = A \cos f_1 + B \cos f_2 + C \cos f_3$$

Mathmatic equations

Ken Simons (and others) have carried out the rather complex algebraic and trigonometric computations to show that the third power expansion of e (i.e. e^3) results in sets of trigonometric functions (i.e. cosines) of the following combinations of the three frequencies, f_1, f_2 , and f_3 :

(1) $f_{13}; f_{23}$; and f_{33} . *Third harmonics.*

(2) $2f_1 + f_2$. *Sometimes called inter-modulation.*

(3) $f_1 - f_2 + f_3$. *The triple beat.*

Ken Simons (and others) have also shown that the third harmonics are 15.5 dB weaker than the triple beat component; and the $2f_1 + f_2$ components are 6 dB weaker than the triple beat. Thus, the triple beat component is dominant.

Moreover, when the triple beat frequencies are equally spaced at, say, multiples of 6 MHz, and one frequency is negative while the others are positive, one of the products comes out equal to the negative frequency.

For example, $288 - 300 + 312 \text{ MHz} = 300 \text{ MHz}$. In 1973, Bert Arnold, of the former RCA Community Television Systems, showed that with 30 FDM channels, there would be 239 such combi-

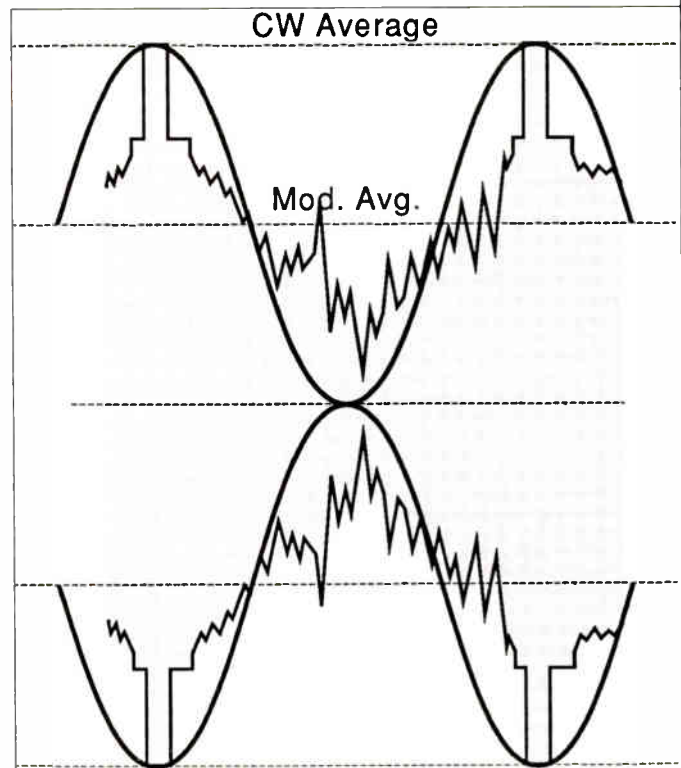
nations close to the frequency of the center channel. With 50 to 60 channels, there will be 900 to 1,200 such co-channel products. For a "non-coherent" head-end, these hundreds of triple beats will occur in a bundle generally within ± 20 kHz of the desired carrier.

The accepted NCTA measurement method employs a spectrum analyzer, set for 30 kHz IF bandwidth, in order to measure the combined, or composite, magnitude of the bundle of hundreds of intermodulation products close to a desired carrier frequency.

The ratio of the desired carrier to the composite value indicated by the spectrum analyzer is called the composite triple beat (CTB) voltage ratio, expressed in decibels. Sometimes the ratio is turned upside down, with a negative value of the decibel ratio of CTB magnitude relative to the carrier (I/C). I prefer the positive value for carrier-to-interference (C/I).

Removing modulation

For repeatable and reliable measure-



ment, the modulation should be removed from all carriers during the test. Obviously, this would not be possible in any operating system with connected customers. The magnitude of the carrier-to-CTB ratio measured in the same

MY VIEW

way, but with normally modulated carriers will be considerably greater than with unmodulated (CW) carriers. This is because the average value of the instantaneous peak RF voltage of the video modulated waveform is about half (-6 dB) that of the unmodulated waveform (see Figure 1). This suggests that the resulting carrier-to-CTB ratio would be 12 dB greater than that measured with CW carriers.

Thus, if a system measures 53 dB carrier-to-CTB ratio with CW carriers, it would probably measure about 65 dB with modulated carriers, everything else being the same.

However, intermodulation at 65 dB below the carrier may be lost in the random noise of the system and the analyzer. For this reason, NCTA recommends raising the level of all modulated carriers (except the pilots) by 3 dB, for the test. This would bring the ratio down to a detectable 59 dB, halfway between the CW and modulated carrier ratio.

Not subjective

NCTA recommends 53 dB as the performance objective for the CW measurement, and 59 dB for the 3 dB increased modulated carrier measurement. This is necessarily a subjective judgment. NCTA does not indicate whether this represents the threshold of perceptibility, or a somewhat annoying quality grade.

Recently conducted tests indicate that even at close viewing distance (5 feet from a 20-inch TV screen) interference is rated only slightly annoying by the average viewer at 39 dB carrier-to-CTB ratio, as measured with CW carriers. This is the same subjective rating as for 45 dB carrier-to-random noise ratio, at the same viewing distance. The 39 dB ratio with CW carriers would be roughly equivalent to 51 dB with modulated carriers, without the 3 dB increase in carrier level.

The proper objective for the CTB ratio using the only practicable method, modulated carriers, has not been well established experimentally. However, operators indicate that the conventional objective of 53 dB is a practical minimum acceptable working standard for maintenance testing in the field, using the normally modulated carriers at normal levels.

Nothing in the foregoing discussion relates to coherent headends, in which all carriers are phase-locked to a precise 6 MHz comb. This must be left for another column. There are some surprises! ■

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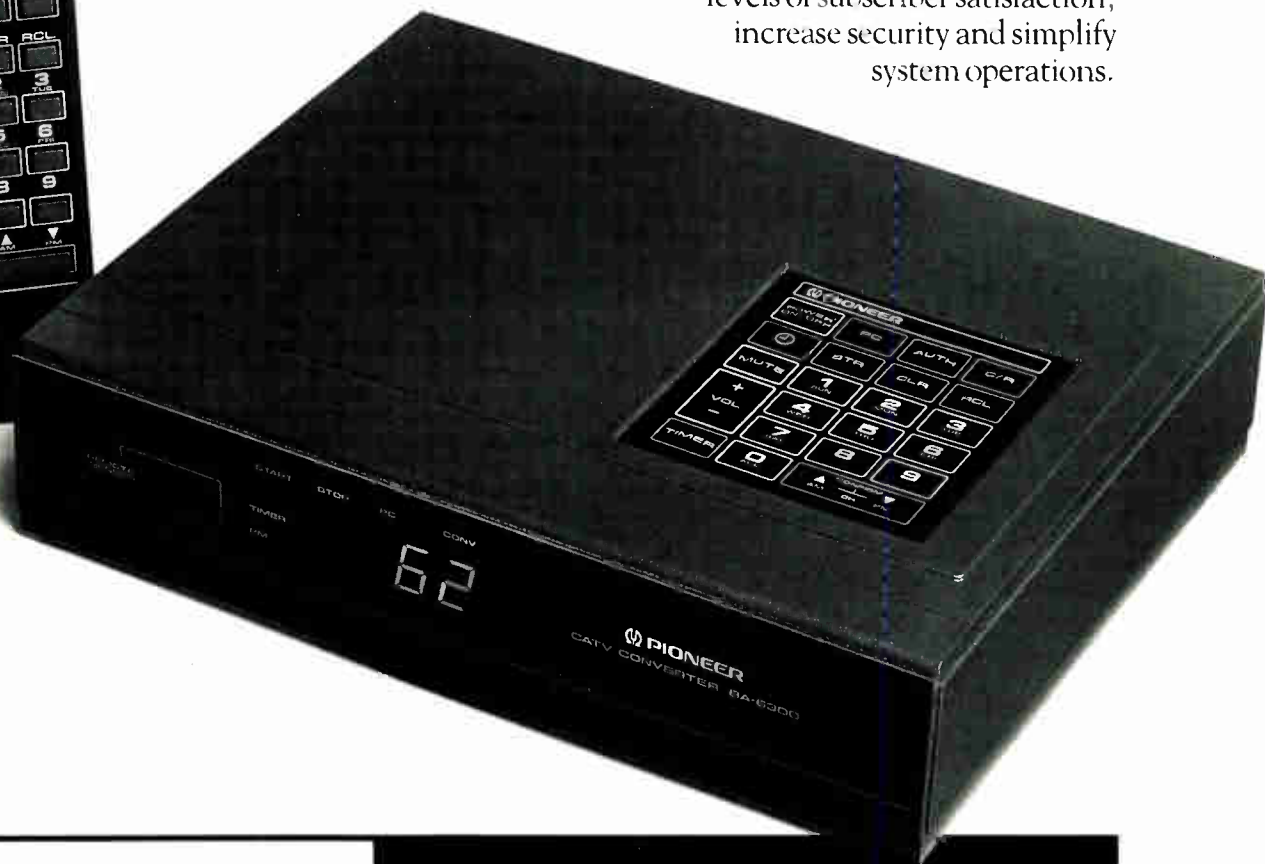
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Home taping of digital audio (CED), Jeff Krauss, Telecommunications and Technology Policy of Rockville, Md., March 1991, p.22. An investigation of Washington's latest debate: Digital audio taping.

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MultiPort: Another missed opportunity? (CED), Kathy Berlin, February 1991, p.40. Closed captioning legislation and how it affects (or doesn't affect) MultiPort development.

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Peaks and valleys along the FCC paper trail (CED), George Sell, July 1991, p.65. How the FCC is updating its CLI database.

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What we don't know about PCN (CED), Archer Taylor, Malarkey-Taylor Associates, July 1991, p.22. Discussion of spread spectrum, frequency allocation, intrabuilding of propagation and capital investments as it relates to PCN.

Fiber optics

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Aerial fiber construction (CT), Jeffrey Weech, ATC Construction, October 1991, p.70

Aerial plant fiber performs well in lightning (CT), P.D. Patel and Terry Coffman, AT&T Bell Labs, January 1991, p.32

Alternate access and the cable operator (CED), Andy Paff, Optical Networks International, Fiber Optics Special Supplement, September 1991, p.14. A review of the basic considerations surrounding alternate access including products, legal issues and recommended first steps.

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Avoiding obsolescence (CV), Chuck Moozakis, June 3, 1991, p.18. Flexible networking as a system design tool.

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Circle sweeping using a fiber medium (CT), Dewayne Lipp, CaLan Inc., April 1991, p.30

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Conference promotes fiber planning and use (CT), Ron Hranac, February 1991, p.12

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Design considerations with fiber (CT), Mark Bowers, CableSoft Engineering Services, December 1990, p.29

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Emergency fiber restoration (CED), Mike Genovese, Siecor Corp., November 1990, p.48. Steps to take during pre-installation and post-installation, record keeping, personnel and cross training.

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Fiber attractiveness grows (CED), Chuck Moozakis, June 1991, p.104. Survey statistics regarding AM fiber optic pricing, fiber/rebuilds, FTF concerns.

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Fiber fever! (CV), Fred Dawson, December 17, 1990, p.13. Cable has less to fear from telcos and DBS as the cost/benefit of fiber networks grows.

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"Hello, (cable) operator?" (CED), George Sell, Fiber Optics Special Supplement, March 1991, p.8. Cable television's opportunities in the personal communications infrastructure.

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Major issues in network design (CED), The CableLabs Staff, September 1991, p.24. An investigation of CATV system design, including fiber optics, power/loss budgets, spectrum allocation, drop

concerns and network migration.

Mapping fiber's path (CV), Fred Dawson, August 12, 1991, p.18. A Rogers/CableLabs study finds the ultimate benefits of fiber can be achieved from nodes serving as few as 22 users.

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Network architecture (CED), Archer Taylor, Malarkey-Taylor Associates, December 1990, p.30. VSB/AM fiber optic architectures, compression, television receivers and PCN.

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Not just for big players (CV), Chuck Moozakis, February 11, 1991, p.34. Sun Country Cable finds fiber cheaper than coax.

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CableLabs PCN conference attracts

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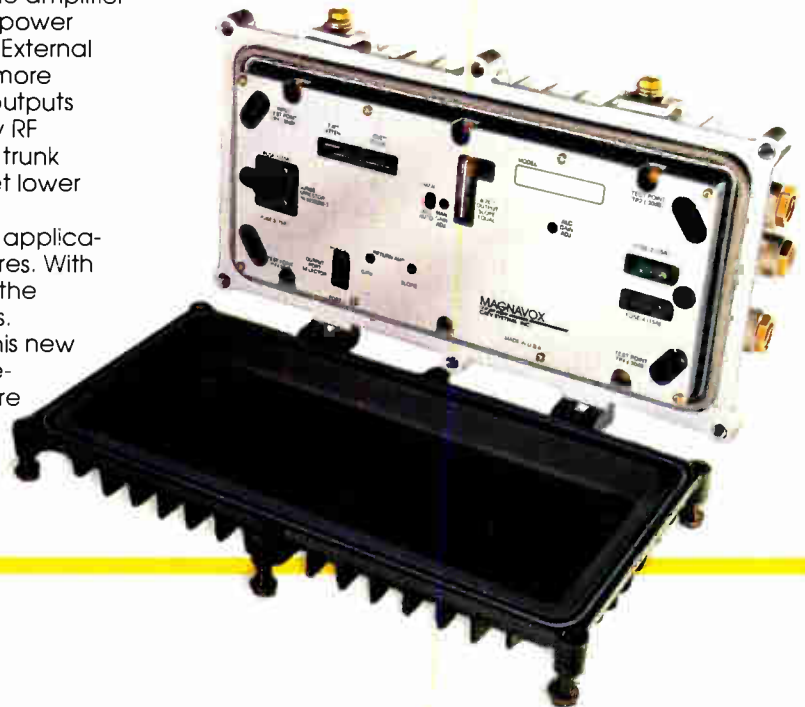
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out with the crawl message to capture the viewer's attention.

A "bare-bones" ACM system that addresses four channels would cost a cable operator about \$7,000, according to Ken Lawson, VP of marketing at Dynatech Cable Products. The system can be expanded in increments of four channels at about \$2,500 per chassis, he added.

In New Jersey, the ACM system can be accessed from a variety of locations and by different means, including the microwave network, telephone modem and voice (see Figure on page 32). The ACM chassis are installed in the headend ahead of the modulators and each chassis feeds up to four channels.

KAS Cable, which operates the on-base cable system at Wright-Patterson Air Force Base in Dayton, installed the ACM system on all 36 channels about two years ago, according to Dan Kinney, system technician. Since then, it's been used to warn the base's 2,500 subscribers of high winds and tornadoes. It's also been used to deliver "Welcome Home" messages to troops returning from the Persian Gulf, for syndex switching requirements, to advise of impending outages and for pay-per-view.

Kinney said the system cost about \$20,000 to install and has worked flaw-

lessly. The base's headquarters command post serves as the home for the remote control terminal, he added.

These systems are fine for anyone watching television, but what happens if an emergency occurs when the television isn't on or if it's being used for another purpose (i.e. video games)?

Hollyanne Corp. has one answer. The Safety Alert Monitor system can alert even sleeping residents by delivering an audio alert for impending disasters or emergency situations. An in-home receiver about the size of a cable converter is connected to the cable system is addressed by a headend controller. Large geographical areas can be split up into as many as 31 zones and each zone can be addressed separately or in any combination.

The headend controller requires no cable system intervention; it is activated by local emergency officials via touch-tone telephone, two-way radio or by the National Weather Service. Besides the controller, a cable system needs a National Weather Service receiver and a modulator to make the system work. The frequency agile system requires just 30 kHz of bandwidth to send its message.

The in-home receivers cost about \$70

each, although cable operators using the receivers are expected to rent the units to their subscribers for just a few dollars per month.

So, will cable operators commit to EBS? At this early stage, it's hard to say. But one thing is certain: If cable is to participate, the system must be inexpensive and not require additional personnel to monitor its functions. The rest is a policy question that will have to be answered by cable industry officials.

But on the technology front, things are beginning to happen. The SCTE, under the auspices of its Engineering Committee, has established an EBS subcommittee to help establish recommended practices for cable operators who are willing to interface with EBS. The subcommittee's goal will be to design an applications standard and disseminate information to all members.

According to Tom Elliot, vice president of research and development at TCI and the chairman of SCTE's Engineering Committee, this subcommittee will rely heavily on cooperation from the NCTA and its engineering committee, as well as input from Cable Television Laboratories. ■

—Roger Brown

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with no sharp bends. The strand attachment needs to be a by-metal connection (press-type preferable). The ground rod attachment needs to be a solid connection to a clean surface. Any resistance at the connections will reduce the value of the ground.

If an existing ground is in place, it would be preferable to use a separate down lead and bond at the ground rod. The parallel down leads will provide a lower impedance path for the higher frequency transients. This needs to be approved by the administrator of the pole attachment agreement.

Should this location be a problem area, the ground resistance could be reduced by the addition of another ground rod. The ground rods are most effective when separated by a distance of 1.1 times the length of the rods. Separate ground rods need to be bonded together with #6 or larger copper wire.

Places to avoid. Grounding should be avoided at pole locations where the electric utility has spark gaps, lightning arresters or primary switching. These locations have the capability to discharge some extremely high electrical potential. A significant portion of that discharge could be transferred to the CATV plant. Grounding should also be avoided at lo-

cations that indicate a high current in the bonding conductor.

Cost. Grounding costs will vary in dif-



Longitudinal sheath currents are an unwanted electrical energy induced on the messenger and sheath of the cable.

ferent parts of the country, again depending on labor costs. Material costs will differ only slightly unless there is a requirement for some exotic types of grounding like chemical rods or extremely long rods.

Estimated costs for labor and material for grounding to an existing electrode would require a separate down lead, exposing and cleaning the electrode to make the bend. This costs about \$ per

hour for labor and materials. Driving an additional separate grounding electrode can have a wide range of pricing. If access is available for a normal grounding electrode to be driven, the cost for labor and materials is about \$30.

If minimum grounding is completed by installing a down lead and using the power company electrode, the cost for four contacts per mile would be about \$80 per mile. On the other hand, if a down lead and newly driven electrode is required, the cost could be \$1 per mile or more. These costs do not consider the cost of removing sections of concrete and then repairing the opening after the grounding is complete.

Any area that experiences multiple failures that indicate they are because of power-related problems needs to be investigated in the following method: Test grounds; measure sheath currents; measure bonds for current flow; and lift bonds if there is high current.

Problems of high currents or high ground resistance should be referred to the power company and their assistance should be requested to resolve the problem. Improving the ground resistance and lowering neutral current flow is a benefit to both parties.

If the power company is unable to provide the assistance needed, the bond could be relocated to another location. The important requirement is that four bonds per mile remain.

Longitudinal sheath currents

Longitudinal sheath currents (LSC) are an unwanted electrical energy induced on the messenger and sheath of the cable. This is the result of bonding to the power company multigrounded neutral.

Most of the power distribution systems today are wye-connected four wire primary and three wire secondary with one of the wires being the common neutral. When all the loads are perfectly balanced there is zero current flowing in the neutral.

The probability of all loads being perfectly balanced is unlikely. Consequently, there is usually some current flowing most of the time.

It is not unusual to find 50 to 150 amperes of neutral current under normal conditions and well in excess of 300 amperes in a fault condition. The strand and coaxial cable system that has multiple cables will carry a substantial portion of the neutral currents.

Not only will the cable company share the load—in many cases, it will carry the major portion of the load. Typical

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GROUND #	NEUTRAL Ω	CATV Size Type	%LOAD Strand +	%LOAD CATV	%LOAD Neutral	%LOAD Ground	CATV Amps*
4	20	4-0 ALM	412+500	26.0	52.0	22.0	15.6
4	20	4-0 ALM	500+750	36.7	44.5	18.8	22.1
4	20	4-0 ALM	625+750	41.5	41.1	17.4	24.9
4	20	4-0 ALM	1+750+625	65.3	24.4	10.3	39.2
4	5	4-0 ALM	625+750	27.3	27.0	45.7	16.4
4	5	4-0 COP	625+750	21.3	43.1	35.6	12.8
4	5	#4 COP	625+750	32.7	12.9	54.5	19.6
16	20	4-0 ALM	625+750	27.3	27.0	45.7	16.4

* Total potential 60 Amperes

Table 1

trunk feeder systems may be strand, .750-inch and .625 cable, with a total parallel resistance of .099 ohms per 1,000 feet. The power company neutral may be a 4/0 aluminum which would also have a resistance of 0.1 ohms per 1,000 feet. With the same resistance in each path and both paths bonded to the same grounding electrodes the neutral currents would be shared equally (see Table 1).

Load Sharing

The cable system with a 1.0-inch supertrunk, 0.750-inch trunk and 0.625-inch feeder on quarter-inch strand would have a resistance of .037 ohms per 1,000 feet. This compares to the 0.1 ohm of 4/0 aluminum the cable system would be carrying over 65 percent of the total neutral current.

A typical system without supertrunk, with four bonds per mile to power with grounds at about ohms per ground would result in the cable system carrying 41.6 percent of the load, power neutral with 4/0 aluminum 41.1 percent and 17.4 percent dissipated to ground.

The ratios change if the power neutral changes, the ground resistance changes, the number of ground rods change or the CATV plant changes. By changing the grounds from 20 ohms to 5 ohms, for example, the percentage of the load dissipated to ground changes from 17.4 percent to 45.7 percent. The same change would also occur if the number of -ohm grounds were increased from four per mile to 16 per mile. A greater percentage of the load can be dissipated by adding additional grounding electrodes or reducing the resistance of the electrodes.

Another important component to the mix is what the power company is using for a neutral conductor. Changing from a 4-0 aluminum neutral to a 4-0 copper causes the percent of load carried by the neutral to change from 41 percent to 59 percent. Conversely, if the neutral is changed from 4-0 aluminum to #4 copper, the neutral load would change from 41 percent to 22 percent. The CATV

load would increase from 41 percent to 55 percent.

While it is worthwhile to calculate all these numbers to understand the possibilities, the problem is, this is not the real world, all grounds are not 20 or 5 ohms. There are different combinations of cables and there may be different combinations of power company neutral conductors. Other differences include changing power loads and load balance. For the CATV plant to carry 60 percent of a five ampere load would probably not be a problem—but 60 percent of a 300 ampere fault condition load is a serious problem.

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SCTE

Following is a list of SCTE technical seminars with contact name. If known, location and seminar topic are listed.

December 9-11

"Technology for technicians II" National SCTE seminar, Holiday Inn, Phoenix, Ariz. Intensive three-day seminar designed for maintenance technicians, chief technicians and system engineers. To be conducted by SCTE director of training Ralph Haimowitz. Contact SCTE headquarters, (215) 363-6888.

December 10 Badger State Chapter "System design, MDU design and construction." To be held at the Holiday Inn, Fond du Lac, WI. Contact Gary Wesa, (414) 496-2040.

December 10 Chattahoochee Chapter "Signal Leakage, CLI and FCC Form 320." To be held at the Perimeter North Inn, Atlanta, Ga. Contact Hugh McCarley, (404) 843-5517.

December 10 Greater Chicago Chapter "Video and Audio Signals and Systems. BCT/E examinations to be administered. To be held at the Embassy Suites Hotel, Schaumburg, Ill. Contact Bill Whicher, (708) 438-4423.

December 11 Great Plains Chapter BCT/E and installer examinations to be administered at both levels in categories I, III, VI and VII. To be held at the Crown Court Quality Inn, Bellevue, Neb. Contact Jennifer Hays, (402) 333-6484.

December 12 Music City Meeting Group To be held at the Bonanza Trinity, Nashville, Tenn. Contact Jim Romese, (615) 244-7462.

December 12 Northern New England Meeting

Group "Test Equipment" with Joel Welch of Cablevision. To be held in Portland, Maine. Contact Bill DesRochers, (207) 646-4576.

December 13 Miss-Lou Chapter "Fiber Optics" presented by Sumitomo Electric; "Ladder Safety and Care" presented by Batavia and "Safety, Care and Maintenance of Climbers" presented by Rod Paul of Bashlin. Installer and BCT/E examinations to be administered at both levels in all categories. Contact Dave Matthews, (504) 923-0256.

December 13 Wheat State Chapter BCT/E examinations to be administered at both levels in categories I, III, V and VII. To be held at the Red Coach Inn, Wichita, Kan. Contact Mark Wilson, (316) 262-4270.

December 14 Cactus Chapter Installer and BCT/E examinations to be administered at both levels in all categories. To be held at Tucson Cablevision, Tucson, Ariz. Contact Harold Mackey Jr., (602) 352-5860, ext.135.

December 14 Chesapeake Chapter Installer and BCT/E examinations to be administered at both levels in all categories. To be held at Comcast offices in Timonium, Md. Contact Mike Manz, (301) 662-7734.

December 14 Delaware Valley Chapter "Headend maintenance" and "Lightning and surge protection." To be held at Williamson's Restaurant, Willow Grove, Pa. Contact Rich Blandford, (215) 328-0977.

December 14 Piedmont Chapter Installer and BCT/E examinations to be administered at both levels in all categories. To be held

in Asheville, N.C. Contact Rick Hollowell, (919) 757-0279.

December 14 Central Indiana Chapter BCT/E examinations to be administered at the technician level in all categories. To be held at Applied Instruments, Beech Grove, Ind. Contact Joe Shanks, (317) 646-9102.

December 18 New Jersey Chapter "Other Technologies: Friend or Foe." To be held at the Holiday Inn, Wayne, N.J. Contact Jim Miller, (201) 446-3612.

December 18 Snake River Chapter "CLI, Installer Level Drop Specs and NEC Grounding" with Roger Glass of Comm/Scope and "Weak Link" with Bruce Habeck of Anixter. Installer and BCT/E examinations to be administered at the technician level in categories V and VII. To be held at the Weston Plaza, Twin Falls, Idaho. Contact Ron Kline, (208) 376-0230.

December 18 San Diego Meeting Group "Test Equipment Measurements." To be held at the Elks Lodge, Oceanside, Calif. Contact Kathleen Horst, (213) 831-4157.

December 19 Big Country Chapter To be held in Brownwood, Texas. Contact Bill Neely, (915) 236-6375.

December 19-20 Dakota Territories Chapter Installer and BCT/E exams to be administered. Contact Ken Binker, (605) 339-3339.

December 28 Sierra Chapter BCT/E exams to be administered at both levels in all categories. To be held at the Roseville City Hall, Roseville, Calif. Contact Eric Brownwell, (916) 372-2221.

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Universal remotes: Advanced features and dumb ideas

This is the last of three columns on universal remote controls. After a couple more "advanced features and/or dumb ideas," we'll try to estimate what the subscriber really wants and see if there is a way to accommodate it.

There are a few more ideas I've seen on remote controls from satellite receiver integrated receiver descramblers (IRDs) which should be mentioned, in order to be complete.

The first is a lighted remote control. Any time a button was pushed, the translucent buttons lit up so the user could see what he was doing, even in the dark. After a few seconds, the light went out, unless more buttons were pushed. Besides cost, there is a severe battery life penalty to be paid. The reasonable approach is to provide a separate battery for illumination. This provides control after the lights have gone out.

Another idea I've seen involves a locator for the misplaced hand unit. Pressing a button on the IRD sends a signal to the remote control, causing it to emit a tone so it can be found. This is a cute idea, but not inexpensive.

What the subscriber wants?

If you talk to subscribers, visit their homes and listen, you'll find several

By Walter Ciciora, Vice President of Technology, American Television and Communications

things on their minds. If they have an older set without remote control, they consider the remote controlled converter a good feature. They don't even mind paying a modest fee.

It's when they have a relatively new receiver that they get upset. First, they resent having to pay an extra fee for what they have already bought. Second, they wish they could just use their own remotes. It's a pain to use multiple remotes; one to turn on the television and adjust the volume and another to change converter channels.

The universal remote can be helpful here, because it can direct the channel change signals to the converter and the volume control and mute signals to the TV.

In fact, there is little good reason to have a volume control feature on the converter. The TV is the proper place for that function. The only exception to this is when the subscriber's TV has no remote control. This is becoming a rare situation.

Use your own

A decade or so ago, when I first started thinking about remote controls, I had the idea the other way around. I thought the proper place for the intelligence was in the set-top unit. It should have the codes stored from the TVs and VCRs and be able to interpret them. The subscriber would not get a new remote control. That way, the remote control remained an inexpensive item. The subscriber wouldn't feel so bad when it got lost, chewed by the dog, or broken under the rails of the rocking chair.

There is one part of this idea which is a bit untidy. For this to work, the TV's and VCR's infrared (IR) must be covered so that it doesn't see signals from the remote control. The set-top box has to convey IR signals to those windows. The method I suggested was either a plastic fiber taped to the IR windows or an IR light emitting diode (LED) affixed to them.

VCR interface

What subscribers really want is the ability to use their VCRs for time shifting without having to program the VCR. That was the next important feature of the above mentioned configuration.

Since the set-top had to have an IR link via fiber or LED-on-a-wire to the VCR, the set-top could control it. With

an electronic program guide (EPG), the set-top would know what time it was and what the start and stop times and channels of various programs were. The subscriber could simply move the flashing cursor next to the title of the program to be recorded and press the record button, and all the rest would be taken care of by the set-top's microprocessor.

Tyranny of the foggle

But there is yet another untidy detail. Most VCRs and TVs have toggle controls for some functions. One button turns the unit on if it's off, and off if it's on. (Life would be so much simpler if there were two buttons, one for "off" and the other for "on.")

Similarly, on the VCR, there is a toggle button for determining whether the signal to the TV is from the VCR's tapedeck or a bypass of the RF signal at the VCR's input. Older televisions could be plugged into a switched convenience power outlet on the back of the converter. New televisions will not come on when they are repowered. When they are turned on, they will usually be tuned to channel 2. If that isn't the converter's output channel, there's is a problem. This motivates the use of "macros" in universal remote controls (see November 1991 *CED*, p.118.)

There are a number of clever solutions to the tyranny of the toggle. They all add expense and complication to both the converter and the installation. In some cases, the converter would have to access to the VCR's output to determine the state of toggles. The signal would then be routed to the TV for display. But, this contributes to the maze of cables behind the TV.

The dangers of blasters

One last comment on remote controls. There have been a number of poorly designed systems that require careful aiming of the hand unit. Surprisingly, major brand names have suffered this problem.

In an attempt to solve this deficiency, after-market devices have surfaced which amplify the remote control's output. They are generally called "blasters."

These should be avoided. There is danger of eye damage, particularly among children who may pick up the device and look into it while inadvertently (or purposefully) pressing the buttons. The power from IR remotes must be kept low, not only for battery life, but for safety. ■



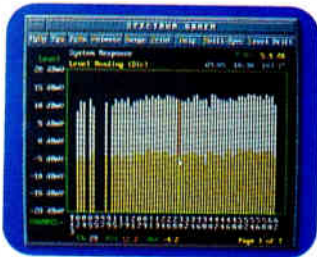
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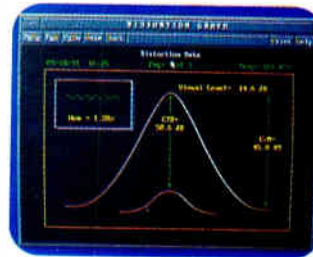
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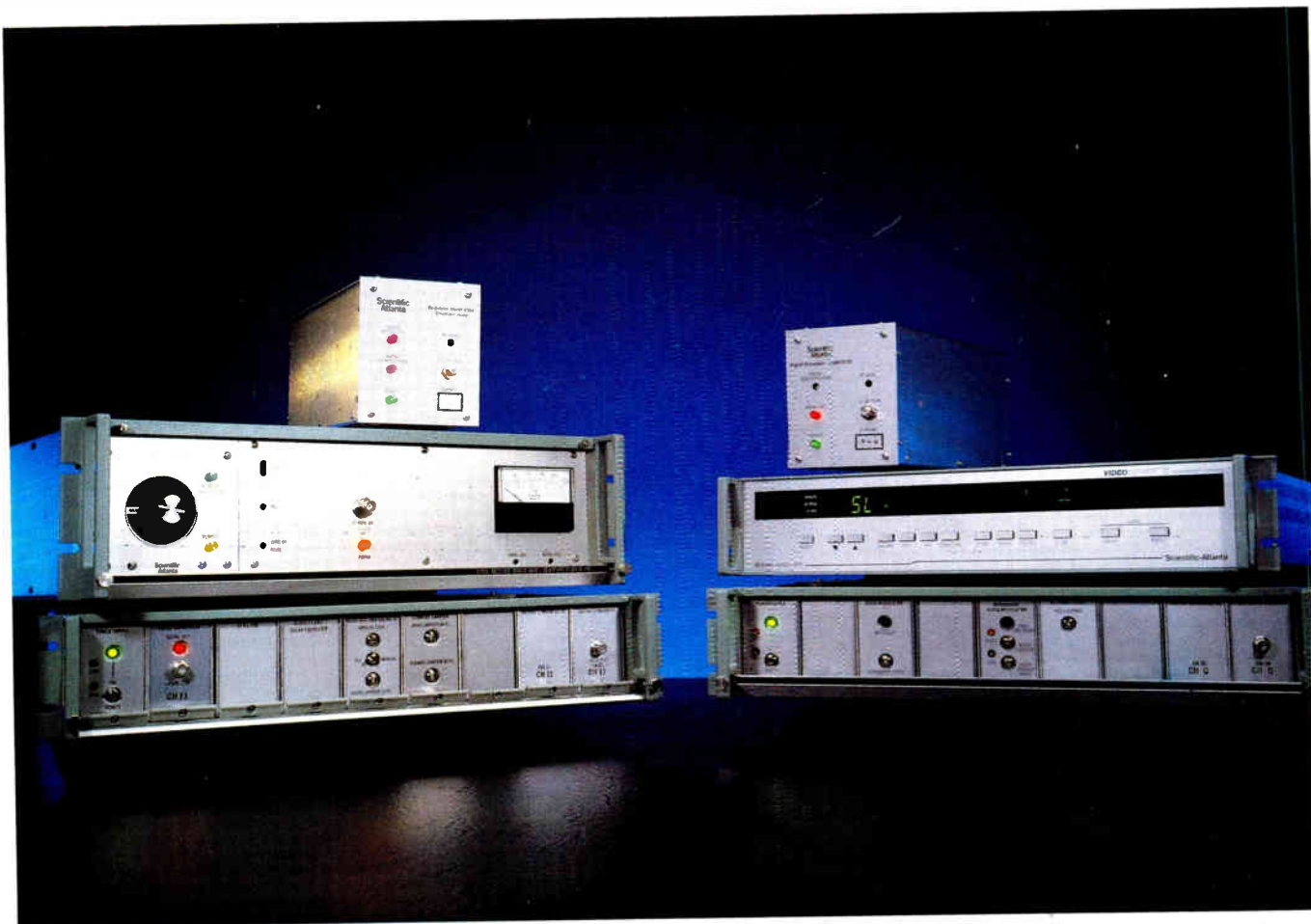
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